

# HW1\_Answer

## P.3-11

**Spherical symmetry:**  $\vec{E} = \overline{a_R} E_R$  Apply Gauss's Law (球面作为高斯面)

1)  $0 \leq R \leq b$   $E_R = \frac{\rho_0}{\epsilon_0} R \left( \frac{1}{3} - \frac{R^2}{5b^2} \right)$

2)  $b \leq R < R_i$   $E_R = \frac{2\rho_0 b^3}{15R^2 \epsilon_0}$

3)  $R_i \leq R < R_0$   $E_R = 0$

4)  $R > R_0$   $E_R = \frac{2\rho_0 b^3}{15R^2 \epsilon_0}$

## P.3-12

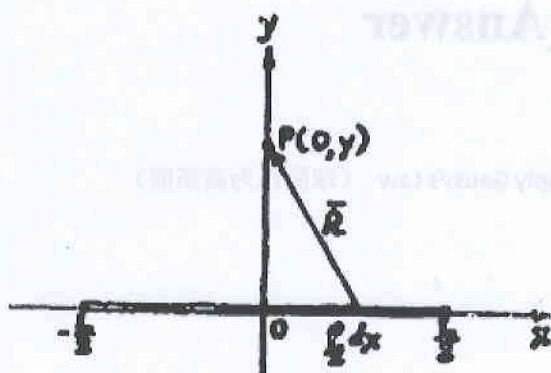
a)  $r < a$   $E = 0$

$a < r < b$   $E = \frac{a\rho_{sa}}{\epsilon_0 r}$

$b < r$   $E = \frac{a\rho_{sa} + b\rho_{sb}}{\epsilon_0 r}$

b)  $b = -a \frac{\rho_{sa}}{\rho_{sb}}$

## P.3-16



a)  $V = 2 \int_0^{L/2} \frac{\rho_l dx}{4\pi\epsilon_0 \sqrt{x^2 + y^2}}$  (换元得到  $\sec \theta d\theta$  积分, 进一步转换成关于  $d(\sin \theta)$  的积分)

分)

$$V = \frac{\rho_l}{2\pi\epsilon_0} \ln \frac{\sqrt{L^2 + 4y^2} + L}{2y}$$

参考答案此处计算的是  $y$  轴上的电势与电场  
实际应该计算  $x=0$  (即  $yz$  平面), 所以答案只需将  
 $y$  改为  $R$ ,  $R$  为  $yz$  平面上到  $O$  点的距离, 即:

b)  $E = 2 \int_0^{L/2} \frac{\rho_l y dx}{4\pi\epsilon_0 R^3} = \frac{\rho_l}{2\pi\epsilon_0 y} \frac{L}{\sqrt{L^2 + 4y^2}}$   $\vec{E} = E \vec{q}$

(a)  $V = \frac{\rho_l}{2\pi\epsilon_0} \ln \frac{\sqrt{L^2 + 4R^2} + L}{2R}$

c)  $\vec{E} = -\nabla V = \frac{dV}{dy} \vec{a}_y$  gives the same answer.

(b) ~~scribbled out~~

### P.3-44

a) Region  $[0, x]$   $\vec{E} = -\nabla V = -\vec{a}_y \frac{V_0}{d}$

$\vec{D} = \epsilon \vec{E} = -\vec{a}_y \frac{\epsilon_0 \epsilon_r V_0}{d}$  Apply formula (3-121b)  $\rho_s = \frac{\epsilon_0 \epsilon_r V_0}{d}$

Region  $(x, l]$   $\vec{E} = -\nabla V = -\vec{a}_y \frac{V_0}{d}$

$\vec{D} = \epsilon \vec{E} = -\vec{a}_y \frac{\epsilon_0 V_0}{d}$   $\rho_s = \frac{\epsilon_0 V_0}{d}$

~~scribbled out~~  
$$\vec{E} = \frac{R \cdot y \cdot L}{2\pi\epsilon_0 R^2 \sqrt{L^2 + 4R^2}} \vec{a}_y + \frac{\rho_l \cdot 2 \cdot L}{2\pi\epsilon_0 R^2 \sqrt{L^2 + 4R^2}} \vec{a}_z$$

b) Apply formula (3-176c)  $W_e = \frac{1}{2} \int_V \epsilon E^2 dv$

To simplify,  $\epsilon_0 \epsilon_r x = \epsilon_0 (L - x)$

We obtain  $x = \frac{L}{1 + \epsilon_r}$

P.4-1 Use subscripts d and a to denote dielectric and air regions respectively.  $\vec{\nabla} \cdot \vec{V} = 0$  in both regions.

$$V_d = c_1 y + c_2, \quad \vec{E}_d = -\vec{a}_y c_1, \quad \vec{D}_d = -\vec{a}_y \epsilon_0 \epsilon_r c_1.$$

$$V_a = c_3 y + c_4, \quad \vec{E}_a = -\vec{a}_y c_3, \quad \vec{D}_a = -\vec{a}_y \epsilon_0 c_3.$$

$$\text{B.C: At } y=0, V_d = 0; \quad \text{at } y=d, V_a = V_0;$$

$$\text{at } y=0.8d: V_d = V_a, \quad \vec{D}_d = \vec{D}_a.$$

$$\text{Solving: } c_1 = \frac{V_0}{(0.8+0.2\epsilon_r)d}, \quad c_2 = 0, \quad c_3 = \frac{\epsilon_r V_0}{(0.8+0.2\epsilon_r)d}, \quad c_4 = \frac{(1-\epsilon_r)V_0}{1+0.2\epsilon_r}.$$

$$a) V_d = \frac{5yV_0}{(4+\epsilon_r)d}, \quad \vec{E}_d = -\vec{a}_y \frac{5V_0}{(4+\epsilon_r)d}.$$

$$b) V_a = \frac{5\epsilon_r y - 4(\epsilon_r - 1)d}{(4+\epsilon_r)d} V_0, \quad \vec{E}_a = -\vec{a}_y \frac{5\epsilon_r V_0}{(4+\epsilon_r)d}.$$

$$c) (\rho_s)_{y=d} = -(\vec{D}_d)_{y=d} = \frac{5\epsilon_r \epsilon_0 V_0}{(4+\epsilon_r)d}.$$

$$(\rho_s)_{y=0} = (\vec{D}_d)_{y=0} = -\frac{5\epsilon_r \epsilon_0 V_0}{(4+\epsilon_r)d}.$$

$$\therefore \epsilon_r = 6 \Rightarrow$$

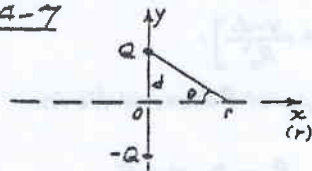
$$\therefore a) V_d = \frac{yV_0}{2d}, \quad \vec{E}_d = -\vec{a}_y \cdot \frac{V_0}{2d}$$

$$b) V_a = \frac{3V_0}{d} y - 2V_0, \quad \vec{E}_a = -\vec{a}_y \cdot \frac{3V_0}{d}$$

$$c) (\rho_s)_{y=d} = \frac{3V_0 \epsilon_0}{d}$$

$$(\rho_s)_{y=0} = -\frac{3V_0 \epsilon_0}{d}$$

P.4-7

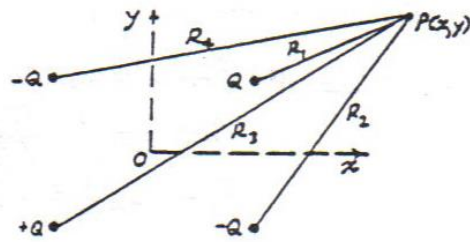
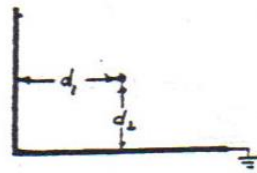


$$\vec{E} \Big|_{y=0} = -\vec{a}_y \frac{Q}{4\pi\epsilon r^2} (2 \sin \theta) = -\vec{a}_y \frac{Qd}{2\pi\epsilon (d^2 + r^2)^{3/2}}$$

$$a) \rho_s = \vec{a}_y \cdot \epsilon \vec{E} \Big|_{y=0} = -\frac{Qd}{2\pi\epsilon (d^2 + r^2)^{3/2}}$$

$$b) \int_0^\infty \rho_s 2\pi r dr = -Q.$$

P.4-8



Consider the conditions in the  $xy$ -plane ( $z=0$ ).

a)  $V_P = \frac{Q}{4\pi\epsilon} \left( \frac{1}{R_1} - \frac{1}{R_2} + \frac{1}{R_3} - \frac{1}{R_4} \right)$ , where

$$R_1 = [(x-d_1)^2 + (y-d_2)^2]^{1/2}, \quad R_2 = [(x-d_1)^2 + (y+d_2)^2]^{1/2},$$

$$R_3 = [(x+d_1)^2 + (y+d_2)^2]^{1/2}, \quad R_4 = [(x+d_1)^2 + (y-d_2)^2]^{1/2}.$$

$$\vec{E}_P = -\nabla V_P = -\bar{a}_x \frac{\partial V_P}{\partial x} - \bar{a}_y \frac{\partial V_P}{\partial y}$$

$$= \bar{a}_x \frac{Q}{4\pi\epsilon} \left[ -\frac{x-d_1}{R_1^3} + \frac{x-d_1}{R_2^3} - \frac{x+d_1}{R_3^3} + \frac{x+d_1}{R_4^3} \right]$$

$$+ \bar{a}_y \frac{Q}{4\pi\epsilon} \left[ -\frac{y-d_2}{R_1^3} + \frac{y+d_2}{R_2^3} - \frac{y+d_2}{R_3^3} + \frac{y-d_2}{R_4^3} \right].$$

$E_P$  will have a  $z$ -component if the point  $P$  does not lie in the  $xy$ -plane.

b) On the conducting half-planes,  $\rho_s = D_n = \epsilon E_n$ .

Along the  $x$ -axis,  $y=0$ :  $R_1 = [(x-d_1)^2 + d_2^2]^{1/2} = R_2$ ,

and  $R_3 = [(x+d_1)^2 + d_2^2]^{1/2} = R_4$ .

$$E_x = 0, \quad E_y = \frac{Q}{2\pi\epsilon} \left[ \frac{d_2}{R_1^3} - \frac{d_2}{R_3^3} \right].$$

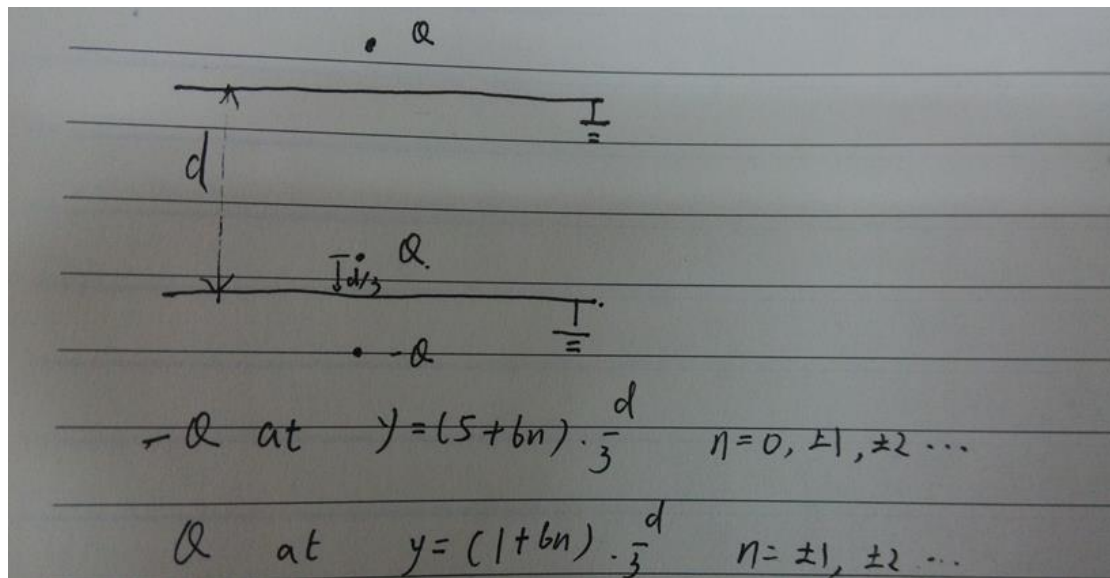
$$\therefore \rho_s(y=0) = \frac{Qd_2}{2\pi} \left\{ \frac{1}{[(x-d_1)^2 + d_2^2]^{3/2}} - \frac{1}{[(x+d_1)^2 + d_2^2]^{3/2}} \right\}$$

$$= \begin{cases} 0, & \text{at } x=0. \\ \text{max.}, & \text{at } x=d_1. \end{cases}$$

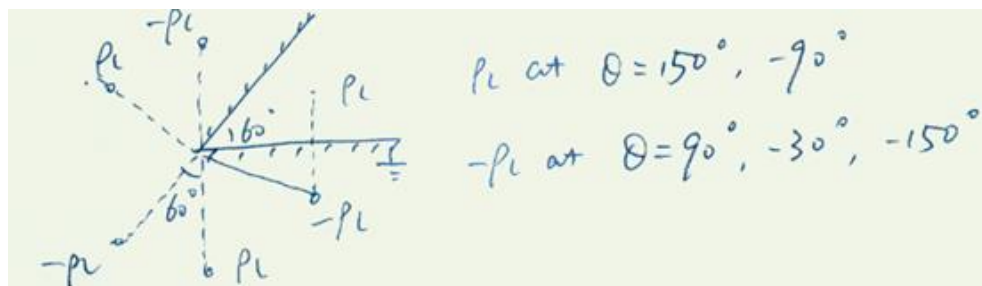
Similarly for  $\rho_s(x=0)$  on the vertical conducting plane by changing  $x$  to  $y$  and  $d_1 \leftrightarrow d_2$ .

P4-9

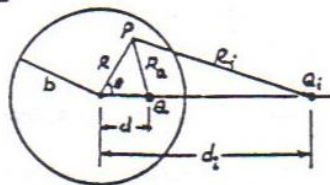
a)



b)



P.4-15



$$Q_i = -\frac{b}{a}Q, \quad d_i = \frac{b^2}{d}$$

$$a) V_p = \frac{Q}{4\pi\epsilon_0} \left( \frac{1}{R_a} - \frac{b}{dR_i} \right);$$

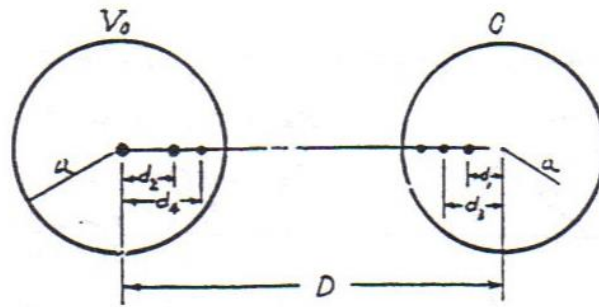
$$R_a = (R^2 + d^2 - 2Rd \cos \theta)^{1/2}$$

$$R_i = (R^2 + d_i^2 - 2Rd_i \cos \theta)^{1/2}$$

$$b) \rho_s = -\epsilon_0 \frac{\partial V}{\partial R} \Big|_{R=b} = -\frac{Q(b^2 - d^2)}{4\pi b (b^2 + d^2 - 2bd \cos \theta)^{3/2}}$$



P. 4-16



a)

$Q_0$  and system of image charges:

In left sphere

In right sphere

$$Q_0 \text{ at } d_0 = 0.$$

$$-Q_1 = -\frac{a}{D} Q_0 \text{ at } d_1.$$

$$Q_2 = \frac{a^2}{D(D-d_1)} Q_0 \text{ at } d_2.$$

$$-Q_3 = -\frac{a}{D-d_2} Q_2 = -\frac{a^3}{D(D-d_1)(D-d_2)} Q_0 \text{ at } d_3.$$

$$Q_4 = \frac{a^4}{D(D-d_1)(D-d_2)(D-d_3)} Q_0 \text{ at } d_4.$$

$\vdots$

$$Q_{2n} = Q_0 \prod_{m=1}^n \frac{a}{D-d_{m-1}} \text{ at } d_n. \quad -Q_{2n-1} = -Q_0 \prod_{m=1}^n \frac{a}{D-d_{m-1}} \text{ at } d_{n-1}.$$

$(n=2, 4, 6, \dots)$

$(n=1, 3, 5, \dots)$

$$d_m = \frac{a^2}{D-d_{m-1}} \quad m=1, 2, 3, \dots; \quad d_0=0.$$

$$b) \quad C = \frac{Q_0 + \sum Q_{2n}}{V_0} = 4\pi\epsilon_0 a \left[ 1 + \sum_{n=1, 3, \dots} \left( \prod_{m=1}^n \frac{a}{D-d_{m-1}} \right) \right].$$

P. 4-17 Required boundary conditions at  $x=0$ :  $V_1 = V_2$ , and  $\epsilon_1 \frac{\partial V_1}{\partial x} = \epsilon_2 \frac{\partial V_2}{\partial x}$ .

