

University of Moratuwa
Faculty of Engineering
Department of Electronic & Telecommunication Engineering



Modelling and Analysis of Physiological Systems

Branched Cylinders
Dendritic Tree Approximations

Bandara D.M.D.V.
Undergraduate (Biomedical engineering)
Department Electronic and Telecommunications
Faculty of Engineering
University of Moratuwa

June 10, 2023

Contents

Question 1	1
Question 2	2
Question 3	4
Question 4	5
Question 5	6
Question 6	10

Question 1

From the given equations,

$$\begin{aligned} V_1(X) &= A_1 e^{-X} + B_1 e^X \\ V_{21}(X) &= A_{21} e^{-X} + B_{21} e^X \\ V_{22}(X) &= A_{22} e^{-X} + B_{22} e^X \end{aligned} \quad (2)$$

$$\left. \frac{dV_1}{dX} \right|_{X=0} = -(r_i \lambda_c)_1 I_{app} \quad (3)$$

Terminal ends of daughter branches held at rest.

$$V_{21}(L_{21}) = V_{22}(L_{22}) = 0 \quad (4)$$

The membrane potential must be continuous at the nodes,

$$V_1(L_1) = V_{21}(L_1) = V_{22}(L_1) = 0 \quad (5)$$

The current is conserved at the nodes,

$$\left. \frac{-1}{(r_i \lambda_c)_1} \frac{dV_1}{dX} \right|_{X=L_1} = \left. \frac{-1}{(r_i \lambda_c)_{21}} \frac{dV_{21}}{dX} \right|_{X=L_1} + \left. \frac{-1}{(r_i \lambda_c)_1} \frac{dV_{22}}{dX} \right|_{X=L_1} \quad (6)$$

From these 5 equations we can approach the required equation. First differentiating equation 2 w.r.t X,

$$\frac{dV_1}{dX} = -A_1 e^{-X} + B_1 e^X$$

At 0,

$$\left. \frac{dV_1}{dX} \right|_{X=0} = -A_1 + B_1$$

From equation 3;

$$-(r_i \lambda_c)_1 I_{app} = -A_1 + B_1$$

$$A_1 - B_1 = (r_i \lambda_c)_1 I_{app} \quad (I)$$

From the remaining Boundary conditions given by equation 4

$$V_{21}(L_{21}) = 0$$

$$A_{21} e^{-L_{21}} + B_{21} e^{L_{21}} = 0 \quad (II)$$

Similarly,

$$A_{22} e^{-L_{22}} + B_{22} e^{L_{22}} = 0 \quad (III)$$

Then at nodes, membrane potential must be same as given in equation 5. i.e,

$$\begin{aligned} V_1(L_1) &= V_{21}(L_1) \\ A_1 e^{-L_1} + B_1 e^{L_1} &= A_{21} e^{-L_1} + B_{21} e^{L_1} \\ A_1 e^{-L_1} + B_1 e^{L_1} - A_{21} e^{-L_1} - B_{21} e^{L_1} &= 0 \end{aligned} \quad (IV)$$

Similarly,

$$V_{22}(L_1) = V_{21}(L_1)$$

$$A_{22}e^{-L_1} + B_{22}e^{L_1} - A_{21}e^{-L_1} - B_{21}e^{L_1} = 0 \quad (V)$$

Now by current conservation given by equation 6;

$$\frac{-1}{(r_i\lambda_c)_1}(-A_1e^{-L_1}+B_1e^{L_1}) = \frac{-1}{(r_i\lambda_c)_{21}}(-A_{21}e^{-L_1}+B_{21}e^{L_1}) + \frac{-1}{(r_i\lambda_c)_1}(-A_{22}e^{-L_1}+B_{22}e^{L_1})$$

Now by substituting results from equations II, III, IV , V and simplifying we get the following equation 7.

$$\frac{A_1e^{-L_1}}{(r_i\lambda_c)_1} + \frac{B_1e^{-L_1}}{(r_i\lambda_c)_1} + \frac{A_{21}e^{-L_1}}{(r_i\lambda_c)_{21}} - \frac{B_{21}e^{-L_1}}{(r_i\lambda_c)_{21}} + \frac{A_{22}e^{-L_1}}{(r_i\lambda_c)_{22}} - \frac{B_{22}e^{-L_1}}{(r_i\lambda_c)_{22}} = 0 \quad (7)$$

Hence, the equation 7 is now verified.

