Acadian Gold Corp

Resource, Reserve and Feasibility Report

for the

Purchase and Operation

of

Scotia Mine,

Gays River, Nova Scotia, Canada

45°02′ North, 63°20′ West

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Summary

Mr Will Felderhof, President of Acadian Gold Corp (ADA, TSX-V) based in Halifax, Canada engaged MineTech International Limited on December 21, 2005 to complete a National Instrument 43-101-compliant resource and reserve estimate. The economic analysis of the proposed operation was to be of feasibility study accuracy, or plus-or-minus ten percent. Mr Douglas Roy, M.A.Sc., P.Eng., who was the Principal Author of this report, is a Qualified Person under Section 1.1 of National Instrument 43-101.

The Scotia Mine property is located approximately sixty kilometres northeast of Halifax, Nova Scotia and one kilometre east of the community of Gays River in the Halifax Regional Municipality. The property's general location is 45°02′ North, 63°20′ West. Access to the property is by paved roads and is approximately fifteen kilometres off the Trans Canada Highway along Route #224. The Halifax International Airport is located twenty kilometres southwest of the mine site.

The site lies along the south side of the Gays River main branch, immediately east of the confluence with the Gays River south branch. The deposit is in a rural-residential area of central Nova Scotia that is typified by rolling topography and abundant surface water.

The climate is variable because of mixed continental and maritime weather patterns. Mean annual temperature is 5.9 ºC, mean annual precipitation is 1,250 mm and yearly evapo-transpiration is estimated to be 560 mm. The relatively mild climate (for Canada) permits year-round operations.

The property consists of 615 hectares of mineral rights, including land with exploration potential for zinc/lead mineralisation, and 568.4 hectares of land ownership (real property). The ScoZinc land package also includes five exploration licenses in the general vicinity of the mine. In total, the 91 claims cover 3,640 acres (1,473 hectares). These licenses are located along strike from the Scotia Mine deposit and include favourable host rocks similar to that at the mine site. All lands were in good standing and were registered to ScoZinc Limited as of February 17, 2006. The range in anniversary dates is from May 2, 2006 for Licence No. 06268 to November 5, 2006 for Licence No. 05851.

Mineral Lease #90-1, which covers the entire mine site, was originally granted by the Nova Scotia Government to Westminer Canada Limited on April 2, 1990. Its anniversary date is April 2, 2006. The lease was transferred to Savage Resources in 1996 and later to Pasminco Resources Canada Company in 1999. It was transferred to ScoZinc in 2002. Savage retains a 2 % net smelter return royalty. Acadian has the option to purchase the royalty for $1.45 million. The duration of the mineral lease is twenty years, at which time it may be renewed. The Mineral Lease grants sufficient rights for mining.

Gallant Aggregates signed a thirty-year lease agreement to mine and remove aggregate from the property for one dollar per tonne of material that is removed from the property. The lease was signed on May 15, 2003 and entitles Gallant, with certain limitations, to mine anywhere on ScoZinc's land. A major condition of Gallant's lease is that metal mining takes precedence

over aggregate mining. Therefore, Gallant's lease will not interfere with zinc and lead mining operations.

An updated Phase I ESA was carried out in conjunction with this Resource/Reserve report. It was completed in March, 2006 by Conestoga-Rovers & Associates (CRA). CRA (then MGI Limited) also carried out a Phase I ESA in 1996. The updated assessment included several site inspections, during which several minor, but no major liabilities were identified.

Between 1997 and 2000, an Environmental Registration Document was prepared. It addressed the environmental concerns of a surface and underground mining operation along with the diversion of a 500 metre section of the Gays River to accommodate the pit design. On August 4, 2000 the Open Pit Lead/Zinc Mine and River Diversion Project proposed by Pasminco Resources Canada Company received environmental assessment approval.

Before mining can begin, the existing Industrial Approval (Industrial Waste Discharge Permit) must be returned to operating status from its current "care and maintenance" status. This should be relatively straightforward process because the proposed operation is nearly identical to the operation for which the Industrial Approval was originally granted.

The Scotia Mine mill, designed and built in 1978/1979, is a flotation process and has a rated capacity of 1,350 tonnes per day. However, it has operated for extended periods at a rate of 2,000 tonnes per day (Thornton, 2006). Other existing site infrastructure includes:

- an administration building containing offices, a dry, warehouses, workshops, a large boardroom, and several heavy equipment bays;
- a compressor building (1,600 square feet);
- a tire shop (2,000 square feet);
- a welding shop;
- a geology building; and,
- a core shed.

Storage and ship loading facilities for lead and zinc concentrates are available at the seaport of Sheet Harbour, a distance of eighty kilometres from the mine site over paved roads. ScoZinc does not own these facilities, but Westminer used them in 1990. Rail transport facilities have also been used for concentrate shipping. A railway siding is located in Milford, eight road-kilometres from the site.

The existing surface rights are sufficient for mining operations. Power is supplied through the regional grid at reasonable rates. Most of the mill's water requirements are satisfied by in-process recycling. Make-up water is drawn from the perennial Gays River. The existing tailings pond has sufficient capacity for the life of the project. There is also sufficient area for waste rock storage on the property.

The Scotia Mine property is underlain by basement rocks of the Cambro-Ordovician Meguma Group which had significant local topographic relief due to rift faulting and erosion. Locally, a veneer of Horton Group, red-brown conglomerate and sandstone mark the base of the unconformably overlying Lower Carboniferous rocks which host the Scotia Mine deposit.

In areas where the basement rocks formed islands in the Carboniferous Sea, coral reefs formed along the shores. These carbonate rocks are the Gays River Formation. The MacCumber Formation is time-equivalent to the Gays River Formation. The MacCumber and Gays River Formations are overlain by evaporites of the Carrolls Corner and Stewiake Formations.

The Scotia Mine mineralisation has long been considered a Mississippi Valley-type lead-zinc deposit - a carbonate-hosted deposit classified as a typical open space filling type, hosted in a dolomitized limestone which developed as a carbonate build-up on an irregular pre-Carboniferous basement topographic high where conditions allowed for growth of reef-building organisms.

In the immediate area of the Scotia Mine, the zinc/lead-bearing Gays River Formation trends in an east-northeast direction across the ScoZinc property. Locally, the mineralisation dips up to 45 ° to the north-northwest which is the depositional slope of the front of the Gays River reef unit but tends to be horizontal in the back reef area. The mineralisation is present as sphalerite and galena and grades from massive Pb-Zn ore-grade material in the fore reef to finely disseminated, lower grade material in the back reef. In the mine area, the Gays River Formation is overlain either by the evaporites of the Carrolls Corner Formation and/or overburden.

The Scotia Mine was discovered in 1973 by the Imperial Oil Enterprises/Cuvier Mines joint venture. Esso initiated mine development in 1978 and commissioned the mill in 1979. From 1979 to 1981 the mine produced 554,000 tonnes of ore containing 2.12 % Zinc and 1.36 % Lead. Esso had difficulty dealing with groundwater conditions along the hanging wall of the mineralised zone, which resulted in having to leave a hanging wall pillar that was comprised of high-grade material. The mine closed in 1982 due to groundwater inflow and operating losses.

Seabright Resources Inc. acquired the mine and mill in 1984. Despite a favourable feasibility study, they did not reactivate the mine due to depressed metal prices at the time. They converted the mill for gold processing and processed gold ore from several satellite properties.

With the takeover of Seabright by Western Mining Corporation (Westminer) in 1988, a review of the potential for mining the deposit was undertaken. Following completion of feasibility studies in 1989, the underground workings were dewatered and test mining was carried out. A total of 187,000 tonnes were mined over a fifteen month period with average grades of 7.47 % Zinc and 3.50% Lead. In 1991, production was suspended again due to groundwater inflow and economic considerations.

In 1997, Savage Resources Canada Limited acquired the Scotia Mine assets from Westminer. Savage concluded that an open pit operation was feasible and initiated environmental permitting, including provisions for a diversion of a portion of the Gays River. Savage was subsequently taken over by Pasminco Resources Canada Company (Pasminco Resources) and

the environmental assessment plan was approved by the Nova Scotia Minister of the Environment in August 2000. The operating plan was never initiated.

Regal Mines Limited (Regal Mines) purchased Pasminco Resources in February 2002. Regal was owned 50 % by OntZinc Corporation (OntZinc) and 50 % by Regal Consolidated Ventures Limited (Regal Consolidated). As part of the sale, Pasminco Canada Holdings Inc (Pasminco Holdings) retained a 2 % net smelter return (NSR) royalty on future production. OntZinc acquired Regal Consolidated's 50 % interest in December 2002 to own 100 % of Pasminco Resources. Savage Resources Limited is the successor of Pasminco Holdings and currently holds the 2 % royalty.

OntZinc later changed its name to HudBay Minerals Inc (Hudbay) after purchasing Hudson's Bay Mining and Smelting in December 2004. Hudbay currently owns Scotia Mine through its wholly-owned subsidiary, ScoZinc Limited.

The author reviewed the sampling results and verified that the sample types and density are adequate for establishing Resources and Reserves. The sampling results are representative of the mineralisation. The available information and sample density allow a reliable estimate to be made of the size, tonnage and grade of the mineralisation in accordance with the level of confidence established by the Mineral Resource categories in the CIM Standards.

The deposit is characterised by complex geometry and is difficult to model in terms of standard techniques. Lying along a 'paleo-shoreline', it features repetitive changes in strike around a general trend of 060º Azimuth, and with varying dip.

For Resource calculation, the deposit was divided into two zones. The Surface Resource Zone, south of Highway 224, includes lower grade, disseminated rock that is amenable to surface mining. The Northeast Underground Zone lies north of the highway. It consists of higher-grade, moderately dipping mineralisation. It lacks the lower grade, disseminated rock, making underground mining more attractive.

For both the Surface and Northeast Underground Zones, manual interpretation was required to properly model the geology. The Surface Zones ore zones were differentiated into a high-grade massive sulphide zone and a low-grade disseminated zone. Drill-hole data and underground openings were then plotted on hard-copy plans at ten metre intervals, and interpretations of the high-grade zone, the low-grade and the hanging-wall 'Trench' were produced. The cut-off grades that were for the high-grade (HG) and low-grade (LG) zones were 7 % Zn-Eq and 2 % Zn-Eq respectively.

The Surface Zone's geometry made it difficult to incorporate the true spatial relationship of the samples for estimation purposes without the use of 'unfolding' techniques that transform the sample data into another co-ordinate space that honours the spatial relationships. Variography and estimation were conducted in the transformed space, and the results are then back-transformed into the original space.

Equal length composites were prepared from uncut assay values in a two step process. Initial composite intervals were defined from the intercepts of the drill holes with the high-grade and

low-grade 3D solids of the mineralised zone. Equal length composites of 1.5 metres were then generated within these intervals – 1.5 metres is approximately the average length of the assay intervals.

Three dimensional experimental correlograms were generated using the transformed (un-folded) Zn and Pb composite data, for both low-grade and high-grade mineralised zones below an elevation of 490 metres (Datum, Mean Sea Level = 500.11 metres). Separate 3D experimental correlograms were generated using un-transformed composite data for the low-grade mineralised zone above 490 metre elevation, where the deposit is essentially horizontal in attitude. Nested correlogram models comprising nugget effect and two spherical components were fitted to all experimental variograms.

No evidence of specific gravity test work was available. Therefore, a formula for specific gravity based on zinc and lead grades was used for the mineralised zones.

Two block models were constructed for interpolation purposes, a primary model in normal (un-transformed) space, and a secondary, smaller model in transformed space for interpolation of the un-folded data.

The standard ordinary kriging (OK) procedure was used to interpolate Zn and Pb block values in the flat lying portions of the deposit above 490 metre elevation. Separate interpolations of Zn and Pb block values for the LG and HG zones were kriged in three passes using ordinary kriging (OK), the transformed composites and the correlograms generated from those composites.

Because it was determined that the Northeast Underground Zone would be most profitably mined using underground mining methods, a cut-off grade of 5 % zinc equivalent was used to outline the mineralisation on sections spaced fifty metres apart. To permit mechanised mining, the minimum mining width and height were both 2.4 metres.

One contiguous body made up the Northeast Underground Resources. To determine the quantity of material, the outline area on each section was multiplied by its strike length (fifty metres) to determine the volume. That figure was multiplied by an average SG of 2.9 to determine mass. To determine grade, the length-weighted average grade and the true width of each intercept was calculated. The average section grade was determined by calculating the true-length-weighted average grade of all of the section's intercepts. The average true width of the intercepts was also calculated.

Using a 0.75 % zinc-equivalent cut-off, the undiluted Surface and Underground Resources were estimated to be:

Mineral Resources

Category	Volume (m^3)	SG	Tonnes	Zinc Grade	Lead Grade
Measured (Surface)	680,000	2.78	1,880,000	3.8%	1.6%
Indicated					
Surface	810,000	2.77	2,250,000	3.2%	1.4%
Underground[1]	381,000	2.90	1,110,000	6.6%	3.7%
Subtotal	1,190,000	2.82	3,360,000	4.3%	2.2%
Measured + Indicated (Surface and Underground)	1,870,000	2.80	5,240,000	4.1%	2.0%
Inferred	652,000	2.76	1,800,000	3.1%	1.1%

Notes:
1. Northeast Underground Zone.
2. Undiluted Resources.

To estimate the Surface Reserves, an optimised pit shell was generated from the block model utilising Whittle 3.4 pit optimisation software. Only blocks in the Measured and Indicated Resource categories were used. A surface mine plan, complete with haul roads, was designed using the optimum pit shells as a guide.

Mine dilution and recovery values were estimated to be 15 % and 90 %, respectively. These values were applied to the Surface Reserves and the Northeast Underground Resources, resulting in the following Reserve estimate:

Mineral Reserves

Category	Volume (m^3)	SG	Tonnes	Zinc Grade	Lead Grade
Proven Reserves (Surface)	630,000	2.78	1,750,000	3.2%	1.3%
Probable Reserves					
Surface	610,000	2.76	1,690,000	2.5%	1.0%
Underground	395,000	2.90	1,150,000	5.7%	3.2%
Subtotal	1,005,000	2.83	2,840,000	3.8%	1.9%
Total Proven and Probable Reserves (Surface and Underground)	1,635,000	2.81	4,590,000	3.6%	1.7%

Notes:
1. Dilution equals 15 % and mining recovery equals 90 %.

The effect of changing metal prices on Surface Reserve size and grade was investigated. Two additional optimum pit shells were generated using plus and minus 25 % of the base case metal prices. The relationship shows that Surface Reserve tonnes drop in an approximately linear manner as the cut-off grade increases:

Zinc Price ($US/lb)	Corresponding Cut-off Grade[1] (Zn-Eq)	Reserve Tonnes	Zinc Grade	Lead Grade	Zn-Eq Grade[2]	Stripping (Tonnes)	Stripping Ratio
$ 0.64	1.20%	2,200,000	3.25%	1.42%	3.86%	17,301,000	7.9
$ 0.85	0.85%	3,321,000	3.30%	1.35%	3.88%	32,855,000	9.9
$ 1.06	0.66%	3,831,000	3.48%	1.46%	4.11%	48,869,000	12.8

Notes:
1. Cut-off grade calculated according to zinc price and base case operating parameters.
2. Zinc-Equivalent equals zinc grade + 0.43 x lead grade.

For the first few years, mining will be by surface methods using standard methods of drilling, blasting, and excavating using excavators and truck haulage. This equipment will be leased from a local dealer. The pit will have an oval shape with its long axis oriented along the northeast-southwest strike of the deposit.

To the northeast, the pit is constrained by Gays River and Highway 224. Gays River will be diverted slightly to allow the pit to expand toward the highway. This was incorporated in the project's environmental registration that was approved in 2000.

After the pit reaches an elevation of approximately 480 metres (approximately 50 metres depth), underground development can begin from a portal in the northeast end of the pit, extending along strike to the northeast.

For underground mining of the Northeast Zone, a main haulage drift will be established on the 480 metre level. It will extend from the pit along strike to the northeast. It will pass underneath the river but it will be entirely situated within the competent footwall quartzites. A second decline and portal will be located at the northeast end of the Northeast Zone to provide a second access for the underground workings.

As part of minimising the operational and safety hazards posed by the hanging wall Trench clay, the groundwater table will be lowered below the active mine workings. The cut-and-fill mining method was chosen specifically to address the weak hanging wall issue. The mining method is a modified form of mechanised cut and fill mining. It is a combination of undercut and fill and conventional (overhand) cut and fill mining. It will be mechanised, meaning drill jumbos will do the development and production drilling. LHD's (Load-Haul-Dump vehicles) will muck the broken rock back to re-muck stockpile bays. In narrower stopes, slushers may be used to muck the broken rock. Underground dump trucks will haul the rock to surface.

When processing lower grade, carbonate ore, the mill performs well at production rates of 2,000 tonnes per day (Thornton, 2006 (1)). A production rate of 2,000 tonnes per day is planned for the surface operation. Operating 350 days per year, that translates to 700,000 tonnes of ore per year. That translates to 85 tonnes of dry zinc concentrate per day (30,000 tonnes per year) with a concentrate grade of 60 % zinc. The lead concentrate production rate will be 29 tonnes per day (10,000 tonnes per year) with a concentrate grade of 75 % lead.

Stripping operations will start at the beginning of the fourth quarter of Year One. Milling will begin two months later, during the eleventh month of Year 1, after a sufficient amount of material has been stockpiled.

Because of the higher grade of the underground ore, a production rate of 1,350 tonnes per day is planned for the underground operation. This is so as not to overwhelm the filtering and drying sections of the mill. Operating 350 days per year, that translates to 472,000 tonnes of ore per year. Because the grades are higher underground, zinc concentrate production during underground mining will increase, despite a slower mine production rate. The zinc

concentrate production rate will be 115 tonnes of dry zinc concentrate per day (40,000 tonnes per year) with a concentrate grade of 60 % zinc. The lead concentrate production rate will increase to 54 tonnes per day (19,000 tonnes per year) with a concentrate grade of 75 % lead.

The on-site processing plant will concentrate zinc and lead in mineral form (sphalerite and galena, respectively). These separate concentrates will be sold to one or more outside smelters within North America or overseas. The Scotia Mine concentrate has very few impurities and is high grade. Currently, world-wide smelter capacity is under-utilised and the demand for concentrate exceeds what the mines can supply. Therefore, there should be no trouble selling the concentrate.

At the time of report writing, spot prices for zinc and lead were both at historically high levels. The zinc and lead spot prices were approximately $US 3,590 ($1.63 per pound) and $US 1,156 per tonne ($0.53 per pound) of refined metal, respectively. The prices of both metals were recovering from near-historic low levels experienced in 2002/2003, when zinc and lead spot prices were approximately $US 800 and $US 500 per tonne of refined metal, respectively.

The following economic and technical parameters were adopted for the base case economic scenario:

Item	Value
Zinc Spot Price ($US/lb)	1.10
Lead Spot Price ($US/lb)	0.40
Zinc Treatment Charge ($US/tonne)	170
Lead Treatment Charge ($US/tonne)	160
Exchange Rate ($US/$CAN)	0.86

Using those values, net yearly revenue (after smelting costs) during the surface mining operation will be $43 million. For the underground operation, yearly revenue will be $60 million.

The purchase price for ScoZinc Limited and all of its assets was $7.5 million. Purchasing Savage's 2 % NSR royalty will cost another $1.45 million at the end of Year 1. General project capital costs include permitting costs, a highway semi-dump truck for concentrate hauling and office equipment. The mill, which has been under a care and maintenance condition for the past fifteen years, must be cleaned-up and re-commissioned. This will require a relatively minor amount of work (compared with building an entirely new mill). The overall capital cost for the surface mining operation, excluding pre-production stripping, is $2.9 million. The surface mobile equipment fleet will be leased.

As the surface mine nears completion in Year 6, the underground mine will start developing. The capital cost for the underground operation is $5.6 million.

Operating the surface mine and processing plant is expected to cost $19 million per year ($27 per tonne of ore or $US 0.34 per pound of zinc-equivalent). Operating the underground mine and processing plant is expected to cost $23 million per year ($49 per tonne of ore or $US 0.30 per pound of zinc-equivalent). The operating cost for Scotia Mine will be competitive with other major producers.

Reclamation will be an on-going process. The goal will be to minimise the overall land disturbance at any point in time. As much as possible, stripped waste rock and soil will be placed in their final resting places. After the mine is decommissioned, it was proposed to allow the pit to fill with ground and surface water to create a deep lake.

For the base case scenario ($US 1.10 per pound zinc, $US 0.40 per pound lead, $US 0.86 exchange rate), the economic analysis indicated that the project is very profitable. The project's after-tax, net present value using a 8 % discount rate ($NPV_{8\%}$) was $73.6 million. The internal rate of return was 76 %. The payback period was twenty-one months. The profitability using other discount rates was:

$NPV_{7.5\%}$	$	75,687,000
$NPV_{8.0\%}$	$	73,628,000
$NPV_{10.0\%}$	$	66,028,000
$NPV_{12.5\%}$	$	57,789,000
$NPV_{15.0\%}$	$	50,723,000
Internal Rate of Return (IRR)		76%

The surface operation will last almost six years. The underground operation will last more than two years for a total mine life of just over eight years. The best possibility for extending the mine life lies with the adjacent Getty Deposit. There are also In-pit Inferred Resources that could extend the surface mine life.

A sensitivity analysis was carried out to determine the sensitivity of the project's profitability to changes in metal prices, mine dilution, grade, initial capital costs, operating costs and exchange rate. The profitability indicators that were observed were the project's net present value using a 8 % discount rate ($NPV_{8\%}$) and the project's internal rate of return (IRR). For both the surface and underground operations, the greatest risk for project profitability is metal price fluctuation. The best methods for controlling this risk are mining as quickly as possible and selling forward (hedging) while prices are high.

Water inflow to the underground workings provides a less quantifiable, technical risk to the underground portion of the project. The modified undercut-and-fill mining method that has been adopted for this deposit was designed for very poor ground conditions and offers a high level of protection against potentially unstable ground. Other measures, such as lowering the groundwater table below the level of the mine workings, will also be taken to further alleviate the risk.

Table of Contents

1. Introduction 1
1.1 Terms of Reference 1
1.2 Purpose of Report 1
1.3 Sources of Information 1
1.4 Extent of Field Involvement of the Qualified Person(s) 1
1.5 Units of Measure 2
1.6 Site Grid Parameters 2
2. Disclaimer 2
3. Property Description and Location 3
3.1 Exploration Licences 4
3.2 Mineral Lease 5
3.3 Surface Rights (Real Property) 6
3.4 Aggregate Leases 7
3.5 Environmental Liabilities 7
3.6 Environmental Permitting Work 8
4. Accessibility, Climate, Local Resources, Infrastructure and Physiography 9
5. History 12
5.1 Historical Mineral Resource and Mineral Reserve Estimates 14
6. Regional Geology and Mineralisation 16
7. Property Geology and Mineralisation 19
8. Deposit Type 25
9. Mineralisation 26
10. Exploration History 26
11. Drilling 33
11.1 Sample Statistics 37
12. Sampling Method and Approach 39
13. Sample Preparation, Analysis and Security 40
14. Data Verification 40
14.1 Database Validation 41
14.1.1 Methodology 41
14.1.2 Results 41
14.1.3 Conclusion 42
14.2 Verification Sampling 42
15. Adjacent Properties – Getty Deposit 44
15.1 Geology 44
15.2 Mineralisation 45
16. Mineral Processing and Metallurgical Test Work 46
17. Resources 47
17.1 Surface Resources 47
17.1.1 General 47
17.1.2 3-D Surface and Solids Modelling 47
17.1.3 “Unfolding” Process 48
17.1.4 Drillhole Data 50
17.1.5 Mineralised Envelope 50

17.1.6 Statistical Analysis and Capping 50
17.1.7 Compositing 54
17.1.8 Variography 54
17.1.9 Specific Gravity/Density 59
17.1.10 Block Model and Grade Interpolation 59
17.1.11 Mineral Resource Classification 63
17.1.12 Results 65
17.2 Underground Resources – Northeast Zone 67
17.3 Gypsum 73
18. Reserves 76
18.1 Surface Reserves 76
18.2 Underground Reserves – Northeast Zone 82
19. Additional Requirements for Technical Reports on Development Properties and Production Properties – Feasiblity Analysis 84
19.1 Mining Operations 84
19.1.1 Initial Surface Mining 84
19.1.2 Underground Mining 84
19.1.3 Dewatering 86
19.2 Mine Dilution and Recovery 86
19.3 Mineral Processing Operations 87
19.3.1 Production Forecast 89
19.3.2 Recoverability 89
19.4 Geotechnical Aspects 90
19.4.1 Underground Geotechnical Investigation of Trench Material 92
19.5 Mine Water and River Diversion 92
19.6 Markets 93
19.6.1 Gypsum Market 94
19.7 Contracts 95
19.7.1 Smelter Returns 95
19.7.2 Spot Prices 96
19.7.3 Futures Markets 102
19.8 Water and Sewer 103
19.9 Environmental Considerations 103
19.9.1 Progressive Reclamation 103
19.9.2 Final Reclamation 103
19.10 Revenue 105
19.11 Taxes and Royalties 105
19.11.1 Taxes 105
19.11.2 Royalties 106
19.12 Capital Cost Estimates 106
19.13 Operating Cost Estimates 107
19.13.1 Labour 107
19.13.2 Electric Power 110
19.13.3 Ongoing Development 110
19.13.4 Yearly Operating Costs 110
19.14 Timing of Cash Flows 112

19.15 Working Capital 112
19.16 Financing 113
19.17 Economic Analysis 113
19.18 Sensitivity Analysis 117
19.19 Discussion of Risks 119
19.20 Payback Period 119
19.21 Mine Life 120
20. Conclusions 121
21. Recommendations 121
22. References 122

Appendix 1: Westminer monthly mill report for November, 1990.
Appendix 2: Mineral lease and exploration licence claims and ownership history
Appendix 3: Real property titles and lease agreements.
Appendix 4: Surface Reserves.
Appendix 6: Economic analysis.
Appendix 7: Diamond drill hole logs.

Index of Figures

Figure 1: Location Map, Gays River, Nova Scotia. 3
Figure 2: Location relative to Halifax. 4
Figure 3: Claim Reference Map 11E03B showing exploration licences, mineral lease and real property boundary (surface rights). 7
Figure 4: Site infrastructure (facing northwest). 11
Figure 5: Tailings pond (facing south). 12
Figure 6: Decline and portal access to the underground workings (circa 1990). 13
Figure 7: Flotation circuit (circa 1990). 13
Figure 8: Regional geology. 18
Figure 9: Stratigraphy. 20
Figure 10: Bottom of carbonate (top of Goldenville quartzite) contours. 21
Figure 11: Section A---A′. 22
Figure 12: Section B---B′. 23
Figure 13: Section C---C′. 24
Figure 14: Plan map of diamond drill holes. 34
Figure 15: Plan map of diamond drill holes that ScoZinc drilled in 2004. 35
Figure 16: 3D Polyline slabs and axes. 49
Figure 17: Zn and Pb assay lognormal histograms. 52
Figure 18: Zn and Pb assay probability plots. 53
Figure 19: Composite statistics and histograms 55
Figure 20: Experimental and model correlograms 56
Figure 21: 3D view - transformation and block model definition. 61
Figure 22: Transformation - plan view. 61
Figure 23: Plan section through the block model on the 460 metre level. 64

Figure 24: Cross-section through Row 208 of the block model, facing northeast. 65
Figure 25: Grade-tonnage curve for Measured and Indicated surface Resources (undiluted). 67
Figure 26: Site plan showing Northeast Zone Reserves and proposed underground development. 69
Figure 27: Section 6650 Through Northeast Zone Reserves. 70
Figure 28: Section 7050 Through Northeast Zone Reserves. 71
Figure 29: Section 7250 Through Northeast Zone Reserves. 72
Figure 30: Gypsum and chloride histograms. 75
Figure 31: Site layout showing planned mining. 78
Figure 32: Grade-tonnage relationship for diluted and recoverable, Proven and Probable Surface Reserves. 81
Figure 33: Undiluted Proven + Probable Reserves, above 0.75 % zinc-equivalent, at various cut-off grades. 82
Figure 34: Cross-sectional conceptual schematic of modified mechanised cut-and-fill mining method (showing lift sequence). 86
Figure 35: Views of the outside (left) and inside (right) of the mill. 87
Figure 36: Process flowsheet. 88
Figure 37: LME spot price history for zinc ($US per tonne of refined zinc). 97
Figure 38: LME spot price history for lead ($US per tonne of refined lead). 98
Figure 39: Conceptual reclamation plan (CBCL, 1999). 104
Figure 40: Zinc producer cost curve for 2005 (RBC, 2005). 111
Figure 41: Sensitivity analysis. 117
Figure 42: Project payback period according to cumulative net income after interest and taxes. 120

Index of Tables

Table 1: Site grid parameters. 2
Table 2: Exploration Licence No. 06268 (28 claims). 4
Table 3: Exploration Licence No. 06304 (one claim). 5
Table 4: Exploration Licence No. 06303 (five claims). 5
Table 5: Exploration Licence No. 05851 (15 claims). 5
Table 6: Exploration Licence No. 05792 (42 claims). 5
Table 7: Claims comprising Mineral Lease 90-1. 6
Table 8: Property ownership, ScoZinc Limited. 6
Table 9: Historical milling records. 12
Table 10: Recent historical resource and reserve estimates. 16
Table 11: Historical Surface and Underground Diamond Drilling Activity. 36
Table 12: Descriptive statistics. 37
Table 13: Sample histograms. 38
Table 14: Holes that were verified during the database validation. 41
Table 15: Results of verification sampling. 43
Table 16: Metallurgical balance. 46
Table 17: Correlogram models. 54

Table 18: Undiluted surface Resources. 66
Table 19: Underground resources (Northeast Underground Zone). 68
Table 20: Resources summary (0.75 % zinc-equivalent cut-off grade). 68
Table 21: Raw (non-weighted) assay statistics. 74
Table 22: Surface Reserves. 79
Table 23: Northeast Zone Probable Diluted & Recoverable Reserves. 83
Table 24: Reserves summary (Proven & Probable, diluted and recoverable Surface and Underground Reserves). 83
Table 25: Equipment list for the surface mine. 84
Table 26: Yearly production forecast. 89
Table 27: Mineral processing parameters. 90
Table 28: Prediction of metal prices to 2012 (Roberts, 2006). 99
Table 29: Summary of zinc mine production changes (kilotonnes) (RBC, 2005). 99
Table 30: Production expansions at existing mines and approved projects (kilotonnes) (RBC, 2005). 100
Table 31: Production expansions at potential zinc mine projects (kilotonnes) (RBC, 2005). 101
Table 32: Production reductions at existing zinc mines (kilotonnes) (RBC, 2005). 101
Table 33: Zinc price prediction to 2009 (RBC, 2005). 102
Table 34: Adopted metal price, treatment charge and exchange rate model. 102
Table 35: LME spot and futures prices for July 13, 2006 [$US per tonne of refined metal ($US per pound)]. 103
Table 36: Capital costs. 107
Table 37: Staffing requirements. 109
Table 38: Summary of labour force. Salaries include burden. 110
Table 39: Average yearly operating cost estimate for the surface mining operation. 111
Table 40: Average yearly operating cost estimate during underground mining. 111
Table 41: Timing of cash flows. 112
Table 42: Required project financing. 113
Table 43: Accounting income. 114
Table 44: Sensitivity analysis. 118
Table 45: Sensitivity of the project's profitability to changes in metal prices. 118

Acadian Gold Corp
Resource, Reserve and Feasibility Report for the Purchase and Operation of Scotia Mine
Gays River, Nova Scotia

1. Introduction

1.1 Terms of Reference

Mr Will Felderhof, President of Acadian Gold Corp (ADA, TSX-V) based in Halifax, Canada engaged MineTech International Limited on December 21, 2005 to complete a National Instrument 43-101-compliant resource and reserve estimate. The economic analysis of the proposed operation was to be of feasibility study accuracy, or plus-or-minus ten percent.

1.2 Purpose of Report

The purpose this report was to provide a complete, independent, resource and reserve report conforming to NI 43-101 standards and Form 43-101F. The report was to determine the feasibility of exploiting Scotia Mine Resources using a combination of surface and underground mining methods.

1.3 Sources of Information

This report is based, in part, on internal company technical reports and maps, published government reports, company letters and memoranda, and public information as listed in the "References" section at the conclusion of this report. Several sections from reports authored by other consultants have been directly quoted in this report, and are so indicated in the appropriate sections.

Digitised and hard copy material for all exploration activity since inception of exploration on the property was supplied by Hudbay.

1.4 Extent of Field Involvement of the Qualified Person(s)

Mr. Douglas Roy, M.A.Sc., P.Eng., who was the Principal Author of this report, is a Qualified Person under Section 1.1 of National Instrument 43-101. As an independent contractor, he supervised surface exploration work, including diamond drilling and trenching, on the Scotia Mine site during 2004. Mr. Roy spotted many of the holes and logged the core for ScoZinc's twenty-five hole program that they carried out in 2004.

Mr. Tim Carew (M.Sc., Geology, P.Geo.) visited the mine site in 1998. The visit was part of a resource estimate that was carried out by Savage Resources Canada. Mr. Carew is a Qualified Person under Section 1.1 of National Instrument 43-101.

Mr. Reg Comeau (M.Sc., Geology, P.Geo.) visited the mine site and offices of ScoZinc and the Nova Scotia Department of Natural Resources on June 17, June 21, September 22 and September 27 to familiarize himself with the data and collect core samples from two separate drilling campaigns (1997 and 2004) for data verification. Discussions were carried out with respect to the property with representatives of ScoZinc including Mr. Patrick Hannon, P. Eng. (President of ScoZinc). Mr. Comeau is a Qualified Person under Section 1.1 of National Instrument 43-101.

1.5 Units of Measure

Unless otherwise stated, all units used in this report are metric. Unless otherwise stated, the legal currency used is the Canadian dollar.

1.6 Site Grid Parameters

A site grid was used throughout the report. The grid is a simple translation with almost no rotational deviation from the Nova Scotia Grid, which is a 3 ° Modified Transverse Mercator projection using an ATS 77 datum. The site grid elevation datum is 500.11 metres above Mean Sea Level. For reference, the co-ordinates of two points, in both site and Nova Scotia grids, are reported in Table 1.

Table 1: Site grid parameters.

Site Control	Site Grid			Nova Scotia Grid		
Monument	North (m)	East (m)	Elev. (m)	North (m)	East (m)	Elev. (m)
No. 4	6,869.72	8,597.50	531.33	4,988,509.11	5,591,210.89	31.25
No. 7	7,019.95	8,866.55	530.69	4,988,659.37	5,591,479.94	30.58

2. Disclaimer

MineTech has assumed that all the information and technical documents listed in the References section of this report are accurate and complete in all material aspects. While all of the available information that was presented was carefully reviewed and believed to be correct, MineTech cannot guarantee its accuracy and completeness. MineTech reserves the right, but will not be obligated to revise this report and conclusions if additional information becomes known subsequent to the date of this report.

The authors relied on Colleen Keyes of McInnes Cooper, Barristers and Solicitors, Halifax, Canada to carry out title searches on the mineral exploration properties surrounding Mineral Lease 90-1 and the real property (surface rights) (Section 3). The authors also relied on Peter Oram of Conestoga-Rovers & Associates Ltd, Halifax, Canada to carry out a Phase I Environmental Site Assessment that forms the basis of Section 3.6 and Section 19.9.

The authors have relied largely on the documents listed in the Sources of Information and the site visits for the information in this report. However, the conclusions and recommendations are exclusively the principal author's. The results and opinions outlined in this report are dependent on the aforementioned information being current, accurate and complete as of the date of this report and it has been assumed that no information has been withheld which would impact the conclusions or recommendations made herein.

3. Property Description and Location

The Scotia Mine property is located approximately sixty kilometres northeast of Halifax, Nova Scotia and one kilometre east of the community of Gays River in the Halifax Regional Municipality. The property's general location is 45°02′ North, 63°20′ West. It consists of 615 hectares of mineral rights, including land with exploration potential for zinc/lead mineralisation, and 568.4 hectares of land ownership (real property) (Figure 1 and Figure 2).

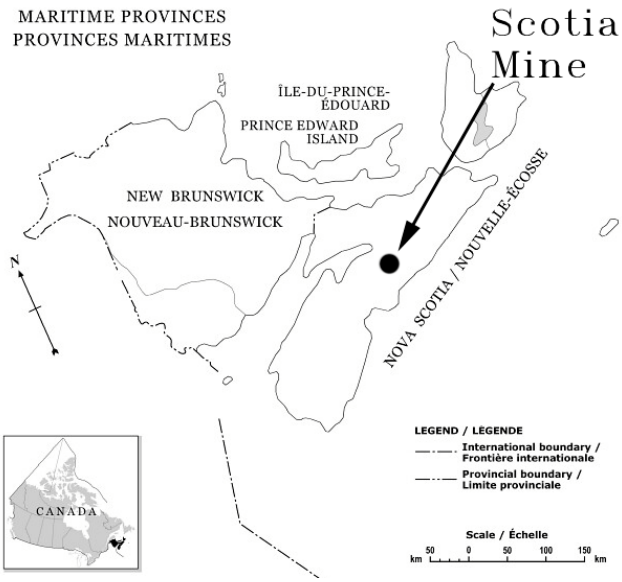

Figure 1: Location Map, Gays River, Nova Scotia.

Figure 2: Location relative to Halifax.

3.1 Exploration Licences

The ScoZinc land package also includes five exploration licenses in the general vicinity of the mine (Figure 3). Each individual claim covers an area of forty acres (16.2 hectares). In total, the 91 claims cover 3,640 acres (1,473 hectares). These licenses are located along strike from the Scotia Mine deposit and include favourable host rocks similar to that at the mine site. All lands were in good standing and were registered to ScoZinc Limited as of July 13, 2006. The range in anniversary dates is from May 2, 2006 (with a renewal application pending) for Licence No. 06268 to November 5, 2006 for Licence No. 05851. Table 2 through Table 6 report the exploration licences and individual claims.

Table 2: Exploration Licence No. 06268 (28 claims).

Claims	Tract	Claim Reference Map	Anniversary Date
ABCD EFGH LMN	19	11E3B	May 2, 2006
ABC EFGH	18	11E3B	Renewal
DE JKLM NOPQ	7	11E3B	Application Pending

Table 3: Exploration Licence No. 06304 (one claim).

Claim	Tract	Claim Reference Map	Anniversary Date
E	29	11E3B	Oct 13, 2006

Table 4: Exploration Licence No. 06303 (five claims).

Claims	Tract	Claim Reference Map	Anniversary Date
LMNOP	29	11E3B	Oct 25, 2006

Table 5: Exploration Licence No. 05851 (15 claims).

Claims	Tract	Claim Reference Map	Anniversary Date
FGH JK OPQ	45	11E3B	Nov. 5, 2006
EFG KM	46	11E3B	

Table 6: Exploration Licence No. 05792 (42 claims).

Claims	Tract	Claim Reference Map	Anniversary Date
DE MN	42	11E3B	Jan 20, 2007
ABCD EFGH JKM NOPQ	41	11E3B	
EF LM NO	32	11E3B	
ABCD EFGH JKM NOPQ	33	11E3B	

3.2 Mineral Lease

Mineral Lease #90-1, which covers the entire mine site, was originally granted by the Nova Scotia Government to Westminer Canada Limited on April 2, 1990. It was originally granted as a "Mining Lease." However, changes to the Nova Scotia Mineral Resources Act that came into effect in November 2004 changed the terminology such that existing "Mining Leases" are now known as "Mineral Leases."

The anniversary date (review date) of Mineral Lease #90-1 is April 2 of each year. Table 7 lists the claims comprising the Mineral Lease. Figure 3 shows its location. The lease conveys the rights to all minerals except coal, uranium, salt and potash. The lease was transferred to Savage Resources in 1996 and later to Pasminco Resources Canada Company in 1999. It was finally transferred to ScoZinc in 2002. Savage retains a 2 % net smelter return royalty. Acadian has entered into an option agreement that would enable it to purchase the royalty for $1.45 million. The duration of the lease is twenty years, at which time it may be renewed.

Table 7: Claims comprising Mineral Lease 90-1.

Tract Map (NTS) 11E-3B

Tract	Claims	Number of Claims
5	NOP	3
19	JKPQ	4
20	BCDE FGK LMNO PQ	13
28	DEKL MNOP	8
29	ABCD FGH JKQ	10
Total		**38**

3.3 Surface Rights (Real Property)

ScoZinc owns outright approximately 568 hectares (1,404.6 acres) of land (real property) containing the entire surface infrastructure; the tailings area and most of the outlined mineralisation (Table 8 and Figure 3). The boundaries were established through legal surveys. Details of a title search on the ScoZinc's real property are reported in Appendix 3.

Table 8: Property ownership, ScoZinc Limited.

Property ID #	Acres	Hectares
00369363	50.0	20.2
00522623	90.0	36.4
20080495	49.0	19.8
20080529	10.0	4.0
20158176	8.7	3.5
20158184	4.4	1.8
20223400	6.0	2.4
20223413	3.0	1.2
20313250	4.5	1.8
20416384	1.6	0.6
40227936	3.0	1.2
40227951	7.5	3.0
40757577	115.4	46.7
40227963	181.3	73.4
40227985	5.6	2.3
40290256	0.72	0.3
40227963	171.8	69.5
40290264	110.0	44.5
40291452	544.6	220.4
40292553	4.5	1.8
40312092	33.0	13.4
Total	**1,404.59**	**568.4**

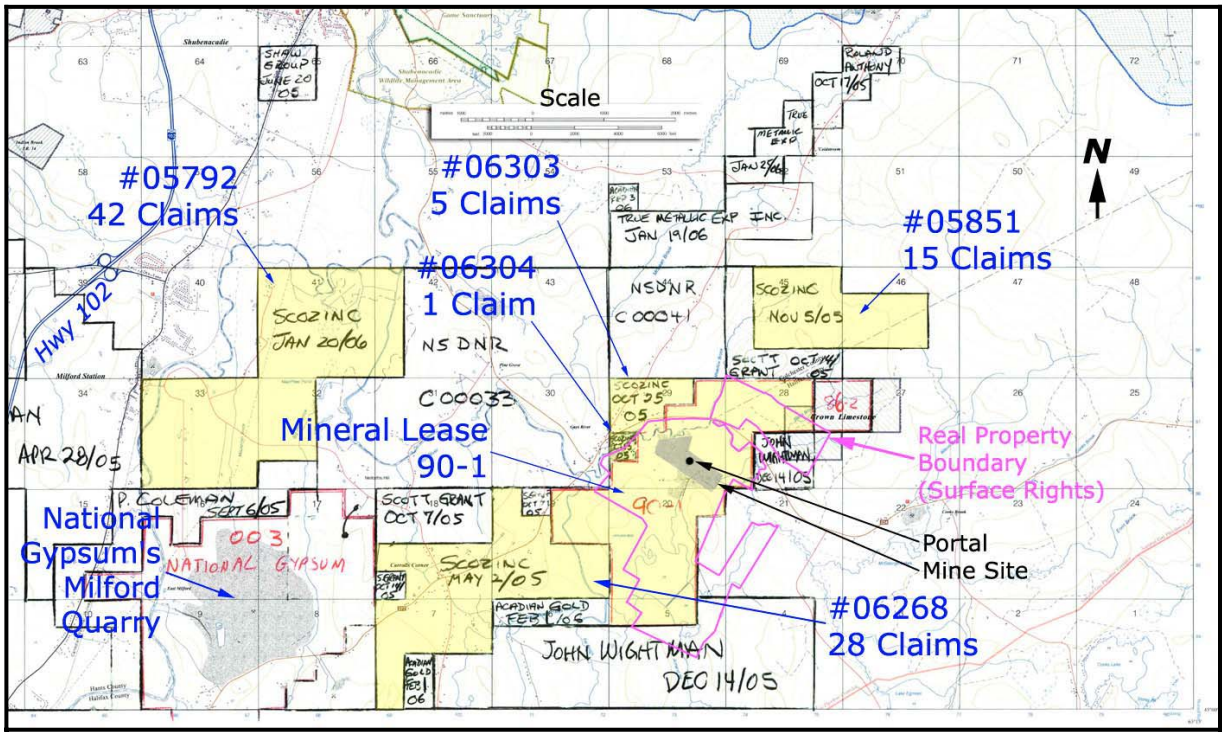

Figure 3: Claim Reference Map 11E03B showing exploration licences, mineral lease and real property boundary (surface rights).

3.4 Aggregate Leases

Gallant Aggregates signed a thirty-year lease agreement to mine and remove aggregate from the property for one dollar per tonne of material that is removed from the property. The lease was signed on May 15, 2003 and entitles Gallant, with certain limitations, to mine anywhere on ScoZinc's land. The agreement contains a renewal clause and gives Gallant the right of first refusal to purchase the surface rights (real property titles). A major condition of Gallant's lease is that metal mining takes precedence over aggregate mining. Therefore, Gallant's lease will not interfere with zinc and lead mining operations.

Another, older agreement was made between Seabright and Nova Recreation Development Company Limited (Nova) on December 19, 1985. The 99-year lease gave Nova the right to mine and process sand on ScoZinc's land. Two million tonnes of sand would be left for Seabright's use. Again, the agreement stated that metal mining takes precedence over sand mining. A copy of this lease is attached in Appendix 3.

3.5 Environmental Liabilities

An updated Phase I ESA was carried out in conjunction with this Resource/Reserve report. It was completed in March, 2006 by Conestoga-Rovers & Associates (CRA). CRA (then MGI Limited) also carried out a Phase I ESA in 1996. The updated assessment included several site inspections, during which the following, relatively minor liabilities were identified.

Solid waste (garbage) is currently collected and taken to a local landfill. A former on-site landfill is located southwest of the mill. It was abandoned in 1991 and covered with clay till. There is also a scrap yard (bone yard) next to the abandoned landfill. It contains mainly steel refuse, but there are several containers and drums with unknown contents.

The laboratory, located in the mill, contains many containers filled with chemicals, some with unknown contents.

There are several fuel and oil storage tanks both above ground and underground. There is no evidence that these tanks are leaking, but their condition must be assessed before operations begin.

3.6 Environmental Permitting Work

A number of reports regarding the environmental conditions at the Scotia Mine site have been completed since the deposit's discovery in the 1970's. These were reviewed as part of the initial Phase I Environmental Site Assessment (ESA) that was completed in 1996.

An updated Phase I ESA, carried out in conjunction with this Resource/Reserve report, was completed in March, 2006 by Conestoga-Rovers & Associates (CRA). They reported that the following environmental or related permits have been issued for the Scotia Mine site:

1. Industrial Waste Discharge Permit (IWDP) #88-073, a Milling Permit for Full Scale Operations at the Gays River Mill, 1990.
2. IWDP #90-007, Lead/Zinc Mine and Mill, 1990;
3. IWDP #90-023, Transhipment of Lead/Zinc Concentrates from Gays River Mine to Sheet Harbour, 1990;
4. NSDOE Water Rights Permit Authorisation #2891 and #2892 for Water Withdrawal from Annand Brook and Gays River, respectively;
5. Excavation Permit E-118 issued September, 1997;
6. Environmental Assessment Approval for full-scale Surface and Underground mining operations; and,
7. Environmental Approval #2003-037381, issued December 10, 2003 to Gallant Aggregates to construct, operate and reclaim a sand pit on site.

Item 1, the milling permit stipulated that liquid effluent, sound level, and particulate emission monitoring at several stations be carried out. The monitoring requirements have been fulfilled, and all parameters have been within limits, since the permit was issued in 1990. Under the terms of the latest version of Nova Scotia's Mineral Resources Act, milling permits no longer exist. The requirements that had been covered by a milling permit are now included under the Industrial Approval.

Item 2, an IWDP, was almost identical to Item 1, with the addition of total fecal coliform testing, blast monitoring, and waste oil handling stipulations. An amendment to this permit was issued April 20, 1998 to return the mine to "care and maintenance" status. The requirements included maintaining annual groundwater and effluent monitoring starting in October, 1998. Those monitoring activities have been maintained to the present day.

Item 3, regarding concentrate shipment to Sheet Harbour, dealt with the prevention and clean-up of concentrate spills.

Item 4, regarding water rights permits, dealt with limits for withdrawing water from Annand Brook (between the tailings pond discharge and Gays River (Main Branch)) and Gays River (Main Branch). The limits were 2650 and 1210 litres per minute. They both expire on December 31, 2006.

Item 6 had to do with the environmental registration of a proposed surface and underground mine. Between 1997 and 2000 work proceeded on an Environmental Registration Document. This document, which was submitted with the regulatory authorities in September 1999, addressed the environmental concerns of a surface and underground mining operation along with the diversion of a 500 metre section of the Gays River to accommodate the pit design. On August 4, 2000 the Open Pit Lead/Zinc Mine and River Diversion Project proposed by Pasminco Resources Canada Company received environmental assessment approval. The approval is still in place; however, because six years have elapsed since approval was granted, the environmental registration document will likely need to be updated before mining can begin. This update will address whether the existing environment has changed since 2000.

Before mining can begin, the existing Industrial Approval for the site must be returned to operating status from its current “care and maintenance” status. This should be relatively straightforward process because the proposed operation is nearly identical to the operation for which the Industrial Approval was originally granted.

The Industrial Approval and Environmental Registration documents are the only environmental permits that are to start production. It will require approximately six months to update those documents.

4. Accessibility, Climate, Local Resources, Infrastructure and Physiography

The Scotia Mine property is located approximately fifty-five kilometres northeast of Halifax, Nova Scotia along the border between Colchester and Halifax Counties (45º01'55" North Latitude and 63º21'30" West Longitude). It lies approximately one kilometre east of the community of Gays River. Access to the property is by paved roads and is approximately fifteen kilometres off the Trans Canada Highway along Route #224. The Halifax International Airport is located twenty kilometres southwest of the mine site.

A portion of Highway #224 is subjected to Spring weight restrictions. Truck weights are limited for a period that normally lasts six weeks.

The site lies along the south side of the Gays River main branch, immediately east of the confluence with the Gays River south branch. The deposit is in a rural-residential area of central Nova Scotia that is typified by rolling topography and abundant surface water.

Descriptions of the climate at the site are reported as average data collected at the Halifax International Airport. Climate is variable because of mixed continental and maritime weather patterns. Mean annual temperature is 5.9 ºC, mean annual precipitation is 1,250 mm and yearly evapo-transpiration is estimated to be 560 mm. The relatively mild climate (for Canada) permits year-round operations.

The Gays River watershed is characterised by gently rolling topography, having a maximum elevation of 170 metres, an extensive cover of deciduous forest, a small population and local agricultural land development. Lakes, ponds and rivers are sparsely distributed throughout the watershed. Typical vegetation consists of northern black spruce, balsam fir and juniper with birch in more wet areas. Areas of open bog occur on part of the claims. Currently, parts of the forest are being harvested or thinned.

The Scotia Mine mill, designed and built in 1978/1979 has a nominal capacity of 1,350 tonnes per day (Figure 4). It was initially built to treat the zinc/lead ore from the Gays River Mine. In 1986, it was modified to treat gold ores using gravity and flotation circuits. In 1989, it was again reworked to treat zinc/lead ore from the Scotia Mine then being operated by Westminer Canada Ltd. ("WMC"). The concentrator has been properly maintained and is ready for quick start-up at minimum cost.

The mill is equipped with two stage crushing, two stage grinding, flotation cells, thickening, disk filtration and rotary kiln concentrate drying. The concentrator building contains a complete analytical laboratory, metallurgical testing laboratory, control room, maintenance area and office facilities. Its total area is approximately 32,000 square feet.

The administration building has an area of approximately 26,000 square feet. It contains offices, a dry, warehouses, workshops, a large boardroom, several heavy equipment bays. Other, smaller surface facilities include:

- a compressor building (1,600 square feet);
- a tire shop (2,000 square feet);
- a welding shop;
- a geology building;
- a core shed; and,
- several shipping containers.

Storage and ship loading facilities for lead and zinc concentrates are available at the seaport of Sheet Harbour, a distance of eighty kilometres from the mine site over paved roads. ScoZinc does not own these facilities, but Westminer used them in 1990. Sheet Harbour is a natural harbour on the Atlantic coast that remains ice free in the winter months and can handle vessels up to 40,000 tonnes in displacement. Rail transport facilities have also been used for concentrate shipping. A railway siding is located in Milford, eight road-kilometres from the site. The 500 tonne per hour ship loader that had been installed at the wharf in Sheet Harbour was dismantled in 2005 and brought to the Scotia Mine site.

The existing surface rights are sufficient for mining operations.

Power is supplied through the regional grid at reasonable rates. Scotia Mine owns and maintains step-down transformers adjacent to the mill.

Most of the mill's water requirements are satisfied by in-process recycling. Make-up water is drawn from the perennial Gays River.

The existing tailings pond is large enough for the life of the proposed operation. It is located just south of the mill on the footwall side of the deposit. Its design capacity was ten million tonnes. Just over one million tonnes of tailings have been stored there, leaving a current capacity of over eight million tonnes. The proposed operation will generate just over six million tonnes of tailings over the project's life.

There is sufficient area for waste rock and overburden storage on the property. The main area for waste rock storage lies adjacent to the tailings pond on its northwest shore, on the footwall side of the deposit.

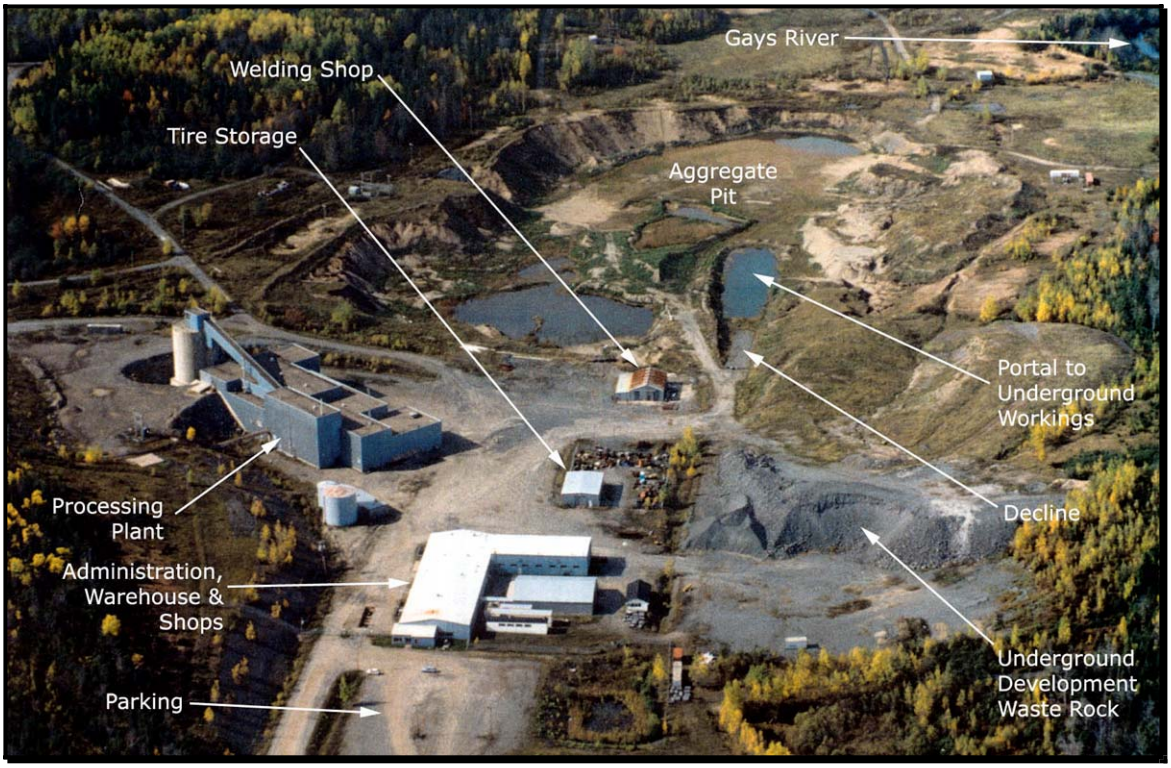

Figure 4: Site infrastructure (facing northwest).

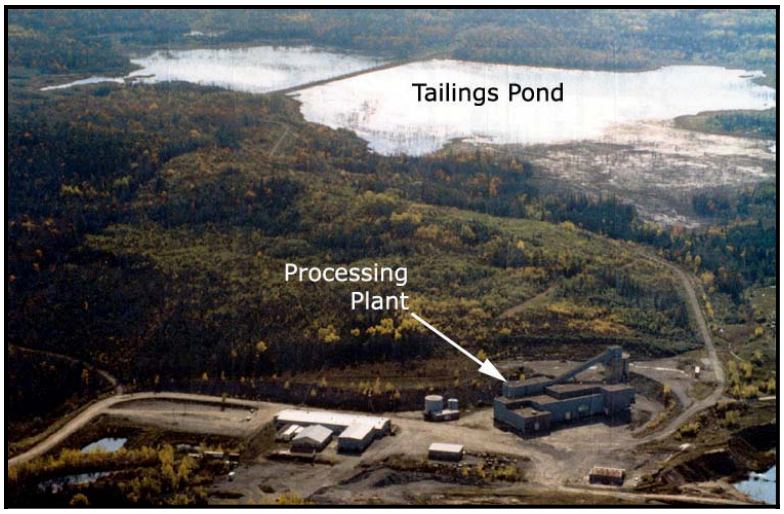

Figure 5: Tailings pond (facing south).

5. History

The history of the project begins with its discovery in the early 1970's by Cuvier Mines. Cuvier and Imperial Oil Limited (ESSO) carried out exploration work and delineated the mineralised zone which was then identified as being four kilometres long, 220 metres wide with depths varying from 20 to 200 metres. Initial development consisted of an exploration decline driven in 1975/76 with mine development starting in 1978 and mill commissioning in October 1979.

From 1979 until 1981, ESSO operated the mine and targeted the lower grade ore using a lower cost, bulk room and pillar mining method approach. The higher grade mineralisation near the carbonate contact was not part of the mine plan at that time. During this period, 554,000 tonnes of lead/zinc ore was mined with and average grade of 2.12 % zinc and 1.36 % lead (Table 9). Due to low metal prices, problems caused by high rates of water influx and difficult ground conditions, mining was suspended in 1981 and the mine was allowed to flood.

Table 9: Historical milling records.

	Mill Feed			Concentrate Produced				Metal Recovery	
	Tonnes	% Pb	% Zn	Pb Tonnes	Zn Tonnes	% Pb	% Zn	% Pb	% Zn
Esso (1979-1981)	550,000	1.4	2.1	10,000	17,000	73.60	61.50	95.30	89.70
WMC (1989-1991)	190,000	3.5	7.5	8,000	21,000	75.60	61.20	90.90	88.90
Total	740,000	1.9	3.5	18,000	38,000			93.25	89.27

In 1985, Seabright Resources purchased the property and modified the mill circuits to treat gold ore from other Nova Scotian properties.

In 1988, Westminer Canada Limited (WMC) purchased Seabright Resources. WMC began dewatering the underground mine in 1989. Their extraction method was to use narrow vein, cut and fill mining to extract the higher grade ore zones. The mine was placed back into operation and reached commercial production in March 1990 (Figure 6 and Figure 7). During the period of operations by WMC, August 1989 to May 1991, the mine produced 190,000 tonnes of ore at an average grade of 7.5 % zinc and 3.5 % lead. Mining was curtailed due to low metal prices, mining method problems and high rates of water influx. Also, for corporate reasons, WMC decided to focus on larger scale mining ventures. Following suspension of mining at Gays River Mine, WMC commissioned several studies to characterise the local hydrology of the mine and to control the ground water in the mine. These results were never tested during mining, since a cyclic low in metal prices, among other factors, prompted WMC to place the property for sale.

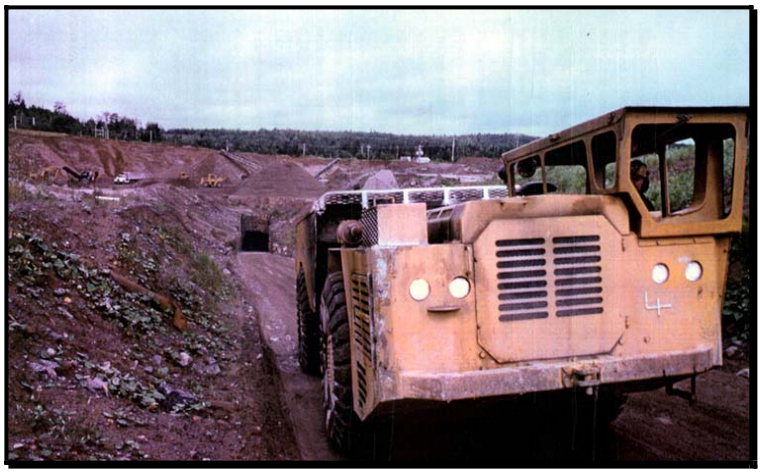

Figure 6: Decline and portal access to the underground workings (circa 1990).

Figure 7: Flotation circuit (circa 1990).

In late 1996, Savage Zinc, Inc. purchased the Gays River Mine property from WMC and formed a wholly owned subsidiary named Savage Resources Canada Company (Savage). Savage started to rehabilitate the property, shops, equipment and office with the aim of starting production in 1997.

When Savage took over the operation of the former Gays River mining facility, the underground workings were flooded to the surface. After purchasing equipment and hiring employees, the mine dewatering phase started on June 7, 1997. With an installed pumping capacity of 9,000 USGPM, the average pumping rate to reach the 425 metre level was 5,200 USGPM. This level was reached during late August 1997. During this period of dewatering, men and equipment went underground to clean out the workings while management carefully examined the ground conditions. They decided to prepare a mine plan that considered an open pit design. Later, after much review during a period of depressed metal prices, it was decided to abandon the proposed underground mining activities and keep the mine dewatered to the 425 level. The electrical equipment was removed and the pumps were shut off on April 1, 1998. At present the mine is flooded above the portal.

Savage concluded that an open pit operation was feasible and initiated environmental permitting, including provisions for a diversion of a portion of the Gays River. The environmental assessment plan was approved August 2000. The operating plan was never initiated.

A detailed account of the Mineral Lease and exploration claim history is reported in Appendix 2.

5.1 Historical Mineral Resource and Mineral Reserve Estimates[1]

Numerous resource estimates have been carried out over the past thirty years since the discovery of the Scotia Mine mineralisation. These resource estimates have been based on differing underlying parameters including varying minimum thickness of intercept, differing cut-off grades, utilisation of zinc equivalent or independent lead and zinc minimum grades, etc. Resource figures have ranged throughout the years from an initial 12,000,000 tons at 7 % zinc-equivalent (drill-indicated) in 1974 (Patterson, 1993) to the 1985 figure of 980,000 tonnes at 5.35 % lead and 9.42% zinc (mineable) at a 7 % zinc-equivalent cut-off (Hale and Adams, 1985).

Westminer (Nesbitt Thompson, 1991; WMC, 1995) reported resources that were outlined by over 1,300 underground and surface holes in addition to the information derived from the underground workings. The calculations were based on a minimum true thickness of two metres with a cut-off of 7 % zinc-equivalent. The total geologic reserves were quoted as 2,400,000 tonnes averaging 6.3 % Pb and 8.7 % Zn (Table 10). A mineable reserve was also quoted as 1,370,000 tonnes averaging 5.3 % Pb and 9.8 % Zn.

[1] The resource estimates referred to in this section are historical in nature and are quoted as such. These estimates have not been reviewed by the authors of this report and thus should not be relied upon.

In 1992, Campbell, Thomas and Hudgins reported that there was potential for mining an additional 800,000 tonnes of lower grade mineralisation via open pit methods. The authors went on to say "there is excellent potential to expand the underground reserves, particularly in the eastern section of the mine. Underground development in the western and central zones resulted in significant expansion of the reserves as ore zone continuity has generally been better than had been originally interpreted from the drill information."

The most recent resource and reserve estimate was carried out in 1998. In Claude Poulin's July 1, 1998 memo titled "Scotia Mine, Mineral Resource Status," he reported the deposit's resources. Higher grade [greater than 7 % Zn-equivalent (% Zn + 0.5 x % Pb)] and lower grade zones (greater than 2 % but less than 7 %) were outlined by Savage's geologists. The higher grade zone consists of massive sulphide and lies at the contact between the dolomite and the Trench or evaporite units. The lower grade zone consists of disseminated zinc and lead within the dolomite. These outlines were transferred to a block model by Tim Carew, manager of Gemcom Services in Reno, Nevada. Inverse-distance squared weighting was used to calculate block grades. Top-cut values of 15 % Zn and 10 % Pb were used. No dilution or mining recovery factors were applied to the calculations. Undiluted resources are reported in Table 10.

The reader should note that the Resources were unclassified. They were not separated into Measured, Indicated and Inferred categories "due to the lack of geostatistical information" [Poulin, 1998 (1)]. Those Resources were not entirely independent and did not follow NI 43-101 guidelines, as the report predated that Standard.

Reserves were estimated through a pit optimisation process carried out on the Central portion of the deposit. These were reported in Claude Poulin's July 1, 1998 memo titled "Scotia Mine, Mining Reserve Status." Zinc and lead prices were $US 0.55 and 0.36 per pound, respectively. The optimised pit, which considered diverting Gays River by moving it toward the highway, was sent to Mine Design Associates (MDA) for practical pit design. Savage supplied the economic and geotechnical parameters to MDA. Dilution and recovery factors of 20 % and 90 %, respectively, were used.

Reserves included Resources that lie northeast of the highway. These would be accessed using underground methods. For this material, dilution and recovery factors of 25 % and 90 %, respectively, were used. The estimated Reserves are reported in Table 10. Those Reserves were not entirely independent and did not follow NI 43-101 guidelines, as the report predated that Standard.

It was discovered during the current Resource estimation process that an error was made when calculating resource and reserve grades during the 1998 estimate. When estimating block grades in the High Grade Zone, lower grade (less than 7 % Zn-Eq) assays in the zone were filtered-out because they were thought to belong to a separate domain. Likewise in the lower grade Disseminated Zone, higher grade (greater than 7 % Zn-Eq) were filtered-out. This incorrectly increased the grade of the high grade zone, which increased the overall resource and reserve grade by approximately 1 % Zn-Eq. The error had less of an effect on the lower grade zone. The error was corrected during the current Resource and Reserve estimate.

Table 10: Recent historical resource and reserve estimates.

Estimator	Category	Tonnes	Zinc Grade	Lead Grade
Westminer (1991)	"Geologic Reserve" (Undifferentiated)	2,400,000	8.7 %	6.3 %
	Reserve (Underground)	1,370,000	9.8 %	5.3 %
Savage (1998)	Resource (Undifferentiated):			
	Higher Grade	1,700,000	11.1 %[1]	4.7 %[1]
	Lower Grade	3,400,000	2.6 %[1]	1.3 %[1]
	Total	5,100,000	5.5 %[1]	2.4 %[1]
	Reserve (Undifferentiated):			
	Northeast (Underground)	360,000	8.6 %	4.3 %
	Central (Open Pit)	1,900,000[1]	4.1 %[1]	1.6 %[1]
	Total	2,260,000	4.8 %	2.0 %

[1] It was discovered during the current study that an error had been made during the grade estimation process in 1998.

It should be noted that the above referenced Resources and Reserves estimates were not carried out in accordance with the Canadian Institute of Mining and Metallurgy and Petroleum CIM standards on Mineral resources and Reserve Definitions ("CIM Standards") and therefore do not conform to Sections 1.3 and 1.4 of NI 43-101.

6. Regional Geology and Mineralisation

An excellent summary of the regional and deposit geological settings of the Scotia Mine deposit is supplied by Patterson (1993). There is also a recent "special issue devoted to zinc-lead mineralisation and basinal brine movement, lower Windsor Group (Viséan), Nova Scotia Canada" released as Volume 93 by ***Economic Geology*** in 1998. The bulk of the descriptions below are taken from those publications.

The Scotia Mine deposit occurs along the southern margin of the large (more than 250,000 km^2) and deep (more than 12 kilometres) late Palaeozoic Fundy (Magdalen) Basin, bordered on the northwest by the New Brunswick platform, and on the south by the Meguma platform (Figure 8). During the late Palaeozoic, the Fundy Basin was divided or segregated through a complex series of grabens into deep linear successor basins or sub-basins, which are now interpreted (Fralic and Schenk, 1981) as small pull-apart basins. Subsequent basement subsidence, fragmentation and block faulting produced the irregular pre-Carboniferous topography that was partly filled-in by early Carboniferous clastics, and later flooded by middle Carboniferous seas. Carboniferous sediments consisting of terrestrial conglomerates, and sandstones, siltstones and marine limestones and evaporites, were deposited in this Fundy Basin probably remained active during and after the Carboniferous, and may have had a major impact in the ore-forming process. These sub-basins contained thick accumulations of terrestrial and shallow marine sediments, and therefore could provide substantial volumes of basinal fluids (Ravenhurst, 1987).

The Gays River area is underlain by the Cambro-Ordovician metasediments of the Meguma Group which form the pre-Carboniferous basement upon which the Gays River carbonate host rock was deposited. The Meguma rocks were tightly folded during the Acadian Orogeny into long northeast-southwest anticlines and synclines which have been faulted and jointed. Erosion of this basement into irregular knobs and ridges was controlled by these structures prior to the deposition of overlying sediments (the Gays River carbonate). Unconformably overlying the Meguma Group are clastic sedimentary rocks of the Horton Group and marine sedimentary rocks of the Windsor Group which overstep the Horton near the basin margins and rest directly on Meguma basement. It is these Windsor Group carbonates which have been the host for the carbonate-hosted base metal sulphide and associated sulphate deposits in Nova Scotia.

Over 100 base metals occurrences, including a few deposits, are hosted by Lower Windsor Group marine carbonate rocks in Nova Scotia. About half of these occur within the Kennetcook, Shubenacadie, Musquodoboit and River Denys sub-basins. In addition to the Scotia Mine deposit, the most significant examples include the Walton deposit and the Jubilee deposit. Walton has two types of mineralisation: concordant sheets of barite contain lenses of lead-rich and copper-rich mineralisation. Between 1941 and 1978, 4.5 million tonnes containing over 90% $BaSO_4$, and 0.4 million tonnes containing 0.52% Cu, 4.28% Pb, 1.29% Zn and 350 g/t Ag were produced (Sangster, Savard and Kontak, 1998). At the Jubilee deposit on Cape Breton sulphides cement fault-related breccias and replace adjacent limestone; there are reported, unclassified resources (e.g. Fallara and Savard, 1998) of 0.9 million tonnes containing 5.3% Zn and 1.4% Pb.

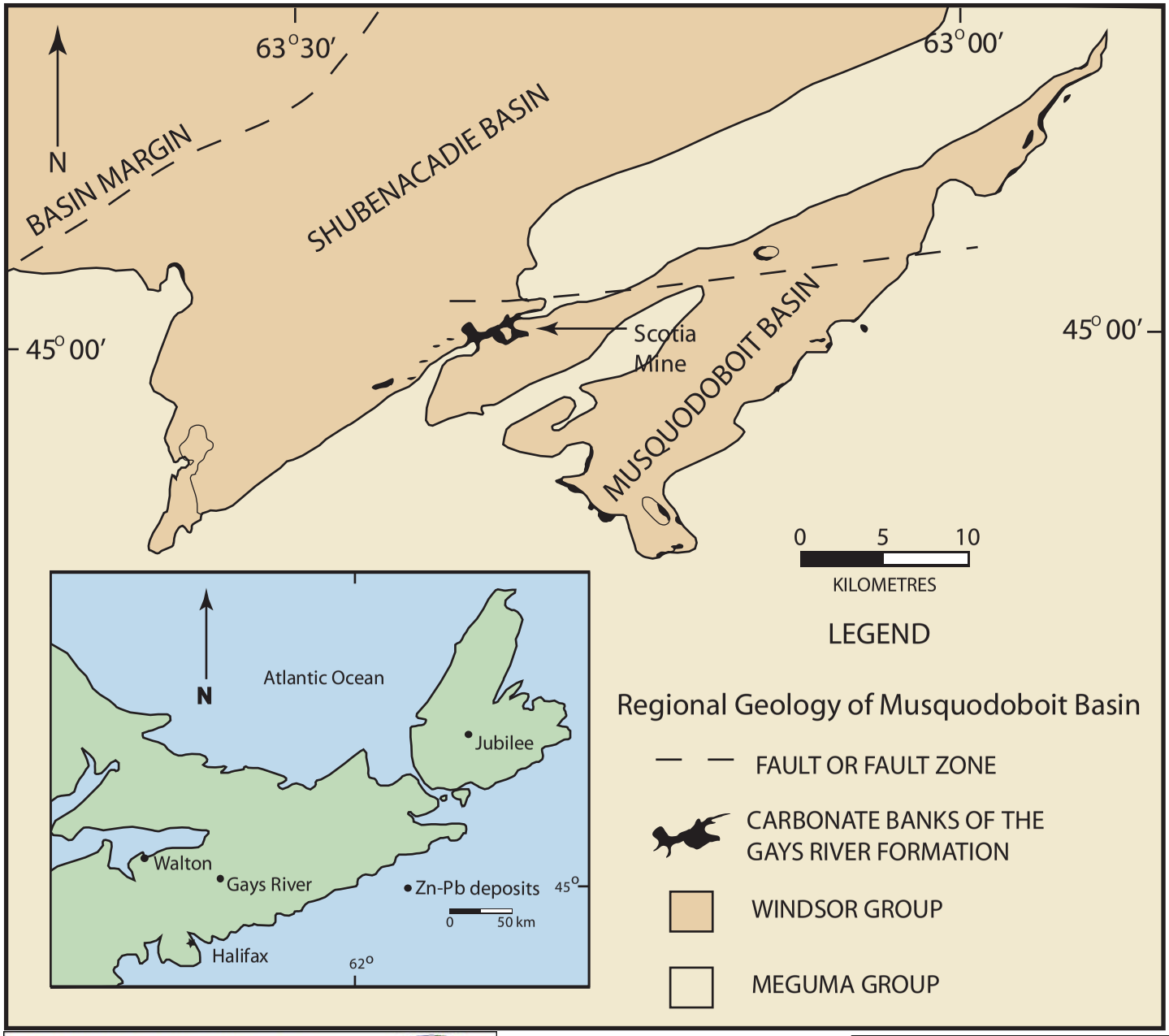

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Figure 8: Regional geology.

7. Property Geology and Mineralisation

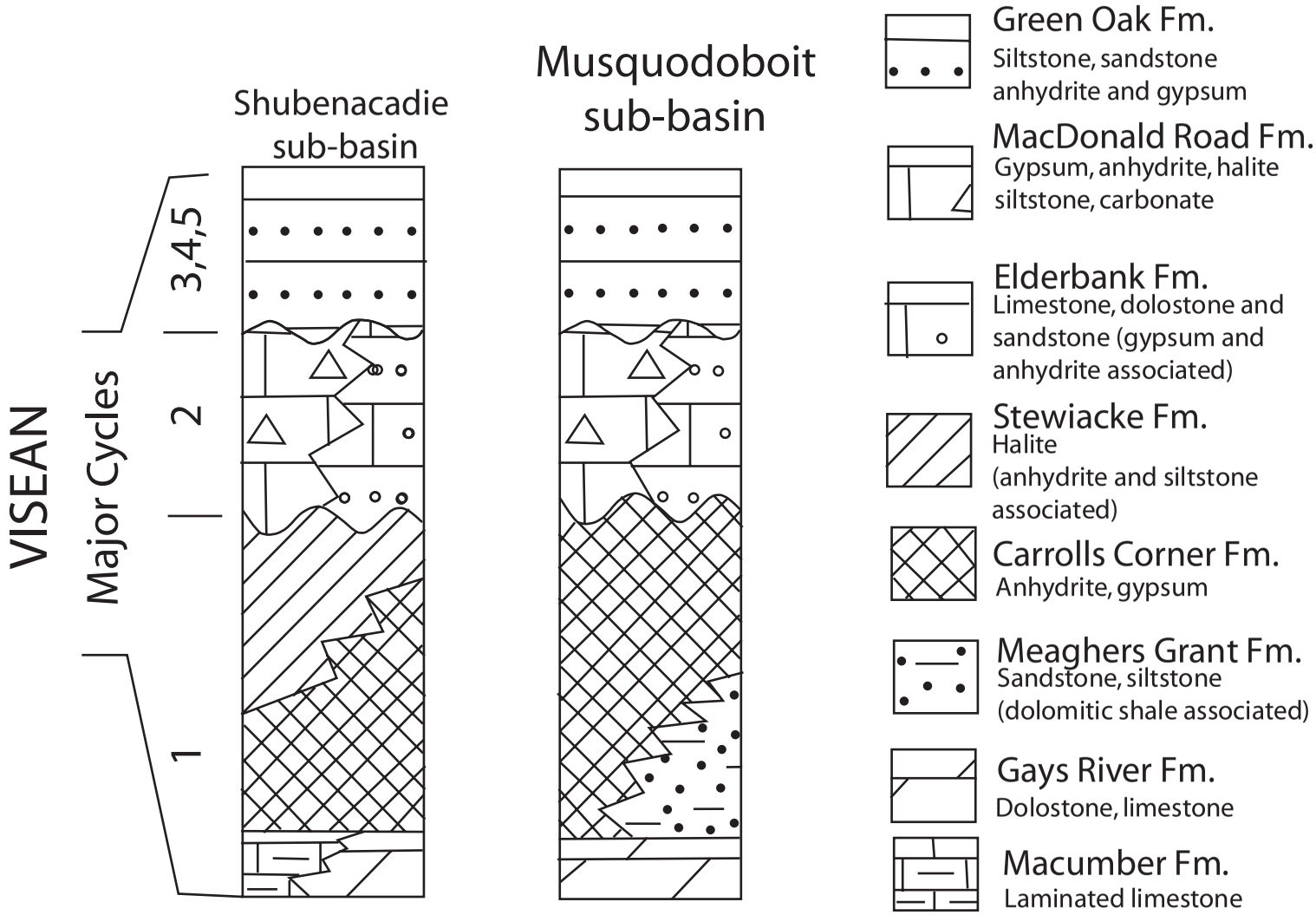
The Gays River Formation and its lateral equivalent, the Macumber Formation, form the basal carbonate units of the Windsor Group. The underlying 380-400 million-year-old basement rocks consist of greenschist facies meta-turbidites of the Meguma Group that form a northeast-trending, paleotopographic high which separates the Shubenacadie and Musquodoboit basins, and over which the Gays River carbonate bank developed (Kontak, 1998; Savard & Chi, 1998). The property's stratigraphy is shown in Figure 9. The basement is overlain by a laterally extensive, but discontinuous, talus breccia composed of centimetre- to metre-size, rounded to sub-rounded fragments of Meguma Group lithologies cemented by dolostone. Overlying the basal breccia or directly in contact with the basement rocks is a carbonate build-up composed of various bank and interbank facies: algal, coral and bryozoan bafflestones, skeletal packstones and wackestones. Contours for the top of Goldenville / bottom of carbonate contact are shown in Figure 10. The carbonate bank can be traced basinward into a laterally extensive, thinly laminated, 3 to 18 metre thick argillaceous, bituminous dolostone or limestone unit referred to as the Macumber Formation.

Overlying the carbonate rocks are evaporites (gypsum, anhydrite, halite and minor potash) with minor interbeds of dolostone and mudstone, all of which constitute the Carrolls Corner Formation. Nearby, (5 kilometres to the southwest), the gypsum is being mined at the National Gypsum Quarry.

In the deposit area, the contact between the evaporites of the Carrolls Corner Formation and the carbonates of the Gays River Formation was deeply incised by a palaeochannel during a period of uplift and erosion. It was filled-in by sedimentary debris (boulders, sands, silts, clay and gypsum fragments) to which a Cretaceous age has been assigned. This dense, over-compacted debris has been termed "Trench" material; it occurs adjacent to the massive sulphide mineralisation. Near the contacts, highly permeable, open channel-type structures have caused locally high rates of water flow that have been an impediment to underground mining.

Both the bedrock and "trench" sediments are overlain by 20-40 m of glacial till, which is locally cut by glacial-fluvial sands and gravels. Three geological cross sections are included as Figure 11, Figure 12, and Figure 13. Figure 13 represents the prototypical cross-sectional geology for the deposit.

STRATIGRAPHY - WINDSOR GROUP



From Chagnon and others, 1998

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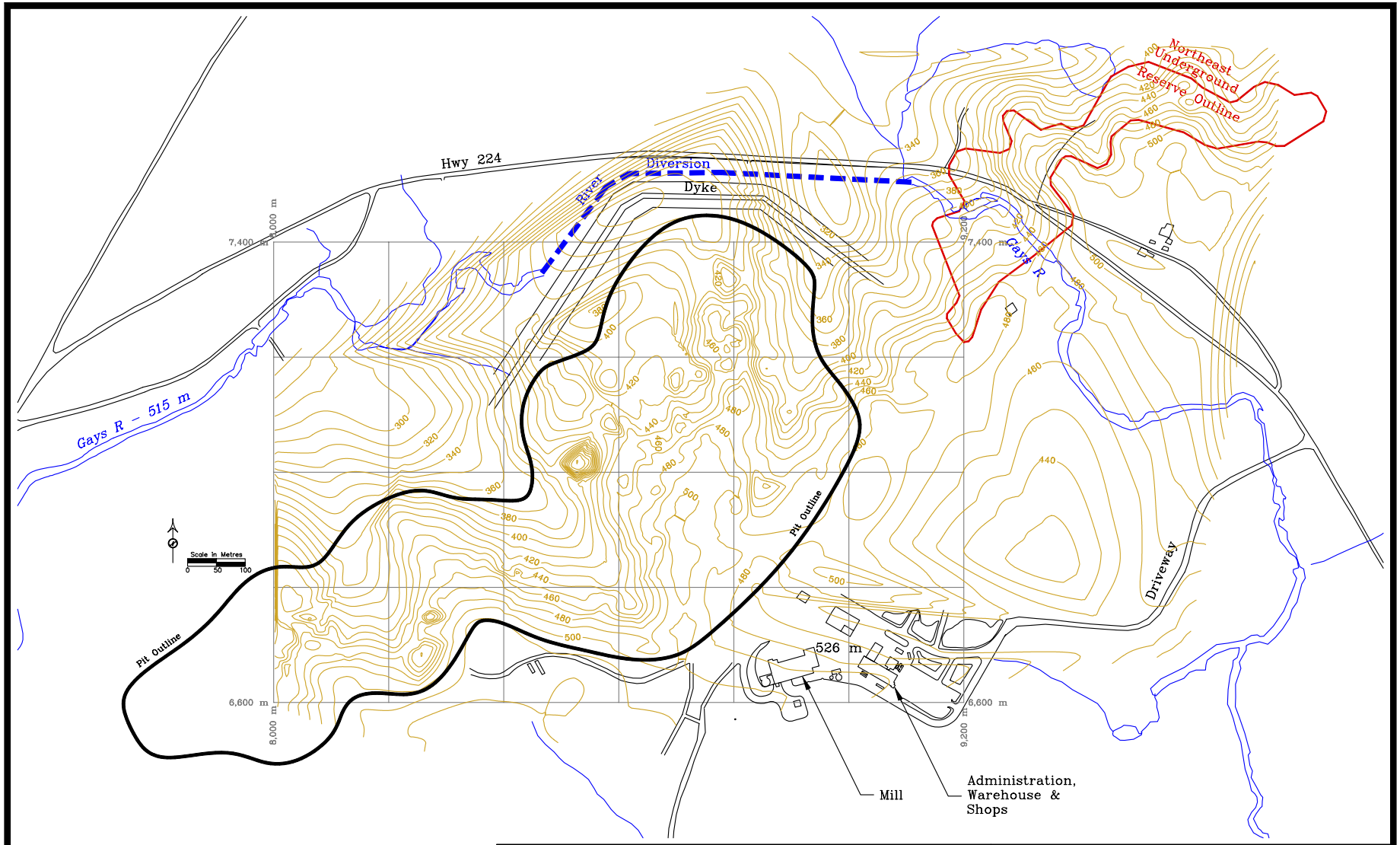
Figure 9: Stratigraphy.



Site grid.
Dimensions in metres.
10 m contour interval.

Date: March 16, 2006

Scale: Bar Scale

Drawn by: Douglas Roy, M.A.Sc., P.Eng.