From Fig. 4-23 and the hypotheses in parts a) and b):

$$V_1 = \frac{Q}{4\pi\epsilon_1 \sqrt{(x-d)^2 + y^2 + z^2}} - \frac{Q_1}{4\pi\epsilon_1 \sqrt{(x+d)^2 + y^2 + z^2}},$$

$$V_2 = \frac{Q+Q_1}{4\pi\epsilon_2 \sqrt{(d-x)^2 + y^2 + z^2}}.$$

In order to satisfy the b.c.'s at  $x=0$ , we require

$$\frac{Q-Q_1}{\epsilon_1} = \frac{Q+Q_1}{\epsilon_2} \text{ and } Q+Q_1 = Q+Q_2 \rightarrow Q_1 = Q_2 = \frac{\epsilon_1 - \epsilon_2}{\epsilon_1 + \epsilon_2} Q.$$

$$P. 4-21 \quad V(x, y) = \sum_n \sin \frac{n\pi}{a} x \left[ A_n \sinh \frac{n\pi}{a} y + B_n \cosh \frac{n\pi}{a} y \right].$$

$$\text{At } y=0, \quad V(x, 0) = V_2 = \sum_n B_n \sin \frac{n\pi}{a} x \rightarrow B_n = \begin{cases} \frac{4V_2}{n\pi}, & n=\text{odd.} \\ 0, & n=\text{even.} \end{cases}$$

$$\text{At } y=b, \quad V(x, b) = V_1 = \sum_n \sin \frac{n\pi}{a} x \left[ A_n \sinh \frac{n\pi}{a} b + B_n \cosh \frac{n\pi}{a} b \right]$$

$$\rightarrow A_n \sinh \frac{n\pi}{a} b + B_n \cosh \frac{n\pi}{a} b = \begin{cases} \frac{4V_1}{n\pi}, & n=\text{odd.} \\ 0, & n=\text{even.} \end{cases}$$

$$\therefore A_n = \begin{cases} \frac{4}{n\pi \sinh(n\pi b/a)} (V_1 - V_2 \cosh \frac{n\pi}{a} b), & n=\text{odd.} \\ 0, & n=\text{even.} \end{cases}$$

P.4-23 Solution:  $V(\phi) = A_0\phi + B_0$ .

$$\begin{aligned} \text{a) B.C. ①: } V(0) = 0 &\longrightarrow B_0 = 0. \\ \text{B.C. ②: } V(\alpha) = V_0 = A_0\alpha &\longrightarrow A_0 = \frac{V_0}{\alpha}. \end{aligned} \left. \vphantom{\begin{aligned} \text{a) B.C. ①: } V(0) = 0 &\longrightarrow B_0 = 0. \\ \text{B.C. ②: } V(\alpha) = V_0 = A_0\alpha &\longrightarrow A_0 = \frac{V_0}{\alpha}. \end{aligned}} \right\} \therefore V(\phi) = \frac{V_0}{\alpha}\phi, \quad 0 \leq \phi \leq \alpha.$$

$$\begin{aligned} \text{b) B.C. ①: } V(\alpha) = V_0 = A_1\alpha + B_1 \\ \text{B.C. ②: } V(2\pi) = 0 = 2\pi A_1 + B_1 \end{aligned} \left. \vphantom{\begin{aligned} \text{b) B.C. ①: } V(\alpha) = V_0 = A_1\alpha + B_1 \\ \text{B.C. ②: } V(2\pi) = 0 = 2\pi A_1 + B_1 \end{aligned}} \right\} \longrightarrow A_1 = -\frac{V_0}{2\pi - \alpha}, \quad B_1 = \frac{2\pi V_0}{2\pi - \alpha}.$$
$$\therefore V(\phi) = \frac{V_0}{2\pi - \alpha}(2\pi - \phi), \quad \alpha \leq \phi \leq 2\pi.$$

P.5-6  $\rho_0 = \frac{Q_0}{(4\pi/3)b^3} = \frac{10^{-3}}{(4\pi/3)(0.1)^3} = 0.239 \text{ (C/m}^3\text{)}, \quad \rho = \rho_0 e^{-(r/\epsilon)t}$

a)  $R < b: \vec{E}_i = \vec{a}_R \frac{(4\pi/3)R^3\rho}{4\pi\epsilon R^2} = \vec{a}_R \frac{\rho_0 R}{3\epsilon} e^{-(r/\epsilon)t} = \vec{a}_R 7.5 \times 10^9 R e^{-9.42 \times 10^{10} t} \text{ (V/m)}$

$R > b: \vec{E}_o = \vec{a}_R \frac{Q_0}{4\pi\epsilon_0 R^2} = \vec{a}_R \frac{q}{R^2} \times 10^6 \text{ (V/m)}$

b)  $R < b: \vec{J}_i = \sigma \vec{E}_i = \vec{a}_R 7.5 \times 10^{10} R e^{-9.42 \times 10^{10} t}$

$R > b: \vec{J}_o = 0.$

P.5-9 a) Eq. (3-118):  $E_{1t} = E_{2t} \rightarrow E_1 \sin \alpha_1 = E_2 \sin \alpha_2$

Eq. (5-58):  $J_{1n} = J_{2n} \rightarrow \sigma_1 E_{1n} = \sigma_2 E_{2n} \rightarrow \sigma_2 E_2 \cos \alpha_2 = \sigma_1 E_1 \cos \alpha_1$

$\therefore E_2 = E_1 \sqrt{\sin^2 \alpha_1 + \left(\frac{\sigma_1}{\sigma_2} \cos \alpha_1\right)^2}$  ①

$\tan \alpha_2 = \frac{\sigma_2}{\sigma_1} \tan \alpha_1 \rightarrow \alpha_2 = \tan^{-1} \left( \frac{\sigma_2}{\sigma_1} \tan \alpha_1 \right)$  ②

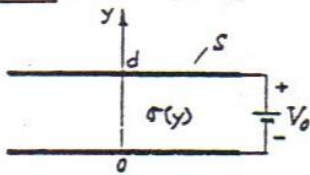
b) Eq. (3-121b):  $D_{2n} - D_{1n} = \rho_s \rightarrow \epsilon_2 E_{2n} - \epsilon_1 E_{1n} = \rho_s$

$\rho_s = \left( \frac{\sigma_1}{\sigma_2} \epsilon_2 - \epsilon_1 \right) E_{1n} = \left( \frac{\sigma_1}{\sigma_2} \epsilon_2 - \epsilon_1 \right) E_1 \cos \alpha_1$

c) If both media are perfect dielectrics,  $\sigma_1 = \sigma_2 = 0$ , Eqs.

① and ② revert to Eqs. (3-130) and (3-129) respectively and  $\rho_s = 0$ .

P.5-10



$\sigma(y) = \sigma_1 + (\sigma_2 - \sigma_1) \frac{y}{d}$

a) Neglecting fringing effect and assuming a current density

$\vec{J} = -\vec{a}_y J_0 \rightarrow \vec{E} = \frac{\vec{J}}{\sigma} = -\vec{a}_y \frac{J_0}{\sigma(y)}$

$V_0 = -\int_0^d \vec{E} \cdot \vec{a}_y dy = \int_0^d \frac{J_0 dy}{\sigma_1 + (\sigma_2 - \sigma_1) \frac{y}{d}} = \frac{J_0 d}{\sigma_2 - \sigma_1} \ln \frac{\sigma_2}{\sigma_1}$

$R = \frac{V_0}{I} = \frac{V_0}{J_0 S} = \frac{d}{(\sigma_2 - \sigma_1) S} \ln \frac{\sigma_2}{\sigma_1}$

b)  $(\rho_s)_u = \epsilon_0 E_y(d) = \frac{\epsilon_0 J_0}{\sigma_2} = \frac{\epsilon_0 (\sigma_2 - \sigma_1) V_0}{\sigma_2 d \ln(\sigma_2/\sigma_1)}$  on upper plate,

$(\rho_s)_l = -\epsilon_0 E_y(0) = -\frac{\epsilon_0 J_0}{\sigma_1} = -\frac{\epsilon_0 (\sigma_2 - \sigma_1) V_0}{\sigma_1 d \ln(\sigma_2/\sigma_1)}$  on lower plate.

c)  $\rho = \vec{\nabla} \cdot \vec{D} = \frac{d}{dy} (\epsilon_0 E) = -\epsilon_0 J_0 \frac{d}{dy} \left[ \frac{1}{\sigma_1 + (\sigma_2 - \sigma_1) y/d} \right] = \epsilon_0 J_0 \frac{(\sigma_2 - \sigma_1)/d}{[\sigma_1 + (\sigma_2 - \sigma_1) y/d]^2}$

P.5-12 Refer to Fig. 5-6. In the transient state, the equation of continuity must be satisfied at the interface.

$-\frac{\partial \rho_{si}}{\partial t} = J_2 - J_1 = \sigma_2 E_2 - \sigma_1 E_1$  ①

Now

$E_1 d_1 + E_2 d_2 = V$  ②

$\epsilon_2 E_2 - \epsilon_1 E_1 = \rho_{si}$  ③



Solving ② and ③ for  $E_1$  and  $E_2$  in terms of  $V$  and  $\rho_{si}$ :

$$E_1 = \frac{\epsilon_2 V - d_2 \rho_{si}}{\epsilon_2 d_1 + \epsilon_1 d_2} \quad (4); \quad E_2 = \frac{\epsilon_1 V + d_1 \rho_{si}}{\epsilon_2 d_1 + \epsilon_1 d_2} \quad (5).$$

a) Substituting ④ and ⑤ in ①:

$$-\frac{\partial \rho_{si}}{\partial t} = \frac{\sigma_2 d_1 + \sigma_1 d_2}{\epsilon_2 d_1 + \epsilon_1 d_2} \rho_{si} + \frac{\epsilon_1 \sigma_1 - \epsilon_2 \sigma_2}{\epsilon_2 d_1 + \epsilon_1 d_2} V. \quad (6)$$

Solution of ⑥:

$$\rho_{si} = \left( \frac{\epsilon_2 \sigma_1 - \epsilon_1 \sigma_2}{\epsilon_2 d_1 + \epsilon_1 d_2} \right) V \left[ 1 - e^{-t/\tau} \right], \quad (7)$$

$$\text{where } \tau = \text{Relaxation time} = \frac{\epsilon_2 d_1 + \epsilon_1 d_2}{\sigma_2 d_1 + \sigma_1 d_2}. \quad (8)$$

b) Using ④ and ⑤:

$$E_1 = \frac{\sigma_2 V}{\sigma_2 d_1 + \sigma_1 d_2} (1 - e^{-t/\tau}) + \frac{\epsilon_1 V}{\epsilon_2 d_1 + \epsilon_1 d_2} e^{-t/\tau};$$

$$E_2 = \frac{\sigma_1 V}{\sigma_2 d_1 + \sigma_1 d_2} (1 - e^{-t/\tau}) + \frac{\epsilon_2 V}{\epsilon_2 d_1 + \epsilon_1 d_2} e^{-t/\tau}.$$

P.5-14  $\nabla^2 V = 0 \rightarrow \frac{1}{r} \frac{\partial}{\partial r} \left( r \frac{\partial V}{\partial r} \right) = 0.$

Solution:  $V(r) = c_1 \ln r + c_2.$

Boundary conditions:  $V(a) = V_0; \quad V(b) = 0.$

$$\rightarrow V(r) = V_0 \frac{\ln(b/r)}{\ln(b/a)}.$$

$$\bar{E}(r) = -\bar{a}_r \frac{\partial V}{\partial r} = \bar{a}_r \frac{V_0}{r \ln(b/a)}.$$

$$\bar{J}(r) = \sigma \bar{E}(r).$$

$$I = \int_S \bar{J} \cdot d\bar{S} = \int_0^{2\pi} \int_a^b \bar{J} \cdot (\bar{a}_r h r d\phi) = \frac{\pi \sigma h V_0}{2 \ln(b/a)}.$$

$$R = \frac{V_0}{I} = \frac{2 \ln(b/a)}{\pi \sigma h}.$$

P.5-17 Assume  $I$ .  $\bar{J}(R) = \bar{a}_R \frac{I}{S(R)}.$

$$S(R) = \int_0^{2\pi} \int_0^{\theta_0} R^2 \sin \theta d\theta d\phi = 2\pi R^2 (1 - \cos \theta_0).$$

$$\bar{E}(R) = \frac{1}{\sigma} \bar{J}(R) = \bar{a}_R \frac{I}{2\pi \sigma R^2 (1 - \cos \theta_0)}.$$

$$V_0 = -\int_{R_2}^{R_1} E(R) dR = \frac{I(R_2 - R_1)}{2\pi \sigma R_1 R_2 (1 - \cos \theta_0)}.$$

$$R = \frac{V_0}{I} = \frac{1}{2\pi (1 - \cos \theta_0)} \left( \frac{1}{R_1} - \frac{1}{R_2} \right).$$

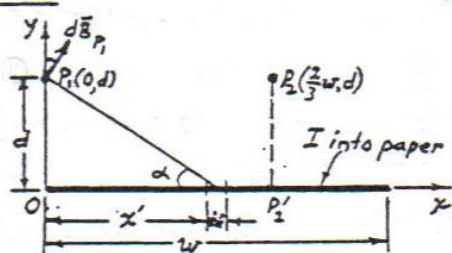
P.6-3 Application of Ampère's circuital law.

$$0 \leq r \leq a, \quad \bar{B} = \bar{a}_\phi \frac{\mu_r I}{2\pi a^2}.$$

$$a \leq r \leq b, \quad \bar{B} = \bar{a}_\phi \frac{\mu I}{2\pi r}.$$

$$b \leq r \leq c, \quad \bar{B} = \bar{a}_\phi \left( \frac{c^2 - r^2}{c^2 - b^2} \right) \frac{\mu I}{2\pi r}.$$

P.6-4



a) Using Eq. (6-33c):

$$d\bar{B}_P = \bar{a}_x dB_x + \bar{a}_y dB_y$$

$$= \bar{a}_x (dB_P) \sin \alpha + \bar{a}_y (dB_P) \cos \alpha,$$

$$dB_P = \frac{\mu_0 (I/w) dx'}{2\pi (x'^2 + d^2)^{3/2}}$$

$$\sin \alpha = \frac{d}{(x'^2 + d^2)^{1/2}}, \quad \cos \alpha = \frac{x'}{(x'^2 + d^2)^{1/2}}$$

$$\therefore \bar{B}_{P_1} = \bar{a}_x B_x + \bar{a}_y B_y,$$

$$\text{where } B_x = \frac{\mu_0 I d}{2\pi w} \int_0^w \frac{dx'}{x'^2 + d^2} = \frac{\mu_0 I}{2\pi w} \tan^{-1} \left( \frac{w}{d} \right),$$

$$B_y = \frac{\mu_0 I}{2\pi w} \int_0^w \frac{x' dx'}{x'^2 + d^2} = \frac{\mu_0 I}{4\pi w} \ln \left( 1 + \frac{w^2}{d^2} \right).$$

b) To find  $B$  at  $P_2(\frac{2}{3}w, d)$ , we add vectorially the contributions of the current strips to the right and to the left of point  $P_2'$  using the result in part (a).

$$\bar{B}_{P_2} = \bar{B}_{2R} + \bar{B}_{2L}.$$

$$\bar{B}_{2R} = \frac{\mu_0 I}{2\pi w} \left[ \bar{a}_x \tan^{-1} \left( \frac{w}{3d} \right) + \bar{a}_y \frac{1}{2} \ln \left( 1 + \frac{w^2}{9d^2} \right) \right],$$

$$\bar{B}_{2L} = \frac{\mu_0 I}{2\pi w} \left[ -\bar{a}_x \tan^{-1} \left( \frac{2w}{3d} \right) - \bar{a}_y \frac{1}{2} \ln \left( 1 + \frac{4w^2}{9d^2} \right) \right].$$

$$\therefore \bar{B}_{P_2} = \frac{\mu_0 I}{2\pi w} \left[ \bar{a}_x \left( \tan^{-1} \frac{w}{3d} + \tan^{-1} \frac{2w}{3d} \right) - \bar{a}_y \ln \sqrt{\frac{1 + (2w/3d)^2}{1 + (w/3d)^2}} \right].$$

P.6-6 The problem can be decomposed into two subproblems (assuming  $b$  = radius of solenoid):

1. A cylindrical tube carrying a uniformly distributed longitudinal surface current  $2\pi b n I \sin \alpha$ .

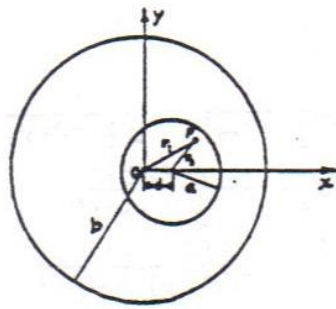
$$\longrightarrow \bar{B}_1 = \begin{cases} 0, & 0 < r < b, \\ \bar{a}_\phi \frac{b n I}{r} \sin \alpha, & r > b. \end{cases}$$

2. A solenoid with  $n$  turns per unit length carrying a current  $I \cos \alpha$ .

$$\longrightarrow \bar{B}_2 = \begin{cases} \bar{a}_z \mu_0 n I \cos \alpha, & 0 < r < b, \\ 0, & r > b. \end{cases}$$

$$\text{Total } \bar{B} = \bar{B}_1 + \bar{B}_2.$$

P.6-15  $\vec{J} = \vec{a}_z J$ ,  $\oint \vec{B} \cdot d\vec{L} = \mu_0 I$ .