Question 2

Defining the matrices as given,

$$x = \begin{pmatrix} A_1 \\ B_1 \\ A_{21} \\ B_{21} \\ A_{22} \\ B_{22} \end{pmatrix} \quad (8)$$

Then equation 7 can be written as,

$$Ax = b \quad (9)$$

Where,

$$b = \begin{pmatrix} (r_i\lambda_c)_1 I_{app} \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{pmatrix} \quad (10)$$

And,

$$A = \begin{pmatrix} 1 & -1 & 0 & 0 & 0 & 0 \\ 0 & 0 & e^{-L_{21}} & e^{L_{21}} & 0 & 0 \\ 0 & 0 & 0 & 0 & e^{-L_{22}} & e^{L_{22}} \\ e^{-L_1} & e^{L_1} & -e^{-L_1} & -e^{L_1} & 0 & 0 \\ 0 & 0 & e^{-L_1} & e^{L_1} & -e^{-L_1} & -e^{L_1} \\ \frac{-e^{-L_1}}{(r_i\lambda_c)_1} & \frac{e^{L_1}}{(r_i\lambda_c)_1} & \frac{e^{-L_1}}{(r_i\lambda_c)_{21}} & \frac{-e^{L_1}}{(r_i\lambda_c)_{21}} & \frac{e^{-L_1}}{(r_i\lambda_c)_{22}} & \frac{-e^{L_1}}{(r_i\lambda_c)_{22}} \end{pmatrix} \quad (11)$$

By simplifying equation 9 by substituting equations 8, 10, and 11.

$$Ax = b$$

$$\begin{pmatrix} 1 & -1 & 0 & 0 & 0 & 0 \\ 0 & 0 & e^{-L_{21}} & e^{L_{21}} & 0 & 0 \\ 0 & 0 & 0 & 0 & e^{-L_{22}} & e^{L_{22}} \\ e^{-L_1} & e^{L_1} & -e^{-L_1} & -e^{L_1} & 0 & 0 \\ 0 & 0 & e^{-L_1} & e^{L_1} & -e^{-L_1} & -e^{L_1} \\ \frac{-e^{-L_1}}{(r_i \lambda_c)_1} & \frac{e^{L_1}}{(r_i \lambda_c)_1} & \frac{e^{-L_1}}{(r_i \lambda_c)_{21}} & \frac{-e^{L_1}}{(r_i \lambda_c)_{21}} & \frac{e^{-L_1}}{(r_i \lambda_c)_{22}} & \frac{-e^{L_1}}{(r_i \lambda_c)_{22}} \end{pmatrix} \begin{pmatrix} A_1 \\ B_1 \\ A_{21} \\ B_{21} \\ A_{22} \\ B_{22} \end{pmatrix} = \begin{pmatrix} (r_i \lambda_c)_1 I_{app} \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{pmatrix}$$

$$\begin{pmatrix} A_1 & -B_1 & 0 & 0 & 0 & 0 \\ 0 & 0 & A_{21}e^{-L_{21}} & B_{21}e^{L_{21}} & 0 & 0 \\ 0 & 0 & 0 & 0 & A_{22}e^{-L_{22}} & B_{22}e^{L_{22}} \\ A_1e^{-L_1} & B_1e^{L_1} & -A_{21}e^{-L_1} & -B_{21}e^{L_1} & 0 & 0 \\ 0 & 0 & A_{21}e^{-L_1} & B_{21}e^{L_1} & -A_{22}e^{-L_1} & -B_{22}e^{L_1} \\ \frac{-A_1e^{-L_1}}{(r_i \lambda_c)_1} & \frac{B_1e^{L_1}}{(r_i \lambda_c)_1} & \frac{A_{21}e^{-L_1}}{(r_i \lambda_c)_{21}} & \frac{-B_{21}e^{L_1}}{(r_i \lambda_c)_{21}} & \frac{A_{22}e^{-L_1}}{(r_i \lambda_c)_{22}} & \frac{-B_{22}e^{L_1}}{(r_i \lambda_c)_{22}} \end{pmatrix} = \begin{pmatrix} (r_i \lambda_c)_1 I_{app} \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{pmatrix}$$

Now by equating both sides of each row,

$$A_1 - B_1 = (r_i \lambda_c)_1 I_{app} \quad (\text{I})$$

$$A_{21}e^{-L_{21}} + B_{21}e^{L_{21}} = 0 \quad (\text{II})$$

$$A_{22}e^{-L_{22}} + B_{22}e^{L_{22}} = 0 \quad (\text{III})$$

$$A_1e^{-L_1} + B_1e^{L_1} - A_{21}e^{-L_1} - B_{21}e^{L_1} = 0 \quad (\text{IV})$$

$$A_{22}e^{-L_1} + B_{22}e^{L_1} - A_{21}e^{-L_1} - B_{21}e^{L_1} = 0 \quad (\text{V})$$

$$\frac{A_1e^{-L_1}}{(r_i \lambda_c)_1} + \frac{B_1e^{L_1}}{(r_i \lambda_c)_1} + \frac{A_{21}e^{-L_1}}{(r_i \lambda_c)_{21}} - \frac{B_{21}e^{L_1}}{(r_i \lambda_c)_{21}} + \frac{A_{22}e^{-L_1}}{(r_i \lambda_c)_{22}} - \frac{B_{22}e^{L_1}}{(r_i \lambda_c)_{22}} = 0 \quad (7)$$

Hence, the equation 7 is obtained from the matrices.