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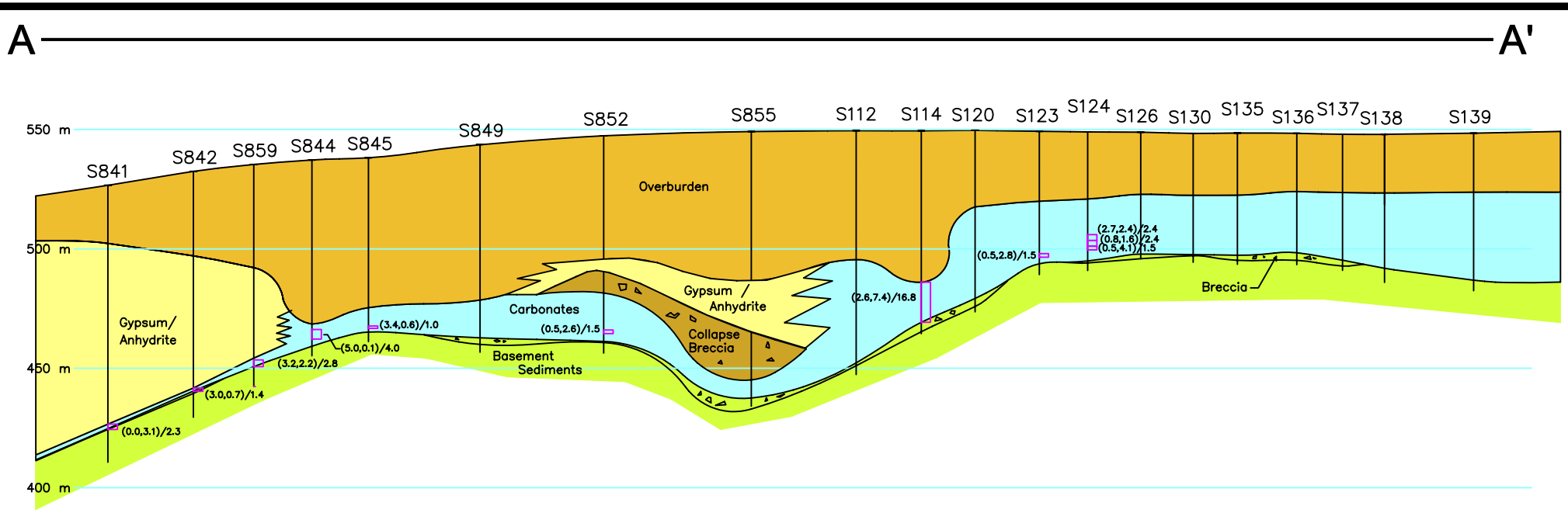
HALIFAX, CANADA

Scotia Mine
Gays River, Nova Scotia

Site Plan Showing Bottom of Carbonate (Bottom of Ore) Contours (Top of Goldenville Quartzite Basement Rock)

Figure 10



Legend:

(0.0,3.1)/2.3 Sample Composite (Avg Percent Zinc, Avg Percent Lead)/Composite Length

7. Overburden – Till, Sand, Silt

6. 'Trench': Collapse Breccia, Ancient Till

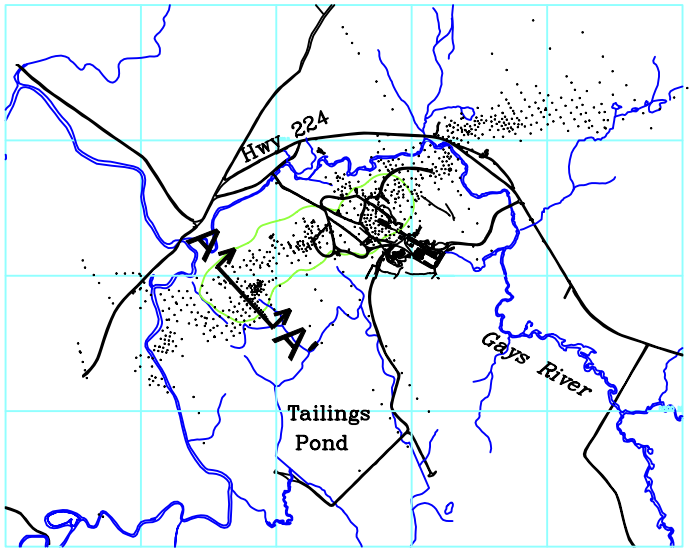
5. Carroll's Corner Formation:
Evaporites – Anhydrite, Gypsum, Siltstone, Dolomite, Limestone

4. Gays River Formation (MacCumber):
Carbonates – Dolomite, Limestone

3. Horton Formation:
Sediments – Shale, Siltstone, Sandstone, Conglomerate

2. Breccia: Goldenville Clast in Dolomite Matrix

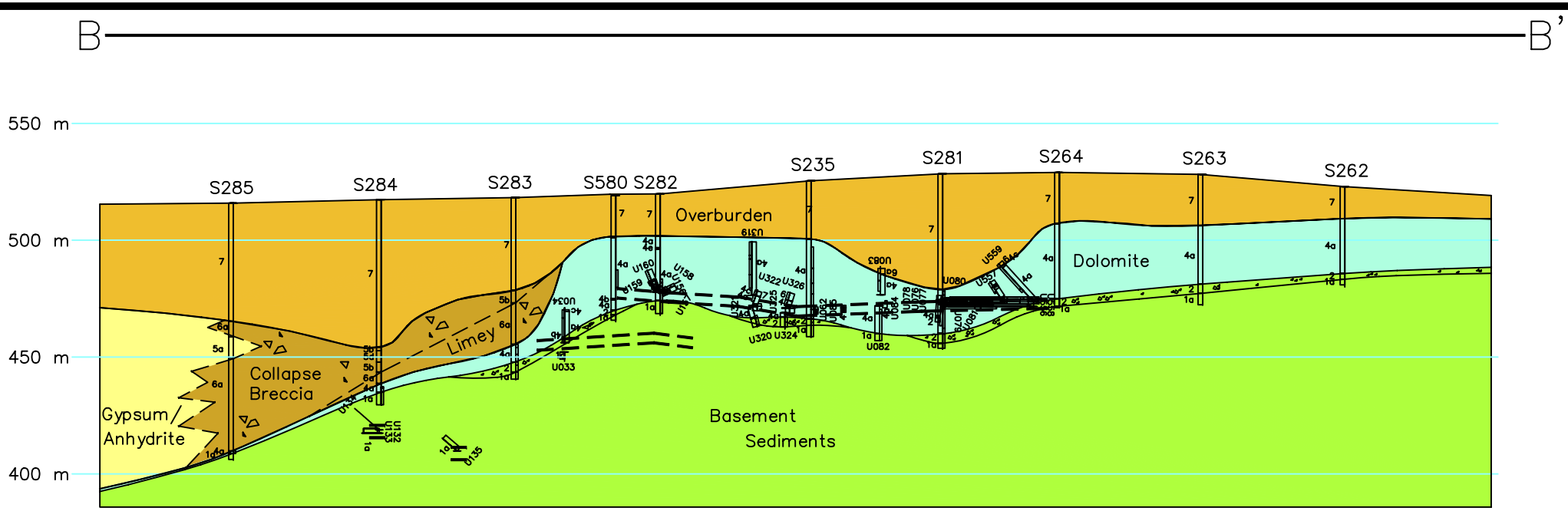
1. Goldenville Formation
Metasediments – Greywacke, Slates



Scale in Metres
0 25 50

Dimensions in metres.
Looking Northeast.
See sample sheets for complete sampling data.

Date: June 22, 2004	**Scotia Mine** **Gays River, Nova Scotia** **Cross-Section A---A'**
Scale: Bar Scale	
Drawn by: Douglas Roy, M.A.Sc., P.Eng. MINETECH INTERNATIONAL LIMITED CONSULTANT ENGINEERS & GEOLOGISTS HALIFAX, CANADA	Figure 11



Legend:

(0.0,3.1)/2.3 Sample Composite (Avg Percent Zinc, Avg Percent Lead)/Composite Length

7. Overburden – Till, Sand, Silt

6. 'Trench': Collapse Breccia, Ancient Till

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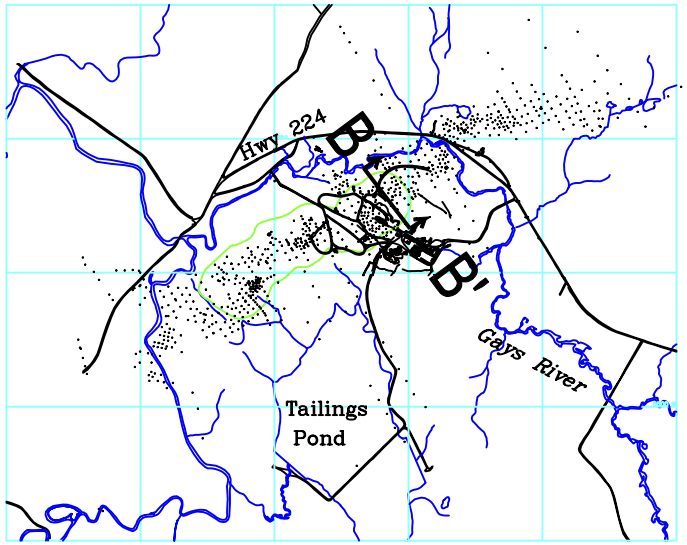
4. Gays River Formation (MacCumber):
Carbonates – Dolomite, Limestone

3. Horton Formation:
Sediments – Shale, Siltstone, Sandstone, Conglomerate

2. Breccia: Goldenville Clast in Dolomite Matrix

1. Goldenville Formation
Metasediments – Greywacke, Slates

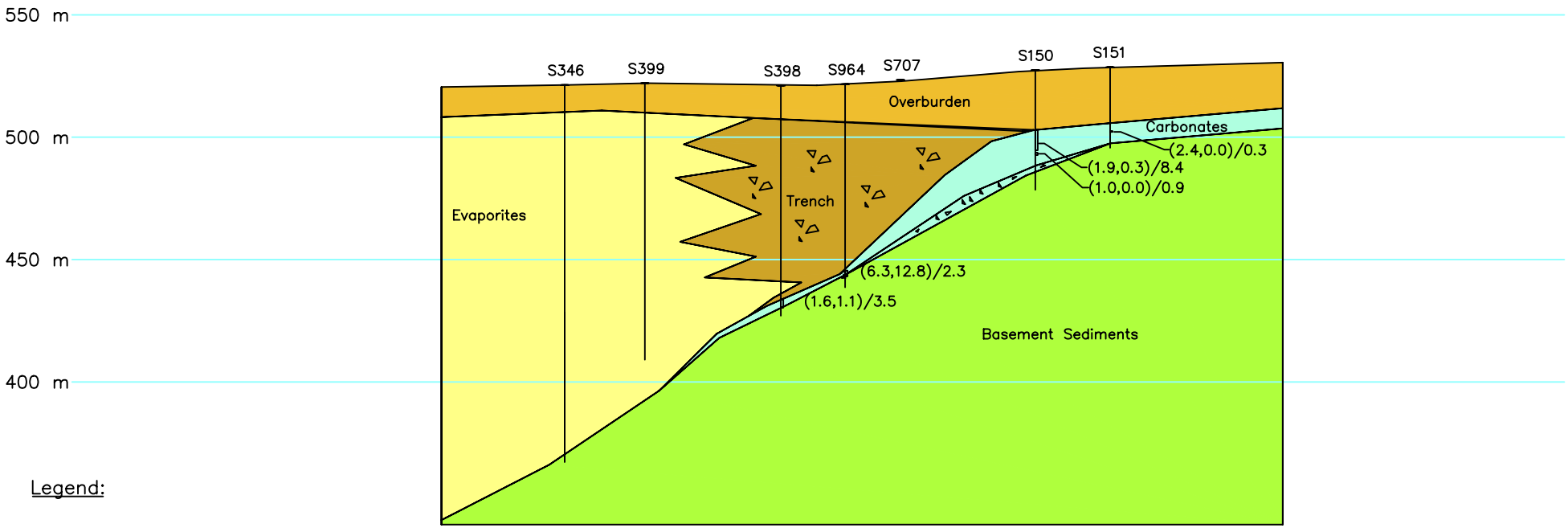
Intersected Underground Workings



Scale in Metres
0 25 50

Dimensions in metres.
Looking Northeast.
Refer to data table for sampling data.

Date: June 22, 2004	**Scotia Mine** Gays River, Nova Scotia **Cross-Section B---B'**
Scale: Bar Scale	
Drawn by: Douglas Roy, M.A.Sc., P.Eng. MINETECH INTERNATIONAL LIMITED CONSULTANT ENGINEERS & GEOLOGISTS HALIFAX, CANADA	Figure 12



Legend:

(0.0,3.1)/2.3 Sample Composite (Avg Percent Zinc, Avg Percent Lead)/Composite Length

7. Overburden – Till, Sand, Silt

6. 'Trench': Collapse Breccia, Ancient Till

5. Carroll's Corner Formation:
Evaporites – Anhydrite, Gypsum, Siltstone, Dolomite, Limestone

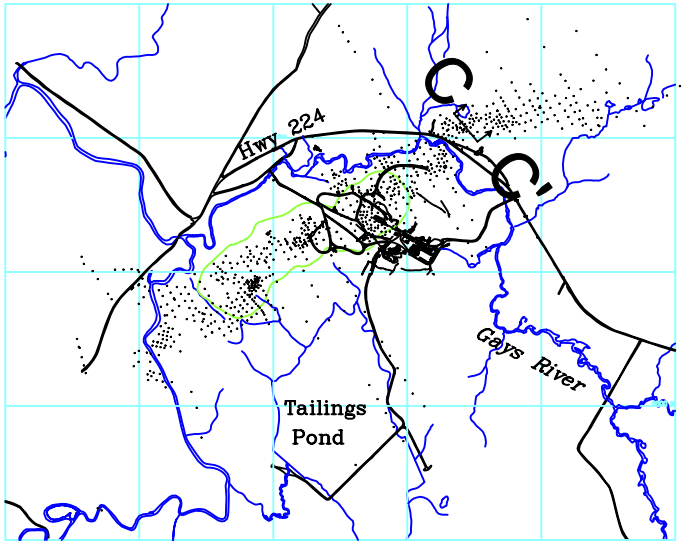
4. Gays River Formation (MacCumber):
Carbonates – Dolomite, Limestone

3. Horton Formation:
Sediments – Shale, Siltstone, Sandstone, Conglomerate

2. Breccia: Goldenville Clast in Dolomite Matrix

1. Goldenville Formation
Metasediments – Greywacke, Slates

Intersected Underground Workings



Scale in Metres
0 25 50

Dimensions in metres.
Looking Northeast.
Refer to data table for sampling data.

Date: September 21, 2004	**Scotia Mine** Gays River, Nova Scotia **Cross-Section C---C'**
Scale: Bar Scale	
Drawn by: Douglas Roy, M.A.Sc., P.Eng. MINETECH INTERNATIONAL LIMITED CONSULTANT ENGINEERS & GEOLOGISTS HALIFAX, CANADA	Figure 13

8. Deposit Type

The Scotia Mine mineralisation has long been considered a Mississippi Valley-type ("MVT") lead-zinc deposit. Characteristics of sedimentary formations that host MVT lead-zinc mineralisation include shallow-water, shelf-type carbonate rocks with reefs around the peripheries of intracratonic basins, karst structures, limestone-dolomite interfaces and proximity to a major hydrocarbon-bearing basin. The archetypical MVTs occur in the United States in several famous districts surrounding the Michigan-Illinois Basin which also has significant hydrocarbon production. Each of the districts is enormous, with resource potential of 75 million to 750 million tonnes and individual deposits in the order of 1 to 100 million tonnes.

Other MVTs have been mined in the past in Canada (e.g. Pine Point in the Northwest Territories, Nanisivik mine in Nunavut, and Newfoundland Zinc) and in Ireland.
MVTs are thought to have formed when hot, basin-derived, oil field-type brines, formed at depth of >2 km, migrated towards lower pressure areas around the basin periphery. Mineralisation precipitated from the brines when they encountered porous areas like reefs, karst breccias or sedimentary traps.

Sangster and others (1998) draw on their own and others' evidence to conclude that all Windsor Group lead-zinc deposits are epigenetic relative to their enclosing strata, exhibiting both open-space filling and host-rock replacement. At the Scotia Mine deposit, textures (including fossils) have been preserved; representing volume-for-volume replacement of original limestones by dolomite, and the sulphides are, in turn, replacements and porosity fillings within the previously altered host rocks. Kontak (2002) feels that petroleum in fluid inclusions in the Scotia Mine mineralisation suggest a role of hydrocarbons in the mineralising process, like many MVTs, but Sangster and others (1998) point to basement rocks underlying the Palaeozoic sedimentary rocks as the source of the mineralising fluids.

The temperatures of formation of the Scotia Mine deposit (and others in Nova Scotia) are higher than most North American MVTs, and compare more favourably with the clearly epigenetic MVTs of the Central Ireland Basin (Sangster and others, 1998). The Irish deposits also occur in Upper Paleozoic (Carboniferous) carbonate rocks, predominantly in shallow-water carbonates and a mudbank limestone (reef). The Irish deposits are also preferentially associated with east-northeast-trending faults which are thought to have acted as conduits for mineralising hydrothermal fluids; basement lineaments may also have controlled deposition. As with the Scotia Mine, sphalerite and galena are the main sulphides; barite is also usually present (Exploration and Mining Division Ireland, 2004). Seven economic deposits have been mined or are currently in production in Ireland. The largest of these, the world-class Navan deposit, had total production and proven + probable reserves of 82.1 million tonnes containing about 10.6% Zn+Pb; its annual production is 2.5 million tonnes of ore. Other producers and former producers had resources between about 8 and 18 million tonnes and grades of 9-25% Zn+Pb (Exploration and Mining Division Ireland, 2004).

It is noteworthy that two major carbonate-hosted zinc-lead deposits discovered in Ireland since 1986 occur down-dip from areas where considerable exploration, including diamond

drilling, had been carried out over the prior 20 years (Patterson, 1993). Similarly, the MVT deposits of the Viburnum trend in the U.S.A. were discovered at depths of 300 metres by understanding of the regional geology of the hosts rocks of the Old Lead Belt about 80 km away.

9. Mineralisation

Nesbitt Thomson Inc. (1991) describe the high-grade mineralisation as consisting of a massive sulphide zone in contact with the evaporite or Trench, ranging in thickness from 0.1 to 5.0 metres and locally containing up to 78 % Pb and 57 % Zn. On the footwall of the massive sulphide, there is a zone of disseminated material (>7% Zn equivalent[2]) which, in places, is up to 12 metres in thickness. Locally disseminated mineralisation (>2% Zn equivalent) extends up to twenty metres into the footwall.

The Scotia Mine deposit is essentially controlled by a sinuous paleo coastline. The main part of the deposit is shallow (generally <150 m deep), has a dip length of approximately 100 m and a strike length following the paleo-coastline over a straight line distance of 2 km (Nesbitt Thomson Inc., 1991).

The mineralisation at the Scotia Mine deposit consists of massive and/or disseminated ore hosted predominantly by the carbonate rocks, with extensions down into the basal breccia unit. The massive mineralisation consists of fine-grained (<10-20 μm), Fe-poor, beige-coloured sphalerite and medium to coarse-grained, Ag-poor galena (<10-20 ppm Ag in galena concentrates) (Kontak, 1998; Savard and Kontak, 1998), is restricted to the carbonate-evaporite contact and is 1 to 3 metres in true thickness. Disseminated mineralisation, consisting of yellow to orange, millimetre-size euhedral sphalerite and millimetre-to-centimetre-size euhedral galena, fills in primary porosity in the dolomitized carbonates and walls of primary cavities (Kontak, 1998).

Sphalerite and galena constitute about 99.5% of metallic minerals. Other sulphide minerals are marcasite, pyrite and chalcopyrite, while gangue minerals include calcite, dolomite, fluorite, barite and selenite (Patterson, 1993).

10. Exploration History

Lead-zinc mineralisation at Gays River was first mentioned in records dating back to 1824. Knowledge of the occurrence may even go back to the early 1700's when French soldiers reportedly used the lead for making ammunition (MacEachern and Hannon, 1974). Other early references to Gays River lead were made in 1868 by J. W. Dawson in "Acadian Geology" and by H. Howe in "Mineralogy of Nova Scotia".

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[2] The parameters used to calculate "Zn equivalent" are unknown, but would have reflected the prices of zinc and lead at the time.

The earliest recorded prospecting may have been trenching along the outcrops in 1873-1874. Additional trenching and pit sinking was carried out in 1928. Assessment records do not indicate any resumption of interest in the area until 1951. From the first reports of mineralisation in the area in the early 1800's, exploration activity up to 1950 had yielded best values of 3 % lead (Patterson, 1993).

1951

Maritime Barytes Limited acquired the property at Gays River and carried out a surface exploration program involving some trenching and sampling. Gays River Lead Mines subsequently became involved in the evaluation of the property and commenced a drill program to delineate the occurrences of lead and zinc. A total of 67 delineation drill holes were completed by mid-1952 and an additional seven holes were completed for exploration in the vicinity.

The drilling by Gays River Lead Mines Limited outlined four zones of mineralisation in an area about 400 metres by 900 metres. Over 800,000 tonnes of mineralised (galena, sphalerite, pyrite, marcasite and chalcopyrite) Windsor carbonate were defined overlying and flanking a northeast-trending anticlinal Meguma greywacke basement high. Grades for the four zones ranged from 1.10% to 3.50% combined lead plus zinc with an average of 2.32% combined lead plus zinc. Most, if not all, assays were apparently from sludge samples.

1962

Gunnex Limited carried out extensive soil sampling in the Gays River area in 1962. Anomalies were encountered only over areas of previously known mineralisation where overburden was thin. An induced polarisation survey indicated only a very weak response over known mineralisation and did not add any new target areas. The lack of encouraging response on the periphery of the earlier defined mineralised area prompted Gunnex to forego any further exploration activity.

1968 – 1969

In 1968 and 1969 Penarroya Canada Limited completed extensive soil sampling and geological mapping in the Gays River and Meaghers Grant areas. Two diamond drill holes in the Meaghers Grant area intersected minor zinc mineralisation. No drilling was carried out in the Gays River area even though a number of soil anomalies had been identified. Most of the major anomalies corresponded with previously known mineralisation. Two new anomalous areas were, however, defined. They occur near Carrolls Corner and in the Black Brook area east of the Gays River and define a northeast trending geochemical high. The latter area is close to the northeast end of the presently defined Gays River deposit itself.

1971

Texasgulf Inc. drilled four diamond drill holes in the Gays River area in 1971. One hole adjacent to a Gays River Lead Mines drill hole confirmed significant mineralisation in the carbonates. The remaining holes tested one soil anomaly southeast of Gays River and two areas northwest of Gays River. No encouraging mineralisation or carbonate build-ups were intersected in the last three holes and work was terminated.

1972 - 1984

In 1972 personnel of Cuvier Mines Limited ("Cuvier") prospected the Gays River area and located significant mineralised float material to the south of the old occurrence (MacEachern and Hannon, 1974) and subsequently acquired the ground. Cuvier also outlined geophysical and geochemical anomalies. In September of 1972 Cuvier optioned the property to Imperial Oil Enterprises ("Esso") with Esso holding a 60% interest and acting as the operator. Cuvier formed a joint venture with Preussag Canada Ltd. ("Preussag") to finance Cuvier's 40 % interest in the property.

Both Cuvier and Esso were of the opinion that the area had the proper geological setting for a Mississippi Valley-type deposit. Esso recognised the possible existence of a reef complex trending north-easterly from the old Gays River drilling site. The source of the mineralised boulders had not been located and a combination of deep glacial till and lack of outcrop would necessitate fence-type drilling in geologically favourable areas for the purpose of obtaining geological information as well as locating any mineralised areas.

A total of 20 holes were drilled prior to drilling the discovery hole 2.5 kilometres northeast of the original showing along the postulated reef trend. The discovery hole intersected 3.35 metres averaging 7 % zinc (MacEachern and Hannon, 1974).

From October 1972 to August 1974, Esso/Cuvier drilled off the deposit and identified 12,000,000 tons averaging 7 % Zn + Pb (Patterson, 1993) over an area of approximately 4 kilometres by 220 metres at depths ranging from 20 to 200 metres (450 surface core holes)[3].

The initial mine development by Esso began with developing the exploration decline in 1976 across the central portion of the mineralised zone to verify mining conditions, the grade and continuity of the mineralisation and to provide bulk samples for metallurgical testing. The decline was 760 metres in length but by mid-1979 some 1,800 metres of drifting and 744 metres of underground development had been completed. The deepest workings were at a vertical depth of 100 metres. In December of 1977 Esso purchased Cuvier's and Preussag's interests in the property and formed Canada Wide Mines to develop and mine the deposit.

During the next two years various feasibility studies were carried out. Recoverable proven plus probable reserves were then estimated at 4.7 million tonnes at 2.8% Pb and 4.2% Zn

[3] A summary table of all known drilling at the Gays River deposit by all exploration companies over the years is included as Table 11. A map depicting the location of the surface holes is included as Figure 14.

(WMC, 1995). Esso commenced with the construction of the mill and other facilities in August of 1977. The 1,350 tonne processing plant was commissioned in October of 1979 and the mine was further developed to support a 1,350 tonne per day operation.

From 1978 until 1981, Esso operated the mine and targeted the lower grade mineralisation using a trackless, lower cost, bulk room and pillar mining method approach. The higher grade mineralisation near the carbonate contact was not part of the mine plan. Operations continued until August 1981 when production was suspended except for an underhand cut and fill technique test stope. Mining conditions exacerbated by bad ground conditions and excessive water inflow caused the operation to be suspended. During the operation, a total of 553,688 tonnes of mineralised material averaging 1.36% Pb and 2.12% Zn were produced and run through the mill – 272,000 tonnes of waste were also removed. Throughout this period efforts to achieve the full production rate, as well as efforts to mine areas of higher grade mineralisation were complicated by the combination of the complex geological setting and the severe hydrological problems.

The plant was shut down in 1982 as a result of operating losses due to lower than expected grades, higher than expected operating costs, the difficult water problems and low metal prices.

Seabright Resources Inc. acquired the mine and mill in 1984 but despite a favourable feasibility study did not reactivate the mine due to depressed metal prices at the time.

1985 - 1987

Seabright's primary intention was the usage of the mill facility to process gold ore from their outlying properties, and a secondary intent to later re-open the Gays River mine (WMC, 1995). At the time, Seabright was mining (bulk sampling) gold-bearing quartz veins from four small operations; Beaver Dam, Forest Hill, Caribou and Moose River, all located within the Meguma Group (Cambro-Ordovician).

The milling facility was converted for gold processing. The mine was not re-opened at that time by Seabright as a sharp drop in zinc prices rendered the underground mining operation uneconomic.

1987 - 1991

In 1988 Westminer Canada Limited ("WMC") purchased Seabright Resources. A review of the deposit, including the drilling of 89 surface core holes, led WMC to a positive production decision based on a reinterpretation of the geology and mining method. They began dewatering the underground workings in early 1989. Following the success of the mine dewatering and a test mining period to assess the suitability of the proposed narrow vein cut and fill mining method to extract the high grade ore zones, the mine was placed back into production. It reached commercial production rates in March 1990 (WMC, 1995) at a rate of 800 tonnes per day.

WMC's initial approach was to drive small 2.5x2.5 metre cut and fill stopes adjacent to the "Trench" material. Dry waste rock backfill was placed after each lift. In most areas, the method allowed the high grade ore on the carbonate-Trench contact to be extracted. In one area WMC successfully tested the room and pillar mining method (Nesbitt Thomson, 1991). A total of 187,010 tonnes of ore at an average grade of 3.5% Pb and 7.47% Zn were mined during WMC's involvement on the property.

Hydrological difficulties causing poor ground conditions continued to play a factor in the mine operation. In May 1991, rising water levels due to the spring run off forced the cessation of mining in a number of stopes and WMC decided to place the mine in project mode. Following the suspension of production in 1991, WMC carried out an extensive program to understand the mine hydrology and concluded that the groundwater could be successfully managed so that mining operations would no longer be adversely affected.

WMC has identified the Eastern zone of the deposit as an area for possible early development because ground conditions are substantially better due to the hanging wall being generally gypsum/anhydrite rather than Trench. The grade is also higher relative to other sections of the deposit. The Eastern area appears promising for additional resources.

WMC thoroughly assessed the property in 1991 and prepared a revised mine plan to resume mine production. The revised plan provided for more mechanisation of the mining method, institution of paste backfill, increased groundwater drainage through screened drainage wells and a revised pumping system. However, the operation was WMC's only lead and zinc producer, was not associated with any downstream smelting facilities and was a smaller operation relative to other corporate assets. For these reasons, the property did not fit within WMC's corporate strategy to focus on large scale operations and for this reason the property was sold to Savage Resources.

1996 - 1999

After acquiring the Scotia Mine in 1996, Savage conducted two exploration drilling programs to fill in the gaps from prior drilling and improve the mineral resource estimate on the mine property. In December 1996, 36 diamond drill holes, totalling 1,325 metres were drilled in the central mine area adjacent to the underground mine entrance to test the continuity of the disseminated low grade mineralisation in the back reef (known as the sand pit area –an area of commercial aggregate)[4]. In April and May 1997, an additional 30 diamond drill holes totalling 2,339 metres were drilled in the Northeast zone (as identified by WMC). Both programs were successful and confirmed the presence of low grade (in the central area) and high grade mineralisation (in the Northeast zone). According to Cullen (1997), the results of the drilling (based on a 7% Zn-equivalent cut-off grade) enhanced some areas of the Northeast zone and diminished other areas. He also states that a complete revision of some of this area (with additional drilling evaluation) be completed prior to any production decision.

[4] Aggregate mining is currently being carried out by a local aggregate company.

Savage dewatered the underground workings from June to August 1997 and started to rehabilitate the mine before a decision was made to extract the ore in the main, central zone using open pit methods. An open pit design was prepared using appropriate technical criteria for ore mining and waste stripping (Gemcom and Whittle 3-D Optimisation). The preliminary mine plan assumed the processing of 1,350 tonnes per day with the ore coming from a combination of underground (1,000 tonnes per day) and open pit operations (350 tonnes per day).

In early 1999 ownership of Savage was transferred to the Australian mining company Pasminco Canada Limited ("Pasminco").

2001-2003

Regal Mines Limited (Regal Mines) purchased Pasminco Resources Canada Company (Pasminco Resources) and its assets in February 2002. Regal was owned 50 % by OntZinc Corporation (OntZinc) and 50 % by Regal Consolidated Ventures Limited (Regal Consolidated). As part of the sale, Pasminco Canada Holdings Inc (Pasminco Holdings) retained a 2 % net smelter return (NSR) royalty on future production. OntZinc acquired Regal Consolidated's 50 % interest in December 2002 to own 100 % of Pasminco Resources. Savage Resources Limited is the successor of Pasminco Holdings and currently holds the 2 % royalty. Pasminco Resources was later renamed ScoZinc Limited (ScoZinc). The mining and environmental permits are still in force and are held by ScoZinc along with all the Scotia Mine assets.

2004 – Present

Exploration activity by ScoZinc has included diamond core drilling, a hydraulic mining test, prospecting of the general area, geological compilation of past relevant data and two lines (ten samples) of Mobile Metal Ion Geochemistry (MMI) across areas of known mineralisation covered by thick accumulations of glacial till. MMI is a relatively new and powerful geochemical exploration tool that is enabling companies to explore areas that have been previously too difficult for surface geochemistry. The results of the MMI survey were inconclusive.

A hydraulic mining test was performed to determine whether such a method might be useful to uncover the glacial overburden and some of the Trench material in the area of the low grade potentially open-pitable resources. This was primarily performed near the area of the sand pit next to the original portal.

At the bottom of the existing "sand pit," there is very little soil (average of two metres) covering the flat-lying dolomite. Based on diamond drilling results, the dolomite contains galena and sphalerite in low, but potentially economic concentrations. The intention of the excavation work was to remove the soil from the dolomite to better characterize the potential resource. In the process, the possibility of using dredging to strip overburden was evaluated, utilizing a small dredge that would pump a soil/water slurry from the pit floor through a

temporary, plastic pipeline to a small, purpose-built settling pond. The soil would settle in the pond and the decanted water would flow back to the portal pond through a short network of ditches. The design capacity of the settling pond was approximately 13,000 m^3. The total footprint of the pond was approximately 8,200 m^2.

It was originally intended that the dredge would operate and would enlarge the pond as it dredged, gradually moving out of the pond and over the bedrock. However, there was not enough water depth over the bedrock to allow the dredge to work properly.

Bulldozers were used to push material toward the dredge, but the productivity of the bulldozers was far less than the dredge's productivity. As a result, the dredge operated at only a fraction of its capacity.

Generally, the test showed that it is possible to mine the sandy overburden in the current pit bottom using dredging methods.

A commercial aggregate sand deposit (fine aggregate for concrete and masonry mortar or grout) on the property was operated under lease by an independent company. The lease required the sand operation to conduct its activities such that it did not interfere with the metal mining and milling operations. The lease also made provision for free access to the sand deposit for material required in the mining operation.

Six holes were drilled through the Trench using a soil drilling rig. The Trench is a geological unit that separates the gypsum and dolomite units. The purpose of this program was to characterize the soils that make up the Trench. Four holes were drilled in the Central Zone near the current pit. The two other holes were drilled near the highway (Hwy 224) in the East Zone.

The holes in the Central Zone around the current pit consisted mainly of dark brown clay with fine-to-medium grained sand. Rock fragments, rounded-to-angular, were occasionally noted.

The holes in the East Zone near the river and highway consisted of fine-to-medium grained sand with minor clay. This observation may be an important factor during future mining. Permeability underneath the river is expected to be high to a depth of at least 20-30 metres. This will adversely affect slope stability should the walls of an open pit approach the river.

Twenty five diamond core drill holes (1,845.3 metres) were completed by ScoZinc on the Scotia Mine property. Seventeen of these holes were meant to further define the lead and zinc mineralisation contained within the reef carbonate while the remaining eight holes were meant to test the gypsum potential immediately overlying the mineralised zones.

Four holes (477 metres) were completed in the north-eastern portion of the deposit while thirteen holes (1,172 metres) were completed in the central area of possible lower grade open pit mineralisation. The program was moderately successful in the central area with zinc values consistently in the 2 to 4% range over 1 to 2 metres (Table 11). The drilling program in the north-eastern zone proved less successful with mineralised intervals being quite thin.

Four holes (673.3 metres) were drilled in the northeast zone and an additional four in the central area to test the overlying gypsum in the hanging wall of the base metal mineralisation. The holes were drilled to obtain core samples of the gypsum deposits that immediately overlie the mineralised zones. The purpose of the samples was to carry out early tests of gypsum consistency and quality as well as to confirm preliminary estimates of the probable size of the gypsum resource adjacent to the mineralised trend.

In most holes, a gypsum "cap," 20-30 metres thick was encountered. Grade was highest (greater than 90 % gypsum) near the bedrock surface and decreased with depth. At 20-30 metres depth, gypsum grade dropped below 80 %, transitioning to anhydrite over an interval of approximately ten metres. Because the gypsum was quite hard, it was difficult to visually determine the contact between gypsum and anhydrite.

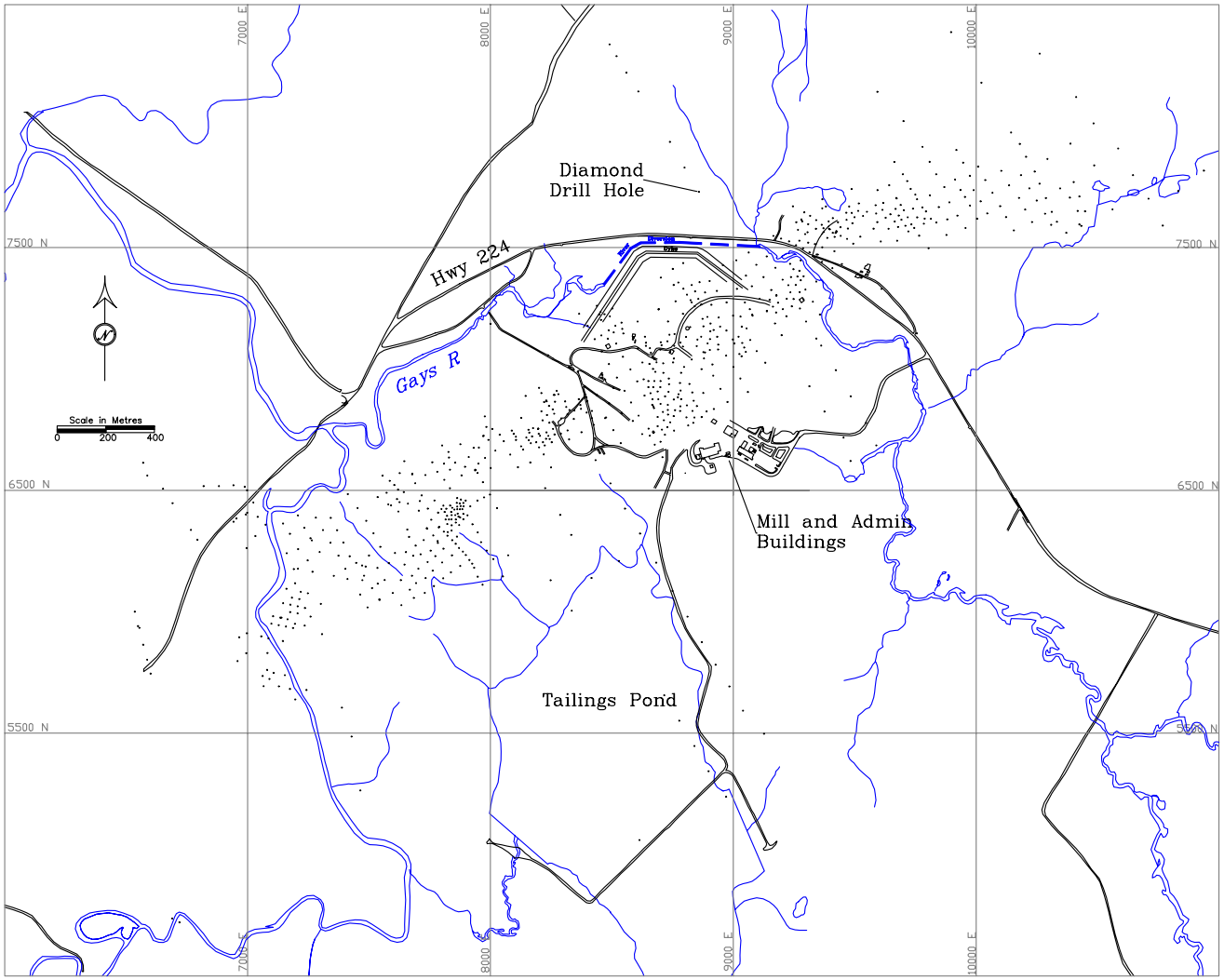
11. Drilling

To date, over 1,300 diamond core drill holes have been drilled on the Scotia Mine property (Figure 14, Figure 15 and Table 11). The majority were drilled to determine the characteristics of the zinc- and lead-mineralised dolomite. Eight holes were drilled in 2004 to determine the characteristics of the gypsum hanging wall rock.

Most of the 896 surface holes were drilled vertically. The azimuth and dip of the 467 holes drilled from the underground workings was variable.

Generally, holes were drilled so as to fully penetrate the dolomite reef and continue on until no more mineralisation is found. Generally, holes were drilled a few metres beyond the dolomite reef.

A compilation of core logs and sample assays is given in Appendix 6. The sample intervals do not necessarily represent true widths. The orientation of the mineralisation is well known and is described in Section 8.



Date: April 26, 2006

Scale: Bar Scale

Drawn by: Douglas Roy, M.A.Sc., P.Eng.

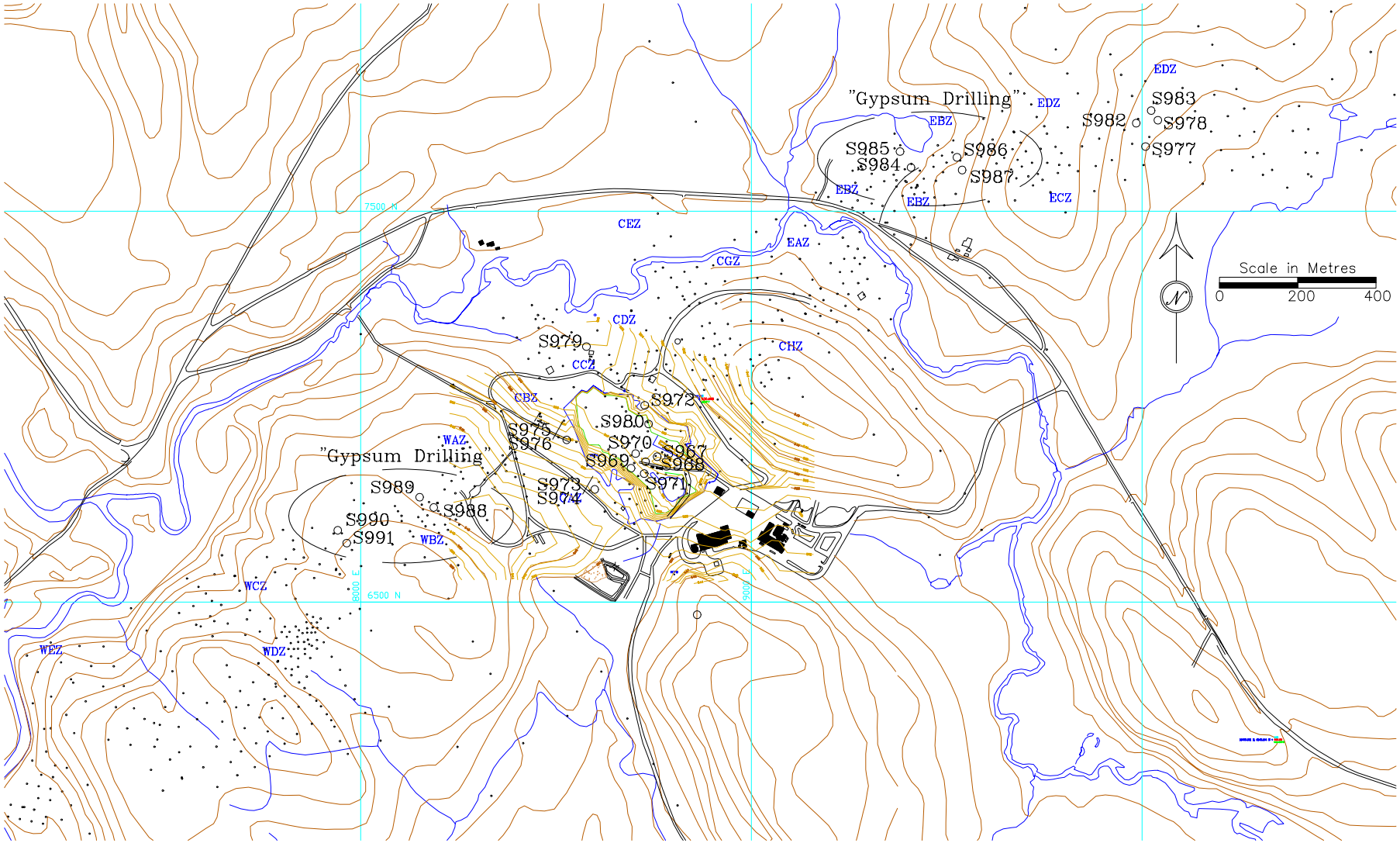
MINETECH INTERNATIONAL LIMITED
CONSULTANT ENGINEERS & GEOLOGISTS
HALIFAX, CANADA

Scotia Mine
Gays River, Nova Scotia

Site Plan Showing
Diamond Drill Holes

Site grid.
Dimensions in metres.

Figure 14



Legend:
- ◦ Diamond Drill Hole
- ○ S980 Diamond Drill Hole (2004)

Contour interval = 5 m, 2 m around current pit.
Site grid.
Dimensions in metres.

Date: December 14, 2004	Scozinc Limited Scotia Mine Gays River, Nova Scotia
Scale: 1:1500 (Bar Scale)	
Drawn by: Douglas Roy, M.A.Sc., P.Eng. MINETECH INTERNATIONAL LIMITED CONSULTANT ENGINEERS & GEOLOGISTS HALIFAX, CANADA	2004 Drilling Figure 15

Table 11: Historical Surface and Underground Diamond Drilling Activity[5].

From	To	Holes with Info[6]	Metres	Time Frame	Company
Surface Holes					
1	72	70	2,951.7	1951-1952	Gays River Lead Mines
73	740	646	59,123.6	1972-1982	Imperial Oil/Canada Wide Mines
741	900	89	7,596.8	1985-1995	Seabright, then Westminer (undifferentiated)
901	966	66	3,664.0	1997	Savage/Pasminco
967	991	25	1,864.3	2004	ScoZinc
Subtotal		**896**	**75,204.4**		
Underground Holes					
1	341	318	7,460.7	1979-1982	Imperial Oil/Canada Wide Mines
342	651	149	4,434.9	1985-1995	Seabright, then Westminer (undifferentiated)
Subtotal		**467**	**11,895.6**		
Total		**1,363**	**87,096.0**		

[5] Data supplied by ScoZinc.
[6] The electronic database does not contain information for underground holes 342-499.

11.1 Sample Statistics

Sample statistics were calculated for sampling within the carbonate. All samples for which at least one metal (zinc or lead) was assayed were considered. Most samples were assayed for both zinc and lead. Depending on the amount of visible mineral, some samples were assayed for only one metal. The total sample count was 8,022.

The mean sample interval length was 1.44 metres with a standard deviation of 0.82 metres (Table 12). Skewness is a measure of symmetry, or more precisely, the lack of symmetry. The positive value for skewness indicates that the data is skewed right, meaning that the right tail is heavier than the left tail. This is also shown in the histogram in Table 13. The aggregate sample length was 11,522 metres.

The mean zinc grade was 3.55 %. From the histogram, we can see that zinc assays are approximately lognormal. The range in zinc content was zero to 62.10 %. Theoretically, the maximum possible zinc assay is 67.10 % - the zinc content of pure sphalerite.

The mean lead grade was 1.91 %. From the histogram, we can see that lead assays are also approximately lognormal. The range in lead content was zero to 79.50 %. Theoretically, the maximum possible lead assay is 86.6 % - the lead content of pure galena.

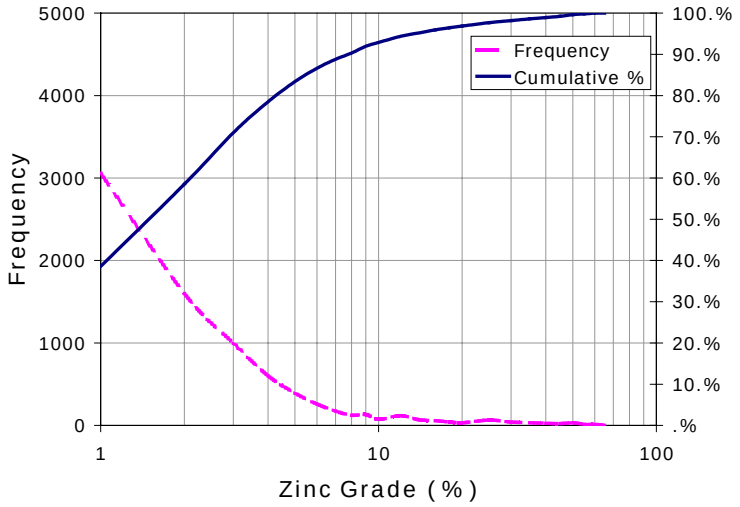
Table 12: Descriptive statistics.

Descriptive Statistic	Zinc Grade (%)	Lead Grade (%)	Sample Interval (m)
Mean	3.55	1.91	1.44
Standard Error	0.08	0.07	0.01
Median	1.52	0.12	1.43
Mode	0.02	0.01	1.52
Standard Deviation	6.79	6.24	0.82
Sample Variance	46.17	38.99	0.67
Kurtosis	25.17	52.86	16.91
Skewness	4.60	6.56	2.50
Range	62.10	79.50	13.39
Minimum	0.00	0.00	0.03
Maximum	62.10	79.50	13.42
Sum	n/a	n/a	11,522
Count	8,022	8,022	8,022

Table 13: Sample histograms.

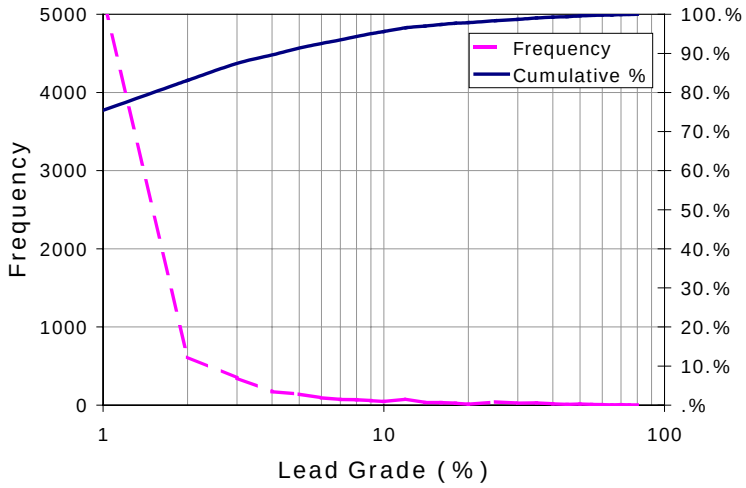
Zinc Histogram

Range	Frequency	Cumulative %
0	39	.49%
0-1	3056	38.58%
1-2	1599	58.51%
2-3	999	70.97%
3-4	603	78.48%
4-5	393	83.38%
5-6	259	86.61%
6-7	174	88.78%
7-8	123	90.31%
8-9	132	91.96%
9-10	74	92.88%
10-12	118	94.35%
12-14	68	95.20%
14-16	58	95.92%
16-18	42	96.45%
18-20	33	96.86%
20-25	65	97.67%
25-30	41	98.18%
30-35	33	98.59%
35-40	27	98.93%
40-45	23	99.21%
45-50	32	99.61%
50-55	15	99.80%
55-60	14	99.98%
60-65	2	100.00%
65+	0	100.00%



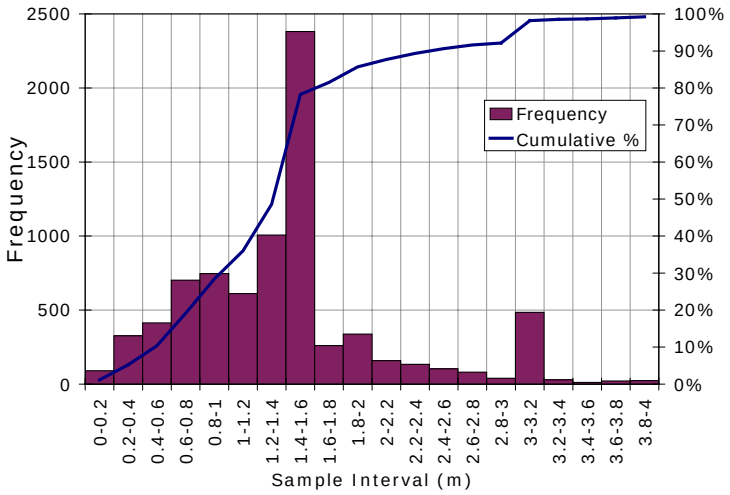
Lead Histogram

Range	Frequency	Cumulative %
0	851	10.61%
0-1	5200	75.43%
1-2	616	83.11%
2-3	347	87.43%
3-4	173	89.59%
4-5	141	91.35%
5-6	94	92.52%
6-7	73	93.43%
7-8	70	94.30%
8-9	59	95.04%
9-10	45	95.60%
10-12	77	96.56%
12-14	34	96.98%
14-16	33	97.39%
16-18	25	97.71%
18-20	12	97.86%
20-25	41	98.37%
25-30	26	98.69%
30-35	29	99.05%
35-40	17	99.26%
40-45	10	99.39%
45-50	15	99.58%
50-55	10	99.70%
55-60	7	99.79%
60-65	3	99.83%
65-70	7	99.91%
70-75	3	99.95%
75-80	4	100.00%
80+	0	100.00%



Sample Interval Histogram

Range	Frequency	Cumulative %
0	0	.00%
0-0.2	91	1.13%
0.2-0.4	326	5.20%
0.4-0.6	413	10.35%
0.6-0.8	702	19.10%
0.8-1	746	28.40%
1-1.2	611	36.01%
1.2-1.4	1007	48.57%
1.4-1.6	2381	78.25%
1.6-1.8	260	81.49%
1.8-2	338	85.70%
2-2.2	159	87.68%
2.2-2.4	134	89.35%
2.4-2.6	103	90.64%
2.6-2.8	80	91.64%
2.8-3	40	92.13%
3-3.2	485	98.18%
3.2-3.4	29	98.54%
3.4-3.6	11	98.68%
3.6-3.8	21	98.94%
3.8-4	23	99.23%
4+	62	100.00%



12. Sampling Method and Approach

There is no written record regarding the sampling method employed during the early exploration years (i.e.: pre-1970's) in the Scotia Mine area.

The exploration approach and sample collection procedures employed by the more recent exploration efforts reflects thorough sampling methodology and documentation procedures. Exploration activity was carried out in a professional manner by a team of local, experienced geologists and technicians supervised by Esso's, Seabright's, Westminer's, Savage's and ScoZinc's professional staff. The work has been well organised throughout their exploration efforts and more recently computer facilities were available to generate reports and prepare maps, etc. from the vast database.

The assay data and other parameters for all core drilling programs and underground work were entered into a computerised database using Microsoft Excel and resource-generating software programs. The quality control and validation of the coded data included steps to ensure that the assay intervals and the sample locations were correct. To ensure accuracy of the database, all assays were coded and the data entry system automatically checked for interval overlaps. The coded assays were also printed and a visual inspection was completed for comparison with the original (logged) data sheets. The sample locations were validated with appropriate plotting and visual checks against the original sections and plans.

Core drilling was carried out using North American service providers with the collection of BQ and NQ core. The portions of core to be analysed were either split or sawed into two sections with one half submitted for analysis, the other half remaining in the core tray. All sampling procedures were carried out on site.

Sampled core lengths were determined visually. All drill holes were logged, noting lithology, structure, alteration and mineralisation. Core recovery was generally greater than 90 %. Early in the exploration program, the samples were been sent via air cargo to several analytical laboratories; however, after the construction of the mill facility, the internal laboratory was used.

13. Sample Preparation, Analysis and Security

Core samples from Savage's 1997 drilling program and ScoZinc's 2004 drilling program were submitted to the Minerals Engineering Centre of Dalhousie University (formerly Technical University of Nova Scotia) in Halifax. The laboratory was not International Standard Organisation (ISO) accredited.

According to the Minerals Engineering Centre; the core sample preparation procedure was as follows. The samples were dried, and then crushed in one or more jaw crushers, depending on the original size, to under one-quarter inch. The sample was then split in a Jones riffle to a mass of 150-200 grams. The sample was then pulverised using a ring and puck pulverisor to 80 % minus 200 mesh (75 microns). Then it was put into either a bag or a vial. Rejects were kept for six months.

The sample analysis procedure consisted of the following: one gram sample lots were digested with hydrochloric-nitric-hydrofluoric-perchloric acids. Elements were determined by Flame Atomic Absorption with detection limit of 1 ppm. Arsenic was determined by atomic absorption/hydride generation method.

Soil and rock samples may also be digested with aqua regia only to partially extract soluble elements. On a 10 gram sample, the detection limit is 0.1 ppm for base metals. The arsenic detection limit is 1 ppb on a 10 gram sample using the hydride generation atomic absorption technique.

Reference standards from CANMET were routinely used as internal checks on the accuracy of the analysis.

14. Data Verification

The author has reviewed the sampling results and verified that the sample types and density are adequate for establishing Resources and Reserves. The sampling results are representative of the mineralisation. The available information and sample density allow a reliable estimate to be made of the size, tonnage and grade of the mineralisation in accordance with the level of confidence established by the Mineral Resource categories in the CIM Standards.

14.1 Database Validation

A sample of 59 drill holes (4.3%) was selected for database validation. The collar locations, downhole survey data, geological logs and assay data in the database was compared against the original, written logs.

14.1.1 Methodology

ScoZinc provided scanned original drill logs in Adobe .pdf format. An up-to-date copy of the electronic database of all drill hole information was also provided. An additional data file of drill hole co-ordinates was supplied as many of the original drill logs did not have co-ordinates.

A total of 59 holes were selected (Table 14). Most of the holes were located within areas with the highest economic potential, but the selection process also strived to provide good coverage for the whole deposit. This amounted to 4.3% of the more than 1400 holes drilled on the property.

Print-outs were made of the relevant sections of each of the holes and also of the assay data of the corresponding assay intervals The assays were printed on the reverse of the drill logs. Co-ordinates on the log and database were manually compared.

14.1.2 Results

The data in the Excel database and original drill logs were manually compared. They were found to be, for the most part, comparable. Many of the original drill logs, both underground and surface, did not have collar co-ordinates or downhole survey data. Another database was located that contained the required information. It is more than likely that the holes were surveyed and the information filed in a separate location from the original logs.

Table 14: Holes that were verified during the database validation.

S61	S352	S613	S882	U047	U206
S69	S390	S634	S938	U057	U217
S71	S404	S648	S939	U061	U218
S85	S423	S663	S943	U073	U246
S94	S431	S690	S956	U087	U259
S110	S466	S703	S975	U093	U290
S183	S473	S705	S976	U106	U297
S220	S555	S726	S980	U129	U321
S251	S568	S843	U003	U148	U337
S268	S574	S857	U008	U174	

The following holes were found to have discrepancies between the original data from the drill logs and the final database:

S 69
Data base 73.76-75.59 lead 0.01% Original Log 73.76-75.59 lead 0.32%

S110
Assay data for database match that on original log. However, a hand-written correction on the log shows reduced lead and zinc values.

S 663
Minor sample depth errors - not significant.

S703
Assays on original log for interval 89.0-99.83 metres not shown. These were likely assayed at a later date.

S 726
Assay section on original log 77.72- 83.82 m (6.1m) used on database. Original log interval was corrected by hand at a later date to 2 ft. (0.61m)

U 129
Sample from 115'-125' (10') misread as 115' -128' (13'). Written entry on original log looks like 128'.

U218
Azimuth on database shows 235 degrees, which is consistent with other angle holes with the same co-ordinates. However, a listing in another database shows an azimuth of 180 degrees. It is more than likely that the database listing is correct.

14.1.3 Conclusion

With the exception of Hole S 110 and S 726 where significant assay intervals and values were involved, the remainder of the holes do not represent any factor that would change the status of the deposit. In general, the data transfer from the original logs was of high quality and the database was considered a valid representation of the mineral deposit.

14.2 Verification Sampling

The Scotia Mine property was visited by Mr. Reg Comeau of ACA Howe (Howe) on June 17 and June 21 and on September 22 and September 26, 2004 in order to become familiar with the area and to conduct verification sampling on the property. Split, random, core samples were inspected and sampled from the site on the second visit from the 2004 drilling campaign in the area of the proposed low grade open pit in the central portion of the deposit as well as the higher grade zone in the Northeast zone. A second set of core samples from the 1997 drilling campaign were later collected by Mr. Doug Roy.

Samples from 1997 and 2004 drilling campaigns were collected, packaged and independently shipped by Reg Comeau. All samples were taken from the remaining half core samples in the core boxes and were sawed in half reflecting a quarter core sample. The remaining quarter

core was left in the core tray. The samples were packaged and shipped to ACA Howe's office in Toronto, then shipped to and analysed by SGS Toronto. The comparison of assay results is shown in Table 15.

SGS is an internationally recognised organisation that operates over 320 laboratories world-wide and has ISO 9002 certification for many of their laboratories. In North America, the central laboratory is located in Toronto with specialised laboratories located in Red Lake, Ontario and Rouyn-Noranda, Quebec. The SGS Toronto office is an ISO 9002 registered geochemical laboratory and the centre for SGS' international geochemical network.

Each SGS Canada branch office specialises in areas of independent testing, inspection and certification services. SGS Canada is certified or accredited by a wide variety of independent, third party programs such as Agriculture Canada, the Standards Council of Canada and ISO 9000. The comparison of analytical results between SGS and the original 1997 samples and the samples from the 2004 drilling program (analysed at Minerals Engineering Centre of Dalhousie University) was excellent. The author is satisfied that the assay data base for the property is sound and sufficient to guide the next exploration phases of the programs.

Table 15: Results of verification sampling.

				Original Assay		Howe Sampling	
Hole #	**From (m)**	**To (m)**	**Interval (m)**	**% Zn**	**% Pb**	**% Zn**	**% Pb**
2004 Drilling Program by ScoZinc							
Pit Area							
S968	2.70	4.70	2.00	3.38	0.29	3.62	0.14
S969	8.00	10.00	2.00	2.15	0.00	2.22	0.00
S971	2.90	4.90	2.00	4.63	0.00	3.91	0.00
S972	14.30	16.30	2.00	1.86	0.18	2.06	0.17
S973	74.00	75.00	1.00	11.90	14.98	14.18	17.25
S974	66.80	68.00	2.00	2.46	2.22	2.59	1.95
S976	98.10	98.45	0.35	7.66	0.23	7.19	0.17
Northeast Zone							
S977	96.00	96.40	0.40	6.77	0.01	9.47	0.01
S982	133.30	133.60	0.30	0.84	0.32	0.84	0.18
1997 Drilling Program by Westminer							
Pit Area							
S926	18.40	19.90	1.50	2.82	0.01	3.16	<0.01
	19.90	21.40	1.50	3.27	0.01	2.86	<0.01
S933	12.10	13.60	1.50	1.40	0.01	1.47	0.01
	13.60	14.90	1.30	2.78	0.01	2.45	<0.01
S936	8.50	9.80	1.30	3.73	0.01	4.20	<0.01
	11.00	12.20	1.20	1.02	0.01	0.98	<0.01
Northeast Zone							
S943	60.75	62.00	1.25	7.56	2.63	6.95	2.76
	62.00	63.00	1.00	3.16	5.70	2.78	3.30
S950	36.00	37.15	1.15	5.20	3.02	3.99	2.19
	37.15	38.25	1.10	17.37	1.07	15.54	0.67
S953	91.80	92.65	0.85	4.41	7.34	3.97	7.47

15. Adjacent Properties – Getty Deposit

The "Getty Deposit" is located on contiguous land to the immediate northwest of the Scotia Mine deposit on lands presently set aside by the provincial government (Figure 3). The deposit was discovered at approximately the same time as the Scotia Mine deposit by a joint venture enterprise consisting of Getty Mining Northeast Limited and Skelly Mining Company.

A potentially viable lead zinc deposit was outlined which, although perhaps not economic on its own, might prove successful if incorporated as part of the ScoZinc overall resources. Both open pit and underground areas of potential development have been defined.

Drilling activity defined potential lead-zinc ore in one, possibly two, open pitable zones and in two possible underground zones. The deposit overlies a northward projecting segment of the Meguma greywacke high that continues south-westerly through the Carrolls Corner area. An irregular conglomeratic and breccia unit at the base of the Windsor Group locally overlies the basement and is in places interbedded with units at the base of the overlying carbonate section. Thicknesses as great as 30 metres are attained in what may represent talus-type deposition. The conglomerate is composed of angular to sub-rounded and unsorted Meguma Group lithologies cemented by finely crystalline dolostone. The contact with overlying carbonates of the Windsor Group is often gradational with Meguma clasts decreasing in quantity upwards until only carbonate is present.

15.1 Geology

When Mississippian seas covered this area, the biogenic activity was concentrated along, around and on top of this and other basement highs. Local reefal development occurred and it is mainly within these reefal carbonates that the lead-zinc mineralisation is located. The carbonates are predominantly dolostone. Buff to grey, finely bedded algal units account for much of the carbonate accumulation. Irregular zones rich in brachiopod, gastropod and bryozoa assemblages and algal stromatolites and coral growth account for the remainder of the carbonate build-up.

The northward projecting, undulating reefal structure now covers an area approximately 1,250 metres east-west by 600 metres north-south. The reef developed along the flanks of, and eventually over most of the Meguma basement high during early Mississippian time. Carbonate accumulations are minor near the axis of the basement high and then to a maximum of approximately 40 metres on the flanks. The reef may have extended much higher prior to erosion. From the present maximum thickness along the flanks the carbonates rapidly thin basin ward to less than 2 metres within a lateral distance of as little as 60 to 70 metres. Further out from the basement high the carbonate grades laterally into muddy carbonate, limy shale, mudstone and non-calcareous sandstones.

A thick evaporitic sequence with minor shale and carbonate beds pinches out against the reefal carbonates overlying the basement high. As a result, the evaporite beds are usually thinnest near the Meguma high and rapidly thicken with distance away from the reef.

Although the evaporite beds are thin or absent on top of the basement high, the thickness exceeds 400 metres about 1 kilometre of the seaward side of the reefal complex.

The deposit is overlain completely by poorly sorted glacial till, the thickness of which ranges from 3 metres to 100 metres. The maximum thicknesses are encountered in the evaporite pinch-out zone.

15.2 Mineralisation

Lead-zinc mineralisation has been delineated within three separate zones on the original Getty/Skelly lands but confined to a more or less continuous reefal complex. The Southeast mineralised zone lies immediately south of the village of Gays River and is an extension of the original Gays River deposit. Both the central and southwest zones are west of the main highway. The central zone is crescent-shaped and conforms to the shape of the reefal complex developed around the northerly protruding paleo-topographic high. Minor mineralisation has been located between the three main zones.

Sulphide mineralisation is found throughout the reefal carbonate complex as well as in the carbonate matrix of the underlying conglomeratic unit. Galena and sphalerite are the main sulphide minerals with pyrite, marcasite and chalcopyrite present in minor to trace amounts. Strong zones of mineralisation occur throughout all sections of the conglomeratic and reefal rock units with no apparent preference for specific horizons. There is, however, a tendency for the higher grade mineralisation to occur along the flanks of the carbonate reef which appears to represent the general fore-reef area. The Gays River deposit also contains its more massive mineralised zones along the fore-reef area to the northwest of the reefal trend with lesser amounts of ore-grade material along the reef crest.

The sphalerite is honey yellow to light buff, finely crystalline and generally tends to occur as irregular disseminations in weak to intense concentrations varying from discrete segregated crystals to concentrations greater than 10% but can also occur as semi-massive to massive seams along bedding planes, coating fossils, and infilling vugs.

Galena is less abundant than sphalerite and often occurs as fine to medium size cubic crystals. It is found throughout the carbonate and conglomeratic sections most commonly as irregular disseminations in high to low concentrations as discrete crystals to concentrations greater than 10%. It also commonly occurs as irregular veins and semi-massive to massive seams.

Based on a 1.5 % zinc-equivalent cut-off grade (1 % Pb = 0.6 % Zn in 1975 and a minimum core length of 3 metres) resources at the Getty deposit were estimated by Hudgins and Lamb (1992) at 4.5 million tons at an average grade of 1.3 % Pb and 1.9 % Zn.[7]

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[7] The resource estimates referred to in this section are historical in nature and are quoted as such. These estimates have not been reviewed by the authors of this report and thus should not be relied upon.

16. Mineral Processing and Metallurgical Test Work

Within the mill building, in addition to the lead and zinc processing equipment, is a complete analytical and metallurgical laboratory. Provision for replacing some of the analytical equipment have been made in the capital cost section (Section 19.12) of the economic analysis.

The very high grade of the concentrates, coupled with the absence of any appreciable amount of elements that complicate the smelting process, make the concentrates desirable material for smelter operators. In the past, WMC trucked the concentrates from the mine site to the storage and loading facility at Sheet Harbour. Rail transport facilities have also been used.

Scotia Mine's past production history is reported in Table 9. The expected metallurgical balance, based on the past performance of the mill, is reported in Table 16. A complete description of the mineral processing operation is reported in Section 19.3.

Table 16: Metallurgical balance.

		Assays		Metal Content		Metal Distribution	
Product	Weight Percent	Percent Lead	Percent Zinc	Units of Lead	Units of Zinc	Percent Lead	Percent Zinc
Lead Concentrate	1.8%	75.0%	4.0%	1.33	0.071	95.0%	1.8%
Zinc Concentrate	6.1%	0.4%	60.0%	0.024	3.64	1.7%	91.0%
Tailings	92.2%	0.05%	0.31%	0.046	0.289	3.3%	7.2%
Feed	100.0%	1.4%	4.0%	1.40	4.00	100.0%	100.0%

Based on head (mill feed) grades of 1.4 % lead and 4.0 % zinc.

17. Resources

Surface Resources were calculated by Tim Carew, P.Geo., who was a co-author of this report and is a Qualified Person under Section 1.1 of National Instrument 43-101.

Underground Resources, in the Northeast Underground Zone, were calculated by Douglas Roy, M.A.Sc., P.Eng., who was this report's Principal Author and is a Qualified Person under Section 1.1 of National Instrument 43-101.

17.1 Surface Resources

17.1.1 General

The deposit is characterised by complex geometry and is difficult to model in terms of standard techniques. Lying along a 'paleo-shoreline', it features repetitive changes in strike of 90º and more around a general trend of 060º Azimuth, and with varying dip.

The deposit has been mined by underground methods in the past and is therefore intersected by numerous openings along the hanging wall contact. This geometry makes it difficult to incorporate the true spatial relationship of the samples for estimation purposes without the use of 'unfolding' techniques that transform the sample data into another co-ordinate space that honours the spatial relationships. Variography and estimation are conducted in the transformed space, and the results are then back-transformed into the original space.

17.1.2 Geological Modelling Approach

The drill-hole data entered in the database was displayed in 3D graphics mode (G4W), and a number of triangulated surfaces (TINs or Triangulated Irregular Networks) were created to represent the base of the overburden, and the lower and upper contacts of the carbonate (ore) horizon. The surfaces were developed by selecting the relevant down-the-hole intersects (with interactive inspection and adjustment), and calculating a best-fit plane through the data points derived. The selection process for the underground holes was complicated by the fact that some holes were drilled from footwall to hanging-wall, and some in the opposite direction. To assist in differentiating the contacts, a new field (T/B) was added to the Geology table of the database to contain a numeric code designating the contact as either a top or bottom contact. Codes were also defined to designate carbonate intervals that were either the first or the last interval in a hole, indicating that the hole had been either collared or ended in carbonate. The codes were calculated by a formula in the original Excel spreadsheets and then merged into the 'T/B' field in the Geology table. The drill-holes were grouped by orientation (vertical up, vertical down and inclined) to further facilitate this process. A smooth 3D surface through the active data was then created by Laplace interpolation, relative to the best-fit plane.

Topographic contour data derived from the AutoCAD drawing files provided was utilised to create a TIN of the original topography over the project area.

A 3D solid of the carbonate formation was initially created from the top and bottom surfaces developed above. In the initial absence of detailed geologic plans and sections, the surfaces used were based solely on drill hole intersections. The drill holes utilised were the surface holes, up-holes from underground, and horizontal underground holes that had clearly defined 'top' and 'bottom' contacts, as designated by the 'TJB" numeric code described above. A set of 3D solid models of the existing underground development and stope areas developed by Mr. Bruce Hudgins of Hudgtec Consultants was imported from the AutoCAD DXF files provided. It should be noted that these solids could not be validated in G4W, indicating that they were probably not completely closed. This problem again reflects the complexity of the models, but does not significantly affect the results of volume determinations or block model 'stamping' in G4W.

Subsequent Inspection of the 3D solid in section and plan indicated that although the overall geometry of the deposit was being honoured, there were significant variances from existing manual interpretations and underground mapping in a number of areas. After a number of re-interpolations utilising both drill-hole and digitised data, it was concluded that inconsistencies in lithological coding in the drill holes would negate the contact modelling approach.

It was further decided that manual interpretation was required, and that the ore zone be differentiated into a high-grade massive sulphide zone and a low-grade disseminated zone. Drill-hole data and underground openings were then plotted on hard-copy plans at ten metre intervals, and interpretations of the high-grade zone, the low-grade and the hanging-wall 'Trench' were produced. The cut-off grades that were for the high- grade and low-grades zones were 7% Zn-Eq and 2% Zn-Eq respectively. These values were selected to correspond with cut-offs utilised in earlier resource evaluations. The plan-view interpretations were digitised as closed polygons, then tied together in the solids modelling system to create separate 3D solid models of the high-grade, low-grade and trench zones of the deposit. This work was completed by Mr. Peter Irwin, of Resource Data Management Inc., under contract to Savage Resources Canada Co. The geometric complexity of the deposit is reflected in the large number of tie lines required to adequately control the triangulation process utilised to create 3D solid models. The modelling was, therefore, time consuming but produced valid solids for the ore and trench zones. These models were adopted for use during the previous resource estimate in 1998 (Carew, 1998) and again for the current resource estimate.

17.1.3 “Unfolding” Process

As stated in Section 17.1.1, the deposit is characterised by complex geometry and is difficult to model in terms of standard techniques. An ‘unfolding’ technique was used that transformed the sample data into another co-ordinate space while honouring the spatial relationships.

The Gemcom® unfold application was used for the transformation in this case. This approach is based on the concept of slabs – a slab being a region of space that is topologically equivalent to a cube. The edges are 3D polylines and are not necessarily straight from end to end. Each face is defined by four polylines on its perimeter and the nominally vertical edges of the slab may also have more than two points. The geological feature of interest, e.g. a folded and/or faulted vein or seam is broken down into a collection of adjacent slabs, the only

proviso being that any two adjacent slabs must share an entire common face. The algorithm highlights three of the edge polylines of a representative slab that are nominally orthogonal and allows them to be associated with X, Y and Z axes of the unfolded space. All of the polylines are then categorised into three sets of lines corresponding to these unfolded axes. The unfolded slabs are displayed below the original polylines, and the unfolded lines will be aligned approximately to the X. Y, and Z axes. The average length of each of the sets is calculated and a nominal graticule size, or spacing, is entered. The unfolding transformation includes two graticules – one for the folded region and one for the unfolded region. The points in the two graticules have an exact 1:1 correspondence, which provides for a check that the transformation will be reasonable. If any graticule cells are highly skewed, for example, the folded region can be subdivided into smaller slabs. In addition, the interior vertices can be allowed to slide on the various sets of lines in order to minimise distortion.

The graticule points are simply samples of the transformation, and are connected by straight lines to make the visualisation easier. Various combinations of the sliding axes can be experimented with, particularly in cases where the polyline lengths along the feature are different, in order to minimise the distortion in these cases. The 3D polylines were generated by contouring the 3D solid of the mineralised carbonate developed for the deposit in earlier studies at 10m plan intervals, as the original polylines are no longer available. These polylines were subdivided into a series of smaller adjacent slabs corresponding to the alternating strike direction of the deposit. A section showing the slabs and the allocation of the association with the unfolded axes is illustrated in Figure 16. The unfolded space is illustrated later in Figure 21.

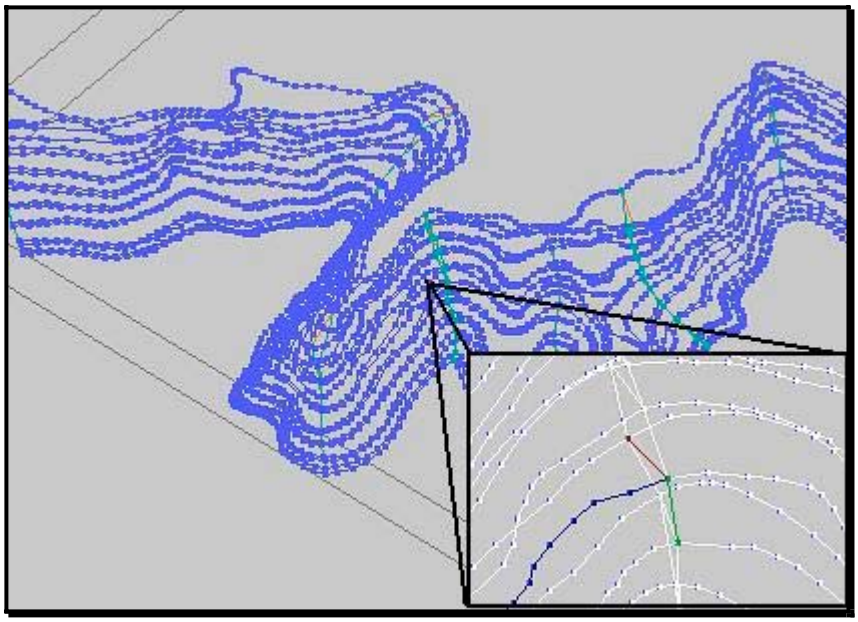


Figure 16: 3D Polyline slabs and axes.

The basic procedure is as follows:

- Creation of the unfolding transformation;

- Forward transformation (unfold) of the sample data points;
- Variography and block modelling in the transformed space;
- Back-transformation of the estimated block data (Zn and Pb) into normal (folded) space; and,
- Allocation of the values to a block model in normal (folded) space by nearest neighbour interpolation.

17.1.4 Drillhole Data

A subset of the overall drillhole database was utilised for estimation purposes, comprising those drill holes that intersected the 3D solid model of the carbonate mineralisation. This subset comprises 623 holes and includes both surface and underground drilling.

17.1.5 Mineralised Envelope

The mineralised envelope for estimation purposes was restricted to the carbonate material within the 3D solid models created from plan view interpretations. These interpretations and 3D model are regarded as the most representative constraints on the mineralisation available. Separate 3D models were developed for the low grade, disseminated portion of the deposit, and for the less continuous high grade zone that lies along the footwall contact, and which was exploited by previous underground mining.

17.1.6 Statistical Analysis and Capping

The sample sets for zinc and lead mineralisation comprised those assay intervals falling within the 3D solids and were compiled separately for the low-grade (LG) and high-grade (HG) zones. The sample statistics, histograms and probability plots are shown in Figure 17 and Figure 18.

While both Zn and Pb assay grades exhibit fairly typical positively skewed distributions, the Pb values exhibit evidence of a multi-modal distribution, with a set of values falling in the 0.01 to 0.1% range - this may be related to the use of arbitrary and variable values for detection limits in the Pb data. In general, Zn and Pb values are not particularly well correlated, with a correlation coefficient of 0.32. There is also some evidence of possible misclassification of some values between low grade and high grade zones in both cases, either in terms of original typing, or in geometric boundary effects relative to the 3D solids. The Zn values are generally well behaved, with relatively low Coefficients of Variation (COV), whereas the Zn values exhibit a relatively high COV.

Whereas initial studies on the deposit by Savage Resources Canada Co. considered a capping value of 13% on both Zn and Pb, examination of the probability plots indicates that although the number of high values steadily decreases, the upper tail for the all distributions are fairly continuous and unbroken up to values considerably higher than this, suggesting that higher capping values could be utilised. In later studies, discussions with Savage personnel led to an alternative approach in which the high-grade outliers in the distributions were retained in the

data set prior to any compositing, but severely restricted in terms of interpolation. Block centroids were required to be within 5 metres of the sample before it could be used in the estimation of the block in question. Given the indication that higher capping values could be considered, and to maintain consistency, this approach was retained for this study. No grade capping was applied prior to compositing, but the range restriction was subsequently applied in estimation for Zn and Pb composites above 26%.

Figure 17: Zn and Pb assay lognormal histograms.

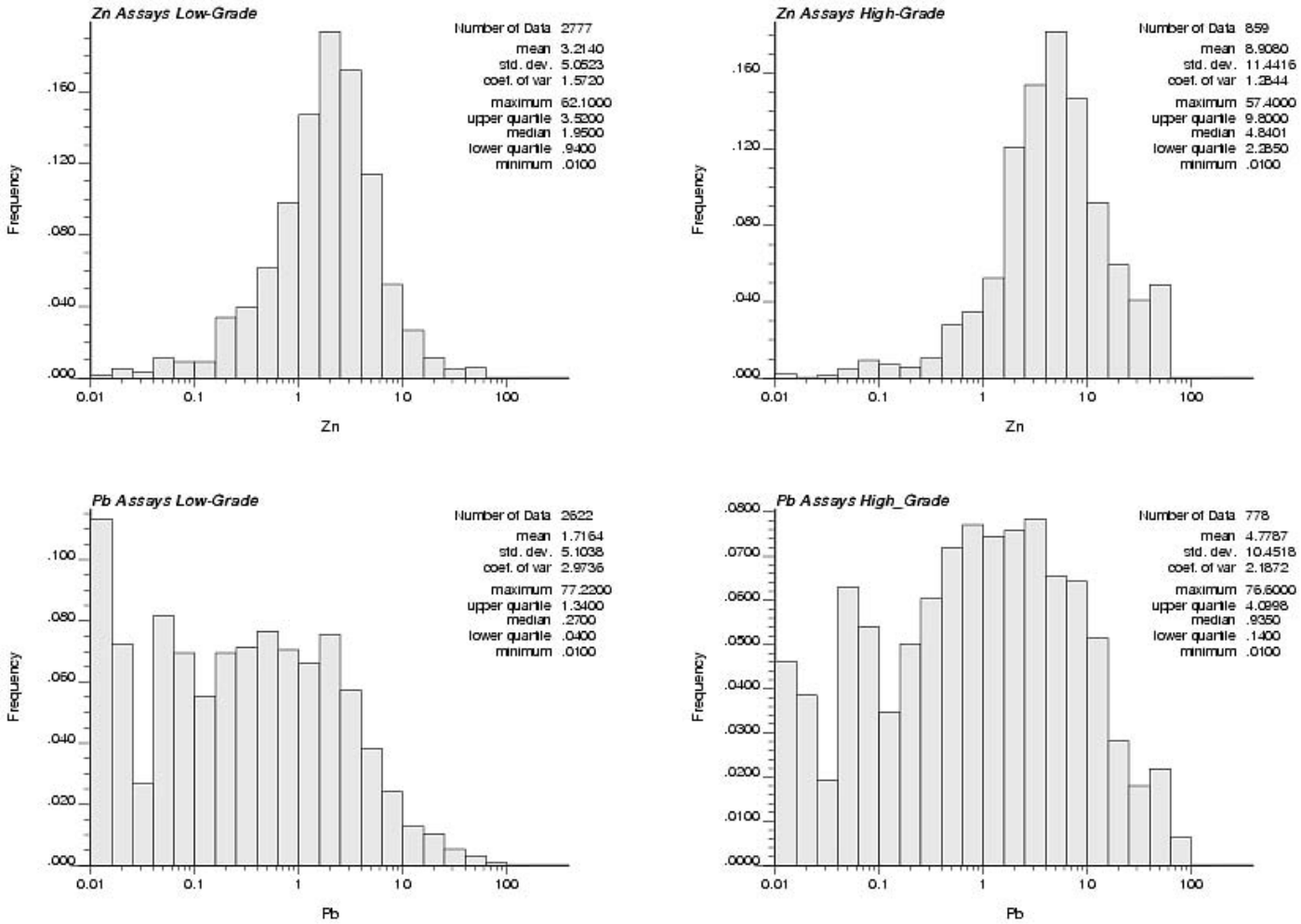
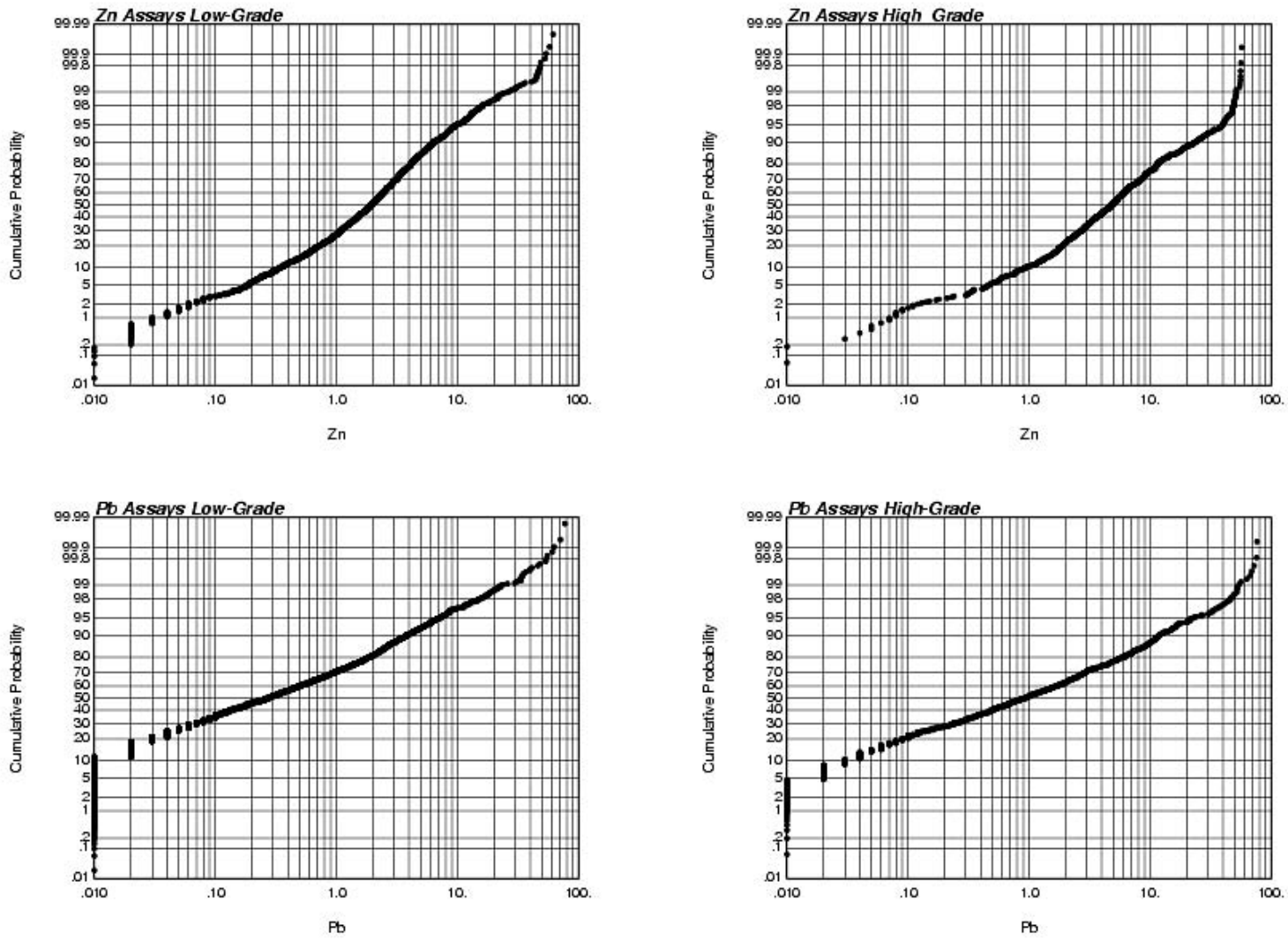


Figure 18: Zn and Pb assay probability plots.



17.1.7 Compositing

Equal length composites were prepared from uncut assay values in a two step process. Initial composite intervals were defined from the intercepts of the drill holes with the high-grade and low-grade 3D solids of the mineralised zone. Equal length composites of 1.5 metres were then generated within these intervals – 1.5 metres is approximately the average length of the assay intervals. Residual intervals of less than 1.5 metres at the top and bottom contacts were retained if the length was at least 0.6 m (40% of composite length). Intervals less than 0.6 m in length were discarded. The low-grade composites set was further subdivided into those falling below 490 m elevation (below which the deposit dips at varying angles) and those above 490 m where the deposit is essentially flat-lying. The composite statistics and histograms for the overall high grade and low grade Zn and Pb are shown in Figure 19.

17.1.8 Variography

Three dimensional experimental correlograms were generated using the transformed (un-folded) Zn and Pb composite data, for both low-grade and high-grade mineralised zones below an elevation of 490 m. Separate 3D experimental correlograms were generated using un-transformed composite data for the low-grade mineralised zone above 490 m elevation, where the deposit is essentially horizontal in attitude. Nested correlogram models comprising nugget effect and two spherical components were fitted to all experimental variograms as tabulated in Table 17 and shown in Figure 20.

Table 17: Correlogram models.