If there is no hole,

$$2\pi r_1 B_{\phi 1} = \mu_0 \pi r_1^2 J$$

$$\rightarrow B_{\phi 1} = \frac{\mu_0 r_1}{2} J \rightarrow \begin{cases} B_{x1} = -\frac{\mu_0 J}{2} y_1 \\ B_{y1} = +\frac{\mu_0 J}{2} x_1 \end{cases}$$

For  $-\vec{J}$  in the hole portion:

$$B_{\phi 2} = -\frac{\mu_0 r_2}{2} J \rightarrow \begin{cases} B_{x2} = +\frac{\mu_0 J}{2} y_2 \\ B_{y2} = -\frac{\mu_0 J}{2} x_2 \end{cases}$$

Superposing  $B_{\phi 1}$  and  $B_{\phi 2}$  and noting that  $x_1 = y_2$  and  $y_1 = x_2 + d$ ,

we have  $B_x = B_{x1} + B_{x2} = 0$ , and  $B_y = B_{y1} + B_{y2} = \frac{\mu_0 J}{2} d$ .

P.6-18 Eq. (6-34) for one wire:  $\vec{A} = \vec{a}_z \frac{\mu_0 I}{4\pi} \ln \frac{\sqrt{L^2 + r^2} + L}{\sqrt{L^2 + r^2} - L}$ .

For two wires carrying equal and opposite currents:

a)  $\vec{A} = \vec{a}_z \frac{\mu_0 I}{4\pi} \ln \left[ \frac{\sqrt{L^2 + r_1^2} + L}{\sqrt{L^2 + r_1^2} - L} \cdot \frac{\sqrt{L^2 + r_2^2} - L}{\sqrt{L^2 + r_2^2} + L} \right] = \vec{a}_z \frac{\mu_0 I}{2\pi} \ln \left[ \frac{r_1}{r_2} \frac{\sqrt{L^2 + r_2^2} - L}{\sqrt{L^2 + r_1^2} + L} \right]$ .

b) For a very long two-wire transmission line,  $L \rightarrow \infty$ :

$$\vec{A} = \vec{a}_z \frac{\mu_0 I}{2\pi} \ln \left( \frac{r_1}{r_2} \right) = \vec{a}_z \frac{\mu_0 I}{4\pi} \ln \frac{(\frac{d}{2} + y)^2 + x^2}{(\frac{d}{2} - y)^2 + x^2}$$

c)  $\vec{B} = \nabla \times \vec{A} = \vec{a}_x \frac{\partial A_z}{\partial y} - \vec{a}_y \frac{\partial A_z}{\partial x}$

$$= \vec{a}_x \frac{\mu_0 I}{2\pi} \left[ \frac{\frac{d}{2} + y}{(\frac{d}{2} + y)^2 + x^2} - \frac{\frac{d}{2} - y}{(\frac{d}{2} - y)^2 + x^2} \right] - \vec{a}_y \frac{\mu_0 I}{2\pi} \left[ \frac{x}{(\frac{d}{2} + y)^2 + x^2} - \frac{x}{(\frac{d}{2} - y)^2 + x^2} \right]$$

$$= \frac{\mu_0 I}{2\pi} \left[ \vec{a}_{\phi 1} \frac{1}{r_1} - \vec{a}_{\phi 2} \frac{1}{r_2} \right]$$

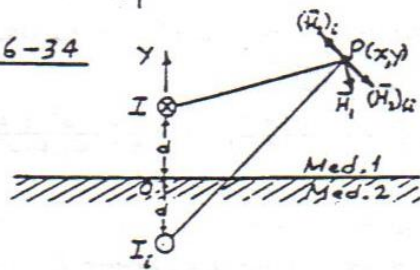
d) To find the equation for magnetic flux lines:

$$\frac{dx}{B_z} = \frac{dy}{B_y} \rightarrow \frac{\partial A}{\partial x} dx + \frac{\partial A}{\partial y} dy = 0$$

$$\rightarrow dA = 0 \rightarrow A = \text{constant}$$

Thus,  $\frac{r_1^2}{r_2^2} = \frac{(\frac{d}{2} + y)^2 + x^2}{(\frac{d}{2} - y)^2 + x^2} = K$ .

P.6-34



a) (i) If  $\sigma_2 \rightarrow \infty$ ,  $\bar{B}_2 = \bar{H}_2 = 0$ .

$B_n$  continuous  $\rightarrow B_{1n} = H_{1n} = 0$ ;

$\bar{a}_y \times \bar{H}_1 = \bar{J}_s \rightarrow \bar{J}_s = -\bar{a}_z H_{1x}$ .

Image  $I_i (= -I)$  flowing out of the paper.

(ii) If  $\mu_2 \rightarrow \infty$ ,  $\bar{H}_2 = 0$ , but  $\bar{B}_2$  is finite.

No surface current.  $\rightarrow H_{1t} = H_{2t} = 0$ ;

$B_n$  continuous  $\rightarrow B_{1n} = B_{2n}$ .

Image  $I_i (= I)$  flowing into the paper.

b) (i)  $\bar{H}_p = \bar{H}_1 + (\bar{H}_2)_i$ , where  $\bar{H}_1 = \frac{I}{2\pi} \left[ \bar{a}_x \frac{y-d}{x^2 + (y-d)^2} - \bar{a}_y \frac{x}{x^2 + (y-d)^2} \right]$ ,  
 $(\bar{H}_2)_i = \frac{I}{2\pi} \left[ -\bar{a}_x \frac{y+d}{x^2 + (y+d)^2} + \bar{a}_y \frac{x}{x^2 + (y+d)^2} \right]$ .

(ii)  $\bar{H}'_p = \bar{H}_1 + (\bar{H}_2)_{ii} = \bar{H}_1 - (\bar{H}_2)_i$ .

c) (i)  $\bar{J}_s = -\bar{a}_z (H_p)_x|_{y=0} = \bar{a}_z \left( \frac{Id}{x^2 + d^2} \right)$ .

(ii)  $\bar{J}_s = 0$ .



P.7-6 a) Flux enclosed in the ring in Fig. 7-12(w):  $\Phi = \pi r^2 B(t)$  ①

The induced emf in the ring referring to the assigned direction for current:  $\mathcal{V} = iR_r = \frac{d\Phi}{dt} = \pi r^2 \frac{dB(t)}{dt}$  ②

Resistance of differential circular ring:  $R_r = \frac{2\pi r}{\sigma h dr}$  ③

Combining ② and ③:  $i = \frac{\pi r^2}{R_r} \frac{dB(t)}{dt} = \frac{\sigma h}{2} r dr \left(\frac{dB}{dt}\right)^2$  ④

$dP = i^2 R_r = \frac{\pi \sigma h}{2} r^3 dr \left(\frac{dB}{dt}\right)^2$  ⑤

$P = \int dP = \frac{\pi \sigma h}{8} a^4 \left(\frac{dB}{dt}\right)^2 = \frac{\pi \sigma h}{8} a^4 \omega^2 B_0^2 \cos^2 \omega t$  ⑥

$P_{av} = \frac{\pi \sigma h}{16} a^4 \omega^2 B_0^2$  ⑦

b) For  $N$  insulated filamentary parts, each with an area

$$S = \frac{0.95 \pi a^2}{N} = \pi b^2 \rightarrow b = \sqrt{\frac{S}{\pi}} = a \sqrt{\frac{0.95}{N}}$$

Power loss in  $N$  filaments in Fig. 7-12 (b) from ⑥  $P' = N \left( \frac{\pi \sigma h}{8} \right) \left( a \sqrt{\frac{0.95}{N}} \right)^4 \omega^2 B_0^2 \cos^2 \omega t = \frac{0.95}{N} P$   
 $P'_{av} = \frac{0.95}{N} P_{av}$

P.7-7  $\Phi(t) = \vec{B}(t) \cdot \vec{S}(t) = -(5 \cos \omega t) \times 0.2 (0.7 - x)$   
 $= -0.35 \cos \omega t (1 + \cos \omega t) \quad (\text{mT})$   
 $i = -\frac{1}{R} \frac{d\Phi}{dt} = -\frac{1}{R} 0.35 \omega (\sin \omega t + \sin 2\omega t)$   
 $= -1.75 \omega \sin \omega t (1 + 2 \cos \omega t) \quad (\text{mA})$

P.7-10 a)  $\mu_r = 1 + \chi_m$ ,  $\chi_m = 5000 - 1 = 4999$ ,  
 $\vec{H} = \frac{\vec{M}}{\chi_m} = \vec{a}_z \frac{M_0}{4999}$ ;  $\vec{B} = \mu_0 \mu_r \vec{H} = \vec{a}_z \frac{5000}{4999} \mu_0 M_0$

b)  $V_0 = \oint \vec{u} \times \vec{B} \cdot d\vec{L} = \int_a^b (\vec{a}_\phi \omega r) \times (\vec{a}_z B) \cdot \vec{a}_r dr$   
 $= -\frac{\omega B}{2} (b^2 - a^2) = -\frac{2500}{4999} \mu_0 M_0 \omega (b^2 - a^2)$

c)  $\vec{E}_r = \vec{E}'_r - \vec{u} \times \vec{B} = \frac{\vec{J}_r}{\sigma} - (\vec{a}_\phi \omega r) \times (\vec{a}_z B) = \vec{a}_r \left( \frac{i}{2\pi r h \sigma} - \omega r B \right)$   
 Induced voltage  $V = \int_a^b E_r dr = \frac{i}{2\pi h \sigma} \ln \frac{b}{a} - \frac{\omega B}{2} (b^2 - a^2)$   
 $= iR + V_0$

Short circuit:  $V_0 = 0$ ,  $i_{sc} = \frac{\omega B}{2R} (b^2 - a^2)$ , where  $R = \frac{\ln(b/a)}{2\pi h \sigma}$

P.7-18 a) Eq. (3-89):  $\vec{\nabla} \cdot \vec{P} = -\rho_p \rightarrow \vec{a}_{n2} \cdot (\vec{P}_1 - \vec{P}_2) = -\rho_{ps}$

b)  $\epsilon_0 \vec{E} = \vec{D} - \vec{P} \begin{cases} \vec{\nabla} \cdot \vec{D} = \rho_f \rightarrow \vec{a}_{n2} \cdot (\vec{D}_1 - \vec{D}_2) = \rho_{fs} & ① \\ -\vec{\nabla} \cdot \vec{P} = \rho_p \rightarrow \vec{a}_{n2} \cdot (\vec{P}_1 - \vec{P}_2) = -\rho_{ps} & ② \end{cases}$

Combining ① & ②  $\vec{a}_{n2} \cdot (\vec{E}_1 - \vec{E}_2) = \frac{1}{\epsilon_0} (\rho_{fs} + \rho_{ps})$  Subscript f signifies free charge.



P. 7-19 Medium 1: Free space.

Medium 2:  $\mu_2 \rightarrow \infty$ .  $H_2$  must be zero so that  $B_2$  is not infinite.

Boundary Conditions:  $\vec{a}_{n1} \times \vec{H}_1 = \vec{J}_s$ ,  $B_{1n} = B_{2n}$ .

$E_{1t} = E_{2t}$ ,  $\vec{a}_{n2} \cdot (\vec{D}_1 - \vec{D}_2) = \rho_s$ .

P. 7-23  $\vec{E}_1(z,t) = \vec{a}_x 0.03 \sin 10^8 \pi (t - \frac{z}{c}) = \vec{a}_x \mathcal{R}_e [0.03 e^{-j\pi/2} e^{j10^8 \pi (t - z/c)}]$ ,

$\vec{E}_2(z,t) = \vec{a}_x 0.04 \cos [10^8 \pi (t - \frac{z}{c}) - \frac{\pi}{3}] = \vec{a}_x \mathcal{R}_e [0.04 e^{j\pi/3} e^{j10^8 \pi (t - z/c)}]$ .

Phasors:  $\vec{E} = \vec{E}_1 + \vec{E}_2 = \vec{a}_x [0.03 e^{-j\pi/2} + 0.04 e^{j\pi/3}]$

$= \vec{a}_x [-j0.03 + (0.02 - j0.02\sqrt{3})] = \vec{a}_x (0.065 e^{j1.27}) = \vec{a}_x E_0 e^{j\theta}$

$\therefore E_0 = 0.065$ ,  $\theta = -1.27 \text{ (rad)}$ , or  $-72.8^\circ$

P. 7-29  $\vec{H} = j\omega \epsilon_0 \vec{\nabla} \times \vec{\pi}_e$ . ①

$\vec{\nabla} \times \vec{E} = -j\omega \mu_0 \vec{H} = \omega^2 \mu_0 \epsilon_0 \vec{\nabla} \times \vec{\pi}_e$ , ②

$\rightarrow \vec{\nabla} \times (\vec{E} - k_0^2 \vec{\pi}_e) = 0$ . Let  $\vec{E} - k_0^2 \vec{\pi}_e = \vec{\nabla} V_e$ . ③

$\vec{\nabla} \times \vec{H} = j\omega \vec{D} = j\omega (\epsilon_0 \vec{E} + \vec{P}) = j\omega \epsilon_0 (\vec{E} + \frac{\vec{P}}{\epsilon_0})$ . ④

Substituting ① and ② in ③:

$j\omega \epsilon_0 \vec{\nabla} \times \vec{\nabla} \times \vec{\pi}_e = j\omega \epsilon_0 (k_0^2 \vec{\pi}_e + \vec{\nabla} V_e + \frac{\vec{P}}{\epsilon_0})$   
 $= j\omega \epsilon_0 (\vec{\nabla} \vec{\nabla} \cdot \vec{\pi}_e - \nabla^2 \vec{\pi}_e)$ . ⑤

Choose  $\vec{\nabla} \cdot \vec{\pi}_e = V_e$ . Eq. ④ becomes

b)  $\nabla^2 \vec{\pi}_e + k_0^2 \vec{\pi}_e = -\frac{\vec{P}}{\epsilon_0}$ . (7-119)

a) Eq. ② becomes

$\vec{E} = k_0^2 \vec{\pi}_e + \vec{\nabla} \vec{\nabla} \cdot \vec{\pi}_e$   
 $= k_0^2 \vec{\pi}_e + (\nabla^2 \vec{\pi}_e + \vec{\nabla} \times \vec{\nabla} \times \vec{\pi}_e)$ . ⑥

Combination of Eqs. (7-119) and ⑥ gives

$\vec{E} = \vec{\nabla} \times \vec{\nabla} \times \vec{\pi}_e - \frac{\vec{P}}{\epsilon_0}$ .