Question 3

Matlab Code:

```
% electrical constants and derived quantities for typical
% mammalian dendrite

% Dimensions of compartments

d1 = 75e-4; % cm
d21 = 30e-4; % cm
d22 = 15e-4; % cm
%d21 = 47.2470e-4; % E9 cm
%d22 = d21; % E9 cm

l1 = 1.5; % dimensionless
l21 = 3.0; % dimensionless
l22 = 3.0; % dimensionless

% Electrical properties of compartments

Rm = 6e3; % Ohms cm^2
Rc = 90; % Ohms cm
Rs = 1e6; % Ohms

c1 = 2*(Rc*Rm)^(1/2)/pi;

r11 = c1*d1^(-3/2); % Ohms
r121 = c1*d21^(-3/2); % Ohms
r122 = c1*d22^(-3/2); % Ohms

% Applied current

iapp = 1e-9; % Amps

% Coefficient matrices

A = [1 -1 0 0 0 0;
     0 0 exp(-l21) exp(l21) 0 0;
     0 0 0 exp(-l22) exp(l22);
     exp(-l1) exp(l1) -exp(-l1) -exp(l1) 0 0;
     0 0 exp(-l1) exp(l1) -exp(-l1) -exp(l1);
     -exp(-l1) exp(l1) r11*exp(-l1)/r121 -r11*exp(l1)/r121
     r11*exp(-l1)/r122 -r11*exp(l1)/r122];

b = [r11*iapp 0 0 0 0 0]';

%% Question 03%%
x=A\b;
display(x)
```

Results are.

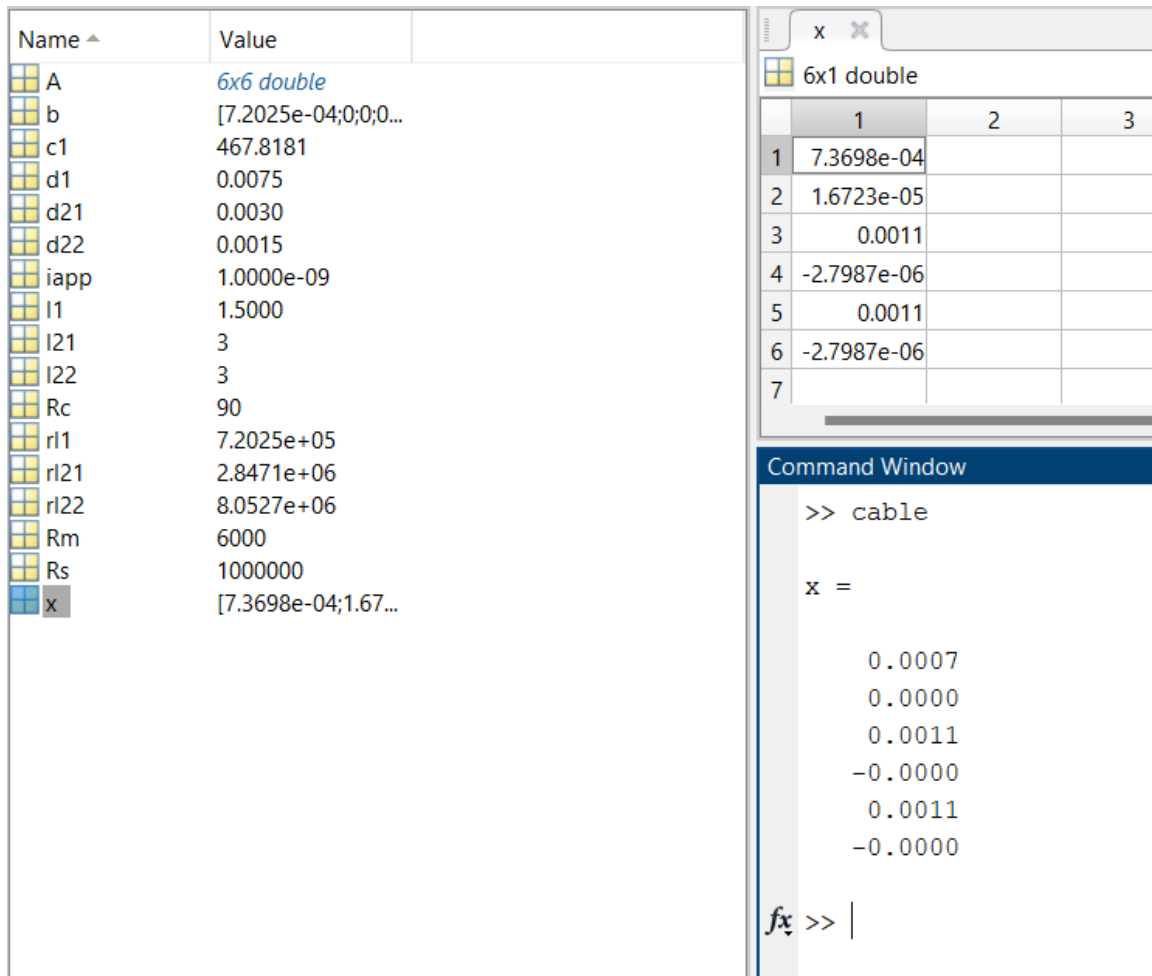


Figure 1: 03

Question 4

After copying the following code we get the plot below that.

```

%% Question 04%%
y1=linspace(0,l1,20);
y21=linspace(l1,l21,20);
y22=linspace(l1,l22,20);
v1=x(1)*exp(-y1)+x(2)*exp(y1);
v21=x(3)*exp(-y21)+x(4)*exp(y21);
v22=x(5)*exp(-y22)+x(6)*exp(y22);
plot(y1,v1,'y-',y21,v21,'r-',y22,v22,'b-');
xlabel('X (dimensionless)');
ylabel('V (Volts)');
title('Steady-state voltage - E5');