		Spherical components						
			Ranges					
	Nugget		Maximum		Intermediate		Minimum	
Zone	Effect	Sill	m	Az/Dip	m	Az/Dip	m	Az/Dip
LG – Zn <490	0.337	0.103	48	181/-4	11	232/84	8	92/5
		0.560	32	258/-50	23	275/39	3	178/8
HG - Zn	0.250	0.305	231	98/20	15	133/-66	9	13/-13
		0.445	412	87/63	118	351/3	10	80/-27
LG – Pb <490	0.517	0.402	75	121/-72	7	84/15	4	177/10
		0.081	267	96/16	69	268/74	22	5/2
HG – Pb	0.579	0.270	39	78/-19	21	134/59	11	357/24
		0.151	186	126/51	170	169/-31	17	65/-22
LG>490-Zn	0.306	0.443	46	174/-2	21	262/44	4	85/46
		0.251	442	239/22	30	144/0	17	59/68
LG>490- Pb	0.395	0.474	58	77/-4	20	168/-6	7	131/83
		0.131	113	222/83	61	243/-7	42	153/-3

Figure 19: Composite statistics and histograms

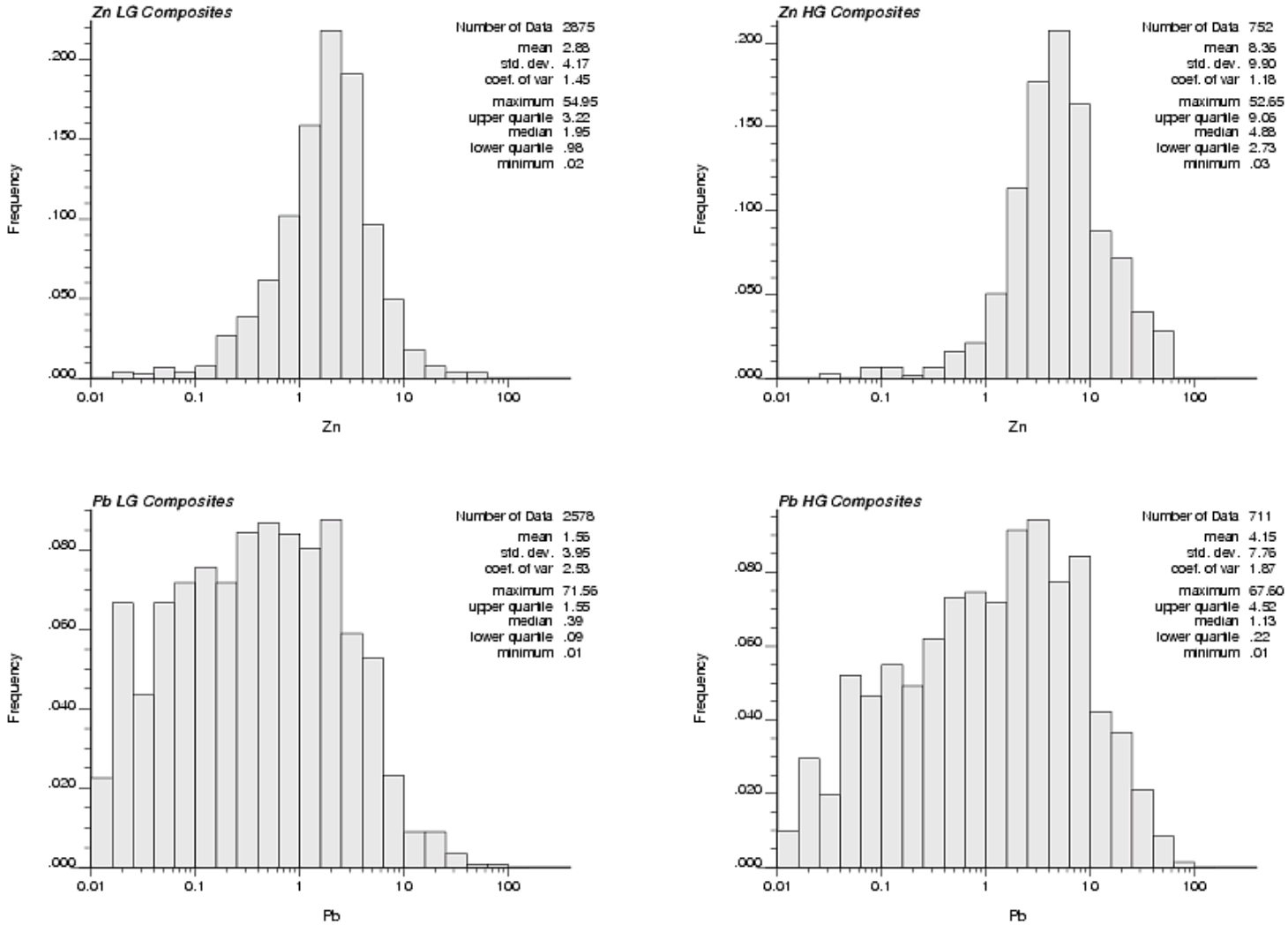
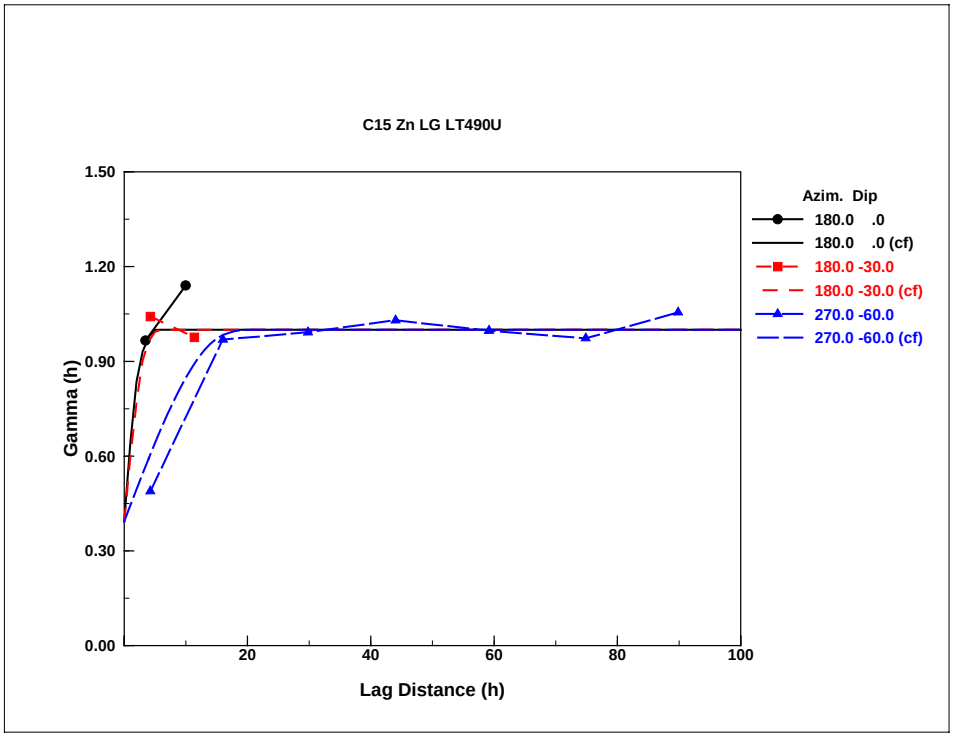
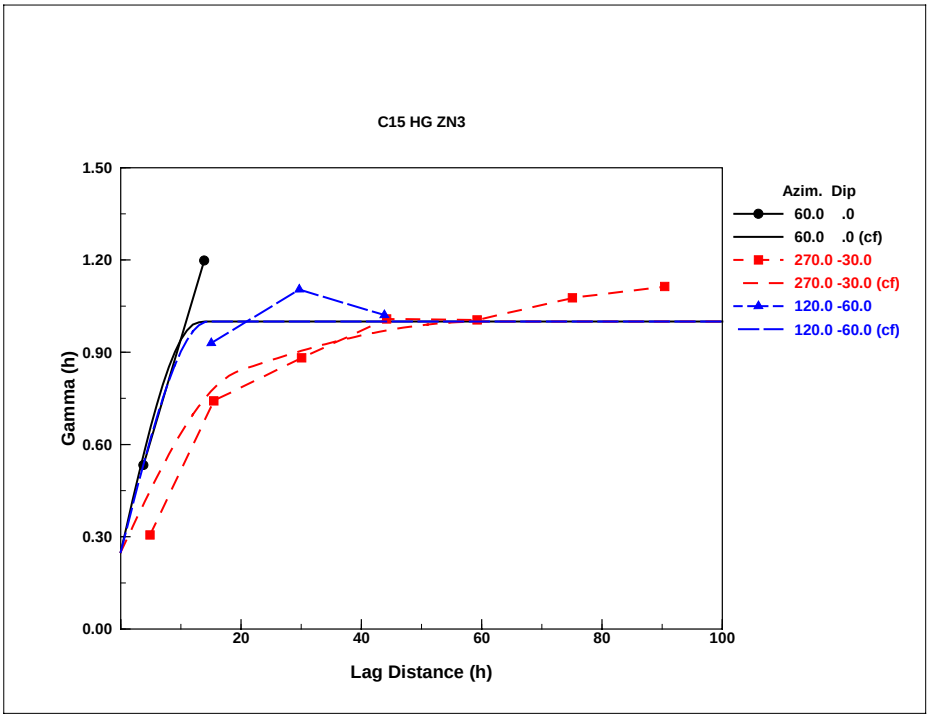
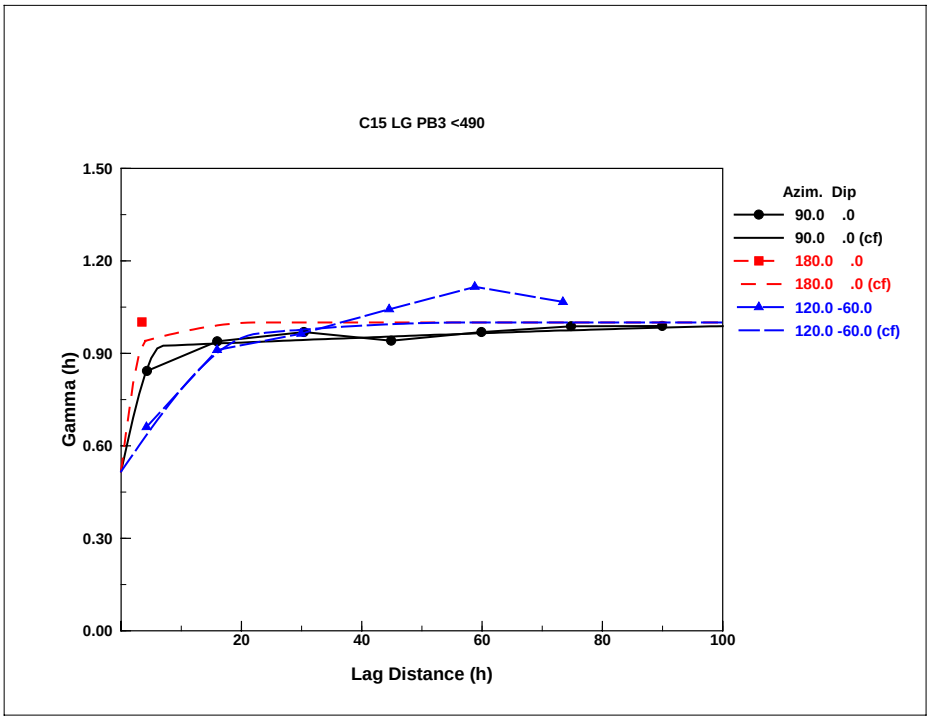


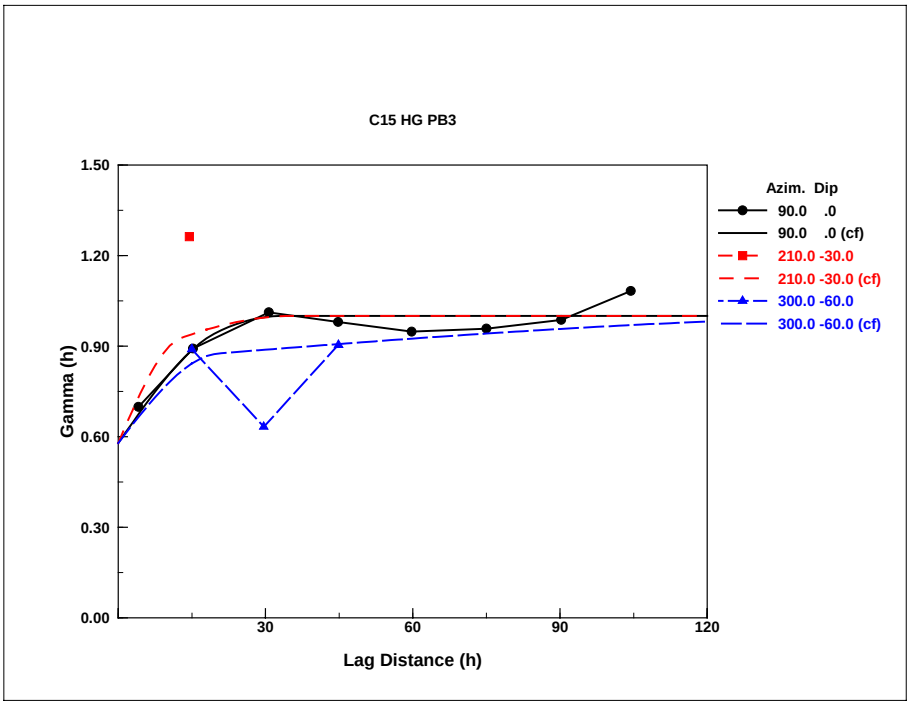
Figure 20: Experimental and model correlograms.

<u>Transformed Space - <490m Elevation</u>

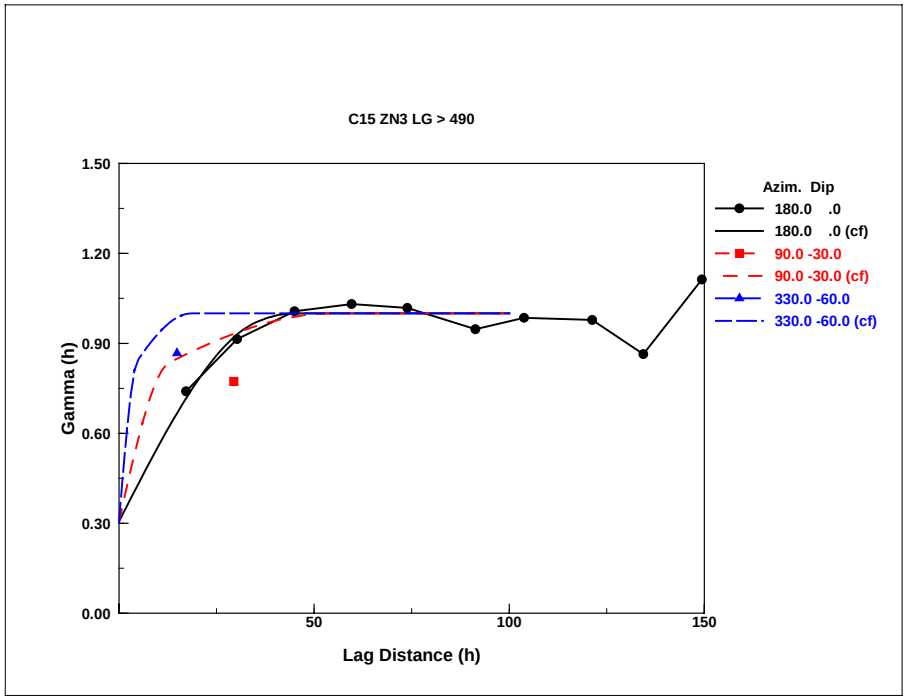


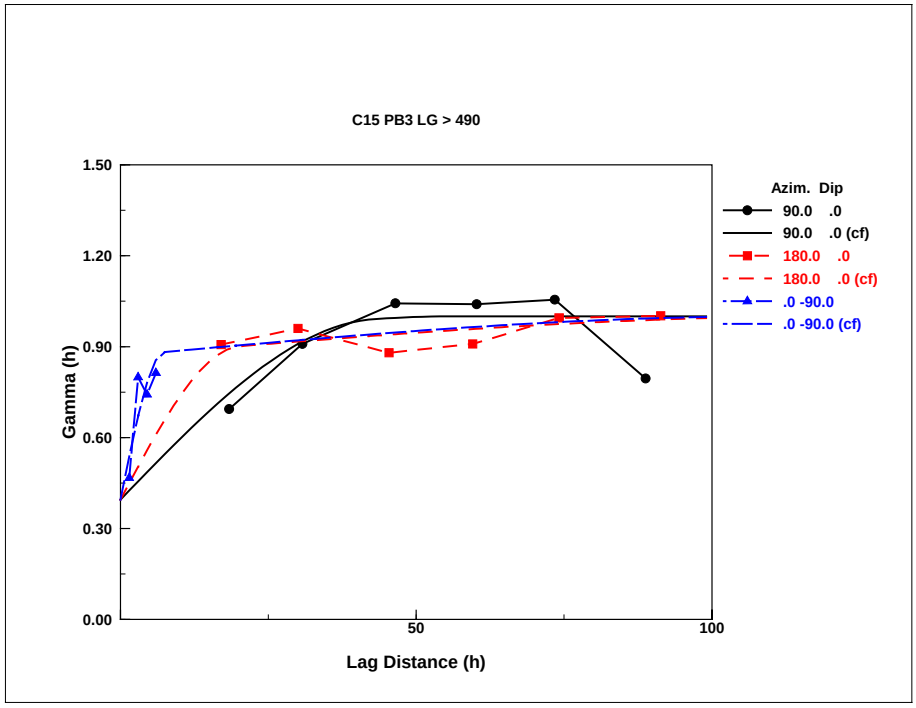



C15 LG PB3 <490
Gamma (h)
Lag Distance (h)
1.50
1.20
0.90
0.60
0.30
0.00
20
40
60
80
100
Azim. Dip
90.0 .0
90.0 .0 (cf)
180.0 .0
180.0 .0 (cf)
120.0 -60.0
120.0 -60.0 (cf)


C15 HG PB3
Gamma (h)
Lag Distance (h)
1.50
1.20
0.90
0.60
0.30
0.00
30
60
90
120
Azim. Dip
90.0 .0
90.0 .0 (cf)
210.0 -30.0
210.0 -30.0 (cf)
300.0 -60.0
300.0 -60.0 (cf)

Untransformed Space – 490m Elevation Plus





17.1.9 Specific Gravity/Density

No evidence of specific gravity test work was available. Therefore, a formula for specific gravity based on zinc and lead grades was used for the mineralised zones. This formula, which was also used by Savage Resources for their 1998 resource estimate, was:

$$\mathbf{SG = 1/(Pb\%/(86.6x7.6) + Zn\% /(67.0x4.0) + (1 – Pb\% /86.6 – Zn\% /67.0)/2.7)}$$

A default density of 2.7 t/m^3 was utilised for mineralisation where grade data was not available. The densities utilised for other materials were:

Evaporites (Average)	2.40 t/m^3
Quartzite	2.65 t/m^3
Overburden and Trench	2.00 t/m^3

17.1.10Block Model and Grade Interpolation

Two block models were constructed for interpolation purposes, a primary model in normal (un-transformed) space, and a secondary, smaller model in transformed space for interpolation of the un-folded data. The primary block model was defined to cover the volume of interest, and has the following Gemcom® parameters:

Origin:	7200.00E / 6592.82N / 375.00 AMSL (Lower Left)
Block Size:	5m x 5m x5m
Columns:	160
Rows:	400
Levels:	45
Rotation:	-60º (To align with overall strike of deposit – Azimuth 060)

The primary block model is configured as a ‘partial’ block model, which allows the percentage of various rock types within the block to be stored and utilised for manipulation and reporting purposes. The rock type model was initialised with the default rock code for air and all blocks below the topographic surface were set to the Evaporites (gypsum) rock code. The model was then overprinted with rock codes for the overburden, Trench and Goldenville (quartzite) using 3D solids created from surfaces and sectional interpretations. This rock type model is referred to as the ‘Standard’ rock type model. The final step was overprinting with rock codes for the existing U/G mining excavations, the high-grade (HG) carbonate and the low-grade (LG) carbonate. The percentage of these three material types in blocks intersecting the solids was calculated and stored separately, with the excavations having the highest priority, and the high-grade zone the next highest priority, in blocks where the solids overlapped. This procedure ensures that the mined-out material in the model is correctly accounted for. The rock code for any other material in these blocks was taken from the standard rock type model, i.e. a block on the hanging wall contact might comprise 50 % U/G excavation, 20 % HG carbonate and 30 % Trench material.

The 3D solid of the existing U/G excavations was generated by Mr. Bruce Hudgins of Hudgtec Consulting and was supplied by ScoZinc. The 3D solids of the HG and LG zones were generated by Mr. Peter Irwin of Resource Data Management, Inc. from plan interpretations. Zinc equivalent cut-offs of 2 % and 7 % were utilised for the LG and HG zones, respectively in developing the interpretations.

The standard ordinary kriging (OK) procedure was used to interpolate Zn and Pb block values in the flat lying portions of the deposit above 490 m elevation. This estimation was restricted to the LG zone, as the HG zone does not extend above this elevation. The kriging was done in three passes with parameters as follows:

Pass1

Minimum # of samples:	3
Maximum # samples:	8
Max. # samples/hole:	2 (ensures that samples come from at least 2 holes)
Search Radius/Direction:	Based on first component ranges and anisotropy

	Ranges					
	Maximum		Intermediate		Minimum	
Zone	m	Az/Dip	m	Az/Dip	m	Az/Dip
LG>490-Zn	46	174/-2	21	262/44	4	85/46
LG>490- Pb	58	77/-4	20	168/-6	7	131/83

Pass 2

Minimum # of samples:	3
Maximum # samples:	8
Max. # samples/hole:	2 (ensures that samples come from at least 2 holes)
Search Radius/Direction:	Pass 1 x 2

Pass 3

Minimum # of samples:	2
Maximum # samples:	8
Max. # samples/hole:	0 (no restriction)
Search Radius/Direction:	Pass 1 x 3

Mineralised blocks in the dipping portion of the deposit below 490 m elevation were populated separately following interpolation in transformed space and back-transformation of the generated values (at block centroids) into normal space, as described below. The back-transformed data was then used to interpolate the Zn, Pb and Classification values in normal space by the nearest-neighbour technique, separately for the LG and HG zones.

The secondary block model is a standard block model (every block has only one rock code), defined in 3D space to cover the volume of interest. As described earlier, the transformation process associates three of the edge polylines of a representative slab that are nominally orthogonal with the X, Y and Z axes of the unfolded space – this space is orthogonal with respect to the original co-ordinate axes, and offset by a specified amount. The transformation selected in this case results in a space in which the X axis corresponds to the unfolded strike component of the deposit (approximately 3050 m), the Y axes with cross-strike component

(12 m), and the Z axis with the down-dip component (143 m), as shown in Figure 21 and Figure 22, which also show transformed and un-transformed composite data.

Figure 21: 3D view - transformation and block model definition.

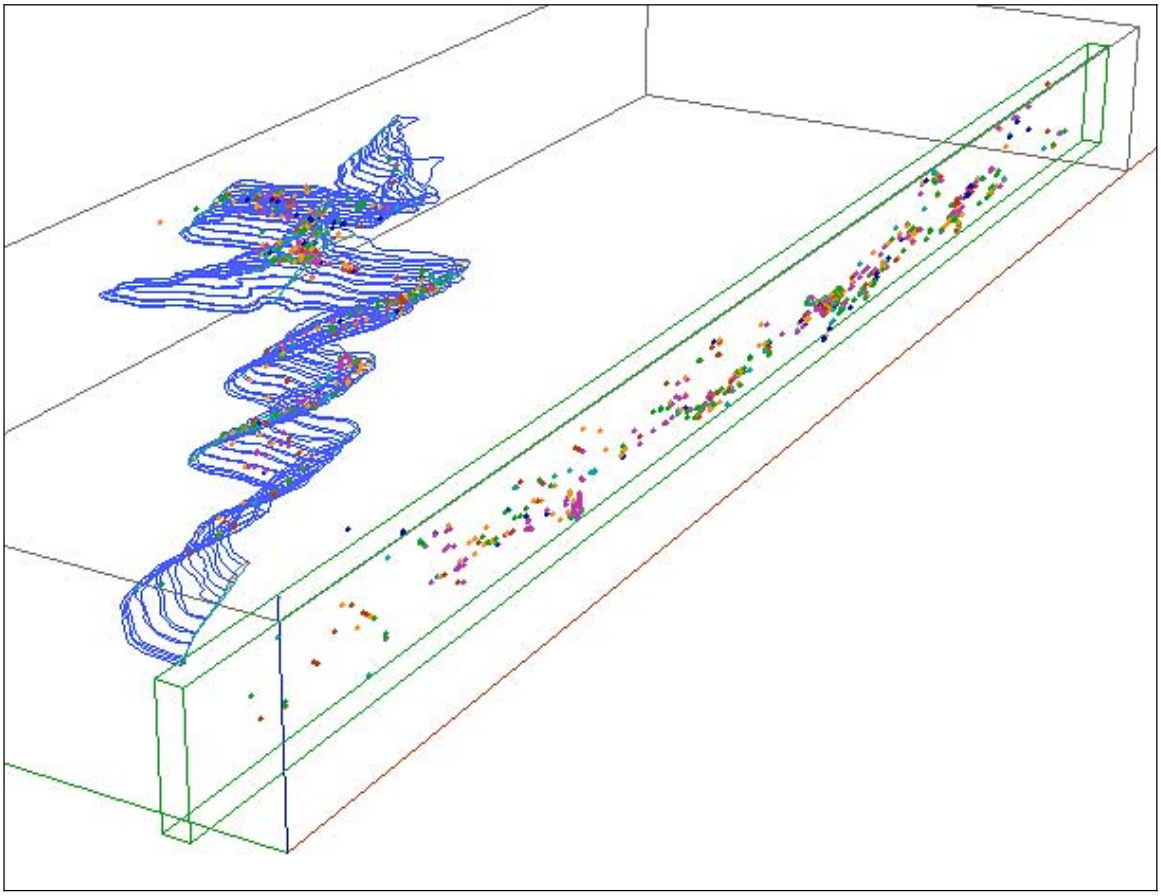
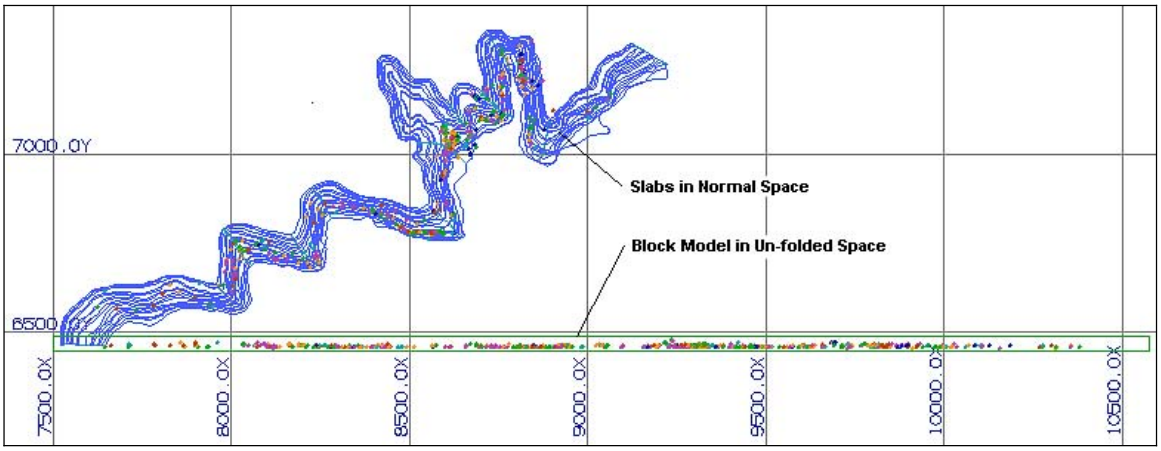


Figure 22: Transformation - plan view.



The secondary block model definition is as follows:

Origin:	7500.00E / 6450.00N / 200.00 AMSL (Lower Left)
Block Size:	7.5m x 5m x5m
Columns:	410 (7.5m)
Rows:	8 (5m)
Levels:	40 (5m)
Rotation:	No rotation

Separate interpolations of Zn and Pb block values for the LG and HG zones were kriged in three passes using ordinary kriging (OK), the transformed composites and the correlograms generated from those composites. The parameters were as follow:

Pass 1
Minimum # of samples: 3
Maximum # samples: 8
Max. # samples/hole: 2 (ensures that samples come from at least 2 holes)
Search Radius/Direction: Based on first component ranges and anisotropy

	Ranges					
	Maximum		Intermediate		Minimum	
Zone	m	Az/Dip	m	Az/Dip	m	Az/Dip
LG – Zn <490	48	181/-4	11	232/84	8	92/5
HG - Zn	231	98/20	15	133/-66	9	13/-13
LG – Pb <490	75	121/-72	7	84/15	4	177/10
HG – Pb	39	78/-19	21	134/59	11	357/24

Pass 2
Minimum # of samples: 3
Maximum # samples: 8
Max. # samples/hole: 2 (ensures that samples come from at least 2 holes)
Search Radius/Direction: Pass 1 x 2

Pass 3
Minimum # of samples: 2
Maximum # samples: 8
Max. # samples/hole: 0 (no restriction)
Search Radius/Direction: Pass1 x 3

An additional block model variable (Class) was updated according to the pass in which the block was interpolated; with a default value of 3. The Zn, Pb and Class block values were then back-transformed into normal space, using the block centroid as the 3D co-ordinate. These points do not correspond to block centroids in the original rotated block model and are used as input data in the nearest-neighbour interpolation to assign values to corresponding models in the primary model. The HG and LG models are interpolated into separate grade models associated with the percentage models that store the percentage of HG and LG material in a particular block.

The primary density model for the mineralised zone was then generated, utilising the Zn and Pb block values and the formula:

SG = 1/(Pb%/(86.6x7.6) + Zn% /(67.0x4.0) + (1 – Pb% /86.6 – Zn% /67.0)/2.7)

The Zn and Pb block values were also used to generate a zinc equivalent model (Zn-Eq) using the following formula:

Zn-Eq% = Zn% + (Pb% x 0.68)

Typical cross- and plan sections through the block model are illustrated in Figure 23 and Figure 24.

17.1.11 Mineral Resource Classification

The mineral Resources were classified according to the pass in which a block was interpolated, as recorded in the Class variable. Blocks interpolated in Pass 1 were considered to be in the Measured category. The Pass 1 ranges are based on the ranges of the first spherical component of the corresponding correlogram, and vary from 10% to 80% of the maximum ranges of the correlograms. Blocks interpolated in the second and third passes are considered to be in the Indicated and Inferred categories, respectively.

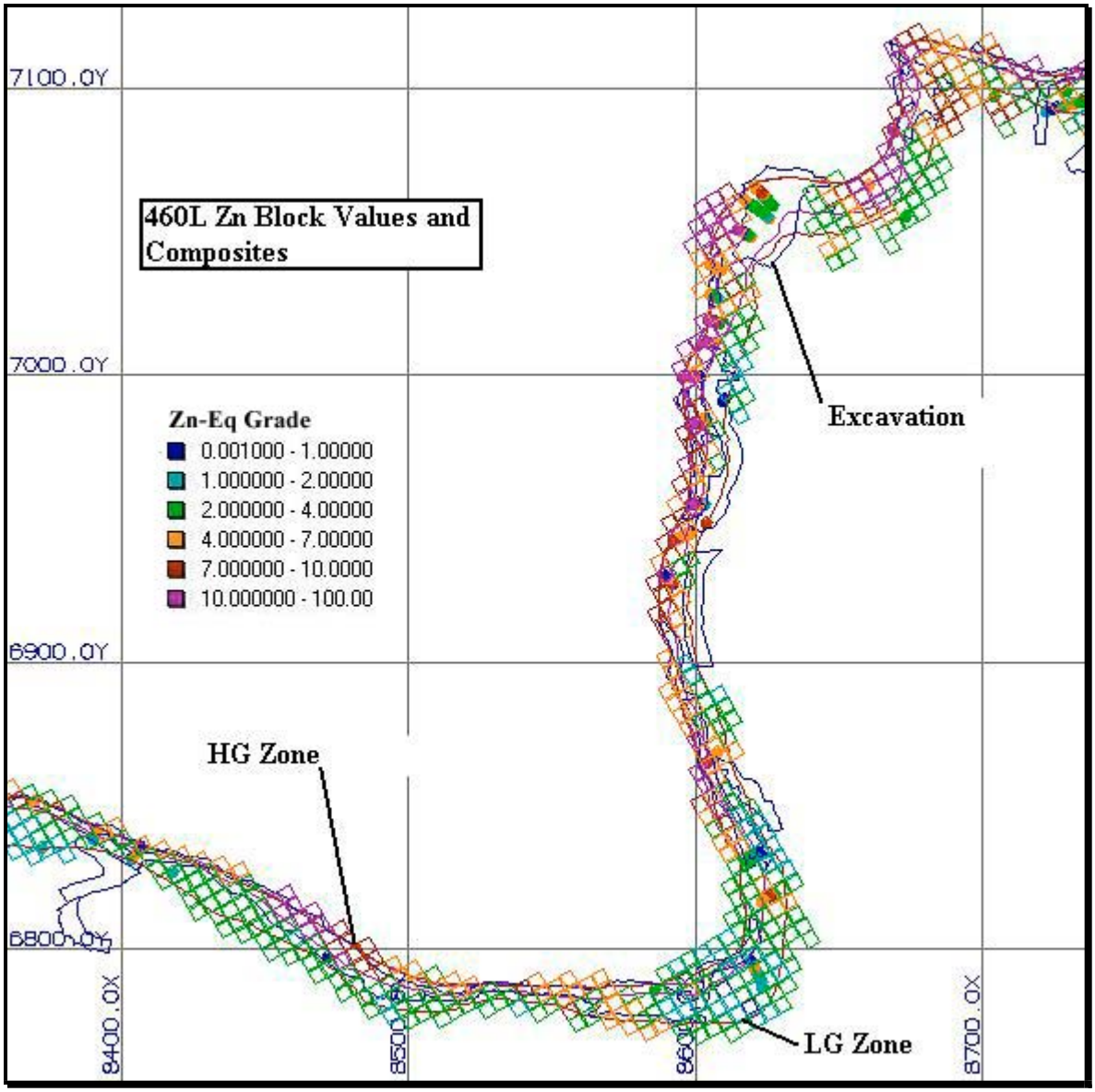


Figure 23: Plan section through the block model on the 460 metre level.

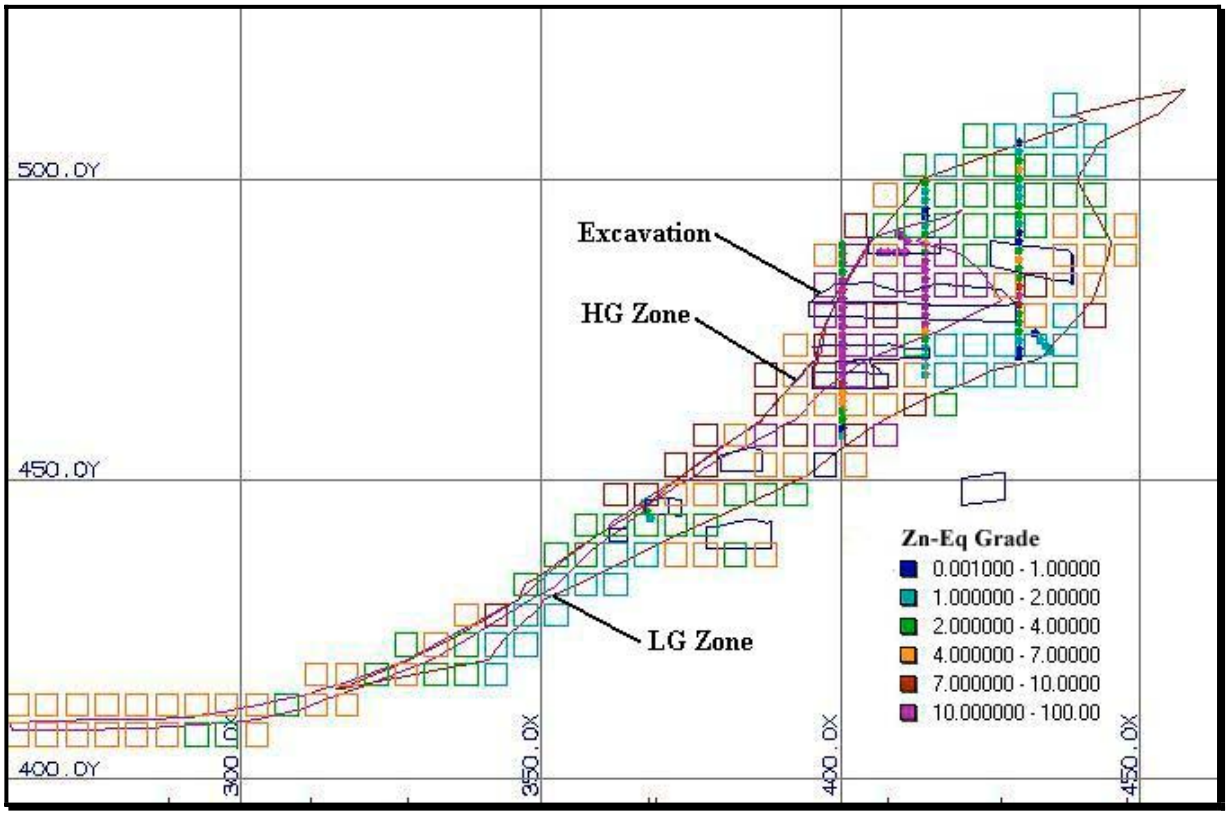


Figure 24: Cross-section through Row 208 of the block model, facing northeast.

17.1.12 Results

As described in previous paragraphs, Surface Resources for the High-grade and Low-grade zones were calculated separately (Table 18). Resources are reported using a cut-off grade of 0.75 % zinc-equivalent. For both zones, undiluted Measured Resources total 1.9 million tonnes containing 3.8 % zinc and 1.6 % lead. Indicated Resources total 2.2 million tonnes containing 3.5 % zinc and 1.5 % lead. The combined Measured + Indicated Resources total 4.1 million tonnes containing 3.5 % zinc and 1.5 % lead.

Undiluted Inferred Surface Resources total 1.8 million tonnes containing 3.1 % zinc and 1.1 % lead.

Table 18: Undiluted surface Resources.

Category	Volume (m^3)	SG	Tonnes	Zinc Grade	Lead Grade
Measured Resources					
High Grade Zone					
>=7 % ZnEq	124,800	2.91	363,400	8.9%	4.0%
2-7 % ZnEq	65,200	2.79	181,700	3.9%	1.7%
1.5-2 % ZnEq	900	2.73	2,300	1.4%	0.5%
0.75-1.5 % ZnEq	400	2.72	1,100	0.9%	0.4%
Subtotal	191,300	2.87	548,500	7.2%	3.2%
Low Grade Zone					
>=7 % ZnEq	21,100	2.87	60,300	7.5%	2.9%
2-7 % ZnEq	295,300	2.76	814,800	2.7%	1.2%
1.5-2 % ZnEq	80,600	2.73	219,800	1.5%	0.3%
0.75-1.5 % ZnEq	88,600	2.72	240,700	1.0%	0.2%
Subtotal	485,600	2.75	1,335,600	2.4%	0.9%
Total Measured	677,000	2.78	1,884,000	3.8%	1.6%
Indicated Resources					
High Grade Zone					
>=7 % ZnEq	96,100	2.89	278,000	7.4%	4.1%
2-7 % ZnEq	31,900	2.80	89,200	4.2%	2.0%
1.5-2 % ZnEq	79	2.73	216	1.6%	0.3%
0.75-1.5 % ZnEq	183	2.70	495	0.0%	0.0%
Subtotal	128,300	2.87	367,900	6.6%	3.6%
Low Grade Zone					
>=7 % ZnEq	36,000	2.86	103,000	7.0%	3.0%
2-7 % ZnEq	441,800	2.76	1,220,200	2.8%	1.2%
1.5-2 % ZnEq	106,400	2.73	290,000	1.5%	0.3%
0.75-1.5 % ZnEq	97,400	2.72	264,700	1.1%	0.2%
Subtotal	681,600	2.76	1,877,900	2.6%	1.0%
Total Indicated	810,000	2.77	2,246,000	3.2%	1.4%
Total Measured and Indicated Resources	1,490,000	2.77	4,130,000	3.5%	1.5%
Inferred Resources					
High Grade Zone					
>=7 % ZnEq	23,100	2.90	67,200	6.9%	4.9%
2-7 % ZnEq	16,800	2.79	47,000	4.1%	1.8%
1.5-2 % ZnEq					
0.75-1.5 % ZnEq	15	2.71	40	0.8%	0.2%
Subtotal	39,900	2.86	114,200	5.7%	3.6%
Low Grade Zone					
>=7 % ZnEq	49,800	2.85	142,300	7.0%	2.7%
2-7 % ZnEq	397,500	2.76	1,097,800	3.1%	1.0%
1.5-2 % ZnEq	80,000	2.73	218,300	1.4%	0.5%
0.75-1.5 % ZnEq	84,800	2.72	230,400	1.0%	0.2%
Subtotal	612,100	2.76	1,688,800	2.9%	1.0%
Total Inferred	652,000	2.76	1,800,000	3.1%	1.1%

Notes:

1. ZnEq = Equivalent Zinc, where 1 % lead equals 0.67 % zinc.
2. Undiluted Resources.

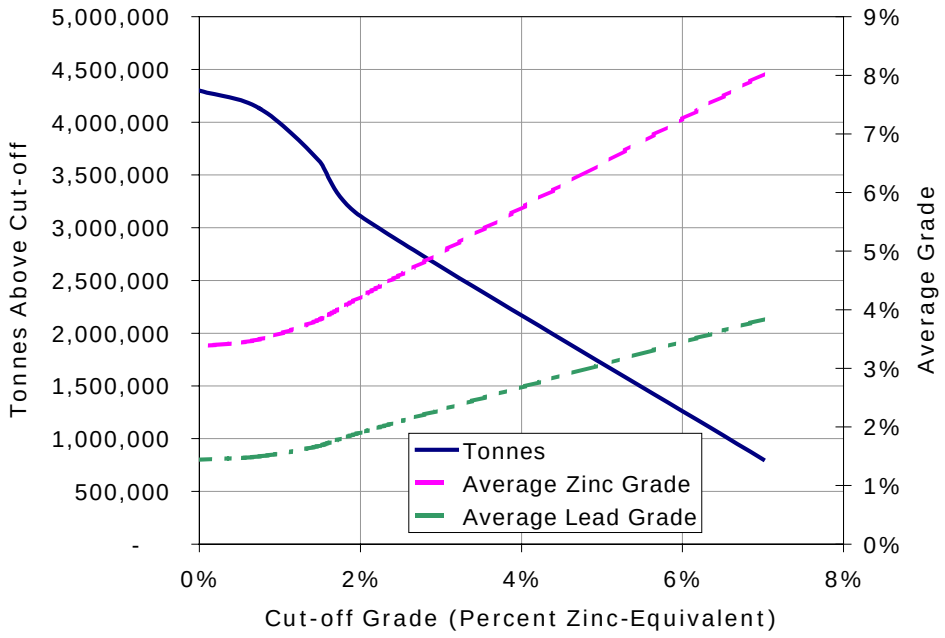


Figure 25: Grade-tonnage curve for Measured and Indicated surface Resources (undiluted).

17.2 Underground Resources – Northeast Zone

Resources in the Northeast Zone were estimated. Because it was determined that this area would be most profitably mined using underground mining methods, a cut-off grade of 5 % zinc equivalent was used to outline the mineralisation on sections spaced fifty metres apart. To permit mechanised mining, the minimum mining width and height were both 2.4 metres. An additional 0.1 metre "skin" dilution was incorporated into the resource outlines. This resulted in a widening of the outline beyond the grade cut-off point. Although the dilution material was below cut-off, in most cases it contained some metal.

The section outlines were drawn under the assumption that selective mining could be carried out within the carbonate. Meaning, it would be possible to mine along either the footwall or the hanging wall contact rather than mining the full width of the carbonate unit.

To determine the quantity of material, the outline area on each section was multiplied by its strike length (fifty metres) to determine the volume. That figure was multiplied by an average SG of 2.9 to determine mass. To determine grade, the length-weighted average grade and the true width of each intercept was calculated. The average section grade was determined by calculating the true-length-weighted average grade of all of the section's intercepts. The average true width of the intercepts was also calculated.

One contiguous body made up the underground resources that lie northeast and along strike from the proposed pit (Figure 26). Cross-sections showing the resource outline are shown in Figure 27 through Figure 29. The average grade of each body was determined by calculating

the average-true-width-weighted grade of the sections that made up the body. The average true width of the body was determined by calculating the volume-weighted average true section width.

Because of the 20-30 m sample spacing and the lack of bulk or underground sampling in this area, these Resources were classified as Indicated Resources. Indicated Resources in the Northeast Underground Zone were estimated to be 1,110,000 tonnes containing 6.6 % zinc and 3.7 % lead. The average true width was estimated to be 3.6 metres (Table 23).

Table 19: Underground resources (Northeast Underground Zone).

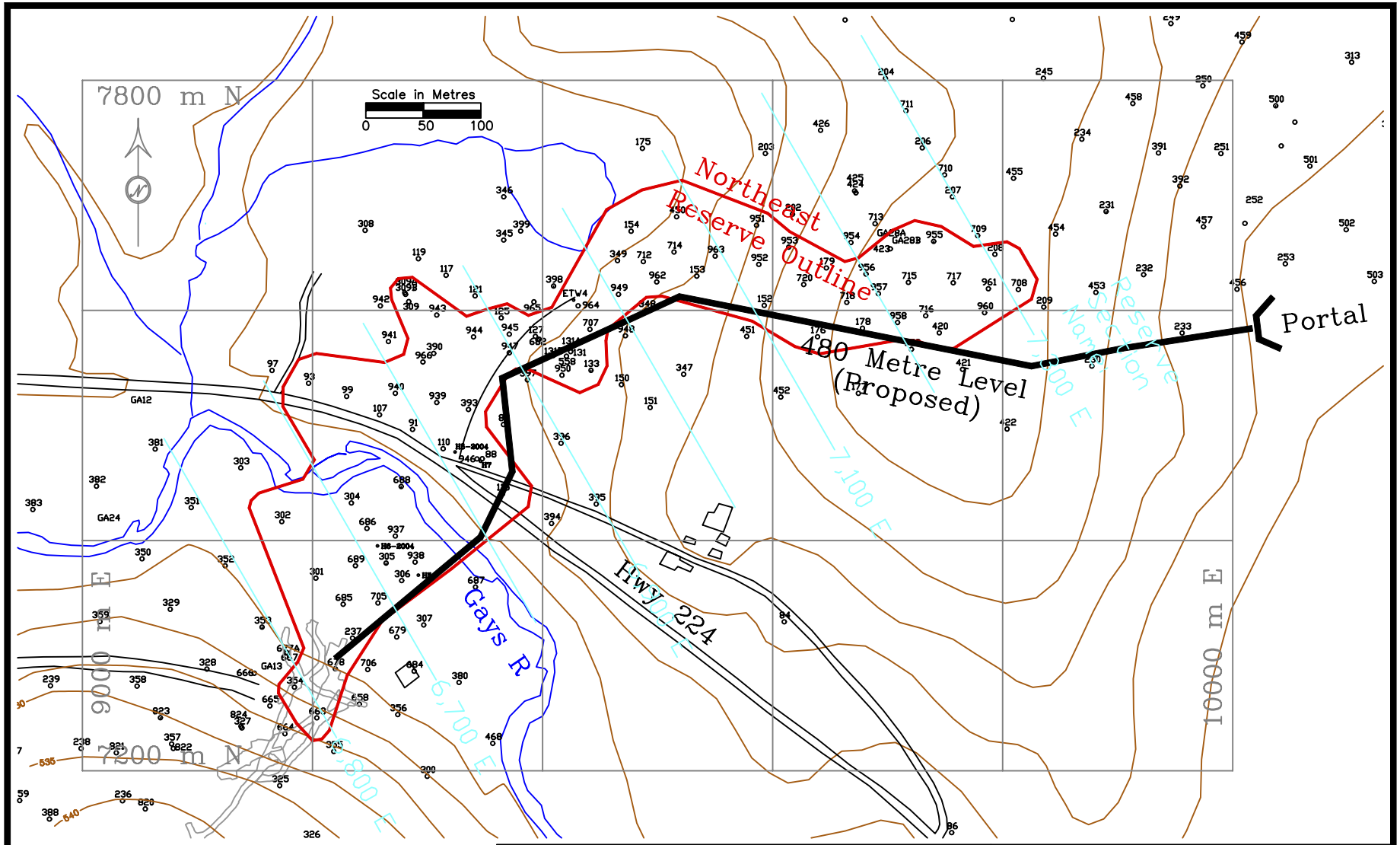
Outline Name	Section Name	Area (m^2)	Volume (m^3)	Tonnes	Average True Thickness[1] (m)	Average Grade (%) Zn	Pb
1	6,600	230	11,500	33,000	4.4	5.0	1.8
2	6,650	723	36,100	105,000	3.7	5.8	3.1
3	6,700	387	19,300	56,000	3.4	13.4	10.2
14	6,750	813	40,600	118,000	2.7	3.3	3.7
15	6,800	677	33,900	98,000	3.1	7.3	4.0
4	6,850	948	47,400	137,000	3.9	5.1	1.5
5	6,900	211	10,500	30,000	2.3	4.6	1.2
6	6,950	498	24,900	72,000	5.4	6.9	5.1
13	7,000	164	8,200	24,000	2.6	1.7	1.2
7	7,050	391	19,500	57,000	4.0	7.1	2.9
8	7,100	547	27,400	79,000	2.3	2.6	4.1
9	7,150	628	31,400	91,000	4.1	6.5	4.3
10	7,200	420	21,000	61,000	4.1	7.7	4.5
11	7,250	741	37,100	108,000	3.2	12.6	4.1
12	7,300	248	12,400	36,000	4.5	7.0	1.2
Total			381,200	1,110,000	3.6	6.6	3.7

Notes:
1. A 10 cm "skin" dilution was incorporated.
2. SG = 2.9

Table 20: Resources summary (0.75 % zinc-equivalent cut-off grade).

Category		Volume (m^3)	SG	Tonnes	Zinc Grade	Lead Grade
Measured (Surface)		680,000	2.78	1,880,000	3.8%	1.6%
Indicated						
	Surface	810,000	2.77	2,250,000	3.2%	1.4%
	Underground[1]	381,000	2.90	1,110,000	6.6%	3.7%
	Subtotal	1,190,000	2.82	3,360,000	4.3%	2.2%
Measured + Indicated (Surface and Underground)		1,870,000	2.80	5,240,000	4.1%	2.0%
Inferred		652,000	2.76	1,800,000	3.1%	1.1%

Notes:
1. Northeast Underground Zone.
2. Undiluted Resources.



Legend:
- Diamond Drill Hole

Contour interval = 5 m
Site grid.
Dimensions in metres.

Date: February 15, 2006	Scotia Mine Gays River, Nova Scotia
Scale: Bar Scale	
Drawn by: Douglas Roy, M.A.Sc., P.Eng. MINETECH INTERNATIONAL LIMITED CONSULTANT ENGINEERS & GEOLOGISTS HALIFAX, CANADA	Site Plan Showing Northeast Zone Reserves and Planned Development

Figure 26

MineTech International Limited
Scotia Mine – Gays River NS

Cross-Sections Through Northeast Reserves
Section 6650, Facing Southwest

Author WD Roy
Scale 1:1500
Date 10 Mar 2006
Section E-6650.0
File 6650.MAP
Notes :
Dimensions in metres.

Figure 27

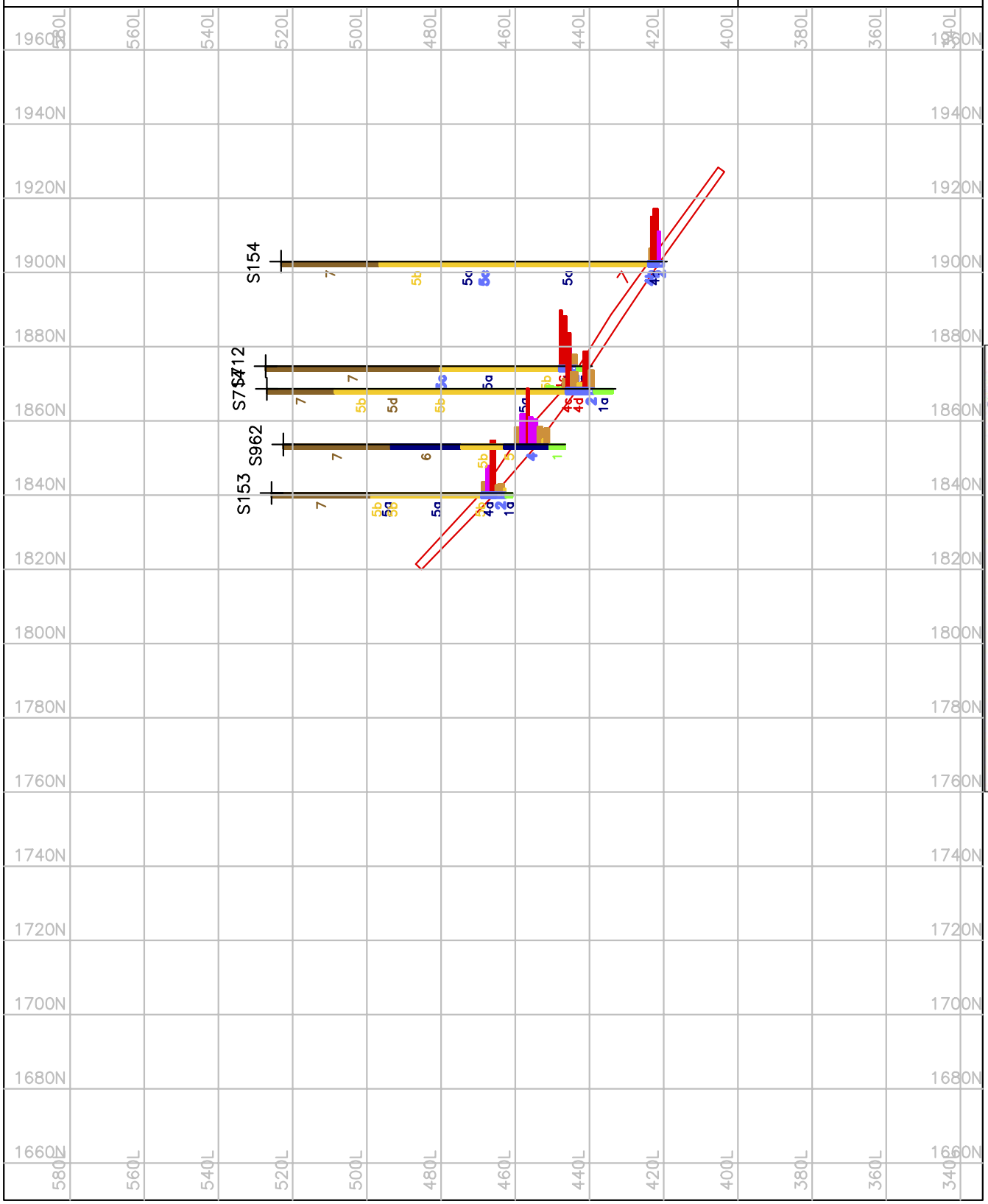
MineTech International Limited
Halifax, Canada

MineTech International Limited
Scotia Mine – Gays River NS

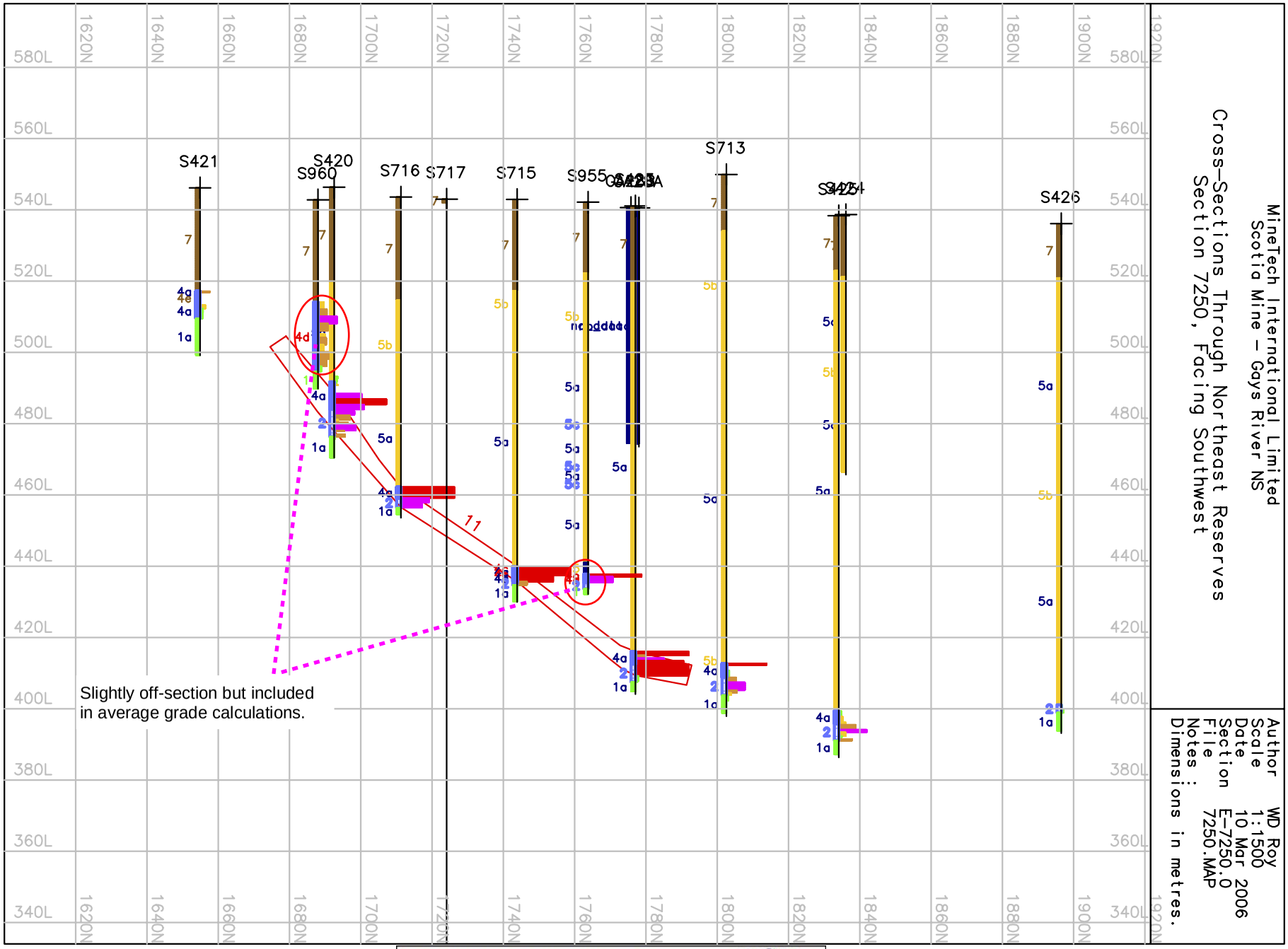
Cross-Sections Through Northeast Reserves
Section 7050, Facing Southwest

Author WD Roy
Scale 1:1500
Date 10 Mar 2006
Section E-7050.0
File 7050.MAP
Notes :
Dimensions in metres.

Figure 28



MineTech International Limited
Halifax, Canada



MINETECH INTERNATIONAL LIMITED
HALIFAX, CANADA

Figure 29

17.3 Gypsum

Prior to 2004, very little sampling and assaying for gypsum was done. Past drilling campaigns focused solely on zinc and lead. Prior to 2004, much of the gypsum core was saved; however, much of it was improperly stored and the gypsum weathered away.

In 2004, fourteen vertical holes were drilled that penetrated the gypsum resource. These holes, which are shown in Figure 15, were sampled and assayed for gypsum. Most of the samples were also assayed for chloride. The chloride assay was for all chlorides – chloride ions from any source.

Examination of the core revealed that the gypsum was relatively hard and pure. There were very few clay interbeds as appear at National Gypsum's deposit in nearby Milford. The gypsum graded into anhydrite, typical of Nova Scotia gypsum deposits. There was no clear contact between the two rock types.

A preliminary assessment of gypsum quality was carried out using the holes that were drilled in 2004. A cut-off grade of 85 % gypsum was used. Where the hole entered the gypsum was defined as the top contact. Where the hole left the gypsum, meaning where the hole left the gypsum horizon and passed into material with an average gypsum grade of less than 85 % (in other words, into anhydrite), was defined as the bottom contact.

The average gypsum thickness was 31 metres with a range of 9-85 metres. The gypsum was covered by 16-61 metres of overburden, averaging 38 metres. The average stripping ratio was 1.7.

The subset of samples within the gypsum consisted of sixty-nine (69) samples from fourteen holes. More than half of these samples (44 of them) were also assayed for chloride. The length-weighted average grade was 93 % gypsum. The length-weighted average chloride content was 43 ppm. Only one sample contained over 100 ppm chloride – this sample averaged 142 ppm over three metres.

Table 21: Raw (non-weighted) assay statistics.

Statistic	Gypsum	Cl
Mean	92.8	41.3
Standard Error	0.41	3.88
Median	93.9	43
Mode	93.9	11
Standard Deviation	3.4	26
Sample Variance	11.8	661
Kurtosis	0.4	3.9
Skewness	-1.1	1.2
Range	14.17	138
Minimum	83.57	4
Maximum	97.74	142
Count	69	44

The reader should note that this analysis represents only an arithmetic analysis of gypsum quality and chloride content. No spatial statistics were calculated. Therefore, this is only an indication of gypsum quality – not an accurate estimate. The gypsum sample spacing is currently too wide for meaningful calculation of Resources or Reserves.

There are many bags of sample rejects available for mineral processing work. These are stored at the Scotia Mine site. Also, the core was sawed in half for sampling and the remaining halves were stored in a dry facility. The sample pulps are also readily available for further assay work.

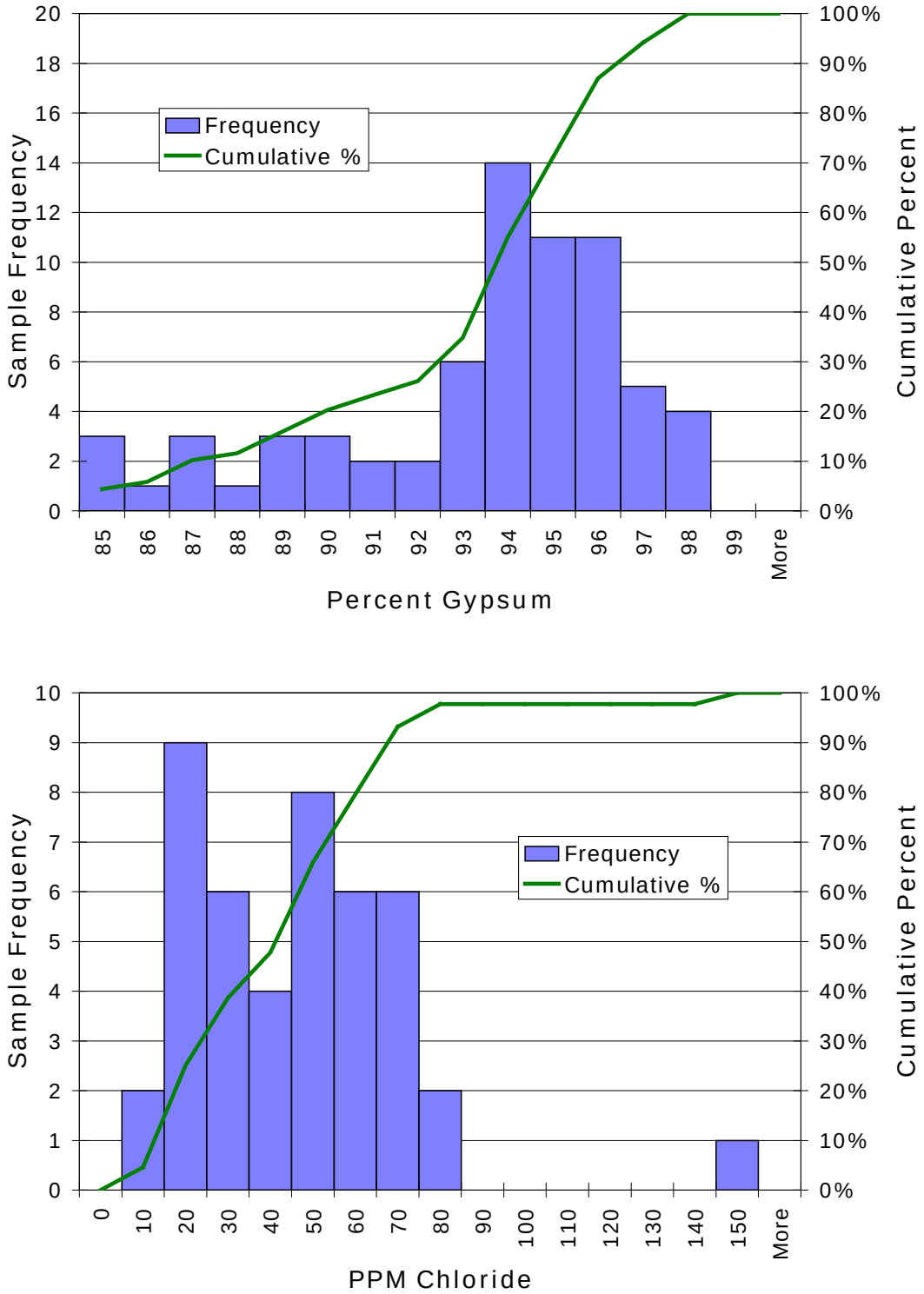


Figure 30: Gypsum and chloride histograms.

18. Reserves

18.1 Surface Reserves

To estimate the Surface Reserves, an optimised pit shell was generated from the block model utilising Whittle 3.4 pit optimisation software. Tim Carew, P.Geo., carried out the optimisation process using a set of economic and geotechnical parameters that were supplied by Mr. Douglas Roy, P.Eng of MineTech International Limited. Only blocks in the Measured and Indicated Resource categories were used. The base case economic and geotechnical parameters were:

Revenue

- Prices ($US per tonne of Metal)
  - Zn $1,760
  - Pb $990
- Exchange Rate ($US per $CAN) $0.75
- Dilution 15 % at Zero Grade
- Processing Recovery
  - Zn 90 %
  - Pb 95 %
- Smelter Return
  - Zn 85 %
  - Pb 95 %
- Concentrate Grade
  - Zn 60 %
  - Pb 75 %
- Moisture Content of Concentrate (by Mass)
  - Zn 8 %
  - Pb 6 %
- Treatment Charges ($US per tonne of Dry Concentrate)
  - Zn $170
  - Pb $160

Costs ($CAN/tonne)

- Drilling and Blasting (Carbonate and Evaporites) $1.25
- Loading and Hauling (Rock and Soil) $1.70
- Processing (Not including Concentrate Shipping) $8.52
- Overhead & Support $0.27
- Concentrate Shipping ($CAN per Wet tonne) - Zn $36.50
- Concentrate Shipping ($CAN per Wet tonne) - Pb $24.20

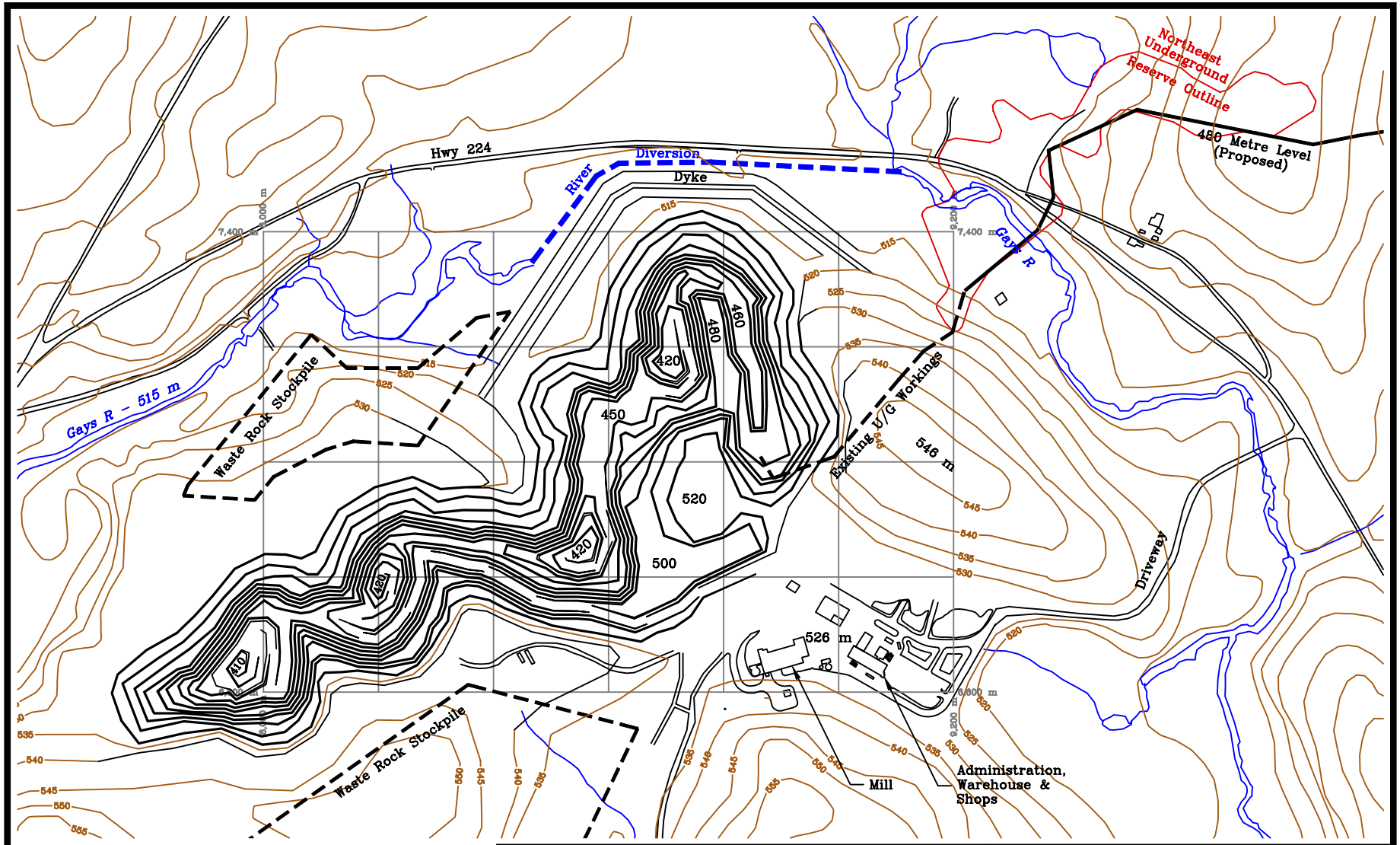
Maximum Slopes

- Carbonate (Dolomite) 45 °
- Trench/Till 27 ° (2:1)
- Evaporites (Gypsum / Anhydrite) 55 °

A surface mine plan, complete with haul roads, was designed using the optimum pit shells as a guide (Figure 31). Table 22 reports the Reserves that are contained within the pit design. Figure 32 shows a grade-tonnage curve for diluted, recoverable, Proven and Probable Reserves.

Using a 0.75 % zinc-equivalent cut-off grade, diluted, recoverable Proven Reserves total 1.8 million tonnes containing 3.2 % zinc and 1.3 % lead. Probable Reserves total 1.7 million tonnes containing 2.9 % zinc and 1.2 % lead. Proven + Probable Reserves total 3.4 million tonnes containing 2.9 % zinc and 1.2 % lead.

In-Pit Inferred Resources total 510,000 tonnes containing 2.2 % zinc and 1.1 % lead. The reader should note that in-pit Inferred Resources cannot be considered Reserves.



Site grid.
Dimensions in metres.
5 m contour interval.
10 m bench height.

Scale in Metres
0 50 100

Date: April 26, 2006

Scale: Bar Scale

Drawn by: Douglas Roy, M.A.Sc., P.Eng.

MINETECH INTERNATIONAL LIMITED
CONSULTANT ENGINEERS & GEOLOGISTS
HALIFAX, CANADA

Scotia Mine
Gays River, Nova Scotia

Site Plan Showing
Planned Mining

Figure 31

Table 22: Surface Reserves.

Undiluted Reserves

Category		Volume (m^3)	SG	Tonnes	Zinc Grade	Lead Grade
Proven Reserve						
High Grade Zone						
	>=7 % ZnEq	97,230	2.92	283,620	9.1%	4.1%
	2-7 % ZnEq	52,780	2.78	146,930	3.9%	1.5%
	1.5-2 % ZnEq	860	2.73	2,350	1.4%	0.5%
	0.75-1.5 % ZnEq	390	2.72	1,070	0.9%	0.4%
	Subtotal	151,300	2.87	434,000	7.3%	3.2%
Low Grade Zone						
	>=7 % ZnEq	20,700	2.87	59,310	7.5%	2.9%
	2-7 % ZnEq	282,480	2.76	779,430	2.7%	1.1%
	1.5-2 % ZnEq	76,410	2.73	208,370	1.5%	0.3%
	0.75-1.5 % ZnEq	77,660	2.72	211,120	1.1%	0.2%
	Subtotal	457,300	2.75	1,258,200	2.4%	0.9%
Total Proven		609,000	2.78	1,692,000	3.7%	1.5%
Probable Reserve						
High Grade Zone						
	>=7 % ZnEq	27,390	2.91	79,700	7.5%	4.8%
	2-7 % ZnEq	8,250	2.80	23,070	4.4%	1.7%
	1.5-2 % ZnEq					
	0.75-1.5 % ZnEq					
	Subtotal	35,600	2.89	102,800	6.8%	4.1%
Low Grade Zone						
	>=7 % ZnEq	32,580	2.86	93,130	7.0%	2.9%
	2-7 % ZnEq	362,040	2.76	999,590	2.8%	1.1%
	1.5-2 % ZnEq	87,020	2.73	237,290	1.5%	0.3%
	0.75-1.5 % ZnEq	72,160	2.72	196,110	1.1%	0.2%
	Subtotal	553,800	2.76	1,526,100	2.7%	1.0%
Total Probable		589,000	2.77	1,629,000	2.9%	1.2%
Total Proven & Probable Reserves		1,198,000	2.77	3,321,000	3.3%	1.3%
In-Pit Inferred Resources						
High Grade Zone						
	>=7 % ZnEq	1,820	2.98	5,410	7.0%	8.1%
	2-7 % ZnEq	120	2.78	320	4.6%	0.7%
	1.5-2 % ZnEq					
	0.75-1.5 % ZnEq					
	Subtotal	1,900	3.00	5,700	6.9%	7.7%
Low Grade Zone						
	>=7 % ZnEq	13,630	2.86	38,910	6.6%	3.0%
	2-7 % ZnEq	98,190	2.77	271,540	2.8%	1.4%
	1.5-2 % ZnEq	29,300	2.73	80,000	1.3%	0.6%
	0.75-1.5 % ZnEq	34,560	2.72	93,930	1.1%	0.2%
	Subtotal	175,700	2.76	484,400	2.5%	1.1%
Total In-Pit Inferred		178,000	2.75	490,000	2.6%	1.2%

Table 22 (cont.)

Diluted and Recoverable Reserves[1]

Category		Volume (m^3)	SG	Tonnes	Zinc Grade	Lead Grade
Proven Reserve						
High Grade Zone						
	>=7 % ZnEq	100,630	2.92	293,550	7.9%	3.6%
	2-7 % ZnEq	54,630	2.78	152,070	3.4%	1.3%
	1.5-2 % ZnEq	890	2.73	2,430	1.2%	0.4%
	0.75-1.5 % ZnEq	400	2.78	1,110	0.8%	0.4%
	Subtotal	156,600	2.87	449,200	6.3%	2.8%
Low Grade Zone						
	>=7 % ZnEq	21,420	2.87	61,390	6.5%	2.5%
	2-7 % ZnEq	292,370	2.76	806,710	2.3%	1.0%
	1.5-2 % ZnEq	79,080	2.73	215,660	1.3%	0.3%
	0.75-1.5 % ZnEq	80,380	2.72	218,510	0.9%	0.2%
	Subtotal	473,300	2.75	1,302,300	2.1%	0.8%
Total Proven		630,000	2.78	1,752,000	3.2%	1.3%
Probable Reserve						
High Grade Zone						
	>=7 % ZnEq	28,350	2.91	82,490	6.5%	4.1%
	2-7 % ZnEq	8,540	2.80	23,880	3.8%	1.5%
	1.5-2 % ZnEq	-		-	0.0%	0.0%
	0.75-1.5 % ZnEq	-		-	0.0%	0.0%
	Subtotal	36,900	2.88	106,400	5.9%	3.6%
Low Grade Zone						
	>=7 % ZnEq	33,720	2.86	96,390	6.1%	2.5%
	2-7 % ZnEq	374,710	2.76	1,034,580	2.5%	1.0%
	1.5-2 % ZnEq	90,070	2.73	245,600	1.3%	0.3%
	0.75-1.5 % ZnEq	74,690	2.72	202,970	0.9%	0.1%
	Subtotal	573,200	2.76	1,579,500	2.3%	0.9%
Total Probable		610,000	2.76	1,686,000	2.5%	1.0%
Total Proven & Probable Reserves		1,240,000	2.77	3,438,000	2.9%	1.2%
In-Pit Inferred Resources						
High Grade Zone						
	>=7 % ZnEq	1,880	2.98	5,600	6.1%	7.0%
	2-7 % ZnEq	120	2.75	330	4.0%	0.6%
	1.5-2 % ZnEq	-		-	0.0%	0.0%
	0.75-1.5 % ZnEq	-		-	0.0%	0.0%
	Subtotal	2,000	2.95	5,900	6.0%	6.7%
Low Grade Zone						
	>=7 % ZnEq	14,110	2.85	40,270	5.8%	2.6%
	2-7 % ZnEq	101,630	2.77	281,040	2.4%	1.2%
	1.5-2 % ZnEq	30,330	2.73	82,800	1.2%	0.5%
	0.75-1.5 % ZnEq	35,770	2.72	97,220	0.9%	0.2%
	Subtotal	181,800	2.76	501,300	2.2%	1.0%
Total In-Pit Inferred		184,000	2.76	507,000	2.2%	1.1%
Overburden (Till and Sand)		12,980,000				
Trench Clay		1,655,000				
Quartzite Waste Rock		143,000				
Gypsum/Anhydrite Waste Rock		1,341,000				

Notes:
1. Dilution equals 15 % and mining recovery equals 90 %.
2. ZnEq = Equivalent Zinc, where 1 % lead equals 0.67 % zinc.

Cut-off Grade	Volume Above Cut-off (m^3)	Tonnes Above Cut-off	Average Grade Zinc	Average Grade Lead
7.0%	184,120	533,820	7.2%	3.3%
2.0%	914,370	2,551,060	3.5%	1.5%
1.5%	1,084,410	3,014,750	3.1%	1.3%
0.75%	1,239,880	3,437,340	2.9%	1.2%
0.0%	1,267,190	3,511,320	2.8%	1.1%

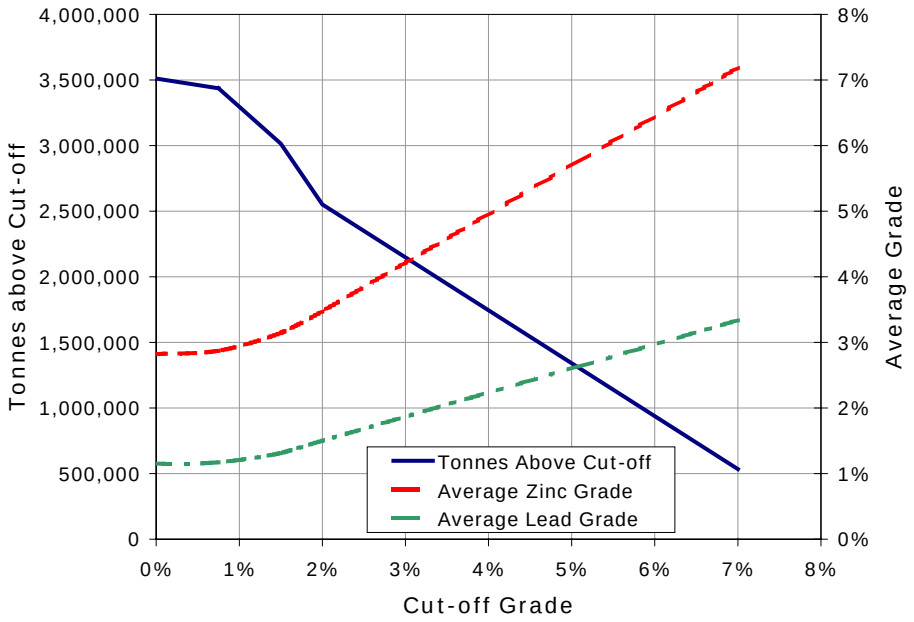


Figure 32: Grade-tonnage relationship for diluted and recoverable, Proven and Probable Surface Reserves.

The effect of changing metal prices on Reserve size and grade was investigated. Two additional optimum pit shells were generated using plus and minus 25 % of the base case metal prices. The relationship shows that Reserve tonnes drop in an approximately linear manner as the cut-off grade increases (Figure 33). Interestingly, the average Reserve grade is fairly insensitive to a change in cut-off, implying that for this deposit, a drop in cut-off (increase in metal price) means that more ore can be mined at a higher stripping ratio.

Zinc Price ($US/lb)	Corresponding Cut-off Grade[1] (Zn-Eq)	Reserve Tonnes	Zinc Grade	Lead Grade	Zn-Eq Grade[2]	Stripping (Tonnes)	Stripping Ratio
$ 0.64	1.20%	2,200,000	3.25%	1.42%	3.86%	17,301,000	7.9
$ 0.85	0.85%	3,321,000	3.30%	1.35%	3.88%	32,855,000	9.9
$ 1.06	0.66%	3,831,000	3.48%	1.46%	4.11%	48,869,000	12.8

Notes:
1. Cut-off grade calculated according to zinc price and base case operating parameters.
2. Zinc-Equivalent equals zinc grade + 0.43 x lead grade.

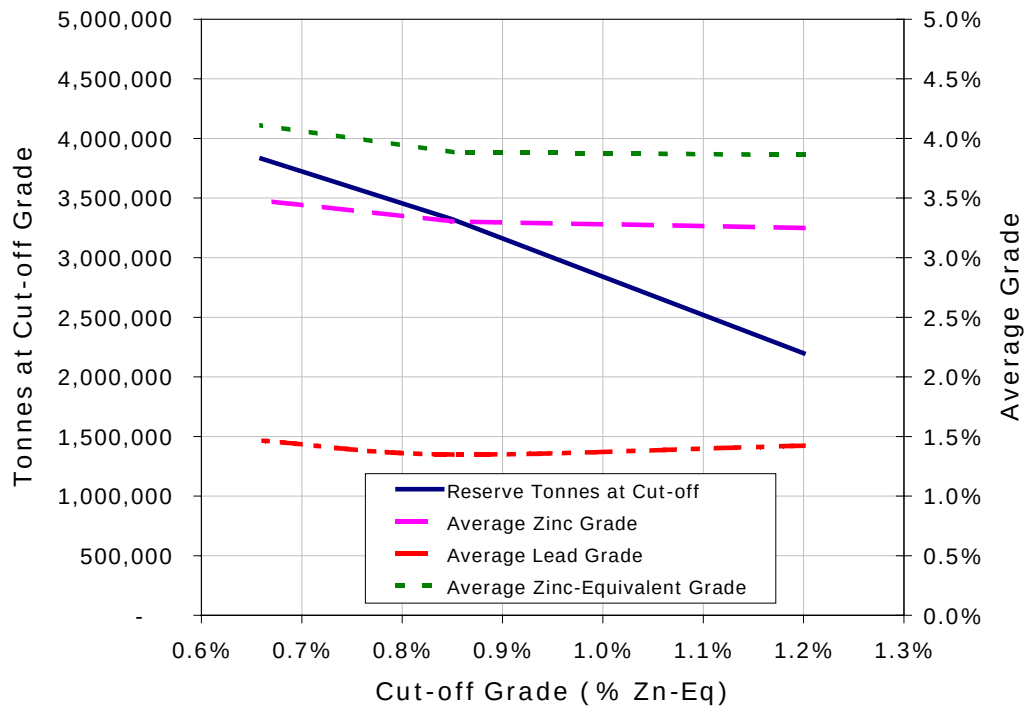


Figure 33: Undiluted Proven + Probable Reserves, above 0.75 % zinc-equivalent, at various cut-off grades.

18.2 Underground Reserves – Northeast Zone

To determine the Underground Reserves, the estimated dilution and mining recovery factors of 15 % and 90 %, respectively, were applied to the Northeast Zone Underground Resources (Section 17.2). Diluted and recoverable Probable Reserves were estimated to be 1,150,000 tonnes containing 5.7 % zinc and 3.2 % lead. The average true width was estimated to be 3.6 metres (Table 23).

The overall, diluted and recoverable, Surface and Underground, Proven and Probable Reserve totals 4.6 million tonnes containing 3.6 % zinc and 1.7 % lead (Table 24)

Table 23: Northeast Zone Probable Diluted & Recoverable Reserves.

Outline Name	Section Name	Area (m^2)	Diluted & Recovered Volume[3] (m^3)	Diluted & Recovered[3] Tonnes	Average True Thickness[1] (m)	Diluted[3] Average Grade (%) Zn	Pb
1	6,600	230	11,900	34,000	4.4	4.3	1.6
2	6,650	723	37,400	109,000	3.7	5.0	2.7
3	6,700	387	20,000	58,000	3.4	11.7	8.9
14	6,750	813	42,000	122,000	2.7	2.9	3.2
15	6,800	677	35,100	101,000	3.1	6.3	3.5
4	6,850	948	49,100	142,000	3.9	4.4	1.3
5	6,900	211	10,900	31,000	2.3	4.0	1.0
6	6,950	498	25,800	75,000	5.4	6.0	4.4
13	7,000	164	8,500	25,000	2.6	1.5	1.0
7	7,050	391	20,200	59,000	4.0	6.2	2.5
8	7,100	547	28,400	82,000	2.3	2.3	3.6
9	7,150	628	32,500	94,000	4.1	5.7	3.7
10	7,200	420	21,700	63,000	4.1	6.7	3.9
11	7,250	741	38,400	112,000	3.2	11.0	3.6
12	7,300	248	12,800	37,000	4.5	6.1	1.0
Total			394,500	1,150,000	3.6	5.7	3.2

Notes:
1. A 10 cm "skin" dilution was incorporated.
2. SG = 2.9
3. Dilution = 10 %, mining recovery = 90 %.

Table 24: Reserves summary (Proven & Probable, diluted and recoverable Surface and Underground Reserves).

Category	Volume (m^3)	SG	Tonnes	Zinc Grade	Lead Grade
Proven Reserves (Surface)	630,000	2.78	1,750,000	3.2%	1.3%
Probable Reserves					
Surface	610,000	2.76	1,690,000	2.5%	1.0%
Underground	395,000	2.90	1,150,000	5.7%	3.2%
Subtotal	1,005,000	2.83	2,840,000	3.8%	1.9%
Total Proven and Probable Reserves (Surface and Underground)	1,635,000	2.81	4,590,000	3.6%	1.7%

Notes:
1. Dilution equals 15 % and mining recovery equals 90 %.

19. Additional Requirements for Technical Reports on Development Properties and Production Properties – Feasiblity Analysis

19.1 Mining Operations

19.1.1 Initial Surface Mining

For the first few years, mining will be by surface methods using standard methods of drilling, blasting, and excavating using excavators and truck haulage. An equipment list is reported in Table 25. This equipment will be leased from a local dealer. The pit will have an oval shape with its long axis oriented along the northeast-southwest strike of the deposit. To the northeast, the pit is constrained by Gays River and Highway 224. Gays River will be diverted slightly to allow the pit to expand toward the highway.

The pit haul road will traverse the footwall of the deposit, generally along the carbonate/quartzite contact. The overall pit slope angle for the footwall will be less than 45 °. The gypsum/anhydrite evaporite hanging wall is more stable, allowing a steeper overall slope angle of 55°. Overburden slope angles will be kept below a 2:1 grade (27 °). The over-compacted Trench clay will also be kept below a 2:1 grade (27 °). A complete description of geotechnical work is reported in Section 19.4.