P.7-30

$$a) \left| \frac{\text{Displacement current}}{\text{Conduction current}} \right| = \frac{\omega \epsilon}{\sigma} = \frac{(2\pi \times 100 \times 10^3) \times \frac{1}{36\pi} \times 10^{-9}}{5.70 \times 10^7} = 9.75 \times 10^{-8}.$$

b) In a source-free conductor:

$$\vec{\nabla} \times \vec{H} = \sigma \vec{E}, \quad (1)$$

$$\vec{\nabla} \times \vec{E} = -j\omega\mu\vec{H}. \quad (2)$$

$$\vec{\nabla} \times (1): \vec{\nabla} \times \vec{\nabla} \times \vec{H} = \vec{\nabla}(\vec{\nabla} \cdot \vec{H}) - \vec{\nabla}^2 \vec{H} = \sigma \vec{\nabla} \times \vec{E}. \quad (3)$$

But  $\vec{\nabla} \cdot \vec{H} = 0$ , Eq. (3) becomes

$$\vec{\nabla}^2 \vec{H} + \sigma \vec{\nabla} \times \vec{E} = 0. \quad (4)$$

Combining (2) and (4):

$$\vec{\nabla}^2 \vec{H} - j\omega\mu\sigma\vec{H} = 0.$$

P. 8-6 Phasor:  $\vec{E} = \vec{a}_x 2 e^{-jz/\sqrt{3}} + \vec{a}_y j e^{-jz/\sqrt{3}}$  (V/m).

a)  $\omega = 10^8$  (rad/s)  $\rightarrow f = 10^8/2\pi = 1.59 \times 10^7$  (Hz),

$\beta = 1/\sqrt{3}$  (rad/m)  $\rightarrow \lambda = 2\pi/\beta = 2\sqrt{3}\pi$  (m).

b)  $u = \frac{c}{\sqrt{\epsilon_r}} = \frac{\omega}{\beta} \rightarrow \epsilon_r = \left(\frac{\beta c}{\omega}\right)^2 = 3.$

c) Left-hand elliptically polarized.

d)  $\eta = \sqrt{\frac{\mu}{\epsilon}} = \frac{120\pi}{\sqrt{\epsilon_r}} = \frac{120\pi}{\sqrt{3}}$  ( $\Omega$ ),

$\vec{H} = \frac{1}{\eta} \vec{a}_z \times \vec{E} = \frac{\sqrt{3}}{120\pi} (\vec{a}_y 2 e^{-jz/\sqrt{3}} - \vec{a}_x j e^{-jz/\sqrt{3}}),$

$\vec{H}(z,t) = \frac{\sqrt{3}}{120\pi} [\vec{a}_x \sin(10^8 t - z/\sqrt{3}) + \vec{a}_y \cos(10^8 t - z/\sqrt{3})]$  (A/m).

P. 8-9 For conducting media:  $k_c = \beta - j\alpha.$

$k_c^2 = \beta^2 - \alpha^2 - 2j\alpha\beta$

$= \omega^2 \mu \epsilon_c = \omega^2 \mu \epsilon (1 - j \frac{\sigma}{\omega \epsilon}).$

$\therefore \beta^2 - \alpha^2 = \Re(k_c^2) = \omega^2 \mu \epsilon, \quad \textcircled{1}$

$\beta^2 + \alpha^2 = |k_c^2| = \omega^2 \mu \epsilon \sqrt{1 + \left(\frac{\sigma}{\omega \epsilon}\right)^2}. \quad \textcircled{2}$

From ① and ② we obtain

$\alpha = \omega \sqrt{\frac{\mu \epsilon}{2}} \left[ \sqrt{1 + \left(\frac{\sigma}{\omega \epsilon}\right)^2} - 1 \right]^{1/2}, \quad \beta = \omega \sqrt{\frac{\mu \epsilon}{2}} \left[ \sqrt{1 + \left(\frac{\sigma}{\omega \epsilon}\right)^2} + 1 \right]^{1/2}.$

P.8-10 All three metals are good conductors,  $(\frac{\sigma}{\omega\epsilon})^2 \gg 1$ .  
 $\alpha = \sqrt{\pi f \mu \sigma}$ ,  $\delta = \frac{1}{\alpha}$ ,  $\eta_c = (1+j) \frac{\alpha}{\sigma}$ .

a)  $f = 60 \text{ (Hz)}$

	$\eta_c (\Omega)$	$\alpha \text{ (Np/m)}$	$\alpha \text{ (dB/m)}$	$\delta \text{ (m)}$
Copper	$2.02(1+j) \times 10^{-5}$	$0.117 \times 10^3$	$1.02 \times 10^3$	$8.53 \times 10^{-3}$
Silver	$2.08(1+j) \times 10^{-5}$	$0.121 \times 10^3$	$1.05 \times 10^3$	$8.29 \times 10^{-3}$
Brass	$2.86(1+j) \times 10^{-5}$	$0.061 \times 10^3$	$0.53 \times 10^3$	$16.3 \times 10^{-3}$

b)  $f = 1 \text{ (MHz)}$

	$\eta_c (\Omega)$	$\alpha \text{ (Np/m)}$	$\alpha \text{ (dB/m)}$	$\delta \text{ (m)}$
Copper	$2.61(1+j) \times 10^{-4}$	$1.51 \times 10^4$	$1.31 \times 10^5$	$6.61 \times 10^{-5}$
Silver	$2.57(1+j) \times 10^{-4}$	$1.58 \times 10^4$	$1.35 \times 10^5$	$6.32 \times 10^{-5}$
Brass	$4.98(1+j) \times 10^{-4}$	$0.79 \times 10^4$	$0.69 \times 10^5$	$12.6 \times 10^{-5}$

c)  $f = 1 \text{ (GHz)}$

	$\eta_c (\Omega)$	$\alpha \text{ (Np/m)}$	$\alpha \text{ (dB/m)}$	$\delta \text{ (m)}$
Copper	$8.25(1+j) \times 10^{-3}$	$4.79 \times 10^5$	$4.16 \times 10^6$	$2.09 \times 10^{-6}$
Silver	$8.01(1+j) \times 10^{-3}$	$4.93 \times 10^5$	$4.28 \times 10^6$	$2.03 \times 10^{-6}$
Brass	$15.8(1+j) \times 10^{-3}$	$2.51 \times 10^5$	$2.18 \times 10^6$	$3.99 \times 10^{-6}$

P.8-11  $f = 3 \times 10^9 \text{ (Hz)}$ ,  $\epsilon_r = 2.5$ ,  $\tan \delta_c = \frac{\epsilon''}{\epsilon'} = 10^{-2}$

a) Eq. (8-48):  $\alpha = \frac{\omega \epsilon''}{2} \sqrt{\frac{\mu}{\epsilon'}} = \frac{\omega}{2} \left( \frac{\epsilon''}{\epsilon'} \right) \frac{\sqrt{\epsilon_r}}{c} = 0.497 \text{ (Np/m)}.$

$e^{-\alpha x} = \frac{1}{2} \rightarrow x = \frac{1}{\alpha} \ln 2 = 1.395 \text{ (m)}.$

b) Eq. (8-50):  $\eta_c = \frac{1}{\sqrt{\epsilon_r}} \sqrt{\frac{\mu_0}{\epsilon_0}} \left( 1 + j \frac{\epsilon''}{2\epsilon'} \right) = 238(1 + j0.005) = 238 \angle 0.29^\circ (\Omega),$

Eq. (8-49):  $\beta = \omega \sqrt{\mu \epsilon} \left[ 1 + \frac{1}{8} \left( \frac{\epsilon''}{\epsilon'} \right)^2 \right] = 31.6\pi \text{ (rad/m)}.$

$\lambda = \frac{2\pi}{\beta} = 0.063 \text{ (m)},$

$u_p = \frac{\omega}{\beta} = 1.8973 \times 10^8 \text{ (m/s)}.$

$u_g = \frac{1}{\frac{d\beta}{d\omega}} = \frac{c}{\sqrt{\epsilon_r}} \left[ 1 + \frac{1}{8} \left( \frac{\epsilon''}{\epsilon'} \right)^2 \right] = 1.8975 \times 10^8 \text{ (m/s)}.$

c) At  $x=0$ ,  $\bar{E} = \bar{a}_y e^{j\pi/3}$

$\bar{H} = \frac{1}{\eta_c} \bar{a}_x \times \bar{E} = \bar{a}_x 0.210 e^{j(\frac{\pi}{3} - 0.0016\pi)}$

$\bar{H}(x,t) = \bar{a}_x 0.210 e^{-0.497x} \sin(6\pi 10^9 t - 31.6\pi x + 0.332\pi) \text{ (A/m)}.$



P.8-12  $\sigma/\omega\epsilon = 4/10^{10}\pi \times 80 \times (\frac{1}{36} \times 10^{-9}) = 0.18$ .

a)  $\alpha = \omega\sqrt{\frac{\mu\epsilon}{2}} \left[ \sqrt{1 + \left(\frac{\sigma}{\omega\epsilon}\right)^2} - 1 \right]^{1/2} = 84 \text{ (Np/m)},$

$\beta = \omega\sqrt{\frac{\mu\epsilon}{2}} \left[ \sqrt{1 + \left(\frac{\sigma}{\omega\epsilon}\right)^2} + 1 \right]^{1/2} = 300\pi \text{ (rad/m)},$

$\eta_c = \sqrt{\frac{\mu}{\epsilon_c}} = \frac{120\pi}{\sqrt{\epsilon_r} \left[ 1 + (\sigma/\omega\epsilon)^2 \right]^{1/4}} e^{\frac{j}{2} \tan^{-1}(\sigma/\omega\epsilon)} = 41.8 e^{j0.0283\pi} \text{ } (\Omega),$

$u_p = \omega/\beta = 33.3 \times 10^6 \text{ (m/s)}, \lambda = 2\pi/\beta = 0.67 \text{ (cm)}, \delta = \frac{1}{\alpha} = 1.19 \text{ (cm)}.$

b)  $e^{-\alpha y} = \frac{1}{10}, \quad y = \frac{1}{\alpha} \ln 10 = 2.74 \text{ (cm)}.$

c)  $\bar{H}(y, t) = \bar{a}_x 0.1 e^{-84 \times 0.5} \sin(10^{10}\pi t - 300\pi \times 0.5 - \pi/3)$

$= \bar{a}_x 5.75 \times 10^{-20} \sin(10^{10}\pi t - \pi/3) \text{ (A/m)},$

$\bar{E}(y, t) = \Im_m [\eta_c \bar{H}(y) \times \bar{a}_y] e^{j\omega t} = \bar{a}_z 2.41 \times 10^{-18} \sin(10^{10}\pi t - \frac{\pi}{3} + 0.0283\pi) \text{ (V/m)}.$

P.8-16  $\mathcal{P}_{av} = |\bar{E}|^2 / 2\eta_0 = 10^{-2} \text{ (W/cm}^2\text{)}.$

a)  $|\bar{E}| = \sqrt{0.02}\eta_0 = 2.75 \text{ (V/cm)} = 275 \text{ (V/m)},$

$|\bar{H}| = |\bar{E}|/\eta_0 = 7.25 \times 10^{-3} \text{ (A/cm)} = 0.725 \text{ (A/m)}.$

b)  $\mathcal{P}_{av} = |\bar{E}|^2 / 2\eta_0 = 1300 \text{ (W/m}^2\text{)}.$

$|\bar{E}| = 990 \text{ (V/m)}, \quad |\bar{H}| = 2.63 \text{ (A/m)}.$

P.8-17 Assume circularly polarized plane wave:

$\bar{E}(z, t) = \bar{a}_x E_0 \cos(\omega t - kz + \phi) + \bar{a}_y E_0 \sin(\omega t - kz + \phi),$

$\bar{H}(z, t) = \bar{a}_y \frac{E_0}{\eta} \cos(\omega t - kz + \phi) - \bar{a}_x \frac{E_0}{\eta} \sin(\omega t - kz + \phi).$

Poynting vector,  $\bar{\mathcal{P}} = \bar{E} \times \bar{H} = \bar{a}_z \frac{E_0^2}{\eta} [\cos^2(\omega t - kz + \phi) + \sin^2(\omega t - kz + \phi)]$   
 $= \bar{a}_z \frac{E_0^2}{\eta}, \text{ a constant independent of } t \text{ and } z.$

P.8-18  $\bar{E} = \bar{a}_\theta E_\theta + \bar{a}_\phi E_\phi,$

$\bar{H} = \frac{1}{\eta} \bar{a}_r \times \bar{E} = \frac{1}{\eta} (\bar{a}_\phi E_\theta - \bar{a}_\theta E_\phi).$

$\bar{\mathcal{P}}_{av} = \frac{1}{2} \Re_e (\bar{E} \times \bar{H}^*) = \bar{a}_z \frac{1}{2\eta} (|E_\theta|^2 + |E_\phi|^2).$



P.8-21 Given  $\vec{E}_i = E_0 (\bar{a}_x - j\bar{a}_y) e^{-j\beta z}$

a) Assume reflected  $\vec{E}_r(z) = (\bar{a}_x E_{rx} + \bar{a}_y E_{ry}) e^{j\beta z}$

Boundary condition at  $z=0$ :  $\vec{E}_i(0) + \vec{E}_r(0) = 0$ .

→  $\vec{E}_r(z) = E_0 (-\bar{a}_x + j\bar{a}_y) e^{j\beta z}$  a left-hand circularly polarized wave in  $-z$  direction.

b)  $\bar{a}_{n1} \times (\vec{H}_i - \vec{H}_r) = \vec{J}_s \rightarrow -\bar{a}_z \times [\vec{H}_i(0) + \vec{H}_r(0)] = \vec{J}_s$  ( $\vec{H}_2 = 0$  in perfect conductor)

$\vec{H}_i(0) = \frac{1}{\eta_0} \bar{a}_z \times \vec{E}_i(0) = \frac{E_0}{\eta_0} (j\bar{a}_x + \bar{a}_y)$ ,  $\vec{H}_r(0) = \frac{1}{\eta_0} (-\bar{a}_z) \times \vec{E}_r(0) = \frac{E_0}{\eta_0} (j\bar{a}_x + \bar{a}_y)$ .

$\vec{H}_1(0) = \vec{H}_i(0) + \vec{H}_r(0) = \frac{2E_0}{\eta_0} (j\bar{a}_x + \bar{a}_y)$ ,

$\vec{J}_s = -\bar{a}_z \times \vec{H}_1(0) = \frac{2E_0}{\eta_0} (\bar{a}_x - j\bar{a}_y)$ .

c)  $\vec{E}_t(z,t) = \text{Re} [\vec{E}_i(z) + \vec{E}_r(z)] e^{j\omega t}$   
 $= \text{Re} E_0 [(\bar{a}_x - j\bar{a}_y) e^{-j\beta z} + (-\bar{a}_x + j\bar{a}_y) e^{j\beta z}] e^{j\omega t}$   
 $= \text{Re} E_0 [-2j(\bar{a}_x - j\bar{a}_y) \sin \beta z] e^{j\omega t}$   
 $= 2E_0 \sin \beta z (\bar{a}_x \sin \omega t - \bar{a}_y \cos \omega t)$ .

P.8-22 Given  $\vec{E}_i(x,z) = \bar{a}_y 10 e^{-j(6x+8z)}$  (V/m).

a)  $k_x = 6$ ,  $k_z = 8 \rightarrow k = \beta = \sqrt{k_x^2 + k_z^2} = 10$  (rad/m).