```

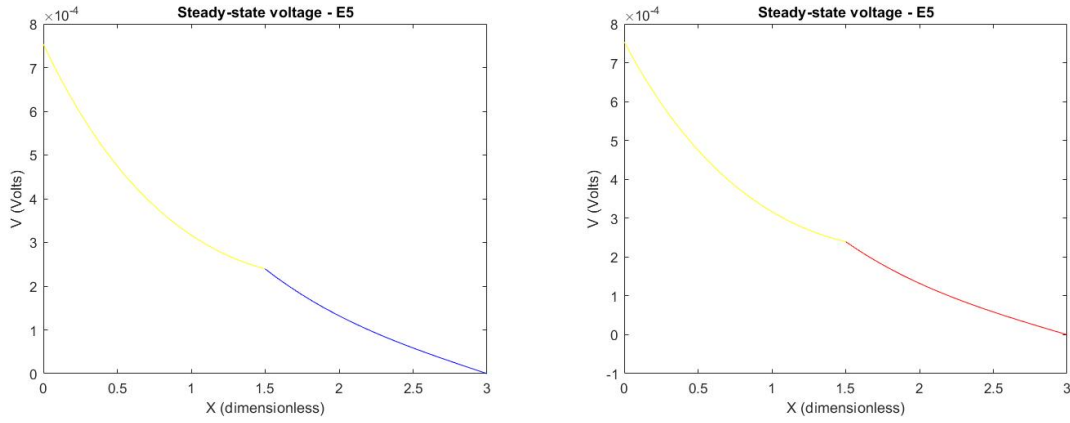


Figure 2: 04

Though I have shown two plots, both blue and red overlap with each other. The yellow line indicates the steady-state voltage profile of the parent branch. Since red and blue overlap, both daughter branches have the same steady voltage profile.

Question 5

For the each given conditions,

$$\begin{array}{lcl}
 \text{(a)} & \frac{dV_1}{dX} \Big|_{X=0} = -(r_i \lambda_c)_1 I_{app} & \begin{array}{l} \frac{dV_{21}}{dX} \Big|_{X=L_{21}} = 0 \\ V_{22}(L_{22}) = 0 \end{array}
 \end{array}$$

```

%% Question 05%%
%% part (a)%
Aa = A;
Aa(2,:) = [0 0 -exp(-121) exp(121) 0 0];
x= Aa\b;
y1=linspace(0,11,20);
y21=linspace(11,121,20);
y22=linspace(11,122,20);
v1=x(1)*exp(-y1)+x(2)*exp(y1);
v21=x(3)*exp(-y21)+x(4)*exp(y21);
v22=x(5)*exp(-y22)+x(6)*exp(y22);
plot(y1,v1,'y-',y21,v21,'r-',y22,v22,'b-');
xlabel('X (dimensionless)');
ylabel('V (Volts)');
title('Steady-state voltage - E5');