Working benches in ore will be five metres high for grade control purposes. Final bench heights in ore will be up to twenty metres. Higher benches, up to twenty metres high, taken in one or more cuts, are planned for the hanging wall evaporites.

After the pit reaches an elevation of approximately 480 metres (approximately 50 metres depth), underground development can begin from a portal in the northeast end of the pit, extending along strike to the northeast.

Table 25: Equipment list for the surface mine.

Equipment	Number	Hourly Owning & Operating Cost
CAT 345 Excavator	1	$124
CAT 385 Excavator	1	$185
CAT 773 Haul Truck	3-4	$146
CAT 14H Grader	1	$107
CAT 980 Wheel Loader	1	$111
CAT D8 Bulldozer	1	$134

19.1.2 Underground Mining

A main haulage drift will be established on the 480 metre level. It will extend from the pit along strike to the northeast. It will pass underneath the river but it will be entirely situated within the competent footwall quartzites. A second decline and portal will be located at the

northeast end of the Underground Reserves to provide a second access for the underground workings.

The weak hanging wall Trench clay poses the greatest technical challenge to underground mining. The Trench material is relatively strong for clay because it is overconsolidated (compacted). However, groundwater influx weakens it and also poses a dewatering challenge. As part of minimising the operational and safety hazards posed by the weak Trench clay, dewatering operations will lower the groundwater table below the active mine workings.

The cut-and-fill mining method was chosen specifically to address the weak hanging wall issue. It will be mechanised, meaning drill jumbos will do the development and production drilling. LHD's (Load-Haul-Dump vehicles) will muck the broken rock back to re-muck stockpile bays. In narrower stopes, slushers may be used to muck the broken rock. Underground dump trucks will haul the rock to surface.

From the main haulage drift on the 480 metre level, the main ramp will spiral downwards on the footwall side of the stope (Figure 34). A "lift ramp" will extend from the main ramp downward to Lift 1, approximately twenty metres from the planned top of the stope.

The mining method is a modified form of mechanised cut and fill mining. It is a combination of undercut and fill and conventional (overhand) cut and fill mining. Lift 1 (Figure 34) will be five metres high, at least 2.5 metres wide and its along strike length will be limited by ground conditions and haulage efficiencies. Generally, cut and fill lifts can be as long as two hundred metres. The overall stope height will be a maximum of eighty metres.

Every 50-100 metres, as required, raises will be driven, in ore, upward from lower levels. These will provide valuable geologic information, grade information, alternate escape routes and ventilation pathways. During the fill cycle, cribbing will be built around the raises to keep them open.

When Lift 1 has finished, the fill cycle will begin. As no sill pillars will be left, Lift 1 fill will form the back for Lift 8 (Figure 34). Therefore, the first few metres of Lift 1's fill will contain a higher cement content (up to 15 % cement:solids) and possibly some reinforcing material. The remaining fill will contain only enough cement (approximately 3 %) to hold together the aggregate fill, providing a stable floor on which to work. The aggregate in the fill will consist of sand and gravel that will be sourced from on-site glacial-fluvial deposits. It will be filled to within one-two metres of the back to allow for blasting swell during Lift 2 mining. Production will be accomplished using breasting. The mining will progress upwards to Lift 4 in the same manner. After Lift 4 has been filled, production will move to Lift 5 and the cycle will be continue.

The eastern half of the underground reserves lie under Gays River. If groundwater influx presents an unacceptable operational or safety hazard in this area, mining the first group of lifts (Lifts 1-4, Figure 34) in this area can be carried out during the drier months.

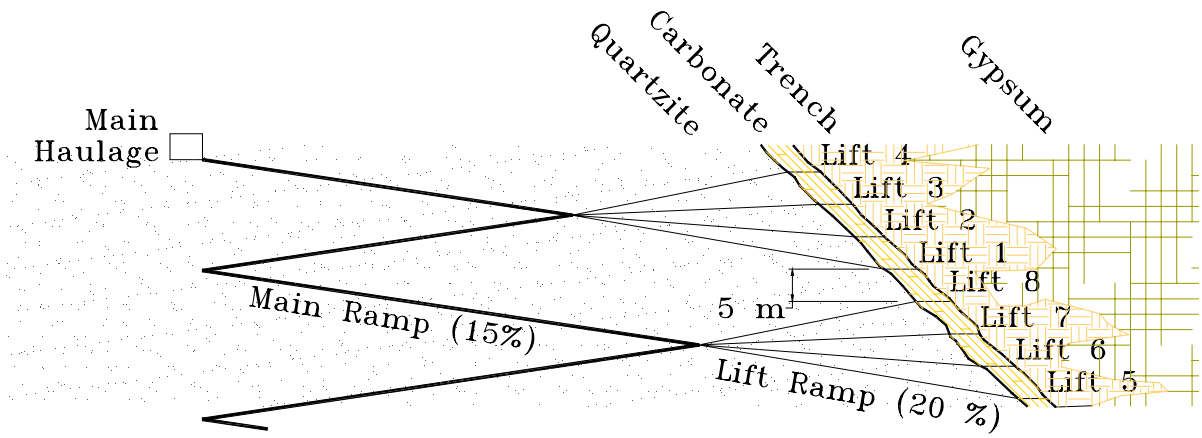


Figure 34: Cross-sectional conceptual schematic of modified mechanised cut-and-fill mining method (showing lift sequence).

19.1.3 Dewatering

Mine dewatering will be important for both surface and underground mining, but particularly for underground mining. In the underground mine, prior to starting a new lift cycle, the ramp will be continued deeper so that sumps can be established. Typical of soils, the hanging wall Trench clay is stronger when it is dry. Therefore, dewatering operations will strive to maintain the local water table at a level lower than the current workings. This will also significantly reduce the possibility of a sudden inrush of water. In the past, dewatering operations removed an average 4,000 gallons per minute (gpm) from the underground workings. The flowrate ranged from as little as 2,000 gpm in drier months to 6,000 gpm in months with heavier precipitation.

A significant portion of the inflow to the mine was groundwater recharge from Gays River. The river diversion plan includes lining part of the river with clay, which should reduce the recharge flowrate.

Drainage from backfilling operations is not expected to form a significant component of the overall dewatering requirement.

19.2 Mine Dilution and Recovery

Dilution was estimated at 15 %. The amount of ore that will be recovered from the mine was estimated at 90 %.

19.3 Mineral Processing Operations

The Scotia Mine processing plant was constructed during the late 1970's by Canada Wide Mines (Esso) (Figure 35). Esso operated for less than two years during the period 1979-1981. Seabright converted the mill to process gold during the mid-to-late 1980's. Westminer later re-converted and updated the mill to process zinc and lead, then operated it for a short time during the period 1989-1991. In all, 740,000 tonnes of zinc and lead ore have been processed in the mill (Table 9).

From a stockpile adjacent to the mill, a wheel loader loads ore into the primary jaw crusher (Figure 36). It is further crushed to –1/2 inch and stored in a fine ore bin. From there, it passes to the grinding mills, then to a lead flotation section. The ore, with most of the galena (lead sulphide *or* PbS) removed, passes to the sphalerite (zinc sulphide or ZnS) flotation section. The zinc and lead concentrates are separately thickened, filtered and dried before being stockpiled for shipment to the smelter.

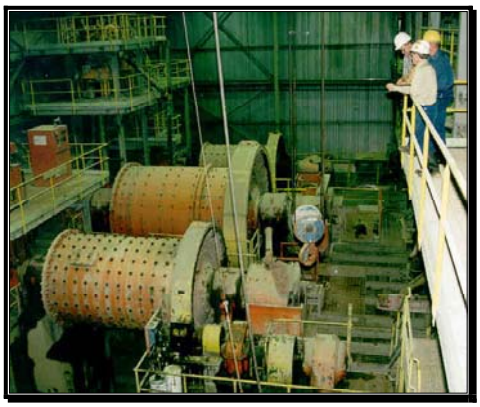


Figure 35: Views of the outside (left) and inside (right) of the mill.

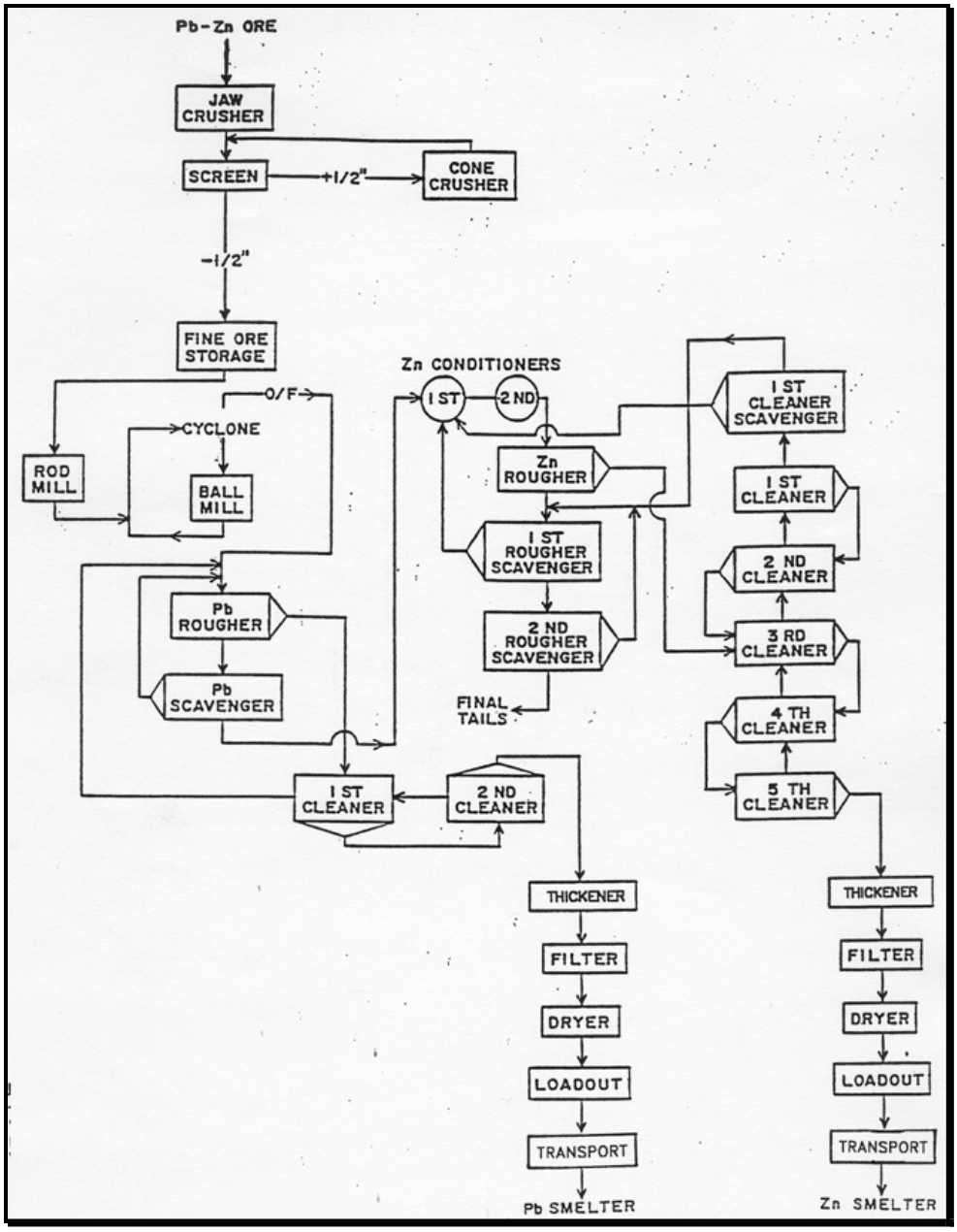


Figure 36: Process flowsheet.

Bulk concentrate will be stored on site. A front-end loader will be used to load concentrate into a highway semi-dump truck for the short trip to a railway siding in Milford, NS. Milford is eight kilometres along the highway from the mine site. The truck will dump from a ramp directly into gondola-style, 100 tonne railway cars. Canadian National will retrieve the cars and take them to the smelters. Lead concentrate will be taken Noranda's Belledune smelter in Northern New Brunswick and zinc concentrate will be taken to Noranda's Valleyfield smelter outside Montreal.

19.3.1 Production Forecast

The mill has a nominal capacity of 1,350 tonnes per day of higher grade (greater than seven percent zinc), quartzite breccia ore. When processing lower grade, carbonate ore, the mill performs well at production rates as high as 2,000 tonnes per day (Thornton, 2006 (1)). A production rate of 2,000 tonnes per day is planned for the surface operation. Operating 350 days per year, that translates to 700,000 tonnes of ore per year (Table 26).

Stripping operations will start at the beginning of the fourth quarter of Year One. Milling will begin two months later, during the eleventh month of Year 1, after a sufficient amount of material has been stockpiled. Each year, surface operations will produce 30,000 tonnes of zinc concentrate and 10,000 tonnes of lead concentrate.

Because of the higher grade of the underground ore, a production rate of 1,350 tonnes per day is planned for the underground operation. This is so as not to overwhelm the filtering and drying sections of the mill. Operating 350 days per year, that translates to 473,000 tonnes of ore per year Table 26). Each year, underground operations will produce 40,000 tonnes of zinc concentrate and 19,000 tonnes of lead concentrate.

Table 26: Yearly production forecast.

	Surface Operation	Underground Operation
Production (Diluted Tonnes)	700,000	473,000
Grade (Diluted):		
Zinc	2.9%	5.7%
Lead	1.1%	3.2%
Tonnes of Metal Processed		
Zinc	20,090	26,960
Lead	7,910	15,140
Tonnes of Metal Recovered	-	-
Zinc	18,080	24,260
Lead	7,510	14,380
Concentrate Produced (Dry Tonnes)		
Zinc	30,130	40,430
Lead	10,010	19,170
Tonnes of Metal Returned from Smelter		
Zinc	15,370	20,620
Lead	7,130	13,660

19.3.2 Recoverability

Over its operating history, whenever the feed contained a consistent grade, zinc and lead recovery values were 90 % and 95 %, respectively (Thornton, 2006 (1)). In a monthly report for November, 1990, Westminer reported recovery values of 90 % and 93 % for zinc and lead, respectively (Appendix 1). Thornton (2006 (1)) reported that Westminer encountered some oxidised zinc and lead that did not float well, thereby decreasing their recovery values.

Table 27 reports the mineral processing parameters that were used for this report. Smelter return is expected to be 85 % and 95 % for zinc and lead, respectively. Treatment charges also apply (Table 27).

Mining Recovery was estimated at 90 %.

Table 27: Mineral processing parameters.

Dilution	15 % at Zero Grade
Mining Recovery	90 %
Processing Recovery	
Zn	90 %
Pb	95 %
Smelter Return	
Zn	85 %
Pb	95 %
Concentrate Grade	
Zn	60 %
Pb	75 %
Moisture Content of Concentrate (by Mass)	
Zn	8 %
Pb	6 %
Treatment Charges (**$US** per tonne of Dry Concentrate)	
Zn	$170
Pb	$160

19.4 Geotechnical Aspects

No detailed geotechnical fieldwork was carried out to determine the optimum slope angles in rock. However, laboratory strength testing was carried out by CANMET. Triaxial testing of six dolomite samples and eight quartzite samples yielded the following mechanical properties:

Property	Quartzite	Dolomite
Number of Samples	8	6
SG	2.69	2.73
Diameter (mm)	45	45
Length (mm)	100	100
UCS (MPa)	240	120
Tensile Strength (MPa)	16	6
E (GPa)	61	55
ν	0.26	0.45
Confining Pressure (MPa)	2-20	1-20

Hoek and Brown material constants were also determined on those samples:

Property	Quartzite	Dolomite
Q_c (MPa)	240	110
m	15	12
s	1	1
r^2	0.98	0.97
m_r	2.8	5.7
s_r	0	0
r^2_r	0.86	0.98

The footwall at the carbonate/quartzite contact has an average dip of less than 45 °. The haul road will also be incorporated into the footwall, further reducing the overall pit slope angle. The footwall consists of strong, competent quartzite with no major adverse geotechnical features such as faulting that are the major causes of slope instability. The overall slope will be less than 45 °, which is more than adequate.

The hanging wall consists of gypsum/anhydrite evaporites and Trench clays. The Trench is wider near the surface and pinches at depth. Gypsum and anhydrite are strong, competent rocks that make for stable slopes. Evidence of this stability can be observed at National Gypsum's quarry in nearby Milford/Dutch Settlement. An overall slope angle of 55 ° in evaporites is warranted. Trench clays are more competent than glacial till because they are over-compacted. A maximum grade of 2:1 is warranted. However, whenever possible, the Trench clay will be stripped flat, back to the evaporite contact.

The overburden consists of a thick mantle of clayey-glacial till with localised glacio-fluvial deposits (McKee and Hannon, 1985). It will be pushed back five metres from the edge of the pit and sloped at a maximum grade of 2:1. CBCL (1999) determined that the factor of safety was 1.5 using that grade. Loose surficial sands or soft silts will be graded under 2.5:1 (CBCL, 1999). The till stratum ranges in thickness from 10-40 m. It has been cut in turn by glacial-fluvial deposits of sand, silty sand and gravel including the Gays River sediments. It was noted that fluvial sediments many contact the bedrock in some locations.

Aston and Lamb (1993) identified two main aquifers associated with the property. First is the Overburden Aquifer consisting of highly permeable fluvial-glacial coarse sands and gravels, interlaced with less permeable bands of fine sand and silt. Second is the Bedrock Aquifer with consists of highly permeable interconnected karstic gypsum cavities along with hydraulically connected but less permeable jointed and fractured carbonates and quartzites. The two aquifers are hydraulically connected in areas where the permeable overburden sediments are in contact with permeable bedrock zones.

19.4.1 Underground Geotechnical Investigation of Trench Material

In 1981, Jacques, Whitford and Associates carried out a geotechnical investigation of the hanging wall Trench clay (Brown, 1981). They inspected three underground Trench exposures in the 101, 104 and 107 areas. They also drilled three surface boreholes using a power augur. Clay and rock samples were taken for laboratory testing.

They observed that the unsupported stand-up time for the Trench material is at least several days – an adequate length of time for installing ground support. They recommended that grouted soil anchors and wire mesh screen be installed to support underground Trench exposures. Shotcrete could be added as an additional stabilising feature, if and where conditions were particularly unstable.

They stressed that dewatering efforts must be sufficient to prevent pore pressure from developing around the opening, that blasting vibrations be within safe limits and that changes in the stress field caused by mining be within acceptable limits. They recommended that wherever shotcrete is employed, weep holes be provided to prevent hydrostatic pressures from building.

They carried out three direct shear tests on a sample of Trench clay and determined the shear strength to be:

$$\tau = 16.5 \text{ kPa} + \sigma_n' \tan(23°)$$

where: τ = shear strength (kPa)

σ_n' = normal stress (kPa)

19.5 Mine Water and River Diversion

Groundwater infiltration into the Scotia Mine has historically posed a safety hazard and an operational problem. Water decreases the strength of soil and rock masses. There have also been several high pressure inrushes of soil laden water. Mine dewatering operations typically removed 4,000 gpm, on average. When Gays River was high during spring flooding, up to 6,000 gpm was removed. Golder Associates (1992) determined that one-quarter to one-half of that water originated from Gays River, apparently due to seepage through the riverbed.

Several sinkholes have developed due to mine dewatering operations. Groundwater flow through the gypsum hanging-wall rocks cause rapid dissolution of the gypsum, creating karst features, the surface expression of which are sinkholes. These can present a hazard to equipment and personnel.

To allow the northeast end of the proposed open pit to expand closer toward Highway 224 and to decrease the water seepage from the river into the proposed mine, CBCL (1999) designed a minor diversion of Gays River after carrying out a geotechnical investigation. The design was based on a 1998 field investigation that included drilling twelve boreholes at six sites. At each site, they found a 1.2-1.8 m layer of surficial silt overlying interbedded, alluvial silt and sand.

The recommended design consisted of digging a new channel for part of the river that would be separated from the pit by a dyke. Rather than using a single, wide dyke, CBCL recommended using two narrower dykes to mitigate the hazard of sinkholes causing damage to the dyke. Their rationale was that if sinkholes cause a breech in one dyke, the other would hold back the water.

The overall structure would be 600 metres long, fifty metres wide at the base and have a crest elevation of 519 metres. The dyke will be set back a minimum of ten metres from the top of the pit slope. The pit side of the dyke would have a 3:1 slope while the river side would have a 5:1 slope. Because of its low permeability, CBCL recommended that the dyke be constructed using the till that was stripped from the area of the pit. It should be built up in layers, allowing time for pore pressure to dissipate before placing the next layer. The riverbank would be lined with rip-rap for erosion control.

The new river channel would be lined with 60 centimetres of till to prevent water from seeping down through the riverbed. This will greatly reduce the amount of water that seeps into the mine workings.

19.6 Markets

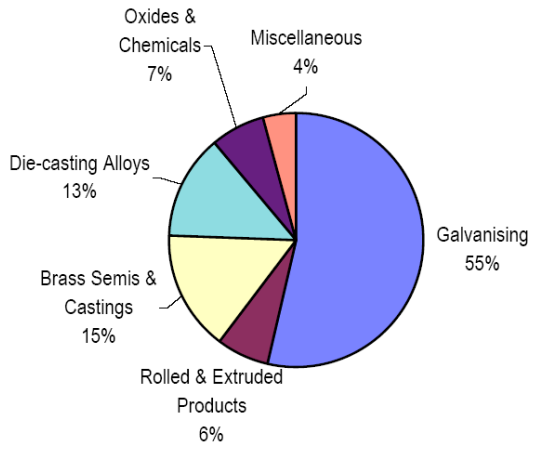
The on-site processing plant will concentrate zinc and lead in mineral form (sphalerite and galena, respectively). These separate concentrates will be sold to one or more outside smelters within North America or overseas. The Scotia Mine concentrate is high in purity without any penalty-attracting impurities. Currently, world-wide smelter capacity is under-utilised and the demand for concentrate exceeds what the mines can supply. Therefore, there should be no trouble selling the concentrate.

The principal use for zinc is in galvanising, with continuous galvanised sheet demand accounting for around two-thirds of this. Other major uses are die-casting and brass goods and both these are used in a very wide range of manufactured goods. Galvanising applications are principally to be found in construction and automobiles. Investment in infrastructure and manufacturing facilities are important factors in this rapid expansion of consumption in China. Growth of global demand is estimated to have averaged 3.7 % between 2000 and 2005; whilst Chinese consumption has increased by 16 % on average over this period, growth has been much more modest in the rest of world, at only 0.6 % (Roberts, 2006). Zinc demand outside China has suffered as a result of the rapid increase in China's exports of manufactured goods but, on the other hand, has benefited from China's need to import increasing quantities of galvanised sheet and die-casting alloys.

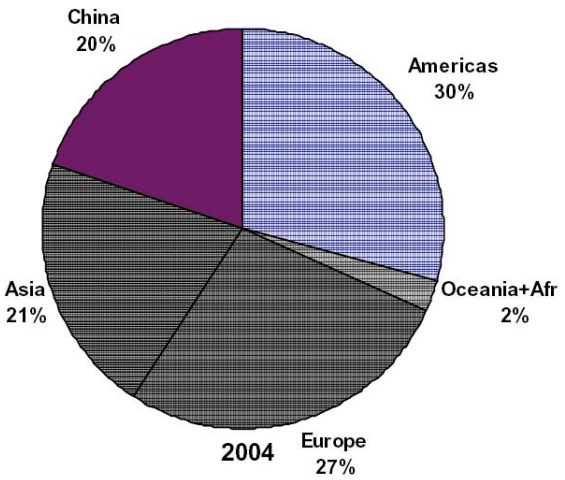
World-wide, approximately 10.7 million tonnes of refined zinc metal was consumed in 2005 (Roberts, 2006). Unlike zinc, where more than 90 % of refined metal production derives directly from zinc and bulk concentrates, less than 40 % of total refined lead production is produced directly from lead and bulk concentrates (Roberts, 2006). This is because the principal end use of lead, the manufacture of lead-acid batteries, accounts for 80 % of total demand. The useful life of these batteries is rather short, typically no more than five or six years at best, and often shorter, and virtually all these batteries are recycled to recover the

lead. Thus a large share of production increases in line with consumption, but with a lag of a few years. Essentially, mine production only needs to meet the incremental use of lead in batteries, and the remaining dissipative uses which currently account for only 20 % of total demand.

World-wide, approximately 7.5 million tonnes of refined lead metal was consumed in 2005 (Roberts, 2006). The main use for lead is in the manufacture of lead-acid batteries used in almost all motor vehicles for starting, lighting and ignition (SLI batteries) and industrial batteries which have widespread application providing back-up, portable and motive power (Roberts, 2006). There has been good growth in global lead demand since 2003, albeit that most of this growth has been in China. With global economic growth expected to be sound over the next few years, demand growth is expected to continue.



World-wide zinc consumption (RBC, 2005).



World-wide lead consumption (Roberts, 2006).

While there are alternatives to lead-acid batteries, for the foreseeable future lead-acid will remain the technology of choice in almost all of its current applications. This is because lead-acid batteries are relatively cheap, the technology is very well proven and robust and there is a well-established infrastructure to recycle batteries. Over the longer term the emergence of mass-produced hybrid and pure electric vehicles may threaten the use of lead in automobiles, and some industrial applications may also be lost to new battery technologies. However, such developments are not expected to have a material impact on the lead market over the next ten years.

19.6.1 Gypsum Market

Gypsum is the main ingredient in plaster. Most gypsum that is produced in the world is made into gypsum wallboard. Another major use of gypsum is as a set retarder for portland cement. Synthetic gypsum, made during the flue gas desulphurisation process, can substitute for natural gypsum in wallboard manufacture and is gaining in market share.

In 2004, world gypsum production totalled 106 million tonnes. The United States produced the most gypsum at 18 million tonnes. Canada ranked Third, producing 9.3 million tonnes, 7.9 million of which came from Nova Scotia. Approximately half of Nova Scotia's gypsum production came from National Gypsum Canada Limited's Milford quarry, approximately ten kilometres from the Scotia Mine site. This quarry has been operating for over fifty years.

Specifications for gypsum used in wallboard manufacture vary slightly among producers. Typically, they require the gypsum content to be greater than 85 % and the total chloride ion content to be less than 100 ppm (parts per million).

The gypsum industry consists almost exclusively of vertically integrated corporations. Gypsum wallboard manufacturers typically own and operate their own mines. As a consequence, there is no spot market for gypsum.

Several companies have expressed an interest in the gypsum on the Scotia Mine site. A large quantity of gypsum will be removed as waste rock to uncover the zinc and lead Reserves. No formal contracts have yet been signed.

19.7 Contracts

No smelter contracts have been established. But, because the demand for concentrate by smelters currently exceed what mines can produce, there should be no trouble establishing smelter contracts at reasonable terms if production can commence within the year. As evidence of that statement, some smelters have recently been *paying* for zinc concentrate rather than adding a treatment charge (Roberts, 2006).

19.7.1 Smelter Returns

For zinc concentrates, a treatment charge must be paid to the smelter for each tonne of concentrate submitted that is linearly related to the spot market zinc price. There is a fixed charge per tonne plus a price escalator clause. The price escalator charge increases linearly for every dollar by which the spot price exceeds a certain value. For example, the benchmark fixed charge for 2005 was $US 126 (Roberts, 2006). At the end of 2005, the spot market zinc price was $US 1,900 per tonne of zinc metal. The average price escalator value was $US 0.14 for every dollar by which the price exceeded $US 1,400. Therefore the price escalator clause amounted to $US 70 per tonne extra ($0.14 x $500), for a total of $US 196 per tonne of concentrate.

Because of a zinc concentrate shortage in 2005, some smelters were actually paying for zinc concentrate rather than applying a treatment charge.

In addition to the treatment charge, the smelter generally retains 15 % of the zinc metal submitted. In other words, the smelter charges a treatment charge, then pays for 85 % of the zinc metal submitted.

Generally, the same arrangement also applies to lead. On average, in 2005, the fixed portion of the treatment charge was $US 135 and the price escalator value was $US 0.075, basis $US 800 (Roberts, 2006). On top of the treatment charge, the smelter pays for 95 % of the lead metal submitted.

19.7.2 Spot Prices

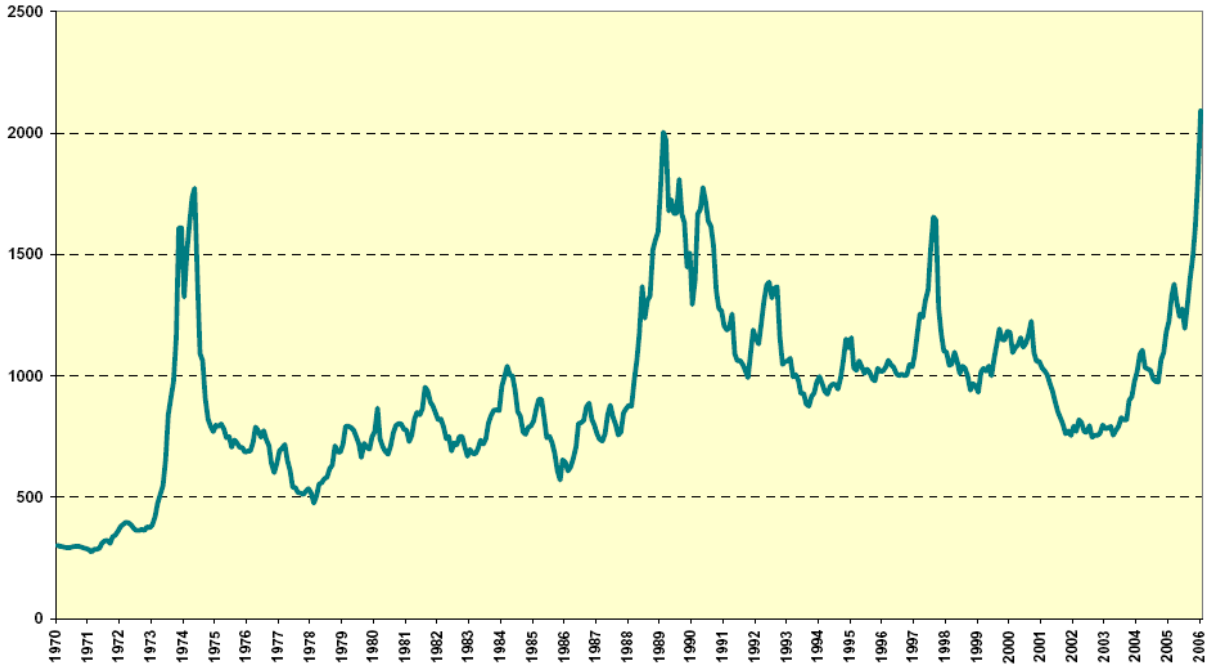
For both zinc and lead, concentrate treatment charges and the price that a smelter will pay for concentrate both depend on the spot markets. The London Metals Exchange (LME) publishes spot market prices for zinc and lead.

At the time of report writing, spot prices for zinc and lead were both at historic high levels (Figure 37 and Figure 38). The zinc and lead spot prices were approximately $US 3,590 ($1.63 per pound) and $US 1,156 per tonne ($0.53 per pound) of refined metal, respectively. The prices of both metals were recovering from near-historic low levels experience in 2002/2003, when zinc and lead spot prices were approximately $US 800 and $US 500 per tonne of refined metal, respectively.

From Figure 37, it appears that zinc prices have historically been cyclical. Generally, the price has been fairly steady and increasing at a slow, but steady rate. Every fifteen years, there has been a large price increase that lasted one or two years before falling again to a price that was somewhat higher than the pre-spike price.

Historically, lead prices (Figure 38) have also seemed cyclical, but with not as regular a frequency. High lead prices have not always occurred with high zinc prices.

Since 1970:



Three Months Ending July 10, 2006:

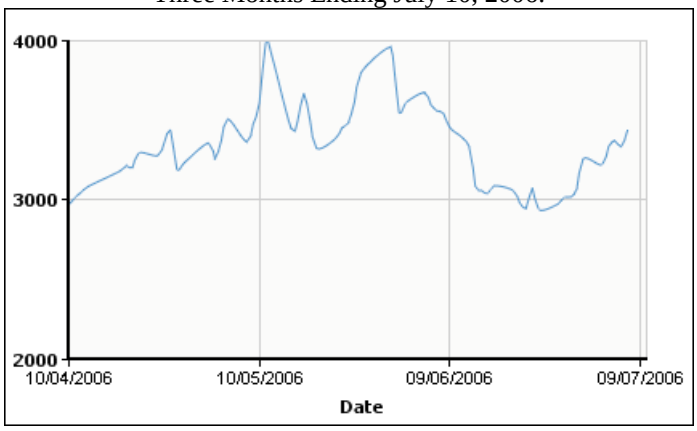
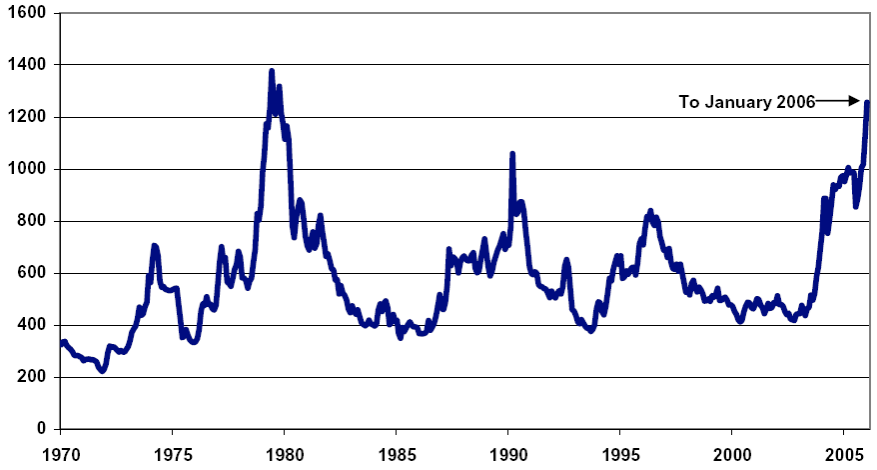


Figure 37: LME spot price history for zinc ($US per tonne of refined zinc).

Since 1970:



Three Months Ending July 10, 2006:

Figure 38: LME spot price history for lead ($US per tonne of refined lead).

Low metal prices during the late 1990's and early 2000's led to a swathe of mine closures. The effect on mine output was not limited to closures. Cash flow problems at many mines led to a reduction in exploration and development expenditures, which in turn led to attrition of output at existing operations. These effects are still negatively affecting the current level of output at some mines, though the increase in prices since late 2003 has led to substantial improvement in mine cash flow. Prices increased after 2003 as demand for zinc and lead increased, exceeding what the existing mines could supply.

The current high metal prices are causing new mines to come online and existing ones to expand production. In 2007, just a year away, the greenfield mine project pipeline starts to look much fuller, with some major projects expected to be commissioned. The largest of these is Apex Silver's San Cristobal open-pit project in Bolivia, expected to produce well over 200 kt/a contained zinc when it reaches full capacity (Roberts, 2006).

If supply starts growing at a faster rate without a corresponding increase in the demand growth rate, prices may begin to decline. Some analysts feel that this is about to occur,

starting in 2007 (Roberts, 2006). If they are correct, prices will drop from current levels, but not down to 2002/2003 levels (Table 28).

The anticipated (by some) drop in metal prices will likely be accompanied by a strengthening of the US dollar. Because most of the Scotia Mine's costs would be in Canadian dollars, a strengthening US dollar will soften the blow of decreasing metal prices.

Table 28: Prediction of metal prices to 2012 (Roberts, 2006).

Metal	2006	2007	2008	2009	2010	2011	2012
Zinc Spot Price							
($US/tonne)	1,800	1,700	1,200	1,000	1,100	950	950
($US/lb)	0.82	0.77	0.54	0.45	0.50	0.43	0.43
Lead Spot Price							
($US/tonne)	1,120	770	550	540	700	775	750
($US/lb)	0.51	0.35	0.25	0.25	0.32	0.35	0.34

Other analysts' forecasts are not so dismal. They believe that although the zinc supply will grow over the coming years, it will not keep pace with growth in demand (RBC, 2005). The market may remain in deficit until 2008 at the earliest. By 2009, RBC expects that production increases at existing operations and previously approved new projects will contribute 2.1 million tonnes of new supply, relative to 2004 (Table 29, Table 30 and Table 31). Permanent closures between 2006 and 2009 include the Brunswick and Mattagami (Bell Allard) mines in Canada, Bougrine in Tunisia and Poland's second largest zinc mine (Trzebionka) (Table 32).

Table 29: Summary of zinc mine production changes (kilotonnes) (RBC, 2005).

Change Type	**2006E**	**2007E**	**2008E**	**2009E**
Increases Existing Operations	1,418	1,809	2,083	2,073
New Projects	68	313	818	917
Sub-Total	**1,485**	**2,122**	**2,901**	**2,989**
Reductions Existing Operations	(474)	(536)	(621)	(762)
Total	**1,011**	**1,585**	**2,280**	**2,227**

Table 30: Production expansions at existing mines and approved projects (kilotonnes) (RBC, 2005).

Country Mine	2006E	2007E	2008E	2009E
Australia, Broken Hill	29	29	29	29
Australia, Endeavor	26	26	26	26
Australia, Golden Grove	80	95	70	70
Australia, Mount Isa	94	99	109	109
Bolivia, San Cristobal	-	105	210	210
Brazil, Vazante	9	28	28	28
Canada, Duck Pond	5	30	34	34
Canada, Kidd	42	42	37	22
Canada, Langlois	-	27	54	54
China, Lanping	56	56	56	56
India, Rampura-Agucha	130	150	170	170
Iran, Angouran	-	-	50	70
Ireland, Lisheen	19	24	29	29
Ireland, Tara	17	27	27	27
Kazakhstan, Shaimerden	20	50	60	60
Mongolia, Tumurtin Ovoo	30	35	36	36
Morocco, Guemassa	45	35	-	-
Pakistan, Duddar	-	5	55	55
Peru, Antamina	45	45	45	45
Portugal, Aljustrel	-	49	74	92
Portugal, Neves Corvo	14	27	46	40
Russia, Tarnyer	25	30	30	30
USA, Balmat	27	54	54	54
USA, Pend Oreille	25	25	25	25
USA, Red Dog	36	36	36	36
Other < 25ktpa	645	681	694	666
Sub-Total	**1,418**	**1,809**	**2,083**	**2,073**

Table 31: Production expansions at potential zinc mine projects (kilotonnes) (RBC, 2005).

Country Mine	2006E	2007E	2008E	2009E
Australia, Beltana -Flinders	-60	-	-	-
Australia, Hellyer Tailings	--	-	54	54
Australia, Lady Loretta	--	-	185	185
Australia, Pillara	--	205	205	205
Australia, Angas	--	23	46	46
Australia, Jaguar	-5	30	37	33
Burkina Faso, Perkoa	--	10	54	54
Canada, Caribou	-40	80	78	64
Canada, Perseverance	--	-	-	70
Canada, Wolverine	--	-	54	54
China, Lanping Phase 2	--	24	132	132
Indonesia, Dairi	--	60	188	183
Iran, Mehdiabad	--	-	80	160
Kazakhstan, Artemovsky	--	30	75	75
Mexico, Cozamin	--	25	25	25
Peru, Cerro Lindo	--	-	152	152
Russia, Ozernoe	--	-	-	70
Russia, Rubtsovsky	-30	60	60	60
Spain, Aguas Tenidas	--	24	68	68
Uzbekistan, Khandiza	--	35	76	76
Yemen, Jabali	--	17	63	63
Other < 25ktpa	--	2	4	4
Sub-Total	**-135**	**625**	**1,636**	**1,833**
Base Case = 50% of Potential Projects	**-68**	**313**	**818**	**917**

Table 32: Production reductions at existing zinc mines (kilotonnes) (RBC, 2005).

Country Mine	2006E	2007E	2008E	2009E
Canada, Bell Allard	(99)	(99)	(99)	(99)
Canada, Bouchard-Hebert	(58)	(58)	(58)	(58)
Canada, Brunswick	-	(6)	(20)	(20)
Canada, Trout Lake	(13)	(17)	(26)	(31)
Japan, Toyoha	(33)	(48)	(48)	(48)
Mexico, Bismark	-	-	(1)	(50)
Morocco, Guemassa	-	-	-	(30)
Poland, Trzebionka	(15)	(15)	(30)	(60)
Tunisia, Bougrine	(29)	(29)	(29)	(29)
Other < 25 ktpa	(227)	(264)	(310)	(337)
Sub-Total	**(474)**	**(536)**	**(621)**	**(762)**

RBC's price prediction for zinc is shown in Table 33. They predict relatively high zinc prices until 2009. In 2010 and beyond, as supply catches up with demand, prices will decrease toward $US 0.50 per pound. They also expect that treatment charges will remain low to 2009, at $US 90-110 per tonne of concentrate (Table 33). With a drop in prices in 2010 and beyond, treatment charges will increase to $US 180 per tonne.

Table 33: Zinc price prediction to 2009 (RBC, 2005).

	2006	2007	2008	2009	2010 and Beyond
Zinc Spot Price					
($US/tonne)	1,750	2,000	1,550	1,650	1,100
($US/lb)	0.80	0.90	0.70	0.75	0.50
Zinc Treatment Charge (base $US 1,000) ($US/tonne)	90	90	110	100	$180

Some analysts are even more optimistic. Based on falling inventory levels and increasing industrial demand in the short-term in Asia and the OECD nations, they believe that prices will increase over the near term to give average prices of $US 1.35 per pound of zinc for 2006 and $1.50 for 2007 (Rajeev, 2006).

Table 34 shows the metal price, treatment charge and exchange rate model that was adopted for this report. A sensitivity analysis was also carried out on those prices (Section 19.18).

Table 34: Adopted metal price, treatment charge and exchange rate model.

Item	Value
Zinc Spot Price ($US/lb)	1.10
Lead Spot Price ($US/lb)	0.40
Zinc Treatment Charge ($US/tonne)	170
Lead Treatment Charge ($US/tonne)	160
Exchange Rate ($US/$CAN)	0.86

19.7.3 Futures Markets

The London Metals Exchange reports the futures market prices for many metals including zinc and lead. For zinc, it reports futures contract prices for the next twenty-seven months. For lead, prices for the next fifteen months are reported. The LME spot and futures prices for July 13, 2006 are reported in Table 35. Futures prices take investment risk, inflation and supply and demand factors into account. Therefore, the expected spot price in say, fifteen months may be different from the 15-month futures price.

Selling future production is known as *hedging*. Hedging during falling prices partially insulates the mine's revenue. Generally, mines sell a portion of production at spot or contract prices and hedge the remainder.

Table 35: LME spot and futures prices for July 13, 2006 [$US per tonne of refined metal ($US per pound)].

Contract	Zinc	Lead
Immediate Cash Seller & Settlement	$3,590 ($1.63)	$1,156 ($0.53)
3-Months Seller	$3,595 ($1.63)	$1,151 ($0.52)
15-Months Seller	$2,985 ($1.37)	$1,143 ($0.52)
27-Months Seller	$2,408 ($1.09)	Not Reported

19.8 Water and Sewer

In the past, most of the process water was recycled from the polishing pond. It was pumped from there, through a pipeline back to the mill. Process make-up water, potable water and water for fire suppression was drawn from Gays River using another pump and pipeline. For showers, toilets *et cetera,* part of that water was filtered in a small, on-site filtration plant. Bottled water was provided for drinking. The proposed mining operation will continue that practice.

A relatively small septic field, of a size appropriate for the care-and-maintenance status of the site, was installed in 2005. Sewage and grey water used to disposed in the tailings pond. If permitted, that practice will be reinstated. If not permitted, it will be a straightforward matter to expand the current septic field.

19.9 Environmental Considerations

19.9.1 Progressive Reclamation

Reclamation will be an on-going process. The goal will be to minimise the overall land disturbance at any point in time. As much as possible, stripped waste rock and soil will be placed in their final resting places. As mining progresses, final grading and seeding will be carried out as soon as possible. At the end of the mine life, there should be very little reclamation left to carry out.

19.9.2 Final Reclamation

A conceptual reclamation plan was submitted during the environmental registration process. It was included as an appendix to the registration document (MGI, 1999). After the mine is decommissioned, it was proposed to allow the pit to fill with ground and surface water to create a deep lake. The temperature of the incoming groundwater will assist in the creation of conditions necessary for the lake waters to undertake seasonal turnovers, resulting in good mixing conditions and maintenance of acceptable dissolved oxygen levels.

Prior to the flooding of the pit, the edge areas and slopes that will become the new shoreline will be graded to a maximum allowable 2:1 slope. As appropriate, graded slopes ranging from 3:1 to 5:1 will be created in some areas of the new shoreline. Extending from above the projected water line to depths approaching ten metres, these shores will allow the development of a variety of shoreline habitats (terrestrial, riparian, emergent and submergent) and provide the potential for human recreational use. Submergent and emergent species will assist in the maintenance of water oxygen levels, improve the quality of water reaching the lake and provide a diverse habitat for a variety of terrestrial and aquatic species. The remainder of the area of the bottom of the lake will retain its rugged conditions to provide additional diverse and irregular substrate and subsurface habitat.

When the lake has filled with water to the same elevation as the water in the adjacent River channel, the dyke will be breached in two locations to connect the lake to the Gays River system. Future use of the lake could include artificial stocking with game fish species and/or fresh water aquaculture. However, water and habitat conditions and water quality would first need to be stabilised, and the ramifications of the introduction of non-local game fish carefully examined.

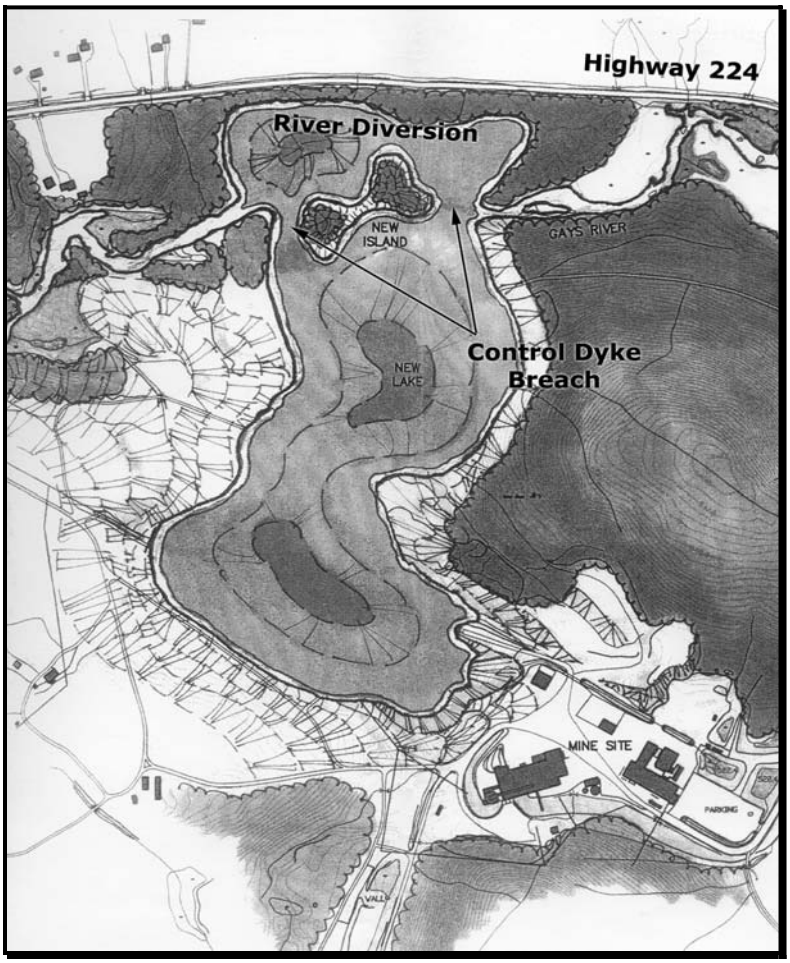


Figure 39: Conceptual reclamation plan (CBCL, 1999).

The final reclamation plan also includes dismantling the buildings, removing scrap from the property, contouring the property such that it blends with the surrounding topography, and seeding.

19.10 Revenue

The mill will start production in Month 11 of Year 1. Using the base case scenario (Table 34), net yearly revenue (after smelting costs) during the surface mining operation will be $43 million. For the underground operation, yearly revenue will be $58 million. See Table 43 for more details.

19.11 Taxes and Royalties

19.11.1 Taxes

Acadian purchased ScoZinc Limited as opposed to the Scotia Mine asset. Purchasing the company rather than the asset complicates the project from a taxation perspective. The ownership history, tax history, etc must be considered. To avoid overly complicating the tax model, the feasibility study was carried out on a project basis rather than a corporate one.

Net income is subject to Federal and Provincial tax at rates of 29.12 % and 16 %, respectively. There are several tax-related issues for the project, including Canadian Exploration Expenses (CEE), Canadian Development Expenses (CDE), capital cost allowances (CCA), resource allowance and the Atlantic Investment Tax Credit.

Most Canadian Exploration Expenses (CEE) are 100 % deductible against mining income. Eligible expenses include exploration, delineation and pre-production development.

Canadian Development Expenses (CDE) are depreciated on a 30 % declining balance. Eligible expenses include the cost of acquiring a mining property in Canada, sinking a mine shaft, main haulage way or similar underground work. It applies to development that is designed to be used for life use of the mine. The mine can deduct up to 30 % of the unclaimed balance in that pool at the end of each year. Unclaimed balances may be carried forward indefinitely.

Capital costs are depreciated according to a capital cost allowance. The rate for most mining equipment is 25 % per year (Class 41). In most cases, the amount deductible in the first year that an asset is acquired is subject to the "half-year" convention, which means that only one-half of the amount that would be deductible at the normal CCA rate of that asset class can be claimed.

In addition to the normal 25% rate of depreciation accorded to Class 41 assets, an accelerated capital cost allowance (ACCA) can provide for an additional depreciation allowance of up to 100 % of asset cost. To be eligible for that accelerated depreciation, however, assets must have been acquired before the beginning of commercial production or for major expansions.

In the calculation of taxable income, the ACCA deduction is taken after the normal CCA, but before the resource allowance, CEE and CDE. Essentially, the ACCA acts to provide the full write-off of capital costs before a mine starts to pay income tax.

The resource allowance is a tax deduction equal to 25 % of "resource profits." Resource profits are equal to revenue, less operating costs (excluding head office costs, royalties and mining taxes), less capital cost allowances. The resource allowance is being phased-out and will no longer exist after January 1, 2007. Replacing it will be a deduction for corporate income tax purposes of all payments of provincial and other Crown royalties and mining taxes.

An investment tax credit of 10% is available for capital investments in the Atlantic provinces. A business may deduct ten percent of eligible costs from its federal income tax liability. Eligible investments include qualifying buildings, machinery and equipment used or leased by the taxpayer.

19.11.2 Royalties

As stated in Section 3.2, Savage retains a 2 % net smelter return royalty. Acadian entered into an option agreement that would enable it to purchase the royalty for $1.45 million at the end of Year 1. That scenario was modelled in the economic analysis. Also, the Province of Nova Scotia levies another 2 % of net revenue royalty. For the purpose of calculating the royalty, net revenue is essentially equal to net smelter return, minus shipping costs.

19.12 Capital Cost Estimates

The purchase price for ScoZinc Limited and all of its assets was completed on July 6, 2006 for $CAN 7.5 million.

Capital costs are listed in Table 36. General project capital costs include permitting costs, a highway semi-dump truck for concentrate hauling and office equipment.

The mill, which has been under a care and maintenance condition for the past fifteen years, must be cleaned-up and re-commissioned. This will require a relatively minor amount of work (compared against building an entirely new mill). Belts will be replaced and gear oil will be changed. Heat will be applied to all of the motors to drive out any moisture. Bearings will be checked. Circuit breakers will be cleaned. The mill will be thoroughly cleaned and painted. The major capital items include labour for the re-commissioning work, a spare parts inventory and a heating system.

Because the mobile mining equipment will be leased, capital costs for the surface mine will be relatively minor. The most significant cost will be a fleet of four utility pick-up trucks.

Pre-production stripping will take approximately two months and cost approximately two million dollars. In the economic analysis, this cost was applied as an operating cost rather than a capital cost.

The overall capital cost for the surface mining operation, excluding pre-production stripping, is $2.9 million.

As the surface mine nears completion, the underground mine will start developing. For this work, drill jumbos, scooptrams (load-haul-dump units), a haul truck, utility vehicles, tractors, a compressor, fans, a raise climber, a backfill mixing plant and numerous other pieces of equipment must be purchased. The overall capital cost for the underground mining operation is $5.6 million.

Table 36: Capital costs.

Item	Cost
ScoZinc Purchase Price (Sale Completed)	$7.5 million
Savage Royalty Purchase	$1.45 million
Surface Mining Operation	$2.9 million
Subtotal	$11.9 million
Underground Mining Operation	$5.6 million

19.13 Operating Cost Estimates

Operating costs were based on producing 2,000 tonnes per day from the surface mine, then 1,350 tonnes per day from the underground mine. The operation would run 350 days per year, twenty-four hours per day in two shifts of ten hours each.

19.13.1Labour

At the time of report writing, there was a Canada-wide shortage of trades-people and mineral industry professionals. However, recruiting for this project will not be nearly as difficult as an equivalent project in a remote location. Its closeness to Halifax will be attractive for many people. Also, for the first few years of operation, relatively few skilled workers will be required. The majority of processing plant operators and surface mine equipment operators can be trained on-the-job.

For the staff, pay rates will range from $40,000 for clerical work to $100,000 for the manager (without burden) (Table 36 and Table 37). Salary burden includes Canada Pension Plan, unemployment insurance, vacation pay, Workers Compensation Board premiums, a basic pension plan and a basic health plan. Burden averages 19 % of salary.

For the surface shift workers including processing plant workers and equipment operators, salaries range from $30,000 for general labourers to $60,000 for supervisors. Burden averages 19 % of salary.

Pay rates are much higher for underground miners. Salaries for underground miners average $100,000, plus burden.

There is no history of unionised labour at Gays River. However, part of the workforce is unionised at National Gypsum's quarry in nearby Milford, Nova Scotia.

Table 37: Staffing requirements.

Staff

Department	Members	Salary	Burden[3]	Yearly Total
Engineering	2	$ 60,000	12,000	$ 144,000
Engineering Technicians	2	$ 50,000	10,000	$ 120,000
Management	1	$ 100,000	17,000	$ 117,000
Mine Superintendent	1	$ 80,000	14,000	$ 94,000
Mill Superintendent	1	$ 80,000	14,000	$ 94,000
Health and Safety	1	$ 60,000	12,000	$ 72,000
Accounting	1	$ 50,000	10,000	$ 60,000
Human Resources / Payroll	1	$ 40,000	9,000	$ 49,000
Geology	2	$ 50,000	10,000	$ 120,000
Secretarial	1	$ 40,000	9,000	$ 49,000
Purchaser	1	$ 60,000	12,000	$ 72,000
Subtotal:	14			$ 1,000,000

Surface Shift Workers:

Department	Members per Shift	Salary	Burden[3]	Number of Shifts	Number of Workers	Yearly Total
Indirect Labour:						
Mechanic	1	$ 40,000	9,000	2	2	$ 98,000
Electrician	1	$ 50,000	10,000	2	2	$ 120,000
Clerk	1	$ 30,000	8,000	2	2	$ 76,000
Security	1	$ 30,000	8,000	3	3	$ 114,000
Cleaning Staff	1	$ 30,000	8,000	3	3	$ 114,000
Subtotal	5				12	$ 500,000
Direct Labour:						
Front-end Loader Operator	1	$ 40,000	9,000	1	1	$ 49,000
Supervision (Pit Foreman)	1	$ 60,000	12,000	1	1	$ 72,000
Mill Foreman	1	$ 60,000	12,000	1	1	$ 72,000
Crusher Operator	1	$ 40,000	9,000	2	2	$ 98,000
Grinding Mill Operator	2	$ 40,000	9,000	2	4	$ 196,000
Flotation Section Operator	2	$ 50,000	10,000	2	4	$ 240,000
Dewatering	2	$ 40,000	9,000	2	4	$ 196,000
Millwrights	1	$ 50,000	10,000	3	3	$ 180,000
Assay Office:						
Chief Assayer	1	$ 50,000	10,000	1	1	$ 60,000
Assayers	2	$ 40,000	9,000	2	4	$ 196,000
Buckers	1	$ 35,000	8,000	2	2	$ 86,000
Helpers	2	$ 35,000	8,000	2	4	$ 172,000
Subtotal	17				31	$ 1,617,000
Total	22				43	$ 2,117,000

Underground Shift Workers:

Department	Members per Shift	Salary	Burden[3]	Number of Shifts	Number of Workers	Yearly Total
Drill Jumbo Operators	2	$ 100,000	17,000	3	6	$ 702,000
Nippers/Scoop/Slusher Operators	2	$ 100,000	17,000	3	6	$ 702,000
Jackleg Miners	1	$ 100,000	17,000	3	3	$ 351,000
Scoop Operators	2	$ 100,000	17,000	3	6	$ 702,000
Truck Drivers	1	$ 100,000	17,000	3	3	$ 351,000
Raise Miners	2	$ 100,000	17,000	3	6	$ 702,000
Ground Control	2	$ 100,000	17,000	3	6	$ 702,000
Underground Supervisor	1	$ 100,000	17,000	3	3	$ 351,000
Diamond Driller	1	$ 100,000	17,000	3	3	$ 351,000
General Labour	2	$ 80,000	14,000	3	6	$ 564,000
Fill Plant Operator (Surface)	1	$ 40,000	9,000	1	1	$ 49,000
					49	$ 5,527,000

Table 38: Summary of labour force. Salaries include burden.

Surface Mining:

	Number	Average Salary[1]	Total
Salaried	14	$ 71,000	$ 1,000,000
Indirect Labour	12	$ 42,000	$ 500,000
Direct Labour	31	$ 52,000	$ 1,617,000
Equipment Operators	28	$ 56,000	$ 1,568,000
Total	85	$ 55,000	$ 4,685,000

Underground Mining:

	Number	Average Salary[4]	Total
Salaried	14	$ 71,000	$ 1,000,000
Indirect Labour	12	$ 42,000	$ 500,000
Direct Labour	49	$ 113,000	$ 5,527,000
Total	75	$ 94,000	$ 7,027,000

19.13.2 Electric Power

The Scotia Mine site is currently supplied with three-phase power from the grid. Nova Scotia Power will supply electricity to the site using Rate 22. Peak demand is charged monthly at $8.01 per kVA (kilovolt-ampere) per month when customers use their own transformers. Usage is charged at a rate of $0.048 per kWh (kilowatt-hour).

19.13.3 Ongoing Development

For the surface mine, ongoing development is included in the operating costs and includes stripping, haul road construction and waste rock removal.

For the underground mine, ongoing development includes drift, ramp, cross-cut and raise construction. In total, approximately 4,000 metres of drifts and ramps are required. For an underground mine life of 2 ½ years, the average yearly development requirement is 1,600 metres per year. Also, a minimum of 1,000 metres of raising is required over the mine life for a yearly average of 400 metres.

19.13.4 Yearly Operating Costs

Operating the surface mine and processing plant is expected to cost $19 million per year or $27 per tonne of ore (Table 39). Operating the underground mine and processing plant is expected to cost $23 million per year or $49 per tonne of ore (Table 40).

Table 39: Average yearly operating cost estimate for the surface mining operation.

Item	Yearly Cost ($)	Cost per Tonne of Ore ($)	Cost per Pound of Zinc-Equivalent* ($US)
Overhead			
General	$ 1,600,000	$ 2.30	$ 0.03
Support	$ 700,000	$ 1.00	$ 0.01
Processing	$ 6,700,000	$ 9.60	$ 0.12
Surface Mining	$ 9,700,000	$ 13.80	$ 0.18
Subtotal	$ 18,700,000	$ 26.70	$ 0.34

* One pound of lead equals 0.43 pounds of zinc.

Table 40: Average yearly operating cost estimate during underground mining.

Item	Yearly Cost ($)	Cost per Tonne of Ore ($)	Cost per Pound of Zinc-Equivalent* ($US)
Overhead			
General	$ 1,600,000	$ 3.40	$ 0.02
Support	$ 700,000	$ 1.50	$ 0.01
Processing	$ 6,700,000	$ 14.20	$ 0.09
Underground Mining	$ 14,100,000	$ 29.70	$ 0.18
Subtotal	$ 23,100,000	$ 48.80	$ 0.30

* One pound of lead equals 0.43 pounds of zinc.

The operating costs per pound of zinc-equivalent are $US 0.34 and $US 0.30 for surface and underground mining, respectively. Figure 40 shows the zinc producer cost curve for 2005. It shows that approximately half of world-wide zinc is produced for $US 0.25-0.37 per pound. The estimated operating cost for Scotia Mine is competitive with other major producers.

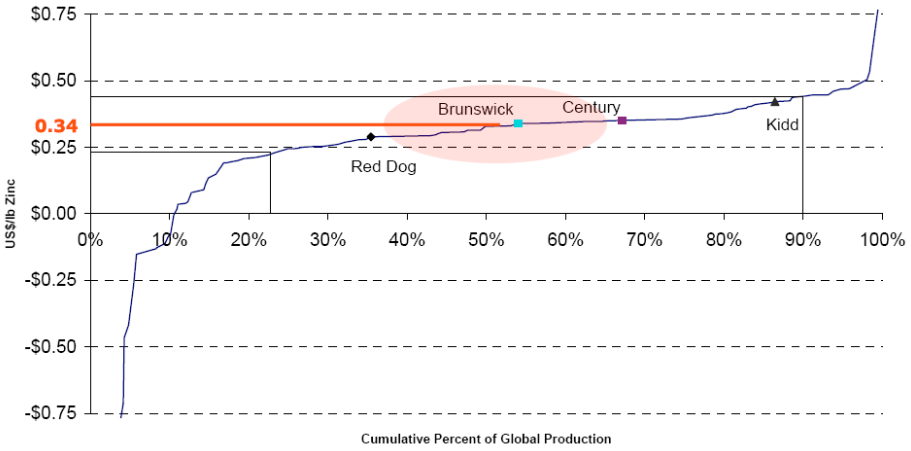


Figure 40: Zinc producer cost curve for 2005 (RBC, 2005).

19.14 Timing of Cash Flows

The timing of cash flows determines the amount of initial working capital that is required. Mill repair will take 4-6 months and will start in Month 6 (Table 41). Pre-production stripping will last two months and will begin in Month 10, or as soon as the equipment is delivered. Ore production will begin two months later in Month 12.

It will take approximately two weeks to stockpile enough concentrate for an initial shipment of ten rail cars (1,000 tonnes). The initial payment, consisting of 85 % of the concentrate value, is paid thirty days after the concentrate is shipped.

The timing and amount of the final payment depends on several factors. Firstly, the price per pound of metal is determined by averaging the spot metal prices for one month after the concentrate is shipped. Secondly, the average concentrate grade is determined through an exhaustive assaying process. The results are shared with the mine and if they disagree, samples are sent to an independent umpire. This process can take at least 2-3 months. If the mine agrees with the assays, the final payment may be paid in as little as 6-8 weeks after concentrate shipment.

Table 41: Timing of cash flows.

Activity	Start Time (Month)
Mill Repair	6
Pre-production Stripping	10
Ore Production	12
Initial Payment (85 %)	13 ½
Remaining Payment (15 %)	15 ½ (or later)

19.15 Working Capital

The minimum initial working capital requirement is equal to the minimum cash balance during start-up. This was determined through analysing the project's start-up cash flow, on a month-by-month basis, for the first twenty-four months (Appendix 5). The minimum cash balance was calculated to be -$5.1 million, occurring during Month 13. A contingency amount, equal to four months operating costs or $6.0 million, should also be added to cover any initial start-up challenges. Therefore, the total initial working capital requirement, including contingency, is $11.1 million.

During the project's operation, enough cash will be retained to cover operating costs for the following three months. At a total operating cost of approximately $1.5 million per month during surface mining, $4.5 million in working capital will continually be maintained. During underground mining, working capital will be maintained at $5.9 million.

19.16 Financing

The project will be financed through debt and equity financing. Equity financing was raised to cover the $7.5 million purchase price of ScoZinc Limited. The minimum level of project financing that is required is $15,500,000 (Table 42).

Table 42: Required project financing.

ScoZinc Purchase Price	$7,500,000
Savage Royalty Purchase	$1,450,000
Capital Costs	$2,900,000
Initial Working Capital	$11,100,000
Project Financing Required	**$23,000,000**
Debt	*$15,500,000*
Equity	*$7,500,000*

19.17 Economic Analysis

The economic analysis indicated that the project is very profitable. The analysis was carried out on an after-tax basis. Table 43 shows the project's income. The complete economic analysis is reported in Appendix 5.

The after-tax, net present value of the project, using base case parameters (Table 34) and an 8 % discount rate ($NPV_{8\%}$) was $73.6 million. The internal rate of return was 76 %. The profitability using other discount rates was:

$NPV_{7.5\%}$	$	75,687,000
$NPV_{8.0\%}$	$	73,628,000
$NPV_{10.0\%}$	$	66,028,000
$NPV_{12.5\%}$	$	57,789,000
$NPV_{15.0\%}$	$	50,723,000
Internal Rate of Return (IRR)		76%

Table 43

Accounting Income

Initial Capital Costs

Scozinc Purchase Price	$ 7,500,000
Savage 2% NSR Royalty Purchase	$ 1,450,000
Capital Costs	$ 2,931,000
Initial Working Capital[6]	$ 11,100,000
Percentage Debt Financing	67%
Total Financing Required	$ 22,981,000
Debt	*$ 15,481,000*
Equity	*$ 7,500,000*

Schedule for Initial Capital Outlay

Multiplying Factor: 100%

	Year 1 (Beginning)	***Year 1 Q3***	***Year 1 Q4***	Year 1 (End)	Year 2	Year 3	Year 4	Year 5	Year 6	Year 7	Year 8	Year 9
General		*$ 320,000*										
Mine Site		*$ 203,000*			$ 95,000							
Processing Plant		*$ 2,408,000*										
Underground				$ -	$ -	$ -	$ -	$ -	$ 5,582,000	$ -	$ -	$ -
Subtotal	$ -	*$ 2,931,000*	*$ -*	$ -	$ 95,000	$ -	$ -	$ -	$ 5,582,000	$ -	$ -	$ -
Tonnes of Ore Mined			*58,000*	58,000	700,000	700,000	700,000	700,000	662,000	473,000	473,000	124,000

Revenue

Revenue[4]			*$ 3,532,000*	$ 3,532,000	$ 42,618,000	$ 42,618,000	$ 42,618,000	$ 42,618,000	$ 45,623,000	$ 60,274,000	$ 60,274,000	$ 15,810,000
Subtotal			*$ 3,532,000*	$ 3,532,000	$ 42,618,000	$ 42,618,000	$ 42,618,000	$ 42,618,000	$ 45,623,000	$ 60,274,000	$ 60,274,000	$ 15,810,000
Per Tonne of Ore			*$ 60.90*	*$ 60.90*	*$ 60.90*	*$ 60.90*	*$ 60.90*	*$ 60.90*	*$ 68.90*	*$ 127.40*	*$ 127.40*	*$ 127.50*

Royalties Paid

Nova Scotia Government (2 %)[9]			*$ 68,000*	$ 68,000	$ 820,000	$ 820,000	$ 820,000	$ 820,000	$ 880,000	$ 1,173,000	$ 1,173,000	$ 308,000
Subtotal			*$ 68,000*	$ 68,000	$ 820,000	$ 820,000	$ 820,000	$ 820,000	$ 880,000	$ 1,173,000	$ 1,173,000	$ 308,000

Direct Operating Costs[1]

Multiplying Factor: 100%

	Year 1 (Beginning)	***Year 1 Q3***	***Year 1 Q4***	Year 1 (End)	Year 2	Year 3	Year 4	Year 5	Year 6	Year 7	Year 8	Year 9
Mining Costs			*$ 2,038,000*	*$ 2,038,000*	*$ 9,912,000*	*$ 10,527,000*	*$ 10,652,000*	*$ 10,777,000*	*$ 11,449,000*	*$ 15,220,000*	*$ 15,220,000*	*$ 3,990,000*
Processing Costs			*$ 557,000*	*$ 557,000*	*$ 6,685,000*	*$ 6,685,000*	*$ 6,685,000*	*$ 6,685,000*	*$ 6,685,000*	*$ 6,685,000*	*$ 6,685,000*	*$ 1,753,000*
Subtotal			*$ 2,595,000*	$ 2,595,000	$ 16,597,000	$ 17,212,000	$ 17,337,000	$ 17,462,000	$ 18,134,000	$ 21,905,000	$ 21,905,000	$ 5,743,000
Per Tonne of Ore			*$ 44.70*	*$ 44.70*	*$ 23.80*	*$ 24.60*	*$ 24.80*	*$ 25.00*	*$ 27.40*	*$ 46.30*	*$ 46.30*	*$ 46.30*
Mining Costs per Tonne of Ore:	*$ -*	*$ -*	*$ 35.10*	*$ 35.10*	*$ 14.20*	*$ 15.00*	*$ 15.20*	*$ 15.40*	*$ 17.30*	*$ 32.20*	*$ 32.20*	*$ 32.20*
Processing Costs per Tonne of Ore:	*$ -*	*$ -*	*$ 9.60*	*$ 9.60*	*$ 9.60*	*$ 9.60*	*$ 9.60*	*$ 9.60*	*$ 10.10*	*$ 14.10*	*$ 14.10*	*$ 14.10*

Operating Cash Flow

Revenue	$ -		*$ 3,532,000*	$ 3,532,000	$ 42,618,000	$ 42,618,000	$ 42,618,000	$ 42,618,000	$ 45,623,000	$ 60,274,000	$ 60,274,000	$ 15,810,000
Royalties Paid	$ -		*$ 68,000*	$ 68,000	$ 820,000	$ 820,000	$ 820,000	$ 820,000	$ 880,000	$ 1,173,000	$ 1,173,000	$ 308,000
Direct Operating Costs	$ -		*$ 2,595,000*	$ 2,595,000	$ 16,597,000	$ 17,212,000	$ 17,337,000	$ 17,462,000	$ 18,134,000	$ 21,905,000	$ 21,905,000	$ 5,743,000
Subtotal	$ -		*$ 869,000*	$ 869,000	$ 25,201,000	$ 24,586,000	$ 24,461,000	$ 24,336,000	$ 26,609,000	$ 37,196,000	$ 37,196,000	$ 9,759,000
Per Tonne of Ore	*$ -*		*$ 15.00*	*$ 15.00*	*$ 36.00*	*$ 35.10*	*$ 34.90*	*$ 34.80*	*$ 40.20*	*$ 78.60*	*$ 78.60*	*$ 78.70*

Overhead Costs

Overhead		*$ 407,000*	*$ 407,000*	$ 815,000	$ 1,629,000	$ 1,629,000	$ 1,629,000	$ 1,629,000	$ 1,629,000	$ 1,629,000	$ 1,629,000	$ 834,000
Subtotal	$ -	*$ 407,000*	*$ 407,000*	$ 815,000	$ 1,629,000	$ 1,629,000	$ 1,629,000	$ 1,629,000	$ 1,629,000	$ 1,629,000	$ 1,629,000	$ 834,000
Per Tonne of Ore		*$ -*	*$ 7.00*	*$ 14.10*	*$ 2.30*	*$ 2.30*	*$ 2.30*	*$ 2.30*	*$ 2.50*	*$ 3.40*	*$ 3.40*	*$ 6.70*

Net Operating Income (Gross Margin)

	Year 1 (Beginning)	***Year 1 Q3***	***Year 1 Q4***	Year 1 (End)	Year 2	Year 3	Year 4	Year 5	Year 6	Year 7	Year 8	Year 9
Operating Cash Flow	$ -	*$ -*	*$ 869,000*	$ 869,000	$ 25,201,000	$ 24,586,000	$ 24,461,000	$ 24,336,000	$ 26,609,000	$ 37,196,000	$ 37,196,000	$ 9,759,000
Overhead Costs	$ -	*$ 407,000*	*$ 407,000*	$ 815,000	$ 1,629,000	$ 1,629,000	$ 1,629,000	$ 1,629,000	$ 1,629,000	$ 1,629,000	$ 1,629,000	$ 834,000
Net Operating Income (Gross Margin)	$ -	*-$ 407,000*	*$ 462,000*	$ 54,000	$ 23,572,000	$ 22,957,000	$ 22,832,000	$ 22,707,000	$ 24,980,000	$ 35,567,000	$ 35,567,000	$ 8,925,000
Per Tonne of Ore	*n/a*	*$ -*	*$ 8.00*	*$ 0.90*	*$ 33.70*	*$ 32.80*	*$ 32.60*	*$ 32.40*	*$ 37.70*	*$ 75.20*	*$ 75.20*	*$ 72.00*

Taxes and Interest

Net Operating Income (Gross Margin)	$ -	*-$ 407,000*	*$ 462,000*	$ 54,000	$ 23,572,000	$ 22,957,000	$ 22,832,000	$ 22,707,000	$ 24,980,000	$ 35,567,000	$ 35,567,000	$ 8,925,000
Minus Loss Carried Forward	$ -	*$ -*	*$ -*	$ -	$ 1,305,000	$ -	$ -	$ -	$ -	$ -	$ -	$ -
Capital Cost Allowance Deduction	$ -	*$ -*	*$ -*	$ 54,000	$ 2,972,000	$ -	$ -	$ -	$ 5,582,000	$ -	$ -	$ -
Resource Allowance Deduction	$ -	*$ -*	*$ -*	$ 221,000	$ 5,762,000	$ 6,352,000	$ 6,320,000	$ 6,289,000	$ 5,477,000	$ 9,592,000	$ 9,592,000	$ 2,517,000
Interest Expenses	$ -	*$ -*	*$ -*	$ 1,084,000	$ 1,084,000	$ 232,000	$ -	$ -	$ -	$ -	$ -	$ -
Taxable Income	$ -	*-$ 407,000*	*$ 462,000*	-$ 1,305,000	$ 12,449,000	$ 16,373,000	$ 16,512,000	$ 16,418,000	$ 13,921,000	$ 25,975,000	$ 25,975,000	$ 6,408,000
Federal Income Tax (29.12 %)				$ -	$ 3,625,000	$ 4,768,000	$ 4,808,000	$ 4,781,000	$ 4,054,000	$ 7,564,000	$ 7,564,000	$ 1,866,000
Nova Scotia Income Tax (16 %)				$ -	$ 1,992,000	$ 2,620,000	$ 2,642,000	$ 2,627,000	$ 2,227,000	$ 4,156,000	$ 4,156,000	$ 1,025,000
Total Income Tax Payable				$ -	$ 5,617,000	$ 7,388,000	$ 7,450,000	$ 7,408,000	$ 6,281,000	$ 11,720,000	$ 11,720,000	$ 2,891,000

Net Income After Interest and Taxes

Net Operating Income (Gross Margin)	$ -	*-$ 407,000*	*$ 462,000*	$ 54,000	$ 23,572,000	$ 22,957,000	$ 22,832,000	$ 22,707,000	$ 24,980,000	$ 35,567,000	$ 35,567,000	$ 8,925,000
Total Income Tax Payable	$ -	*$ -*	*$ -*	$ -	$ 5,617,000	$ 7,388,000	$ 7,450,000	$ 7,408,000	$ 6,281,000	$ 11,720,000	$ 11,720,000	$ 2,891,000
Interest on Capital	$ -	*$ -*	*$ -*	$ 1,084,000	$ 1,084,000	$ 232,000	$ -	$ -	$ -	$ -	$ -	$ -
Net Income After Interest and Taxes	$ -	*-$ 407,000*	*$ 462,000*	-$ 1,030,000	$ 16,871,000	$ 15,337,000	$ 15,382,000	$ 15,299,000	$ 18,699,000	$ 23,847,000	$ 23,847,000	$ 6,034,000

Present Value of Net Income	Year 1 (Beginning)	***Year 1 Q3***	***Year 1 Q4***	Year 1 (End)	Year 2	Year 3	Year 4	Year 5	Year 6	Year 7	Year 8	Year 9
Net Income After Interest and Taxes	$ -	-$ 407,000	$ 462,000	-$ 1,030,000	$ 16,871,000	$ 15,337,000	$ 15,382,000	$ 15,299,000	$ 18,699,000	$ 23,847,000	$ 23,847,000	$ 6,034,000
Less Scozinc Purchase Price	$ 7,500,000											
Less Pasminco Royalty Purchase	$ 50,000			$ 1,400,000								
Less Initial Capital Costs	$ 2,931,000			$ -	$ -	$ -	$ -	$ -	$ -	$ -	$ -	$ -
Less Capital Additions	$ -			$ -	$ 95,000	$ -	$ -	$ -	$ 5,582,000	$ -	$ -	$ -
Subtotal	-$ 10,481,000	-$ 407,000	$ 462,000	-$ 2,430,000	$ 16,776,000	$ 15,337,000	$ 15,382,000	$ 15,299,000	$ 13,117,000	$ 23,847,000	$ 23,847,000	$ 6,034,000
Cumulative	-$ 10,481,000			-$ 12,856,000	$ 3,920,000	$ 19,257,000	$ 34,639,000	$ 49,938,000	$ 63,055,000	$ 86,902,000	$ 110,749,000	$ 116,783,000

$NPV_{7.5\%}$	$ 75,687,000
$NPV_{8.0\%}$	$ 73,628,000
$NPV_{10.0\%}$	$ 66,028,000
$NPV_{12.5\%}$	$ 57,789,000
$NPV_{15.0\%}$	$ 50,723,000
Internal Rate of Return (IRR)	76%

Overall Cash Flow

Net Income After Interest and Taxes	$ -	-$ 407,000	$ 462,000	-$ 1,030,000	$ 16,871,000	$ 15,337,000	$ 15,382,000	$ 15,299,000	$ 18,699,000	$ 23,847,000	$ 23,847,000	$ 6,034,000
Capital Additions (Recurring Capital)	$ -	$ -	$ -	$ -	$ 95,000	$ -	$ -	$ -	$ 5,582,000	$ -	$ -	$ -
Debt Financing Repayment	$ -	$ -	$ -	$ -	$ 12,161,000	$ 3,320,000	$ -	$ -	$ -	$ -	$ -	$ -
Distributed Cash Flow[8]	$ -	-$ 407,000	$ 462,000	-$ 1,030,000	$ 4,615,000	$ 12,017,000	$ 15,382,000	$ 15,299,000	$ 13,117,000	$ 23,847,000	$ 23,847,000	$ 6,034,000
Cumulative Cash Flow	*$ -*	*-$ 407,000*	*$ 55,000*	*-$ 975,000*	*$ 3,640,000*	*$ 15,657,000*	*$ 31,039,000*	*$ 46,338,000*	*$ 59,455,000*	*$ 83,302,000*	*$ 107,149,000*	*$ 113,183,000*

Tax Calculations Capital Cost Allowance Accelerated Rate (100 %)	Year 1 (Beginning)	***Year 1*** ***Q3***	***Year 1*** ***Q4***	Year 1 (End)	Year 2	Year 3	Year 4	Year 5	Year 6	Year 7	Year 8	Year 9
Beginning Balance	$ -			$ -	$ 2,877,000	$ -	$ -	$ -	$ -	$ -	$ -	$ -
Additions	$ -			$ 2,931,000	$ 95,000	$ -	$ -	$ -	$ 5,582,000	$ -	$ -	$ -
Allowable Deduction[2]	$ -			$ 2,931,000	$ 2,972,000	$ -	$ -	$ -	$ 5,582,000	$ -	$ -	$ -
Deduction Taken	$ -			$ 54,000	$ 2,972,000	$ -	$ -	$ -	$ 5,582,000	$ -	$ -	$ -
Ending Balance	$ -			$ 2,877,000	$ -	$ -	$ -	$ -	$ -	$ -	$ -	$ -
Resource Allowance												
Revenue				$ 3,532,000	$ 42,618,000	$ 42,618,000	$ 42,618,000	$ 42,618,000	$ 45,623,000	$ 60,274,000	$ 60,274,000	$ 15,810,000
Expenses and Deductions												
Operating Costs				*$ 2,595,000*	*$ 16,597,000*	*$ 17,212,000*	*$ 17,337,000*	*$ 17,462,000*	*$ 18,134,000*	*$ 21,905,000*	*$ 21,905,000*	*$ 5,743,000*
Capital Cost Allowance				*$ 54,000*	*$ 2,972,000*	*$ -*	*$ -*	*$ -*	*$ 5,582,000*	*$ -*	*$ -*	*$ -*
Subtotal, Expenses				$ 2,649,000	$ 19,569,000	$ 17,212,000	$ 17,337,000	$ 17,462,000	$ 23,716,000	$ 21,905,000	$ 21,905,000	$ 5,743,000
Resource Profits				$ 883,000	$ 23,049,000	$ 25,406,000	$ 25,281,000	$ 25,156,000	$ 21,907,000	$ 38,369,000	$ 38,369,000	$ 10,067,000
Earned Depletion Allowance[13]				$ 221,000	$ 5,762,000	$ 6,352,000	$ 6,320,000	$ 6,289,000	$ 5,477,000	$ 9,592,000	$ 9,592,000	$ 2,517,000
Debt Financing												
Opening Debt Balance[7]	$ 15,481,000			$ 15,481,000	$ 15,481,000	$ 3,320,000	$ -	$ -	$ -	$ -	$ -	$ -
Net Income After Interest and Taxes	$ -			-$ 1,030,000	$ 16,871,000	$ 15,337,000	$ 15,382,000	$ 15,299,000	$ 18,699,000	$ 23,847,000	$ 23,847,000	$ 6,034,000
Working Capital Required[12]				$ 4,557,000	$ 4,710,000	$ 4,742,000	$ 4,773,000	$ 4,941,000	$ 5,884,000	$ 5,884,000	$ 1,644,000	$ -
Debt Repayment[7]	$ -			$ -	$ 12,161,000	$ 3,320,000	$ -	$ -	$ -	$ -	$ -	$ -
Closing Debt Balance	$ 15,481,000			$ 15,481,000	$ 3,320,000	$ -	$ -	$ -	$ -	$ -	$ -	$ -

Notes:
1. Considering pre-production requirements (pre-stripping).
2. Allowable deduction, under ACCA, is up to 100 % of taxable income.
4. Net Smelter Return.
6. Minimum cash balance during start-up, plus contingency.
7. Proportion of debt capital paid back reflects the overall proportion of debt financing.
8. The Board of Directors may choose to pay out a portion of this figure as dividends.
9. Royalty is a percentage of Net Revenue (after smelting charges and concentrate shipping costs have been deducted.
10. Royalties are a percentage of net revenue (after smelting charges have been deducted).
11. After capital repayment.
12. Three months operating expenses.
13. 25 % of Resource Profits.

19.18 Sensitivity Analysis

A sensitivity analysis was carried out to gauge the sensitivity of the project's profitability to changes in metal prices, mine dilution, grade, initial capital costs, operating costs and exchange rate. The profitability indicators that were observed were the project's net present value, using a 8 % discount rate ($NPV_{8\%}$), and the project's internal rate of return (IRR).

Most parameters were varied to plus or minus 20 % of the base case value. Metal prices were varied to minus 50 % and plus 30 % of the base case values. As one parameter was varied, the other parameters maintained their base case values.

From Figure 41, one can see that factors affecting the revenue, such as metal prices, grade, dilution and exchange rate, had a greater effect on profitability than factors affecting the costs, such as operating costs and initial capital costs. In other words, profitability is most sensitive to changes in metal prices, grade, dilution and exchange rate. It is less sensitive to changes in operating costs and relatively insensitive to changes in initial capital costs. Recall that the surface mobile equipment fleet will be leased.

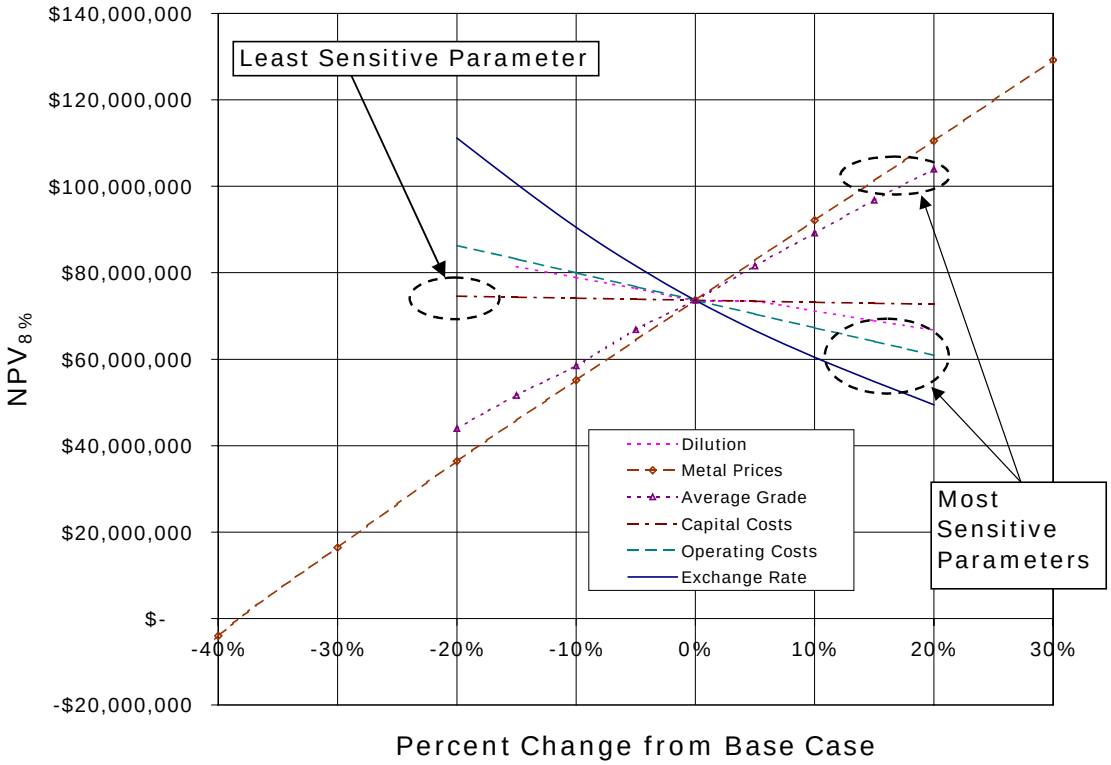


Figure 41: Sensitivity analysis.

Table 44: Sensitivity analysis.