$\lambda = 2\pi/k = 2\pi/10 = 0.628$  (m);  $f = c/\lambda = 4.78 \times 10^8$  (Hz);  $\omega = kc = 3 \times 10^9$  (rad/s)

b)  $\vec{E}_i(x,z;t) = \bar{a}_y 10 \cos(3 \times 10^9 t - 6x - 8z)$  (V/m).

$\vec{H}_i(x,z) = \frac{1}{\eta_0} \bar{a}_{ni} \times \vec{E}_i$  ( $\bar{a}_{ni} = \frac{k}{k} = \bar{a}_x 0.6 + \bar{a}_z 0.8$ )  
 $= \frac{1}{j20\pi} (\bar{a}_x 0.6 + \bar{a}_z 0.8) \times \bar{a}_y 10 e^{-j(6x+8z)} = (-\bar{a}_x \frac{1}{15\pi} + \bar{a}_z \frac{1}{20\pi}) e^{-j(6x+8z)}$   
 $\vec{H}_i(x,z;t) = (-\bar{a}_x \frac{1}{15\pi} + \bar{a}_z \frac{1}{20\pi}) \cos(3 \times 10^9 t - 6x - 8z)$  (A/m).

c)  $\cos \theta_i = \bar{a}_{ni} \cdot \bar{a}_z = \left(\frac{k}{k}\right) \cdot \bar{a}_z = 0.8 \rightarrow \theta_i = \cos^{-1} 0.8 = 36.9^\circ$

d)  $\vec{E}_i(x,0) + \vec{E}_r(x,0) = 0 \rightarrow \vec{E}_r(x,z) = -\bar{a}_y 10 e^{-j(6x-8z)}$

$\vec{H}_r(x,z) = \frac{1}{\eta_0} \bar{a}_{nr} \times \vec{E}_r(x,z)$  ( $\bar{a}_{nr} = \bar{a}_x 0.6 - \bar{a}_z 0.8$ )  
 $= -(\bar{a}_x \frac{1}{15\pi} + \bar{a}_z \frac{1}{20\pi}) e^{-j(6x-8z)}$

e)  $\vec{E}_t(x,z) = \vec{E}_i(x,z) + \vec{E}_r(x,z) = \bar{a}_y 10 (e^{-j8z} - e^{j8z}) e^{-j6x}$   
 $= -\bar{a}_y j20 e^{-j6x} \sin 8z$  (V/m).

$\vec{H}_t(x,z) = \vec{H}_i(x,z) + \vec{H}_r(x,z) = -(\bar{a}_x \frac{2}{15\pi} \cos 8z + \bar{a}_z \frac{2}{10\pi} \sin 8z) e^{-j6x}$  (A/m).

P.8-23 Given  $\vec{E}_i(y, z) = 5(\vec{a}_y + \vec{a}_z\sqrt{3})e^{j6(\sqrt{3}y - z)}$  (V/m).

a)  $k_y = -6\sqrt{3}$ ,  $k_z = 6 \rightarrow k = \sqrt{k_y^2 + k_z^2} = 12$  (rad/m).

$\lambda = 2\pi/k = \pi/6 = 0.524$  (m);  $f = c/\lambda = 5.73 \times 10^8$  (Hz);  $\omega = kc = 3.60 \times 10^9$  (rad/s).

b)  $\vec{E}_i(y, z; t) = 5(\vec{a}_y + \vec{a}_z\sqrt{3})\cos(3.60 \times 10^9 t + 6\sqrt{3}y - 6z)$  (V/m).

$\vec{H}_i(y, z) = \frac{1}{\eta_0} \vec{a}_{ni} \times \vec{E}_i = \frac{1}{120\pi} (-\vec{a}_y \frac{\sqrt{3}}{2} + \vec{a}_z \frac{1}{2}) \times 5(\vec{a}_y + \vec{a}_z\sqrt{3})e^{j6(\sqrt{3}y - z)}$   
 $= \vec{a}_x (-\frac{1}{12\pi}) e^{j6(\sqrt{3}y - z)}$

$\vec{H}_i(y, z; t) = \vec{a}_x (-\frac{1}{12\pi}) \cos(3.60 \times 10^9 t + 6\sqrt{3}y - 6z)$  (A/m).

c)  $\cos \theta_i = \vec{a}_{ni} \cdot \vec{a}_z = \frac{1}{2} \rightarrow \theta_i = \cos^{-1}(\frac{1}{2}) = 60^\circ$ .

d) Conditions  $\vec{a}_{nr} \cdot \vec{E}_r(y, z) = 0$  and  $E_{iy}(y, 0) + E_{ry}(y, 0) = 0$  lead to:

$\vec{E}_r(y, z) = 5(-\vec{a}_y + \vec{a}_z\sqrt{3})e^{j6(\sqrt{3}y + z)}$  (V/m).

$\vec{H}_r(y, z) = \frac{1}{\eta_0} \vec{a}_{nr} \times \vec{E}_r(y, z) = \frac{1}{120\pi} (-\vec{a}_y \frac{\sqrt{3}}{2} - \vec{a}_z \frac{1}{2}) \times 5(-\vec{a}_y + \vec{a}_z\sqrt{3})e^{j6(\sqrt{3}y + z)}$   
 $= \vec{a}_x (-\frac{1}{12\pi}) e^{j6(\sqrt{3}y + z)}$  (A/m).

e)  $\vec{E}_t(y, z) = \vec{E}_i(y, z) + \vec{E}_r(y, z) = (-\vec{a}_y j10 \sin 6z + \vec{a}_z 10\sqrt{3} \cos 6z) e^{j6\sqrt{3}y}$  (V/m).

$\vec{H}_t(y, z) = \vec{H}_i(y, z) + \vec{H}_r(y, z) = \vec{a}_x (-\frac{1}{6\pi}) \cos 6z \cdot e^{j6\sqrt{3}y}$  (A/m).

P.8-24 a) From Eqs. (8-113) and (8-114):

$\vec{E}_t(x, z; t) = \vec{a}_y 2E_{i0} \sin(\beta_z z \cos \theta_i) \sin(\omega t - \beta_x x \sin \theta_i)$

$\vec{H}_t(x, z; t) = \frac{2E_{i0}}{\eta_1} \left[ -\vec{a}_x \cos \theta_i \cos(\beta_z z \cos \theta_i) \cos(\omega t - \beta_x x \sin \theta_i) \right.$   
 $\left. + \vec{a}_z \sin \theta_i \sin(\beta_z z \cos \theta_i) \sin(\omega t - \beta_x x \sin \theta_i) \right]$ .

b)  $\vec{P}_{av} = \frac{1}{2} \mathcal{Q}_s(\vec{E} \times \vec{H}^*) = \vec{a}_x \frac{2E_{i0}^2}{\eta_1} \sin \theta_i \sin^2(\beta_z z \cos \theta_i)$ .

P.8-25 a) From Eqs. (8-128) and (8-129):

$\vec{E}_t(x, z; t) = -2E_{i0} \left[ \vec{a}_x \cos \theta_i \sin(\beta_z z \cos \theta_i) \cos(\omega t - \beta_x x \sin \theta_i) \right.$   
 $\left. + \vec{a}_z \sin \theta_i \cos(\beta_z z \cos \theta_i) \sin(\omega t - \beta_x x \sin \theta_i) \right]$ .

$\vec{H}_t(x, z; t) = \vec{a}_y \frac{2E_{i0}}{\eta_1} \cos(\beta_z z \cos \theta_i) \sin(\omega t - \beta_x x \sin \theta_i)$ .

b)  $\vec{P}_{av} = \frac{1}{2} \mathcal{Q}_s(\vec{E} \times \vec{H}^*) = \vec{a}_x \frac{2E_{i0}^2}{\eta_1} \sin \theta_i \cos^2(\beta_z z \cos \theta_i)$ .

P.8-27 a) In the lossy medium (medium 2):

$$\vec{E}_z = \vec{a}_x E_{z0} e^{-\alpha_2 z} e^{-j\beta_2 z},$$

where, from Problem P.8-9,  $\alpha_2 = \omega \sqrt{\frac{\mu \epsilon_2}{2}} \left[ \sqrt{1 + \left( \frac{\sigma_2}{\omega \epsilon_2} \right)^2} - 1 \right]^{\frac{1}{2}}$ ,  $\beta_2 = \omega \sqrt{\frac{\mu \epsilon_2}{2}} \left[ \sqrt{1 + \left( \frac{\sigma_2}{\omega \epsilon_2} \right)^2} + 1 \right]^{\frac{1}{2}}$ .

Given:  $\beta_1 = 6 \text{ (rad/m)} \rightarrow \omega = \beta_1 c = 1.8 \times 10^9 \text{ (rad/s)}$ .

$\tan \delta_c = \frac{\sigma_2}{\omega \epsilon_2} = 0.5 \rightarrow \alpha_2 = 2.30 \text{ (Np/m)}, \beta_2 = 9.76 \text{ (rad/m)}$

$\eta_2 = \sqrt{\frac{\mu_2}{\epsilon_2}} = \frac{120\pi}{\sqrt{\epsilon_{r2}(1 + \tan^2 \delta_c)}} e^{j\frac{1}{2} \tan^{-1}(\sigma_2/\omega \epsilon_2)} = 225 e^{j13.3^\circ}$

$\vec{E}_z = \vec{a}_x E_{z0} e^{-2.30z} e^{-j9.76z}$ ,  $\vec{H}_z = \vec{a}_y \times \frac{\vec{E}_z}{\eta_2} = \vec{a}_y \frac{E_{z0}}{225} e^{-j13.3^\circ} e^{-2.30z} e^{-j9.76z}$

Let  $\vec{E}_r = \vec{a}_x E_{r0} e^{j6z} \rightarrow \vec{H}_r = -\vec{a}_y \frac{E_{r0}}{120\pi} e^{j6z}$ ,  $\vec{H}_i = \vec{a}_y \frac{10}{120\pi} e^{-j6z}$

Boundary conditions for  $\vec{E}$  and  $\vec{H}$  at  $z=0$ :  $\begin{cases} 10 + E_{r0} = E_{z0} \\ 10 - E_{r0} = E_{z0} \sqrt{\epsilon_{r2}} (1 + \tan^2 \delta_c)^{1/4} e^{-j13.3^\circ} \end{cases}$

$\rightarrow E_{r0} = 2.77 e^{j13.3^\circ}; E_{z0} = 7.53 e^{-j17.2^\circ}$

$\therefore \vec{E}_r(z, t) = \vec{a}_x 2.77 \cos(1.8 \times 10^9 t + 6z + 157^\circ) \text{ (V/m)}$

$\vec{H}_r(z, t) = -\vec{a}_y 0.073 \cos(1.8 \times 10^9 t + 6z + 157^\circ) \text{ (A/m)}$

$\vec{E}_z(z, t) = \vec{a}_x 7.53 e^{-2.30z} \cos(1.8 \times 10^9 t - 9.76z - 172^\circ) \text{ (V/m)}$

$\vec{H}_z(z, t) = \vec{a}_y 0.033 e^{-2.30z} \cos(1.8 \times 10^9 t - 9.76z + 174.7^\circ) \text{ (A/m)}$

b)  $(\vec{P}_{av})_1 = \vec{a}_z \left( \frac{10^2}{2 \times 120\pi} - \frac{2.77^2}{2 \times 120\pi} \right) = \vec{a}_z 0.122 \text{ (W/m}^2\text{)}$

$(\vec{P}_{av})_2 = \vec{a}_z \frac{7.53^2}{2 \times 225} (\cos 13.3^\circ) e^{-4.60z} = \vec{a}_z 0.122 e^{-4.60z} \text{ (W/m}^2\text{)}$

P.8-28 a)  $\Gamma = \frac{E_r}{E_i} = \frac{\eta_2 - \eta_0}{\eta_2 + \eta_0}$ ;  $\eta_0 = \sqrt{\frac{\mu_0}{\epsilon_0}} = 120\pi$ ,  $\eta_2 = \sqrt{j\omega\mu/\sigma}$ .  
 $|\eta_2| \ll \eta_0$ .

b)  $|\Gamma|^2 = \left| \frac{\eta_2 - \eta_0}{\eta_2 + \eta_0} \right|^2 = \left| \frac{1 - \eta_0/\eta_2}{1 + \eta_0/\eta_2} \right|^2 \approx \left| 1 - 2\eta_0/\eta_2 \right|^2$   
 $= (1 - 2\eta_0/\eta_2)(1 - 2\eta_0^*/\eta_2^*) \approx 1 - 4\Re(\eta_0/\eta_2)$

Fraction of power absorbed,  $F = 1 - |\Gamma|^2 = \frac{4}{\eta_0} \Re \sqrt{\frac{j\omega\mu}{\sigma}}$   
 $= \frac{4}{\eta_0} \sqrt{\frac{\omega\mu}{2\sigma}}$

c)  $\omega = 2\pi \times 10^6 \text{ (Hz)}$ . For iron:  $\mu = 4000 \times (4\pi \times 10^{-7}) \text{ (H/m)}$ ,  
 $\sigma = 10^7 \text{ (S/m)}$ .

$F = 4.21 \times 10^{-4}$ , or 0.0421%.



P. 8-32

$$\bar{E}_1 = \bar{a}_x (E_{i0} e^{-j\beta_1 z} + E_{r0} e^{j\beta_1 z}),$$

$$\bar{H}_1 = \bar{a}_y \frac{1}{\eta_1} (E_{i0} e^{-j\beta_1 z} - E_{r0} e^{j\beta_1 z}),$$

$$\bar{E}_2 = \bar{a}_x (E_2^+ e^{-j\beta_2 z} + E_2^- e^{j\beta_2 z}),$$

$$\bar{H}_2 = \bar{a}_y \frac{1}{\eta_2} (E_2^+ e^{-j\beta_2 z} - E_2^- e^{j\beta_2 z}).$$

$$\text{At } z = d, \bar{E}_2 = 0 \longrightarrow E_2^- = -E_2^+ e^{-j2\beta_2 d}.$$

$$\bar{E}_1 = \bar{a}_x E_2^+ [e^{-j\beta_1 z} - e^{j\beta_1(z-2d)}],$$

$$\bar{H}_1 = \bar{a}_y \frac{E_2^+}{\eta_1} [e^{-j\beta_1 z} + e^{j\beta_1(z-2d)}].$$

$$\text{Boundary conditions: } E_1(0) = E_2(0) \longrightarrow E_{i0} + E_{r0} = E_2^+ (1 - e^{-j2\beta_2 d}),$$

$$\text{at } z=0: H_1(0) = H_2(0) \longrightarrow E_{i0} - E_{r0} = E_2^+ \frac{\eta_1}{\eta_2} (1 + e^{-j2\beta_2 d}).$$

$$E_2^+ = \frac{2\eta_2 E_{i0}}{(\eta_0 + \eta_2) + (\eta_0 - \eta_2) e^{-j2\beta_2 d}}.$$

$$E_{r0} = - \left( \frac{\eta_0 - j\eta_2 \tan \beta_2 d}{\eta_0 + j\eta_2 \tan \beta_2 d} \right) E_{i0}.$$

$$a) \bar{E}_1(z, t) = \bar{a}_x E_{i0} \cos \left[ \omega \left( t - \frac{z}{u_p} \right) + \theta \right], \quad \theta = \pi - 2 \tan^{-1} \left( \frac{\eta_2}{\eta_0} \tan \beta_2 d \right).$$

$$b) \bar{E}_1(z, t) = \bar{a}_x E_{i0} \left\{ \cos \omega \left( t - \frac{z}{u_p} \right) + \cos \left[ \omega \left( t - \frac{z}{u_p} \right) + \theta \right] \right\}.$$

$$c) \bar{E}_2(z, t) = \bar{a}_x \frac{2\eta_2 E_{i0}}{\sqrt{2[(\eta_0^2 + \eta_2^2) + (\eta_0^2 - \eta_2^2) \cos 2\beta_2 d]}} \left\{ \cos \left[ \omega \left( t - \frac{z}{u_p} \right) + \psi \right] - \cos \left[ \omega \left( t + \frac{z}{u_{p2}} \right) - \frac{2\omega d}{u_{p2}} + \psi \right] \right\},$$

$$\psi = \tan^{-1} \left[ \frac{(\eta_0 - \eta_2) \sin 2\beta_2 d}{(\eta_0 + \eta_2) + (\eta_0 - \eta_2) \cos 2\beta_2 d} \right].$$

$$d) (\bar{P}_{av})_1 = \frac{1}{2} \operatorname{Re} (\bar{E}_1 \times \bar{H}_1^*) = 0.$$

$$e) (\bar{P}_{av})_2 = 0.$$

$$f) \text{ Let } E_r = -E_{i0} \longrightarrow \tan \beta_2 d = 0 \longrightarrow d = n\lambda_2/2, \quad n = 0, 1, 2, \dots$$

P.8-34 Given  $f = f_p/2$  and  $\theta_i = 60^\circ$ .

$$\rightarrow \eta_p = \eta_0 / \sqrt{1 - (f_p/f)^2} = -j\eta_0/\sqrt{3}, \quad \eta_p/\eta_0 = -j/\sqrt{3}.$$

From Eq. (8-185):  $\sin \theta_t = \frac{\eta_p}{\eta_0} \sin \theta_i = -j/2$ ,  $\cos \theta_t = \sqrt{5}/2$ ,  $\cos \theta_i = 1/2$ .

a) From Eq. (8-206):  $\Gamma_{\perp} = \frac{(\eta_p/\eta_0) \cos \theta_i - \cos \theta_t}{(\eta_p/\eta_0) \cos \theta_i + \cos \theta_t} = e^{j209^\circ}$

From Eq. (8-207):  $\tau_{\perp} = \frac{2(\eta_p/\eta_0) \cos \theta_i}{(\eta_p/\eta_0) \cos \theta_i + \cos \theta_t} = 0.5 e^{-j75.5^\circ}$

b) From Eq. (8-221):  $\Gamma_{\parallel} = \frac{(\eta_p/\eta_0) \cos \theta_t - \cos \theta_i}{(\eta_p/\eta_0) \cos \theta_t + \cos \theta_i} = e^{j76^\circ}$

From Eq. (8-222):  $\tau_{\parallel} = \frac{2(\eta_p/\eta_0) \cos \theta_i}{(\eta_p/\eta_0) \cos \theta_t + \cos \theta_i} = 0.177 e^{-j33^\circ}$

$|\Gamma_{\perp}| = |\Gamma_{\parallel}| = 1$ , but the phase shift of the reflected wave depends on the polarization of the incident wave. There are standing waves in the air and exponentially decaying transmitted waves in the ionosphere.