```

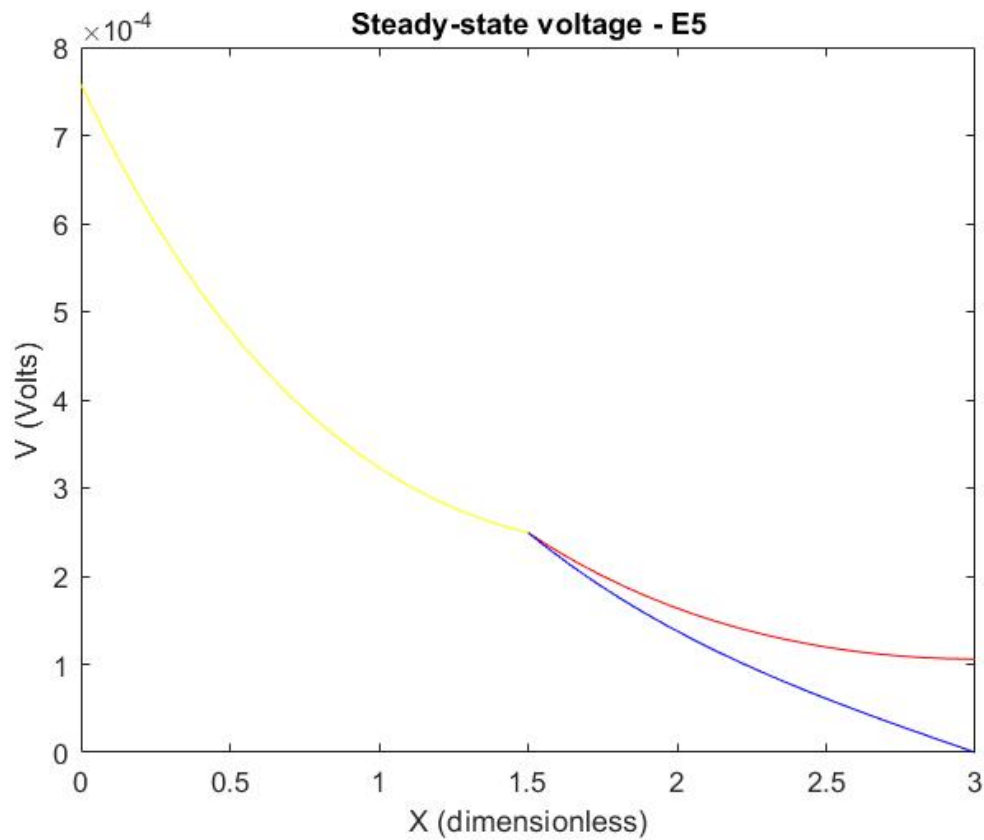



Figure 3: 05.01

(b) $\frac{dV_1}{dX}\bigg|_{X=0} = -(r_i\lambda_c)_1 I_{app}$ $\frac{dV_{21}}{dX}\bigg|_{X=L_{21}} = 0$ $\frac{dV_{22}}{dX}\bigg|_{X=L_{22}} = 0$

```

%% part (b)%%
Ab = Aa;
Ab(3,:) = [0 0 0 0 -exp(-122) exp(122)];
x=Ab\b;
y1=linspace(0,11,20);
y21=linspace(11,121,20);
y22=linspace(11,122,20);
v1=x(1)*exp(-y1)+x(2)*exp(y1);
v21=x(3)*exp(-y21)+x(4)*exp(y21);
v22=x(5)*exp(-y22)+x(6)*exp(y22);
plot(y1,v1,'y-',y21,v21,'r-',y22,v22,'b-');
xlabel('X(dimensionless)');
ylabel('V(Volts)');
title('Steady state voltage - E5');

```

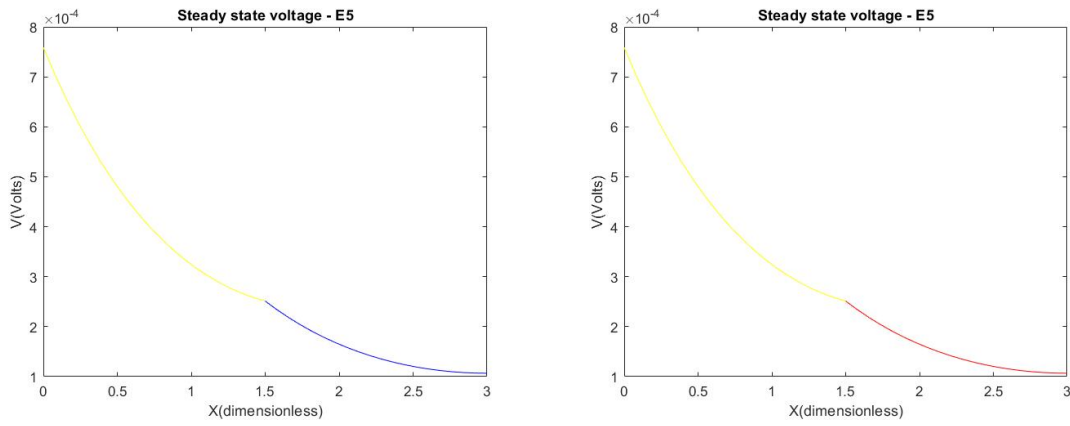


Figure 4: 05.02

(c) $\frac{dV_1}{dX}\bigg|_{X=0} = 0$

$\frac{dV_{21}}{dX}\bigg|_{X=L_{21}} = (r_i\lambda_c)_{21}I_{app}$

$V_{22}(L_{22}) = 0$

```
%% part (c)%%
Ac = A;
Ac(2,:) = [0 0 -exp(-l21) exp(l21) 0 0];
bc = b;
bc(1) = 0;
bc(2) = rl21*iapp;
x=Ac\bc;
y1=linspace(0,l1,20);
y21=linspace(l1,l21,20);
y22=linspace(l1,l22,20);
v1=x(1)*exp(-y1)+x(2)*exp(y1);
v21=x(3)*exp(-y21)+x(4)*exp(y21);
v22=x(5)*exp(-y22)+x(6)*exp(y22);
plot(y1,v1,'y-',y21,v21,'r-',y22,v22,'b-');
xlabel('X(dimensionless)');
ylabel('V(Volts)');
title('Steady state voltage - E5');
```