Parameter: Metal Prices

Percent Change	Zinc Price ($US per lb)	Lead Price ($US per lb)	$NPV_{8\%}$	IRR
-50.0%	$ 0.55	$ 0.20	-$ 32,040,000	Undefined
-40.0%	$ 0.66	$ 0.24	-$ 3,990,000	Undefined
-30.0%	$ 0.77	$ 0.28	$ 16,430,000	29%
-20.0%	$ 0.88	$ 0.32	$ 36,410,000	48%
-10.0%	$ 0.99	$ 0.36	$ 55,140,000	63%
0.0%	$ 1.10	$ 0.40	$ 73,630,000	76%
10.0%	$ 1.21	$ 0.44	$ 92,110,000	89%
20.0%	$ 1.32	$ 0.48	$ 110,510,000	100%
30.0%	$ 1.43	$ 0.52	$ 129,200,000	111%
40.0%	$ 1.54	$ 0.56	$ 147,580,000	121%

Parameter: Dilution

Percent Change	Dilution	$NPV_{8\%}$	IRR
-15%	0.0%	$ 81,410,000	90%
-10%	5.0%	$ 78,890,000	85%
-5%	10.0%	$ 76,370,000	81%
0%	15.0%	$ 73,630,000	76%
5%	20.0%	$ 73,343,000	73%
10%	25.0%	$ 71,170,000	69%
15%	30.0%	$ 68,910,000	65%
20%	35.0%	$ 66,720,000	61%

Parameter: Average Grade (Surface & Underground)

Percent Change	Surface Zinc Grade (%)	Surface Lead Grade (%)	$NPV_{8\%}$	IRR
-20%	2.64%	1.04%	$ 43,960,000	54%
-15%	2.81%	1.11%	$ 51,620,000	60%
-10%	2.97%	1.17%	$ 58,470,000	66%
-5%	3.14%	1.24%	$ 66,850,000	71%
0%	3.30%	1.30%	$ 73,630,000	76%
5%	3.47%	1.37%	$ 81,550,000	82%
10%	3.63%	1.43%	$ 89,180,000	86%
15%	3.80%	1.50%	$ 96,780,000	91%
20%	3.96%	1.56%	$ 103,960,000	96%

Parameter: Initial Capital Costs

Percent Change	Capital Cost	$NPV_{8\%}$	IRR
-20%	$ 2,345,000	$ 74,560,000	79%
-15%	$ 2,491,000	$ 74,330,000	78%
-10%	$ 2,638,000	$ 74,100,000	78%
-5%	$ 2,784,000	$ 73,860,000	77%
0%	$ 2,931,000	$ 73,630,000	76%
5%	$ 3,078,000	$ 73,390,000	76%
10%	$ 3,224,000	$ 73,160,000	75%
15%	$ 3,371,000	$ 72,930,000	74%
20%	$ 3,517,000	$ 72,690,000	74%

Parameter: Operating Costs
Base Case Value (Year 2): $ 18,128,000

Percent Change	Operating Cost	$NPV_{8\%}$	IRR
-20%	$ 14,500,000	$ 86,290,000	86%
-15%	$ 15,400,000	$ 83,150,000	83%
-10%	$ 16,300,000	$ 79,980,000	81%
-5%	$ 17,200,000	$ 76,800,000	79%
0%	$ 18,100,000	$ 73,630,000	76%
5%	$ 19,000,000	$ 70,450,000	74%
10%	$ 19,900,000	$ 67,270,000	71%
15%	$ 20,800,000	$ 64,090,000	69%
20%	$ 21,800,000	$ 60,880,000	66%

Parameter: Exchange Rate
Base Case Value: $ 0.86

Percent Change	Exchange Rate	$NPV_{8\%}$	IRR
-20%	$ 0.69	$ 111,120,000	100%
-15%	$ 0.73	$ 100,580,000	94%
-10%	$ 0.77	$ 90,500,000	87%
-5%	$ 0.82	$ 81,580,000	82%
0%	$ 0.86	$ 73,630,000	76%
5%	$ 0.90	$ 66,660,000	72%
10%	$ 0.95	$ 60,460,000	67%
15%	$ 0.99	$ 54,820,000	63%
20%	$ 1.03	$ 49,450,000	59%

The sensitivity of the project's profitability to changes in metal prices, expressed in even, ten-cent steps in zinc price, is given in Table 45.

Table 45: Sensitivity of the project's profitability to changes in metal prices.

Percent Change	Zinc Price ($US per lb)	Lead Price ($US per lb)	$NPV_{8\%}$	IRR
-45.5%	$ 0.60	$ 0.22	-$ 18,740,000	Undefined
-36.0%	$ 0.70	$ 0.26	$ 3,690,000	14%
-27.0%	$ 0.80	$ 0.29	$ 22,080,000	35%
-18.0%	$ 0.90	$ 0.33	$ 40,090,000	51%
-9.0%	$ 1.00	$ 0.36	$ 56,430,000	64%
0.0%	$ 1.10	$ 0.40	$ 73,630,000	76%
9.0%	$ 1.20	$ 0.44	$ 90,830,000	88%
18.0%	$ 1.30	$ 0.47	$ 106,930,000	98%
27.0%	$ 1.40	$ 0.51	$ 124,050,000	108%
36.0%	$ 1.50	$ 0.54	$ 140,480,000	117%

At the time of report writing, prices for zinc and lead were experiencing historic high values of $US 1.63 and $0.53 per pound, respectively. The exchange rate was approximately

$0.89 (US dollars per Canadian dollar). Using slightly more conservative zinc and lead prices of $US 1.50 and $0.45 per pound, an exchange rate of $0.89 and maintaining the other parameters at their base case values (Table 34), the project's net present value and internal rate of return were:

Metal Prices ($US per pound):	
Zinc	$1.50
Lead	$0.45
Exchange Rate	$0.89
$NPV_{7.5\%}$	$ 130,500,000
$NPV_{8.0\%}$	$ 127,200,000
$NPV_{10.0\%}$	$ 115,000,000
$NPV_{12.5\%}$	$ 101,700,000
$NPV_{15.0\%}$	$ 90,300,000
Internal Rate of Return (IRR)	110%

19.19 Discussion of Risks

For both the surface and underground operations, the greatest risk for project profitability is metal price fluctuation. At the time of report writing, zinc and lead prices were at historical highs. For example, the zinc price increased more than three-fold since 2002. Some analysts believe that the zinc price will remain stable and high through 2006 and 2007, then start to decrease. They disagree on when it will start to decrease and by how much. There is the possibility of the zinc price decreasing to $US 0.50-0.60 per pound by 2010. Other analysts are more bullish regarding metal prices, believing that world demand will outpace supply. Whichever view is correct, the best methods for controlling this risk are mining as quickly as possible and selling a portion of production forward (hedging) while prices are high.

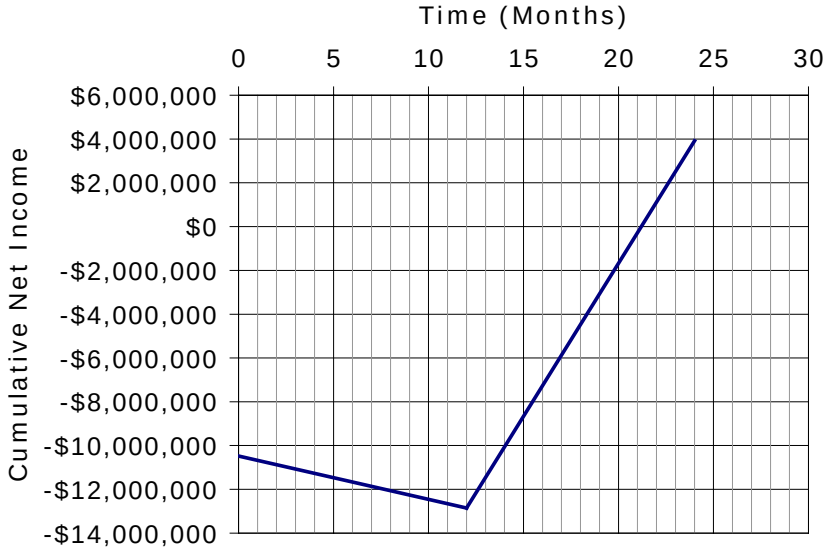
Water inflow to the underground workings provides a less quantifiable, technical risk to the underground portion of the project. Because of the past history of water inflow problems, a "worse case" mine plan has already been adopted. The modified undercut-and-fill mining method that has been adopted for this deposit was designed for very poor ground conditions and offers a high level of protection against potentially unstable ground. Other measures, such as lowering the groundwater table below the level of the mine workings, will also be taken to further alleviate the risk. Because the underground portion of the project begins so far in the future (Year 8), major changes in the underground mining costs and revenue have only a minor effect on the project's net present value.

19.20 Payback Period

The payback period for the project, according to cumulative net income after interest and taxes, is twenty-one months (Figure 42).

Figure 42: Project payback period according to cumulative net income after interest and taxes.

	Month 0	Month 12	Month 24
Cumulative Net Income	-$ 10,481,000	-$ 12,856,000	$ 3,920,000



19.21 Mine Life

The surface operation will last almost six years. The underground operation will last more than two years for a total mine life of just over eight years.

The best possibility for extending the mine life lies with the Getty Deposit. Based on a 1.5 % zinc-equivalent cut-off grade (1 % Pb = 0.6 % Zn in 1975 using a minimum core length of three metres), resources at the Getty deposit were reported by Hudgins and Lamb (1992) to be 4.5 million tons at an average grade of 1.3 % Pb and 1.9 % Zn.[8]

There are also In-pit Inferred Resources that could potentially extend the surface mine life. The diluted and recoverable In-pit Inferred Resources amounted to 510,000 tonnes containing 2.2 % zinc and 1.1 % lead. The reader should note that there is no guarantee that any of this material can be profitably mined. Grade control sampling during surface mining operations will identify which part(s), if any, of this material could be profitably mined and processed.

[8] The resource estimates referred to in this section are historical in nature and are quoted as such. These estimates have not been reviewed by the authors of this report and thus should not be relied upon.

20. Conclusions

Using a combination of surface and underground mining methods, the overall mine life is just over eight years.

The project's capital cost is $2.9 million. The surface mobile equipment fleet will be leased. The purchase price for ScoZinc Limited is $7.5 million and purchasing Savage's 2 % NSR royalty will cost $1.45 million, for a total initial capital cost of $11.85 million. The capital cost for the underground operation, starting in Year 6, is $5.6 million. The initial working capital requirement, including contingency is $11.1 million.

Operating the surface mine and processing plant is expected to cost $19 million per year ($27 per tonne of ore or $US 0.34 per pound of zinc-equivalent). Operating the underground mine and processing plant is expected to cost $23 million per year ($49 per tonne of ore or $US 0.30 per pound of zinc-equivalent).

Net yearly revenue (after smelting costs) during the surface mining operation will be $43 million. For the underground operation, yearly revenue will be $60 million.

For the base case scenario ($US 1.10 per pound zinc, $US 0.45 per pound lead, $US 0.86 exchange rate), the project's after-tax, net present value using a 8 % discount rate ($NPV_{8\%}$) was $73.6 million. The internal rate of return was 76 %. The payback period was twenty-one months.

Profitability is most sensitive to changes in metal prices, grade, dilution and exchange rate. It is less sensitive to changes in operating costs and relatively insensitive to changes in initial capital costs.

The greatest risk for project profitability is metal price fluctuation. Water inflow to the underground workings provides a less quantifiable, technical risk to the underground portion of the project.

21. Recommendations

The technical and economic analysis indicates that the project will be very profitable.

Because the project's profitability is most sensitive to metal prices, production must begin as soon as possible while metal prices remain high.

The Getty Deposit's Resources should be estimated. A feasibility study should also be carried out to determine if the Getty Deposit has any Reserves. This work should cost $30,000-40,000.

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Certificate of Principal Author

I, William Douglas Roy, M.A.Sc., P.Eng., do hereby certify that:

1) I am currently employed by MineTech International Limited, with an office at 1152 Cartaret St, Halifax, Canada.
2) I graduated with a B.Eng. degree in Mining Engineering from the Technical University of Nova Scotia (now Dalhousie University) in 1997 and with a M.A.Sc. degree in Mining Engineering from Dalhousie University in 2000.
3) I am a Professional Engineer (Mining), registered with the Association of Professional Engineers of Nova Scotia (Registered Professional Engineer, No. 7472) and the Association of Professional Engineers and Geoscientists of Saskatchewan (Registered Professional Engineer, No. 13175).
4) I have worked as a mining engineer for nine years since graduating from university. This work has included the estimation of resources and reserves for precious metals, base metals and industrial minerals, as well as participation in pre-feasibility and feasibility studies.
5) I have read the definition of "qualified person" set out in National Instrument 43-101 ("NI 43- 101") and certify that by reason of my education, affiliation with a professional association (as defined in NI 43-101) and past relevant work experience, I fulfil the requirements to be a "qualified person" for the purposes of NI 43-101.
6) I was the Principal Author of the report titled "Acadian Gold Corp, Resource, Reserve and Feasibility Report for the Purchase and Operation of Scotia Mine, Gays River, Nova Scotia, Canada," dated July 13, 2006. Specifically, I carried out the mine feasibility work that led to the Reserve calculation. I calculated the "Northeast Underground Reserves" and authored the portions of the report pertaining to the feasibility work. As the Principal Author of the report, I directed and reviewed work that was carried out by the other authors.
7) I have read NI 43-101 and Form 43-101F1. This Technical Report has been prepared in accordance with that Instrument and Form.
8) I visited the property many times in 2004 and 2005 when, as an independent contractor, I supervised exploration work including diamond drilling and trenching. I last visited the property on February 21, 2006.
9) I have had prior involvement with ScoZinc Limited and the property that is the subject of the Technical Report. During 2004 and 2005, as an independent contractor, I supervised exploration work including diamond drilling and trenching.
10) I am not aware of any material fact or material change with respect to the subject matter of the Technical Report that is not reflected in the Technical Report, the omission to disclose which makes the Technical Report misleading.
11) I am independent of the issuer applying all of the tests in Section 1.4 of NI 43-101.
12) I consent to the filing of the Technical Report with any stock exchange and other regulatory authority and any publication by them, including electronic publication in the public company files on their websites accessible by the public.
13) As of the date of this certificate, to the best of my knowledge, information and belief, the Technical Report contains all scientific and technical information that is required to be disclosed to make the report not misleading.

Dated this 13th Day of July, 2006.
William Douglas Roy, M.A.Sc., P. Eng.
Consultant Mining Engineer
MineTech International Limited

Co-Author's Certificate – Tim Carew

I, Timothy J Carew, do hereby certify that:

1. I reside at 12955 Fieldcreek Lane, Reno, NV 89511, USA.

2. I am a graduate from the University of Rhodesia with a B.Sc. (Hons) Degree in Geology (1970), and of the University of London (RSM - 1982), with a M.Sc. Mineral Production Management degree, and I have practiced my profession continuously since that time.

3. I am a member of the Association of Professional Geoscientists and Engineers of British Columbia (Membership Number 19706).

4. I am a consulting geoscientist and the Principal of Reserva International LLC., a company incorporated in Nevada, USA.

5. I have read the definition of "qualified person" set out in National Instrument 43-101 ("NI 43-101") and certify by reason of my education, affiliation with professional association (as defined in NI 43-101), and past relevant work experience, I fulfill the requirements to be a "Qualified Person" for purposes of NI 43-101.

6. I was responsible for surface resource and pit optimization sections (Section 17.1 and 18.1) of the report entitled "Acadian Gold Corp - Resource, Reserve and Feasibility Report for the Purchase and Operation of Scotia Mine, Gays River, Nova Scotia, Canada" dated July 13, 2006 (the "Technical Report").

7. I am personally familiar with the characteristics of the deposit in the Technical Report from previous work on the deposit. I last visited the deposit in 1998 while estimating the resources for Savage Resources Canada.

8. As of the date of this certificate, to the best of my knowledge, information and belief, the Technical Report contains all scientific and technical information that is required to be disclosed to make the report not misleading.

9. I have read NI 43-101 and Form 43-101F1 and have prepared this report in compliance with NI 43-101 and Form 43-101F1, and have prepared the above mentioned sections of the report in conformity with generally accepted Canadian mining industry practice.

10. I consent to the filing of this report with any stock exchange and other regulatory authority and any publication by them, including electronic publication in the public company files on their websites accessible by the public.

11. I am independent of the issuer applying all the tests in Section 1.4 of NI 43-101.

Signed by

Timothy J. Carew, P.Geo., B.Sc., M.Sc.
Dated this 13th Day of July, 2006.

Co-Author's Certificate - R. L. Comeau

I, R. L. Comeau, M.Sc., P.Geo., do hereby certify that:

1. I am currently employed as a Associate Consulting Geologist by:

   A.C.A. Howe International Limited
   Suite 830, 330 Bay Street
   Toronto, Ontario
   Canada M5H 2S6

2. I graduated with a Bachelor of Science degree in Geology from Dalhousie University in Halifax, Nova Scotia in 1968. In addition, I obtained a Master of Science (M.Sc.) in Geology in 1972 from Memorial University of Newfoundland, St. John's, Newfoundland.

3. I am a Professional Geoscientist (P.Geo.) registered with the Association of Professional Geoscientists and Engineers of Saskatchewan (APEGS: #10472). I am also a Professional Geoscientist registered with the APGO in Ontario (#679) and a member of the Prospectors and Developers Association of Canada, the Mining Society of Nova Scotia and through that affiliation a member or the Canadian Institute of Mining and Metallurgy.

4. I have worked as a geologist for a total of 32 years since graduation from Memorial University.

5. I have read the definition of "qualified person" set out in National Instrument 43-101 ("NI 43-101") and certify by reason of my education, affiliation with professional association, and past relevant work experience, I fulfil the requirements to be a "qualified person" for purposes of NI 43-101.

6. I have been directly involved in numerous base metal exploration projects including exploration and evaluation of Mississippi Valley Type deposits, both in eastern Canada as well as the United Sates of America since 1972.

7. I am familiar with the ScoZinc (formerly Gays River) Zn-Pb deposit as, in 1973 - 1974, I was responsible for the diamond drilling activity on what is now referred to as the "Getty Deposit", which forms part of the present day deposit and located on the contiguous ground northwest and adjoining the ScoZinc land package. Most recently, site visits were made and core samples taken from the ScoZinc deposit, for verification purposes, on June 17, June 21, September 22 and September 26, 2004.

8. I am the author of he script forming Sections 5.1, 6.0, 7.0, 8.0, 9.0, 10.0, 12.0, 13.0, 14.0, 14.2 and 15.0 of the report entitled "Acadian Gold Corp - Resource, Reserve and Feasibility Report for the Purchase and Operation of Scotia Mine, Gays River, Nova Scotia, Canada" dated July 13, 2006 and authored by Douglas Roy, M.A.Sc., P.Eng., Tim Carew, P.Geo., and Reg Comeau, P.Geo. (the "Technical Report").

9. As of the date of this Certificate, to the best of my knowledge, information and belief, the Technical Report contains all scientific and technical information that is required to be disclosed to make the report not misleading.

10. I am independent of the issuer applying all of the tests in Section 1.4 of National Instrument 43-101.

11. I have read National Instrument 43-101 and Form 43-101F1, and the Technical Report has been prepared in compliance with that instrument and form.

12. This report has been prepared in conformity with generally accepted Canadian mining industry practice and standards.

13. I consent to the filing of this report with any stock exchange and other regulatory authority and any publication by them, including electronic publication in the public company files on their websites accessible by the public.

R. L. Comeau, M.Sc., P. Geo
Dated this 13th Day of July, 2006.

Appendix 1: Westminer monthly mill report for November, 1990.

GAYS RIVER MILL PRODUCTION FOR 30-Nov-90

	MONTH			Y.T.D.	
	DAY	ACTUAL	BUDGET	ACTUAL	BUDGET
TONNES MILLED(DMT)	734	13,499	17,360	68,794	80,960
MOISTURE (%)	4.54	3.56		3.08	
HEAD GRADE(%Pb)	5.20	3.08	5.15	3.10	5.20
(%ZN)	9.82	7.45	8.11	7.48	9.14
OPERATING TIME(HR)	21.5	390.2	476.8	1,911.3	2,394.0
SCHEDULED TIME(HR)	24.0	504.0	504.0	2,568.0	2,520.0
AVAILABILITY (%)	89.6	77.4	95.0	74.4	95.0
MILLING RATE(DT/HR)	34.1	34.6	36.3	36.0	33.8
RECOVERY					
Pb TO Pb CONC(%)	90.5	92.0	94.0	93.0	96.0
Zn TO Pb CONC(%)	2.8	2.4	3.7	2.1	3.3
Pb TO Zn CONC(%)	3.1	1.9	1.0	2.0	1.0
Zn TO Zn CONC(%)	91.5	89.0	91.0	89.7	91.0
TONNES TO TAILS(DMT)	580	11,523	14,134	58,768	64,641
TAIL GRADE(%Pb)	0.42	0.22	0.19	0.18	0.20
(%Zn)	0.70	0.76	0.53	0.72	0.65
CONCENTRATE PROD.					
LEAD CONC (DMT)	44.63	506.47	1159.84	2588.42	5462.89
GRADE(%Pb)	77.39	75.62	74.00	76.52	74.00
GRADE(%Zn)	4.60	4.71	4.50	4.11	4.50
GRADE(Ag gm/MT)	13.70	22.10	35.00	25.59 [2]	35.00
ZINC CONC (DMT)	109.52	1469.53	2066.43	7437.81	10856.28
GRADE(%Zn)	60.21	60.86	62.00	62.09	62.00
GRADE(%Pb)	1.08	0.53	0.43	0.57	0.39
GRADE(%Cd)	0.28	0.29	0.30	0.30 [3]	0.30
GRADE(%Mg)	0.75	0.74	0.40	0.51	0.40

COMMENTS:

VARIATIONS IN MILL FEED: Pb 7.19% TO 3.8%(STEADY DROP ALL DAY).
Zn 11.22% TO 8.03%(STEADY DROP ALL DAY).

SCHEDULED SHUTDOWN AT 5:30 AM.

[2] Y-T-D Silver Since Sept 1/90
[3] Y-T-D Cadmium Since Oct 1/90

Appendix 2: Mineral lease and exploration licence claims and ownership history

NOVA SCOTIA
Natural Resources

PO Box 698
Halifax, Nova Scotia
B3J 2T9

902 424-7735 F
www.gov.ns.ca
73300-28/.05

By FAX : 902-425-6350

February 17, 2006

Ms. Barbara (Basia) H. Dzieranowska
McInnes Cooper Barristers & Solicitors
P.O. Box 730
Halifax, NS B3J 2V1

Dear Ms. Dzieranowska:

Re: Search of Title - Scozinc Limited

Mining Lease No. 90-1

Please accept this letter as confirmation that Registry records indicate that Mining Lease No. 90-1 is in good standing and issued to Scozinc Limited as at today's date. Specifically, Mining Lease No. 90-1 consists of the following thirty-eight (38) claims:

LEASE NUMBER	CLAIMS	TRACT	CLAIM REFERENCE MAP	ANNIVERSARY DATE
90-1	NOP	5	11E3B	Apr. 2/06
	JKPQ	19	11E3B	
	BCDE FGK	20	11E3B	
	LMNO PQ			
	DEKL MNOP	28	11E3B	
	ABCD FGH JKQ	29	11E3B	

The following table outlines the chronology of title which resulted in the issuance of Lease No. 90-1. The beginning of title begins at the bottom of the table with the issuance of five (5) Prospector Licences. Only the claims that are currently held under lease 90-1 are listed.

Licence/ Lease Number	Claims	Tract	Claim Reference Map	Licensee	Date	Comments
L 90-1	NOP JKPQ BCDE FGK LMNO PQ DEKL MNOP ABCD FGH JKQ	5 19 20 28 29	11E3B 11E3B 11E3B 11E3B 11E3B	Scozinc Limited	Nov. 13, 2002	November 13, 2002 receipt of the Certificate of Name Change, dated November 5, 2002, confirming the name change from Pasminco Resources Canada Ltd. to Scozinc Limited. (Certificate of Name Change - RJSC Registry No. 3064626.)
				Pasminco Resources Canada Ltd.	March 20, 2002	March 20, 2002 receipt of Certificate of Amendment, dated March 4, 2002, confirming the name change from Pasminco Resources Canada Company to Pasminco Resources Canada Ltd. (Certificate of Amendment - RJSC Registry Number 3064626.)
				Pasminco Resources Canada Company	March 28, 2000	March 28, 2000 receipt of Certificate of Name Change, dated October 29, 1999, confirming the name change from Savage Resources Canada Company to Pasminco Canada Company. (Certificate of Name Change - RJSC Registry No. 3002877.)
				Savage Resources Canada Company	Dec. 23, 1996	Transfer of Lease No. 90-1 from WMC International Limited to Savage Resources Canada Company. (Transfer No. 4792 registered Dec. 23, 1996.)
				WMC International Limited	July 18, 1994	Receipt of notice of name change from Westminer Canada Limited to WMC International Limited.
				Westminer Canada Limited	Apr 2, 1990	Lease issued effective April 2, 1990. Issuance authorized by Order in Council No. 90-483.

Licence/ Lease Number	Claims	Tract	Claim Reference Map	Licensee	Date	Comments
DL 0092	NOP JKPQ	5 19	11E3B 11E3B	Seabright Resources Inc.	Sept. 25, 1985	Transfer of Development Licence Nos. 0092 & 0091 from Esso Resources Canada Limited to Seabright Resources Inc. (Transfer No. 4372 registered Sept. 25, 1985).
DL 0091	BCDE FGK LMNO PQ DEKL MNOP ABCD FGH JKQ	20 28 29	11E3B 11E3B 11E3B	Esso Resources Canada Limited	July 4, 1982	Development Licence Nos. 0092 & 0091 issued to Esso Resources Canada Limited effective July 4, 1982 to replace Mining Lease 78-3 which was surrender effective July 3, 1982.
L 78-3	NOP JKPQ BCDE FGK LMNO PQ DEKL MNOP ABCD FGH JKQ	5 19 20 28 29	11E3B 11E3B 11E3B 11E3B 11E3B		July 3, 1982	Lease No. 78-3 surrendered July 3, 1982.
				Esso Resources Canada Limited	Feb. 14, 1979	Transfer of Lease No. 78-3 from Imperial Oil Limited to Esso Resources Canada Limited (Transfer No. 4032 registered February 14, 1979).
				Imperial Oil Limited	July 4, 1978	Lease 78-3 issued effective July 4, 1978 as the result of the consolidation of Lease Nos. 78-1 & 78-2.
L 78-2	DEKL MNOP ABGH JKQ	28 29	11E3B 11E3B	Imperial Oil Limited	July 4, 1978	Lease Nos. 78-2 & 78-1 consolidated and recorded as Lease No. 78-3.
L 78-1	NOP JKPQ BCDE FGK LMNO PQ CDF	5 19 20 29	11E3B 11E3B 11E3B 11E3B			Lease Nos. 78-2 & 78-1 issued effective July 4, 1978.

Licence/ Lease Number	Claims	Tract	Claim Reference Map	Licensee	Date	Comments
DL 0039	DEKL MNOP ABGH JKQ	28 29	11E3B 11E3B	Imperial Oil Limited	Dec. 21, 1977	Transfer of *"all the right title and interest in and to"* Development Licence Nos 0039 & 0040 from Preuvier Mines Ltd. to Imperial Oil Limited. (Transfer No. 3972 registered December 21, 1977).
DL 0040	CDF NOP JKPQ BCDE FGK LMNO PQ	29 5 19 20	11E3B 11E3B 11E3B 11E3B	Imperial Oil Limited - Preuvier Mines Ltd.	July 4, 1977	Development Licence Nos. 0039 & 0040 issued to Imperial Oil Limited & Preuvier Mines Ltd. effective July 4, 1977.
EL 0052	DEKL MNOP ABCD FGH JKQ	28 29	11E3B 11E3B	Imperial Oil Limited - Preuvier Mines Ltd.	Jan 20, 1977	Transfer of Exploration Licence No. 0052 from Cuvier Mines Ltd. to Imperial Oil Limited (60% undivided interest) & Preuvier Mines Limited (40% undivided interest) by means of Transfer No. 3930 which was registered on January 20, 1977.
				Cuvier Mines Ltd.	July 2, 1975	Licence issued in its 4th year of issue to Cuvier Mines Ltd. effective July 2, 1975.

Licence/ Lease Number	Claims	Tract	Claim Reference Map	Licensee	Date	Comments
EL 0122	NOP JKPQ BCDE FGK LMNO PQ	5 19 20	11E3B 11E3B 11E3B	Imperial Oil Limited - Preuvier Mines Ltd.	Jan 20, 1977	Transfer of Exploration Licence No. 0122 from Cuvier Mines Ltd. to Imperial Oil Limited (60% undivided interest) & Preuvier Mines Limited (40% undivided interest) by means of Transfer No. 3930 which was registered on January 20, 1977.
				Cuvier Mines Ltd.	July 24, 1975	Licence issued in its 4th year of issue to Cuvier Mines Ltd. effective July 24, 1975.
New Mineral Resources Act in force June 1, 1975						
PL 4061	BCDE FGK LMNO PQ	20	11E3B	Cuvier Mines Ltd.	July 24, 1974	Prospector Licence Nos. 4061, 4058 & 4060 issued to Cuvier Mines Ltd. effective July 24, 1974.
PL 4058	NOP	5	11E3B			
PL 4060	JKPQ	19	11E3B			
PL 3190	ABCD FGH JKQ	29	11E3B	Cuvier Mines Ltd.	May 22, 1974	Prospector Licence Nos. 3190 & 3191 issued to Cuvier Mines Ltd. effective May 22, 1974.
PL 3191	DEKL MNOP	28	11E3B			
PL 10161	BCDE FGK LMNO PQ	20	11E3B	Cuvier Mines Ltd	July 24, 1973	Prospector Licence Nos. 10161, 10158 & 10160 issued to Cuvier Mines Ltd. effective July 24, 1973.
PL 10158	NOP	5	11E3B			
PL 10160	JKPQ	19	11E3B			
PL 9112	ABCD FGH JKQ	29	11E3B	Cuvier Mines Ltd	May 22, 1973	Prospector Licence Nos. 9122 & 9113 issued to Cuvier Mines Ltd. effective May 22, 1973.
PL 9113	DEKL MNOP	28	11E3B			

Licence/ Lease Number	Claims	Tract	Claim Reference Map	Licensee	Date	Comments
PL 6573	BCDE FGK LMNO PQ	20	11E3B	Cuvier Mines Ltd		Transfer of Prospector Licence Nos. 6573, 6566 & 6574 from J. H. Morgan to Cuvier Mines Ltd. (Transfer No. 3649).
PL 6566	NOP	5	11E3B			
PL 6574	JKPQ	19	11E3B	J. H. Morgan	July 24, 1972	Prospector Licence Nos. 6573, 6566 & 6574 issued to J. H. Morgan effective July 24, 1972.
PL 6044	ABCD FGH JKQ	29	11E3B	Cuvier Mines Ltd.		Transfer of Prospector Licence Nos. 6044 & 6043 from Avard Hudgins to Cuvier Mines Ltd. (Transfer No. 3641).
PL 6043	DEKL MNOP	28	11E3B	Avard Hudgins	May 13, 1972	Prospector Licence Nos. 6044 & 6043 issued to Avard Hudgins effective May 13, 1972.

EL - Exploration Licence
DL - Development Licence
PL - Prospector Licence
L - Lease

RJSC - Registry of Joint Stock Companies

A review of the Registry Agreement Ledger for documents recorded on Mining Lease No. 90-1 and prior mineral titles, as outlined in the above chronology, and in the name of the current and previous title holders, indicates that the following documents have been recorded as agreements:

Agreement Number	Date	Parties to the Agreement	Comments
788	May 29, 1973 *(Date Received)*	Cuvier Mines Limited Lura Corporation Imperial Oil Limited	Agreement dated 1st November 1972
792	June 26, 1973 *(Date of Letter)*	Imperial Oil Limited	Letter of Incorporation

Agreement Number	Date	Parties to the Agreement	Comments
793	May 29, 1973 *(Date Received)*	Cuvier Mines Limited Lura Corporation Imperial Oil Limited	Agreement dated 1st November 1972
846	Feb 1, 1976 *(Agreement Date)*	Cuvier Mines Ltd. Preussag Canada Limited	
847	Feb 1, 1976 *(Agreement Date)*	R.P. Mills J.H. Morgan Preussag Canada Limited	Financing Agreement
848	Feb 1, 1976 *(Agreement Date)*	Cuvier Mines Ltd. Preussag Canada Limited	Preuvier Shareholders Agreement
849	Feb 1, 1976 *(Agreement Date)*	Cuvier Mines Ltd. Preuvier Mines Limited	
850	Feb 1, 1976 *(Agreement Date)*	Cuvier Mines Ltd. Preussag Canada Limited	Joint Venture Agreement
860	Dec 15, 1976 (Date Registered)	Preuvier Mines Limited Montreal Trust Company	Agreement dated March 15, 1976 Trust Indenture
883	Nov 15, 1977 *(Date Registered)*	Cuvier Mines Ltd. Preuvier Mines Limited Imperial Oil Limited	Agreement dated Sept 30, 1977
884	Nov 15, 1977 *(Date Registered)*	Cuvier Mines Ltd. Preuvier Mines Limited Preussag Canada Limited	Agreement dated Sept 30, 1977
885	*Dec 15, 1977 (Date Registered)*	Preuvier Mines Limited Montreal Trust Company	Release of Trust Indenture
892	Feb 1, 1978 *(Date of Letter)*	Esso Minerals Division of Imperial Oil Limited	Gays River Project
1279	Aug 3, 1982 *(Date of Agreement)*	Mosher Limestone Company Limited Esso Resources Canada Limited	
A0191	Oct 19, 2001 *(Date Registered)*	Pasminco Resources Canada Company Regal Consolidated Ventures Limited	Agreement dated Sep 20, 2001

The above review of the Registry's Agreement Index also included the following two (2) agreements that referenced a former title holder. No reference to a mineral right could be determined as at the time of the search.

Agreement Number	Parties to the Agreement	Comments
1277	Seabright Resources Inc.	Agreements & Letters of Intent
1320	Seabright Resources Inc. Tri-Explorations Inc.	

Exploration Licence No. 06268

Registry records indicate that Exploration Licence No. 06268 is in good standing and issued to Scozinc Limited as at today's date. Specifically, Exploration Licence No. 06268 consists of the following twenty-eight (28) claims:

LICENCE NUMBER	CLAIMS	TRACT	CLAIM REFERENCE MAP	ANNIVERSARY DATE
06268	ABCD EFGH LMN ABC EFGH DE JKLM NOPQ	19 18 7	11E3B 11E3B 11E3B	May 2/06

The following table outlines the chronology of title which resulted in the issuance of 06268. The beginning of title starts at the bottom of the table with the issuance of four (4) Exploration Licences. Only the claims that are currently held under exploration licence no. 06268 are listed.

Licence Number	Claims	Tract	Claim Reference Map	Licensee	Date	Comments
06268	ABCD EFGH LMN ABC EFGH DE JKLM NOPQ	19 18 7	11E3B 11E3B 11E3B	Scozinc Limited	May 2, 2005	Exploration Licence No. 06268 issued in its 9th year of issue to Scozinc Limited effective May 2, 2005. Exploration Licence No 06268 replaced Exploration Licence No. 06166.

Licence Number	Claims	Tract	Claim Reference Map	Licensee	Date	Comments
06166	ABCD EFGH LMN ABC EFGH DE JKLM NOPQ	19 18 7	11E3B 11E3B 11E3B	Scozinc Limited	May 2, 2004	Exploration Licence No. 06166 issued in its 8th year of issue to Scozinc Limited effective May 2, 2005. Exploration Licence No. 06166 was issued as the result of the regrouping of Exploration Licence Nos. 04727, 02684, 04460 & 06165.
04727	DE JKLM NOPQ ABC EFGH	7 18	11E3B 11E3B	Scozinc Limited	Sept 28, 2004	Exploration Licence No. 04727 transferred from Alex C. Thomson to Scozinc Limited. Transfer No. 4926 registered September 28, 2004.
				Alex C. Thomson	Oct 25, 2001	Exploration Licence No. 04727 issued to Alex C. Thomson effective October 25, 2001.

Licence Number	Claims	Tract	Claim Reference Map	Licensee	Date	Comments
02684	AB FGH	19	11E3B	Scozinc Limited	Nov. 13, 2002	November 13, 2002 receipt of the Certificate of Name Change, dated November 5, 2002, confirming the name change from Pasminco Resources Canada Ltd. to Scozinc Limited. (Certificate of Name Change - RJSC Registry No. 3064626.)
				Pasminco Resources Canada Ltd.	March 20, 2002	March 20, 2002 receipt of Certificate of Amendment, dated March 4, 2002, confirming the name change from Pasminco Resources Canada Company to Pasminco Resources Canada Ltd. (Certificate of Amendment - RJSC Registry Number 3064626.)
				Pasminco Resources Canada Company	March 28, 2000	March 28, 2000 receipt of Certificate of Name Change, dated October 29, 1999, confirming the name change from Savage Resources Canada Company to Pasminco Canada Company. (Certificate of Name Change - RJSC Registry No. 3002877.)
				Savage Resources Canada Company	Nov 11, 1999	Exploration Licence No. 04727 transferred from Michael P. Cullen to Savage Resources Canada Company. Transfer No. 4855 registered November 1, 1999.
				Michael P. Cullen	Nov 5, 1996	Exploration Licence No. 02684 issued to Michael P. Cullen effective November 5, 1996.

Licence Number	Claims	Tract	Claim Reference Map	Licensee	Date	Comments
04460	CDE	19	11E3B	Scozinc Limited	Sept 28, 2004	Exploration Licence No. 04460 transferred from Alex C. Thomson to Scozinc Limited. Transfer No. 4926 registered September 28, 2004.
				Alex C. Thomson	Nov. 10, 2000	Exploration Licence No. 04460 issued to Alex C. Thomson effective November 10, 2000.
06165	LMN	19	11E3B	Scozinc Limited	Sept 28, 2004	Exploration Licence No. 06165 issued to Scozinc Limited effective Sept 28, 2004.

Exploration Licence No. 06304

Registry records indicate that Exploration Licence No. 06304 is in good standing and issued to Scozinc Limited as at today's date. Specifically, Exploration Licence No. 06304 consists of the following one (1) claim:

LICENCE NUMBER	CLAIMS	TRACT	CLAIM REFERENCE MAP	ANNIVERSARY DATE
06304	E	29	11E3B	Oct 13/06

The following table outlines the chronology of title which resulted in the issuance of 06304. The beginning of title starts at the bottom of the table with the issuance of Exploration Licence No. 05743.

Licence Number	Claims	Tract	Claim Reference Map	Licensee	Date	Comments
06304	E	29	11E3B	Scozinc Limited	Oct 13, 2005	Exploration Licence No. 06304 issued in its 2nd year of issue to Scozinc Limited effective Oct 13 2, 2005. Exploration Licence No 06304 replaced Exploration Licence No. 05743.
05743	E	29	11E3B	Scozinc Limited	Oct 13, 2004	Exploration Licence No. 05743 issued to Scozinc Limited effective Oct 13 2, 2004.

Exploration Licence No. 06303

Registry records indicate that Exploration Licence No. 06303 is in good standing and issued to Scozinc Limited as at today's date. Specifically, Exploration Licence No. 06303 consists of the following five (5) claim:

LICENCE NUMBER	CLAIMS	TRACT	CLAIM REFERENCE MAP	ANNIVERSARY DATE
06303	LMNOP	29	11E3B	Oct 25/06

The following table outlines the chronology of title which resulted in the issuance of 06303. The beginning of title starts at the bottom of the table with the issuance of Exploration Licence No. 04728.

Licence Number	Claims	Tract	Claim Reference Map	Licensee	Date	Comments
06303	LMNOP	29	11E3B	Scozinc Limited	Oct 25, 2005	Exploration Licence No. 06303 issued in its 5th year of issue to Scozinc Limited effective Oct 25 2, 2005. Exploration Licence No 06303 replaced Exploration Licence No. 04728.
04728	LMNOP	29	11E3B	Scozinc Limited	Sept 28, 2004	Exploration Licence No. 04728 transferred from Alex C. Thomson to Scozinc Limited. Transfer No. 4926 registered September 28, 2004.
				Alex C. Thomson	Oct 25, 2001	Exploration Licence No. 04728 issued to Alex C. Thomson effective Oct 25, 2001.

Exploration Licence No. 05851

Registry records indicate that Exploration Licence No. 05851 is in good standing and issued to Scozinc Limited as at today's date. Specifically, Exploration Licence No. 05851 consists of the following fifteen (15) claims:

LICENCE NUMBER	CLAIMS	TRACT	CLAIM REFERENCE MAP	ANNIVERSARY DATE
05851	FGH JKL OPQ EFG KLM	45 46	11E3B 11E3B	Nov 5/06

The following table outlines the chronology of title which resulted in the issuance of 05851. The beginning of title starts at the bottom of the table with the issuance of Exploration Licence No. 02689.

Licence Number	Claims	Tract	Claim Reference Map	Licensee	Date	Comments
05851	FGH JKL OPQ EFG KLM	45 46	11E3B 11E3B	Scozinc Limited	Nov 5, 2004	Exploration Licence No. 05851 issued in its 10th year of issue to Scozinc Limited effective Nov 5 , 2004. Exploration Licence No 05851 replaced Exploration Licence No. 02689.

Licence Number	Claims	Tract	Claim Reference Map	Licensee	Date	Comments
02689	FGH JKL OPQ EFG KLM	45 46	11E3B 11E3B	Scozinc Limited	Nov. 13, 2002	November 13, 2002 receipt of the Certificate of Name Change, dated November 5, 2002, confirming the name change from Pasminco Resources Canada Ltd. to Scozinc Limited. (Certificate of Name Change - RJSC Registry No. 3064626.)
				Pasminco Resources Canada Ltd.	March 20, 2002	March 20, 2002 receipt of Certificate of Amendment, dated March 4, 2002, confirming the name change from Pasminco Resources Canada Company to Pasminco Resources Canada Ltd. (Certificate of Amendment - RJSC Registry Number 3064626.)
				Pasminco Resources Canada Company	March 28, 2000	March 28, 2000 receipt of Certificate of Name Change, dated October 29, 1999, confirming the name change from Savage Resources Canada Company to Pasminco Canada Company. (Certificate of Name Change - RJSC Registry No. 3002877.)
				Savage Resources Canada Company	Nov 1, 1999	Exploration Licence No. 04727 transferred from Michael P. Cullen to Savage Resources Canada Company. Transfer No. 4855 registered November 1, 1999.
				Michael P. Cullen	Nov 5, 1996	Exploration Licence No. 02689 issued to Michael P. Cullen effective Nov 5, 1996.

Exploration Licence No. 05792

Registry records indicate that Exploration Licence No. 05792 is in goodstanding and issued to Scozinc Limited as at today's date. Specifically, Exploration Licence No. 05792 consists of the following forty-two(42) claims:

LICENCE NUMBER	CLAIMS	TRACT	CLAIM REFERENCE MAP	ANNIVERSARY DATE
05792	DE MN ABCD EFGH JKLM NOPQ EF LM NO ABCD EFGH JKLM NOPQ	42 41 32 33	11E3B 11E3B 11E3B 11E3B	Jan 20/06

The following table outlines the chronology of title for Exploration Licence No. 05792.

Licence Number	Claims	Tract	Claim Reference Map	Licensee	Date	Comments
05792	DE MN ABCD EFGH JKLM NOPQ EF LM NO ABCD EFGH JKLM NOPQ	42 41 32 33	11E3B 11E3B 11E3B 11E3B	Scozinc Limited	Jan 20, 2005	Exploration Licence No. 05792 issued to Scozinc Limited effective Jan 20, 2005.

A review of the Registry Agreement Ledger for documents recorded on Exploration Licence Nos. 06268, 06304, 06303, 05851 & 05792 and prior mineral titles, as outlined in the above five chronologies, and in the name of the current and previous title holders, indicates that the following documents have been recorded as agreements:

Agreement Number	Date	Parties to the Agreement	Comments
A0191	Oct 19, 2001 *(Date Registered)*	Pasminco Resources Canada Company Regal Consolidated Ventures Limited	Agreement dated Sep 20, 2001 L 90-1 EL 02684, 02689
S0224	Jul 20, 2004 *(Date Received)*	Alex C. Thomson Scozinc Ltd.	EL 04727, 04460

Agreement Number	Date	Parties to the Agreement	Comments
A0228	Oct 8, 2004 *(Date Received)*	Alex C. Thomson Scozinc Ltd.	Document dated Oct 1, 2002 EL 04727, 04460
A - Agreement S - Summary of Agreement			L - Lease EL - Exploration Licence

If you have any questions please do not hesitate to get in contact with me at (902) 424-8156. I remain,

Yours truly,

Andrew Wenning
Assistant Registrar of
Mineral & Petroleum Titles

AW/

Encl. Invoice

Appendix 3: Real property titles and lease agreements.

TITLE SEARCH SUMMARY CHART
LANDS OF SCOZINC LIMITED AT MARCH 2006

HALIFAX COUNTY PARCELS

Our Parcel Number	PID	Description	Encumbrances/Comments
1	369363	No. 277 Hwy. (No Lot Number)	(1) 30 Year Lease to Gallant Aggregates Ltd. Commencing May 15, 2003.
2	522623	No. 224 Hwy. (No Lot Number)	(1) Subject to Gallant Lease
3	40227936	No. 224 Hwy. Lot T & T1	(1) Subject to Gallant Lease; (2) Lot T1 is separated from Lot T by Hwy. 224; (3) Lot T is situated in both Halifax County and Colchester County (2 pids) (4) Last Subdivision Plan on file approved consolidation of Lots T and G to form TG, however, Lot G not owned by Scozinc and has own PID.
4	40227951	No. 224 Hwy. Lot B-2	Subject to Gallant Lease
5	40227969	No. 224 Hwy. Lot B-3	Subject to Gallant Lease
6	40227985	No. 224 Hwy. Lot B-4	Subject to Gallant Lease
7	40290256	No. 224 Hwy. Lot A-4	(1) Subject to Gallant Lease; (2) Subject to Possible Old Road Easement in favour of Crown – No longer signs of Road in 1976, but still appears in desc.
8	40290264	15601 Hwy. 224 Lot B&C-2	(1) Subject to Gallant Lease; (2) Consolidated Description Req'd as parcel is still described using 2 descriptions.
9	40291452	No. 224 Hwy. Lots A, A1, A2, A3	(1) Subject to Gallant Lease; (2) Consolidated Description Req'd as parcel is still described using 4 descriptions.
10	40292559	No. 224 Hwy. Lot T-2	(1) Subject to Gallant Lease; (2) Similar to parcel 3, Lot T-2 is situated in both Halifax and Colchester County (2 pids).
11	40312092	No. 227 Hwy.	Subject to Gallant Lease

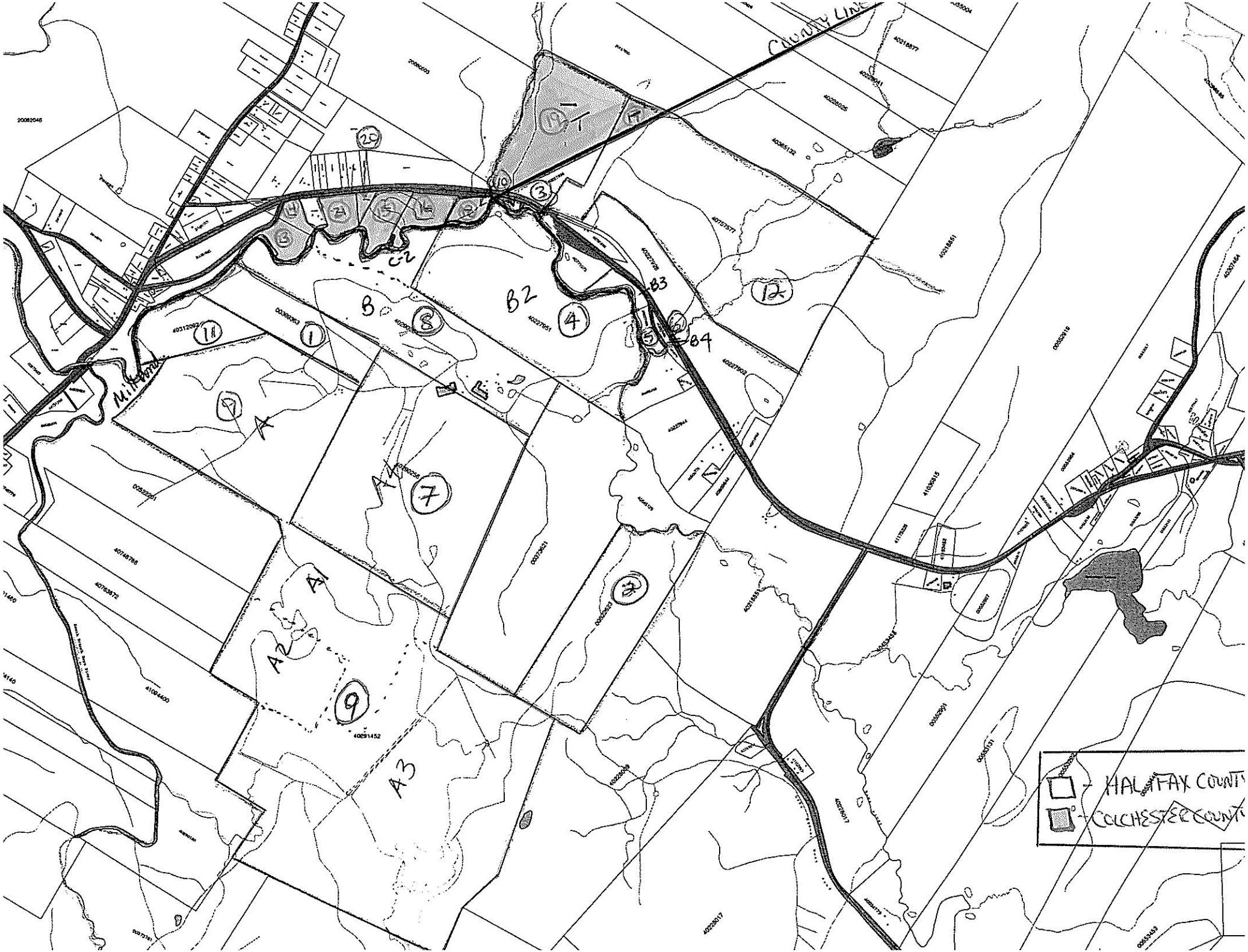
		(No Lot Number)	
12	40757577	No. 224 Hwy. Lot 89-1	(1) Subject to Gallant Lease; (2) Together With and Subject To Easement for Road Crossing Lot; (3) Lot 89-1 is situated in both Halifax and Colchester County (2 pids).

COLCHESTER COUNTY PARCELS

Our Parcel Number	PID	Description	Encumbrances/Comments
13	20158176	No. 224 Hwy. (No Lot Number)	NIL
14	20416384	No. 224 Hwy. (No Lot Number)	NIL
15	20080529	No. 224 Hwy. Lot C-1	Subject to 99 Year Sand Removal Lease in favour of Nora Recreation Development Company Limited, commencing Jan. 1, 1986.
16	20080511	No. 224 Hwy.	Subject to Sand Lease
17	20223400	No. 224 Hwy. Lot 89-1	Same as Parcel 12 – this is the Colchester County portion of the same lot.
18	20223418	No. 224 Hwy. Lot T-2	(1) Same as Parcel 10 – this is the Colchester County portion of the same lot; (2) Subject to Sand Lease.
19	20080495	No. 224 Hwy. Lot T	(1) Same of Parcel 3 – this is the Colchester County portion of Lot T; (2) Subject to Sand Lease.
20	20313250	No. 224 Hwy. Lot 3	Subject to Sand Lease
21	20158184	No. 224 Hwy.	NIL

Note: Our Colchester Title Searcher failed to find any record of the Gallant Lease against the Colchester parcels. Similarly, our Halifax Title Searcher failed to find any record of the Sand Lease against the Halifax parcels. There is also a Mortgage and Debenture that affected many of these parcels, both of which were released by a document recorded in both counties despite the wording of the document only referring to one of the counties. In summary, the fact that the parcels overlap both counties has caused some confusion in the past. Any future documents to be recorded against the properties should be sent to both county registries.

** Please see attached map for overview of the parcels and their locations.


County Line
Milford
A
A1
A2
A3
A4
B
B2
B3
B4
C2
HALIFAX COUNTY
COLCHESTER COUNTY

THIS MEMORANDUM OF LEASE made this 19th day of December, 1985,

BETWEEN:

SEABRIGHT RESOURCES INC., a body corporate, incorporated under the laws of Canada, having an office at Halifax, Nova Scotia ("Lessor")

OF THE FIRST PART

- and -

NOVA RECREATION DEVELOPMENT COMPANY LIMITED, a body corporate, incorporated under the laws of the Province of Nova Scotia, having an office at Yarmouth, Nova Scotia ("Lessee")

OF THE SECOND PART

THIS INDENTURE WITNESSETH THAT:

Demised Premises

1. IN CONSIDERATION of the rents, covenants and agreements herein, the Lessor demises to the Lessee the sand ("Sand") presently on and under the lands of the Lessor located at Gays River, Nova Scotia and described in Schedule "A", ("Demised Premises") which demise shall include:

(a) the right to mine by surface operation only and to take away the Sand from the Demised Premises;

(b) the right to enter upon and to occupy the Demised Premises as may be required for the purpose of mining and processing the Sand;

(c) the right to construct or erect such buildings or structures upon the Demised Premises as may be required for the purpose of mining and processing the Sand;

(d) the right to store and to stockpile the Sand upon the Demised Premises;

(e) the right to wash or otherwise make merchantable the Sand at locations approved by Seabright on the Demised Premises;

(f) to bring on to the Demised Premises such equipment, vehicles and other machinery as may be required for the purpose of mining and processing the Sand.

Reservations and Exceptions

Provided, however, the following are also excepted from the grant to the Lessee in respect of the Demised Premises:

(a) Two million tonnes of lower grade Sand reserved to the Lessor for the purpose of carrying out its operations;

(b) such of the Sand as is or may be required for the support of any building, shaft, mine, tailings pond, roadway or other structure presently standing or which may hereafter be constructed upon the Demised Premises, together with such reasonable surrounding areas as the Lessor shall require;

(c) such of the Demised Premises as may at any time and from time to time be required by the Lessor for the purpose of carrying out its operations upon the Demised Premises including without limitation the rehabilitation and operation of the lead/zinc mine and the reactivation of the processing mill located on the Demised Premises.

Provided, however, that the Lessor and the Lessee shall use their best efforts to carry out their respective operations in a manner compatible one to the other on the Demised Premises.

Subject, however, that wherever the grant of the Demised Premises to the Lessee hereunder shall, in the Lessor's reasonable opinion, in any way interfere with or affect any of the operations of the Lessor upon the Demised Premises this grant of the Demised Premises shall be limited and restricted so as to ensure that such operations of the Lessor are not interferred with or affected in any way;

Term

2. THE TERM for which the Lessee shall hold the Demised Premises is the period of Ninety-Nine (99) years, commencing on the 1st day of January, 1986, herein called the "Commencement Date" and ending on the 31st day of December, 2084, both dates inclusive, and herein called the "Term".

Rent/Royalty

3. THE RENT that the Lessee shall pay is in accordance with the conditions and terms set out in Paragraph 3 of the Lease dated December 19, 1985.

4. Any notice required or permitted hereunder shall be sufficiently given if by hand or sent by prepaid registered mail as follows:

(a) To Seabright:
Seabright Resource Inc.
Suite 301
6100 Young Street
Halifax, Nova Scotia
B3K 2A4
Attention: Terence D. Coughlan

(b) To Nova:

Nova Recreation Development
Company Limited
P.O. Box 455
Yarmouth, Nova Scotia
B5A 4B4
Attention: John Z. Miller, Jr.

Any notice mailed shall be deemed to have been given and received on the third business day following the date of mailing.

Each of the parties hereto shall bear the fees and expenses of its own counsel, accountants and other advisors in connection with this Lease and the transactions provided for herein.

This Lease shall be construed in accordance with the laws of the Province of Nova Scotia and the laws of Canada.

This Lease may be executed in separate counterparts, each of which when so executed shall together constitute one Lease.

This Lease may be assigned by either party.

This Lease shall be binding upon and shall enure to the benfit of the parties, their respective successors and assigns.

IN WITNESS WHEREOF the parties hereto have executed These Presents the day and year first above written.

SIGNED, SEALED AND DELIVERED	) SEABRIGHT RESOURCES INC.
in the presence of:	)Per:
David H. Reardon	) NOVA RECREATION DEVELOPMENT COMPANY LIMITED
David H. Reardon	)Per:

Appendix 4: Surface Reserves.

High Grade Zone, Proven Reserve, >= 7 % Equivalent Zinc

Level Elev. (m)	Volume (m˘)	SG	Tonnes	Zinc Grade	Lead Grade
495	160	2.85	440	9.3%	1.0%
490	460	2.90	1,340	9.3%	3.3%
485	1,190	2.97	3,540	9.7%	5.7%
480	1,820	2.98	5,440	11.7%	4.9%
475	4,410	2.88	12,720	8.9%	2.7%
470	8,510	2.88	24,530	9.6%	2.2%
465	15,010	2.89	43,450	9.7%	2.7%
460	15,910	2.91	46,370	10.1%	3.3%
455	15,850	2.93	46,370	8.7%	4.7%
450	10,010	2.90	29,000	8.6%	3.5%
445	6,480	2.91	18,890	8.4%	4.4%
440	4,320	2.96	12,780	8.2%	6.4%
435	4,070	2.97	12,090	7.6%	7.4%
430	2,650	2.97	7,880	7.7%	7.2%
425	2,430	2.95	7,160	7.9%	6.2%
420	2,260	2.97	6,720	8.5%	6.6%
415	1,350	2.93	3,950	6.6%	6.3%
410	300	2.90	870	3.8%	6.9%
405	30	2.93	80	6.1%	6.6%
Subtotal	97,230	2.92	283,620	9.1%	4.1%

High Grade Zone, Proven Reserve, 2-7 % Equivalent Zinc

Level Elev. (m)	Volume (m˘)	SG	Tonnes	Zinc Grade	Lead Grade
495	540	2.77	1,480	3.6%	0.9%
490	770	2.76	2,120	3.8%	0.5%
485	2,600	2.77	7,210	3.5%	1.1%
480	3,640	2.77	10,100	3.5%	1.4%
475	6,940	2.77	19,230	3.6%	1.2%
470	9,250	2.78	25,660	3.9%	1.1%
465	9,350	2.79	26,080	4.1%	1.6%
460	7,130	2.79	19,900	4.2%	1.6%
455	5,150	2.80	14,410	4.1%	1.9%
450	3,070	2.79	8,580	4.2%	1.7%
445	1,810	2.79	5,070	4.6%	1.5%
440	970	2.78	2,690	4.1%	1.4%
435	360	2.80	1,000	3.7%	2.4%
430	260	2.80	720	3.6%	2.5%
425	160	2.81	440	4.1%	2.7%
420	350	2.83	990	3.1%	4.2%
415	330	2.85	950	1.9%	6.0%
410	110	2.84	320	2.1%	5.5%
Subtotal	52,780	2.78	146,930	3.9%	1.5%

High Grade Zone, Proven Reserve, 1.5-2 % Equivalent Zinc

Level Elev. (m)	Volume (m˘)	SG	Tonnes	Zinc Grade	Lead Grade
495	160	2.73	440	1.4%	0.6%
490	220	2.73	610	1.3%	0.6%
485	100	2.73	290	1.7%	0.2%
480	20	2.73	50	1.5%	0.6%
475	70	2.73	200	1.5%	0.3%
470	220	2.73	600	1.5%	0.3%
460	40	2.73	100	1.4%	0.6%
455	20	2.73	60	1.5%	0.5%
Subtotal	860	2.73	2,350	1.4%	0.5%

High Grade Zone, Proven Reserve, 0.75-2 % Equivalent Zinc

Level Elev. (m)	Volume (m˘)	SG	Tonnes	Zinc Grade	Lead Grade
495	180	2.72	490	0.8%	0.5%
490	170	2.72	450	1.2%	0.3%
485	10	2.72	20	0.8%	0.5%
480	10	2.72	20	1.1%	0.2%
455	30	2.72	90	0.3%	0.8%
Subtotal	390	2.72	1,070	0.9%	0.4%

High Grade Zone, Probable Reserve, >=7 % Equivalent Zinc

Level Elev. (m)	Volume (m^3)	SG	Tonnes	Zinc Grade	Lead Grade
495	50	2.85	130	9.0%	1.2%
490	280	2.86	810	8.0%	2.1%
485	150	2.87	420	8.3%	2.3%
480	100	2.86	300	8.3%	2.3%
475	290	2.87	820	7.7%	2.8%
470	1,190	2.86	3,410	8.7%	1.9%
465	1,190	2.86	3,400	9.1%	1.5%
460	1,290	2.89	3,720	9.8%	2.3%
455	3,050	2.91	8,900	7.7%	4.9%
450	5,170	2.89	14,950	6.9%	4.3%
445	4,140	2.88	11,910	7.3%	3.6%
440	4,380	2.93	12,850	7.8%	5.6%
435	1,910	3.00	5,710	7.1%	8.8%
430	1,460	2.95	4,310	6.6%	7.1%
425	1,260	2.94	3,690	6.6%	6.5%
420	820	2.94	2,410	7.8%	5.8%
415	540	2.90	1,570	6.1%	5.5%
410	130	2.93	380	4.9%	7.2%
Subtotal	27,390	2.91	79,700	7.5%	4.8%

High Grade Zone, Probable Reserve, 2-7 % Equivalent Zinc

Level Elev. (m)	Volume (m^3)	SG	Tonnes	Zinc Grade	Lead Grade
495	250	2.78	690	4.7%	1.0%
490	310	2.77	850	3.0%	1.6%
485	690	2.78	1,920	3.1%	1.8%
480	220	2.79	620	3.0%	2.3%
475	270	2.75	760	3.5%	0.4%
470	440	2.79	1,230	4.9%	1.2%
465	770	2.79	2,140	5.0%	1.3%
460	1,080	2.79	3,010	4.8%	1.1%
455	780	2.81	2,190	4.8%	1.9%
450	1,170	2.80	3,260	4.7%	1.7%
445	1,020	2.81	2,870	4.8%	2.0%
440	690	2.81	1,940	4.5%	2.1%
435	80	2.81	210	4.7%	2.3%
430	160	2.83	450	3.6%	3.9%
425	220	2.83	620	4.4%	3.1%
415	10	2.82	40	4.1%	3.3%
410	100	2.84	270	2.2%	5.1%
Subtotal	8,250	2.80	23,070	4.4%	1.7%

High Grade Zone, In-Pit Inferred Resource, >=7 % Equivalent Zinc

Level Elev. (m)	Volume (m^3)	SG	Tonnes	Zinc Grade	Lead Grade
490	40	2.86	110	9.1%	1.7%
450	240	2.90	690	7.7%	4.1%
445	20	2.91	70	5.1%	6.3%
440	700	3.03	2,120	7.0%	9.9%
435	570	2.99	1,710	7.4%	8.3%
430	200	2.93	590	5.4%	7.0%
425	40	2.95	120	6.3%	7.3%
Subtotal	1,820	2.98	5,410	7.0%	8.1%

High Grade Zone, In-Pit Inferred Resource, 2-7 % Equivalent Zinc

Level Elev. (m)	Volume (m^3)	SG	Tonnes	Zinc Grade	Lead Grade
490	20	2.77	60	3.0%	1.4%
465	10	2.76	40	4.0%	0.2%
450	0	2.80	0	5.1%	1.6%
445	80	2.78	220	5.0%	0.6%
Subtotal	120	2.78	320	4.6%	0.7%

High Grade Zone, In-Pit Inferred Resource, <0.75 % Equivalent Zinc

Level Elev. (m)	Volume (m^3)	SG	Tonnes	Zinc Grade	Lead Grade
500	710	2.70	1,920	0.0%	0.0%
Subtotal	710	2.70	1,920	0.0%	0.0%

Low Grade Zone, Proven Reserve, >=7 % Equivalent Zinc

Level Elev. (m)	Volume (m˘)	SG	Tonnes	Zinc Grade	Lead Grade
490	80	2.91	240	12.2%	1.6%
485	440	2.84	1,250	6.9%	2.0%
480	1,540	2.88	4,450	8.1%	3.1%
475	2,790	2.86	7,970	7.3%	2.7%
470	4,990	2.87	14,310	7.9%	2.8%
465	2,340	2.87	6,700	6.7%	3.5%
460	2,100	2.84	5,960	6.8%	2.2%
455	3,090	2.87	8,870	7.3%	3.1%
450	1,920	2.90	5,570	8.7%	3.5%
445	160	2.86	470	7.7%	2.5%
440	710	2.84	2,020	6.3%	2.5%
435	500	2.83	1,410	6.4%	2.1%
430	30	2.82	100	6.3%	1.6%
Subtotal	20,700	2.87	59,310	7.5%	2.9%

Low Grade Zone, Proven Reserve, 2-7 % Equivalent Zinc

Level Elev. (m)	Volume (m˘)	SG	Tonnes	Zinc Grade	Lead Grade
510	22,390	2.74	61,270	2.5%	0.2%
505	27,680	2.74	75,760	2.3%	0.3%
500	26,430	2.74	72,480	2.4%	0.5%
495	3,480	2.74	9,540	2.0%	0.8%
490	8,510	2.75	23,400	2.1%	1.0%
485	18,850	2.76	51,990	2.4%	1.3%
480	24,640	2.76	68,080	2.6%	1.4%
475	36,830	2.76	101,820	2.7%	1.4%
470	35,840	2.77	99,140	2.9%	1.3%
465	30,190	2.77	83,690	3.0%	1.6%
460	15,500	2.77	42,970	2.9%	1.6%
455	11,040	2.77	30,610	2.9%	1.7%
450	8,520	2.77	23,610	3.1%	1.4%
445	4,620	2.78	12,860	3.6%	1.7%
440	2,740	2.79	7,650	4.0%	1.6%
435	2,760	2.80	7,730	3.5%	2.6%
430	870	2.77	2,420	2.0%	2.2%
425	990	2.77	2,740	1.7%	2.1%
420	600	2.77	1,670	1.8%	2.0%
Subtotal	282,480	2.76	779,430	2.7%	1.1%

Low Grade Zone, Proven Reserve, 1.5-2 % Equivalent Zinc

Level Elev. (m)	Volume (m˘)	SG	Tonnes	Zinc Grade	Lead Grade
510	11,560	2.73	31,500	1.7%	0.2%
505	20,280	2.73	55,280	1.6%	0.3%
500	15,980	2.73	43,570	1.6%	0.3%
495	130	2.73	340	1.2%	0.8%
490	2,950	2.73	8,050	1.4%	0.5%
485	5,170	2.73	14,120	1.5%	0.4%
480	7,920	2.73	21,610	1.5%	0.4%
475	4,880	2.73	13,320	1.5%	0.4%
470	3,620	2.73	9,870	1.4%	0.5%
465	1,340	2.73	3,650	1.3%	0.7%
460	810	2.73	2,220	1.4%	0.5%
455	1,220	2.73	3,320	1.3%	0.6%
450	400	2.74	1,090	1.0%	1.2%
440	150	2.74	420	0.9%	1.4%
Subtotal	76,410	2.73	208,370	1.5%	0.3%

Low Grade Zone, Proven Reserve, 0.75-1.5 % Equivalent Zinc

Level Elev. (m)	Volume (m^3)	SG	Tonnes	Zinc Grade	Lead Grade
510	12,230	2.72	33,220	1.2%	0.1%
505	24,730	2.72	67,210	1.1%	0.2%
500	19,100	2.72	51,930	1.1%	0.2%
495	470	2.72	1,290	0.9%	0.6%
490	3,130	2.72	8,530	1.1%	0.3%
485	6,800	2.72	18,490	1.0%	0.4%
480	4,200	2.72	11,430	1.1%	0.3%
475	2,010	2.72	5,460	1.1%	0.3%
470	2,320	2.72	6,320	1.0%	0.5%
465	420	2.72	1,140	0.8%	0.4%
460	1,000	2.72	2,720	0.8%	0.5%
455	930	2.72	2,530	1.0%	0.5%
450	160	2.72	440	0.6%	0.5%
440	160	2.72	420	0.6%	0.6%
Subtotal	77,660	2.72	211,120	1.1%	0.2%

Low Grade Zone, Proven Reserve, <0.75 % Equivalent Zinc

Level Elev. (m)	Volume (m^3)	SG	Tonnes	Zinc Grade	Lead Grade
510	5,180	2.70	14,020	0.3%	0.0%
505	4,320	2.71	11,700	0.5%	0.1%
500	3,030	2.71	8,200	0.5%	0.1%
495	100	2.71	280	0.7%	0.1%
490	790	2.71	2,130	0.6%	0.1%
485	920	2.71	2,490	0.7%	0.1%
480	340	2.71	910	0.5%	0.2%
475	0	2.71	0	0.6%	0.0%
465	110	2.71	290	0.5%	0.2%
460	110	2.71	290	0.6%	0.1%
Subtotal	14,890	2.71	40,320	0.4%	0.1%

Low Grade Zone, Probable Reserve, >=7 % Equivalent Zinc

Level Elev. (m)	Volume (m^3)	SG	Tonnes	Zinc Grade	Lead Grade
490	1,290	2.84	3,650	7.5%	1.5%
485	3,210	2.84	9,110	7.2%	2.1%
480	2,680	2.84	7,610	6.7%	2.5%
475	2,020	2.84	5,730	6.4%	2.6%
470	2,630	2.86	7,500	7.1%	2.7%
465	4,270	2.85	12,170	7.6%	2.1%
460	4,010	2.87	11,500	7.0%	3.2%
455	3,050	2.89	8,820	7.6%	3.7%
450	4,290	2.87	12,300	7.1%	3.3%
445	2,370	2.88	6,820	6.6%	3.9%
440	1,360	2.87	3,900	5.8%	4.1%
435	900	2.85	2,580	5.6%	3.5%
430	260	2.84	740	5.1%	3.4%
425	250	2.84	700	5.2%	3.3%
Subtotal	32,580	2.86	93,130	7.0%	2.9%

Low Grade Zone, Probable Reserve, 2-7 % Equivalent Zinc

Level Elev. (m)	Volume (m^3)	SG	Tonnes	Zinc Grade	Lead Grade
510	10,690	2.74	29,270	2.3%	0.3%
505	20,690	2.74	56,700	2.2%	0.5%
500	29,380	2.74	80,530	2.3%	0.5%
495	24,150	2.75	66,330	2.3%	0.7%
490	32,820	2.75	90,370	2.5%	1.0%
485	30,880	2.76	85,220	2.7%	1.2%
480	28,750	2.76	79,460	3.2%	1.0%
475	23,280	2.76	64,330	3.1%	1.1%
470	25,140	2.77	69,570	3.2%	1.2%
465	27,490	2.77	76,080	3.1%	1.3%
460	28,300	2.77	78,290	3.0%	1.3%
455	23,000	2.77	63,730	3.1%	1.5%
450	16,640	2.77	46,140	3.1%	1.5%
445	15,680	2.78	43,550	3.1%	1.7%
440	11,230	2.78	31,190	3.3%	1.7%
435	5,340	2.79	14,890	3.7%	1.9%
430	4,060	2.79	11,330	3.6%	1.9%
425	2,040	2.78	5,690	3.2%	2.0%
420	1,560	2.78	4,340	2.2%	2.4%
415	920	2.79	2,570	2.2%	3.0%
Subtotal	362,040	2.76	999,590	2.8%	1.1%

Low Grade Zone, Probable Reserve, 1.5-2 % Equivalent Zinc

Level Elev. (m)	Volume (m^3)	SG	Tonnes	Zinc Grade	Lead Grade
510	12,510	2.72	34,080	1.6%	0.2%
505	19,440	2.73	52,970	1.6%	0.2%
500	14,790	2.72	40,310	1.6%	0.2%
495	7,520	2.73	20,520	1.6%	0.3%
490	12,390	2.73	33,790	1.4%	0.4%
485	8,540	2.73	23,320	1.4%	0.6%
480	3,860	2.73	10,550	1.4%	0.7%
475	2,460	2.73	6,720	1.4%	0.6%
470	2,020	2.73	5,510	1.4%	0.6%
465	1,050	2.73	2,870	1.5%	0.4%
460	1,080	2.73	2,940	1.5%	0.6%
455	690	2.73	1,890	1.4%	0.7%
450	290	2.73	790	1.1%	0.9%
445	150	2.74	400	1.2%	1.0%
440	160	2.73	430	1.3%	0.6%
435	70	2.73	200	1.3%	0.5%
Subtotal	87,020	2.73	237,290	1.5%	0.3%

Low Grade Zone, Probable Reserve, 0.75-1.5 % Equivalent Zinc

Level Elev. (m)	Volume (m^3)	SG	Tonnes	Zinc Grade	Lead Grade
510	20,650	2.72	56,100	1.1%	0.1%
505	19,470	2.72	52,910	1.1%	0.1%
500	12,240	2.72	33,260	1.1%	0.2%
495	4,670	2.72	12,690	0.9%	0.1%
490	4,970	2.72	13,500	1.0%	0.3%
485	4,160	2.72	11,320	1.1%	0.3%
480	1,300	2.72	3,530	1.2%	0.2%
475	790	2.72	2,150	1.2%	0.2%
470	710	2.72	1,920	1.0%	0.3%
465	1,210	2.72	3,290	0.9%	0.3%
460	930	2.72	2,540	1.1%	0.3%
455	570	2.72	1,560	1.2%	0.2%
450	10	2.72	40	1.3%	0.0%
440	470	2.72	1,290	0.7%	0.7%
Subtotal	72,160	2.72	196,110	1.1%	0.2%

Low Grade Zone, Probable Reserve, <0.75 % Equivalent Zinc

Level Elev. (m)	Volume (m˘)	SG	Tonnes	Zinc Grade	Lead Grade
510	4,630	2.71	12,530	0.5%	0.1%
505	3,090	2.71	8,380	0.6%	0.1%
500	1,160	2.71	3,130	0.6%	0.0%
495	1,690	2.71	4,570	0.6%	0.1%
490	580	2.71	1,590	0.6%	0.1%
485	160	2.71	420	0.7%	0.1%
470	0	2.71	0	0.7%	0.0%
465	0	2.71	10	0.5%	0.3%
460	200	2.71	530	0.5%	0.3%
Subtotal	11,500	2.71	31,160	0.5%	0.1%

Low Grade Zone, In-Pit Inferred Resource, >=7 % Equivalent Zinc

Level Elev. (m)	Volume (m˘)	SG	Tonnes	Zinc Grade	Lead Grade
495	2,170	2.85	6,180	7.7%	2.0%
490	3,160	2.83	8,940	6.5%	1.7%
485	1,850	2.84	5,260	6.3%	2.4%
480	230	2.86	650	4.3%	4.8%
475	140	2.86	390	4.0%	4.8%
465	10	3.00	40	3.1%	11.5%
460	630	3.00	1,890	9.6%	7.3%
455	530	2.92	1,560	6.2%	5.9%
450	540	2.85	1,540	5.4%	3.6%
445	1,260	2.83	3,580	6.5%	2.0%
440	470	2.95	1,400	7.0%	6.7%
435	700	2.85	2,000	6.3%	3.1%
430	730	2.86	2,090	6.4%	3.2%
425	470	2.87	1,340	5.9%	3.9%
420	460	2.86	1,320	5.8%	3.7%
415	260	2.86	750	6.1%	3.4%
Subtotal	13,630	2.86	38,910	6.6%	3.0%

Low Grade Zone, In-Pit Inferred Resource, 2-7 % Equivalent Zinc

Level Elev. (m)	Volume (m˘)	SG	Tonnes	Zinc Grade	Lead Grade
510	1,500	2.75	4,110	2.6%	0.6%
505	3,670	2.75	10,080	2.5%	0.6%
500	4,600	2.74	12,610	2.2%	0.6%
495	22,050	2.75	60,620	2.5%	0.8%
490	15,420	2.76	42,620	2.8%	1.3%
485	10,470	2.77	29,020	2.9%	1.6%
480	5,400	2.78	15,010	2.8%	2.1%
475	2,600	2.78	7,220	2.4%	2.2%
470	1,830	2.77	5,080	2.8%	1.6%
465	1,430	2.80	4,000	2.8%	2.8%
460	4,370	2.78	12,180	3.0%	2.1%
455	3,330	2.79	9,270	3.5%	1.9%
450	3,300	2.78	9,160	3.4%	1.5%
445	3,670	2.77	10,160	2.5%	1.8%
440	2,360	2.78	6,550	3.0%	1.8%
435	3,900	2.78	10,860	3.2%	1.9%
430	3,670	2.78	10,200	3.1%	1.9%
425	2,830	2.77	7,840	3.0%	1.4%
420	1,230	2.75	3,390	2.7%	0.8%
415	570	2.77	1,580	2.8%	1.4%
Subtotal	98,190	2.77	271,540	2.8%	1.4%

Low Grade Zone, In-Pit Inferred Resource, 1.5-2 % Equivalent Zinc

Level Elev. (m)	Volume (m^3)	SG	Tonnes	Zinc Grade	Lead Grade
510	760	2.72	2,070	1.4%	0.3%
505	2,580	2.73	7,030	1.4%	0.5%
500	1,710	2.73	4,660	1.5%	0.4%
495	10,750	2.73	29,360	1.3%	0.6%
490	8,880	2.73	24,260	1.3%	0.7%
485	1,430	2.73	3,900	1.1%	0.8%
480	840	2.73	2,300	1.5%	0.5%
475	440	2.73	1,210	1.6%	0.3%
470	100	2.73	270	1.9%	0.0%
465	60	2.73	150	1.9%	0.0%
460	110	2.73	310	1.6%	0.3%
455	10	2.72	20	1.6%	0.0%
450	670	2.73	1,830	1.5%	0.6%
445	510	2.73	1,380	1.5%	0.3%
440	140	2.73	380	1.4%	0.4%
435	150	2.73	410	1.4%	0.3%
430	120	2.72	330	1.6%	0.0%
425	50	2.72	120	1.5%	0.0%
Subtotal	29,300	2.73	80,000	1.3%	0.6%

Low Grade Zone, In-Pit Inferred Resource, 0.75-1.5 % Equivalent Zinc

Level Elev. (m)	Volume (m^3)	SG	Tonnes	Zinc Grade	Lead Grade
510	380	2.72	1,040	1.2%	0.2%
505	1,180	2.72	3,200	1.0%	0.3%
500	2,940	2.72	7,990	0.9%	0.3%
495	19,840	2.72	53,910	1.1%	0.2%
490	7,220	2.72	19,630	1.1%	0.2%
485	1,800	2.72	4,880	1.1%	0.2%
480	700	2.72	1,900	1.0%	0.2%
475	60	2.71	160	1.0%	0.1%
460	0	2.72	10	1.1%	0.3%
450	20	2.72	50	1.3%	0.0%
445	380	2.72	1,030	0.7%	0.7%
440	30	2.73	80	0.6%	0.9%
435	10	2.71	10	1.0%	0.0%
430	10	2.71	20	1.0%	0.0%
Subtotal	34,560	2.72	93,930	1.1%	0.2%

Low Grade Zone, In-Pit Inferred Resource, <0.75 % Equivalent Zinc

Level Elev. (m)	Volume (m^3)	SG	Tonnes	Zinc Grade	Lead Grade
510	4,730	2.71	12,790	0.0%	0.3%
505	9,480	2.70	25,630	0.0%	0.2%
500	13,620	2.71	36,860	0.0%	0.3%
495	1,590	2.71	4,300	0.7%	0.0%
490	700	2.71	1,890	0.7%	0.0%
485	140	2.71	380	0.7%	0.0%
445	10	2.71	40	0.6%	0.0%
440	60	2.71	170	0.6%	0.0%
435	20	2.71	50	0.6%	0.0%
430	50	2.71	140	0.6%	0.0%
425	90	2.70	240	0.0%	0.0%
420	40	2.70	100	0.0%	0.0%
415	120	2.70	330	0.0%	0.0%
Subtotal	30,650	2.71	82,930	0.1%	0.2%

Overburden (Glacial Till and Alluvial Sand)

Level Elev. (m)	Volume (m˘)	SG	Tonnes
555	5,780	2.00	11,560
550	88,790	2.00	177,590
545	224,610	2.00	449,230
540	560,630	2.00	1,121,260
535	781,660	2.00	1,563,320
530	933,890	2.00	1,867,790
525	1,036,670	2.00	2,073,330
520	1,130,220	2.00	2,260,440
515	1,402,510	2.00	2,805,020
510	1,470,070	2.00	2,940,150
505	1,237,540	2.00	2,475,090
500	1,046,170	2.00	2,092,340
495	885,790	2.00	1,771,580
490	737,800	2.00	1,475,600
485	589,700	2.00	1,179,390
480	464,940	2.00	929,870
475	111,430	2.00	222,870
470	79,020	2.00	158,040
465	62,370	2.00	124,750
460	48,510	2.00	97,010
455	35,960	2.00	71,930
450	24,390	2.00	48,790
445	12,520	2.00	25,030
440	5,000	2.00	10,010
435	1,250	2.00	2,500
Subtotal	12,977,240	2.00	25,954,480

Trench Clay

Level Elev. (m)	Volume (m˘)	SG	Tonnes
475	326,040	2.00	652,070
470	287,880	2.00	575,770
465	243,120	2.00	486,240
460	207,180	2.00	414,360
455	179,710	2.00	359,420
450	140,530	2.00	281,060
445	99,340	2.00	198,680
440	66,580	2.00	133,160
435	45,160	2.00	90,310
430	29,870	2.00	59,750
425	18,660	2.00	37,320
420	11,100	2.00	22,190
Subtotal	1,655,160	2.00	3,310,310

Goldenville Quartzite Waste Rock

Level Elev. (m)	Volume (m˘)	SG	Tonnes
500	6,650	2.65	17,610
495	5,420	2.65	14,370
490	7,190	2.65	19,050
485	200	2.65	520
480	510	2.65	1,350
475	3,690	2.65	9,790
470	8,220	2.65	21,790
465	13,710	2.65	36,340
460	16,210	2.65	42,960
455	18,560	2.65	49,190
450	17,810	2.65	47,190
445	14,340	2.65	38,010
440	9,750	2.65	25,850
435	4,900	2.65	12,980
430	3,710	2.65	9,840
425	2,400	2.65	6,370
420	1,670	2.65	4,430
415	5,040	2.65	13,360
410	2,240	2.65	5,930
405	350	2.65	920
Subtotal	142,590	2.65	377,860

Evapourite (Gypsum & Anhydrite)

Level Elev. (m)	Volume (m^3)	SG	Tonnes
515	870	2.40	2,100
510	12,260	2.40	29,430
505	46,100	2.40	110,650
500	68,990	2.40	165,590
495	88,180	2.40	211,640
490	108,330	2.40	260,000
485	151,740	2.40	364,170
480	184,410	2.40	442,580
475	133,990	2.40	321,580
470	123,660	2.40	296,780
465	108,930	2.40	261,440
460	88,190	2.40	211,660
455	63,180	2.40	151,630
450	46,260	2.40	111,020
445	41,540	2.40	99,700
440	32,570	2.40	78,160
435	21,980	2.40	52,760
430	12,340	2.40	29,610
425	4,810	2.40	11,540
420	760	2.40	1,830
415	1,500	2.40	3,590
Subtotal	1,340,610	2.40	3,217,470

Appendix 5: Economic analysis.

General Parameters

July 12, 2006

All prices are expressed in Canadian dollars unless otherwise stated.

Item	Base Case	Factor	Factored Value
Parameters with Multiplicative Factors[1]			
Production Rate (tonnes per day)			
Surface	2,000	100%	2,000
Underground	1,350	100%	1,350
Metal Prices ($US per lb):			
Zinc	1.10	100%	1.10
Lead	0.40	100%	0.40
Surface Reserves (Undiluted):			
Tonnes	3,320,000	100%	3,320,000
Average Grade:			
Zinc	3.3%	100%	3.3%
Lead	1.3%	100%	1.3%
Underground Reserves (Undiluted):			
Tonnes	1,110,000	100%	1,110,000
Average Grade:			
Zinc	6.6%	100%	6.6%
Lead	3.7%	100%	3.7%
Capital Costs:		100%	
Mine		100%	
Processing Plant		100%	
Operating Costs		100%	
Exchange Rate ($US per $CAN)	$ 0.86	100%	$ 0.86
Parameters with Additive Factors[2]			
Dilution:			
Open Pit	15%	0%	15.0%
Underground	15%	0%	15.0%
Mining Recovery:			
Open Pit	90%	0%	90.0%
Underground	90%	0%	90.0%
Processing Recovery:			
Zinc	90.0%	0%	90.0%
Lead	95.0%	0%	95.0%
Cost of Capital	7.0%	0%	7.0%

Notes:

1. "Factored Value" equals "Base Case" value multiplied by "Factor."
2. "Factored Value" equals "Base Case" value plus "Factor." This applies to values, other than grade, that are expressed as a percentage.