P.8-35  $k_{zx}^2 + k_{zy}^2 = k_z^2 = \omega^2 \mu_0 \epsilon_2 - j\omega \mu_0 \sigma_2$ . ①

Continuity conditions at  $z=0$  for all  $x$  and  $y$  require:

$$k_{zx} = k_{1x} = \omega \sqrt{\mu_0 \epsilon_0} \sin \theta_i = \beta_x = 2.09 \times 10^{-4} \quad ②$$

$$k_{zy} = \beta_{zy} - j\alpha_{zy} \quad ③$$

Combining ①, ② and ③, we can solve for  $\alpha_{zx}$  and  $\beta_{zx}$  in terms of  $\omega$ ,  $\mu_0$ ,  $\epsilon_2$ ,  $\sigma_2$ , and  $\beta_x$ . But, since

$$\beta_x^2 \ll \omega^2 \mu_0 \epsilon_2,$$

we have  $\alpha_z = \alpha_{zx} \approx \beta_{zx} \approx \frac{1}{\delta} = \sqrt{\pi f \mu_0 \sigma_2} = 0.3974 \text{ (m}^{-1}\text{)}.$

a)  $\theta_t = \tan^{-1} \frac{\beta_x}{\beta_{zx}} \approx \tan^{-1} \frac{2.09}{0.3974} \times 10^{-4} \approx 5.26 \times 10^{-4} \text{ (rad)}$   
 $= 0.03^\circ$

b)  $\Gamma_{\perp} = \frac{2\eta_1 \cos \theta_i}{\eta_2 \cos \theta_t + \eta_0 \cos \theta_i}$   $\eta_2 = \frac{\alpha_2}{\sigma_2} (1+j) = 0.0993 (1+j).$   
 $= \frac{2 \times 0.0993 (1+j)}{0.0993 (1+j) + 377 \cos 33^\circ}$   $\cos \theta_t = \cos 0.03^\circ \approx 1.$   
 $\approx 0.0151 (1+j) = 0.0214 e^{j\pi/4}$

c)  $(\mathcal{P}_{av})_i = \frac{E_{i0}^2}{2\eta_0}$

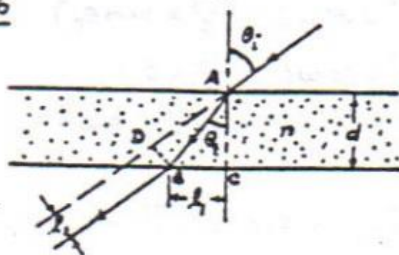
$$E_{t0} \approx 2E_{i0} \frac{\eta_1}{\eta_0}, \quad H_{t0} \approx \frac{2E_{i0}}{\eta_0} \rightarrow (\mathcal{P}_{av})_t = 2 \frac{E_{i0}^2 \alpha_2}{\eta_0^2 \sigma_2} e^{-2\alpha_2 z}$$

$$\therefore \frac{(\mathcal{P}_{av})_t}{(\mathcal{P}_{av})_i} = \frac{4\alpha_2}{\eta_0 \sigma_2} e^{-2\alpha_2 z} = 1.054 \times 10^{-3} e^{-0.795z}$$

d)  $20 \log_{10} e^{-\alpha_2 z} = -30 \rightarrow z = \frac{1.5}{\alpha_2 \log_{10} e} = 8.69 \text{ (m)}.$



P. 8-36



a) Snell's law:

$$\frac{\sin \theta_t}{\sin \theta_i} = \frac{1}{n},$$

$$\theta_t = \sin^{-1}\left(\frac{1}{n} \sin \theta_i\right).$$

b)  $\cos \theta_t = \sqrt{1 - \left(\frac{1}{n} \sin \theta_i\right)^2}.$

$$l_1 = \overline{BC} = \overline{AC} \tan \theta_t = d \frac{\sin \theta_t}{\cos \theta_t} = \frac{d \sin \theta_t}{\sqrt{n^2 - \sin^2 \theta_i}}.$$

c)  $l_2 = \overline{BD} = \overline{AC} \sin(\theta_i - \theta_t) = \frac{d}{\cos \theta_t} (\sin \theta_i \cos \theta_t - \cos \theta_i \sin \theta_t)$   
 $= d \sin \theta_i \left[1 - \frac{\cos \theta_i}{\sqrt{n^2 - \sin^2 \theta_i}}\right].$

P. 8-37

a)  $\sin \theta_c = \sqrt{\frac{\epsilon_1}{\epsilon_2}} \rightarrow \sin \theta_t = \sqrt{\frac{\epsilon_1}{\epsilon_2}} \sin \theta_i > 1$  for  $\theta_i > \theta_c$ ,  
 $\cos \theta_t = -j \sqrt{\left(\frac{\epsilon_1}{\epsilon_2}\right) \sin^2 \theta_i - 1}.$

From Eqs. (8-200) and (8-201):

$$\bar{E}_t(x, z) = \bar{a}_y E_{t0} e^{-\alpha_2 z} e^{-j\beta_{2x} x},$$

$$\bar{H}_t(x, z) = \frac{E_{t0}}{\eta_2} (\bar{a}_x j \alpha_2 + \bar{a}_z \sqrt{\frac{\epsilon_1}{\epsilon_2}} \sin \theta_i) e^{-\alpha_2 z} e^{-j\beta_{2x} x},$$

where  $\beta_{2x} = \beta_2 \sin \theta_t = \beta_2 \sqrt{\frac{\epsilon_1}{\epsilon_2}} \sin \theta_i,$

$$\alpha_2 = \beta_2 \sqrt{\left(\frac{\epsilon_1}{\epsilon_2}\right) \sin^2 \theta_i - 1},$$

$$E_{t0} = \frac{2 \eta_1 \cos \theta_i E_{i0}}{\eta_2 \cos \theta_i - j \eta_1 \sqrt{\left(\frac{\epsilon_1}{\epsilon_2}\right) \sin^2 \theta_i - 1}} \quad \text{from Eq. (8-207).}$$

b)  $(\Phi_{av})_{zz} = \frac{1}{2} \operatorname{Re} (E_{ty} H_{tx}^*) = 0.$

P. 8-38 Given  $\theta_i = \theta_c \rightarrow \theta_t = \pi/2, \cos \theta_t = 0.$

a) From Eq. (8-207):  $(E_{t0}/E_{i0})_{\perp} = 2.$

b) From Eq. (8-221):  $(E_{t0}/E_{i0})_{\parallel} = 2 \eta_2 / \eta_1.$

c)  $\bar{E}_t(x, z; t) = \bar{a}_y E_{i0} \cos \omega \left[t - \frac{n_1}{c} (x \sin \theta_i + z \cos \theta_i)\right],$

$$\bar{E}_t(x, z; t) = \bar{a}_y 2 E_{i0} e^{-\alpha z} \cos \omega \left(t - \frac{n_2}{c} x \sin \theta_t\right)$$

$$= \bar{a}_y 2 E_{i0} e^{-\alpha z} \cos \omega \left(t - \frac{n_1}{c} x \sin \theta_i\right),$$

where  $\alpha = \frac{n_2 \omega}{c} \sqrt{\left(\frac{n_1}{n_2} \sin \theta_i\right)^2 - 1} = 0$  when  $\theta = \theta_c.$

P.8-39. a)  $\theta_c = \sin^{-1} \sqrt{\epsilon_{r2}/\epsilon_{r1}} = \sin^{-1} \sqrt{1/91} = 6.38^\circ$ .

b)  $\theta_i = 20^\circ > \theta_c$ .  $\sin \theta_t = \sqrt{\frac{\epsilon_1}{\epsilon_2}} \sin \theta_i = 3.0x$ ,  $\cos \theta_t = -j2.91$ .

$$\Gamma_{\perp} = \frac{\sqrt{\epsilon_{r1}} \cos \theta_i - \cos \theta_t}{\sqrt{\epsilon_{r1}} \cos \theta_i + \cos \theta_t} = e^{j18^\circ} = e^{j0.66}$$

c)  $\tau_{\perp} = \frac{2\sqrt{\epsilon_{r1}} \cos \theta_i}{\sqrt{\epsilon_{r1}} \cos \theta_i + \cos \theta_t} = 1.89 e^{j79^\circ} = 1.89 e^{j1.33}$

d) The transmitted wave in air varies as  $e^{-\alpha_2 z} e^{-j\beta_2 x}$ .

Where  $\alpha_2 = \beta_2 \sqrt{\left(\frac{\epsilon_1}{\epsilon_2}\right) \sin^2 \theta_i - 1} = \frac{2\pi}{\lambda_0} (2.91)$ .

Attenuation in air for each wavelength

$$= 20 \log_{10} e^{-\alpha_2 \lambda_0} = 159 \text{ (dB)}.$$

P.8-40 When the incident light first strikes the hypotenuse surface,  $\theta_i = \theta_t = 0$ ,  $\tau_1 = \frac{2\eta_2}{\eta_1 + \eta_0}$ .

$$\frac{(\rho_{av})_{t1}}{(\rho_{av})_i} = \frac{\eta_0}{\eta_2} \tau_1^2 = \frac{4\eta_0\eta_2}{(\eta_2 + \eta_0)^2}.$$

Total reflections occur inside the prism at both slanting surfaces because

$$\theta_i = 45^\circ > \theta_c = \sin^{-1}\left(\frac{1}{2}\right) = 30^\circ.$$

On exit from the prism,  $\tau_2 = \frac{2\eta_0}{\eta_2 + \eta_0}$ .

$$\frac{(\rho_{av})_o}{(\rho_{av})_{t1}} = \frac{\eta_2}{\eta_0} \tau_2^2 = \frac{4\eta_0\eta_2}{(\eta_2 + \eta_0)^2}.$$

$$\therefore \frac{(\rho_{av})_o}{(\rho_{av})_i} = \left[ \frac{4\eta_0\eta_2}{(\eta_2 + \eta_0)^2} \right]^2 = \left[ \frac{4\sqrt{\epsilon_r}}{(1 + \sqrt{\epsilon_r})^2} \right]^2 = 0.79.$$

P.8-41 a)  $n_0 \sin \theta_a = n_1 \sin(90^\circ - \theta_c) = n_1 \cos \theta_c$

$$= n_1 \sqrt{1 - \sin^2 \theta_c} = n_1 \sqrt{1 - (n_2/n_1)^2} = \sqrt{n_1^2 - n_2^2}.$$

$$\sin \theta_a = \frac{1}{n_0} \sqrt{n_1^2 - n_2^2} = \sqrt{n_1^2 - n_2^2}. \quad (n_0 = 1)$$

b) N.A. =  $\sin \theta_a = \sqrt{2^2 - 1.74^2} = 0.9861$ ,

$$\theta_a = \sin^{-1} 0.9861 = 80.4^\circ.$$

P.8-42 Eq. (8-185):  $\frac{\eta_2}{\eta_1} = \frac{\sin \theta_2}{\sin \theta_1}$ .

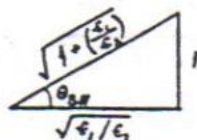
a) Eq. (8-206):  $\Gamma_{\perp} = \frac{(\eta_2/\eta_1) \cos \theta_1 - \cos \theta_2}{(\eta_2/\eta_1) \cos \theta_1 + \cos \theta_2} = \frac{\sin \theta_2 \cos \theta_1 - \cos \theta_2 \sin \theta_1}{\sin \theta_2 \cos \theta_1 + \cos \theta_2 \sin \theta_1}$   
 $= \frac{\sin(\theta_2 - \theta_1)}{\sin(\theta_2 + \theta_1)}$ .

Eq. (8-207):  $\tau_{\perp} = \frac{2(\eta_2/\eta_1) \cos \theta_1}{(\eta_2/\eta_1) \cos \theta_1 + \cos \theta_2} = \frac{2 \sin \theta_2 \cos \theta_1}{\sin(\theta_2 + \theta_1)}$ .

b) Eq. (8-221):  $\Gamma_{\parallel} = \frac{(\eta_2/\eta_1) \cos \theta_1 - \cos \theta_2}{(\eta_2/\eta_1) \cos \theta_1 + \cos \theta_2} = \frac{\sin \theta_2 \cos \theta_1 - \sin \theta_1 \cos \theta_2}{\sin \theta_2 \cos \theta_1 + \sin \theta_1 \cos \theta_2}$   
 $= \frac{\sin 2\theta_1 - \sin 2\theta_2}{\sin 2\theta_1 + \sin 2\theta_2}$ .

Eq. (8-222):  $\tau_{\parallel} = \frac{2(\eta_2/\eta_1) \cos \theta_1}{(\eta_2/\eta_1) \cos \theta_1 + \cos \theta_2} = \frac{4 \sin \theta_2 \cos \theta_1}{\sin 2\theta_1 + \sin 2\theta_2}$ .

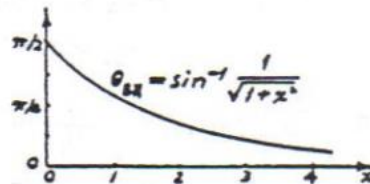
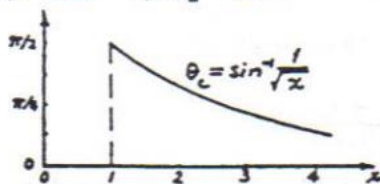
P.8-44 a)  $\sin \theta_c = \sqrt{\frac{\epsilon_1}{\epsilon_2}}$ ;  $\sin \theta_{\text{eff}} = \frac{1}{\sqrt{1 + (\frac{\epsilon_1}{\epsilon_2})}}$



$\rightarrow \tan \theta_{\text{eff}} = \sqrt{\frac{\epsilon_1}{\epsilon_2}}$ .

$\therefore \sin \theta_c = \tan \theta_{\text{eff}} \cdot (\theta_c > \theta_{\text{eff}})$

b) Let  $\epsilon_1/\epsilon_2 = x$ .