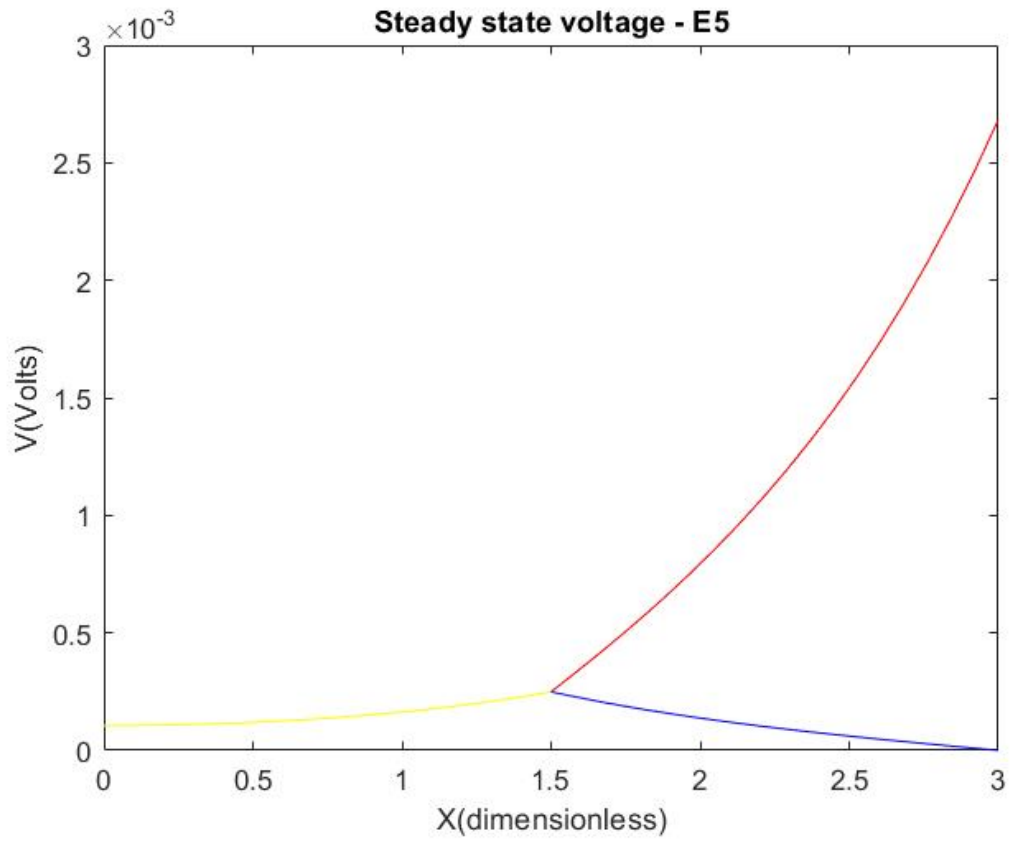


Figure 5: 05.03

(d) $\left. \frac{dV_1}{dX} \right|_{X=0} = 0$

$\left. \frac{dV_{21}}{dX} \right|_{X=L_{21}} = (r_i \lambda_c)_{21} I_{app}$

$\left. \frac{dV_{22}}{dX} \right|_{X=L_{22}} = (r_i \lambda_c)_{22} I_{app}$

```
%% part (d)%%
bd = bc;
bd(3) = rl22*iapp;
x=Ac\bd;
y1=linspace(0,l1,20);
y21=linspace(l1,l21,20);
y22=linspace(l1,l22,20);
v1=x(1)*exp(-y1)+x(2)*exp(y1);
v21=x(3)*exp(-y21)+x(4)*exp(y21);
v22=x(5)*exp(-y22)+x(6)*exp(y22);
plot(y1,v1,'y-',y21,v21,'r-',y22,v22,'b-');
xlabel('X(dimensionless)');
ylabel('V(Volts)');
title('Steady state voltage - E5');
```