Capital Costs

Parameters:

Average Machine Life before Overhaul (hours)	12,000
Miscellaneous Equipment Cost (Percent of Other Capital)	5%
Contingency[4]	0%

General

Item	Number		Unit Cost		Cost
Environmental Permitting	1	$	50,000	$	50,000
Highway Trucks	1	$	160,000	$	160,000
Office Equipment				$	80,000
Water				$	15,000
Miscellaneous				$	15,000
Subtotal, General Costs				$	320,000

Mine Site

Surface Infrastructure		Cost
Shop Equipment	$	15,000
General Site Preparation	$	20,000
Transformer Diagnostics	$	9,000
Pole Line Repairs	$	3,000
General Electrical Work	$	5,000

Mobile Equipment[1]

Type	Number		Unit Cost		Cost
Pick-up Trucks	4	$	25,000	$	100,000
Miscellaneous					
Personal Safety Equipment	82	$	500	$	41,000
Miscellaneous Equipment				$	10,000
Subtotal, Mine Site				$	203,000

Processing Plant

Equipment		Cost ($CAN)
Mill Repair:		
Weightometer - Rod Mill Feed Conveyor	$	12,000
Sampler Pump - Zinc Thickener	$	8,000
Sampler Pump - Lead Thickener	$	8,000
Sample Cutters (x 4)	$	11,000
Sample Cutter for Rod Mill Discharge	$	4,000
Grinding Balls, 30 tonnes	$	20,000
Grinding Rods, 30 tonnes	$	22,500
Rotary Vacuum Pumps (x 2)	$	36,000
Flotation Cell Blower (4500 cfm)	$	13,000
Flotation Cell Blower (2300 cfm)	$	8,000
Reagent Feeders (x 12)	$	18,000
Mettler Balance	$	8,500
Rod Mill Lifter Bars	$	32,000
Ball Mill Lifter Bars (Rubber)	$	75,000
Tailings Pumps (x 2)	$	21,000
Fuel Storage Tank	$	21,000
Heating System	$	220,000
Roof Repair	$	18,000
Electric Motor Rewinding	$	75,000
Ramp at Railroad Siding	$	80,000
Spare Parts Inventory	$	400,000
Truck scale	$	42,000
Assay Office Supplies	$	40,000
Replace Potable and Process Water Supply Pumps	$	2,000
Replace Main Power Supply Cable fr Main Transformer	$	27,000
Equipment Replacement[2]	$	500,000
Subtotal	$	1,722,000
Engineering, Supervision, Labour & Administration Costs	$	600,000
Miscellaneous	$	86,000
Subtotal, Fixed Plant Capital Costs	$	2,408,000
Subtotal, General, Mining & Processing	$	2,931,000
Multiplying Factors:		
Mine		100%
Processing Plant		100%
Factored Total	$	2,931,000
Contingency[4]	$	-
Total, General, Mining & Processing	$	2,931,000

Underground (Year 6)

Item	Number		Unit Cost		Cost
Drill Jumbo (Two Boom)	1	$	883,000	$	883,000
Drill Jumbo (Single Boom)	1	$	465,000	$	465,000
Scooptram (6 yd)	1	$	630,000	$	630,000
Scooptram (3 yd)	1	$	400,000	$	400,000
Repair 5 yd Scooptram	1	$	20,000	$	20,000
U/G Haul Truck (40 tonne)	1	$	900,000	$	900,000
Scissor Lift	1	$	250,000	$	250,000
Boom Truck	1	$	250,000	$	250,000
Tractors	5	$	20,000	$	100,000
Compressor (5000 cfm, 120 psi)	1	$	233,000	$	233,000
Main Fan	1	$	100,000	$	100,000
Auxiliary Fans	4	$	10,000	$	40,000
Jack-leg Drills	15	$	5,000	$	75,000
Stopers	15	$	5,000	$	75,000
Slushers	4	$	20,000	$	80,000
Diamond Drill	1	$	75,000	$	75,000
Alimak Raise Climber	1	$	350,000	$	350,000
Pumps	4	$	4,000	$	16,000
Rock Breaker	1	$	20,000	$	20,000
Underground Electrical	1	$	50,000	$	50,000
Pipe (Water, Air)	1	$	10,000	$	10,000
Mine Rescue Equipment	1	$	40,000	$	40,000
Technical Equipment	1	$	20,000	$	20,000
Communication System	1	$	30,000	$	30,000
Fill Mixing Plant	1	$	200,000	$	200,000
Miscellaneous Equipment	1	$	270,000	$	270,000
Subtotal, Underground Operation				$	5,582,000

Year 2 Capital Costs

Item	Number		Unit Cost		Cost
Re-route Power Line	1,500	$	60	$	90,000
Miscellaneous				$	5,000
Subtotal, Year 2 Capital				$	95,000

Notes:

1. Owning costs for loading and hauling equipment included in an all-inclusive operating cost per tonne.
2. During clean-up and plant run-in, some equipment will require repair or replacing.
4. Reflects variation for Class of estimate (ie: Order of Magnitude, Preliminary or Definitive.).

Workforce

Average Burden[3] 19%

Labour Force

Staff

Department	Members	Salary	Burden[3]	Yearly Total
Engineering	2	$ 60,000	12,000	$ 144,000
Engineering Technicians	2	$ 50,000	10,000	$ 120,000
Management	1	$ 100,000	17,000	$ 117,000
Mine Superintendent	1	$ 80,000	14,000	$ 94,000
Mill Superintendent	1	$ 80,000	14,000	$ 94,000
Health and Safety	1	$ 60,000	12,000	$ 72,000
Accounting	1	$ 50,000	10,000	$ 60,000
Human Resources / Payroll	1	$ 40,000	9,000	$ 49,000
Geology	2	$ 50,000	10,000	$ 120,000
Secretarial	1	$ 40,000	9,000	$ 49,000
Purchaser	1	$ 60,000	12,000	$ 72,000
Subtotal:	14			$ 1,000,000

Surface Shift Workers:

Department	Members per Shift	Salary	Burden[3]	Number of Shifts	Number of Workers	Yearly Total
Support Labour:						
Mechanic	1	$ 40,000	9,000	2	2	$ 98,000
Electrician	1	$ 50,000	10,000	2	2	$ 120,000
Clerk	1	$ 30,000	8,000	2	2	$ 76,000
Security	1	$ 30,000	8,000	3	3	$ 114,000
Cleaning Staff	1	$ 30,000	8,000	3	3	$ 114,000
Subtotal	5				12	$ 500,000
Direct Labour:						
Front-end Loader Operator	1	$ 40,000	9,000	1	1	$ 49,000
Supervision (Pit Foreman)	1	$ 60,000	12,000	1	1	$ 72,000
Mill Foreman	1	$ 60,000	12,000	1	1	$ 72,000
Crusher Operator	1	$ 40,000	9,000	2	2	$ 98,000
Grinding Mill Operator	2	$ 40,000	9,000	2	4	$ 196,000
Flotation Section Operator	2	$ 50,000	10,000	2	4	$ 240,000
Dewatering	2	$ 40,000	9,000	2	4	$ 196,000
Millwrights	1	$ 50,000	10,000	3	3	$ 180,000
Assay Office:						
Chief Assayer	1	$ 50,000	10,000	1	1	$ 60,000
Assayers	2	$ 40,000	9,000	2	4	$ 196,000
Buckers	1	$ 35,000	8,000	2	2	$ 86,000
Helpers	2	$ 35,000	8,000	2	4	$ 172,000
Subtotal	17				31	$ 1,617,000
Total	22				43	$ 2,117,000

Underground Shift Workers:

Department	Members per Shift	Salary	Burden[3]	Number of Shifts	Number of Workers	Yearly Total
Drill Jumbo Operators	2	$ 100,000	17,000	3	6	$ 702,000
Nippers/Scoop/Slusher Operators	2	$ 100,000	17,000	3	6	$ 702,000
Jackleg Miners	1	$ 100,000	17,000	3	3	$ 351,000
Scoop Operators	2	$ 100,000	17,000	3	6	$ 702,000
Truck Drivers	1	$ 100,000	17,000	3	3	$ 351,000
Raise Miners	2	$ 100,000	17,000	3	6	$ 702,000
Ground Control	2	$ 100,000	17,000	3	6	$ 702,000
Underground Supervisor	1	$ 100,000	17,000	3	3	$ 351,000
Diamond Driller	1	$ 100,000	17,000	3	3	$ 351,000
General Labour	2	$ 80,000	14,000	3	6	$ 564,000
Fill Plant Operator (Surface)	1	$ 40,000	9,000	1	1	$ 49,000
					49	$ 5,527,000

Total For Surface Operation

	Number	Average Salary[1]	Total
Salaried	14	$ 71,000	$ 1,000,000
Indirect Labour	12	$ 42,000	$ 500,000
Direct Labour	31	$ 52,000	$ 1,617,000
Equipment Operators	25	$ 56,000	$ 1,400,000
Total	82	$ 55,000	$ 4,517,000

Total For Underground Operation

	Number	Average Salary[1]	Total
Salaried	14	$ 71,000	$ 1,000,000
Indirect Labour	12	$ 42,000	$ 500,000
Direct Labour	49	$ 113,000	$ 5,527,000
Total	75	$ 94,000	$ 7,027,000

Notes:
1. Salaries include burden.
2. Excavator, haul truck and grader operator included in a single, all-inclusive 'cost per tonne' Operating Cost.
3. Burden includes CPP, EI, vacation pay, WCB, basic pension and basic health.

Surface Mine Production

Parameters:

Yearly Diluted Ore Production (tonnes)	700,000
Years of Pre-Stripping	2/12

Approved Mine Plan Reserves ("Pit 5")

Material	Tonnes	Zinc Grade	Lead Grade	SG
Ore				
Undiluted	3,320,000	3.3%	1.3%	2.77
Diluted & Recovered	3,440,000	2.9%	1.1%	2.76
Waste Rock	3,600,000			2.40
Overburden & Trench	29,300,000			2.20

Average SG[1]	2.30
Mine Life (Years)	4 11/12
End of Surface Mining (Year)	5 10/12
Overall Stripping Ratio	9.9

Production Schedule

	Year 1 Q1	*Year 1 Q2*	*Year 1 Q3*	*Year 1 Q4*	Year 1	Year 2	Year 3	Year 4	Year 5	Year 6	Year 7	Year 8	Year 9
Portion in Operation[3]													
Stripping[3,4]				*3/12*	3/12	1	1	1	1	10/12	0	0	0
Ore Production[3]				*1/12*	1/12	1	1	1	1	10/12	0	0	0
Ore (Diluted)				*58,000*	58,000	700,000	700,000	700,000	700,000	582,000	-	-	-
Cumulative	-	-	-	*58,000*	*58,000*	*758,000*	*1,458,000*	*2,158,000*	*2,858,000*	*3,440,000*	*3,440,000*	*3,440,000*	*3,440,000*
Grade (Diluted, %)													
Zinc	*2.87%*	*2.87%*	*2.87%*	*2.87%*	2.87%	2.87%	2.87%	2.87%	2.87%	2.87%	2.87%	2.87%	2.87%
Lead	*1.13%*	*1.13%*	*1.13%*	*1.13%*	1.13%	1.13%	1.13%	1.13%	1.13%	1.13%	1.13%	1.13%	1.13%
All Waste (Rock and Soil)	-	-	-	*2,000,000*	*2,000,000*	*7,050,000*	*6,650,000*	*6,250,000*	*5,850,000*	*4,940,000*	-	-	-
Cumulative	-	-	-	*2,000,000*	2,000,000	9,050,000	15,700,000	21,950,000	27,800,000	32,740,000	32,740,000	32,740,000	32,740,000
Breakdown:													
Waste Rock				-	-	550,000	650,000	750,000	850,000	640,000			
Cumulative	-	-	-	-	-	*550,000*	*1,200,000*	*1,950,000*	*2,800,000*	*3,440,000*	*3,440,000*	*3,440,000*	*3,440,000*
Overburden & Trench				*2,000,000*	2,000,000	6,500,000	6,000,000	5,500,000	5,000,000	4,300,000			
Cumulative	-	-	-	*2,000,000*	*2,000,000*	*8,500,000*	*14,500,000*	*20,000,000*	*25,000,000*	*29,300,000*	*29,300,000*	*29,300,000*	*29,300,000*
Total Tonnes (Ore, Waste Rock & OB)				*2,058,000*	*2,058,000*	*7,750,000*	*7,350,000*	*6,950,000*	*6,550,000*	*5,522,000*	-	-	-

Notes:

3. All portions, even quarterly figures, are expressed as fractions of years.
4. Two months pre-stripping.

Underground Mine Production

Parameters:

Mining Method:	Mechanised Cut-and-Fill
Underground Reserves (Undiluted, tonnes)	1,110,000
Underground Dilution	15%
Underground Mining Recovery	90%
Diluted & Recoverable Reserves (tonnes)	1,150,000
Development Dimensions:	
Width (m)	5
Height (m)	5
Length (m)	4
Development Rounds per Shift	1
Stope Production Round Dimensions:	
Width (m)	3.6
Height (m)	5
Length (m)	4
Production Rounds per Shift	1 1/2
Shifts per Day	2
Production Rate (Diluted Tonnes per Day)	1,350
Tonnes per Year	473,000
Grade (Undiluted, %):	
Zinc	6.6%
Lead	3.7%
Grade (Diluted, %):	
Zinc	5.7%
Lead	3.2%
Underground Ore SG	2.90
Waste Rock SG	2.40

Stoping Productivity

Production per Round:	
m^3	72
tonnes	209
Daily Production per Crew:	
m^3	216
tonnes	626
Number of Crews Required:	
Production	1
Development	1
Total	2

Development Requirements

Development Drifting	Metres
480 m Level Main Haulage	750
430 m Level	750
380 m Level	300
Ramps, 15 % Grade	
6750 East, to 350 m	870
6900 East, to 430 m	330
7100 East, to 400 m	530
Re-Muck Bays and Sumps	150
Subtotal	3,680
Number of Rounds	920
Number of Crew-Shifts	920
Number of Crew-Days	460
Number of Development Jumbos Required	1
Waste Rock Tonnes	230,000
m^3	95,800
m^3 per Year	39,400

Raises (45 deg Average Dip)

Section	Elevation Change (m)	Metres
6650	100	140
6750	100	140
6850	50	70
6950	50	70
7050	100	140
7150	100	140
7250	100	140
Ventilation Raises (Vertical)	100	100
Subtotal		940

Fill Requirements

Concrete SG	2.4
Avg Cement:Sand Ratio (Weight Percent)[1]	5%
Fill Requirement (per day):	
m^3	466
tonnes	1,120
Fill Ingredients (tonnes per day):	
Sand	1,060
Cement	60

Underground Haul Trucks

Tonnes of Waste Rock	230,000
Tonnes of Diluted Ore	1,150,000
Subtotal	1,380,000
Days of Mill Production	850
Tonnes Per Day	1,600
Average One-Way Haul Distance (m)	1,300
Productivity (tonnes per hour, 40 t Truck)	160
tonnes per day	3,200
Number of Trucks Required	1

Production

Section	Vertical Stope Height (m)	Number of Lifts	Metres
6600	40	8	400
6650	90	18	900
6700	40	8	400
6750	120	24	1,200
6800	40	8	400
6850	60	12	600
6900	40	8	400
6950	50	10	500
7000	50	10	500
7050	80	16	800
7100	30	6	300
7150	50	10	500
7200	50	10	500
7250	100	20	1,000
7300	40	8	400
Subtotal			8,800
Number of Rounds			2,200
Number of Crew-Shifts			1,467
Number of Crew-Days			730
Days of Mill Production (U/G Ore)			850
Number of Production Jumbos Required			1

Ground Control Requirements

Horizontal Metres of Support Required	
Development	3,680
Production	8,800
Subtotal	12,480
per Year	5,140
Bolts per Metre	4
Bolts per Year	21,000
Years in Production	2 5/12
Starting Year	6 10/12

Underground Production Schedule

	Year 1	Year 2	Year 3	Year 4	Year 5	Year 6	Year 7	Year 8	Year 9	Year 10	Year 11	Year 12
Portion of Year in Production						2/12	1	1	3/12	0	0	0
Diluted Ore (Tonnes)	-	-	-	-	-	80,000	473,000	473,000	124,000	-	-	-
Cumulative	-	-	-	-	-	*80,000*	*553,000*	*1,026,000*	*1,150,000*	*1,150,000*	*1,150,000*	*1,150,000*
m^3					-	*28,000*	*163,000*	*163,000*	*43,000*	-	-	-
Grade (Diluted, %):												
Zinc	5.7%	5.7%	5.7%	5.7%	5.7%	5.7%	5.7%	5.7%	5.7%	5.7%	5.7%	5.7%
Lead	3.2%	3.2%	3.2%	3.2%	3.2%	3.2%	3.2%	3.2%	3.2%	3.2%	3.2%	3.2%
Waste Rock (m^3)	-	-	-	-	-	6,700	39,400	39,400	10,300	-	-	-
Cumulative	-	-	-	-	-	*6,700*	*46,100*	*85,500*	*95,800*	*95,800*	*95,800*	*95,800*

Revenue

Parameters:	
Dilution	15%
Processing Recovery	
Zinc	90%
Lead	95%
Metal Prices ($US per lb)	
Zinc	1.10
Lead	0.40
Metal Prices ($CAN per tonne)	
Zinc	2,820
Lead	1,030
Concentrate Grades	
Zinc	60%
Lead	75%
Smelter Return for:	
Zinc	85%
Lead	95%

Year-by-Year Revenue

	Year 1 Q4	Year 1 (End)	Year 2	Year 3	Year 4	Year 5	Year 6	Year 7	Year 8	Year 9
Surface Ore:										
Portion of Year in Production	*1/12*	1/12	1	1	1	1	10/12	0	0	0
Diluted Tonnes	*58,000*	58,000	700,000	700,000	700,000	700,000	582,000	-	-	-
Grade (Diluted, %):										
Zinc	*2.87%*	2.87%	2.87%	2.87%	2.87%	2.87%	2.87%	2.87%	2.87%	2.87%
Lead	*1.13%*	1.13%	1.13%	1.13%	1.13%	1.13%	1.13%	1.13%	1.13%	1.13%
Underground Ore:										
Portion of Year in Production	*0*	0	0	0	0	0	2/12	1	1	3/12
Diluted Tonnes	*-*	-	-	-	-	-	80,000	473,000	473,000	124,000
Grade (Diluted, %):										
Zinc	*5.70%*	5.70%	5.70%	5.70%	5.70%	5.70%	5.70%	5.70%	5.70%	5.70%
Lead	*3.20%*	3.20%	3.20%	3.20%	3.20%	3.20%	3.20%	3.20%	3.20%	3.20%
Total Diluted Tonnes	*58,000*	58,000	700,000	700,000	700,000	700,000	662,000	473,000	473,000	124,000
Grade (Diluted, %):										
Zinc	*2.9%*	2.9%	2.9%	2.9%	2.9%	2.9%	3.2%	5.7%	5.7%	5.7%
Lead	*1.1%*	1.1%	1.1%	1.1%	1.1%	1.1%	1.4%	3.2%	3.2%	3.2%
Tonnes of Metal Processed										
Zinc	*1,660*	1,660	20,090	20,090	20,090	20,090	21,260	26,960	26,960	7,070
Lead	*660*	660	7,910	7,910	7,910	7,910	9,140	15,140	15,140	3,970
Tonnes of Metal Recovered										
Zinc	*1,490*	1,490	18,080	18,080	18,080	18,080	19,130	24,260	24,260	6,360
Lead	*630*	630	7,510	7,510	7,510	7,510	8,680	14,380	14,380	3,770
Concentrate Produced (Dry Tonnes)										
Zinc	*2,480*	2,480	30,130	30,130	30,130	30,130	31,880	40,430	40,430	10,600
Lead	*840*	840	10,010	10,010	10,010	10,010	11,570	19,170	19,170	5,030
Tonnes of Metal Returned from Smelter										
Zinc	*1,270*	1,270	15,370	15,370	15,370	15,370	16,260	20,620	20,620	5,410
Lead	*600*	600	7,130	7,130	7,130	7,130	8,250	13,660	13,660	3,580
Metal Prices ($US per tonne)										
Zinc	*2,420*	2,420	2,420	2,420	2,420	2,420	2,420	2,420	2,420	2,420
Lead	*880*	880	880	880	880	880	880	880	880	880
Metal Prices ($US per pound)										
Zinc	*1.10*	*1.10*	*1.10*	*1.10*	*1.10*	*1.10*	*1.10*	*1.10*	*1.10*	*1.10*
Lead	*0.40*	*0.40*	*0.40*	*0.40*	*0.40*	*0.40*	*0.40*	*0.40*	*0.40*	*0.40*
Exchange Rate ($US per $CAN)	*0.86*	0.86	0.86	0.86	0.86	0.86	0.86	0.86	0.86	0.86
Revenue ($CAN)										
Zinc	*$ 3,574,000*	$ 3,574,000	$ 43,250,000	$ 43,250,000	$ 43,250,000	$ 43,250,000	$ 45,755,000	$ 58,024,000	$ 58,024,000	$ 15,223,000
Lead	*$ 614,000*	$ 614,000	$ 7,296,000	$ 7,296,000	$ 7,296,000	$ 7,296,000	$ 8,442,000	$ 13,978,000	$ 13,978,000	$ 3,663,000
Benchmark Smelter Treatment Charges Per Tonne of Dry Concentrate ($CAN):										
Zinc	*$ 200*	*$ 200*	*$ 200*	*$ 200*	*$ 200*	*$ 200*	*$ 200*	*$ 200*	*$ 200*	*$ 200*
Lead	*$ 190*	*$ 190*	*$ 190*	*$ 190*	*$ 190*	*$ 190*	*$ 190*	*$ 190*	*$ 190*	*$ 190*
Smelter Treatment Charges:										
Zinc	*$ 496,000*	$ 496,000	$ 6,026,000	$ 6,026,000	$ 6,026,000	$ 6,026,000	$ 6,376,000	$ 8,086,000	$ 8,086,000	$ 2,120,000
Lead	*$ 160,000*	$ 160,000	$ 1,902,000	$ 1,902,000	$ 1,902,000	$ 1,902,000	$ 2,198,000	$ 3,642,000	$ 3,642,000	$ 956,000
Net Revenue	*$ 3,532,000*	$ 3,532,000	$ 42,618,000	$ 42,618,000	$ 42,618,000	$ 42,618,000	$ 45,623,000	$ 60,274,000	$ 60,274,000	$ 15,810,000
per tonne	*$ 60.80*	*$ 60.80*	*$ 60.90*	*$ 60.90*	*$ 60.90*	*$ 60.90*	*$ 68.90*	*$ 127.40*	*$ 127.40*	*$ 127.50*

Concentrate Trucking

Operating Days per Year	350
Tonnes Processed Per Day	2,000
Diluted Grade	
Zinc	2.81%
Lead	1.11%
Concentrate Grade	
Zinc	60%
Lead	75%
Tonnes of Dry Concentrate per Day	
Zinc	94
Lead	29
Subtotal	123
Moisture Content of Concentrate (by Mass):	
Zinc	8%
Lead	6%
Tonnes of Wet Concentrate per Day	
Zinc	102
Lead	31
Subtotal	133

Productivity

Average Speed (km/h)	50
Capacity (tonnes)	30

Concentrate	Destin.	Distance to Smel-ter (km)	Round Trip Distance	Tonnes per Day	Trips per Day	Kilometres per Day	Travelling Hours per Day
Zinc & Lead	Milford	10	20	133	4.4	88	1.8
Subtotal				133	4.4	88	1.8

Load & Dump Time (hr/trip)	1
(hr/day)	4.4
Rest Hours per Day, per Truck	0
Equipment Availability	95%
Total Trucking Hours per Day	6.2
Available Hours per Day	22.8
Number of Trucks Required[1]	1
Number of Operators Required[2]	1

Owner/Operator

Capital Cost

Tractor (Heavy Duty)[3]	$ 120,000
Trailer	$ 40,000
Total Cost for all Trucks	$ 160,000

Operating Costs

Item		Unit of Measurement	Number of Units	$/Unit	Yearly Cost
Truck Operator[4]		person-yr	1	$ 48,000	$ 48,000
Equipment[3]					
	Fuel	km	30,800	$ 0.42	$ 13,000
	Tires	km	30,800	$ 0.12	$ 4,000
	Maintenance	km	30,800	$ 0.035	$ 1,000
Subtotal					$ 66,000
per tonne-km					$ 0.071

Notes:
1. Rounded up.
2. For 24/7 operation.
3. Estimated by Metro International.
4. Includes burden.

Surface Mine Equipment Fleet

Parameters

Exchange Rate ($US per $CAN)	$ 0.86
Fuel Price ($/L)	$ 0.90
Average SG	2.30
Working Days per Year	350
Working Hours per Day	20
Equipment Availability	95%
Equipment Delivery Lag Time (years)	*9/12*
Lease Rate	7.0%

Capital Costs

Unit	Capital Cost (List Prices) ($US)	($CAN)
345 Excavator	$ 440,000	$ 510,000
365 Excavator	$ 560,000	$ 650,000
385 Excavator	$ 850,000	$ 990,000
769 Haul Truck	$ 540,000	$ 630,000
773 Haul Truck	$ 750,000	$ 870,000
777 Haul Truck	$ 1,030,000	$ 1,200,000
14H Grader	$ 390,000	$ 450,000
980 Wheel Loader	$ 390,000	$ 450,000
D8 Bulldozer	$ 550,000	$ 640,000

Hourly Operating Costs

Unit	Fuel Cnsmptn (L/h)	Fuel Cost	Wear Items: Undercarriage: Undercarriage Cost	Wear Items: Tires: Tire Life (Hours)	Wear Items: Tires: Tire Cost (per)	Wear Items: Tires: Number of Tires	Wear Items: Tires: Tire Cost	Planned Maint. Cost	Unplanned Repair Cost	Equipment Life (Hours)	Financing Charges	Residual Value	Replacement Cost per Hour	Operator Cost per Hour	Total Hourly Operating Cost
345 Excavator	42	$ 38	$ 3.90					$ 8.00	$ 10.40	12,000	$ 3.00	35%	$ 28	$ 24	$ 115
365 Excavator	55	$ 50	$ 4.60					$ 10.00	$ 13.00	12,000	$ 3.80	35%	$ 35	$ 24	$ 140
385 Excavator	68	$ 61	$ 4.80					$ 12.00	$ 15.60	12,000	$ 5.80	35%	$ 54	$ 24	$ 177
769 Haul Truck	40	$ 36		4,000	$ 6,000	6	$ 9.00	$ 3.00	$ 5.00	12,000	$ 3.70	42%	$ 30	$ 24	$ 111
773 Haul Truck	53	$ 48		4,000	$ 7,000	6	$ 10.50	$ 4.00	$ 6.00	12,000	$ 5.10	42%	$ 42	$ 24	$ 140
777 Haul Truck	74	$ 67		4,000	$ 8,000	6	$ 12.00	$ 5.00	$ 7.00	12,000	$ 7.00	42%	$ 58	$ 24	$ 180
14H Grader	26	$ 23		3,000	$ 4,000	6	$ 8.00	$ 10.00	$ 14.00	12,000	$ 2.60	42%	$ 22	$ 24	$ 104
980 Wheel Loader	30	$ 27		3,000	$ 6,000	4	$ 8.00	$ 10.00	$ 14.00	12,000	$ 2.60	42%	$ 22	$ 24	$ 108
D8 Bulldozer	41	$ 37	$ 9.50					$ 10.00	$ 13.00	12,000	$ 3.70	40%	$ 32	$ 24	$ 129

Yearly Operating Costs

	Year 1	Year 2	Year 3	Year 4	Year 5	Year 6	Year 7	Year 8
Portion of Year in Production	*3/12*	*1*	*1*	*1*	*1*	*10/12*	*0*	*0*
345 Excavator	$ 201,000	$ 805,000	$ 805,000	$ 805,000	$ 805,000	$ 668,000	$ -	$ -
385 Excavator	$ 310,000	$ 1,239,000	$ 1,239,000	$ 1,239,000	$ 1,239,000	$ 1,028,000	$ -	$ -
773 Haul Truck	$ 245,000	$ 980,000	$ 980,000	$ 980,000	$ 980,000	$ 813,000	$ -	$ -
Number in Fleet	*3*	*3.5*	*4*	*4*	*4*	*4*	*4*	*4*
Fleet Cost	$ 735,000	$ 3,430,000	$ 3,920,000	$ 3,920,000	$ 3,920,000	$ 3,252,000	$ -	$ -
14H Grader[1]	$ 91,000	$ 364,000	$ 364,000	$ 364,000	$ 364,000	$ 302,000	$ -	$ -
980 Wheel Loader	$ 189,000	$ 756,000	$ 756,000	$ 756,000	$ 756,000	$ 627,000	$ -	$ -
D8 Bulldozer	$ 226,000	$ 903,000	$ 903,000	$ 903,000	$ 903,000	$ 749,000	$ -	$ -
Subtotal	$ 1,796,000	$ 7,672,000	$ 8,162,000	$ 8,162,000	$ 8,162,000	$ 6,771,000	$ -	$ -

Notes:
1. Operates day shift only.
2. Owning and operating costs calculated with input from Ian Palmeter, Atlantic Tractors & Equipment, Halifax.

Operating Costs

General Parameters

Working Days per Year		350
Tonnes Processed per Day		2,000
Per Year		700,000
Working Hours per Day		20
per Year		7,000
Tonnes of Flotation Concentrate per Year		43,038
Power Cost ($/kWh)	$	0.047
Demand Charge ($/kVA-month)	$	8.01
Blasting Supplies (Underground):		
Powder (cost per kg, average)	$	1.00
Powder Factor (kg/m^3)		0.5
Caps (cost per)	$	2.00
Caps (number per m^3)		1.0

Overhead Costs

Item	Pieces of Equipment	Unit of Measurement	Number of Units	$/Unit	Yearly Cost
Office and General					100,000
Professional Fees					150,000
Investor Relations					100,000
Permitting					15,000
Travel and Entertainment					200,000
Labour					1,000,000
Shop/Office Electricity		month	12	2,000	24,000
Office & Shop Heat		sq ft	6,000	5.00	30,000
Shop Equipment		yr	1	10,000	10,000
Subtotal					1,629,000
Per tonne of Ore Mined					2.30

Support Costs

Dewatering					
Maintenance		hr	8,400	2.00	17,000
Power[5]		kWh/yr	1,752,000	0.08	140,000
Pickup Trucks		yr	4	5,000	20,000
Labour		yr			500,000
Subtotal					677,000
Per tonne of Ore Mined					1.00

Processing Costs

Item	Pieces of Equipment	Unit of Measurement	Number of Units	$/Unit	Yearly Cost
Electricity		per tonne	700,000	1.61	1,120,000
Demand Charge		kVA/month	2,700	8.01	260,000
Maintenance Supplies		tonne	700,000	0.75	525,000
Rods, Balls & Liners		tonne	700,000	0.66	463,000
Flotation Reagents		tonne	700,000	0.55	385,000
Tailings Disposal		tonne	700,000	0.20	140,000
Concentrate Dryer Fuel					
Zinc Concentrate		$tonne_{conc.}$	32,730	4.65	152,000
Lead Concentrate		$tonne_{conc.}$	10,310	3.03	31,000
Mill Heating		per day	120	3,000	360,000
Concentrate Shipping:					
Truck to Milford Siding		per year	1	66,000	66,000
Rail Cargo:					
Zinc to Valleyfield		$tonne_{conc.}$	35,700	36.50	1,303,000
Lead to Belledune		$tonne_{conc.}$	10,850	24.20	263,000
Labour[2]					1,617,000
Subtotal					6,685,000
Per tonne of Ore Mined					9.60

w/o shipping:	5,053,000
	7.22

Surface Mining Costs

Item	Pieces of Equipment	Unit of Measurement	Number of Units	$/Unit	Yearly Cost
Mining Costs					
Drilling and Blasting					
Ore		tonne	700,000	1.25	875,000
Waste Rock[4]		tonne	617,000	1.25	771,000
Loading & Hauling		tonne	6,233,000	1.30	8,017,000
Subtotal (Average, per Year)					9,663,000
Per tonne of Ore Mined					13.80

Underground Mining Costs

Item	Pieces of Equipment	Unit of Measurement	Number of Units	$/Unit	Yearly Cost
Drill Jumbo (Two Boom)	1	hour	7,000	55.00	385,000
Drill Jumbo (Single Boom)	1	hour	7,000	40.00	280,000
Scooptram (6 yd)	1	hour	7,000	80.00	560,000
Scooptram (3 yd)	1	hour	7,000	60.00	420,000
Scooptram (5 yd)	1	hour	7,000	80.00	560,000
U/G Haul Truck (40 tonne)	1	hour	7,000	60.00	420,000
Scissor Lift	1	hour	7,000	20.00	140,000
Boom Truck	1	hour	7,000	20.00	140,000
Front-end Loader (Mill)	1	hour	7,000	108.00	756,000
Tractors	5	hour	1,750	10.00	90,000
Compressor	1	hour	7,000	35.00	245,000
Main Fan	1	hour	8,760	6.00	53,000
Auxiliary Fans	4	hour	7,000	2.00	56,000
Jack-leg Drills	15	hour	7,000	0.20	21,000
Stopers	15	hour	7,000	0.20	21,000
Slushers	4	hour	7,000	0.40	11,000
Diamond Drill	1	hour	7,000	4.00	28,000
Alimak Raise Climber	1	hour	7,000	20.00	140,000
Pumps	4	hour	7,000	2.00	56,000
Rock Breaker (On 5 yd Scoop)	1	hour	1,750	5.00	9,000
Underground Electrical	1	hour	7,000	0.71	5,000
Pipe (Water, Air)	1	year	1	10,000	10,000
Mine Rescue Equipment	1	year	1	4,000	4,000
Technical Equipment	1	year	1	2,000	2,000
Communication System	1	year	1	3,000	3,000
Rock Bolts	1	bolt	21,000	10	210,000
Fill Mixing Plant	1	hour	7,000	14.00	98,000
Cement	1	tonne	21,000	180	3,780,000
Miscellaneous Equipment	1	year	1	27,000	27,000
Labour	1	year	1	5,527,000	5,527,000
Subtotal					14,057,000
Per tonne of Ore Mined					29.70

Yearly Operating Costs

	Year 1 Q1	Year 1 Q2	Year 1 Q3	Year 1 Q4	Year 1	Year 2	Year 3	Year 4	Year 5	Year 6	Year 7	Year 8	Year 9
Surface:													
Portion of Year in Operation													
Stripping				3/12	3/12	1	1	1	1	10/12	0	0	0
Ore Production				1/12	1/12	1	1	1	1	10/12	0	0	0
Drilling and Blasting													
Ore				73,000	73,000	875,000	875,000	875,000	875,000	728,000	-	-	-
per tonne				1.25	1.25	1.25	1.25	1.25	1.25	1.25	-	-	-
Waste Rock				-	-	688,000	813,000	938,000	1,063,000	800,000	-	-	-
per tonne				1.25	1.25	1.25	1.25	1.25	1.25	1.25	-	-	-
Loading and Hauling (Ore, Waste Rock & Stripping)				1,796,000	1,796,000	7,672,000	8,162,000	8,162,000	8,162,000	6,771,000	-	-	-
per tonne				0.87	0.87	0.99	1.11	1.17	1.25	1.23	-	-	-
Support				169,000	169,000	677,000	677,000	677,000	677,000	562,000	-	-	-
per tonne				0.09	0.09	0.09	0.08	0.08	0.08	0.08	-	-	-
Subtotal (Surface Mining)				2,038,000	2,038,000	9,912,000	10,527,000	10,652,000	10,777,000	8,861,000	-	-	-
per tonne of ore & waste				1.00	1.00	1.30	1.40	1.50	1.60	1.60	-	-	-
per tonne of ore				35.10	35.10	14.20	15.00	15.20	15.40	15.20	-	-	-
Underground Mining:													
Portion of Year in Operation					0	0	0	0	0	2/12	1	1	3/12
Operating Cost (Excluding Blasting)					-	-	-	-	-	2,390,000	14,057,000	14,057,000	3,685,000
Blasting Cost:													
Ore					-	-	-	-	-	67,000	391,000	391,000	103,000
per m^3					2.40	2.40	2.40	2.40	2.40	2.40	2.40	2.40	2.40
Waste Rock					-	-	-	-	-	16,000	95,000	95,000	25,000
per m^3					2.40	2.40	2.40	2.40	2.40	2.40	2.40	2.40	2.40
Support					-	-	-	-	-	115,000	677,000	677,000	177,000
Subtotal, Underground Mining					-	-	-	-	-	2,588,000	15,220,000	15,220,000	3,990,000
per tonne of ore & waste					-	-	-	-	-	26.50	26.40	26.40	26.40
per tonne of ore					-	-	-	-	-	32.40	32.20	32.20	32.20
Subtotal, Surface and Underground Mining				2,038,000	2,038,000	9,912,000	10,527,000	10,652,000	10,777,000	11,449,000	15,220,000	15,220,000	3,990,000
per tonne of ore & waste				1.00	1.00	1.30	1.40	1.50	1.60	2.00	26.40	26.40	26.40
per tonne of ore				35.10	35.10	14.20	15.00	15.20	15.40	17.30	32.20	32.20	32.20
Processing													
Portion of Year in Operation				1/12	1/12	1	1	1	1	1	1	1	3/12
Processing Cost				557,000	557,000	6,685,000	6,685,000	6,685,000	6,685,000	6,685,000	6,685,000	6,685,000	1,753,000
per tonne of ore				9.60	9.60	9.60	9.60	9.60	9.60	10.10	14.10	14.10	14.10

	Year 1 Q1	Year 1 Q2	Year 1 Q3	Year 1 Q4	Year 1	Year 2	Year 3	Year 4	Year 5	Year 6	Year 7	Year 8	Year 9
Overhead													
Portion of Year in Operation			3/12	3/12	6/12	1	1	1	1	1	1	1	6/12
Overhead Cost			407,000	407,000	815,000	1,629,000	1,629,000	1,629,000	1,629,000	1,629,000	1,629,000	1,629,000	834,000
per tonne of ore and waste			-	0.23	0.45	0.21	0.20	0.20	0.20	0.24	-	-	-
per tonne of ore			-	7.00	14.10	2.30	2.30	2.30	2.30	2.50	3.40	3.40	6.70
Total, Operating Costs			407,000	3,002,000	3,410,000	18,226,000	18,841,000	18,966,000	19,091,000	19,763,000	23,534,000	23,534,000	6,577,000
per tonne of ore			$ -	$ 51.80	$ 58.80	$ 26.00	$ 26.90	$ 27.10	$ 27.30	$ 29.90	$ 49.80	$ 49.80	$ 53.00

Notes:
2. Factored value.
3. Includes owning and operator costs.
4. Average waste rock mined.
5. Two Flygt BIBO 2400's operating continuously at 4000 gpm, price includes demand charge.

Accounting Income

Initial Capital Costs

Scozinc Purchase Price	$ 7,500,000
Savage 2% NSR Royalty Purchase	$ 1,450,000
Capital Costs	$ 2,931,000
Initial Working Capital[6]	$ 11,100,000
Percentage Debt Financing	67%
Total Financing Required	$ 22,981,000
Debt	*$ 15,481,000*
Equity	*$ 7,500,000*

Schedule for Initial Capital Outlay

Multiplying Factor: 100%

	Year 1 (Beginning)	***Year 1 Q3***	***Year 1 Q4***	Year 1 (End)	Year 2	Year 3	Year 4	Year 5	Year 6	Year 7	Year 8	Year 9
General		*$ 320,000*										
Mine Site		*$ 203,000*			$ 95,000							
Processing Plant		*$ 2,408,000*										
Underground				$ -	$ -	$ -	$ -	$ -	$ 5,582,000	$ -	$ -	$ -
Subtotal	$ -	*$ 2,931,000*	*$ -*	$ -	$ 95,000	$ -	$ -	$ -	$ 5,582,000	$ -	$ -	$ -
Tonnes of Ore Mined			*58,000*	58,000	700,000	700,000	700,000	700,000	662,000	473,000	473,000	124,000

Revenue

Revenue[4]			*$ 3,532,000*	$ 3,532,000	$ 42,618,000	$ 42,618,000	$ 42,618,000	$ 42,618,000	$ 45,623,000	$ 60,274,000	$ 60,274,000	$ 15,810,000
Subtotal			*$ 3,532,000*	$ 3,532,000	$ 42,618,000	$ 42,618,000	$ 42,618,000	$ 42,618,000	$ 45,623,000	$ 60,274,000	$ 60,274,000	$ 15,810,000
Per Tonne of Ore			*$ 60.90*	*$ 60.90*	*$ 60.90*	*$ 60.90*	*$ 60.90*	*$ 60.90*	*$ 68.90*	*$ 127.40*	*$ 127.40*	*$ 127.50*

Royalties Paid

Nova Scotia Government (2 %)[9]			*$ 68,000*	$ 68,000	$ 820,000	$ 820,000	$ 820,000	$ 820,000	$ 880,000	$ 1,173,000	$ 1,173,000	$ 308,000
Subtotal			*$ 68,000*	$ 68,000	$ 820,000	$ 820,000	$ 820,000	$ 820,000	$ 880,000	$ 1,173,000	$ 1,173,000	$ 308,000

Direct Operating Costs[1]

Multiplying Factor: 100%

	Year 1 (Beginning)	***Year 1 Q3***	***Year 1 Q4***	Year 1 (End)	Year 2	Year 3	Year 4	Year 5	Year 6	Year 7	Year 8	Year 9
Mining Costs			*$ 2,038,000*	*$ 2,038,000*	*$ 9,912,000*	*$ 10,527,000*	*$ 10,652,000*	*$ 10,777,000*	*$ 11,449,000*	*$ 15,220,000*	*$ 15,220,000*	*$ 3,990,000*
Processing Costs			*$ 557,000*	*$ 557,000*	*$ 6,685,000*	*$ 6,685,000*	*$ 6,685,000*	*$ 6,685,000*	*$ 6,685,000*	*$ 6,685,000*	*$ 6,685,000*	*$ 1,753,000*
Subtotal			*$ 2,595,000*	$ 2,595,000	$ 16,597,000	$ 17,212,000	$ 17,337,000	$ 17,462,000	$ 18,134,000	$ 21,905,000	$ 21,905,000	$ 5,743,000
Per Tonne of Ore			*$ 44.70*	*$ 44.70*	*$ 23.80*	*$ 24.60*	*$ 24.80*	*$ 25.00*	*$ 27.40*	*$ 46.30*	*$ 46.30*	*$ 46.30*
Mining Costs per Tonne of Ore:	*$ -*	*$ -*	*$ 35.10*	*$ 35.10*	*$ 14.20*	*$ 15.00*	*$ 15.20*	*$ 15.40*	*$ 17.30*	*$ 32.20*	*$ 32.20*	*$ 32.20*
Processing Costs per Tonne of Ore:	*$ -*	*$ -*	*$ 9.60*	*$ 9.60*	*$ 9.60*	*$ 9.60*	*$ 9.60*	*$ 9.60*	*$ 10.10*	*$ 14.10*	*$ 14.10*	*$ 14.10*

Operating Cash Flow

Revenue	$ -		*$ 3,532,000*	$ 3,532,000	$ 42,618,000	$ 42,618,000	$ 42,618,000	$ 42,618,000	$ 45,623,000	$ 60,274,000	$ 60,274,000	$ 15,810,000
Royalties Paid	$ -		*$ 68,000*	$ 68,000	$ 820,000	$ 820,000	$ 820,000	$ 820,000	$ 880,000	$ 1,173,000	$ 1,173,000	$ 308,000
Direct Operating Costs	$ -		*$ 2,595,000*	$ 2,595,000	$ 16,597,000	$ 17,212,000	$ 17,337,000	$ 17,462,000	$ 18,134,000	$ 21,905,000	$ 21,905,000	$ 5,743,000
Subtotal	$ -		*$ 869,000*	$ 869,000	$ 25,201,000	$ 24,586,000	$ 24,461,000	$ 24,336,000	$ 26,609,000	$ 37,196,000	$ 37,196,000	$ 9,759,000
Per Tonne of Ore	*$ -*		*$ 15.00*	*$ 15.00*	*$ 36.00*	*$ 35.10*	*$ 34.90*	*$ 34.80*	*$ 40.20*	*$ 78.60*	*$ 78.60*	*$ 78.70*

Overhead Costs

Overhead		*$ 407,000*	*$ 407,000*	$ 815,000	$ 1,629,000	$ 1,629,000	$ 1,629,000	$ 1,629,000	$ 1,629,000	$ 1,629,000	$ 1,629,000	$ 834,000
Subtotal	$ -	*$ 407,000*	*$ 407,000*	$ 815,000	$ 1,629,000	$ 1,629,000	$ 1,629,000	$ 1,629,000	$ 1,629,000	$ 1,629,000	$ 1,629,000	$ 834,000
Per Tonne of Ore		*$ -*	*$ 7.00*	*$ 14.10*	*$ 2.30*	*$ 2.30*	*$ 2.30*	*$ 2.30*	*$ 2.50*	*$ 3.40*	*$ 3.40*	*$ 6.70*

Net Operating Income (Gross Margin)

	Year 1 (Beginning)	***Year 1 Q3***	***Year 1 Q4***	Year 1 (End)	Year 2	Year 3	Year 4	Year 5	Year 6	Year 7	Year 8	Year 9
Operating Cash Flow	$ -	*$ -*	*$ 869,000*	$ 869,000	$ 25,201,000	$ 24,586,000	$ 24,461,000	$ 24,336,000	$ 26,609,000	$ 37,196,000	$ 37,196,000	$ 9,759,000
Overhead Costs	$ -	*$ 407,000*	*$ 407,000*	$ 815,000	$ 1,629,000	$ 1,629,000	$ 1,629,000	$ 1,629,000	$ 1,629,000	$ 1,629,000	$ 1,629,000	$ 834,000
Net Operating Income (Gross Margin)	$ -	*-$ 407,000*	*$ 462,000*	$ 54,000	$ 23,572,000	$ 22,957,000	$ 22,832,000	$ 22,707,000	$ 24,980,000	$ 35,567,000	$ 35,567,000	$ 8,925,000
Per Tonne of Ore	*n/a*	*$ -*	*$ 8.00*	*$ 0.90*	*$ 33.70*	*$ 32.80*	*$ 32.60*	*$ 32.40*	*$ 37.70*	*$ 75.20*	*$ 75.20*	*$ 72.00*

Taxes and Interest

Net Operating Income (Gross Margin)	$ -	*-$ 407,000*	*$ 462,000*	$ 54,000	$ 23,572,000	$ 22,957,000	$ 22,832,000	$ 22,707,000	$ 24,980,000	$ 35,567,000	$ 35,567,000	$ 8,925,000
Minus Loss Carried Forward	$ -	*$ -*	*$ -*	$ -	$ 1,305,000	$ -	$ -	$ -	$ -	$ -	$ -	$ -
Capital Cost Allowance Deduction	$ -	*$ -*	*$ -*	$ 54,000	$ 2,972,000	$ -	$ -	$ -	$ 5,582,000	$ -	$ -	$ -
Resource Allowance Deduction	$ -	*$ -*	*$ -*	$ 221,000	$ 5,762,000	$ 6,352,000	$ 6,320,000	$ 6,289,000	$ 5,477,000	$ 9,592,000	$ 9,592,000	$ 2,517,000
Interest Expenses	$ -	*$ -*	*$ -*	$ 1,084,000	$ 1,084,000	$ 232,000	$ -	$ -	$ -	$ -	$ -	$ -
Taxable Income	$ -	*-$ 407,000*	*$ 462,000*	-$ 1,305,000	$ 12,449,000	$ 16,373,000	$ 16,512,000	$ 16,418,000	$ 13,921,000	$ 25,975,000	$ 25,975,000	$ 6,408,000
Federal Income Tax (29.12 %)				$ -	$ 3,625,000	$ 4,768,000	$ 4,808,000	$ 4,781,000	$ 4,054,000	$ 7,564,000	$ 7,564,000	$ 1,866,000
Nova Scotia Income Tax (16 %)				$ -	$ 1,992,000	$ 2,620,000	$ 2,642,000	$ 2,627,000	$ 2,227,000	$ 4,156,000	$ 4,156,000	$ 1,025,000
Total Income Tax Payable				$ -	$ 5,617,000	$ 7,388,000	$ 7,450,000	$ 7,408,000	$ 6,281,000	$ 11,720,000	$ 11,720,000	$ 2,891,000

Net Income After Interest and Taxes

Net Operating Income (Gross Margin)	$ -	*-$ 407,000*	*$ 462,000*	$ 54,000	$ 23,572,000	$ 22,957,000	$ 22,832,000	$ 22,707,000	$ 24,980,000	$ 35,567,000	$ 35,567,000	$ 8,925,000
Total Income Tax Payable	$ -	*$ -*	*$ -*	$ -	$ 5,617,000	$ 7,388,000	$ 7,450,000	$ 7,408,000	$ 6,281,000	$ 11,720,000	$ 11,720,000	$ 2,891,000
Interest on Capital	$ -	*$ -*	*$ -*	$ 1,084,000	$ 1,084,000	$ 232,000	$ -	$ -	$ -	$ -	$ -	$ -
Net Income After Interest and Taxes	$ -	*-$ 407,000*	*$ 462,000*	-$ 1,030,000	$ 16,871,000	$ 15,337,000	$ 15,382,000	$ 15,299,000	$ 18,699,000	$ 23,847,000	$ 23,847,000	$ 6,034,000

Present Value of Net Income	Year 1 (Beginning)	***Year 1 Q3***	***Year 1 Q4***	Year 1 (End)	Year 2	Year 3	Year 4	Year 5	Year 6	Year 7	Year 8	Year 9
Net Income After Interest and Taxes	$ -	-$ 407,000	$ 462,000	-$ 1,030,000	$ 16,871,000	$ 15,337,000	$ 15,382,000	$ 15,299,000	$ 18,699,000	$ 23,847,000	$ 23,847,000	$ 6,034,000
Less Scozinc Purchase Price	$ 7,500,000											
Less Pasminco Royalty Purchase	$ 50,000			$ 1,400,000								
Less Initial Capital Costs	$ 2,931,000			$ -	$ -	$ -	$ -	$ -	$ -	$ -	$ -	$ -
Less Capital Additions	$ -			$ -	$ 95,000	$ -	$ -	$ -	$ 5,582,000	$ -	$ -	$ -
Subtotal	-$ 10,481,000	-$ 407,000	$ 462,000	-$ 2,430,000	$ 16,776,000	$ 15,337,000	$ 15,382,000	$ 15,299,000	$ 13,117,000	$ 23,847,000	$ 23,847,000	$ 6,034,000
Cumulative	-$ 10,481,000			-$ 12,856,000	$ 3,920,000	$ 19,257,000	$ 34,639,000	$ 49,938,000	$ 63,055,000	$ 86,902,000	$ 110,749,000	$ 116,783,000

$NPV_{7.5\%}$	$ 75,687,000
$NPV_{8.0\%}$	$ 73,628,000
$NPV_{10.0\%}$	$ 66,028,000
$NPV_{12.5\%}$	$ 57,789,000
$NPV_{15.0\%}$	$ 50,723,000
Internal Rate of Return (IRR)	76%

Overall Cash Flow

Net Income After Interest and Taxes	$ -	-$ 407,000	$ 462,000	-$ 1,030,000	$ 16,871,000	$ 15,337,000	$ 15,382,000	$ 15,299,000	$ 18,699,000	$ 23,847,000	$ 23,847,000	$ 6,034,000
Capital Additions (Recurring Capital)	$ -	$ -	$ -	$ -	$ 95,000	$ -	$ -	$ -	$ 5,582,000	$ -	$ -	$ -
Debt Financing Repayment	$ -	$ -	$ -	$ -	$ 12,161,000	$ 3,320,000	$ -	$ -	$ -	$ -	$ -	$ -
Distributed Cash Flow[8]	$ -	-$ 407,000	$ 462,000	-$ 1,030,000	$ 4,615,000	$ 12,017,000	$ 15,382,000	$ 15,299,000	$ 13,117,000	$ 23,847,000	$ 23,847,000	$ 6,034,000
Cumulative Cash Flow	*$ -*	*-$ 407,000*	*$ 55,000*	*-$ 975,000*	*$ 3,640,000*	*$ 15,657,000*	*$ 31,039,000*	*$ 46,338,000*	*$ 59,455,000*	*$ 83,302,000*	*$ 107,149,000*	*$ 113,183,000*

Tax Calculations Capital Cost Allowance Accelerated Rate (100 %)	Year 1 (Beginning)	***Year 1*** ***Q3***	***Year 1*** ***Q4***	Year 1 (End)	Year 2	Year 3	Year 4	Year 5	Year 6	Year 7	Year 8	Year 9
Beginning Balance	$ -			$ -	$ 2,877,000	$ -	$ -	$ -	$ -	$ -	$ -	$ -
Additions	$ -			$ 2,931,000	$ 95,000	$ -	$ -	$ -	$ 5,582,000	$ -	$ -	$ -
Allowable Deduction[2]	$ -			$ 2,931,000	$ 2,972,000	$ -	$ -	$ -	$ 5,582,000	$ -	$ -	$ -
Deduction Taken	$ -			$ 54,000	$ 2,972,000	$ -	$ -	$ -	$ 5,582,000	$ -	$ -	$ -
Ending Balance	$ -			$ 2,877,000	$ -	$ -	$ -	$ -	$ -	$ -	$ -	$ -
Resource Allowance												
Revenue				$ 3,532,000	$ 42,618,000	$ 42,618,000	$ 42,618,000	$ 42,618,000	$ 45,623,000	$ 60,274,000	$ 60,274,000	$ 15,810,000
Expenses and Deductions												
Operating Costs				*$ 2,595,000*	*$ 16,597,000*	*$ 17,212,000*	*$ 17,337,000*	*$ 17,462,000*	*$ 18,134,000*	*$ 21,905,000*	*$ 21,905,000*	*$ 5,743,000*
Capital Cost Allowance				*$ 54,000*	*$ 2,972,000*	*$ -*	*$ -*	*$ -*	*$ 5,582,000*	*$ -*	*$ -*	*$ -*
Subtotal, Expenses				$ 2,649,000	$ 19,569,000	$ 17,212,000	$ 17,337,000	$ 17,462,000	$ 23,716,000	$ 21,905,000	$ 21,905,000	$ 5,743,000
Resource Profits				$ 883,000	$ 23,049,000	$ 25,406,000	$ 25,281,000	$ 25,156,000	$ 21,907,000	$ 38,369,000	$ 38,369,000	$ 10,067,000
Earned Depletion Allowance[13]				$ 221,000	$ 5,762,000	$ 6,352,000	$ 6,320,000	$ 6,289,000	$ 5,477,000	$ 9,592,000	$ 9,592,000	$ 2,517,000
Debt Financing												
Opening Debt Balance[7]	$ 15,481,000			$ 15,481,000	$ 15,481,000	$ 3,320,000	$ -	$ -	$ -	$ -	$ -	$ -
Net Income After Interest and Taxes	$ -			-$ 1,030,000	$ 16,871,000	$ 15,337,000	$ 15,382,000	$ 15,299,000	$ 18,699,000	$ 23,847,000	$ 23,847,000	$ 6,034,000
Working Capital Required[12]				$ 4,557,000	$ 4,710,000	$ 4,742,000	$ 4,773,000	$ 4,941,000	$ 5,884,000	$ 5,884,000	$ 1,644,000	$ -
Debt Repayment[7]	$ -			$ -	$ 12,161,000	$ 3,320,000	$ -	$ -	$ -	$ -	$ -	$ -
Closing Debt Balance	$ 15,481,000			$ 15,481,000	$ 3,320,000	$ -	$ -	$ -	$ -	$ -	$ -	$ -

Notes:
1. Considering pre-production requirements (pre-stripping).
2. Allowable deduction, under ACCA, is up to 100 % of taxable income.
4. Net Smelter Return.
6. Minimum cash balance during start-up, plus contingency.
7. Proportion of debt capital paid back reflects the overall proportion of debt financing.
8. The Board of Directors may choose to pay out a portion of this figure as dividends.
9. Royalty is a percentage of Net Revenue (after smelting charges and concentrate shipping costs have been deducted.
10. Royalties are a percentage of net revenue (after smelting charges have been deducted).
11. After capital repayment.
12. Three months operating expenses.
13. 25 % of Resource Profits.

Cash Flow

Capital Costs

	Month 1	Month 2	Month 3	Month 4	Month 5	Month 6	Month 7	Month 8	Month 9	Month 10	Month 11	Month 12	Month 13
General						$ 64,000	$ 64,000	$ 64,000	$ 64,000	$ 64,000			
Mine Site						$ 41,000	$ 41,000	$ 41,000	$ 41,000	$ 41,000			
Processing Plant						$ 482,000	$ 482,000	$ 482,000	$ 482,000	$ 482,000			
Purchase Pasminco Royalty												$ 1,450,000	
Underground						$ -	$ -	$ -	$ -	$ -			
						$ -	$ -	$ -	$ -	$ -			
Subtotal						$ 587,000	$ 587,000	$ 587,000	$ 587,000	$ 587,000		$ 1,450,000	
Tonnes of Ore Mined												58,000	58,000

Revenue

Revenue[4]													
Subtotal													

Royalties Paid[10]

Nova Scotia Government (2 %)													
Subtotal													

Direct Operating Costs[1]

	Month 1	Month 2	Month 3	Month 4	Month 5	Month 6	Month 7	Month 8	Month 9	Month 10	Month 11	Month 12	Month 13
Mining Costs										679,000	679,000	679,000	$ 826,000
Processing Costs												557,000	$ 557,000
Subtotal										679,000	679,000	1,236,000	$ 1,383,000

Operating Cash Flow

Revenue										$ -	$ -	$ -	$ -
Royalties Paid										$ -	$ -	$ -	$ -
Direct Operating Costs										$ 679,000	$ 679,000	$ 1,236,000	$ 1,383,000
Subtotal										-$ 679,000	-$ 679,000	-$ 1,236,000	-$ 1,383,000

Overhead Costs

Overhead						$ 136,000	$ 136,000	$ 136,000	$ 136,000	$ 136,000	$ 136,000	$ 136,000	$ 136,000
Subtotal						136,000	136,000	$ 136,000	$ 136,000	$ 136,000	$ 136,000	$ 136,000	$ 136,000

Net Operating Income (Gross Margin)

Operating Cash Flow						$ -	$ -	$ -	$ -	-$ 679,000	-$ 679,000	-$ 1,236,000	-$ 1,383,000
Overhead Costs						$ 136,000	$ 136,000	$ 136,000	$ 136,000	$ 136,000	$ 136,000	$ 136,000	$ 136,000
Net Operating Income (Gross Margin)						-$ 136,000	-$ 136,000	-$ 136,000	-$ 136,000	-$ 815,000	-$ 815,000	-$ 1,372,000	-$ 1,519,000

Initial Working Capital Requirement

Cumulative Net Operating Income	$ -	$ -	$ -	$ -	$ -	-$ 136,000	-$ 272,000	-$ 408,000	-$ 544,000	-$ 1,359,000	-$ 2,174,000	-$ 3,546,000	-$ 5,065,000
Minimum Cash Balance	-$ 5,065,000												
Contingency[3]	$ 6,076,000												
Initial Working Capital[5]	$ 11,141,000												

Notes:
1. Considering pre-production requirements (pre-stripping).
3. Four months operating costs.
4. Net Smelter Return
5. Equal to absolute value of minimum cash balance plus contingency.
10. Royalties are a percentage of net revenue (after smelting charges have been deducted).

Cash Flow

Capital Costs

	Month 14	Month 15	Month 16	Month 17	Month 18	Month 19	Month 20	Month 21	Month 22	Month 23	Month 24
General											
Mine Site					$ 95,000						
Processing Plant											
Purchase Pasminco Royalty											
Underground											
Subtotal					$ 95,000						
Tonnes of Ore Mined	58,000	58,000	58,000	58,000	58,000	58,000	58,000	58,000	58,000	58,000	58,000
Revenue											
Revenue[4]	1,509,000	4,084,000	3,552,000	3,552,000	3,552,000	3,552,000	3,552,000	3,552,000	3,552,000	3,552,000	3,552,000
Subtotal	1,776,000	3,552,000	3,552,000	3,552,000	3,552,000	3,552,000	3,552,000	3,552,000	3,552,000	3,552,000	3,552,000
Royalties Paid[10]											
Nova Scotia Government (2 %)		*$ 273,000*			*$ 205,000*			*$ 205,000*			*$ 205,000*
Subtotal		*$ 273,000*			*$ 205,000*			*$ 205,000*			*$ 205,000*

Direct Operating Costs[1]

	Month 14	Month 15	Month 16	Month 17	Month 18	Month 19	Month 20	Month 21	Month 22	Month 23	Month 24
Mining Costs	$ 826,000	$ 826,000	$ 826,000	$ 826,000	$ 826,000	$ 826,000	$ 826,000	$ 826,000	$ 826,000	$ 826,000	$ 826,000
Processing Costs	$ 557,000	$ 557,000	$ 557,000	$ 557,000	$ 557,000	$ 557,000	$ 557,000	$ 557,000	$ 557,000	$ 557,000	$ 557,000
Subtotal	$ 1,383,000	$ 1,383,000	$ 1,383,000	$ 1,383,000	$ 1,383,000	$ 1,383,000	$ 1,383,000	$ 1,383,000	$ 1,383,000	$ 1,383,000	$ 1,383,000
Operating Cash Flow											
Revenue	$ 1,776,000	$ 3,552,000	$ 3,552,000	$ 3,552,000	$ 3,552,000	$ 3,552,000	$ 3,552,000	$ 3,552,000	$ 3,552,000	$ 3,552,000	$ 3,552,000
Royalties Paid	$ -	$ 273,000	$ -	$ -	$ 205,000	$ -	$ -	$ 205,000	$ -	$ -	$ 205,000
Direct Operating Costs	$ 1,383,000	$ 1,383,000	$ 1,383,000	$ 1,383,000	$ 1,383,000	$ 1,383,000	$ 1,383,000	$ 1,383,000	$ 1,383,000	$ 1,383,000	$ 1,383,000
Subtotal	$ 393,000	$ 1,896,000	$ 2,169,000	$ 2,169,000	$ 1,964,000	$ 2,169,000	$ 2,169,000	$ 1,964,000	$ 2,169,000	$ 2,169,000	$ 1,964,000
Overhead Costs											
Overhead	$ 136,000	$ 136,000	$ 136,000	$ 136,000	$ 136,000	$ 136,000	$ 136,000	$ 136,000	$ 136,000	$ 136,000	$ 136,000
Subtotal	$ 136,000	$ 136,000	$ 136,000	$ 136,000	$ 136,000	$ 136,000	$ 136,000	$ 136,000	$ 136,000	$ 136,000	$ 136,000
Net Operating Income (Gross Margin)											
Operating Cash Flow	$ 393,000	$ 1,896,000	$ 2,169,000	$ 2,169,000	$ 1,964,000	$ 2,169,000	$ 2,169,000	$ 1,964,000	$ 2,169,000	$ 2,169,000	$ 1,964,000
Overhead Costs	$ 136,000	$ 136,000	$ 136,000	$ 136,000	$ 136,000	$ 136,000	$ 136,000	$ 136,000	$ 136,000	$ 136,000	$ 136,000
Net Operating Income (Gross Margin)	$ 257,000	$ 1,760,000	$ 2,033,000	$ 2,033,000	$ 1,828,000	$ 2,033,000	$ 2,033,000	$ 1,828,000	$ 2,033,000	$ 2,033,000	$ 1,828,000
Initial Working Capital Requirement											
Cumulative Net Operating Income	-$ 4,808,000	-$ 3,048,000	-$ 1,015,000	$ 1,018,000	$ 2,846,000	$ 4,879,000	$ 6,912,000	$ 8,740,000	$ 10,773,000	$ 12,806,000	$ 14,634,000
Minimum Cash Balance											
Contingency[3]											
Initial Working Capital[6]											

Appendix 6: Diamond drill hole logs.

Collar Coordinates

Hole	East (m)	North (m)	Elev (m)	Length (m)
D11801	8570.27	7110.27	425.82	120.09
D11802	8569.74	7110.35	425.78	121.31
D11803	8570.14	7110.92	426.77	42.37
D11804	8569.98	7110.76	426.66	40.84
D11820	8543.00	6995.70	408.50	23.47
D11821	8542.00	6995.80	408.50	24.99
D11822	8542.00	6995.80	408.80	22.25
D11823	8542.50	6995.80	408.70	22.56
D11824	8543.50	6995.60	408.70	21.95
D11825	8544.00	6995.50	408.50	22.25
D11826	8544.50	6995.40	408.50	23.78
D11827	8528.80	6979.30	409.00	26.22
D11828	8528.80	6979.30	410.00	14.02
D11829	8528.80	6979.30	410.50	9.45
D11830	8529.50	6978.00	409.00	10.68
D11831	8529.50	6978.00	410.00	8.54
D11832	8529.50	6978.00	410.50	6.71
D11833	8533.00	6978.20	410.50	11.28
D11834	8533.00	6978.20	411.00	8.54
D11835	8533.00	6978.20	411.30	9.15
D11836	8533.50	6980.00	411.30	15.24
D11837	8533.50	6980.00	411.00	17.07
D11838	8533.50	6979.00	411.30	12.80
D11839	8533.20	6979.00	411.00	15.85
D11840	8533.20	6979.00	410.50	18.29
D11841	8533.20	6979.00	410.40	20.12
D11842	8533.20	6979.00	410.20	29.27
D119C1	8568.93	7110.45	426.59	46.65
D119C2	8569.30	7110.81	426.67	42.68
D119C3	8569.43	7111.02	426.79	43.89
D119C4	8569.52	7111.13	427.52	39.32
GA10A	7996.88	7223.85	516.17	66.14
GA10B	7997.85	7222.53	516.35	66.14
GA11	8700.97	7525.33	515.52	66.14
GA12	9051.13	7517.02	515.22	66.14
GA13	9153.83	7287.51	525.25	66.14
GA14A	8348.54	7299.49	514.00	66.14
GA14B	8347.56	7300.58	514.03	66.14
GA15	8721.77	7255.88	518.56	66.14
GA16	8535.43	7099.00	519.23	66.14
GA17	7677.69	6572.39	532.57	66.14
GA18	9273.83	7780.54	517.77	66.14
GA19	10105.58	7266.21	517.28	66.14
GA1A	9670.87	7025.33	518.35	66.14
GA1B	9669.34	7026.48	518.31	66.14
GA2	9391.72	6441.55	519.54	66.14
GA20	8674.51	7043.02	521.48	66.14
GA21	8599.72	7235.02	514.11	66.14
GA22A	8263.37	7178.21	518.51	66.14
GA22B	8266.49	7179.55	518.54	66.14
GA23	8538.47	6824.28	535.63	66.14
GA24	9022.80	7414.17	514.98	66.14
GA25	8760.60	7414.78	514.25	66.14
GA26	8466.48	7342.84	514.63	66.14
GA27	8123.09	7128.80	527.78	66.14
GA28A	9701.46	7654.22	540.53	66.14
GA28B	9702.66	7652.35	540.65	66.14
GA3	9155.74	6697.54	523.74	66.14
GA4	8441.97	7138.44	516.96	66.14
GA5	8321.73	7017.35	534.86	66.14
GA6	8149.90	6973.09	539.75	66.14
GA7	7758.69	6774.65	534.76	66.14
GA8A	7242.85	6503.92	513.97	66.14
GA8B	7242.51	6505.99	513.99	66.14
GA9A	7741.69	7035.67	519.36	66.14
GA9B	7743.01	7036.53	519.16	66.14
S001	6958.28	5796.69	524.54	7.92
S002	6965.29	5894.83	522.98	10.97
S003	6996.68	5911.29	519.20	22.86
S004	6994.25	5829.30	518.32	10.97
S005	7056.12	5898.49	514.94	38.10
S006	7080.20	5760.42	521.89	13.41
S007	7085.38	5890.56	516.00	35.66
S008	7061.61	5735.42	522.77	15.85
S009	7089.65	5722.92	522.65	15.85
S010	7065.57	5693.36	525.14	5.79
S011	7081.42	5829.91	516.77	28.96
S012	7107.02	5748.22	520.27	19.81
S013	7145.12	5879.29	515.44	37.80
S014	7128.66	5692.75	519.64	16.15
S015	7174.08	5682.08	518.12	9.45
S016	7196.02	5638.80	516.99	12.50
S017	7153.35	5738.77	516.50	23.77
S018	7097.57	5950.92	519.20	19.51
S019	7127.75	5944.82	520.89	25.91
S020	7242.05	5677.81	517.23	29.26
S021	7134.45	5975.60	521.18	21.95
S022	7104.58	5981.40	519.48	15.85
S023	7164.32	5968.90	522.34	26.21
S024	7174.99	5998.46	521.98	25.91
S025	7139.03	5975.60	522.09	22.86
S026	7146.04	6035.04	521.00	10.36
S027	7205.50	5993.28	520.38	31.70
S028	7159.75	6094.48	524.20	24.99
S029	7258.81	5979.87	526.37	29.57
S030	7175.91	6028.94	523.16	26.82
S031	7182.31	6057.90	525.94	22.86
S032	7212.48	6052.11	526.82	29.26
S033	7157.62	5939.03	521.40	20.42
S034	7186.88	5932.93	521.92	20.73
S035	7194.80	5950.31	522.52	33.53
S036	7218.27	6081.98	531.12	26.21
S037	7247.84	6075.88	534.69	19.51
S038	7206.08	6022.24	522.83	24.99
S040	7235.95	6015.53	524.75	35.36
S041	7195.41	6117.34	531.27	23.77
S042	7301.18	6032.30	538.59	22.25
S043	7207.00	6177.08	536.27	36.58
S044	7234.73	5942.99	522.16	41.76
S045	7267.04	6164.58	542.89	28.96
S046	7354.52	6147.82	549.13	35.36
S047	7306.36	5907.63	526.76	29.57
S048	7410.91	6134.71	550.72	45.11
S049	7485.90	6185.90	550.70	71.93
S050	7645.91	6194.15	551.85	71.32
S051	7472.17	6129.83	550.66	72.54
S052	7535.57	6115.81	551.54	77.72
S053	7691.63	6272.48	557.55	51.51
S054	7581.29	6200.24	550.66	61.57
S055	7702.84	6177.41	554.28	84.43
S056	7787.03	6347.46	550.37	106.07
S057	7762.19	6169.12	557.03	90.22
S058	7712.35	6236.51	557.70	106.07
S059	7651.70	6245.66	555.17	81.69
S060	7630.97	6130.14	551.69	43.59
S061	7693.76	6117.95	551.33	69.19
S062	7684.31	6056.99	549.83	56.69
S063	7724.85	6295.03	557.88	101.19
S064	7664.50	6308.14	557.76	121.01
S065	7772.70	6228.89	556.85	79.25
S067	7783.07	6283.45	554.40	21.95
S068	6689.20	4736.64	555.00	105.77
S069	7606.50	6242.00	553.55	75.59
S070	6719.03	4720.92	555.00	96.62
S071	7676.60	6148.09	551.63	67.06
S072	7681.57	6230.69	556.11	105.77
S073	7464.00	5264.00	522.00	123.75
S074	7471.41	6190.49	550.66	78.64
S075	7428.00	5486.00	523.00	135.94
S076	7667.61	6090.73	550.99	47.85
S077	7729.15	6077.62	551.15	66.45
S078	7732.50	6138.61	553.58	54.25
S079	7388.00	5605.00	522.00	44.50
S080	7767.01	6105.60	553.13	94.49
S081	7805.26	6137.67	556.69	87.78
S082	7836.80	6162.54	557.09	74.68
S083	7753.47	6251.48	550.32	65.84
S084	9610.10	7329.46	528.74	28.04
S085	7800.96	6202.80	558.09	75.29
S086	9755.64	7146.31	519.05	75.29
S087	7740.91	6204.72	558.19	87.48
S088	9347.58	7471.20	519.48	54.86
S089	9365.99	7500.88	521.03	29.87
S090	7875.15	6188.57	553.43	56.39
S091	9286.98	7496.62	518.11	87.48
S092	5902.05	5479.63	555.00	94.79
S093	9196.58	7536.70	517.47	157.28
S094	7841.16	6232.09	553.74	62.48
S096	7806.22	6259.56	554.77	59.13
S097	9164.82	7547.88	517.50	169.77
S098	5934.71	5636.00	555.00	116.74
S099	9229.68	7525.27	517.28	153.31
S100	7782.31	6291.31	554.38	68.88
S101	8528.91	6208.78	533.83	17.68
S102	8415.83	6138.98	531.53	38.71
S103	8334.45	6004.26	530.75	41.76
S104	8247.58	6129.53	540.45	70.10
S105	8072.63	6232.25	547.61	76.50
S106	7764.26	6314.08	554.50	84.73
S107	9258.27	7509.30	517.71	120.70
S109	7738.45	6343.59	553.28	90.83
S110	9313.56	7479.85	518.14	78.64
S111	5751.00	5627.59	555.00	114.00
S112	7788.86	6349.53	549.47	102.11
S114	7807.76	6329.90	549.44	84.73
S115	9365.22	7440.63	519.20	50.29
S117	9316.09	7630.55	522.65	89.00
S119	9292.04	7644.93	521.24	99.67
S120	7822.63	6312.99	549.62	75.59
S121	9341.30	7612.68	522.77	89.61
S123	7842.38	6294.61	549.23	59.74
S124	7856.37	6279.98	548.95	57.30
S125	9364.10	7593.54	520.88	69.49
S126	7870.18	6262.57	548.86	52.43
S127	9393.78	7577.45	521.06	60.35
S128	6586.15	5802.51	556.02	41.15
S130	7886.30	6247.55	548.34	53.64
S131	9424.41	7564.19	522.04	67.97
S131A	9424.42	7567.67	522.04	69.40
S131B	9409.21	7560.75	522.13	60.30
S132	10475.00	10410.00	530.50	57.00
S133	9442.09	7547.98	524.05	60.35
S134	6548.26	5940.86	559.77	79.25
S135	7898.34	6233.46	548.52	54.25
S136	7913.00	6213.17	548.37	54.25
S137	7924.56	6197.86	547.98	56.08
S138	7932.66	6181.40	547.95	61.57
S139	7947.17	6144.19	548.46	65.84
S140	6569.96	5863.93	556.42	53.95
S141	6535.28	6000.32	562.85	166.73
S142	6554.11	5933.54	559.10	98.45

S143	6600.11	5744.96	560.66	34.44
S145	8000.02	7185.75	516.31	257.25
S146	8236.98	7056.27	534.23	224.03
S147	8390.05	6926.06	535.94	160.32
S148	8489.53	6857.85	534.47	128.93
S149	8540.25	6818.89	536.06	107.29
S150	9468.52	7535.51	527.46	48.16
S151	9493.54	7515.67	528.68	32.31
S152	9592.73	7604.36	534.69	49.38
S153	9534.08	7629.81	525.69	64.92
S154	9476.96	7668.83	523.10	103.02
S155	7967.14	6111.27	547.40	70.10
S156	8051.02	6145.44	541.30	75.59
S157	8011.64	6216.88	545.23	54.86
S158	7984.42	6251.57	546.24	41.76
S159	7961.04	6286.44	546.79	38.71
S160	7947.23	6326.70	548.13	29.57
S161	7925.90	6360.14	548.07	44.20
S162	7905.35	6397.02	548.04	59.13
S163	7877.16	6435.09	548.52	61.26
S163A	7883.71	6422.47	548.40	61.20
S163B	7873.53	6446.18	548.80	59.40
S164	7862.53	6468.28	549.47	60.05
S167	7758.00	3884.51	555.00	224.33
S168	7907.56	3635.54	555.00	30.48
S169	8066.35	3476.99	555.00	237.13
S170	8586.16	6785.76	536.39	87.78
S171	8624.56	6731.63	536.88	60.35
S172	8676.04	6688.10	536.03	52.12
S173	8707.98	6636.47	533.41	33.53
S174	8437.53	6892.84	533.68	138.38
S175	9486.78	7740.82	521.85	140.21
S176	9639.03	7577.15	539.96	68.58
S177	9674.53	7527.98	542.49	57.61
S178	9678.10	7584.52	542.25	106.68
S179	9646.71	7636.92	538.65	114.91
S180	7832.81	6508.58	548.68	75.29
S181	7809.71	6543.29	547.73	86.26
S182	7780.69	6576.46	545.20	93.57
S183	7760.15	6615.32	541.91	111.86
S184	7801.11	6684.69	543.40	138.38
S185	7826.75	6657.93	544.29	111.40
S186	7875.88	6689.87	545.54	157.28
S187	7910.08	6637.14	546.02	132.89
S188	7937.45	6584.93	548.31	91.44
S189	7968.72	6533.33	551.24	74.98
S190	8470.44	3122.28	555.00	173.74
S191	8813.98	2822.38	555.00	40.54
S192	8212.49	2513.96	555.00	55.78
S193	7023.41	6449.99	529.05	108.81
S194	8323.63	6709.84	546.07	43.59
S195	8713.74	6788.66	531.24	32.00
S196	8670.86	6845.17	530.78	46.94
S196A	8673.14	6838.52	530.82	41.70
S196B	8666.13	6851.90	530.78	50.90
S197	8634.04	6890.22	529.90	57.00
S198	8604.11	6948.62	526.97	81.69
S199	8576.25	6997.84	521.79	81.69
S202	9617.26	7683.64	533.25	105.77
S203	9593.67	7736.37	528.86	132.28
S204	9698.10	7801.54	540.54	198.73
S205	9662.98	7852.38	539.87	218.85
S206	9730.07	7741.31	541.18	157.89
S207	9756.28	7698.73	542.31	124.36
S208	9793.22	7648.77	541.88	87.78
S209	9835.71	7602.93	541.21	51.21
S210	7997.62	6482.64	552.91	53.64
S211	8026.66	6426.86	553.31	36.88
S212	8007.43	6752.78	548.25	105.16
S213	7976.65	6804.57	547.18	135.94
S214	7741.89	6424.60	545.84	87.17
S215	7716.71	6479.16	534.59	57.00
S216	7690.01	6529.06	533.86	68.58
S217	7546.30	6267.15	550.51	87.17
S218	7518.11	6323.08	546.06	107.90
S219	7488.14	6374.40	539.38	133.20
S220	8286.32	6768.27	544.62	68.58

S221	8112.86	6595.08	555.50	56.39
S222	8081.35	6647.29	553.61	66.14
S223	8054.46	6702.25	550.87	84.12
S224	7625.36	6451.37	541.67	53.95
S225	8545.10	7050.05	518.62	90.83
S226	8517.58	7104.25	519.02	77.42
S227	8486.79	7158.90	518.01	67.06
S228	8469.02	7225.34	518.26	92.05
S229	8605.78	7195.08	518.53	111.86
S230	9877.50	7551.63	535.75	30.48
S231	9889.91	7685.96	536.91	140.21
S232	9922.49	7631.08	531.82	65.53
S233	9955.99	7580.41	527.65	22.86
S234	9868.81	7748.81	540.39	177.70
S235	8828.47	7038.72	527.65	66.75
S236	9034.79	7173.93	541.70	117.65
S237	9234.80	7315.32	515.70	50.90
S238	8998.82	7219.43	536.64	150.27
S239	8972.21	7273.90	529.87	173.13
S240	8932.22	7321.27	524.08	178.61
S241	8902.23	7361.90	516.58	153.92
S242	9069.42	7119.12	547.15	68.28
S243	9096.12	7073.25	548.86	61.87
S244	9131.35	7025.43	548.98	75.90
S245	9835.38	7801.75	544.01	194.46
S246	9808.37	7852.78	545.45	226.47
S247	9778.84	7914.47	546.45	236.83
S248	9918.47	7901.64	539.20	223.42
S249	9946.23	7849.27	534.14	195.38
S250	9974.00	7795.20	532.43	148.74
S251	9989.73	7736.34	530.75	112.17
S252	10018.17	7690.35	526.97	69.49
S253	10045.69	7640.51	523.87	30.78
S254	10176.36	7704.12	523.20	58.22
S255	8656.38	7085.26	519.96	84.73
S256	8683.39	7027.16	522.28	53.34
S257	8734.10	6960.41	524.08	26.82
S258	8782.87	6910.82	525.39	41.76
S259	8836.67	6868.88	526.55	43.59
S260	8869.53	6801.79	525.57	51.21
S261	8920.06	6834.84	531.21	37.80
S262	8975.84	6863.70	525.12	42.06
S263	8946.79	6917.86	530.36	55.78
S264	8917.20	6972.24	531.21	57.91
S265	7590.50	6437.92	542.25	53.95
S266	8219.24	6647.90	551.97	71.93
S267	8249.32	6594.38	554.47	44.50
S268	8188.21	6698.19	547.58	95.55
S269	8156.27	6749.31	545.78	129.54
S270	6792.93	6296.28	539.90	24.99
S271	6766.50	6337.01	543.04	42.98
S272	6690.60	6447.01	556.45	50.90
S273	6651.25	6506.50	559.59	57.00
S274	6586.82	6560.76	563.09	60.05
S275	6569.54	6613.49	565.90	53.95
S276	6988.21	6514.67	531.36	99.06
S277	6997.39	6500.29	530.42	108.81
S278	7073.59	6358.52	515.51	81.38
S279	7041.49	6390.74	525.85	113.39
S281	8869.16	6998.82	530.60	74.68
S282	8792.02	7092.06	522.01	51.21
S283	8757.73	7143.57	520.45	77.72
S284	8730.90	7195.32	519.51	87.78
S285	8691.98	7245.25	518.07	109.73
S286	8773.52	7355.92	515.36	85.95
S287	8809.30	7305.78	519.26	81.08
S288	8840.72	7257.87	522.28	101.80
S289	8873.46	7206.29	529.41	122.22
S290	8905.28	7155.09	533.80	137.77
S291	7452.54	6427.10	531.49	138.38
S292	7412.31	6484.38	517.37	142.34
S293	8359.23	6988.33	534.63	183.49
S294A	8397.61	6868.12	537.49	35.30
S294B	8398.73	6866.20	537.46	108.80
S295	8395.20	6883.69	537.58	130.76
S296	8424.61	6769.94	541.30	65.23
S297	8417.14	6797.34	539.65	78.33

S298	7207.70	6257.94	530.63	69.80
S299	7173.77	6320.82	522.52	84.43
S300	9299.72	7195.20	524.57	61.57
S301	9202.89	7367.38	515.64	87.48
S302	9173.29	7416.52	515.67	118.87
S303	9137.60	7463.27	515.82	128.93
S304	9233.79	7432.70	515.97	93.88
S305	9263.94	7380.49	515.67	50.29
S306	9277.50	7365.28	515.33	68.28
S307	9296.67	7326.72	515.36	52.73
S308	9245.71	7669.59	519.60	136.25
S309	9283.63	7607.66	520.57	81.69
S309A	9280.18	7615.46	520.24	36.50
S309B	9280.89	7614.00	520.33	57.90
S310	10201.66	7656.36	522.07	78.33
S311	10230.06	7604.85	519.11	74.07
S312	10135.42	7756.15	524.99	120.09
S313	10103.33	7815.68	528.07	142.65
S314	10240.98	7812.94	525.80	151.79
S315	10261.09	7762.89	525.79	156.06
S316	10286.76	7703.45	522.62	117.04
S317	10311.46	7646.88	521.82	68.58
S318	10332.32	7605.95	518.81	36.58
S319	10371.00	7560.69	517.80	12.19
S320	8937.83	7100.01	539.59	97.84
S321	8970.08	7054.81	544.71	82.91
S322	8999.98	7007.99	542.79	57.91
S323	9028.66	6960.53	541.30	44.81
S324	9059.78	6904.94	539.68	67.36
S325	9171.49	7187.12	535.23	59.74
S326	9198.86	7138.93	538.74	63.40
S327	9138.61	7237.26	529.26	89.92
S328	9108.19	7288.41	526.88	119.48
S329	9076.33	7340.35	519.99	142.04
S330	8126.36	6798.44	545.05	155.75
S331	7657.25	6338.51	556.33	51.21
S332	7420.02	6228.25	550.05	64.62
S333	7393.93	6285.19	540.36	69.19
S334	7368.20	6335.79	532.86	78.33
S335	7341.99	6386.50	526.61	84.43
S336	7233.06	6345.75	527.65	108.81
S337	7207.00	6396.62	519.60	128.32
S338	7264.45	6293.85	533.28	78.33
S339	7296.30	6245.87	538.47	63.09
S340	10401.32	7769.35	520.57	93.88
S341	10424.98	7710.19	518.62	48.46
S342	10448.30	7649.26	518.75	35.36
S343	10424.83	7595.13	518.04	14.63
S344	10561.26	7656.91	518.38	54.25
S345	9366.17	7661.18	523.38	59.44
S346	9366.23	7698.73	521.37	153.92
S347	9522.65	7544.56	531.73	28.35
S348	9490.31	7599.94	529.50	57.30
S349	9465.14	7643.29	523.59	87.17
S350	9051.80	7384.21	517.74	163.98
S351	9094.53	7428.77	515.51	133.50
S352	9124.04	7378.14	516.95	113.39
S353	9156.16	7324.86	519.08	100.58
S354	9184.26	7272.71	525.94	77.11
S355	9218.46	7216.84	529.90	45.11
S356	9274.12	7248.85	519.26	45.11
S357	9077.52	7223.36	535.91	62.48
S358	9047.47	7273.59	531.27	113.39
S359	9015.13	7329.65	522.98	136.86
S360	8399.71	7177.06	517.68	132.89
S361	8364.84	7226.93	514.48	61.57
S362	8429.30	7122.63	517.89	121.01
S363	8457.41	7072.76	516.86	105.77
S364	8487.70	7020.03	517.28	122.53
S365	8520.38	6964.22	523.62	130.15
S366	8551.83	6909.91	528.10	102.72
S367	8578.84	6861.72	530.91	113.39
S368	8609.87	6807.53	534.66	104.85
S369	8755.90	6745.80	530.69	43.89
S370	8857.91	7729.33	519.54	191.11
S371	8798.94	7829.34	521.21	258.17
S372	8738.98	7935.01	523.38	286.51