P.8-45 a) For perpendicular polarization:

$$\Gamma_{\perp} = \frac{\sqrt{\epsilon_n} \cos \theta_i - \sqrt{\epsilon_{r2}} \cos \theta_t}{\sqrt{\epsilon_{r2}} \cos \theta_i + \sqrt{\epsilon_n} \cos \theta_t}$$

$$\sin \theta_t = \sqrt{\frac{\epsilon_n}{\epsilon_{r2}}} \sin \theta_i, \quad \cos \theta_t = \sqrt{1 - \left(\frac{\epsilon_n}{\epsilon_{r2}}\right) \sin^2 \theta_i}$$

$$\Gamma_{\perp} = \frac{\sqrt{\frac{\epsilon_n}{\epsilon_{r2}}} \cos \theta_i - \sqrt{1 - \frac{\epsilon_n}{\epsilon_{r2}} \sin^2 \theta_i}}{\sqrt{\frac{\epsilon_{r2}}{\epsilon_n}} \cos \theta_i + \sqrt{1 - \frac{\epsilon_{r2}}{\epsilon_n} \sin^2 \theta_i}}$$

$$\tau_{\perp} = \frac{2 \eta_2 \cos \theta_i}{\eta_2 \cos \theta_i + \eta_1 \cos \theta_t} = \frac{2 \sqrt{\frac{\epsilon_{r2}}{\epsilon_n}} \cos \theta_i}{\sqrt{\frac{\epsilon_{r2}}{\epsilon_n}} \cos \theta_i + \sqrt{1 - \frac{\epsilon_{r2}}{\epsilon_n} \sin^2 \theta_i}}$$

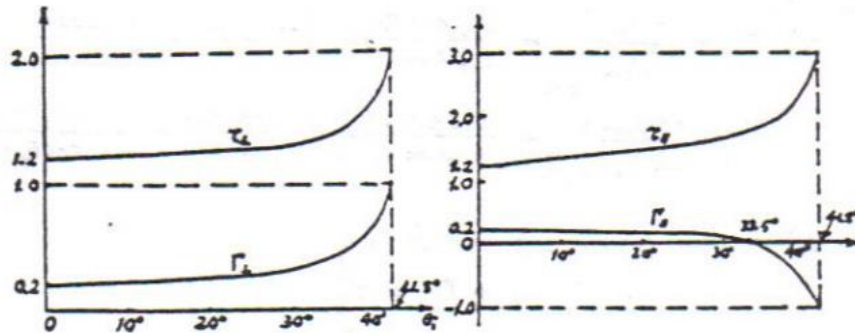


For parallel polarization:

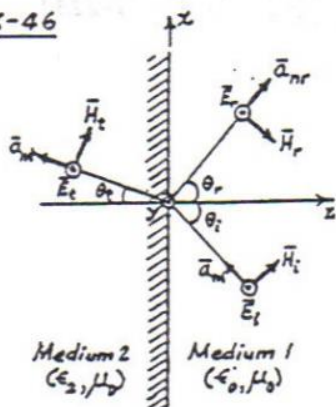
$$\Gamma_{\parallel} = \frac{\sqrt{\frac{\epsilon_2}{\epsilon_1}} \sqrt{1 - \left(\frac{\epsilon_2}{\epsilon_1}\right) \sin^2 \theta_i} - \cos \theta_i}{\sqrt{\frac{\epsilon_2}{\epsilon_1}} \sqrt{1 - \left(\frac{\epsilon_2}{\epsilon_1}\right) \sin^2 \theta_i} + \cos \theta_i}$$

$$\tau_{\parallel} = \frac{2 \sqrt{\frac{\epsilon_2}{\epsilon_1}} \cos \theta_i}{\sqrt{\frac{\epsilon_2}{\epsilon_1}} \sqrt{1 - \left(\frac{\epsilon_2}{\epsilon_1}\right) \sin^2 \theta_i} + \cos \theta_i}$$

b)  $\epsilon_{r1}/\epsilon_{r2} = 2.25$ ,  $\sqrt{\epsilon_{r1}/\epsilon_{r2}} = 1.5 \rightarrow \theta_c = \sin^{-1} \sqrt{\frac{\epsilon_1}{\epsilon_2}} = 41.8^\circ$



P. 8-46



Given:  $\vec{E}_i(x, z) = \vec{a}_y E_{i0} e^{-jk_2(x \sin \theta_i - z \cos \theta_i)}$

$$\vec{a}_{ni} = \vec{a}_x \sin \theta_i - \vec{a}_z \cos \theta_i$$

$$\vec{H}_i(x, z) = \frac{1}{\eta_0} \vec{a}_{ni} \times \vec{E}_i(x, z)$$

$$= \frac{1}{\eta_0} (\vec{a}_x \cos \theta_i + \vec{a}_z \sin \theta_i) e^{-jk_2(x \sin \theta_i - z \cos \theta_i)}$$

$$\epsilon_2 = \epsilon' - j\epsilon'', \quad k_2 = \omega \sqrt{\mu_0 \epsilon_2} = \omega \sqrt{\mu_0 \epsilon_0 \left( \frac{\epsilon'}{\epsilon_0} - j \frac{\epsilon''}{\epsilon_0} \right)}$$

$$= k_0 \sqrt{\epsilon' - j\epsilon''}$$

a) From Eq. (8-207):

$$\tau_{\perp} = \frac{2(\eta_2/\eta_0) \cos \theta_i}{(\eta_2/\eta_0) \cos \theta_i + \cos \theta_t}$$

where  $(\eta_2/\eta_0) = \sqrt{\epsilon_0/\epsilon_2} = 1/\sqrt{\epsilon' - j\epsilon''}$

$$\vec{E}_t(x, z) = \vec{a}_y \tau_{\perp} E_{i0} e^{-jk_2(x \sin \theta_i - z \cos \theta_i)}$$

$$\vec{H}_t(x, z) = \frac{1}{\eta_2} \vec{a}_{nt} \times \vec{E}_t(x, z) = \frac{1}{\eta_2} (\vec{a}_x \cos \theta_t + \vec{a}_z \sin \theta_t) \tau_{\perp} \vec{E}_t(x, z)$$

b) From Eq. (8-185):  $\sin \theta_t = \frac{\sin \theta_i}{\sqrt{\epsilon' - j\epsilon''}}$  (complex).

$$\cos \theta_t = \sqrt{1 - \sin^2 \theta_t} \quad (\text{complex}).$$

The  $x$ - and  $z$ -components of  $\vec{H}_t(x, z)$  in part a) have different amplitudes and are out of phase, indicating that it is elliptically polarized.

P.9-2 a)  $\nabla \times (\bar{a}_x E_x + \bar{a}_y E_y) = -j\omega\mu(\bar{a}_x H_x + \bar{a}_y H_y).$

$$\longrightarrow \begin{cases} \beta E_y = -\omega\mu H_x, & \textcircled{1} \\ \beta E_x = \omega\mu H_y, & \textcircled{2} \\ \frac{\partial E_x}{\partial x} = \frac{\partial E_y}{\partial y} & \textcircled{3} \end{cases}$$

$$\nabla \times (\bar{a}_x H_x + \bar{a}_y H_y) = j\omega\epsilon(\bar{a}_x E_x + \bar{a}_y E_y).$$

$$\longrightarrow \begin{cases} \beta H_y = \omega\epsilon E_x, & \textcircled{4} \\ \beta H_x = -\omega\epsilon E_y, & \textcircled{5} \\ \frac{\partial H_y}{\partial x} = \frac{\partial H_x}{\partial y} & \textcircled{6} \end{cases}$$

From ① and ④:  $\beta = \omega\sqrt{\mu\epsilon}$ . ⑦

From ② or ⑤:  $\frac{E_x}{H_y} = \sqrt{\frac{\mu}{\epsilon}} = \eta$ . ⑧

From ① or ④:  $\frac{E_y}{H_x} = -\sqrt{\frac{\mu}{\epsilon}} = -\eta$ . ⑨

b) From ①:  $\frac{\partial^2 E_y}{\partial y \partial x} = \frac{\partial^2 E_y}{\partial y^2}$ . ⑩

From ④, ⑤, and ⑥:  $\frac{\partial E_x}{\partial x} = -\frac{\partial E_y}{\partial y} \longrightarrow \frac{\partial^2 E_x}{\partial x^2} = -\frac{\partial^2 E_y}{\partial x \partial y}$ . ⑪

Combining ⑩ and ⑪, we have  $\frac{\partial^2 E_x}{\partial x^2} + \frac{\partial^2 E_y}{\partial y^2} = 0$ .

Similarly,  $\frac{\partial^2 H_x}{\partial x^2} + \frac{\partial^2 H_y}{\partial y^2} = 0$ .

P.9-4 Given:  $\sigma_c = 1.6 \times 10^7$  (S/m),  $w = 0.02$  (m),  $d = 2.5 \times 10^{-3}$  (m).  
Lossy dielectric slab:  $\mu = \mu_0$ ,  $\epsilon_r = 3$ ,  $\sigma = 10^{-3}$  (S/m).  
 $f = 5 \times 10^8$  (Hz).

a)  $R = \frac{2}{w} \sqrt{\frac{\pi f \mu_0}{\sigma_c}} = 1.11$  ( $\Omega$ /m)

$L = \mu \frac{d}{w} = 0.157$  ( $\mu$ H/m)

$G = \sigma \frac{w}{d} = 0.008$  (S/m)

$C = \epsilon \frac{w}{d} = 0.212$  (nF/m).

b)  $\frac{|E_x|}{|E_y|} = \sqrt{\frac{\omega\epsilon}{\sigma_c}} = 4.167 \times 10^{-5}$ .

c)  $\omega L = 493.5 \gg R$ ,  $\omega C = 0.667 \gg G$

$\gamma \approx j\omega\sqrt{LC} \left[ 1 + \frac{1}{2j} \left( \frac{R}{\omega L} + \frac{G}{\omega C} \right) \right] = 0.129 + j18.14$  ( $m^{-1}$ )

$Z_0 \approx \sqrt{\frac{L}{C}} \left[ 1 + \frac{1}{2j} \left( \frac{R}{\omega L} - \frac{G}{\omega C} \right) \right] = 27.21 + j0.13$  ( $\Omega$ ).



P.9-17 a) From Eq. (9-117):  $Z_{is} = Z_0 \tanh \gamma l = Z_0 \frac{1 - e^{-2\gamma l}}{1 + e^{-2\gamma l}}$ .

For  $l = \lambda/4$ ,  $\beta l = \pi/2$ ,  $\alpha\lambda/2 \ll 1$ .

$$Z_{is} = Z_0 \frac{1 - e^{-2\alpha(\lambda/4)} e^{-j\pi}}{1 + e^{-2\alpha(\lambda/4)} e^{-j\pi}} \approx Z_0 \frac{1 + (1 - \alpha\lambda/2)}{1 - (1 - \alpha\lambda/2)} \\ \approx 4Z_0/\alpha\lambda.$$

b) From Eq. (9-116):  $Z_{io} = Z_0 \coth \gamma l = Z_0 \frac{1 + e^{-2\gamma l}}{1 - e^{-2\gamma l}}$ .

For  $l = \lambda/4$ ,  $Z_{io} = Z_0 \frac{1 + e^{-2\alpha(\lambda/4)} e^{-j\pi}}{1 - e^{-2\alpha(\lambda/4)} e^{-j\pi}} \approx Z_0 \frac{1 - (1 - \alpha\lambda/2)}{1 + (1 - \alpha\lambda/2)} \\ \approx Z_0 \alpha\lambda/4.$

P.9-18  $\beta l = \frac{2\pi f}{c} l = \frac{8\pi}{3} = 480^\circ$ .

$\tan \beta l = \tan 480^\circ = -1.732$ .

$$Z_i = Z_0 \frac{Z_L + jZ_0 \tan \beta l}{Z_0 + jZ_L \tan \beta l} = 50 \frac{(40 + j30) + j50(-1.732)}{50 + j(40 + j30)(-1.732)} \\ = 26.3 - j9.87 \ (\Omega).$$

P.9-23 a)  $|r| = \frac{s-1}{s+1} = \frac{|\frac{z_L}{Z_0} - 1|}{|\frac{z_L}{Z_0} + 1|} = \frac{\sqrt{(r_L - 1)^2 + x_L^2}}{\sqrt{(r_L + 1)^2 + x_L^2}}$ .

where  $r_L = R_L/Z_0$  and  $x_L = X_L/Z_0$ .

$$\rightarrow x_L = \pm \left[ \frac{(\frac{s-1}{s+1})^2 (r_L + 1)^2 - (r_L - 1)^2}{1 - (\frac{s-1}{s+1})^2} \right]^{1/2}.$$

When  $S = 3$ ,  $x_L = \pm \sqrt{(10r_L - 3r_L^2 - 3)/3}$ .

b)  $S = 3$  and  $r_L = 150/75 = 2 \rightarrow x_L = \pm \sqrt{5/3}$ .

$X_L = x_L Z_0 = \pm 96.8 \ (\Omega).$

c) From Eq. (9-147):  $r_L + jx_L = \frac{r_m + jt}{1 + jr_m t}$ ,

where  $r_m = R_m/Z_0$ , and  $t = \tan \beta l_m$ .

$$\rightarrow r_m = \frac{(1 + r_L^2 + x_L^2) \pm \sqrt{(1 + r_L^2 + x_L^2)^2 - 4r_L^2}}{2r_L} \\ = 3 \text{ or } \frac{1}{3}, \text{ for } r_L = 2 \text{ and } x_L^2 = 5/3.$$

Also,  $x_L = \frac{(1 - r_m^2)t}{1 + r_m^2 t^2} \rightarrow t = \frac{1}{2x_L r_m} \left[ (1 - r_m^2) \pm \sqrt{(1 - r_m^2)^2 - 4x_L^2 r_m^2} \right]$ .

$r_m = 3$  yields negative  $t$  (discard).

For  $r_m = \frac{1}{3}$ ,  $t = \begin{cases} 3\sqrt{3}/5 \rightarrow l_m = 0.1865\lambda \\ \text{or } \sqrt{15} \rightarrow l_m = 0.2098\lambda \end{cases}$

Use  $l_m = 0.2098\lambda$  to obtain  $V_{min}$  nearest to the load at  $(0.5 - 0.2098)\lambda = 0.2902\lambda$ .

P. 9-24 a)  $|r|^2 = \left| \frac{(R_L - Z_0) + jX_L}{(R_L + Z_0) + jX_L} \right|^2 = \frac{(R_L - Z_0)^2 + X_L^2}{(R_L + Z_0)^2 + X_L^2}$

$$\frac{\partial |r|^2}{\partial Z_0} = 0 \longrightarrow Z_0 = \sqrt{R_L^2 + X_L^2}.$$

If  $Z_L = 40 + j30 (\Omega)$ ,  $Z_0 = 50 (\Omega)$ .

b)  $\text{Min. } |r| = \sqrt{\frac{Z_0 - R_L}{Z_0 + R_L}} = \sqrt{\frac{50 - 40}{50 + 40}} = \frac{1}{3}.$

$$\text{Min. } S = \frac{1 + \frac{1}{3}}{1 - \frac{1}{3}} = 2.$$

c) From Eq. (9-147):  $r_i + jx_i = \frac{r_m + jt}{1 + jr_mt} = 0.8 + j0.6.$

$$\longrightarrow t = \frac{1}{2x_i r_m^2} \left[ (1 - r_m^2) \pm \sqrt{(1 - r_m^2)^2 - 4x_i^2 r_m^2} \right] \quad \left( \begin{array}{l} \text{See problem} \\ \text{p. 9-23.} \end{array} \right)$$

At voltage minimum,  $r_m = \frac{1}{S} = \frac{1}{2}.$

$t = 1$  (Use negative sign.)

$$\tan \beta l_m = \tan(2\pi l_m / \lambda) = 1 \longrightarrow l_m = \frac{\lambda}{8}.$$

$\therefore$  Voltage minimum nearest to the load is  $(\frac{\lambda}{2} - \frac{\lambda}{8})$   
or  $3\lambda/8$  from the load.