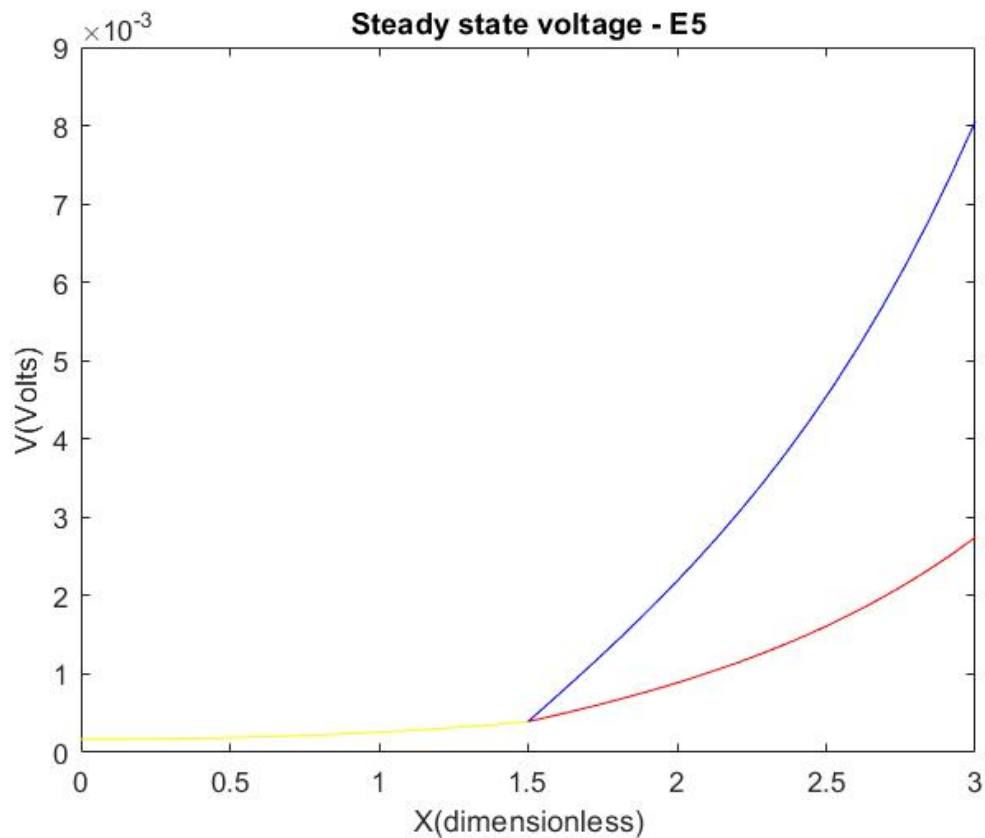


Figure 6: 05.03

Question 6

% electrical constants and derived quantities for typical
% mammalian dendrite

% Dimensions of compartments

```
d1 = 75e-4; % cm
%d21 = 30e-4; % cm
%d22 = 15e-4; % cm
d21 = 47.2470e-4; % E9 cm
d22 = d21; % E9 cm

l1 = 1.5; % dimensionless
l21 = 3.0; % dimensionless
l22 = 3.0; % dimensionless
```

% Electrical properties of compartments

```
Rm = 6e3; % Ohms cm^2
Rc = 90; % Ohms cm
Rs = 1e6; % Ohms

c1 = 2*(Rc*Rm)^(1/2)/pi;
```

```

r11 = c1*d1^(-3/2);          % Ohms
r121 = c1*d21^(-3/2);        % Ohms
r122 = c1*d22^(-3/2);        % Ohms

% Applied current

iapp = 1e-9;      % Amps

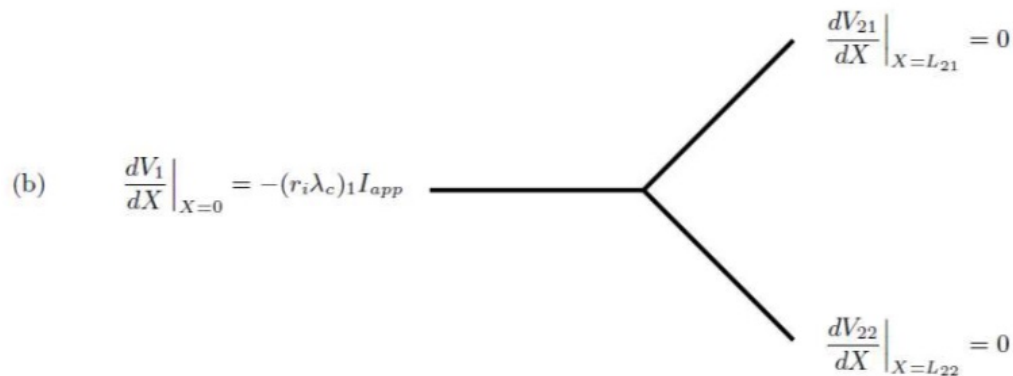
% Coefficient matrices

A = [1 -1 0 0 0 0;
     0 0 exp(-l21) exp(l21) 0 0;
     0 0 0 exp(-l22) exp(l22);
     exp(-l1) exp(l1) -exp(-l1) -exp(l1) 0 0;
     0 0 exp(-l1) exp(l1) -exp(-l1) -exp(l1);
     -exp(-l1) exp(l1) r11*exp(-l1)/r121 -r11*exp(l1)/r121
     r11*exp(-l1)/r122 -r11*exp(l1)/r122];

b = [r11*iapp 0 0 0 0 0]';

%% Question 06%%

```



```

%% Figure - part (b)%
Ab=A;
Ab(2,:) = [0 0 -exp(-l21) exp(l21) 0 0];
Ab(3,:) = [0 0 0 0 -exp(-l22) exp(l22)];
x=Ab\b;
y1=linspace(0,l1,20);
y21=linspace(l1,l21,20);
y22=linspace(l1,l22,20);
v1=x(1)*exp(-y1)+x(2)*exp(y1);
v21=x(3)*exp(-y21)+x(4)*exp(y21);
v22=x(5)*exp(-y22)+x(6)*exp(y22);
plot(y1,v1,'y-',y21,v21,'r-',y22,v22,'b-');
xlabel('X(dimensionless)');
ylabel('V(Volts)');
title('Steady state voltage - E5');