S373	8608.77	8142.55	529.93	270.97
S374	8490.33	8336.34	540.02	108.81
S375	8405.10	8558.33	547.95	69.19
S376	8240.88	8647.76	549.99	104.85
S377	8014.84	8774.19	546.57	119.48
S378	7757.43	8819.94	524.14	87.78
S379	10205.50	7873.59	530.36	154.53
S380	9327.40	7276.80	515.79	50.90
S381	9063.20	7479.55	516.09	159.41
S382	9012.20	7447.33	515.61	199.95
S383	8956.85	7427.03	516.43	198.12
S384	8860.69	7357.20	518.53	138.07
S385	8883.52	7314.99	522.31	133.50
S386	8909.40	7264.27	528.68	151.79
S387	8939.57	7211.60	533.92	151.49
S388	8971.30	7158.08	540.60	115.21
S389	9004.22	7104.77	545.90	83.52
S390	9305.33	7562.67	520.24	57.00
S391	9935.44	7736.83	535.45	142.65
S392	9954.04	7708.18	532.46	123.75
S393	9335.57	7513.93	520.12	38.71
S394	9407.77	7414.96	521.98	25.60
S395	9446.67	7431.79	527.07	25.91
S396	9416.03	7484.61	522.10	18.29
S397	9386.83	7539.65	522.16	24.69
S398	9409.57	7621.19	521.06	93.57
S399	9380.95	7669.01	522.07	112.17
S400	7246.77	6211.43	539.96	60.05
S401	7190.05	6175.52	533.22	44.81
S402	7161.00	6241.02	522.89	60.05
S403	6953.65	6384.10	530.11	49.38
S404	6942.06	6370.78	530.94	56.39
S405	4878.05	6397.75	512.56	239.88
S406	4956.57	6082.80	512.07	254.84
S407	5055.23	5819.94	513.20	77.72
S408	5061.78	5785.74	513.26	244.21
S409	5214.73	5480.58	515.40	93.57
S410	7145.88	6363.25	516.40	108.18
S411	7258.60	6302.68	532.19	85.10
S412	7310.45	6336.40	530.45	94.49
S413	7280.54	6387.48	524.69	111.25
S414	7341.11	6284.18	536.45	83.82
S415	7373.72	6231.12	546.79	65.53
S416	7402.37	6176.77	550.26	53.34
S417	7463.42	6070.85	550.81	71.63
S418	7493.81	6017.67	550.96	56.69
S419	7543.07	6048.27	549.96	43.59
S420	9744.88	7580.56	546.36	75.90
S421	9765.15	7548.83	546.15	46.94
S422	9803.83	7496.98	544.84	34.14
S423	9702.27	7653.56	541.09	136.25
S424	9671.27	7703.85	538.65	72.24
S425	9672.40	7702.17	538.34	151.18
S426	9641.68	7756.55	536.12	142.34
S427	8750.75	7411.85	515.27	56.08
S428	8793.69	7435.90	514.94	69.19
S429	8701.49	7376.01	514.81	86.87
S430	8475.82	6800.03	538.28	73.46
S431	8472.01	6797.38	538.44	82.91
S432	8505.66	6747.88	540.42	63.09
S433	8536.29	6694.41	541.18	35.72
S434	8432.81	6624.10	544.84	28.96
S435	8493.98	6528.54	534.72	17.68
S436	8553.75	6424.70	533.35	6.10
S437	8615.72	6322.10	530.78	23.47
S438	8682.50	6202.04	531.52	29.57
S439	8749.22	6085.82	532.58	20.42
S440	8363.53	6875.22	540.36	117.96
S441	5243.02	5431.35	514.33	30.48
S442	5196.57	5403.40	514.36	59.44
S443	4734.70	5211.26	534.32	57.30
S444	4710.07	5303.09	534.17	81.38
S445	6995.62	6262.12	522.37	96.62
S446	8739.47	7070.26	521.67	40.54
S447	8711.76	6983.70	523.84	31.70
S448	8774.70	6895.76	526.03	38.10
S449	8805.09	7131.68	522.34	38.71
S450	9516.53	7681.42	524.23	117.04
S451	9577.43	7577.48	534.69	28.96
S452	9607.05	7524.78	538.10	35.97
S453	9881.01	7615.70	540.20	63.09
S454	9845.98	7666.36	540.54	103.02
S455	9809.41	7714.85	543.40	139.60
S456	10003.72	7618.45	525.94	37.49
S457	9974.55	7672.73	529.50	96.93
S458	9913.13	7779.81	538.19	163.98
S459	10008.02	7833.24	531.06	160.93
S460	9033.97	7051.97	546.82	64.62
S461	8883.43	7067.73	534.72	114.91
S462	8913.63	7018.26	534.08	77.11
S463	8852.06	7120.68	530.66	85.95
S464	8822.22	7172.16	524.87	68.58
S465	8792.44	7226.99	521.31	55.17
S466	8761.96	7278.35	519.42	55.78
S467	8635.99	7132.53	516.40	89.31
S468	9356.72	7223.85	516.37	50.60
S469	9361.75	7096.02	527.28	39.62
S470	8395.93	6820.27	539.08	80.16
S471	8374.84	6739.22	544.32	36.58
S472	8342.83	6793.96	542.73	64.92
S473	8311.74	6843.28	542.73	83.52
S474	8279.65	6895.98	542.37	41.15
S475	8272.67	6909.72	541.79	117.96
S476	8262.09	6815.60	544.32	95.10
S477	8229.42	6869.92	544.01	90.83
S478	8231.34	6866.35	544.14	84.43
S479	8241.03	6847.70	544.17	102.72
S480	10179.47	7926.42	533.80	187.15
S481	10143.71	7973.63	538.59	206.35
S482	10021.46	8178.70	549.07	44.81
S483	9896.75	8386.97	550.75	50.29
S484	10261.60	8298.48	545.69	56.08
S485	10411.72	8119.60	535.08	93.57
S486	10483.41	8011.18	534.23	215.49
S487	10768.19	7590.28	531.58	5.49
S488	10832.17	7732.72	520.06	31.39
S489	10937.57	7816.57	518.65	63.40
S490	7542.28	6051.26	549.93	96.32
S491	7512.13	6097.16	550.87	87.48
S492	7479.49	6148.43	551.05	81.38
S493	7446.81	6200.97	550.32	72.24
S494	7499.51	6231.45	549.44	67.67
S495	7534.35	6180.61	550.93	58.83
S496	7564.10	6130.47	552.03	61.26
S497	7597.29	6077.29	552.06	65.23
S498	7633.01	6026.93	549.32	69.80
S499	8675.31	7040.36	521.55	58.22
S500	10037.37	7777.83	529.08	124.36
S501	10067.09	7725.40	526.61	63.40
S502	10098.60	7670.17	524.26	59.74
S503	10123.05	7625.24	521.64	35.36
S504	10155.14	7570.41	519.87	22.71
S505	10283.53	7639.05	521.37	83.52
S506	10249.45	7693.40	523.47	131.98
S507	10219.18	7743.60	525.09	112.17
S508	10184.50	7798.00	527.22	121.31
S509	10308.82	7593.36	518.32	45.11
S510	8810.98	5979.75	539.96	17.37
S511	8870.14	5874.78	540.66	14.33
S512	8927.04	5781.75	539.08	11.28
S513	8983.86	5692.20	538.50	11.28
S514	9039.85	5592.59	538.68	15.54
S515	9126.60	5497.53	534.29	32.61
S516	8897.93	5343.14	530.39	6.10
S517	8839.78	5447.05	525.48	23.47
S518	8777.42	5551.17	523.07	23.47
S519	8970.20	5237.90	531.06	41.76
S520	8715.42	5655.96	520.63	75.29
S521	8224.94	6509.03	556.21	40.84
S522	8286.99	6398.94	552.21	33.83
S523	8332.29	6316.46	545.48	27.74
S524	6992.42	6400.31	528.01	76.50
S525	6997.99	6407.84	528.96	93.57
S526	6941.67	6520.86	535.42	68.58
S527	6881.68	6517.20	541.85	52.73
S528	6818.68	6517.20	545.96	35.66
S529	7031.68	6311.65	522.80	60.96
S530	9342.00	7125.04	524.72	42.67
S531	9422.22	6994.82	527.28	70.10
S532	9483.58	6887.17	531.88	81.69
S533	9546.31	6777.87	527.55	68.58
S534	9588.76	6684.90	515.94	87.78
S535	9482.51	6620.84	514.78	65.53
S536	9453.89	6717.24	522.71	70.41
S537	9375.22	6824.56	536.88	109.73
S538	9313.19	6928.53	541.70	64.62
S539	8784.92	6875.50	527.16	38.71
S540	8667.84	7050.08	520.70	66.14
S541	8660.47	7066.70	520.21	71.63
S542	8640.35	7094.92	516.22	88.39
S543	8640.35	7107.81	516.22	87.48
S544	8163.79	6614.62	556.02	54.35
S545	8134.41	6667.74	552.85	67.36
S546	8126.09	6681.34	550.84	87.48
S547	8104.72	6707.34	550.02	93.57
S548	8104.45	6720.78	549.47	88.70
S549	8095.52	6732.54	549.19	102.72
S550	8209.45	6900.55	543.92	93.88
S551	8200.03	6922.10	543.62	136.25
S552	8144.84	6888.69	544.71	168.86
S553	11034.55	7887.31	525.85	87.78
S554	11300.37	7936.17	522.40	99.97
S555	8087.81	6745.93	548.46	103.94
S556	7946.50	6571.58	549.98	87.48
S557	7936.75	6582.10	549.01	94.49
S558	9420.76	7560.23	522.19	63.09
S559	4678.40	5327.50	537.40	81.38
S560	8760.59	7494.24	514.97	56.39
S561	8746.91	7534.32	516.43	70.71
S562	8771.56	6883.33	526.85	39.93
S563	8732.95	6905.70	526.46	33.83
S564	8751.87	7026.77	522.34	30.48
S565	8756.60	7094.89	521.70	50.60
S566	8699.17	7079.38	521.31	53.34
S567	8654.22	7020.67	522.46	59.74
S568	8607.46	7085.44	520.24	74.07
S569	8755.11	7042.89	522.16	35.05
S570	10418.00	7650.57	518.59	29.26
S571	10385.57	7705.65	521.67	65.84
S572	10432.82	7589.00	518.41	8.23
S573	10345.80	7743.38	518.41	118.26
S574	10293.40	7864.69	531.55	199.64
S575	10388.29	7927.73	534.38	200.56
S576	10485.94	7838.02	530.94	154.84
S577	10584.76	7907.70	523.10	173.13
S578	10645.63	7797.97	518.50	94.79
S579	10709.88	7701.05	521.76	48.77
S580	8781.99	7108.30	521.28	53.34
S581	8704.27	7097.60	520.94	57.61
S590	4645.40	5373.96	539.32	116.13
S591	5031.33	5350.31	513.58	38.71
S592	4970.34	5365.27	514.05	46.63
S593	4919.81	5387.71	513.81	20.42
S594	4889.02	5437.69	513.50	17.37
S595	4847.84	5484.27	513.36	41.76
S596	4869.85	5536.75	512.89	65.84
S597	4821.94	5579.82	514.36	78.94
S598	4940.90	5556.47	515.48	85.95
S599	4996.77	5460.61	519.39	41.45
S607	8630.53	6957.06	526.49	64.92
S608	8625.50	7026.52	521.21	69.49
S609	8736.82	7140.73	520.27	91.44
S610	8728.50	7113.73	520.85	76.20
S611	8701.28	7109.61	519.90	69.19
S612	8613.65	5059.68	515.20	44.81
S613	8547.00	7146.00	520.16	78.03
S614	8456.65	7137.98	516.71	96.92
S615	8514.21	7177.54	519.07	82.90
S616	8539.49	7190.50	520.29	94.48
S617	8542.33	7164.81	520.66	87.48
S618	8507.05	7150.34	518.43	65.83

S619	8453.67	7234.51	516.11	85.64
S620	8447.63	7224.23	516.64	74.00
S621	8461.24	6965.83	527.45	161.54
S622	8506.00	6922.09	528.44	150.26
S623	8586.27	7121.18	520.17	78.33
S624	8455.19	7201.62	517.25	78.02
S625	8491.47	7216.51	519.23	107.59
S626	8501.70	7248.96	519.15	124.05
S627	8438.00	7260.00	514.50	87.47
S628	8867.40	7265.56	523.15	121.61
S629	8893.20	7214.18	530.30	139.29
S630	9036.40	7106.82	546.61	72.23
S631	9051.21	7069.97	547.26	66.75
S632	9024.92	7061.33	546.58	72.24
S633	9044.70	7088.23	547.01	66.14
S634	9021.28	7132.53	544.78	80.76
S635	8997.79	7121.21	544.54	102.11
S636	8905.91	7186.97	533.84	148.44
S637	8855.60	7288.44	522.20	117.96
S638	8828.37	7274.23	521.48	93.57
S639	8842.41	7319.41	519.50	108.81
S640	8828.40	7345.50	518.02	94.48
S641	8794.23	7330.27	517.35	114.30
S642	7897.59	6457.78	550.62	50.90
S643	8483.15	7124.32	517.28	77.42
S644	7916.47	6433.99	550.57	44.80
S645	7946.21	6457.87	552.40	39.39
S646	7973.59	6470.96	553.11	45.72
S647	7851.29	6420.75	546.05	71.93
S648	7864.75	6403.84	546.02	78.33
S649	7874.78	6388.27	546.07	73.45
S650	7870.85	6356.92	546.52	54.86
S651	7857.12	6367.21	546.06	69.18
S652	7839.73	6380.58	545.56	87.47
S653	7839.76	6334.40	547.46	81.38
S654	7862.04	6309.18	547.33	63.09
S655	8754.41	7345.83	515.99	85.34
S656	8876.81	7175.32	529.73	127.10
S657	8867.59	7132.61	530.53	112.78
S658	9240.73	7257.94	523.14	38.55
S659	8945.40	7174.19	536.34	139.29
S660	8918.76	7160.10	535.01	140.94
S661	8933.39	7132.36	537.22	129.54
S662	8903.84	7122.84	533.91	143.25
S663	9203.72	7246.02	526.74	58.21
S664	9176.04	7232.21	529.59	63.09
S665	9162.96	7256.42	527.66	64.92
S666	9149.41	7284.79	526.13	99.67
S667	9177.05	7302.33	521.26	77.42
S668	8291.56	6796.61	542.62	72.23
S669	8316.80	6812.96	542.04	69.18
S670	8345.54	6828.70	540.55	81.38
S671	8289.33	6733.62	544.36	65.22
S672	8317.34	6746.63	543.71	49.07
S673	7820.97	6395.08	545.38	92.65
S674	7833.88	6437.42	546.10	61.56
S675	7861.14	6448.51	547.87	57.91
S676	8257.20	6753.04	543.88	81.38
S677	8230.57	6738.51	543.63	99.67
S677A	9177.63	7302.85	521.09	1.00
S678	9219.82	7288.67	521.04	48.77
S679	9273.20	7316.30	515.46	42.06
S680	8159.64	6737.38	545.13	1.00
S681	8824.00	7283.00	521.00	73.15
S682	9397.00	7575.00	521.00	129.24
S683	8693.00	7246.00	518.47	129.20
S684	9288.36	7286.55	515.11	41.76
S685	9226.65	7344.70	515.45	70.10
S686	9247.30	7410.61	515.80	84.43
S687	9341.67	7359.70	516.07	46.33
S688	9277.08	7447.02	516.05	108.20
S689	9237.29	7378.19	515.45	83.67
S690	8243.46	6711.20	544.13	84.73
S691	8215.77	6698.12	545.32	98.45
S692	8203.96	6724.62	544.54	117.65
S693	8263.65	6729.99	544.04	76.20
S694	8252.12	6698.16	544.79	85.34
S695	8223.32	6684.78	545.94	82.90
S696	8238.34	6724.12	543.89	91.74
S697	8200.00	6677.00	550.00	81.38
S698	8228.71	6712.14	544.89	96.92
S699	8256.50	6833.29	543.16	94.79
S700	8418.00	6827.00	538.00	89.61
S701	8372.51	6835.56	539.17	84.12
S702	8325.22	6830.55	541.46	77.42
S703	8369.85	6851.57	539.35	94.18
S704	8242.32	6778.59	543.07	98.75
S705	9256.89	7345.83	515.46	60.35
S706	9248.00	7288.00	516.00	32.61
S707	9441.13	7583.57	523.46	1.00
S708	9813.61	7618.18	542.62	73.15
S709	9778.21	7665.02	542.59	103.63
S710	9749.43	7717.79	542.52	135.94
S711	9715.95	7773.55	540.86	181.66
S712	9487.61	7642.43	527.28	87.17
S713	9689.05	7675.39	549.90	151.18
S714	9514.28	7650.77	526.94	93.27
S715	9718.03	7624.34	542.92	112.78
S716	9733.08	7595.38	543.58	89.92
S717	9757.00	7624.00	543.00	1.00
S718	9664.45	7606.97	541.44	108.50
S720	9627.01	7622.51	538.09	81.87
S723	8196.67	6753.49	543.12	102.41
S724	8196.67	6753.49	543.12	111.25
S725	8196.67	6753.49	543.12	105.77
S726	8198.50	6733.00	544.00	111.25
S727	8175.00	6756.00	544.47	116.43
S728	8171.00	6722.00	544.02	108.53
S729	8166.00	6694.00	544.71	84.14
S730	8147.50	6717.50	544.71	103.65
S731	8157.50	6706.50	545.53	96.23
S732	7854.50	6614.00	542.80	99.39
S733	7881.00	6561.50	545.85	78.04
S734	7952.00	6676.00	547.68	151.83
S735	7977.50	6633.50	548.46	128.98
S736	8001.00	6592.00	550.00	104.87
S737	8020.00	6663.50	546.57	86.89
S738	7991.50	6707.50	549.09	114.02
S739	8038.00	6729.00	549.62	95.42
S740	7930.70	6675.20	546.78	123.79
S801	8780.75	6826.54	517.21	35.98
S802	8754.29	6805.76	517.53	28.96
S803	8710.02	6822.77	518.85	16.46
S804	8832.00	6827.00	517.40	45.12
S805	8806.77	6800.49	517.36	38.41
S806	8718.75	6886.85	518.87	19.82
S807	8688.00	6802.00	530.00	35.98
S808	8728.32	6760.09	529.73	35.98
S809	8688.00	6764.00	529.70	32.93
S811	8730.00	6852.00	519.00	19.51
S812	8760.00	6830.00	517.50	29.88
S813	8731.00	6812.00	518.90	24.39
S814	8849.00	7094.00	530.10	75.61
S815	8879.00	7043.00	531.10	92.99
S816	8877.00	7069.00	531.20	105.18
S817	8894.00	7105.00	531.80	132.93
S818	8903.00	7078.00	532.20	112.17
S819	8937.00	7080.00	533.40	93.27
S820	9054.60	7166.89	542.59	114.91
S821	9029.43	7215.65	536.02	121.31
S822	9078.98	7219.42	535.31	83.21
S823	9067.76	7246.14	532.35	106.07
S824	9137.80	7238.68	531.10	71.63
S825	8307.35	6866.19	541.58	101.19
S826	8260.44	6892.88	542.37	89.61
S826A	8263.44	6893.00	542.37	105.77
S827	8220.92	6863.64	544.02	123.75
S828	8232.51	6810.12	544.20	117.04
S829	8214.77	6788.20	544.27	113.09
S830	8265.40	6864.82	542.89	96.32
S831	8209.57	6825.29	544.53	134.42
S832	7969.96	6723.00	547.56	106.07
S832A	7971.46	6725.50	547.56	134.11
S833	7982.95	6760.99	547.87	122.53
S834	7949.99	6609.99	547.91	120.09
S835	7894.98	6596.98	546.48	106.98
S836	7808.48	6609.83	544.19	106.98
S837	7732.01	6562.90	542.36	90.22
S838	7677.91	6566.95	531.92	21.34
S838A	7677.91	6566.95	531.92	74.98
S839	7625.99	6570.83	528.78	89.61
S840	7644.95	6619.85	526.54	118.26
S841	7555.50	6560.50	526.63	115.52
S842	7584.99	6538.98	532.45	102.41
S843	7572.00	6489.99	537.19	86.87
S844	7619.04	6502.93	537.22	81.08
S845	7643.07	6492.80	538.16	76.20
S846	7614.99	6464.02	540.44	87.17
S847	7535.19	6472.03	536.00	111.56
S848	7579.01	6442.00	541.73	96.32
S849	7659.97	6445.04	543.72	86.56
S850A	7620.75	6412.70	546.39	126.80
S851	7709.04	6456.01	543.02	71.93
S852	7704.99	6416.05	547.33	90.22
S853	7769.03	6458.01	542.71	71.32
S854A	7784.03	6407.99	545.95	96.31
S855	7756.07	6379.00	549.11	114.60
S856	7738.01	6342.92	553.26	102.41
S857	7821.98	6361.15	547.02	81.07
S858	7797.98	6423.05	545.00	81.07
S859	7603.92	6522.04	535.32	92.96
S860	7833.01	6584.96	546.06	96.32
S861	7828.99	6634.98	543.02	114.60
S862	9694.65	8661.39	533.70	59.40
S863	9593.18	8141.13	544.62	110.90
S864	9700.49	8020.49	546.68	282.20
S865	8518.89	8287.99	534.96	78.60
S866	8559.62	8220.23	530.08	81.00
S867	7878.00	6462.00	550.20	58.22
S868	7888.00	6448.00	550.30	66.08
S869	7889.00	6434.00	548.90	55.78
S870	7874.00	6422.00	547.80	61.57
S871	7863.00	6422.00	546.70	68.58
S872	7863.00	6433.00	548.00	65.84
S873	7840.00	6398.00	545.30	81.08
S874	7838.00	6411.00	545.40	73.46
S875	7842.00	6428.00	546.00	71.34
S876	7818.00	6424.00	545.00	74.98
S877	7811.00	6411.00	545.10	83.52
S878	7806.00	6437.00	545.00	74.98
S879	7888.00	6381.00	546.90	57.91
S880	7868.00	6392.00	545.90	78.03
S881	7855.00	6398.00	545.60	85.95
S882	7857.00	6380.00	545.40	76.81
S883	7829.00	6380.00	545.60	90.25
S884	7815.00	6380.00	545.90	101.80
S885	7840.00	6356.00	546.60	84.73
S886	7824.00	6328.00	548.50	79.25
S887	7888.00	6403.00	547.40	66.14
S901	8691.00	6875.00	515.60	26.00
S902	8670.00	6925.00	514.70	30.00
S903	8699.00	6925.00	514.70	30.00
S904	8735.00	6937.00	514.60	29.00
S905	8688.00	6907.00	515.00	20.00
S906	8700.00	6856.00	516.00	20.00
S907	8730.00	6831.00	516.00	23.00
S908	8740.00	6780.00	517.00	27.00
S909	8659.00	6900.00	514.80	29.00
S910	8650.00	6925.00	514.80	32.00
S911	8650.00	6950.00	514.50	43.00
S912	8675.00	6950.00	514.40	29.00
S913	8700.00	6950.00	514.70	20.00
S914	8782.00	6846.00	518.00	29.00
S915	8755.00	6874.00	517.60	23.00
S916	8809.00	6850.00	517.30	32.00
S917	8840.00	6800.00	516.10	49.00
S918	8814.00	6767.00	515.90	44.00
S919	8835.00	6778.00	516.10	50.00
S920	8850.00	6847.00	519.50	50.00
S921	8890.00	6825.00	523.00	44.00
S922	8667.00	6875.00	521.00	53.00

S923	8831.00	6903.00	520.60	50.00
S924	8876.00	6901.00	521.30	51.00
S925	8706.00	6750.00	532.30	37.00
S926	8718.00	6729.00	531.70	32.00
S927	8700.00	6700.00	534.90	47.00
S928	8656.00	6725.00	536.60	56.00
S929	8651.00	6754.00	533.00	56.00
S930	8669.00	7000.00	515.00	40.00
S931	8679.00	6988.00	514.70	31.00
S932	8711.00	7023.00	522.20	44.00
S933	8785.00	6984.00	525.10	35.00
S934	8797.00	7008.00	525.50	44.00
S935	8780.00	6942.00	518.60	35.00
S936	8819.00	6938.00	518.40	35.00
S937	9271.99	7403.99	515.93	50.00
S938	9289.18	7381.34	515.59	70.00
S939	9308.00	7520.00	518.98	54.00
S940	9272.00	7528.00	518.75	85.00
S941	9266.00	7573.00	518.51	95.00
S942	9258.99	7604.00	518.93	97.00
S943	9308.00	7596.00	522.03	68.00
S944	9339.99	7577.00	521.47	59.00
S945	9371.05	7579.39	521.56	53.00
S946	9343.00	7470.99	519.85	87.00
S947	9371.05	7563.13	521.55	37.00
S948	9471.99	7577.99	526.64	41.00
S949	9465.99	7614.00	524.01	62.00
S950	9416.87	7543.74	521.95	50.00
S951	9586.00	7673.99	529.19	71.00
S952	9587.99	7640.00	533.75	96.00
S953	9614.00	7655.00	535.62	98.00
S954	9668.01	7658.99	539.64	131.00
S955	9739.99	7659.99	542.14	110.00
S956	9681.13	7631.62	541.31	129.00
S957	9691.91	7614.58	542.88	116.00
S958	9708.60	7589.53	543.29	98.00
S959	9720.68	7566.26	543.73	74.00
S960	9784.23	7598.04	542.79	53.00
S961	9787.55	7618.86	542.53	65.00
S962	9499.21	7624.78	522.53	76.00
S963	9550.05	7647.20	528.89	74.00
S964	9430.89	7604.02	521.68	83.00
S965	9392.48	7607.45	521.07	92.00
S966	9295.99	7555.20	519.00	65.00
TEST	8088.00	6700.00	420.00	40.00
U001	8619.99	6948.71	482.20	21.70
U002	8620.29	6948.68	483.82	14.63
U003	8626.78	6958.80	481.74	31.94
U004	8626.94	6958.68	483.29	21.33
U005	8655.07	6868.36	491.25	19.20
U006	8653.00	6868.27	489.79	45.72
U007	8710.97	7088.37	467.02	43.10
U008	8710.33	7089.77	466.84	36.88
U009	8710.70	7089.19	466.38	42.06
U010	8710.18	7090.11	466.62	18.07
U011	8700.24	7105.74	466.38	17.38
U012	8686.80	7069.23	471.04	20.73
U013	8687.96	7072.30	466.96	3.05
U014	8616.73	6932.07	481.04	8.96
U015	8616.73	6932.07	484.97	17.68
U016	8623.49	6949.53	480.58	8.99
U017	8623.49	6949.53	483.81	18.96
U018	8638.58	6916.37	482.71	4.79
U019	8638.58	6916.37	486.46	24.29
U020	8642.96	6969.56	480.92	7.28
U021	8642.97	6969.56	485.06	24.69
U022	8659.52	7027.04	472.78	3.20
U023	8659.52	7027.04	476.62	24.48
U024	8669.03	7085.90	441.84	19.81
U025	8642.18	7077.58	437.45	16.76
U026	8686.31	7088.86	444.95	31.09
U027	8715.76	7094.49	450.98	26.49
U028	8729.23	7099.34	453.00	16.76
U029	8744.53	7107.05	456.32	9.14
U030	8755.75	7117.81	458.00	9.60
U031	8755.75	7117.81	454.65	13.71
U032	8753.06	7117.48	455.56	22.86

U033	8767.69	7125.00	454.34	3.04
U034	8767.69	7125.00	458.33	14.05
U035	8771.56	7143.05	456.44	8.53
U036	8760.99	7111.01	460.25	10.88
U037	8742.46	7088.37	463.21	27.43
U038	8732.46	7076.97	465.53	34.14
U039	8719.32	7066.61	467.33	38.10
U040	8706.89	7059.75	469.73	29.72
U041	8691.62	7058.62	472.35	32.00
U042	8673.39	7055.85	474.03	9.75
U043	8673.39	7055.85	469.98	14.60
U044	8638.21	7008.11	479.27	22.52
U045	8637.76	6992.17	481.10	20.24
U046	8637.76	6992.17	477.63	7.68
U047	8697.25	7093.76	468.42	12.50
U048	8638.18	7008.66	475.68	11.58
U049	8636.90	6977.69	483.66	19.72
U050	8636.90	6977.69	479.94	7.22
U051	8642.57	6900.85	488.66	22.86
U052	8651.20	6888.45	490.73	21.34
U053	8651.20	6888.45	486.28	4.88
U054	8755.99	7103.12	461.32	19.81
U055	8685.85	7059.75	468.91	14.23
U056	8626.59	7128.68	421.00	29.57
U057	8630.22	7091.24	428.00	30.78
U058	8656.81	7120.62	429.00	22.56
U059	8833.69	7104.26	477.20	9.45
U060	8831.01	7104.75	476.11	18.29
U061	8831.01	7104.64	480.66	11.28
U062	8833.09	7040.31	472.56	15.54
U063	8800.06	7185.79	481.11	38.40
U064	8794.39	7182.21	479.88	38.40
U065	8799.96	7183.14	479.90	11.58
U066	8678.63	7172.37	419.51	12.50
U067	8677.43	7169.42	419.54	35.66
U068	8799.74	7183.77	483.66	14.32
U069	8826.85	7166.26	480.29	18.29
U070	8834.26	6993.55	480.34	22.25
U071	8834.29	7005.72	479.05	25.91
U073	8591.63	7138.54	424.07	28.04
U074	8580.27	7121.52	429.80	13.72
U075	8581.53	7117.98	429.82	17.07
U076	8870.59	6997.91	476.74	40.23
U077	8870.59	6997.75	476.92	39.62
U078	8868.10	6997.56	476.54	30.48
U079	8866.89	6997.98	476.57	35.05
U080	8866.89	6997.98	476.37	15.24
U081	8870.50	7001.20	476.70	15.24
U082	8854.76	7021.80	474.15	14.93
U083	8854.84	7021.36	478.82	11.27
U084	8856.74	7021.68	475.27	5.79
U085	8833.10	7026.38	473.29	19.20
U086	8831.43	7024.75	472.26	7.62
U087	8831.23	7024.99	476.42	28.34
U088	8772.28	7172.98	457.29	17.37
U089	8772.85	7173.11	458.59	20.42
U090	8775.55	7174.45	459.83	22.56
U091	8762.25	7275.39	482.85	17.68
U092	8762.14	7275.42	482.45	30.78
U093	8762.35	7275.49	481.74	29.87
U094	8766.04	7277.43	482.57	38.30
U095	8766.04	7277.45	482.20	37.50
U096	8764.87	7276.85	481.42	14.94
U097	8785.94	7242.66	481.30	33.53
U098	8786.13	7242.79	480.55	21.03
U099	8789.77	7244.98	481.57	23.77
U100	8788.92	7244.64	480.15	9.14
U101	8789.86	7245.11	480.54	37.80
U102	8789.66	7244.95	482.67	31.09
U103	8788.05	7244.12	483.95	22.25
U104	8786.31	7242.93	480.86	46.63
U105	8766.06	7277.46	483.94	29.26
U106	8796.82	7205.07	479.82	30.48
U107	8797.11	7205.24	479.12	18.28
U108	8806.45	7211.06	479.77	8.53
U109	8806.10	7210.97	478.98	22.25
U110	8801.32	7205.60	479.05	18.89

U111	8800.94	7205.75	484.10	21.64
U112	8777.78	7207.80	483.85	22.56
U113	8776.11	7207.25	479.55	18.28
U114	8820.72	7202.51	450.59	17.67
U115	8820.88	7202.56	452.90	6.70
U116	8822.48	7201.12	450.74	11.89
U117	8825.00	7219.00	455.00	26.51
U118	8716.20	7185.50	421.00	14.02
U119	8822.17	6983.83	482.21	21.34
U120	8811.76	6974.51	485.04	24.38
U121	8799.32	6967.50	487.25	25.30
U122	8784.58	6965.18	489.90	23.16
U123	8770.47	6964.70	491.89	22.00
U124	8754.52	6965.69	494.91	17.37
U125	8750.87	6967.27	493.14	27.43
U126	8745.53	6966.62	494.04	28.95
U127	8774.19	7268.61	480.53	7.92
U128	8774.09	7259.02	484.66	19.81
U129	8776.10	7258.35	481.15	39.01
U130	8776.10	7259.96	481.01	9.14
U131	8763.00	7247.00	481.00	13.10
U132	8725.00	7192.00	419.60	8.53
U133	8725.00	7193.00	419.60	6.10
U134	8725.00	7192.00	421.00	15.24
U135	8754.00	7172.00	412.00	15.24
U137	8776.50	7289.29	484.14	14.57
U139	8799.60	7287.49	484.72	14.63
U140	8804.20	7278.31	483.72	24.38
U141	8810.09	7272.66	483.28	19.20
U143	8785.00	7255.50	481.00	44.20
U144	8701.71	7036.26	483.50	25.30
U145	8715.69	7046.40	483.48	27.12
U146	8694.03	7045.06	484.12	23.77
U147	8685.79	7022.14	483.20	26.82
U148	8671.30	7005.80	483.10	26.82
U149	8664.30	7017.30	483.40	25.90
U150	8675.50	7001.70	482.26	32.91
U151	8691.20	7017.30	482.10	24.38
U152	8764.00	7108.00	460.00	32.30
U153	8764.00	7108.00	460.00	19.81
U154	8764.00	7108.00	460.00	24.38
U155	8764.00	7108.00	460.00	42.67
U156	8790.00	7090.00	480.00	32.00
U157	8790.00	7090.00	480.00	24.38
U158	8790.00	7090.00	480.00	9.14
U159	8793.00	7095.00	480.00	18.29
U160	8793.00	7095.00	480.00	18.29
U161	8792.00	7277.00	493.00	17.68
U162	8802.00	7260.00	492.60	17.68
U163	8805.00	7255.00	482.00	14.02
U164	8733.30	7055.70	483.00	23.77
U165	8733.10	7056.80	483.10	21.34
U166	8740.32	7081.03	482.46	15.24
U167	8749.64	7070.40	483.34	29.32
U168	8844.00	6968.00	479.00	32.00
U169	8844.00	6968.00	479.00	41.45
U170	8770.00	7246.00	485.00	6.10
U171	8770.00	7246.00	485.00	19.20
U172	8770.00	7246.00	484.50	7.16
U173	8789.50	7225.50	484.00	21.34
U174	8740.10	7081.20	483.90	16.76
U175	8840.00	6975.00	481.00	26.52
U176	8670.00	7031.50	480.65	35.05
U177	8715.50	7046.80	482.90	40.84
U178	8665.90	7028.11	480.67	40.84
U179	8660.27	6823.11	488.39	38.40
U180	8660.43	6833.23	490.34	30.00
U181	8661.21	6824.23	491.84	23.77
U182	8663.44	6822.73	488.41	40.23
U183	8663.29	6822.79	489.12	32.00
U184	8775.00	7175.00	457.00	17.06
U185	8777.00	7175.00	460.00	21.64
U186	8637.83	7007.49	476.88	45.72
U187	8637.89	7007.55	476.24	35.35
U188	8627.87	7007.63	479.17	25.90
U189	8615.10	6933.01	481.36	63.09
U190	8614.78	6932.64	482.19	32.30

U191	8670.88	6809.10	486.32	39.93
U192	8671.28	6809.09	488.28	16.15
U193	8757.52	7064.74	488.09	19.20
U194	8683.13	7132.76	427.38	19.20
U195	8682.17	7131.92	427.82	23.16
U196	8681.79	7131.50	427.74	32.30
U197	8776.60	7238.20	491.00	15.84
U198	8776.60	7238.20	491.00	9.14
U199	8775.20	7221.50	491.00	31.40
U200	8635.39	6912.06	483.70	47.55
U201	8635.35	6912.27	483.16	47.24
U204	8702.80	6993.75	496.25	11.60
U205	8725.00	7000.00	496.00	24.69
U206	8725.00	7000.00	496.00	37.79
U208	8775.00	7183.00	457.00	31.09
U209	8725.00	7000.00	496.30	23.16
U210	8634.40	6859.32	482.32	23.47
U211	8634.18	6859.20	482.45	42.67
U212	8633.71	6859.00	483.42	27.43
U213	8634.97	6859.80	485.35	30.78
U214	8658.53	6787.62	481.07	15.24
U215	8658.60	6788.63	484.39	29.26
U216	8657.51	6788.09	483.89	26.51
U217	8657.56	6788.16	480.78	45.11
U218	8658.00	6787.00	481.00	39.01
U220	8765.60	7174.80	457.00	9.75
U221	8766.30	7174.90	458.70	3.65
U222	8769.40	7192.00	457.90	19.20
U223	8769.70	7192.00	459.60	16.15
U224	8675.00	7165.00	423.00	10.97
U225	8625.23	6882.69	477.18	35.35
U226	8625.00	6882.53	477.93	24.69
U227	8625.42	6882.86	479.88	32.00
U228	8679.30	7036.88	480.56	24.38
U229	8775.01	7292.81	473.65	16.46
U230	8775.11	7292.66	475.61	10.97
U231	8604.12	6948.66	468.55	7.92
U232	8604.95	6949.12	468.38	17.06
U233	8620.20	6948.61	482.78	13.41
U234	8625.96	6954.64	482.32	15.84
U235	8697.66	6974.58	497.00	28.65
U236	8697.66	6974.64	498.00	29.60
U237	8697.66	6974.60	496.00	10.67
U238	8758.89	7282.97	474.04	7.92
U239	8638.62	6984.65	479.40	38.70
U240	8597.34	6923.30	469.60	8.38
U241	8597.56	6923.32	468.86	13.41
U242	8631.41	6770.95	476.74	17.37
U243	8630.96	6772.33	473.27	24.69
U244	8635.51	6961.23	480.20	35.66
U245	8630.98	6772.26	472.59	40.54
U246	8628.00	6820.00	465.60	5.88
U247	8628.00	6820.00	464.00	10.67
U248	8630.00	6820.00	481.00	25.91
U249	8689.00	6983.00	496.00	46.33
U250	8645.00	7020.00	473.00	21.94
U251	8645.00	7020.00	474.00	31.40
U252	8645.00	7020.00	475.00	18.90
U253	8765.00	7216.00	458.00	16.15
U254	8765.00	7216.00	459.00	12.80
U255?	8798.00	7027.00	490.40	18.29
U256?	8812.00	7039.00	486.40	10.94
U257?	8803.00	7012.00	487.50	21.95
U258	8740.00	7011.00	498.00	13.40
U259	8740.00	7011.00	498.00	23.16
U260	8564.29	6745.22	475.67	39.62
U261	8564.41	6745.31	476.13	48.16
U262	8564.12	6745.43	477.46	43.90
U263	8835.81	7157.64	479.94	22.56
U264	8835.50	7157.38	479.25	16.15
U265	8679.00	7135.00	425.00	29.70
U266	8835.50	7157.38	479.25	24.38
U267	8808.06	7186.44	483.78	21.94
U268	8808.34	7186.92	481.76	11.00
U269	8808.19	7186.92	480.46	16.76
U270	8846.00	7209.00	414.70	30.48
U271	8846.00	7209.00	414.70	13.10
U272	8837.50	7225.00	415.50	34.75
U273	8837.50	7225.00	415.50	17.06
U274	8837.50	7225.00	415.50	25.29
U275	8845.00	7208.00	418.60	14.33
U276	8845.00	7185.00	404.70	28.04
U277	8845.00	7185.00	408.50	36.88
U278	8765.00	7237.00	459.20	23.00
U279	8765.00	7237.00	459.20	18.00
U280	8763.80	7257.00	460.50	23.00
U281	8763.80	7257.00	460.50	18.00
U282	8717.50	7180.50	420.00	27.43
U283	8717.50	7180.50	420.50	18.89
U284	8717.50	7180.50	420.50	30.40
U285	8717.50	7180.50	423.00	6.10
U286	8717.00	7158.00	417.50	8.23
U287	8717.00	7158.00	418.00	15.48
U288	8717.00	7158.00	419.50	15.24
U289	8766.50	7277.00	462.70	40.23
U290	8766.50	7277.00	462.70	24.38
U291	8775.40	7242.00	459.20	46.94
U292	8775.40	7242.00	459.70	65.84
U293	8777.20	7214.00	458.50	49.68
U294	8777.20	7214.00	459.00	54.25
U295	8811.60	7203.50	453.50	23.16
U296	8811.60	7203.50	454.00	18.90
U297	8777.00	7204.30	458.00	53.65
U298	8777.00	7204.30	458.50	51.21
U299	8777.50	7226.00	458.50	50.29
U301	8485.00	6755.00	481.00	16.46
U304	8485.00	6758.00	484.50	28.04
U305	8485.00	6758.00	482.50	47.85
U307	8623.00	6834.00	466.53	9.45
U309	8623.00	6834.00	465.00	42.67
U310	8623.00	6834.00	464.50	8.84
U311	8623.00	6834.00	470.00	5.79
U312	8623.00	6834.00	464.50	47.24
U314	8777.50	7226.00	459.00	48.77
U315	8771.40	7256.40	460.00	28.96
U316	8771.40	7256.40	461.00	53.95
U317	8771.00	7273.00	462.50	39.93
U318	8771.00	7273.00	463.00	42.67
U319	8831.50	7072.60	478.60	22.86
U320	8832.60	7073.00	473.70	16.76
U321	8832.60	7073.00	474.00	14.32
U322	8832.60	7073.00	474.30	12.41
U324	8833.80	7056.60	471.12	6.10
U325	8835.00	7057.20	473.00	15.54
U326	8835.00	7057.20	473.30	12.80
U330	8242.03	6713.32	488.21	13.72
U331	8242.03	6713.32	488.21	7.93
U332	8242.06	6713.31	489.33	7.62
U333	8257.76	6761.48	495.02	10.80
U334	8257.86	6761.54	493.99	34.74
U336	8804.00	7173.00	454.00	23.77
U337	8804.00	7173.00	454.00	26.82
U500	8633.65	7052.48	453.09	60.66
U501	8633.57	7052.50	453.84	25.30
U502	8633.57	7052.50	453.84	21.94
U503	8632.37	7050.38	453.20	72.54
U504	8632.41	7050.37	454.15	24.99
U505	8632.43	7050.37	454.70	20.73
U506	8627.69	7043.34	454.82	57.00
U507	8627.61	7043.42	455.89	18.59
U508	8614.32	7033.77	456.41	27.43
U509	8614.11	7033.97	457.26	14.63
U510	8612.82	7025.22	457.15	14.63
U511	8612.84	7025.21	457.95	11.28
U512	8609.71	7017.92	458.34	9.45
U513	8609.62	7018.00	459.50	7.62
U514	8607.33	7010.89	459.80	11.28
U515	8607.22	7010.94	461.00	7.92
U516	8602.38	6999.58	461.45	9.75
U517	8602.37	6999.65	462.91	5.49
U518	8640.75	7044.24	465.89	30.18
U519	8640.65	7044.15	467.56	17.68
U520	8636.63	7036.83	466.01	25.60
U521	8636.42	7037.36	467.46	17.37
U522	8628.74	7026.43	466.23	17.98
U523	8628.33	7026.60	467.90	9.14
U524	8623.43	7020.28	466.15	19.81
U525	8623.40	7020.20	468.21	8.84
U526	8622.36	7015.12	466.51	18.90
U527	8622.41	7015.14	468.16	10.97
U528	8615.58	7009.40	468.44	10.06
U529	8615.76	7001.20	468.64	11.58
U530	8588.73	6771.09	469.53	19.20
U531	8590.97	6768.61	470.98	13.11
U532	8592.26	6768.73	469.48	17.37
U533	8591.90	6768.23	471.42	16.76
U534	8563.72	6774.51	469.86	30.18
U535	8563.32	6774.32	471.99	27.43
U536	8563.68	6774.45	470.23	13.11
U537	8563.91	6774.05	471.80	11.28
U538	8511.73	6776.22	474.53	17.68
U539	8507.70	6776.65	471.94	8.23
U540	8504.94	6776.43	473.55	19.51
U541	8511.62	6776.42	471.94	9.14
U542	8509.97	6776.29	473.74	14.02
U543	8531.49	6775.88	471.36	10.06
U544	8531.62	6775.62	473.11	14.02
U545	8494.28	6780.02	472.48	8.23
U546	8481.64	6787.50	473.60	10.06
U547	8481.68	6787.31	475.25	6.71
U548	8471.18	6792.52	473.25	11.58
U549	8471.40	6792.74	475.52	11.89
U550	8459.70	6801.89	472.25	8.54
U551	8459.58	6801.73	473.95	9.76
U552	8603.05	6955.03	460.57	6.10
U553	8603.69	6955.05	462.65	5.49
U554	8570.00	6772.00	470.00	15.24
U555	8604.68	6984.90	461.66	8.23
U556	8883.14	6978.36	475.28	35.06
U557	8883.08	6978.32	477.47	9.45
U558	8906.02	6977.69	473.80	41.45
U559	8906.05	6977.80	475.85	22.87
U560	8934.71	6988.81	471.59	37.50
U561	8935.10	6988.59	472.83	36.58
U562	8934.71	6989.11	470.87	52.13
U563	8940.39	6990.93	471.81	42.99
U564	8940.31	6990.97	470.81	53.96
U565	8971.30	7000.99	469.28	70.12
U566	8971.27	7001.14	469.81	61.59
U567	8971.11	7001.32	470.52	60.98
U568	8106.24	6683.22	467.91	30.49
U569	8106.02	6683.00	468.63	31.70
U570	8124.72	6686.81	470.13	24.08
U571	8124.67	6686.60	470.13	21.34
U572	8142.46	6687.03	473.30	14.94
U573	9086.87	7124.97	464.00	45.42
U574	9086.01	7124.87	465.79	42.06
U575	9089.50	7156.00	467.00	35.97
U576	9089.50	7156.00	467.00	32.00
U577	9094.00	7158.00	466.00	55.17
U578	9094.00	7158.00	467.00	41.76
U579	9094.00	7158.00	467.50	37.49
U583	8432.85	6817.81	469.04	8.23
U584	8432.79	6817.80	470.91	6.10
U585	8417.49	6821.75	467.46	13.72
U586	8417.39	6821.58	469.60	9.75
U587	8402.76	6829.02	464.72	11.28
U588	8402.78	6828.90	467.28	9.14
U589	8389.75	6837.63	463.61	6.71
U590	8389.62	6837.34	465.77	3.96
U591	8362.10	6820.35	463.62	65.53
U592	8362.20	6820.07	464.90	36.58
U593	8360.82	6819.51	463.54	40.23
U594	8361.46	6819.02	464.87	27.13
U595	8565.03	6785.84	449.73	29.87
U596	8567.39	6784.73	449.88	28.96
U597	8485.00	6801.00	441.86	23.47
U598	8485.00	6801.00	442.36	12.50
U599	8517.00	6793.00	443.20	16.76
U600	8517.00	6793.00	443.70	9.45
U601	8047.43	6679.93	459.17	59.74

U602	8044.83	6676.59	460.86	48.77
U603	8043.51	6675.86	459.15	69.80
U604	8043.52	6676.02	460.47	51.20
U605	8042.69	6675.66	459.12	61.87
U606	8042.66	6675.73	460.35	26.85
U607	8042.30	6671.96	459.00	36.88
U608	8042.34	6671.99	460.00	32.61
U609	8042.58	6671.21	459.10	44.19
U610	8042.55	6671.18	459.72	38.40
U611	8045.72	6621.91	455.69	50.59
U612	8046.01	6621.74	457.51	41.45
U613A	8045.34	6621.39	455.99	44.50
U614	8045.85	6621.40	457.50	41.76
U615	8314.03	6797.36	466.33	67.36
U616	8311.19	6796.40	466.36	82.30
U617	8453.17	6811.46	438.89	32.31
U618	8452.93	6811.12	441.22	18.29
U619	8434.92	6816.58	435.34	35.37
U620	8434.78	6816.09	437.23	26.22
U621	8415.83	6819.03	432.16	45.72
U622	8415.69	6818.59	434.27	29.26
U623	8396.42	6822.52	430.42	53.34
U624	8396.36	6822.40	432.23	35.05
U625	8080.11	6724.14	430.65	46.33
U626	8076.84	6720.35	431.98	36.59
U627	8071.88	6739.22	431.44	30.48
U628	8071.88	6739.24	433.55	21.34
U629	8070.66	6739.69	431.46	32.01
U630	8070.68	6738.90	433.41	21.34
U631	8025.25	6694.75	426.68	46.64
U632	8025.25	6694.75	427.75	29.27
U633	8025.25	6691.50	426.77	48.78
U634	8025.25	6691.50	428.85	29.38
U635	8025.24	6695.90	427.70	55.17
U636	8026.48	6695.61	426.99	101.50
U637	8027.69	6695.46	427.44	71.32
U638	8029.48	6695.33	427.48	67.67
U639	8123.80	6694.72	441.04	49.09
U640	8123.76	6694.36	441.58	37.19
U641	8587.17	6793.50	428.68	40.54
U642	8578.54	6829.65	423.63	40.54
U643	8578.44	6829.73	424.86	19.20
U644	8595.02	6832.18	424.19	28.04
U645	8022.04	6692.95	427.38	37.49
U646	8022.01	6693.12	427.36	38.71
U647	8022.11	6693.47	427.36	41.76
U648	8022.00	6691.94	427.40	39.62
U649	8021.97	6692.19	427.35	38.10
U650	8021.83	6691.58	427.38	45.11
U651	8412.00	6868.00	423.73	9.14
U804R1	7978.50	6663.60	416.00	21.00
H1				
U804R1	7978.50	6663.60	416.50	19.50
H2				
U804R1	7978.50	6663.60	417.00	17.40
H3				
U804R1	7978.50	6663.60	417.50	18.90
H4				
U804R1	7978.50	6663.60	418.00	22.90
H5				
U804R2	7985.40	6664.80	417.00	24.10
H1				
U804R2	7985.40	6664.80	417.80	20.40
H2				
U804R2	7985.40	6664.80	418.20	24.70
H3				
U804R2	7985.40	6664.80	418.60	28.30
H4				
U804R2	7985.40	6664.80	419.20	20.70
H5				
U804R3	7985.40	6665.50	418.60	21.30
H4				
U804R3	7985.40	6665.50	419.10	16.80
H5				
U808R1	8099.70	6757.70	421.00	30.49
H1				
U808R2	8099.20	6758.00	421.00	19.82
H1				
U808R2	8099.20	6758.00	421.60	23.78
H2				
U808R3	8098.60	6758.40	421.00	16.16
H1				
U808R3	8098.60	6758.40	421.60	17.38
H2				
U808R3	8098.60	6758.40	422.20	14.33
H3				
U808R3	8098.60	6758.40	422.80	11.28
H4				
U808R3	8098.60	6758.40	423.40	9.76
H5				
U808R4	8098.20	6758.60	421.00	20.73
H1				
U808R4	8098.20	6758.60	421.60	17.07
H2				

Hole Orientation

Hole	Azim	Dip
D11801	193	0
D11802	205	0
D11803	205	40
D11804	205	36
D11820	180	25
D11821	180	25
D11822	180	28
D11823	180	26
D11824	180	26
D11825	180	25
D11826	180	25
D11827	225	0
D11828	225	20
D11829	225	37
D11830	185	0
D11831	185	30
D11832	185	37
D11833	141	30
D11834	141	40
D11835	141	45
D11836	113	45
D11837	113	40
D11838	129	45
D11839	129	40
D11840	129	30
D11841	129	28
D11842	129	24
D119C1	219	21
D119C2	219	22
D119C3	219	35
D119C4	219	45
GA10A	180	-90
GA10B	180	-90
GA11	180	-90
GA12	180	-90
GA13	180	-90
GA14A	180	-90
GA14B	180	-90
GA15	180	-90
GA16	180	-90
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S942	0	-90	U052	180	90	U130	243	-60	U213	242	40	U291	58	0	U541	35	0
S943	0	-90	U053	180	-90	U131	180	-90	U214	181	-18	U292	60	15	U542	0	45
S944	0	-90	U054	180	90	U132	287	0	U215	180	90	U293	60	0	U543	350	0
S945	0	-90	U055	180	-90	U133	307	0	U216	235	30	U294	60	15	U544	350	45
S946	180	-47	U056	286	0	U134	287	35	U217	235	-20	U295	62	0	U545	14	0
S947	0	-90	U057	325	0	U135	259	20	U218	235	0	U296	65	25	U546	13	0
S948	0	-90	U058	89	65	U137	7	0	U220	276	0	U297	61	0	U547	13	45
S949	0	-90	U059	96	0	U139	41	0	U221	276	45	U298	61	20	U548	21	0
S950	0	-90	U060	180	-90	U140	41	0	U222	271	0	U299	67	0	U549	21	45
S951	0	-90	U061	180	90	U141	89	0	U223	271	45	U301	280	0	U550	27	0
S952	0	-90	U062	59	0	U143	125	0	U224	345	38	U304	180	90	U551	27	45
S953	0	-90	U063	293	0	U144	180	90	U225	231	-30	U305	340	45	U552	270	0
S954	0	-90	U064	270	-29	U145	180	90	U226	231	0	U307	240	30	U553	270	45
S955	0	-90	U065	180	-90	U146	180	90	U227	197	45	U309	240	-40	U554	358	0
S956	0	-90	U066	82	0	U147	180	90	U228	322	-4	U310	240	-70	U555	252	0
S957	0	-90	U067	127	0	U148	180	90	U229	301	0	U311	240	90	U556	13	0
S958	0	-90	U068	180	90	U149	0	90	U230	301	45	U312	240	-50	U557	13	45
S959	0	-90	U069	61	0	U150	140	45	U231	241	0	U314	60	10	U558	347	0
S960	0	-90	U070	180	90	U151	120	45	U232	241	-30	U315	60	10	U559	347	45
S961	0	-90	U071	180	90	U152	135	37	U233	268	25	U316	59	-10	U560	310	20
S962	0	-90	U073	303	0	U153	118	37	U234	309	25	U317	61	0	U561	310	45
S963	0	-90	U074	25	45	U154	130	37	U235	255	-10	U318	60	10	U562	320	0
S964	0	-90	U075	180	90	U155	146	37	U236	255	30	U319	180	90	U563	328	25
S965	0	-90	U076	114	0	U156	64	5	U237	255	-30	U320	62	-30	U564	328	0
S966	0	-90	U077	148	0	U157	45	5	U238	324	0	U321	69	0	U565	318	0
TEST	0	-90	U078	220	0	U158	64	15	U239	274	0	U322	65	30	U566	318	16
U001	270	0	U079	237	0	U159	45	15	U240	312	0	U324	180	-90	U567	318	35
U002	270	45	U080	237	-45	U160	40	30	U241	312	-30	U325	68	0	U568	23	0
U003	303	45	U081	57	-2	U161	180	-90	U242	180	90	U326	64	30	U569	22	20
U004	305	0	U082	180	-90	U162	180	-90	U243	316	0	U330	294	0	U570	12	0
U005	180	90	U083	180	90	U163	135	0	U244	306	-30	U331	319	0	U571	12	18
U006	265	0	U084	74	0	U164	180	90	U245	334	-25	U332	299	40	U572	24	0
U007	91	8	U085	60	0	U165	135	45	U246	240	0	U333	265	0	U573	310	0
U008	52	0	U086	180	-90	U166	346	0	U247	240	-30	U334	260	-40	U574	310	45
U009	75	-7	U087	180	90	U167	131	40	U248	180	90	U336	60	20	U575	301	0
U010	37	0	U088	240	0	U168	122	10	U249	270	-60	U337	60	-5	U576	301	40
U011	17	-15	U089	240	45	U169	90	5	U250	330	-30	U500	317	0	U577	346	0
U012	180	90	U090	57	70	U170	180	-90	U251	330	0	U501	317	25	U578	346	21
U013	180	-90	U091	242	0	U171	270	40	U252	330	45	U502	317	35	U579	346	45
U014	180	-90	U092	242	-26	U172	270	6	U253	270	0	U503	306	0	U583	28	0
U015	180	90	U093	242	-55	U173	240	40	U254	270	45	U504	306	25	U584	28	45
U016	180	-90	U094	61	0	U174	345	40	U255?	0	90	U505	306	35	U585	26	0
U017	180	90	U095	61	-28	U175	180	90	U256?	0	90	U506	302	0	U586	26	45
U018	180	-90	U096	61	-55	U176	357	-11	U257?	0	90	U507	302	27	U587	28	0
U019	180	90	U097	238	0	U177	131	40	U258	330	60	U508	299	0	U588	28	45
U020	180	-90	U098	238	-45	U178	350	10	U259	330	30	U509	299	27	U589	26	0
U021	180	90	U099	58	0	U179	245	0	U260	330	-15	U510	294	0	U590	26	45
U022	180	-90	U100	58	-60	U180	245	40	U261	330	0	U511	294	27	U591	305	0
U023	180	90	U101	58	-32	U181	180	90	U262	330	30	U512	288	0	U592	305	27
U024	180	90	U102	58	38	U182	174	5	U263	61	0	U513	288	27	U593	333	0
U025	180	90	U103	180	90	U183	180	10	U264	61	12	U514	280	0	U594	333	30
U026	180	90	U104	237	-24	U184	240	0	U265	135	72	U515	280	27	U595	330	0
U027	180	90	U105	60	25	U185	180	90	U266	61	-15	U516	273	0	U596	25	1
U028	180	90	U106	237	0	U186	240	0	U267	55	65	U517	273	27	U597	25	0
U029	180	90	U107	236	-35	U187	240	-20	U268	60	25	U518	317	0	U598	25	45
U030	180	90	U108	57	0	U188	240	40	U269	59	-35	U519	317	27	U599	23	0
U031	180	-90	U109	57	-45	U189	226	-40	U270	60	0	U520	302	0	U600	23	45
U032	275	-12	U110	180	-90	U190	226	0	U271	60	40	U521	302	27	U601	1	1
U033	180	-90	U111	180	90	U191	241	12	U272	60	0	U522	299	0	U602	357	27
U034	180	90	U112	180	90	U192	233	60	U273	60	40	U523	299	27	U603	343	-1
U035	180	90	U113	180	-90	U193	180	90	U274	0	90	U524	294	0	U604	345	27
U036	180	90	U114	31	0	U194	60	40	U275	0	90	U525	294	27	U605	321	1
U037	180	90	U115	31	45	U195	180	90	U276	60	45	U526	288	0	U606	320	27

U607	255	-1
U608	256	21
U609	239	0
U610	239	14
U611	283	0
U612	279	39
U613A	262	0
U614	260	30
U615	332	0
U616	301	0
U617	12	0
U618	7	42
U619	10	-1
U620	14	44
U621	10	0
U622	10	44
U623	6	0
U624	4	42
U625	40	1
U626	37	26
U627	36	0
U628	35	43
U629	356	0
U630	354	42
U631	283	0
U632	283	30
U633	247	0
U634	250	25
U635	324	22
U636	333	4
U637	347	18
U638	3	16
U639	0	2
U640	359	17
U641	334	20
U642	320	4
U643	319	27
U644	319	41
U645	268	2
U646	271	0
U647	279	1
U648	249	2
U649	255	0
U650	242	1
U651	9	0
U804R1H1	284	0
U804R1H2	284	6
U804R1H3	284	12
U804R1H4	284	18
U804R1H5	284	24
U804R2H1	287	0
U804R2H2	287	6
U804R2H3	287	12
U804R2H4	287	18
U804R2H5	287	24
U804R3H4	294	18
U804R3H5	294	24
U808R1H1	35	0
U808R2H1	25	0
U808R2H2	25	6
U808R3H1	18	0
U808R3H2	18	6
U808R3H3	18	12
U808R3H4	18	18
U808R3H5	18	24
U808R4H1	10	0
U808R4H2	10	6

Geology

Legend:

7. Overburden – Till, Sand, Silt

6. 'Trench': Collapse Breccia, Ancient Till

5. Carroll's Corner Formation:
Evaporites – Anhydrite, Gypsum, Siltstone, Dolomite, Limestone

4. Gays River Formation (MacCumber):
Carbonates – Dolomite, Limestone

3. Horton Formation:
Sediments – Shale, Siltstone, Sandstone, Conglomerate

2. Breccia: Goldenville Clast in Dolomite Matrix

1. Goldenville Formation
Metasediments – Greywacke, Slates

Hole	From (m)	To (m)	Geo
D11801	0.00	78.40	1a
D11801	78.40	81.90	2
D11801	81.90	84.60	4a
D11801	84.60	88.70	2
D11801	88.70	120.09	1a
D11802	0.00	69.49	1a
D11802	69.49	70.87	2
D11802	70.87	75.29	4d
D11802	75.29	86.56	4a
D11802	86.56	88.39	4d
D11802	88.39	106.07	2
D11802	106.07	121.31	1a
D11803	0.00	34.75	1a
D11803	34.75	35.60	2
D11803	35.60	37.45	4a
D11803	37.45	38.15	4c
D11803	38.15	39.01	6a
D11803	39.01	42.37	5a
D11804	0.00	36.05	1a
D11804	36.05	37.10	2
D11804	37.10	38.87	4a
D11804	38.87	40.09	4c
D11804	40.09	40.84	5a
D11820	0.00	19.00	1a
D11820	19.00	19.90	2
D11820	19.90	22.07	4a
D11820	22.07	22.24	6a
D11820	22.24	23.47	5a
D11821	0.00	17.00	1a
D11821	17.00	19.15	2
D11821	19.15	21.10	4a
D11821	21.10	22.64	6a
D11821	22.64	24.99	5a
D11822	0.00	17.68	1a
D11822	17.68	19.70	2
D11822	19.70	21.50	4a
D11822	21.50	22.25	6a
D11823	0.00	18.40	1a
D11823	18.40	20.10	2
D11823	20.10	21.80	4a
D11823	21.80	22.50	6a
D11823	22.50	22.56	5a
D11824	0.00	19.10	1a
D11824	19.10	19.80	2
D11824	19.80	21.85	4a
D11824	21.85	21.95	6a
D11825	0.00	20.10	1a
D11825	20.10	22.22	4a
D11825	22.22	22.25	6a
D11826	0.00	19.65	1a
D11826	19.65	20.30	2
D11826	20.30	22.80	4a
D11826	22.80	23.38	6a
D11826	23.38	23.78	5a
D11827	0.00	7.20	1a
D11827	7.20	10.75	4a
D11827	10.75	26.22	5a
D11828	0.00	5.30	1a
D11828	5.30	5.60	2
D11828	5.60	6.10	4d
D11828	6.10	14.02	5a
D11829	0.00	4.60	1a
D11829	4.60	4.75	2
D11829	4.75	5.15	4d
D11829	5.15	9.45	5a
D11830	0.00	5.45	1a
D11830	5.45	6.45	4d
D11830	6.45	8.05	4a
D11830	8.05	10.68	5a
D11831	0.00	1.52	1a
D11831	1.52	3.25	1a
D11831	3.25	4.35	4d
D11831	4.35	8.54	5a
D11832	0.00	2.75	1a
D11832	2.75	3.80	4a
D11832	3.80	6.71	5a
D11833	0.00	7.00	1a
D11833	7.00	7.62	2
D11833	7.62	10.65	4a
D11833	10.65	11.10	6a
D11833	11.10	11.28	5a
D11834	0.00	6.05	1a
D11834	6.05	8.30	4d
D11834	8.30	8.54	6a
D11835	0.00	6.20	1a
D11835	6.20	7.60	4a
D11835	7.60	8.85	6a
D11835	8.85	9.15	5a
D11836	0.00	9.00	1a
D11836	9.00	12.40	2
D11836	12.40	12.65	4a
D11836	12.65	13.20	4c
D11836	13.20	13.85	4a
D11836	13.85	15.24	6a
D11837	0.00	11.20	1a
D11837	11.20	13.10	2
D11837	13.10	13.60	4d
D11837	13.60	14.15	4a
D11837	14.15	14.70	4d
D11837	14.70	16.50	4a
D11837	16.50	17.07	6a
D11838	0.00	9.75	1a
D11838	9.75	10.75	2
D11838	10.75	11.45	4a
D11838	11.45	11.85	4c
D11838	11.85	12.30	4a
D11838	12.30	12.80	6a
D11839	0.00	11.00	1a
D11839	11.00	11.60	2
D11839	11.60	12.35	4d
D11839	12.35	14.45	4a
D11839	14.45	15.85	6a
D11840	0.00	9.15	1a
D11840	9.15	12.35	2
D11840	12.35	13.85	4a
D11840	13.85	14.00	4c
D11840	14.00	16.75	4a
D11840	16.75	17.00	4c
D11840	17.00	18.29	6a
D11841	0.00	13.20	1a
D11841	13.20	17.70	4a
D11841	17.70	18.65	4d
D11841	18.65	19.45	6a
D11841	19.45	20.12	5a
D11842	0.00	12.50	1a
D11842	12.50	15.60	2
D11842	15.60	29.27	4a
D119C3	0.00	33.65	1a
D119C3	33.65	36.05	2
D119C3	36.05	38.07	4a
D119C3	38.07	39.32	4c
D119C3	39.32	43.85	5a
D119C4	0.00	34.00	1a
D119C4	34.00	34.92	2
D119C4	34.92	36.50	4a
D119C4	36.50	37.10	4c
D119C4	37.10	39.32	5a
GA10A	0.00	66.14	
GA10B	0.00	66.14	
GA11	0.00	66.14	
GA12	0.00	66.14	
GA13	0.00	66.14	
GA14A	0.00	66.14	
GA14B	0.00	66.14	
GA15	0.00	66.14	
GA16	0.00	66.14	
GA17	0.00	66.14	
GA18	0.00	66.14	
GA19	0.00	66.14	
GA1A	0.00	66.14	
GA1B	0.00	66.14	
GA2	0.00	66.14	
GA20	0.00	66.14	
GA21	0.00	66.14	
GA22A	0.00	66.14	
GA22B	0.00	66.14	
GA23	0.00	66.14	
GA24	0.00	66.14	
GA25	0.00	66.14	
GA26	0.00	66.14	
GA27	0.00	66.14	
GA28A	0.00	66.14	
GA28B	0.00	66.14	
GA3	0.00	66.14	
GA4	0.00	66.14	
GA5	0.00	66.14	
GA6	0.00	66.14	
GA7	0.00	66.14	
GA8A	0.00	66.14	
GA8B	0.00	66.14	
GA9A	0.00	66.14	
GA9B	0.00	66.14	
S001	0.00	6.10	4b
S001	6.10	7.92	2
S002	0.00	2.13	7
S002	2.13	10.97	1a
S003	0.00	3.05	7
S003	3.05	16.76	4b
S003	16.76	22.86	1a
S004	0.00	1.52	7
S004	1.52	8.53	4b
S004	8.53	10.97	1a
S005	0.00	3.05	7
S005	3.05	5.18	4b
S005	5.18	10.67	4a
S005	10.67	25.30	4b
S005	25.30	34.14	2
S005	34.14	38.10	1a
S006	0.00	3.05	7
S006	3.05	10.06	4b
S006	10.06	13.41	1a
S007	0.00	8.23	7
S007	8.23	31.09	4b
S007	31.09	35.66	1a
S008	0.00	3.05	7
S008	3.05	12.80	4b
S008	12.80	15.85	2
S009	0.00	1.22	7
S009	1.22	14.63	4b
S009	14.63	15.85	1a
S010	0.00	2.74	7
S010	2.74	4.57	4b
S010	4.57	5.79	2
S011	0.00	7.01	7
S011	7.01	24.69	4b
S011	24.69	26.82	2
S011	26.82	28.96	1a
S012	0.00	1.22	7
S012	1.22	16.15	4b
S012	16.15	19.81	2
S013	0.00	16.46	7
S013	16.46	35.97	4b
S013	35.97	37.80	1a
S014	0.00	1.52	7
S014	1.52	12.19	4b
S014	12.19	12.50	2
S014	12.50	16.15	1a
S015	0.00	1.52	7
S015	1.52	8.69	4b
S015	8.69	9.45	1a
S016	0.00	2.44	7
S016	2.44	9.45	4b
S016	9.45	12.50	1a
S017	0.00	11.58	7
S017	11.58	21.03	4b
S017	21.03	23.77	2
S018	0.00	1.83	7

S018	1.83	3.66	4b
S018	3.66	3.96	4e
S018	3.96	19.20	4b
S018	19.20	19.51	1a
S019	0.00	3.05	7
S019	3.05	22.86	4b
S019	22.86	23.16	2
S019	23.16	25.91	1a
S020	0.00	19.81	7
S020	19.81	21.64	4b
S020	21.64	23.16	2
S020	23.16	29.26	1a
S021	0.00	3.05	7
S021	3.05	16.76	4b
S021	16.76	19.51	2
S021	19.51	21.95	1a
S022	0.00	3.05	7
S022	3.05	9.75	4b
S022	9.75	12.19	2
S022	12.19	15.85	1a
S023	0.00	3.96	7
S023	3.96	23.32	4b
S023	23.32	25.91	2
S023	25.91	26.21	1a
S024	0.00	3.66	7
S024	3.66	17.22	4b
S024	17.22	25.91	2
S025	0.00	3.66	7
S025	3.66	15.24	4b
S025	15.24	22.86	2
S026	0.00	3.35	7
S026	3.35	4.57	4b
S026	4.57	10.36	1a
S027	0.00	3.96	7
S027	3.96	28.35	4b
S027	28.35	31.70	2
S028	0.00	8.84	7
S028	8.84	19.51	4b
S028	19.51	21.34	2
S028	21.34	24.99	1a
S029	0.00	14.94	7
S029	14.94	24.08	4b
S029	24.08	25.30	4e
S029	25.30	28.35	4b
S029	28.35	28.96	4e
S029	28.96	29.57	4b
S030	0.00	4.27	7
S030	4.27	19.51	4b
S030	19.51	26.82	2
S031	0.00	7.62	7
S031	7.62	21.95	4b
S031	21.95	22.86	2
S032	0.00	7.62	7
S032	7.62	20.73	4b
S032	20.73	25.91	2
S032	25.91	29.26	1a
S033	0.00	3.05	7
S033	3.05	10.67	4b
S033	10.67	15.85	2
S033	15.85	20.42	1a
S034	0.00	2.74	7
S034	2.74	15.85	4b
S034	15.85	20.73	2
S035	0.00	4.88	7
S035	4.88	29.87	4b
S035	29.87	33.53	2
S036	0.00	9.75	7
S036	9.75	18.59	4b
S036	18.59	24.38	2
S036	24.38	26.21	1a
S037	0.00	13.41	7
S037	13.41	15.54	4b
S037	15.54	18.59	2
S037	18.59	19.51	1a
S038	0.00	4.27	7
S038	4.27	22.71	4b
S038	22.71	24.99	2
S040	0.00	2.74	7
S040	2.74	28.35	4b
S040	28.35	35.36	2
S041	0.00	11.89	7
S041	11.89	17.07	4b
S041	17.07	19.81	2
S041	19.81	23.77	1a
S042	0.00	14.02	7
S042	14.02	17.83	4a
S042	17.83	22.25	1a
S043	0.00	17.98	7
S043	17.98	33.53	4b
S043	33.53	36.58	1a
S044	0.00	25.60	7
S044	25.60	27.43	4b
S044	27.43	41.15	2
S044	41.15	41.76	1a
S045	0.00	23.16	7
S045	23.16	28.96	1a
S046	0.00	22.86	7
S046	22.86	28.96	4a
S046	28.96	35.36	1a
S047	0.00	29.57	7
S048	0.00	25.60	7
S048	25.60	32.61	4a
S048	32.61	44.81	4b
S048	44.81	45.11	1a
S049	0.00	41.45	7
S049	41.45	42.98	4e
S049	42.98	43.59	4a
S049	43.59	69.49	4e
S049	69.49	71.93	1a
S050	0.00	40.84	7
S050	40.84	46.02	4b
S050	46.02	69.95	4a
S050	69.95	71.32	2
S051	0.00	30.48	7
S051	30.48	33.68	4b
S051	33.68	35.05	4a
S051	35.05	67.06	4b
S051	67.06	72.54	2
S052	0.00	37.19	7
S052	37.19	47.55	4b
S052	47.55	54.56	4a
S052	54.56	68.58	4b
S052	68.58	77.72	1a
S053	0.00	51.51	7
S054	0.00	36.58	7
S054	36.58	60.05	4b
S054	60.05	61.57	1a
S055	0.00	39.93	7
S055	39.93	59.44	4b
S055	59.44	79.25	4a
S055	79.25	82.30	4b
S055	82.30	84.43	1a
S056	0.00	60.96	7
S056	60.96	82.30	5b
S056	82.30	99.97	4b
S056	99.97	103.02	2
S056	103.02	106.07	1a
S057	0.00	44.50	7
S057	44.50	52.43	4b
S057	52.43	55.47	4e
S057	55.47	59.44	4b
S057	59.44	59.89	4a
S057	59.89	60.66	4b
S057	60.66	81.08	4a
S057	81.08	88.39	4b
S057	88.39	90.22	1a
S058	0.00	63.40	7
S058	63.40	66.14	5b
S058	66.14	90.22	6a
S058	90.22	100.89	4a
S058	100.89	104.55	4b
S058	104.55	106.07	2
S059	0.00	81.69	7
S060	0.00	34.44	7
S060	34.44	35.66	4b
S060	35.66	39.78	4a
S060	39.78	42.67	4b
S060	42.67	43.59	1a
S061	0.00	36.58	7
S061	36.58	60.96	4a
S061	60.96	66.14	2
S061	66.14	69.19	1a
S062	0.00	35.05	7
S062	35.05	52.58	4a
S062	52.58	54.86	4b
S062	54.86	56.69	2
S063	0.00	87.48	7
S063	87.48	92.35	4a
S063	92.35	94.03	4b
S063	94.03	94.95	4a
S063	94.95	100.58	4b
S063	100.58	101.19	1a
S064	0.00	94.49	7
S064	94.49	103.63	5b
S064	103.63	111.86	4a
S064	111.86	112.01	4b
S064	112.01	117.96	4a
S064	117.96	118.87	4b
S064	118.87	120.40	4a
S064	120.40	121.01	1a
S065	0.00	40.84	7
S065	40.84	53.95	4b
S065	53.95	76.81	4a
S065	76.81	77.42	2
S065	77.42	79.25	1a
S067	0.00	21.95	7
S068	0.00	7.01	7
S068	7.01	15.24	5b
S068	15.24	21.95	5a
S068	21.95	25.60	5b
S068	25.60	88.70	5a
S068	88.70	92.96	5c
S068	92.96	96.62	5b
S068	96.62	97.84	5c
S068	97.84	98.45	5b
S068	98.45	99.52	4a
S068	99.52	105.77	1a
S069	0.00	71.93	7
S069	71.93	73.46	4b
S069	73.46	75.59	4a
S070	0.00	11.28	7
S070	11.28	20.42	5b
S070	20.42	92.05	5a
S070	92.05	93.88	5b
S070	93.88	94.34	2
S070	94.34	96.62	1a
S071	0.00	36.58	7
S071	36.58	60.66	4a
S071	60.66	62.03	4b
S071	62.03	67.06	1a
S072	0.00	57.91	7
S072	57.91	66.75	5b
S072	66.75	69.19	5d
S072	69.19	71.02	5b
S072	71.02	96.93	6a
S072	96.93	102.11	4b
S072	102.11	102.41	2
S072	102.41	105.77	1a
S073	0.00	20.42	7
S073	20.42	24.99	5b
S073	24.99	114.60	5a
S073	114.60	117.96	5b
S073	117.96	119.48	4a
S073	119.48	123.75	1a
S074	0.00	34.44	7
S074	34.44	71.93	5b
S074	71.93	72.85	2
S074	72.85	78.64	1a
S075	0.00	14.33	7
S075	14.33	21.64	5b
S075	21.64	124.82	5a
S075	124.82	126.80	5b
S075	126.80	128.02	4a
S075	128.02	128.32	4a
S075	128.32	131.06	4a
S075	131.06	131.37	2
S075	131.37	135.94	1a
S076	0.00	36.58	7
S076	36.58	44.20	4a
S076	44.20	47.85	1a
S077	0.00	34.44	7
S077	34.44	60.50	4a
S077	60.50	61.26	2
S077	61.26	62.18	2
S077	62.18	66.45	1a
S078	0.00	54.25	7
S079	0.00	44.50	7
S080	0.00	48.77	7
S080	48.77	51.21	5b
S080	51.21	53.04	5d
S080	53.04	57.30	6b
S080	57.30	69.49	6b
S080	69.49	72.54	4b
S080	72.54	78.79	4a
S080	78.79	80.77	4b
S080	80.77	83.82	4a
S080	83.82	89.00	4b
S080	89.00	91.74	2
S080	91.74	94.49	1a
S081	0.00	44.50	7
S081	44.50	65.84	4b
S081	65.84	66.45	4a
S081	66.45	67.06	4b
S081	67.06	69.49	4a
S081	69.49	74.07	4b
S081	74.07	83.52	4a
S081	83.52	84.12	2
S081	84.12	87.78	1a
S082	0.00	34.75	7
S082	34.75	64.62	4a
S082	64.62	68.88	2
S082	68.88	74.68	1a
S083	0.00	59.44	7
S083	59.44	60.96	2
S083	60.96	65.84	1a
S084	0.00	22.86	7
S084	22.86	28.04	1a
S085	0.00	36.88	7
S085	36.88	36.94	5b
S085	36.94	71.48	4a
S085	71.48	72.09	2
S085	72.09	75.29	1a
S086	0.00	53.64	7
S086	53.64	55.17	5b
S086	55.17	56.69	5d
S086	56.69	62.79	5b
S086	62.79	63.40	5d
S086	63.40	64.31	2
S086	64.31	75.29	1a
S087	0.00	50.90	7
S087	50.90	65.23	4b
S087	65.23	86.56	4a
S087	86.56	87.48	1a
S088	0.00	41.45	7
S088	41.45	44.04	4b
S088	44.04	47.55	4a
S088	47.55	53.34	2
S088	53.34	54.86	1a
S089	0.00	19.20	7
S089	19.20	19.57	4a
S089	19.57	26.52	4b
S089	26.52	29.87	1a
S090	0.00	29.87	7
S090	29.87	49.38	4a
S090	49.38	52.12	2
S090	52.12	56.39	1a
S091	0.00	49.38	7
S091	49.38	51.51	5b
S091	51.51	82.45	5a
S091	82.45	84.73	4a
S091	84.73	86.26	2
S091	86.26	87.48	1a
S092	0.00	5.18	7
S092	5.18	17.37	5b
S092	17.37	85.34	5a
S092	85.34	89.31	4b
S092	89.31	90.98	2
S092	90.98	94.79	1a
S093	0.00	21.95	7
S093	21.95	148.74	5a
S093	148.74	154.08	4a
S093	154.08	155.14	4d
S093	155.14	155.30	2
S093	155.30	157.28	1a

S094	0.00	30.94	7
S094	30.94	52.12	4a
S094	52.12	58.22	4b
S094	58.22	62.48	1a
S096	0.00	32.61	7
S096	32.61	53.04	4a
S096	53.04	54.10	4b
S096	54.10	54.86	4a
S096	54.86	59.13	1a
S097	0.00	20.12	7
S097	20.12	54.56	5a
S097	54.56	57.00	5b
S097	57.00	145.39	5a
S097	145.39	146.00	5c
S097	146.00	160.63	5a
S097	160.63	162.15	5b
S097	162.15	162.46	2
S097	162.46	169.77	1a
S098	0.00	17.37	7
S098	17.37	25.30	5b
S098	25.30	96.62	5a
S098	96.62	97.84	5c
S098	97.84	111.71	5a
S098	111.71	112.17	2
S098	112.17	116.74	1a
S099	0.00	37.19	7
S099	37.19	43.59	5b
S099	43.59	63.40	5a
S099	63.40	72.85	5d
S099	72.85	127.25	5a
S099	127.25	132.44	4a
S099	132.44	134.57	2
S099	134.57	153.31	1a
S100	0.00	35.97	7
S100	35.97	47.85	4a
S100	47.85	49.38	4b
S100	49.38	65.23	4a
S100	65.23	68.88	1a
S101	0.00	2.44	7
S101	2.44	15.85	4b
S101	15.85	17.68	1a
S102	0.00	4.27	7
S102	4.27	34.44	4b
S102	34.44	35.66	2
S102	35.66	38.71	1a
S103	0.00	4.88	7
S103	4.88	40.54	4b
S103	40.54	41.45	2
S103	41.45	41.76	1a
S104	0.00	35.05	7
S104	35.05	69.19	4b
S104	69.19	70.10	2
S105	0.00	23.77	7
S105	23.77	64.31	4b
S105	64.31	72.54	2
S105	72.54	76.50	1a
S106	0.00	39.93	7
S106	39.93	81.69	4a
S106	81.69	83.52	2
S106	83.52	84.73	1a
S107	0.00	35.05	7
S107	35.05	45.72	5b
S107	45.72	46.93	5d
S107	46.93	71.93	5b
S107	71.93	117.65	5a
S107	117.65	120.40	4a
S107	120.40	120.70	1a
S109	0.00	65.53	7
S109	65.53	66.45	5b
S109	66.45	68.58	5d
S109	68.58	69.49	5b
S109	69.49	70.10	5d
S109	70.10	70.41	5b
S109	70.41	75.29	5d
S109	75.29	82.75	5b
S109	82.75	84.73	5d
S109	84.73	90.83	5b
S110	0.00	60.66	7
S110	60.66	61.57	5b
S110	61.57	68.58	5a
S110	68.58	69.49	5b
S110	69.49	73.76	4a
S110	73.76	75.74	2
S110	75.74	78.64	1a
S111	0.00	18.59	7
S111	18.59	28.96	5b
S111	28.96	66.14	5a
S111	66.14	67.06	5c
S111	67.06	97.23	5a
S111	97.23	109.73	5b
S111	109.73	112.17	4a
S111	112.17	112.47	2
S111	112.47	114.00	1a
S112	0.00	53.95	7
S112	53.95	70.10	5b
S112	70.10	95.25	4b
S112	95.25	95.55	4a
S112	95.55	97.23	4b
S112	97.23	98.45	2
S112	98.45	102.11	1a
S114	0.00	63.40	7
S114	63.40	76.20	4a
S114	76.20	80.47	4b
S114	80.47	84.12	2
S114	84.12	84.73	1a
S115	0.00	28.35	7
S115	28.35	30.78	4b
S115	30.78	33.83	4e
S115	33.83	38.25	4a
S115	38.25	48.31	2
S115	48.31	50.29	1a
S117	0.00	53.95	7
S117	53.95	56.69	5b
S117	56.69	78.03	5a
S117	78.03	80.16	5b
S117	80.16	82.60	4b
S117	82.60	89.00	1a
S119	0.00	28.96	7
S119	28.96	43.59	5b
S119	43.59	56.08	5d
S119	56.08	60.35	5a
S119	60.35	60.50	5c
S119	60.50	97.08	5a
S119	97.08	97.69	5b
S119	97.69	98.76	4a
S119	98.76	99.67	2
S120	0.00	32.00	7
S120	32.00	65.53	4a
S120	65.53	70.41	4b
S120	70.41	73.76	2
S120	73.76	75.59	1a
S121	0.00	60.05	7
S121	60.05	63.40	5b
S121	63.40	81.70	5a
S121	81.70	85.67	5c
S121	85.67	86.20	4a
S121	86.20	86.77	4d
S121	86.77	89.61	1a
S123	0.00	29.26	7
S123	29.26	50.90	4a
S123	50.90	52.42	4b
S123	52.42	55.47	4a
S123	55.47	59.74	1a
S124	0.00	28.04	7
S124	28.04	29.57	4a
S124	29.57	35.05	4b
S124	35.05	43.59	4a
S124	43.59	44.20	4b
S124	44.20	46.94	4a
S124	46.94	53.95	4b
S124	53.95	54.86	2
S124	54.86	57.30	1a
S125	0.00	27.74	7
S125	27.74	29.57	5b
S125	29.57	63.40	5a
S125	63.40	65.23	5b
S125	65.23	66.60	4a
S125	66.60	69.49	1a
S126	0.00	26.06	7
S126	26.06	46.33	4a
S126	46.33	51.05	4b
S126	51.05	52.43	2
S127	0.00	35.05	7
S127	35.05	49.68	5b
S127	49.68	51.21	6a
S127	51.21	52.73	4b
S127	52.73	56.24	4d
S127	56.24	57.61	2
S127	57.61	60.35	1a
S128	0.00	26.82	7
S128	26.82	33.53	4a
S128	33.53	37.19	2
S128	37.19	41.15	1a
S130	0.00	25.91	7
S130	25.91	50.75	4a
S130	50.75	51.21	2
S130	51.21	53.64	1a
S131	0.00	32.77	7
S131	32.77	33.83	5b
S131	33.83	37.43	5a
S131	37.43	39.32	6a
S131	39.32	42.06	6a
S131	42.06	47.03	4b
S131	47.03	53.04	4a
S131	53.04	55.78	4c
S131	55.78	56.69	4d
S131	56.69	56.94	4d
S131	56.94	57.00	4b
S131	57.00	58.67	4d
S131	58.67	66.29	2
S131	66.29	67.97	1a
S131A	0.00	34.75	7
S131A	34.75	42.67	5
S131A	42.67	46.02	6
S131A	46.02	66.45	2
S131A	66.45	69.40	1a
S131B	0.00	31.70	7
S131B	31.70	32.62	5c
S131B	32.62	35.67	5d
S131B	35.67	38.11	5c
S131B	38.11	41.16	5c
S131B	41.16	42.98	4b
S131B	42.98	44.21	4c
S131B	44.21	46.34	4d
S131B	46.34	51.21	4a
S131B	51.21	57.30	2
S131B	57.30	60.30	1a
S132	0.00	29.87	7
S132	29.87	44.20	3
S132	44.20	57.00	1b
S133	0.00	31.39	7
S133	31.39	32.92	5b
S133	32.92	36.27	6a
S133	36.27	37.19	4b
S133	37.19	40.69	4a
S133	40.69	43.59	4b
S133	43.59	45.11	4e
S133	45.11	52.43	4d
S133	52.43	53.95	4b
S133	53.95	59.13	2
S133	59.13	60.35	1a
S134	0.00	44.20	7
S134	44.20	46.33	5b
S134	46.33	46.94	5d
S134	46.94	48.16	5b
S134	48.16	49.38	5d
S134	49.38	50.90	5b
S134	50.90	52.73	5a
S134	52.73	53.04	5b
S134	53.04	53.64	5d
S134	53.64	53.95	5b
S134	53.95	57.91	5d
S134	57.91	60.66	5a
S134	60.66	62.18	5d
S134	62.18	64.01	5a
S134	64.01	65.53	5d
S134	65.53	66.14	5b
S134	66.14	68.58	5d
S134	68.58	71.02	5a
S134	71.02	79.25	6a
S135	0.00	25.97	7
S135	25.97	51.21	4a
S135	51.21	53.34	2
S135	53.34	54.25	1a
S136	0.00	24.38	7
S136	24.38	45.42	4a
S136	45.42	49.99	4b
S136	49.99	53.19	2
S136	53.19	54.25	1a
S137	0.00	24.38	7
S137	24.38	40.84	4a
S137	40.84	44.20	4b
S137	44.20	51.21	4a
S137	51.21	52.73	4b
S137	52.73	55.17	2
S137	55.17	56.08	1a
S138	0.00	24.54	7
S138	24.54	40.08	4a
S138	40.08	46.94	4b
S138	46.94	50.44	4a
S138	50.44	51.36	4b
S138	51.36	56.24	4a
S138	56.24	61.57	1a
S139	0.00	24.69	7
S139	24.69	25.15	4a
S139	25.15	40.23	4b
S139	40.23	42.67	4a
S139	42.67	43.28	4b
S139	43.28	61.57	4a
S139	61.57	65.84	1a
S140	0.00	29.26	7
S140	29.26	38.25	4b
S140	38.25	49.38	4a
S140	49.38	53.95	1a
S141	0.00	55.47	7
S141	55.47	57.00	5b
S141	57.00	90.53	5a
S141	90.53	92.66	5b
S141	92.66	109.42	5a
S141	109.42	114.91	5b
S141	114.91	121.92	5a
S141	121.92	128.63	5b
S141	128.63	148.74	5a
S141	148.74	149.66	5b
S141	149.66	157.28	5a
S141	157.28	158.19	5b
S141	158.19	161.85	4b
S141	161.85	164.13	2
S141	164.13	166.73	1a
S142	0.00	72.24	7
S142	72.24	84.43	5d
S142	84.43	85.34	4b
S142	85.34	86.87	4a
S142	86.87	89.31	4e
S142	89.31	92.35	3
S142	92.35	96.62	2
S142	96.62	98.45	1a
S143	0.00	29.57	7
S143	29.57	34.44	1a
S145	0.00	42.67	7
S145	42.67	44.50	5b
S145	44.50	45.11	5a
S145	45.11	49.99	5b
S145	49.99	247.95	5a
S145	247.95	250.85	2
S145	250.85	257.25	1a
S146	0.00	60.66	7
S146	60.66	66.45	5c
S146	66.45	74.68	5b
S146	74.68	223.11	5a
S146	223.11	223.72	2
S146	223.72	224.03	1a
S147	0.00	47.24	7
S147	47.24	53.64	5b
S147	53.64	57.30	5a
S147	57.30	61.26	5b
S147	61.26	78.64	5a
S147	78.64	80.16	5b
S147	80.16	98.76	5a
S147	98.76	104.55	5b
S147	104.55	111.86	5a
S147	111.86	114.30	5b
S147	114.30	116.13	5a
S147	116.13	118.26	5b