P.10-4 Field expressions for  $TM_n$  modes, from Eqs. (10-63, 64 & 65):

$$E_z^o(y) = A_n \sin(n\pi y/b),$$

$$H_x^o(y) = \frac{j\omega\epsilon}{h} A_n \cos(n\pi y/b),$$

$$E_y^o(y) = -\frac{\gamma}{h} A_n \cos(n\pi y/b).$$

Surface charge densities:

$$\rho_{sL} = \bar{a}_n \cdot \bar{D} \big|_{y=0} = \epsilon E_y^o(0) = -\frac{\gamma\epsilon}{h} A_n,$$

$$\rho_{sU} = \bar{a}_n \cdot \bar{D} \big|_{y=b} = -\epsilon E_y^o(b) = (-1)^n \frac{\gamma\epsilon}{h} A_n.$$

Surface current densities:

$$\bar{J}_{sL} = \bar{a}_n \times \bar{H} \big|_{y=0} = \bar{a}_y \times \bar{H}(0) = -\bar{a}_x \frac{j\omega\epsilon}{h} A_n,$$

$$\bar{J}_{sU} = \bar{a}_n \times \bar{H} \big|_{y=b} = -\bar{a}_y \times \bar{H}(b) = \bar{a}_x (-1)^n \frac{j\omega\epsilon}{h} A_n = \begin{cases} \bar{J}_{sL} & \text{for } n \text{ odd} \\ -\bar{J}_{sL} & \text{for } n \text{ even} \end{cases}$$

P. 10-5 Field expressions for  $TE_n$  modes, from Eqs. (10-83, 84 & 85):

$$H_z^o(y) = B_n \cos(n\pi y/b),$$

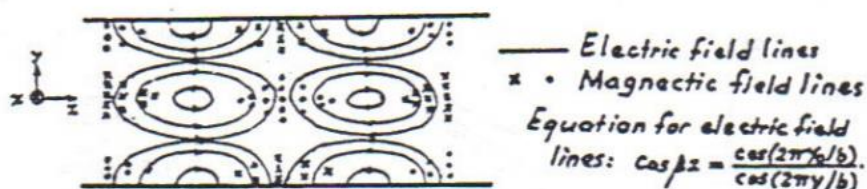
$$H_y^o(y) = \frac{\gamma}{h} B_n \sin(n\pi y/b),$$

$$E_x^o(y) = \frac{j\omega\mu}{h} B_n \sin(n\pi y/b).$$

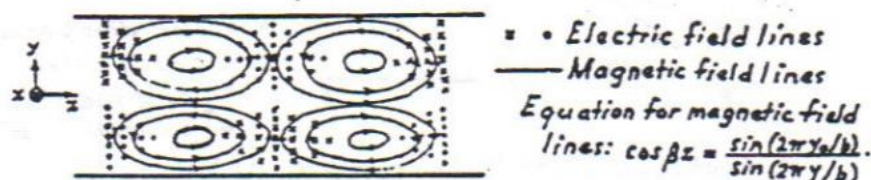
$$\bar{J}_{sL} = \bar{a}_y \times \bar{H}(0) = \bar{a}_x B_n,$$

$$\bar{J}_{sU} = -\bar{a}_y \times \bar{H}(b) = \bar{a}_x (-1)^{n+1} B_n = \begin{cases} \bar{J}_{sL} & \text{for } n \text{ odd} \\ -\bar{J}_{sL} & \text{for } n \text{ even} \end{cases}$$

P. 10-6 a) Set  $n=2$  in the field expressions in problem P. 10-4.



b) Set  $n=2$  in the field expressions in problem P. 10-5.



P.10-11 Parallel-plate waveguide:  $b = 0.03 \text{ (m)}$ ,  $f = 10^9 \text{ (Hz)}$ .

a) TEM mode

From Eqs. (9-1a) and (9-1b):

$$\begin{cases} E_y^o = E_o. \\ H_x^o = -\frac{E_o}{\eta_o}. \end{cases}$$

$$P_{av} = \frac{w}{2} \int_0^b -E_y^o H_x^o dy = \frac{wb}{2\eta_o} E_o^2.$$

Dielectric strength of air:  $\text{Max. } E_o = 3 \times 10^6 \text{ (V/m)}$ .

$$\text{Max.} \left( \frac{P_{av}}{w} \right) = \frac{b}{2\eta_o} (3 \times 10^6)^2 = 358 \times 10^8 \text{ (W/m)} = 358 \text{ (MW/m)}.$$

b) TM<sub>1</sub> mode

From Eqs. (10-64) and (10-65):

$$\begin{cases} E_y^o(y) = E_o \cos\left(\frac{\pi y}{b}\right), \\ H_x^o(y) = -\frac{E_o}{\eta_o \sqrt{1-(f_c/f)^2}} \cos\left(\frac{\pi y}{b}\right), \end{cases}$$
$$f_c = \frac{1}{2b/\mu_o \epsilon_o} = 5 \times 10^9 \text{ (Hz)}.$$

$$P_{av} = \frac{w}{2} \int_0^b -E_y^o(y) H_x^o(y) dy = \frac{wb E_o^2}{4\eta_o \sqrt{1-(f_c/f)^2}}.$$

$$\text{Max.} \left( \frac{P_{av}}{w} \right) = \frac{b (3 \times 10^6)^2}{4\eta_o \sqrt{1-(f_c/f)^2}} = 2.07 \times 10^8 \text{ (W/m)} = 207 \text{ (MW/m)}.$$

c) TE<sub>1</sub> mode

From Eqs. (10-84) and (10-85):

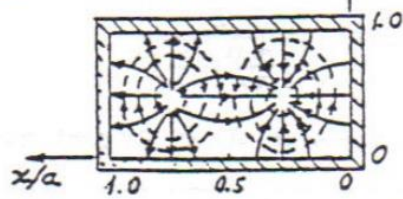
$$\begin{cases} E_z^o(y) = E_o \sin\left(\frac{\pi y}{b}\right), \\ H_y^o(y) = \frac{E_o}{\eta_o \sqrt{1-(f_c/f)^2}} \sin\left(\frac{\pi y}{b}\right). \end{cases}$$

$$P_{av} = \frac{w}{2} \int_0^b E_z^o(y) H_y^o(y) dy = \frac{wb E_o^2}{4\eta_o} \sqrt{1-(f_c/f)^2}.$$

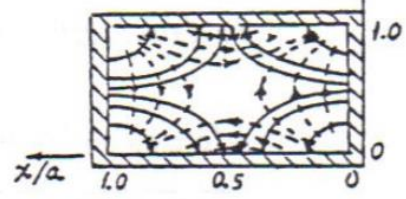
$$\text{Max.} \left( \frac{P_{av}}{w} \right) = \frac{b (3 \times 10^6)^2}{4\eta_o} \sqrt{1-(f_c/f)^2} = 1.55 \times 10^8 \text{ (W/m)} = 155 \text{ (MW/m)}.$$



P.10-12 a)  $TM_{21}$  mode



b)  $TE_{11}$  mode



—— Electric field lines  
 ---- Magnetic field lines

P.10-13 Equations (10-134) through (10-137) for  $TM_{11}$  mode:

$$E_x^0(x,y) = \frac{-j\beta_n}{h^2} \left( \frac{\pi}{a} \right) E_0 \cos\left(\frac{\pi x}{a}\right) \sin\left(\frac{\pi y}{b}\right),$$

$$E_y^0(x,y) = \frac{j\beta_n}{h^2} \left( \frac{\pi}{b} \right) E_0 \sin\left(\frac{\pi x}{a}\right) \cos\left(\frac{\pi y}{b}\right).$$

$$E_x^0(x,y) = E_0 \sin\left(\frac{\pi x}{a}\right) \sin\left(\frac{\pi y}{b}\right),$$

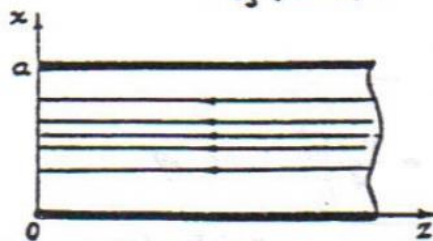
$$H_x^0(x,y) = \frac{j\omega\epsilon}{h^2} \left( \frac{\pi}{b} \right) E_0 \sin\left(\frac{\pi x}{a}\right) \cos\left(\frac{\pi y}{b}\right),$$

$$H_y^0(x,y) = \frac{-j\omega\epsilon}{h^2} \left( \frac{\pi}{a} \right) E_0 \cos\left(\frac{\pi x}{a}\right) \sin\left(\frac{\pi y}{b}\right).$$

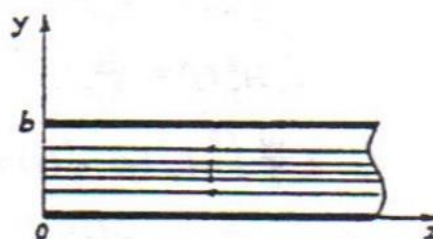
a) Surface current densities:

$$\begin{aligned} \bar{J}_s(y=0) &= \bar{a}_n \times \bar{H} \Big|_{y=0} = \bar{a}_y \times [\bar{a}_x H_x^0(x,0) + \bar{a}_z H_z^0(x,0)] \\ &= -\bar{a}_z H_x^0(x,0) = -\bar{a}_z \frac{j\omega\epsilon}{h^2} \left( \frac{\pi}{b} \right) E_0 \sin\left(\frac{\pi x}{a}\right) e^{-j\beta_n z} \\ &= \bar{J}_s(y=b). \end{aligned}$$

$$\begin{aligned} \bar{J}_s(x=0) &= \bar{a}_n \times \bar{H} \Big|_{x=0} = \bar{a}_x \times [\bar{a}_x H_x^0(0,y) + \bar{a}_z H_z^0(0,y)] \\ &= \bar{a}_z H_y^0(0,y) = -\bar{a}_z \frac{j\omega\epsilon}{h^2} \left( \frac{\pi}{a} \right) E_0 \sin\left(\frac{\pi y}{b}\right) e^{-j\beta_n z} \\ &= \bar{J}_s(x=a). \end{aligned}$$



$\bar{J}_s$  at  $y=b$



$\bar{J}_s$  at  $x=0$ .

P.10-14 Rectangular waveguide:  $a = 7.21 \text{ (cm)}$ ,  $b = 3.40 \text{ (cm)}$ .

$$\text{Eq. (10-140): } (\lambda_c)_{mn} = \frac{2}{\sqrt{\left(\frac{m}{a}\right)^2 + \left(\frac{n}{b}\right)^2}}.$$

Modes with the shortest  $\lambda_c < 5 \text{ (cm)}$  are:

Mode	$TE_{10}$	$TE_{20}$	$TE_{01}$	$TE_{11}/TM_{11}$
$\lambda \text{ (cm)}$	14.4	7.20	6.80	6.15

a) For  $\lambda = 10 \text{ (cm)}$ , the only propagating mode is  $TE_{10}$ .

b) For  $\lambda = 5 \text{ (cm)}$ , the propagating modes are:  
 $TE_{10}$ ,  $TE_{20}$ ,  $TE_{01}$ ,  $TE_{11}$ , and  $TM_{11}$ .

P.10-16  $(f_c)_{mn} = \frac{1}{2\sqrt{\mu\epsilon}} \sqrt{\left(\frac{m}{a}\right)^2 + \left(\frac{n}{b}\right)^2} = \frac{1}{2a\sqrt{\mu\epsilon}} F(m,n).$

a)  $a = 2b$ ,  $F(m,n) = \sqrt{m^2 + 4n^2}$  | b)  $a = b$ ,  $F(m,n) = \sqrt{m^2 + n^2}$ .

Modes	$F(m,n)$
$TE_{10}$	1
$TE_{01}, TE_{20}$	2
$TE_{11}, TM_{11}$	$\sqrt{5}$
$TE_{02}$	4
$TM_{12}$	$\sqrt{17}$
$TM_{22}$	$\sqrt{20}$

Modes	$F(m,n)$
$TE_{10}, TE_{01}$	1
$TE_{11}, TM_{11}$	$\sqrt{2}$
$TE_{02}, TE_{20}$	2
$TM_{12}$	$\sqrt{5}$
$TM_{22}$	$2\sqrt{2}$

P.10-17  $f = 3 \times 10^9 \text{ (Hz)}$ ,  $\lambda = c/f = 0.1 \text{ (m)}$ .

Let  $a = kb$ ,  $1 < k < 2$ .  $(f_c)_{mn} = \frac{3 \times 10^8}{2a} \sqrt{m^2 + k^2 n^2}$ .

a)  $(f_c)_{10} = \frac{1.5 \times 10^8}{a}$  for the dominant  $TE_{10}$  mode.

For  $f > 1.2 (f_c)_{10}$ :  $a > 0.06 \text{ (m)}$ .

The next higher-order mode is  $TE_{01}$  with  $(f_c)_{01} = \frac{1.5 \times 10^8}{b}$ .

For  $f < 0.8 (f_c)_{01}$ :  $b < 0.04 \text{ (m)}$ .

We choose  $a = 6.5 \text{ (cm)}$  and  $b = 3.5 \text{ (cm)}$ .

b)  $u_p = \frac{c}{\sqrt{1 - (\lambda/2a)^2}} = 4.70 \times 10^8 \text{ (m/s)},$

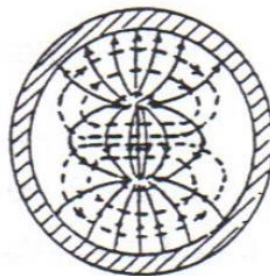
$\lambda_g = \frac{\lambda}{\sqrt{1 - (\lambda/2a)^2}} = 0.157 \text{ (m)} = 15.7 \text{ (cm)},$

$\beta = \frac{2\pi}{\lambda_g} = 40.1 \text{ (rad/m)},$

$(Z_{TE})_{10} = \frac{\eta_0}{\sqrt{1 - (\lambda/2a)^2}} = 590 \text{ (}\Omega\text{)}.$

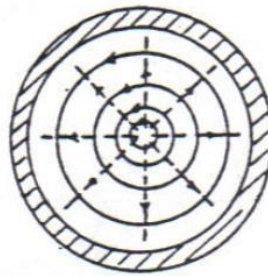
P.10-27 a)

$TM_{11}$



b)

$TE_{01}$



———— Electric field lines.

----- Magnetic field lines.

c) Eq. (10-35):  $f_c = \frac{h}{2\pi\sqrt{\mu\epsilon}} = \frac{1.5 \times 10^8}{\pi} h$

For  $TM_{11}$  mode,  $(h)_{TM_{11}} = \frac{3.832}{a} \rightarrow (f_c)_{TM_{11}} = \frac{1.83 \times 10^8}{a} \text{ Hz}$

For  $TE_{01}$  mode,  $(h)_{TE_{01}} = \frac{3.832}{a} \rightarrow (f_c)_{TE_{01}} = (f_c)_{TM_{11}}$ .  
(Degenerate mode)

P.10-38 From Eq. (10-301):  $f_{mnp} = \frac{u}{2} \sqrt{\left(\frac{m}{a}\right)^2 + \left(\frac{n}{b}\right)^2 + \left(\frac{p}{d}\right)^2}$ .

$f_{mnp} = 1.5 \times 10^{10} F(m,n,p)$ ,  $F(m,n,p) = \sqrt{\left(\frac{m}{8}\right)^2 + \left(\frac{n}{6}\right)^2 + \left(\frac{p}{5}\right)^2}$ .

Lowest-order modes and resonant frequencies:

Modes	$F(m,n,p)$	$(f_c)_{mnp}$ in (Hz)
$TM_{110}$	0.2083	$3.125 \times 10^9$
$TE_{101}$	0.2358	$3.538 \times 10^9$
$TE_{011}$	0.2603	$3.905 \times 10^9$
$TE_{111}, TM_{111}$	0.2888	$4.332 \times 10^9$
$TM_{210}$	0.3005	$4.507 \times 10^9$
$TE_{201}$	0.3202	$4.802 \times 10^9$
$TM_{120}$	0.3560	$5.340 \times 10^9$
$TE_{211}, TM_{211}$	0.3609	$5.414 \times 10^9$
$TE_{021}$	0.3887	$5.831 \times 10^9$
$TE_{121}, TM_{121}$	0.4083	$6.125 \times 10^9$