```

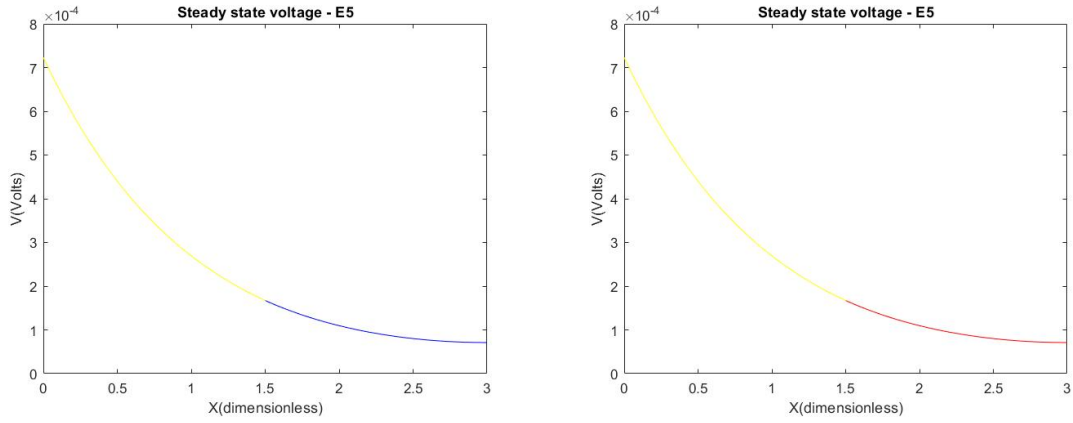


Figure 7: 06.01

(d) $\left. \frac{dV_1}{dX} \right|_{X=0} = 0$

$\left. \frac{dV_{21}}{dX} \right|_{X=L_{21}} = (r_i \lambda_c)_{21} I_{app}$

$\left. \frac{dV_{22}}{dX} \right|_{X=L_{22}} = (r_i \lambda_c)_{22} I_{app}$

```
%% Figure, part (d)%%
Ad = A;
Ad(2,:) = [0 0 -exp(-l21) exp(l21) 0 0];
bd = b;
bd(1) = 0;
bd(2) = rl21*iapp;
bd(3) = rl22*iapp;
x=Ad\bd;
y1=linspace(0,l1,20);
y21=linspace(l1,l21,20);
y22=linspace(l1,l22,20);
v1=x(1)*exp(-y1)+x(2)*exp(y1);
v21=x(3)*exp(-y21)+x(4)*exp(y21);
v22=x(5)*exp(-y22)+x(6)*exp(y22);
plot(y1,v1,'y-',y21,v21,'r-',y22,v22,'b-');
xlabel('X(dimensionless)');
ylabel('V(Volts)');
title('Steady state voltage - E5');
```

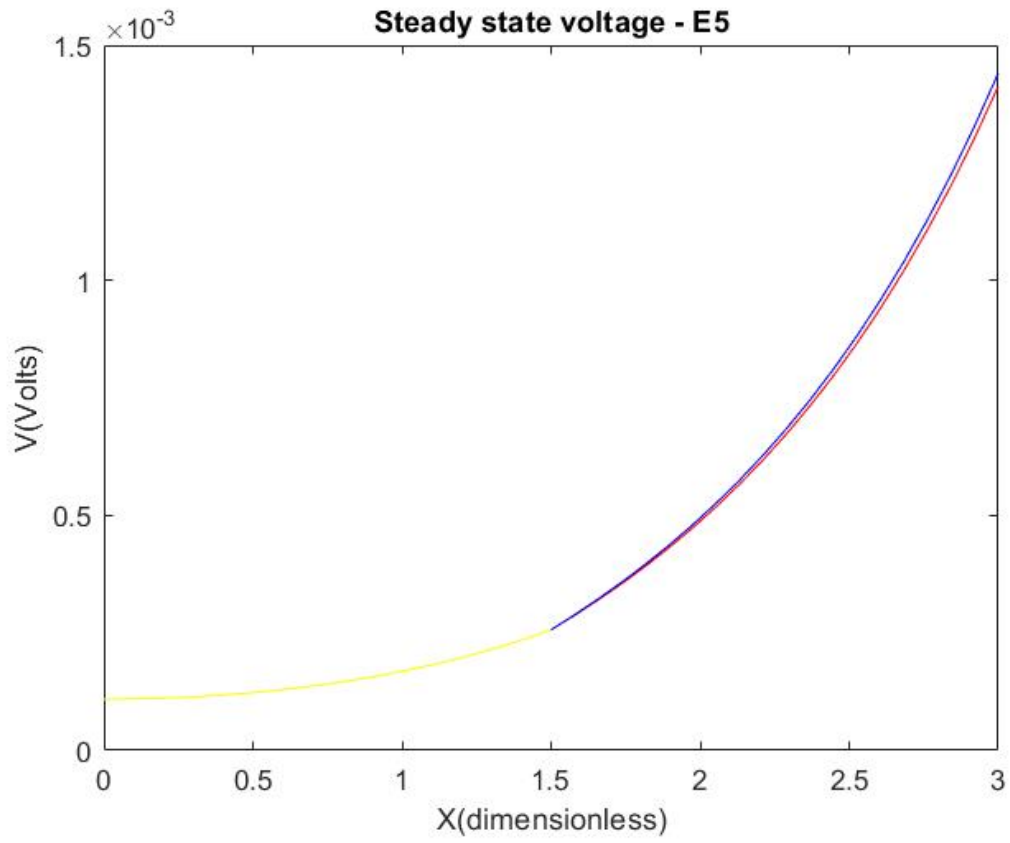


Figure 8: 06.02

When comparing both graphs after changing $d21 = d22 = 47.2470 * 10^4 cm$ both plots became continuously differentiable throughout. Also, there's a slight variation in the two daughter branches which is negligible.