S147	118.26	124.36	5a
S147	124.36	125.88	5b
S147	125.88	152.25	5a
S147	152.25	152.55	4a
S147	152.55	153.62	4a
S147	153.62	156.06	2
S147	156.06	160.32	1a
S148	0.00	49.38	7
S148	49.38	49.68	5c
S148	49.68	54.25	5b
S148	54.25	82.91	5a
S148	82.91	111.86	5b
S148	111.86	116.74	5a
S148	116.74	121.31	6a
S148	121.31	124.66	4b
S148	124.66	126.49	2
S148	126.49	128.93	1a
S149	0.00	101.19	7
S149	101.19	104.39	4a
S149	104.39	105.77	2
S149	105.77	107.29	1a
S150	0.00	24.38	7
S150	24.38	28.35	4b
S150	28.35	30.33	4a
S150	30.33	39.01	4b
S150	39.01	41.76	2
S150	41.76	48.16	1a
S151	0.00	22.86	7
S151	22.86	29.87	4a
S151	29.87	31.39	4b
S151	31.39	32.31	1a
S152	0.00	25.91	7
S152	25.91	45.57	4a
S152	45.57	49.38	1a
S153	0.00	26.82	7
S153	26.82	29.87	5b
S153	29.87	32.31	5a
S153	32.31	32.92	5b
S153	32.92	55.93	5a
S153	55.93	56.69	5b
S153	56.69	60.35	4a
S153	60.35	63.09	2
S153	63.09	64.92	1a
S154	0.00	26.52	7
S154	26.52	46.33	5b
S154	46.33	54.10	5a
S154	54.10	55.32	5c
S154	55.32	99.06	5a
S154	99.06	99.97	4b
S154	99.97	101.35	4a
S154	101.35	103.02	2
S155	0.00	70.10	7
S156	0.00	60.05	7
S156	60.05	60.96	6a
S156	60.96	66.45	6b
S156	66.45	69.49	4b
S156	69.49	70.10	4a
S156	70.10	71.32	4b
S156	71.32	72.24	4a
S156	72.24	73.15	4b
S156	73.15	73.76	2
S156	73.76	75.59	1a
S157	0.00	19.81	7
S157	19.81	20.12	4b
S157	20.12	43.59	4a
S157	43.59	48.16	4b
S157	48.16	53.04	4a
S157	53.04	53.34	2
S157	53.34	54.86	1a
S158	0.00	21.95	7
S158	21.95	31.09	4a
S158	31.09	35.66	4b
S158	35.66	36.12	4a
S158	36.12	40.23	2
S158	40.23	41.76	1a
S159	0.00	25.45	7
S159	25.45	26.52	4b
S159	26.52	28.04	4a
S159	28.04	31.70	2
S159	31.70	38.71	1a
S160	0.00	23.47	7
S160	23.47	29.57	1a
S161	0.00	25.15	7
S161	25.15	33.53	4a
S161	33.53	41.45	2
S161	41.45	44.20	1a
S162	0.00	27.74	7
S162	27.74	51.21	4a
S162	51.21	56.69	2
S162	56.69	59.13	1a
S163	0.00	29.57	7
S163	29.57	57.30	4a
S163	57.30	57.76	2
S163	57.76	61.26	1a
S163A	0.00	28.81	7
S163A	28.81	51.99	4a
S163A	51.99	58.23	2
S163A	58.23	61.20	1a
S163B	0.00	29.56	7
S163B	29.56	46.78	4a
S163B	46.78	57.30	2
S163B	57.30	59.40	1a
S164	0.00	30.33	7
S164	30.33	55.17	4a
S164	55.17	56.08	2
S164	56.08	60.05	1a
S167	0.00	16.76	7
S167	16.76	56.69	5b
S167	56.69	74.98	5a
S167	74.98	78.03	5b
S167	78.03	83.82	5a
S167	83.82	85.04	5b
S167	85.04	149.05	5a
S167	149.05	152.71	5b
S167	152.71	219.76	5a
S167	219.76	219.91	5b
S167	219.91	220.83	4a
S167	220.83	224.33	1a
S168	0.00	30.48	7
S169	0.00	32.31	7
S169	32.31	53.95	5b
S169	53.95	230.43	5a
S169	230.43	235.61	2
S169	235.61	237.13	1a
S170	0.00	74.37	7
S170	74.37	74.98	4b
S170	74.98	84.43	4a
S170	84.43	85.95	2
S170	85.95	87.78	1a
S171	0.00	28.04	7
S171	28.04	47.85	4a
S171	47.85	57.15	2
S171	57.15	60.35	1a
S172	0.00	21.34	7
S172	21.34	41.76	4a
S172	41.76	45.11	2
S172	45.11	52.12	1a
S173	0.00	15.24	7
S173	15.24	28.35	4a
S173	28.35	31.39	2
S173	31.39	33.53	1a
S174	0.00	35.97	7
S174	35.97	40.84	5b
S174	40.84	63.40	5a
S174	63.40	67.36	5d
S174	67.36	86.26	5a
S174	86.26	87.17	5b
S174	87.17	87.78	5d
S174	87.78	103.02	5b
S174	103.02	131.67	5a
S174	131.67	134.26	5b
S174	134.26	136.25	4a
S174	136.25	137.16	2
S174	137.16	138.38	1a
S175	0.00	18.90	7
S175	18.90	101.80	5a
S175	101.80	102.41	5c
S175	102.41	129.54	5a
S175	129.54	131.06	5b
S175	131.06	140.21	1a
S176	0.00	30.48	7
S176	30.48	54.25	5b
S176	54.25	57.30	6b
S176	57.30	58.83	4b
S176	58.83	60.35	4e
S176	60.35	62.79	4b
S176	62.79	63.70	4a
S176	63.70	67.06	2
S176	67.06	68.58	1a
S177	0.00	35.36	7
S177	35.36	36.12	4b
S177	36.12	52.12	2
S177	52.12	57.61	1a
S178	0.00	31.39	7
S178	31.39	37.49	5b
S178	37.49	39.01	5d
S178	39.01	41.00	5b
S178	41.00	42.21	5d
S178	42.21	42.82	5b
S178	42.82	45.11	5d
S178	45.11	46.94	5b
S178	46.94	48.16	5d
S178	48.16	59.44	5b
S178	59.44	60.96	5a
S178	60.96	69.65	5b
S178	69.65	87.48	5a
S178	87.48	87.93	5b
S178	87.93	88.39	5a
S178	88.39	88.70	5b
S178	88.70	90.83	4a
S178	90.83	99.36	2
S178	99.36	106.68	1a
S179	0.00	30.48	7
S179	30.48	37.49	5b
S179	37.49	40.54	5a
S179	40.54	42.06	5b
S179	42.06	98.91	5a
S179	98.91	100.28	5
S179	100.28	100.43	4c
S179	100.43	100.58	5b
S179	100.58	102.41	4c
S179	102.41	103.48	5b
S179	103.48	104.55	2
S179	104.55	114.91	1a
S180	0.00	31.70	7
S180	31.70	65.84	4a
S180	65.84	71.93	2
S180	71.93	75.29	1a
S181	0.00	35.66	7
S181	35.66	63.70	4a
S181	63.70	66.14	4b
S181	66.14	74.98	4a
S181	74.98	81.69	2
S181	81.69	86.26	1a
S182	0.00	81.08	7
S182	81.08	85.65	4b
S182	85.65	92.96	4a
S182	92.96	93.12	2
S182	93.12	93.57	1a
S183	0.00	41.00	7
S183	41.00	49.68	5b
S183	49.68	105.77	5a
S183	105.77	109.88	5b
S183	109.88	110.79	4a
S183	110.79	111.25	2
S183	111.25	111.86	1a
S184	0.00	39.32	7
S184	39.32	50.29	5b
S184	50.29	94.95	5a
S184	94.95	95.86	5b
S184	95.86	132.89	5a
S184	132.89	133.20	2
S184	133.20	138.38	1a
S185	0.00	41.45	7
S185	41.45	67.36	5b
S185	67.36	84.43	5d
S185	84.43	101.50	5b
S185	101.50	103.94	6
S185	103.94	110.95	4a
S185	110.95	111.25	2
S185	111.25	111.40	1a
S186	0.00	45.72	7
S186	45.72	58.22	5b
S186	58.22	89.31	5a
S186	89.31	91.74	5b
S186	91.74	107.90	5a
S186	107.90	112.93	5b
S186	112.93	151.49	5a
S186	151.49	152.86	5b
S186	152.86	153.92	4a
S186	153.92	157.28	1a
S187	0.00	48.71	7
S187	48.71	60.05	5b
S187	60.05	80.47	5a
S187	80.47	81.38	5b
S187	81.38	96.62	5a
S187	96.62	101.19	5d
S187	101.19	103.17	5a
S187	103.17	112.47	5b
S187	112.47	116.59	5a
S187	116.59	121.92	6b
S187	121.92	125.43	4a
S187	125.43	132.89	1a
S188	0.00	58.06	7
S188	58.06	65.23	5a
S188	65.23	65.84	5b
S188	65.84	68.52	5a
S188	68.52	89.95	6b
S188	89.95	91.44	4a
S189	0.00	35.36	7
S189	35.36	67.67	4a
S189	67.67	73.15	2
S189	73.15	74.98	1a
S190	0.00	11.58	7
S190	11.58	24.99	5b
S190	24.99	169.77	5a
S190	169.77	170.99	4a
S190	170.99	173.74	1a
S191	0.00	37.03	7
S191	37.03	37.64	4a
S191	37.64	40.54	1a
S192	0.00	10.97	7
S192	10.97	20.73	5b
S192	20.73	52.12	5a
S192	52.12	53.64	4a
S192	53.64	55.78	1a
S193	0.00	17.98	7
S193	17.98	23.47	5b
S193	23.47	98.15	5a
S193	98.15	98.76	5b
S193	98.76	106.07	4a
S193	106.07	108.81	1a
S194	0.00	31.09	7
S194	31.09	32.77	4a
S194	32.77	40.54	2
S194	40.54	43.59	1a
S195	0.00	16.76	7
S195	16.76	28.04	4a
S195	28.04	28.35	2
S195	28.35	28.96	2
S195	28.96	32.00	1a
S196	0.00	17.37	7
S196	17.37	37.03	4a
S196	37.03	37.95	2
S196	37.95	39.01	4a
S196	39.01	39.62	2
S196	39.62	41.15	4a
S196	41.15	43.28	2
S196	43.28	46.94	1a
S196A	0.00	16.34	7
S196A	16.34	36.48	4
S196A	36.48	39.32	2
S196A	39.32	41.70	1
S196B	0.00	17.77	7
S196B	17.77	40.23	4a
S196B	40.23	48.46	2
S196B	48.46	50.90	1a
S197	0.00	21.95	7
S197	21.95	53.95	4a
S197	53.95	55.78	2
S197	55.78	57.00	1a
S198	0.00	47.24	7
S198	47.24	64.62	4a
S198	64.62	79.25	2

S198	79.25	81.69	1a
S199	0.00	32.61	7
S199	32.61	36.58	5b
S199	36.58	39.01	5d
S199	39.01	39.62	5b
S199	39.62	42.06	5d
S199	42.06	42.98	5b
S199	42.98	45.11	5d
S199	45.11	46.33	5b
S199	46.33	47.24	5d
S199	47.24	49.07	5b
S199	49.07	50.90	5d
S199	50.90	52.43	5b
S199	52.43	74.68	6a
S199	74.68	78.03	4a
S199	78.03	78.33	4b
S199	78.33	79.86	2
S199	79.86	81.69	1a
S202	0.00	28.65	7
S202	28.65	29.87	5b
S202	29.87	32.31	5a
S202	32.31	39.32	5b
S202	39.32	58.52	5a
S202	58.52	60.66	5b
S202	60.66	63.40	5a
S202	63.40	64.31	5b
S202	64.31	89.00	5a
S202	89.00	92.81	5b
S202	92.81	95.10	4a
S202	95.10	95.86	2
S202	95.86	105.77	1a
S203	0.00	18.29	7
S203	18.29	116.13	5a
S203	116.13	118.93	5b
S203	118.93	121.01	2
S203	121.01	132.28	1a
S204	0.00	26.82	7
S204	26.82	29.87	5b
S204	29.87	188.37	5a
S204	188.37	192.63	4a
S204	192.63	195.99	2
S204	195.99	198.73	1a
S205	0.00	35.97	7
S205	35.97	39.01	5b
S205	39.01	211.23	5a
S205	211.23	218.85	1a
S206	0.00	23.16	7
S206	23.16	34.75	5b
S206	34.75	95.71	5a
S206	95.71	103.33	5b
S206	103.33	148.74	5a
S206	148.74	150.72	5b
S206	150.72	151.64	4a
S206	151.64	152.40	2
S206	152.40	157.89	1a
S207	0.00	19.81	7
S207	19.81	34.14	5b
S207	34.14	118.57	5a
S207	118.57	119.18	4a
S207	119.18	124.36	1a
S208	0.00	21.03	7
S208	21.03	77.11	5a
S208	77.11	79.86	5b
S208	79.86	80.47	5c
S208	80.47	80.77	5b
S208	80.77	82.60	4a
S208	82.60	83.82	2
S208	83.82	87.78	1a
S209	0.00	28.65	7
S209	28.65	45.72	4a
S209	45.72	51.21	1a
S210	0.00	35.14	7
S210	35.14	49.47	4a
S210	49.47	53.64	1a
S211	0.00	30.63	7
S211	30.63	33.77	4a
S211	33.77	36.88	1a
S212	0.00	51.97	7
S212	51.97	53.71	5a
S212	53.71	59.38	5d
S212	59.38	78.03	5a
S212	78.03	92.51	6a
S212	92.51	101.96	4a
S212	101.96	105.16	1a
S213	0.00	40.23	7
S213	40.23	42.06	5b
S213	42.06	45.42	5d
S213	45.42	57.00	5b
S213	57.00	91.14	5a
S213	91.14	93.57	5b
S213	93.57	102.72	5d
S213	102.72	115.21	5b
S213	115.21	134.72	5a
S213	134.72	135.79	4a
S213	135.79	135.94	1a
S214	0.00	67.06	7
S214	67.06	68.28	4b
S214	68.28	82.30	4a
S214	82.30	85.65	2
S214	85.65	87.17	1a
S215	0.00	27.74	7
S215	27.74	53.89	4a
S215	53.89	57.00	1a
S216	0.00	24.99	7
S216	24.99	43.89	4a
S216	43.89	44.44	4e
S216	44.44	64.31	4a
S216	64.31	68.58	1a
S217	0.00	69.19	7
S217	69.19	73.91	4b
S217	73.91	80.56	4a
S217	80.56	83.82	2
S217	83.82	87.17	1a
S218	0.00	38.71	7
S218	38.71	44.81	5b
S218	44.81	63.09	5a
S218	63.09	75.29	5b
S218	75.29	81.38	5d
S218	81.38	102.87	5a
S218	102.87	103.48	4b
S218	103.48	104.85	4a
S218	104.85	107.90	1a
S219	0.00	40.23	7
S219	40.23	93.27	5b
S219	93.27	96.47	5d
S219	96.47	101.04	5b
S219	101.04	125.88	5a
S219	125.88	126.61	5b
S219	126.61	127.01	5c
S219	127.01	128.72	5b
S219	128.72	128.78	4a
S219	128.78	129.69	4b
S219	129.69	130.00	2
S219	130.00	133.20	1a
S220	0.00	35.36	7
S220	35.36	64.62	4a
S220	64.62	68.58	1a
S221	0.00	39.32	7
S221	39.32	43.89	4a
S221	43.89	44.50	4e
S221	44.50	51.82	4a
S221	51.82	53.34	2
S221	53.34	56.39	1a
S222	0.00	40.54	7
S222	40.54	62.48	4a
S222	62.48	63.09	2
S222	63.09	66.14	1a
S223	0.00	41.91	7
S223	41.91	50.29	4a
S223	50.29	50.90	4e
S223	50.90	63.70	4a
S223	63.70	64.31	4e
S223	64.31	80.92	4a
S223	80.92	84.12	1a
S224	0.00	53.95	7
S225	0.00	25.30	7
S225	25.30	27.43	5b
S225	27.43	38.40	5d
S225	38.40	45.11	5b
S225	45.11	88.09	5a
S225	88.09	90.83	4a
S226	0.00	47.55	7
S226	47.55	67.97	5b
S226	67.97	69.80	4a
S226	69.80	73.15	2
S226	73.15	77.42	1a
S227	0.00	30.48	7
S227	30.48	31.70	5b
S227	31.70	32.92	5d
S227	32.92	35.97	5b
S227	35.97	40.23	5d
S227	40.23	60.96	5a
S227	60.96	64.31	4a
S227	64.31	67.06	1a
S228	0.00	26.21	7
S228	26.21	32.61	5b
S228	32.61	85.34	5a
S228	85.34	87.33	5b
S228	87.33	89.31	4a
S228	89.31	92.05	1a
S229	0.00	18.29	7
S229	18.29	33.53	5b
S229	33.53	107.90	5a
S229	107.90	110.49	4a
S229	110.49	111.86	1a
S230	0.00	24.38	7
S230	24.38	30.48	1a
S231	0.00	31.70	7
S231	31.70	44.20	5b
S231	44.20	128.93	5a
S231	128.93	131.52	5b
S231	131.52	132.44	4a
S231	132.44	138.07	2
S231	138.07	140.21	1a
S232	0.00	22.86	7
S232	22.86	29.87	5b
S232	29.87	52.73	5a
S232	52.73	53.04	5b
S232	53.04	54.56	5c
S232	54.56	54.86	5b
S232	54.86	57.15	5c
S232	57.15	60.05	5b
S232	60.05	62.18	4a
S232	62.18	65.53	1a
S233	0.00	18.29	7
S233	18.29	22.86	1a
S234	0.00	24.38	7
S234	24.38	26.82	5b
S234	26.82	169.71	5a
S234	169.71	173.28	4a
S234	173.28	175.87	2
S234	175.87	177.70	1a
S235	0.00	24.99	7
S235	24.99	59.13	4a
S235	59.13	61.87	2
S235	61.87	66.75	1a
S236	0.00	56.69	7
S236	56.69	69.49	5a
S236	69.49	108.20	6a
S236	108.20	114.76	4a
S236	114.76	117.35	2
S236	117.35	117.65	1a
S237	0.00	30.18	7
S237	30.18	47.55	4a
S237	47.55	48.01	4b
S237	48.01	50.90	1a
S238	0.00	35.66	7
S238	35.66	36.58	5b
S238	36.58	63.86	5a
S238	63.86	66.45	5d
S238	66.45	145.39	5a
S238	145.39	146.36	5b
S238	146.36	147.43	2
S238	147.43	150.27	1a
S239	0.00	28.96	7
S239	28.96	29.26	5b
S239	29.26	164.96	5a
S239	164.96	168.80	4a
S239	168.80	169.41	2
S239	169.41	173.13	1a
S240	0.00	30.48	7
S240	30.48	173.22	5a
S240	173.22	174.19	4a
S240	174.19	175.50	2
S240	175.50	178.61	1a
S241	0.00	22.25	7
S241	22.25	27.74	5b
S241	27.74	150.91	5a
S241	150.91	151.39	4a
S241	151.39	153.92	1a
S242	0.00	39.32	7
S242	39.32	47.55	4a
S242	47.55	48.16	4e
S242	48.16	50.17	4a
S242	50.17	54.25	4e
S242	54.25	64.37	4a
S242	64.37	68.28	1a
S243	0.00	36.58	7
S243	36.58	59.38	4a
S243	59.38	61.26	2
S243	61.26	61.87	1a
S244	0.00	42.06	7
S244	42.06	69.49	4a
S244	69.49	74.22	2
S244	74.22	75.90	1a
S245	0.00	31.09	7
S245	31.09	34.29	5b
S245	34.29	188.98	5a
S245	188.98	189.89	5b
S245	189.89	190.65	4a
S245	190.65	194.46	1a
S246	0.00	35.05	7
S246	35.05	220.68	5a
S246	220.68	222.66	5b
S246	222.66	222.81	4a
S246	222.81	226.47	1a
S247	0.00	32.92	7
S247	32.92	234.03	5a
S247	234.03	234.24	5b
S247	234.24	235.00	4b
S247	235.00	236.83	1a
S248	0.00	36.27	7
S248	36.27	215.49	5a
S248	215.49	216.65	5b
S248	216.65	219.67	4b
S248	219.67	220.16	2
S248	220.16	223.42	1a
S249	0.00	26.52	7
S249	26.52	30.48	5b
S249	30.48	115.06	5a
S249	115.06	116.13	5b
S249	116.13	188.06	5a
S249	188.06	189.52	5b
S249	189.52	194.46	2
S249	194.46	195.38	1a
S250	0.00	18.29	7
S250	18.29	142.65	5a
S250	142.65	145.54	5b
S250	145.54	145.85	2
S250	145.85	148.74	1a
S251	0.00	32.92	7
S251	32.92	103.94	5a
S251	103.94	105.77	5b
S251	105.77	106.56	4a
S251	106.56	110.64	2
S251	110.64	112.17	1a
S252	0.00	64.01	7
S252	64.01	65.99	4a
S252	65.99	69.49	1a
S253	0.00	24.69	7
S253	24.69	27.89	4a
S253	27.89	30.78	1a
S254	0.00	13.11	7
S254	13.11	19.51	5b
S254	19.51	51.21	5a
S254	51.21	55.02	5b
S254	55.02	56.30	4a
S254	56.30	58.22	1a
S255	0.00	24.99	7
S255	24.99	28.35	5b
S255	28.35	31.09	5a
S255	31.09	40.23	5d
S255	40.23	43.59	5b
S255	43.59	64.31	5a

S255	64.31	66.45	6a
S255	66.45	80.16	4a
S255	80.16	81.38	2
S255	81.38	84.73	1a
S256	0.00	15.85	7
S256	15.85	45.11	4a
S256	45.11	48.16	2
S256	48.16	53.34	1a
S257	0.00	12.80	7
S257	12.80	24.08	4a
S257	24.08	24.38	2
S257	24.38	26.82	1a
S258	0.00	14.94	7
S258	14.94	38.40	4a
S258	38.40	41.76	1a
S259	0.00	16.76	7
S259	16.76	39.01	4a
S259	39.01	43.59	1a
S260	0.00	16.15	7
S260	16.15	18.75	6a
S260	18.75	45.11	4a
S260	45.11	48.77	2
S260	48.77	51.21	1a
S261	0.00	14.02	7
S261	14.02	32.92	4a
S261	32.92	37.80	1a
S262	0.00	13.72	7
S262	13.72	37.19	4a
S262	37.19	39.62	2
S262	39.62	42.06	1a
S263	0.00	21.95	7
S263	21.95	46.94	4a
S263	46.94	50.84	2
S263	50.84	55.78	1a
S264	0.00	21.95	7
S264	21.95	54.10	4a
S264	54.10	57.30	2
S264	57.30	57.91	1a
S265	0.00	53.95	7
S266	0.00	37.80	7
S266	37.80	63.25	4a
S266	63.25	67.97	2
S266	67.97	71.93	1a
S267	0.00	33.83	7
S267	33.83	40.33	4a
S267	40.33	42.06	2
S267	42.06	44.50	1a
S268	0.00	73.15	7
S268	73.15	73.82	4b
S268	73.82	86.59	4a
S268	86.59	92.96	2
S268	92.96	95.55	1a
S269	0.00	59.44	7
S269	59.44	78.33	5b
S269	78.33	84.43	5d
S269	84.43	96.62	5b
S269	96.62	105.77	5d
S269	105.77	117.96	5b
S269	117.96	119.79	6a
S269	119.79	120.09	4b
S269	120.09	121.92	4a
S269	121.92	125.27	2
S269	125.27	129.54	1a
S270	0.00	16.46	7
S270	16.46	24.99	1a
S271	0.00	18.90	7
S271	18.90	42.98	1a
S272	0.00	27.74	7
S272	27.74	40.69	4a
S272	40.69	46.63	2
S272	46.63	50.90	1a
S273	0.00	31.09	7
S273	31.09	36.73	4a
S273	36.73	46.33	2
S273	46.33	57.00	1a
S274	0.00	34.44	7
S274	34.44	45.11	4a
S274	45.11	46.33	2
S274	46.33	60.05	1a
S275	0.00	35.66	7
S275	35.66	40.23	4a
S275	40.23	41.15	4b
S275	41.15	44.50	4a
S275	44.50	45.11	2
S275	45.11	53.95	1a
S276	0.00	35.66	7
S276	35.66	41.76	5b
S276	41.76	49.99	5d
S276	49.99	54.41	5b
S276	54.41	57.00	5d
S276	57.00	66.14	5b
S276	66.14	99.06	6a
S277	0.00	31.39	7
S277	31.39	35.66	5b
S277	35.66	41.15	5a
S277	41.15	41.45	5b
S277	41.45	55.17	5a
S277	55.17	63.09	5b
S277	63.09	89.46	5a
S277	89.46	90.71	5b
S277	90.71	91.90	4a
S277	91.90	108.81	1a
S278	0.00	17.22	7
S278	17.22	23.47	5b
S278	23.47	77.39	5a
S278	77.39	77.48	4a
S278	77.48	81.38	1a
S279	0.00	24.99	7
S279	24.99	29.57	5b
S279	29.57	93.57	5a
S279	93.57	94.64	4a
S279	94.64	94.95	2
S279	94.95	113.39	1a
S281	0.00	49.53	7
S281	49.53	68.28	4a
S281	68.28	72.54	2
S281	72.54	74.68	1a
S282	0.00	17.98	7
S282	17.98	23.01	4a
S282	23.01	23.62	4e
S282	23.62	45.60	4a
S282	45.60	51.21	1a
S283	0.00	39.62	7
S283	39.62	45.11	5b
S283	45.11	62.79	6a
S283	62.79	70.41	4a
S283	70.41	74.68	2
S283	74.68	77.72	1a
S284	0.00	63.09	7
S284	63.09	64.62	5b
S284	64.62	69.49	5d
S284	69.49	73.76	5b
S284	73.76	78.64	6a
S284	78.64	82.39	4a
S284	82.39	87.78	1a
S285	0.00	50.60	7
S285	50.60	106.07	6a
S285	106.07	107.14	4a
S285	107.14	109.73	1a
S286	0.00	29.87	7
S286	29.87	36.21	5b
S286	36.21	40.84	5d
S286	40.84	46.48	5b
S286	46.48	46.79	5d
S286	46.79	73.46	5a
S286	73.46	76.75	5b
S286	76.75	80.62	4a
S286	80.62	85.95	2
S287	0.00	43.59	7
S287	43.59	70.71	4b
S287	70.71	75.13	4a
S287	75.13	75.59	2
S287	75.59	81.08	1a
S288	0.00	27.13	7
S288	27.13	45.11	5b
S288	45.11	77.63	5c
S288	77.63	91.23	5b
S288	91.23	94.79	6a
S288	94.79	98.21	4a
S288	98.21	100.64	2
S288	100.64	101.80	1a
S289	0.00	27.74	7
S289	27.74	29.87	5b
S289	29.87	65.23	5a
S289	65.23	66.60	5b
S289	66.60	67.67	5d
S289	67.67	69.19	5b
S289	69.19	69.49	5d
S289	69.49	75.44	5b
S289	75.44	104.55	5a
S289	104.55	112.07	5b
S289	112.07	115.98	6a
S289	115.98	117.62	4a
S289	117.62	118.17	2
S289	118.17	122.22	1a
S290	0.00	32.00	7
S290	32.00	32.31	5b
S290	32.31	42.03	5a
S290	42.03	42.37	5b
S290	42.37	46.33	5a
S290	46.33	48.62	5b
S290	48.62	85.28	5a
S290	85.28	88.85	5b
S290	88.85	124.05	5a
S290	124.05	125.03	5b
S290	125.03	126.80	6a
S290	126.80	128.56	4a
S290	128.56	129.63	4b
S290	129.63	136.89	4a
S290	136.89	137.34	2
S290	137.34	137.77	1a
S291	0.00	26.52	7
S291	26.52	41.45	5b
S291	41.45	95.71	5a
S291	95.71	96.47	5c
S291	96.47	130.45	5a
S291	130.45	132.77	5b
S291	132.77	133.93	4a
S291	133.93	135.33	2
S291	135.33	138.38	1a
S292	0.00	19.20	7
S292	19.20	28.04	5b
S292	28.04	136.09	5a
S292	136.09	138.01	5b
S292	138.01	138.68	4b
S292	138.68	140.60	2
S292	140.60	142.34	1a
S293	0.00	53.95	7
S293	53.95	69.19	5b
S293	69.19	90.53	5a
S293	90.53	96.62	5b
S293	96.62	111.25	5a
S293	111.25	116.59	5b
S293	116.59	178.92	5a
S293	178.92	179.83	5b
S293	179.83	180.14	4b
S293	180.14	180.38	2
S293	180.38	183.49	1a
S294A	0.00	35.30	7
S294B	0.00	44.60	7
S294B	44.60	108.80	5b
S295	0.00	43.74	7
S295	43.74	65.23	5b
S295	65.23	83.82	5a
S295	83.82	85.95	5b
S295	85.95	86.87	5d
S295	86.87	96.62	5a
S295	96.62	97.23	5d
S295	97.23	98.45	5c
S295	98.45	99.06	5d
S295	99.06	118.26	5a
S295	118.26	120.09	5d
S295	120.09	120.40	5c
S295	120.40	126.49	5a
S295	126.49	127.86	4a
S295	127.86	128.63	2
S295	128.63	130.76	1a
S296	0.00	30.48	7
S296	30.48	60.99	4a
S296	60.99	61.97	4b
S296	61.97	65.23	1a
S297	0.00	31.24	7
S297	31.24	64.13	4a
S297	64.13	74.83	2
S297	74.83	78.33	1a
S298	0.00	54.25	7
S298	54.25	57.91	5a
S298	57.91	58.83	5d
S298	58.83	60.05	5b
S298	60.05	67.88	6a
S298	67.88	69.34	4a
S298	69.34	69.80	1a
S299	0.00	21.95	7
S299	21.95	26.58	5b
S299	26.58	49.83	5a
S299	49.83	52.67	5d
S299	52.67	56.39	5b
S299	56.39	58.22	5d
S299	58.22	60.05	5b
S299	60.05	61.57	5d
S299	61.57	66.90	5b
S299	66.90	77.72	5a
S299	77.72	81.59	5b
S299	81.59	82.58	4a
S299	82.58	83.21	2
S299	83.21	84.43	1a
S300	0.00	48.16	7
S300	48.16	51.21	4a
S300	51.21	52.73	4b
S300	52.73	60.23	4a
S300	60.23	60.96	2
S300	60.96	61.57	1a
S301	0.00	43.89	7
S301	43.89	51.82	5b
S301	51.82	73.30	5a
S301	73.30	78.64	5b
S301	78.64	81.69	4a
S301	81.69	84.28	2
S301	84.28	87.48	1a
S302	0.00	24.69	7
S302	24.69	36.88	5b
S302	36.88	39.01	5d
S302	39.01	39.93	5b
S302	39.93	44.99	5d
S302	44.99	53.64	5b
S302	53.64	55.47	5c
S302	55.47	60.96	5b
S302	60.96	110.03	5a
S302	110.03	112.35	5b
S302	112.35	116.74	2
S302	116.74	118.87	1a
S303	0.00	23.16	7
S303	23.16	44.04	5b
S303	44.04	124.36	5a
S303	124.36	125.27	5b
S303	125.27	126.77	4a
S303	126.77	128.93	1a
S304	0.00	32.92	7
S304	32.92	60.96	5b
S304	60.96	61.57	5c
S304	61.57	61.87	5b
S304	61.87	77.72	5a
S304	77.72	79.55	5c
S304	79.55	84.12	5a
S304	84.12	87.17	5b
S304	87.17	91.56	4a
S304	91.56	91.81	2
S304	91.81	93.88	1a
S305	0.00	50.29	7
S306	0.00	36.58	7
S306	36.58	39.93	5b
S306	39.93	64.01	6a
S306	64.01	65.99	4a
S306	65.99	67.36	2
S306	67.36	68.28	1a
S307	0.00	29.87	7
S307	29.87	47.70	4a
S307	47.70	50.60	2
S307	50.60	52.73	1a
S308	0.00	27.43	7
S308	27.43	28.35	5b
S308	28.35	64.92	5a
S308	64.92	67.21	5b
S308	67.21	129.08	5a

S308	129.08	132.44	5b
S308	132.44	132.71	4b
S308	132.71	133.50	2
S308	133.50	136.25	1a
S309	0.00	49.38	7
S309	49.38	54.56	5b
S309	54.56	74.83	5a
S309	74.83	76.11	5b
S309	76.11	78.30	4a
S309	78.30	79.46	2
S309	79.46	81.69	1a
S309A	0.00	36.50	7
S309B	0.00	57.90	7
S310	0.00	12.50	7
S310	12.50	19.66	5b
S310	19.66	70.59	5a
S310	70.59	73.40	4a
S310	73.40	76.11	2
S310	76.11	78.33	1a
S311	0.00	17.07	7
S311	17.07	24.38	5b
S311	24.38	65.23	5a
S311	65.23	65.53	5b
S311	65.53	67.67	4b
S311	67.67	68.64	4a
S311	68.64	71.08	2
S311	71.08	74.07	1a
S312	0.00	14.02	7
S312	14.02	16.15	5b
S312	16.15	24.84	5a
S312	24.84	28.65	5b
S312	28.65	114.97	5a
S312	114.97	116.74	4a
S312	116.74	118.41	2
S312	118.41	120.09	1a
S313	0.00	17.07	7
S313	17.07	17.68	5b
S313	17.68	137.31	5a
S313	137.31	139.14	5b
S313	139.14	139.60	4a
S313	139.60	142.65	1a
S314	0.00	14.94	7
S314	14.94	17.68	5b
S314	17.68	147.49	5a
S314	147.49	147.65	4a
S314	147.65	150.27	2
S314	150.27	151.79	1a
S315	0.00	12.80	7
S315	12.80	149.35	5a
S315	149.35	152.55	5b
S315	152.55	152.83	4a
S315	152.83	155.14	2
S315	155.14	156.06	1a
S316	0.00	7.92	7
S316	7.92	16.46	5b
S316	16.46	111.56	5a
S316	111.56	114.60	5b
S316	114.60	115.09	4a
S316	115.09	117.04	1a
S317	0.00	6.10	7
S317	6.10	26.82	5b
S317	26.82	60.66	5a
S317	60.66	63.79	5b
S317	63.79	65.62	4a
S317	65.62	66.02	4b
S317	66.02	68.58	1a
S318	0.00	29.25	7
S318	29.26	31.85	4a
S318	31.85	35.20	2
S318	35.20	36.58	1a
S319	0.00	10.06	7
S319	10.06	12.19	1a
S320	0.00	52.73	7
S320	52.73	53.19	5c
S320	53.19	57.30	5b
S320	57.30	68.58	5a
S320	68.58	78.64	5b
S320	78.64	93.88	6a
S320	93.88	95.40	4a
S320	95.40	96.32	2
S320	96.32	97.84	1a

S321	0.00	33.83	7
S321	33.83	70.41	4a
S321	70.41	79.74	2
S321	79.74	82.91	1a
S322	0.00	30.18	7
S322	30.18	53.49	4a
S322	53.49	55.63	2
S322	55.63	57.91	1a
S323	0.00	26.21	7
S323	26.21	42.06	4a
S323	42.06	42.49	2
S323	42.49	44.81	1a
S324	0.00	22.56	7
S324	22.56	59.13	4a
S324	59.13	63.61	2
S324	63.61	67.36	1a
S325	0.00	39.62	7
S325	39.62	56.02	4a
S325	56.02	59.74	1a
S326	0.00	36.58	7
S326	36.58	59.83	4a
S326	59.83	61.11	2
S326	61.11	63.40	1a
S327	0.00	89.92	7
S328	0.00	28.35	7
S328	28.35	99.97	5a
S328	99.97	101.19	5b
S328	101.19	102.87	5c
S328	102.87	103.94	5b
S328	103.94	107.29	5a
S328	107.29	108.45	5b
S328	108.45	115.06	4a
S328	115.06	116.43	2
S328	116.43	119.48	1a
S329	0.00	21.03	7
S329	21.03	38.71	5b
S329	38.71	56.24	5a
S329	56.24	61.26	5b
S329	61.26	75.90	5a
S329	75.90	103.78	5b
S329	103.78	111.56	5a
S329	111.56	113.69	5b
S329	113.69	124.05	5a
S329	124.05	136.40	5b
S329	136.40	136.82	4a
S329	136.82	138.68	2
S329	138.68	142.04	1a
S330	0.00	43.28	7
S330	43.28	45.26	5b
S330	45.26	148.74	5a
S330	148.74	151.79	5b
S330	151.79	153.25	4a
S330	153.25	155.75	1a
S331	0.00	51.21	7
S332	0.00	29.87	7
S332	29.87	59.98	4a
S332	59.98	64.62	1a
S333	0.00	41.45	7
S333	41.45	43.65	4b
S333	43.65	63.86	4a
S333	63.86	65.07	2
S333	65.07	69.19	1a
S334	0.00	27.74	7
S334	27.74	50.90	5b
S334	50.90	53.95	5d
S334	53.95	66.14	5b
S334	66.14	72.24	5d
S334	72.24	72.85	5b
S334	72.85	73.97	6b
S334	73.97	75.47	4a
S334	75.47	75.62	2
S334	75.62	78.33	1a
S335	0.00	29.57	7
S335	29.57	35.66	5b
S335	35.66	53.64	5d
S335	53.64	54.25	5b
S335	54.25	56.39	5d
S335	56.39	57.30	5b
S335	57.30	58.83	5c
S335	58.83	60.05	5b
S335	60.05	76.96	5a

S335	76.96	80.16	5b
S335	80.16	82.08	4a
S335	82.08	82.48	2
S335	82.48	84.43	1a
S336	0.00	19.20	7
S336	19.20	35.05	5b
S336	35.05	68.88	5a
S336	68.88	72.69	5b
S336	72.69	73.15	5c
S336	73.15	79.25	5a
S336	79.25	80.77	5b
S336	80.77	81.23	5c
S336	81.23	82.91	5b
S336	82.91	105.70	5a
S336	105.70	108.11	4a
S336	108.11	108.81	1a
S337	0.00	15.54	7
S337	15.54	23.47	5b
S337	23.47	74.52	5a
S337	74.52	78.79	5b
S337	78.79	125.58	5a
S337	125.58	126.55	5b
S337	126.55	126.64	4b
S337	126.64	126.83	2
S337	126.83	128.32	1a
S338	0.00	55.17	7
S338	55.17	66.14	5b
S338	66.14	69.19	5a
S338	69.19	78.33	6b
S339	0.00	24.69	7
S339	24.69	59.44	4a
S339	59.44	63.09	1a
S340	0.00	10.27	7
S340	10.27	24.69	5b
S340	24.69	87.78	5a
S340	87.78	88.39	4b
S340	88.39	89.31	2
S340	89.31	93.88	1a
S341	0.00	4.88	7
S341	4.88	11.89	5b
S341	11.89	14.33	5d
S341	14.33	38.40	5a
S341	38.40	43.59	5b
S341	43.59	46.02	4a
S341	46.02	48.46	1a
S342	0.00	12.50	7
S342	12.50	14.33	5b
S342	14.33	30.48	4a
S342	30.48	32.61	2
S342	32.61	35.36	1a
S343	0.00	6.10	7
S343	6.10	9.81	4a
S343	9.81	14.63	1a
S344	0.00	9.75	7
S344	9.75	11.28	5b
S344	11.28	18.90	5a
S344	18.90	47.40	5b
S344	47.40	49.53	4b
S344	49.53	50.35	4a
S344	50.35	52.21	2
S344	52.21	54.25	1a
S345	0.00	59.44	7
S346	0.00	11.13	7
S346	11.13	18.59	5b
S346	18.59	45.57	5a
S346	45.57	47.55	5b
S346	47.55	72.24	5a
S346	72.24	78.64	5b
S346	78.64	149.05	5a
S346	149.05	150.88	5b
S346	150.88	153.92	1a
S347	0.00	24.32	7
S347	24.32	25.15	4a
S347	25.15	28.35	1a
S348	0.00	54.25	7
S348	54.25	54.96	2
S348	54.96	57.30	1a
S349	0.00	48.16	7
S349	48.16	49.68	5a
S349	49.68	49.87	5c
S349	49.87	50.29	5d

S349	50.29	50.93	5c
S349	50.93	54.25	5a
S349	54.25	54.44	5c
S349	54.44	54.77	5d
S349	54.77	54.89	5c
S349	54.89	57.79	5a
S349	57.79	58.70	5b
S349	58.70	74.52	5a
S349	74.52	75.35	5b
S349	75.35	83.27	5a
S349	83.27	83.67	4b
S349	83.67	84.34	4a
S349	84.34	85.04	2
S349	85.04	87.17	1a
S350	0.00	21.64	7
S350	21.64	21.95	5c
S350	21.95	36.88	5b
S350	36.88	61.87	5a
S350	61.87	65.07	5b
S350	65.07	156.36	5a
S350	156.36	159.35	5b
S350	159.35	161.67	4b
S350	161.67	161.97	2
S350	161.97	163.98	1a
S351	0.00	27.43	7
S351	27.43	63.70	5b
S351	63.70	69.49	5c
S351	69.49	72.54	5b
S351	72.54	78.64	5a
S351	78.64	79.40	5c
S351	79.40	100.28	5a
S351	100.28	100.58	5c
S351	100.58	127.71	5a
S351	127.71	129.48	5b
S351	129.48	130.76	2
S351	130.76	133.50	1a
S352	0.00	27.43	7
S352	27.43	39.32	5b
S352	39.32	41.61	5d
S352	41.61	45.26	5b
S352	45.26	57.15	5a
S352	57.15	64.62	5b
S352	64.62	72.54	5a
S352	72.54	75.90	5b
S352	75.90	95.86	5a
S352	95.86	96.80	5b
S352	96.80	96.93	5c
S352	96.93	98.76	5b
S352	98.76	105.61	5a
S352	105.61	109.15	5b
S352	109.15	109.32	5c
S352	109.32	110.02	4c
S352	110.02	110.64	4a
S352	110.64	110.70	2
S352	110.70	113.39	1a
S353	0.00	50.60	7
S353	50.60	59.53	5b
S353	59.53	61.26	5c
S353	61.26	63.09	5b
S353	63.09	68.12	5a
S353	68.12	69.49	5c
S353	69.49	94.64	5a
S353	94.64	95.71	5b
S353	95.71	95.95	5c
S353	95.95	96.16	5b
S353	96.16	97.63	4b
S353	97.63	99.76	2
S353	99.76	100.58	1a
S354	0.00	38.40	7
S354	38.40	57.15	5b
S354	57.15	65.50	4a
S354	65.50	70.56	4b
S354	70.56	71.17	4a
S354	71.17	72.15	4b
S354	72.15	75.29	2
S354	75.29	77.11	1a
S355	0.00	38.25	7
S355	38.25	38.50	4b
S355	38.50	38.68	4a
S355	38.68	40.29	4b
S355	40.29	44.04	4a

S355	44.04	44.65	4b
S355	44.65	44.90	4a
S355	44.90	45.11	1a
S356	0.00	29.08	7
S356	29.08	39.17	4a
S356	39.17	40.69	2
S356	40.69	45.11	1a
S357	0.00	62.48	7
S358	0.00	29.87	7
S358	29.87	30.78	5b
S358	30.78	97.84	5a
S358	97.84	101.04	5b
S358	101.04	103.17	5a
S358	103.17	105.92	5b
S358	105.92	106.31	5c
S358	106.31	106.59	5b
S358	106.59	107.44	4a
S358	107.44	111.19	2
S358	111.19	113.39	1a
S359	0.00	22.25	7
S359	22.25	23.77	5b
S359	23.77	79.25	5a
S359	79.25	86.11	5b
S359	86.11	94.03	5a
S359	94.03	98.45	5b
S359	98.45	113.69	5a
S359	113.69	115.21	5b
S359	115.21	130.61	5a
S359	130.61	132.28	5b
S359	132.28	133.05	4a
S359	133.05	136.86	1a
S360	0.00	23.16	7
S360	23.16	96.32	5b
S360	96.32	121.77	5a
S360	121.77	124.82	5b
S360	124.82	127.10	4b
S360	127.10	127.56	2
S360	127.56	132.89	1a
S361	0.00	61.57	7
S362	0.00	24.38	7
S362	24.38	58.83	5b
S362	58.83	73.00	5a
S362	73.00	78.33	5b
S362	78.33	84.73	5a
S362	84.73	86.26	5b
S362	86.26	111.86	5a
S362	111.86	116.13	5b
S362	116.13	117.90	4a
S362	117.90	121.01	1a
S363	0.00	44.81	7
S363	44.81	52.43	5b
S363	52.43	60.05	5a
S363	60.05	62.48	5b
S363	62.48	91.74	5a
S363	91.74	94.49	5b
S363	94.49	96.32	5a
S363	96.32	98.88	5b
S363	98.88	99.79	4a
S363	99.79	105.77	1a
S364	0.00	18.75	7
S364	18.75	53.64	5b
S364	53.64	68.43	5a
S364	68.43	73.15	5b
S364	73.15	79.86	5a
S364	79.86	81.84	5b
S364	81.84	103.48	5a
S364	103.48	106.07	5b
S364	106.07	112.47	5a
S364	112.47	112.72	5c
S364	112.72	114.82	5b
S364	114.82	115.24	4a
S364	115.24	122.53	1a
S365	0.00	47.85	7
S365	47.85	48.16	5c
S365	48.16	55.47	5b
S365	55.47	69.80	5a
S365	69.80	74.98	5b
S365	74.98	83.21	5a
S365	83.21	85.34	5c
S365	85.34	91.14	5b
S365	91.14	118.90	5a
S365	118.90	120.27	4a
S365	120.27	122.29	5b
S365	122.29	124.15	4a
S365	124.15	124.30	2
S365	124.30	130.15	1a
S366	0.00	46.94	7
S366	46.94	47.55	5d
S366	47.55	53.95	5b
S366	53.95	54.86	5d
S366	54.86	57.00	5b
S366	57.00	58.52	5d
S366	58.52	69.19	5b
S366	69.19	70.41	5d
S366	70.41	72.24	5b
S366	72.24	78.03	5d
S366	78.03	78.33	5b
S366	78.33	87.02	5d
S366	87.02	87.33	5c
S366	87.33	87.48	5b
S366	87.48	88.09	5d
S366	88.09	91.44	5b
S366	91.44	97.54	5d
S366	97.54	99.67	5b
S366	99.67	102.41	5d
S366	102.41	102.72	5b
S367	0.00	100.19	7
S367	100.19	110.34	4a
S367	110.34	110.49	2
S367	110.49	113.39	1a
S368	0.00	79.86	7
S368	79.86	84.73	4a
S368	84.73	88.70	4b
S368	88.70	96.10	2
S368	96.10	104.85	1a
S369	0.00	18.59	7
S369	18.59	35.81	4a
S369	35.81	39.35	4b
S369	39.35	40.08	2
S369	40.08	43.89	1a
S370	0.00	34.44	7
S370	34.44	36.58	5b
S370	36.58	182.58	5a
S370	182.58	186.23	5b
S370	186.23	191.11	1a
S371	0.00	53.34	7
S371	53.34	57.91	5b
S371	57.91	255.12	5a
S371	255.12	255.67	4a
S371	255.67	256.03	2
S371	256.03	258.17	1a
S372	0.00	68.58	7
S372	68.58	181.05	5a
S372	181.05	181.51	5c
S372	181.51	284.23	5a
S372	284.23	285.29	5b
S372	285.29	285.57	4b
S372	285.57	285.90	2
S372	285.90	286.51	1a
S373	0.00	34.14	7
S373	34.14	65.23	5b
S373	65.23	70.41	5c
S373	70.41	125.58	5b
S373	125.58	259.84	5b
S373	259.84	260.91	4a
S373	260.91	270.05	2
S373	270.05	270.97	1b
S374	0.00	28.96	7
S374	28.96	34.14	5b
S374	34.14	65.53	5a
S374	65.53	68.43	5b
S374	68.43	69.04	4a
S374	69.04	69.65	4b
S374	69.65	71.26	4a
S374	71.26	82.91	2
S374	82.91	108.81	1b
S375	0.00	46.79	7
S375	46.79	64.98	5a
S375	64.98	65.53	6a
S375	65.53	65.56	4b
S375	65.56	66.05	4a
S375	66.05	66.45	4b
S375	66.45	66.90	2
S375	66.90	69.19	1b
S376	0.00	50.75	7
S376	50.75	53.95	5b
S376	53.95	93.24	5a
S376	93.24	95.04	4a
S376	95.04	99.82	2
S376	99.82	104.85	1b
S377	0.00	49.07	7
S377	49.07	49.59	5c
S377	49.59	53.95	5b
S377	53.95	108.51	5a
S377	108.51	110.19	5b
S377	110.19	111.10	6a
S377	111.10	113.84	4a
S377	113.84	119.48	3
S378	0.00	16.86	7
S378	16.86	17.37	5b
S378	17.37	20.42	5d
S378	20.42	35.51	5b
S378	35.51	35.66	5c
S378	35.66	36.12	5c
S378	36.12	50.90	5b
S378	50.90	51.91	5c
S378	51.91	53.95	5b
S378	53.95	55.02	5c
S378	55.02	57.91	5b
S378	57.91	87.78	5c
S379	0.00	15.24	7
S379	15.24	20.73	5b
S379	20.73	90.13	5a
S379	90.13	94.00	5b
S379	94.00	114.76	5a
S379	114.76	114.97	5c
S379	114.97	148.86	5a
S379	148.86	149.05	5c
S379	149.05	151.79	5a
S379	151.79	152.10	4a
S379	152.10	154.53	1a
S380	0.00	25.30	7
S380	25.30	43.16	4a
S380	43.16	46.73	4b
S380	46.73	48.34	2
S380	48.34	50.90	1a
S381	0.00	23.47	7
S381	23.47	26.82	5b
S381	26.82	57.15	5a
S381	57.15	58.98	5b
S381	58.98	77.72	5a
S381	77.72	83.21	5b
S381	83.21	83.52	5c
S381	83.52	85.95	5b
S381	85.95	92.35	5a
S381	92.35	93.42	5b
S381	93.42	94.18	5c
S381	94.18	95.40	5b
S381	95.40	117.35	5a
S381	117.35	118.41	5b
S381	118.41	156.70	5a
S381	156.70	157.00	4b
S381	157.00	157.70	2
S381	157.70	159.41	1a
S382	0.00	32.92	7
S382	32.92	66.90	5a
S382	66.90	71.63	5b
S382	71.63	90.68	5a
S382	90.68	109.12	5b
S382	109.12	144.17	5a
S382	144.17	145.08	5b
S382	145.08	197.66	5a
S382	197.66	198.42	5b
S382	198.42	198.85	4a
S382	198.85	199.03	2
S382	199.03	199.95	1a
S383	0.00	29.26	7
S383	29.26	33.62	5b
S383	33.62	67.36	5a
S383	67.36	72.69	5b
S383	72.69	90.68	5a
S383	90.68	97.38	5b
S383	97.38	105.16	5a
S383	105.16	110.95	5b
S383	110.95	194.46	5a
S383	194.46	195.68	5b
S383	195.68	197.78	2
S383	197.78	198.12	1a
S384	0.00	17.37	7
S384	17.37	17.98	5b
S384	17.98	19.20	5d
S384	19.20	20.88	5b
S384	20.88	79.71	5a
S384	79.71	91.29	5b
S384	91.29	93.27	5c
S384	93.27	101.50	5b
S384	101.50	102.26	5c
S384	102.26	132.89	5a
S384	132.89	133.90	5b
S384	133.90	135.09	4a
S384	135.09	136.73	2
S384	136.73	138.07	1a
S385	0.00	24.08	7
S385	24.08	51.21	5b
S385	51.21	75.29	5a
S385	75.29	75.59	5d
S385	75.59	96.01	5a
S385	96.01	118.26	5c
S385	118.26	129.24	5a
S385	129.24	130.45	5b
S385	130.45	130.76	4b
S385	130.76	133.50	1a
S386	0.00	32.31	7
S386	32.31	36.88	5b
S386	36.88	80.31	5a
S386	80.31	117.04	5b
S386	117.04	122.38	5a
S386	122.38	126.03	5b
S386	126.03	147.68	5a
S386	147.68	149.17	5b
S386	149.17	149.84	4a
S386	149.84	151.79	1a
S387	0.00	32.31	7
S387	32.31	148.74	5a
S387	148.74	149.14	5b
S387	149.14	149.75	4b
S387	149.75	151.49	2
S388	0.00	36.58	7
S388	36.58	39.01	5a
S388	39.01	43.28	5b
S388	43.28	64.22	5a
S388	64.22	65.07	5b
S388	65.07	71.93	5a
S388	71.93	92.05	5d
S388	92.05	97.23	5b
S388	97.23	103.33	5a
S388	103.33	106.07	5d
S388	106.07	109.88	5b
S388	109.88	111.04	4a
S388	111.04	112.23	4b
S388	112.23	113.84	2
S388	113.84	115.21	1a
S389	0.00	68.88	7
S389	68.88	79.31	4a
S389	79.31	81.08	2
S389	81.08	83.52	1a
S390	0.00	45.42	7
S390	45.42	53.16	4b
S390	53.16	55.02	2
S390	55.02	57.00	1a
S391	0.00	21.64	7
S391	21.64	35.97	5b
S391	35.97	44.35	5a
S391	44.35	45.87	5b
S391	45.87	82.91	5a
S391	82.91	84.12	5b
S391	84.12	84.43	5c
S391	84.43	85.65	5b
S391	85.65	103.02	5a
S391	103.02	103.33	5c
S391	103.33	135.33	5a
S391	135.33	138.53	5b
S391	138.53	138.68	4a
S391	138.68	140.88	2

S391	140.88	142.65	1a
S392	0.00	18.59	7
S392	18.59	36.58	5b
S392	36.58	60.50	5a
S392	60.50	60.81	5b
S392	60.81	73.76	5a
S392	73.76	75.29	5b
S392	75.29	95.10	5a
S392	95.10	96.32	5b
S392	96.32	110.95	5a
S392	110.95	111.56	5c
S392	111.56	113.90	5b
S392	113.90	118.57	4a
S392	118.57	119.94	5a
S392	119.94	120.09	5b
S392	120.09	121.68	4a
S392	121.68	123.29	2
S392	123.29	123.75	1a
S393	0.00	21.34	7
S393	21.34	26.94	4a
S393	26.94	29.35	4e
S393	29.35	30.72	4a
S393	30.72	31.52	4e
S393	31.52	34.90	4a
S393	34.90	36.27	2
S393	36.27	38.71	1a
S394	0.00	23.10	7
S394	23.10	25.60	1a
S395	0.00	24.38	7
S395	24.38	25.91	1a
S396	0.00	16.46	7
S396	16.46	18.29	1a
S397	0.00	16.76	7
S397	16.76	22.86	4a
S397	22.86	24.69	1a
S398	0.00	81.08	7
S398	81.08	81.69	5c
S398	81.69	82.30	5d
S398	82.30	86.26	5b
S398	86.26	87.23	6a
S398	87.23	90.68	4a
S398	90.68	90.77	2
S398	90.77	93.57	1a
S399	0.00	9.14	7
S399	9.14	38.71	5a
S399	38.71	39.01	5d
S399	39.01	56.39	5b
S399	56.39	112.17	5a
S400	0.00	24.17	7
S400	24.17	37.64	4a
S400	37.64	38.56	4b
S400	38.56	47.46	4a
S400	47.46	57.76	2
S400	57.76	60.05	1a
S401	0.00	16.25	7
S401	16.25	29.57	4a
S401	29.57	40.84	2
S401	40.84	44.81	1a
S402	0.00	23.62	7
S402	23.62	40.54	4b
S402	40.54	51.39	4a
S402	51.39	56.39	2
S402	56.39	60.05	1a
S403	0.00	49.38	7
S404	0.00	40.84	7
S404	40.84	54.04	4a
S404	54.04	55.60	2
S404	55.60	56.39	1a
S405	0.00	12.65	7
S405	12.65	23.01	5b
S405	23.01	58.83	5a
S405	58.83	60.35	5b
S405	60.35	71.02	5a
S405	71.02	72.54	5b
S405	72.54	239.88	5a
S406	0.00	34.08	7
S406	34.08	89.12	5a
S406	89.12	90.83	5b
S406	90.83	99.52	5a
S406	99.52	103.94	5b
S406	103.94	243.84	5a
S407	0.00	36.27	7
S407	36.27	67.97	5a
S407	67.97	69.49	5c
S407	69.49	71.93	5d
S407	71.93	75.44	5c
S407	75.44	77.72	5a
S408	0.00	68.88	7
S408	68.88	138.99	5a
S408	138.99	139.60	5b
S408	139.60	244.21	5a
S409	0.00	23.47	7
S409	23.47	84.28	5a
S409	84.28	85.34	4a
S409	85.34	85.53	2
S409	85.53	93.57	1a
S410	0.00	12.50	7
S410	12.50	25.30	5b
S410	25.30	35.97	5a
S410	35.97	38.10	5b
S410	38.10	69.49	5a
S410	69.49	69.95	5c
S410	69.95	101.50	5a
S410	101.50	103.33	5b
S410	103.33	106.07	2
S410	106.07	108.18	1a
S411	0.00	63.52	7
S411	63.52	75.29	5b
S411	75.29	76.66	5d
S411	76.66	78.33	5b
S411	78.33	83.48	6a
S411	83.48	84.83	4a
S411	84.83	85.10	2
S412	0.00	42.06	7
S412	42.06	51.82	5b
S412	51.82	56.39	5a
S412	56.39	60.35	5b
S412	60.35	63.09	5a
S412	63.09	64.01	5c
S412	64.01	87.48	5a
S412	87.48	90.07	5b
S412	90.07	93.67	4a
S412	93.67	94.49	1a
S413	0.00	26.52	7
S413	26.52	28.04	5b
S413	28.04	67.97	5a
S413	67.97	72.54	5b
S413	72.54	98.76	5a
S413	98.76	99.97	5b
S413	99.97	101.96	4a
S413	101.96	103.94	5a
S413	103.94	106.07	4a
S413	106.07	107.47	2
S413	107.47	111.25	1a
S414	0.00	67.67	7
S414	67.67	80.77	4a
S414	80.77	83.82	1a
S415	0.00	28.96	7
S415	28.96	57.70	4a
S415	57.70	62.70	2
S415	62.70	65.53	1a
S416	0.00	27.13	7
S416	27.13	38.40	4a
S416	38.40	39.53	4b
S416	39.53	39.78	4a
S416	39.78	40.39	4b
S416	40.39	42.15	4a
S416	42.15	42.49	4b
S416	42.49	47.27	4a
S416	47.27	50.90	2
S416	50.90	53.34	1a
S417	0.00	26.82	7
S417	26.82	27.16	4a
S417	27.16	27.52	4e
S417	27.52	63.09	4a
S417	63.09	69.65	2
S417	69.65	71.63	1a
S418	0.00	56.69	7
S419	0.00	43.59	7
S420	0.00	26.82	7
S420	26.82	54.65	5a
S420	54.65	62.33	4a
S420	62.33	70.04	2
S420	70.04	75.90	1a
S421	0.00	28.96	7
S421	28.96	29.26	4a
S421	29.26	32.58	4e
S421	32.58	36.58	4a
S421	36.58	46.94	1a
S422	0.00	27.13	7
S422	27.13	34.14	1a
S423	0.00	21.34	7
S423	21.34	125.06	5a
S423	125.06	128.53	4a
S423	128.53	133.62	2
S423	133.62	136.25	1a
S424	0.00	17.37	7
S424	17.37	42.67	5a
S424	42.67	45.72	5b
S424	45.72	72.24	5a
S425	0.00	15.42	7
S425	15.42	138.99	5a
S425	138.99	142.49	4a
S425	142.49	147.22	2
S425	147.22	151.18	1a
S426	0.00	15.24	7
S426	15.24	75.59	5a
S426	75.59	76.81	5b
S426	76.81	135.03	5a
S426	135.03	137.22	2
S426	137.22	142.34	1a
S427	0.00	39.62	7
S427	39.62	47.98	6a
S427	47.98	48.22	4a
S427	48.22	48.31	4b
S427	48.31	48.77	4a
S427	48.77	51.27	4b
S427	51.27	51.82	4a
S427	51.82	56.08	1a
S428	0.00	54.86	7
S428	54.86	58.22	4b
S428	58.22	58.52	4a
S428	58.52	60.38	4b
S428	60.38	65.23	2
S428	65.23	69.19	1a
S429	0.00	18.20	7
S429	18.20	36.52	5b
S429	36.52	50.96	5a
S429	50.96	59.19	5b
S429	59.19	78.33	5a
S429	78.33	82.54	5b
S429	82.54	84.98	4a
S429	84.98	85.77	2
S429	85.77	86.87	1a
S430	0.00	71.02	7
S430	71.02	73.46	4a
S431	0.00	47.40	7
S431	47.40	74.62	4a
S431	74.62	82.91	2
S432	0.00	32.92	7
S432	32.92	50.84	4a
S432	50.84	62.18	2
S432	62.18	63.09	1a
S433	0.00	26.58	7
S433	26.58	27.86	4a
S433	27.86	34.99	2
S433	34.99	35.72	1a
S434	0.00	27.43	7
S434	27.43	28.96	1a
S435	0.00	14.63	7
S435	14.63	17.68	1a
S436	0.00	4.57	7
S436	4.57	6.10	1a
S437	0.00	7.62	7
S437	7.62	19.51	2
S437	19.51	23.47	1a
S438	0.00	6.10	7
S438	6.10	23.47	2
S438	23.47	29.57	1a
S439	0.00	6.71	7
S439	6.71	17.37	4a
S439	17.37	18.04	2
S439	18.04	20.42	1a
S440	0.00	52.73	7
S440	52.73	81.38	5b
S440	81.38	84.12	5a
S440	84.12	85.34	5b
S440	85.34	94.61	5a
S440	94.61	107.29	5b
S440	107.29	110.95	6b
S440	110.95	111.65	4a
S440	111.65	115.21	2
S440	115.21	117.96	1a
S441	0.00	30.48	7
S442	0.00	47.85	7
S442	47.85	49.77	5b
S442	49.77	51.82	6a
S442	51.82	53.46	4a
S442	53.46	54.56	2
S442	54.56	59.44	1a
S443	0.00	45.72	7
S443	45.72	46.02	4b
S443	46.02	48.46	4a
S443	48.46	49.74	4b
S443	49.74	52.33	4a
S443	52.33	52.79	2
S443	52.79	57.30	1a
S444	0.00	25.91	7
S444	25.91	43.59	5b
S444	43.59	67.06	6a
S444	67.06	75.59	4a
S444	75.59	77.72	2
S444	77.72	81.38	1a
S445	0.00	85.04	7
S445	85.04	90.68	2
S445	90.68	96.62	1a
S446	0.00	16.76	7
S446	16.76	39.11	4a
S446	39.11	40.54	1a
S447	0.00	12.80	7
S447	12.80	29.35	4a
S447	29.35	30.91	2
S447	30.91	31.70	1a
S448	0.00	13.87	7
S448	13.87	34.75	4a
S448	34.75	36.18	2
S448	36.18	38.10	1a
S449	0.00	18.29	7
S449	18.29	34.90	4a
S449	34.90	38.69	1a
S450	0.00	9.39	7
S450	9.39	19.51	5b
S450	19.51	21.34	5a
S450	21.34	24.29	5b
S450	24.29	24.99	5d
S450	24.99	110.43	5a
S450	110.43	113.17	4a
S450	113.17	113.69	2
S450	113.69	117.04	1a
S451	0.00	26.21	7
S451	26.21	26.91	4a
S451	26.91	28.96	1a
S452	0.00	32.92	7
S452	32.92	35.97	1a
S453	0.00	26.52	7
S453	26.52	50.90	5a
S453	50.90	53.64	5b
S453	53.64	56.14	4a
S453	56.14	62.18	2
S453	62.18	63.09	1a
S454	0.00	24.99	7
S454	24.99	38.34	5b
S454	38.34	43.59	5a
S454	43.59	44.65	5b
S454	44.65	65.68	5a
S454	65.68	66.26	5d
S454	66.26	99.91	5a
S454	99.91	101.38	4a
S454	101.38	103.02	1a
S455	0.00	22.86	7
S455	22.86	137.16	5a
S455	137.16	137.80	4a
S455	137.80	139.60	1a
S456	0.00	26.24	7

S456	26.24	28.86	4a
S456	28.86	35.81	2
S456	35.81	37.49	1a
S457	0.00	26.21	7
S457	26.21	63.49	5a
S457	63.49	65.17	5b
S457	65.17	92.02	5a
S457	92.02	93.88	5b
S457	93.88	95.40	4a
S457	95.40	96.93	1a
S458	0.00	25.60	7
S458	25.60	27.55	5b
S458	27.55	59.74	5a
S458	59.74	62.18	5c
S458	62.18	81.08	5a
S458	81.08	81.87	5c
S458	81.87	159.72	5a
S458	159.72	160.20	5b
S458	160.20	162.76	2
S458	162.76	163.98	1a
S459	0.00	21.64	7
S459	21.64	27.74	5b
S459	27.74	75.59	5a
S459	75.59	76.20	5b
S459	76.20	158.34	5a
S459	158.34	159.72	2
S459	159.72	160.93	1a
S460	0.00	35.97	7
S460	35.97	62.58	4a
S460	62.58	64.62	1a
S461	0.00	49.68	7
S461	49.68	55.78	5b
S461	55.78	66.75	5a
S461	66.75	67.97	5c
S461	67.97	68.88	5a
S461	68.88	69.49	5d
S461	69.49	84.73	5a
S461	84.73	99.67	6a
S461	99.67	100.13	4a
S461	100.13	104.55	4b
S461	104.55	107.59	4a
S461	107.59	113.48	2
S461	113.48	114.91	1a
S462	0.00	52.12	7
S462	52.12	55.47	4b
S462	55.47	55.81	4a
S462	55.81	56.17	4b
S462	56.17	68.61	4a
S462	68.61	75.29	2
S462	75.29	77.11	1a
S463	0.00	41.45	7
S463	41.45	48.46	5a
S463	48.46	57.03	5d
S463	57.03	57.18	5c
S463	57.18	71.32	5a
S463	71.32	77.42	6a
S463	77.42	81.44	4a
S463	81.44	83.18	2
S463	83.18	85.95	1a
S464	0.00	21.70	7
S464	21.70	62.91	4a
S464	62.91	63.09	2
S464	63.09	68.58	1a
S465	0.00	18.29	7
S465	18.29	38.65	4a
S465	38.65	39.75	4b
S465	39.75	44.71	4a
S465	44.71	46.42	4b
S465	46.42	49.56	4a
S465	49.56	52.94	2
S465	52.94	55.17	1a
S466	0.00	30.18	7
S466	30.18	50.44	4a
S466	50.44	50.60	2
S466	50.60	55.78	1a
S467	0.00	28.35	7
S467	28.35	53.95	5a
S467	53.95	59.53	5b
S467	59.53	84.43	5a
S467	84.43	87.02	4a
S467	87.02	87.48	2
S467	87.48	89.31	1a
S468	0.00	37.80	7
S468	37.80	40.90	4a
S468	40.90	41.64	4b
S468	41.64	48.46	4a
S469	0.00	39.62	7
S470	0.00	38.44	7
S470	38.44	68.21	4a
S470	68.21	77.57	2
S470	77.57	80.16	1a
S471	0.00	28.96	7
S471	28.96	31.85	2
S471	31.85	36.58	1a
S472	0.00	34.59	7
S472	34.59	58.28	4a
S472	58.28	60.96	2
S472	60.96	64.92	1a
S473	0.00	67.06	7
S473	67.06	79.98	4a
S473	79.98	83.52	1a
S474	0.00	41.15	7
S475	0.00	47.85	7
S475	47.85	63.09	5a
S475	63.09	63.73	5b
S475	63.73	107.29	5a
S475	107.29	108.63	5d
S475	108.63	108.81	5b
S475	108.81	109.09	5c
S475	109.09	110.15	5d
S475	110.15	111.31	5a
S475	111.31	112.68	4a
S475	112.68	113.84	2
S475	113.84	117.96	1a
S476	0.00	43.16	7
S476	43.16	79.46	4a
S476	79.46	89.52	2
S476	89.52	95.10	1a
S477	0.00	72.39	7
S477	72.39	75.59	5b
S477	75.59	90.83	6a
S478	0.00	70.41	7
S478	70.41	84.43	5b
S479	0.00	89.31	7
S479	89.31	91.14	4c
S479	91.14	92.84	4e
S479	92.84	94.27	4b
S479	94.27	97.20	4a
S479	97.20	99.30	2
S479	99.30	102.72	1a
S480	0.00	13.26	7
S480	13.26	51.21	5a
S480	51.21	51.36	5b
S480	51.36	76.75	5a
S480	76.75	77.91	5b
S480	77.91	181.45	5a
S480	181.45	182.42	4a
S480	182.42	183.43	2
S480	183.43	187.15	1a
S481	0.00	25.97	7
S481	25.97	200.86	5a
S481	200.86	206.35	1a
S482	0.00	39.62	7
S482	39.62	44.81	1b
S483	0.00	47.70	7
S483	47.70	50.29	1b
S484	0.00	51.82	7
S484	51.82	52.30	3
S484	52.30	56.08	1b
S485	0.00	52.12	7
S485	52.12	82.60	5a
S485	82.60	93.57	5d
S486	0.00	16.76	7
S486	16.76	23.47	5b
S486	23.47	64.47	5a
S486	64.47	64.62	5d
S486	64.62	200.25	5a
S486	200.25	200.44	4a
S486	200.44	200.86	2
S486	200.86	215.49	1a
S487	0.00	3.05	7
S487	3.05	5.49	1a
S488	0.00	29.26	7
S488	29.26	30.18	2
S488	30.18	31.39	1a
S489	0.00	16.46	7
S489	16.46	27.13	5b
S489	27.13	47.24	5a
S489	47.24	48.00	5d
S489	48.00	50.14	5a
S489	50.14	51.05	5d
S489	51.05	57.30	5a
S489	57.30	58.83	5b
S489	58.83	60.29	4a
S489	60.29	63.40	1a
S490	0.00	73.40	7
S490	73.40	79.28	5b
S490	79.28	87.29	4a
S490	87.29	91.44	2
S490	91.44	96.32	1a
S491	0.00	54.86	7
S491	54.86	59.59	2
S491	59.59	66.14	4b
S491	66.14	79.71	4a
S491	79.71	83.67	2
S491	83.67	87.48	1a
S492	0.00	33.68	7
S492	33.68	39.01	4b
S492	39.01	40.54	4a
S492	40.54	42.67	4b
S492	42.67	43.89	4a
S492	43.89	69.19	4b
S492	69.19	78.33	2
S492	78.33	81.38	1a
S493	0.00	37.49	7
S493	37.49	63.09	4a
S493	63.09	72.24	1a
S494	0.00	33.53	7
S494	33.53	65.87	4a
S494	65.87	66.26	2
S494	66.26	67.67	1a
S495	0.00	29.87	7
S495	29.87	55.84	4a
S495	55.84	58.83	1a
S496	0.00	28.16	7
S496	28.16	56.54	4a
S496	56.54	61.26	1a
S497	0.00	28.04	7
S497	28.04	59.98	4a
S497	59.98	61.23	4b
S497	61.23	62.39	2
S497	62.39	65.23	1a
S498	0.00	58.52	7
S498	58.52	61.72	4b
S498	61.72	62.03	4a
S498	62.03	62.45	4b
S498	62.45	65.99	4a
S498	65.99	66.63	2
S498	66.63	69.80	1a
S499	0.00	17.37	7
S499	17.37	20.60	4a
S499	20.60	23.10	4e
S499	23.10	51.45	4a
S499	51.45	55.29	2
S499	55.29	58.22	1a
S500	0.00	18.29	7
S500	18.29	22.56	5b
S500	22.56	60.20	5a
S500	60.20	60.50	5b
S500	60.50	115.06	5a
S500	115.06	117.65	5b
S500	117.65	118.41	4a
S500	118.41	120.85	2
S500	120.85	124.36	1a
S501	0.00	39.93	7
S501	39.93	55.78	5a
S501	55.78	58.22	5b
S501	58.22	60.66	4a
S501	60.66	61.57	2
S501	61.57	63.40	1a
S502	0.00	16.15	7
S502	16.15	43.59	5a
S502	43.59	45.23	5b
S502	45.23	45.42	4b
S502	45.42	46.33	4a
S502	46.33	47.43	4b
S502	47.43	51.21	4a
S502	51.21	57.61	2
S502	57.61	59.74	1a
S503	0.00	21.34	7
S503	21.34	27.74	4a
S503	27.74	34.44	2
S503	34.44	35.36	1a
S504	0.00	21.34	7
S504	21.34	22.71	1a
S505	0.00	14.33	7
S505	14.33	20.73	5b
S505	20.73	36.73	5a
S505	36.73	40.54	5b
S505	40.54	78.33	5a
S505	78.33	80.77	4a
S505	80.77	83.52	2
S506	0.00	14.63	7
S506	14.63	90.07	5a
S506	90.07	90.83	5c
S506	90.83	114.51	5a
S506	114.51	114.85	4b
S506	114.85	115.92	4a
S506	115.92	117.81	4b
S506	117.81	124.11	4a
S506	124.11	128.63	2
S506	128.63	131.98	1a
S507	0.00	14.02	7
S507	14.02	14.63	5b
S507	14.63	83.52	5a
S507	83.52	83.82	5b
S507	83.82	107.29	5a
S507	107.29	108.56	5b
S507	108.56	109.42	4a
S507	109.42	110.09	2
S507	110.09	112.17	1a
S508	0.00	15.24	7
S508	15.24	17.68	5b
S508	17.68	41.21	5a
S508	41.21	41.67	5b
S508	41.67	62.00	5a
S508	62.00	62.18	5b
S508	62.18	92.23	5a
S508	92.23	92.42	5c
S508	92.42	115.21	5a
S508	115.21	117.50	5b
S508	117.50	117.71	4a
S508	117.71	121.31	1a
S509	0.00	12.80	7
S509	12.80	13.72	5b
S509	13.72	29.57	5a
S509	29.57	33.83	5c
S509	33.83	34.29	5b
S509	34.29	35.05	4a
S509	35.05	35.66	4e
S509	35.66	40.90	4a
S509	40.90	45.11	2
S510	0.00	10.21	7
S510	10.21	11.83	4a
S510	11.83	13.11	2
S510	13.11	17.37	1a
S511	0.00	11.58	7
S511	11.58	14.33	1a
S512	0.00	9.75	7
S512	9.75	11.28	1a
S513	0.00	7.92	7
S513	7.92	11.28	1a
S514	0.00	11.58	7
S514	11.58	14.81	2
S514	14.81	15.54	1a
S515	0.00	22.25	7
S515	22.25	25.12	4a
S515	25.12	32.61	1a
S516	0.00	4.57	7
S516	4.57	5.79	2
S516	5.79	6.10	1a
S517	0.00	5.79	7
S517	5.79	18.23	2
S517	18.23	23.47	1a

S518	0.00	3.05	7
S518	3.05	17.37	3
S518	17.37	19.81	2
S518	19.81	23.47	1a
S519	0.00	3.48	7
S519	3.48	36.58	3
S519	36.58	38.74	2
S519	38.74	41.76	1a
S520	0.00	27.43	7
S520	27.43	72.24	3
S520	72.24	72.54	2
S520	72.54	75.29	1a
S521	0.00	39.62	7
S521	39.62	40.84	1a
S522	0.00	30.48	7
S522	30.48	33.83	1a
S523	0.00	25.91	7
S523	25.91	27.74	1a
S524	0.00	39.62	7
S524	39.62	41.76	5b
S524	41.76	44.50	5d
S524	44.50	45.42	5a
S524	45.42	46.33	5d
S524	46.33	52.12	5a
S524	52.12	53.64	5d
S524	53.64	53.95	5b
S524	53.95	60.05	5d
S524	60.05	61.57	5a
S524	61.57	67.06	5d
S524	67.06	69.19	5a
S524	69.19	76.50	5d
S525	0.00	26.21	7
S525	26.21	41.76	5b
S525	41.76	53.19	5a
S525	53.19	53.95	5d
S525	53.95	59.74	5b
S525	59.74	64.31	5a
S525	64.31	65.84	5d
S525	65.84	69.86	5b
S525	69.86	72.82	5a
S525	72.82	75.80	5b
S525	75.80	81.50	5a
S525	81.50	83.52	5b
S525	83.52	85.65	5a
S525	85.65	86.87	6a
S525	86.87	87.48	4a
S525	87.48	89.55	2
S525	89.55	93.57	1a
S526	0.00	45.11	7
S526	45.11	60.66	4a
S526	60.66	64.01	2
S526	64.01	68.58	1a
S527	0.00	20.12	7
S527	20.12	44.71	4a
S527	44.71	49.19	2
S527	49.19	52.73	1a
S528	0.00	19.81	7
S528	19.81	21.95	4a
S528	21.95	32.71	2
S528	32.71	35.66	1a
S529	0.00	60.96	7
S530	0.00	42.67	7
S531	0.00	70.10	7
S532	0.00	42.37	7
S532	42.37	44.99	5b
S532	44.99	57.30	5a
S532	57.30	60.72	4a
S532	60.72	66.45	4e
S532	66.45	67.48	4a
S532	67.48	69.49	4e
S532	69.49	76.38	4a
S532	76.38	79.00	2
S532	79.00	81.69	1a
S533	0.00	20.12	7
S533	20.12	20.73	5b
S533	20.73	62.97	5a
S533	62.97	65.84	4a
S533	65.84	66.29	2
S533	66.29	68.58	1a
S534	0.00	16.15	7
S534	16.15	80.16	5a
S534	80.16	82.91	4a
S534	82.91	83.21	2
S534	83.21	87.78	1a
S535	0.00	31.70	7
S535	31.70	36.55	5b
S535	36.55	37.70	5a
S535	37.70	43.59	5b
S535	43.59	55.17	5d
S535	55.17	57.91	5b
S535	57.91	64.89	5a
S535	64.89	65.53	4a
S536	0.00	17.07	7
S536	17.07	24.60	5b
S536	24.60	26.70	5a
S536	26.70	32.00	5b
S536	32.00	35.97	5a
S536	35.97	37.95	5b
S536	37.95	64.31	5a
S536	64.31	65.84	5b
S536	65.84	68.92	4a
S536	68.92	70.41	1a
S537	0.00	38.40	7
S537	38.40	43.95	5b
S537	43.95	51.51	5a
S537	51.51	55.78	5d
S537	55.78	58.52	5a
S537	58.52	60.35	5b
S537	60.35	86.26	5a
S537	86.26	89.31	5b
S537	89.31	98.27	5a
S537	98.27	106.92	4a
S537	106.92	108.39	2
S537	108.39	109.73	1a
S538	0.00	64.62	7
S539	0.00	15.24	7
S539	15.24	37.55	4a
S539	37.55	38.71	1a
S540	0.00	41.61	7
S540	41.61	42.49	4b
S540	42.49	51.88	4a
S540	51.88	52.73	4b
S540	52.73	57.61	4a
S540	57.61	62.97	2
S540	62.97	66.14	1a
S541	0.00	53.95	7
S541	53.95	65.11	4a
S541	65.11	68.92	2
S541	68.92	71.63	1a
S542	0.00	20.51	7
S542	20.51	37.19	5b
S542	37.19	38.40	5d
S542	38.40	54.68	5b
S542	54.68	56.08	5d
S542	56.08	57.00	5b
S542	57.00	67.97	5a
S542	67.97	68.43	5d
S542	68.43	69.13	5a
S542	69.13	79.00	4a
S542	79.00	84.73	2
S542	84.73	88.39	1a
S543	0.00	28.16	7
S543	28.16	36.88	5b
S543	36.88	49.13	5d
S543	49.13	56.08	5b
S543	56.08	56.69	5d
S543	56.69	60.05	5b
S543	60.05	78.21	5a
S543	78.21	78.55	5c
S543	78.55	79.86	5b
S543	79.86	83.94	4a
S543	83.94	85.50	2
S543	85.50	87.48	1a
S544	0.00	44.81	7
S544	44.81	50.29	4a
S544	50.29	53.64	2
S544	53.64	54.35	1a
S545	0.00	40.23	7
S545	40.23	66.54	4a
S545	66.54	67.36	1a
S546	0.00	42.52	7
S546	42.52	84.43	4a
S546	84.43	87.48	1a
S547	0.00	42.67	7
S547	42.67	42.82	4a
S547	42.82	44.10	4e
S547	44.10	44.87	4a
S547	44.87	45.42	4e
S547	45.42	52.43	4a
S547	52.43	54.56	4e
S547	54.56	57.45	4a
S547	57.45	59.86	4e
S547	59.86	87.72	4a
S547	87.72	91.44	2
S547	91.44	93.57	1a
S548	0.00	87.78	7
S548	87.78	88.70	4a
S549	0.00	64.01	7
S549	64.01	64.68	5b
S549	64.68	66.14	5d
S549	66.14	66.75	5b
S549	66.75	68.88	5d
S549	68.88	72.24	5b
S549	72.24	90.22	6b
S549	90.22	90.37	4b
S549	90.37	98.36	4a
S549	98.36	101.19	2
S549	101.19	102.72	1a
S550	0.00	44.41	7
S550	44.41	46.02	5b
S550	46.02	47.24	5d
S550	47.24	49.68	5b
S550	49.68	66.14	5a
S550	66.14	66.60	5b
S550	66.60	70.10	5d
S550	70.10	93.88	5a
S551	0.00	49.07	7
S551	49.07	72.24	5a
S551	72.24	72.85	5b
S551	72.85	121.01	5a
S551	121.01	124.05	5b
S551	124.05	125.15	4a
S551	125.15	136.25	1a
S552	0.00	45.72	7
S552	45.72	55.38	5b
S552	55.38	89.70	5a
S552	89.70	92.14	5b
S552	92.14	124.91	5a
S552	124.91	125.18	5b
S552	125.18	136.25	5a
S552	136.25	137.46	5b
S552	137.46	146.09	5a
S552	146.09	146.91	5b
S552	146.91	157.58	5a
S552	157.58	157.89	5b
S552	157.89	165.81	5a
S552	165.81	166.54	2
S552	166.54	168.86	1a
S553	0.00	10.67	7
S553	10.67	16.15	5b
S553	16.15	44.81	5a
S553	44.81	51.21	5b
S553	51.21	67.67	5a
S553	67.67	68.12	5c
S553	68.12	77.27	5a
S553	77.27	77.42	5c
S553	77.42	81.38	5a
S553	81.38	84.06	5b
S553	84.06	84.37	4a
S553	84.37	87.08	2
S553	87.08	87.78	1a
S554	0.00	12.19	7
S554	12.19	14.63	5b
S554	14.63	43.59	5a
S554	43.59	43.89	5b
S554	43.89	45.26	5a
S554	45.26	50.44	5b
S554	50.44	67.51	5a
S554	67.51	67.91	5c
S554	67.91	91.74	5a
S554	91.74	94.60	5b
S554	94.60	95.04	4a
S554	95.04	96.77	2
S554	96.77	99.97	1a
S555	0.00	50.60	7
S555	50.60	90.53	5b
S555	90.53	102.20	6b
S555	102.20	103.94	4a
S556	0.00	39.01	7
S556	39.01	39.79	4a
S556	39.79	40.44	4e
S556	40.44	56.40	4a
S556	56.40	58.23	4b
S556	58.23	61.89	4e
S556	61.89	81.25	4a
S556	81.25	83.23	2
S556	83.23	87.48	1a
S557	0.00	56.69	7
S557	56.69	57.00	5
S557	57.00	75.59	6a
S557	75.59	77.00	4c
S557	77.02	87.33	4a
S557	87.33	90.71	2
S557	90.71	94.49	1a
S558	0.00	27.43	7
S558	27.43	37.73	5b
S558	37.73	41.61	6a
S558	41.61	45.26	4b
S558	45.26	55.72	4a
S558	55.72	60.53	2
S558	60.53	63.09	1a
S559	0.00	29.26	7
S559	29.26	37.80	5b
S559	37.80	41.76	5a
S559	41.76	50.29	5b
S559	50.29	57.00	5d
S559	57.00	57.45	4b
S559	57.45	59.44	5d
S559	59.44	59.80	4a
S559	59.80	68.12	5d
S559	68.12	68.70	4b
S559	68.70	72.24	5d
S559	72.24	75.29	4b
S559	75.29	78.24	5d
S559	78.24	79.25	4a
S559	79.25	81.38	1a
S560	0.00	15.54	7
S560	15.54	23.47	5b
S560	23.47	46.63	6a
S560	46.63	47.85	4b
S560	47.85	48.74	4a
S560	48.74	51.39	4b
S560	51.39	52.73	2
S560	52.73	56.39	1a
S561	0.00	27.58	7
S561	27.58	33.22	5b
S561	33.22	38.71	5d
S561	38.71	43.28	5b
S561	43.28	65.11	5a
S561	65.11	67.36	4a
S561	67.36	70.71	1a
S562	0.00	14.94	7
S562	14.94	35.05	4a
S562	35.05	36.82	2
S562	36.82	39.93	1a
S563	0.00	14.33	7
S563	14.33	27.68	4a
S563	27.68	31.18	2
S563	31.18	33.83	1a
S564	0.00	14.02	7
S564	14.02	28.65	4a
S564	28.65	30.48	1a
S565	0.00	35.67	7
S565	35.67	35.98	4b
S565	35.98	36.13	4c
S565	36.13	39.33	4b
S565	39.33	39.48	4c
S565	39.48	41.31	4a
S565	41.31	41.46	4c
S565	41.46	41.92	4a
S565	41.92	46.50	4a
S565	46.50	50.60	4d
S566	0.00	23.47	7
S566	23.47	50.54	4a

S566	50.54	51.02	2
S566	51.02	53.34	1a
S567	0.00	17.68	7
S567	17.68	52.43	4a
S567	52.43	56.69	2
S567	56.69	59.74	1a
S568	0.00	37.19	7
S568	37.19	41.91	5b
S568	41.91	60.96	5d
S568	60.96	65.84	5b
S568	65.84	67.06	5d
S568	67.06	67.67	5b
S568	67.67	68.88	6b
S568	68.88	72.30	4a
S568	72.30	74.07	1a
S569	0.00	18.29	7
S569	18.29	21.79	4a
S569	21.79	26.52	4e
S569	26.52	28.65	4a
S569	28.65	29.57	4e
S569	29.57	29.78	2
S569	29.78	35.05	1a
S570	0.00	14.02	7
S570	14.02	26.91	4a
S570	26.91	29.26	1a
S571	0.00	8.53	7
S571	8.53	11.58	5b
S571	11.58	62.79	5a
S571	62.79	63.61	4a
S571	63.61	65.84	1a
S572	0.00	4.57	7
S572	4.57	8.23	1a
S573	0.00	6.10	7
S573	6.10	55.93	5a
S573	55.93	62.79	5b
S573	62.79	111.62	5a
S573	111.62	114.76	4a
S573	114.76	118.26	1a
S574	0.00	21.95	7
S574	21.95	24.08	5b
S574	24.08	196.81	5a
S574	196.81	197.51	4a
S574	197.51	199.64	1a
S575	0.00	17.68	7
S575	17.68	18.29	5b
S575	18.29	194.77	5a
S575	194.77	196.81	5b
S575	196.81	197.82	4a
S575	197.82	200.56	1a
S576	0.00	7.92	7
S576	7.92	13.72	5b
S576	13.72	27.95	5a
S576	27.95	28.96	5b
S576	28.96	152.74	5a
S576	152.74	153.01	4a
S576	153.01	153.71	2
S576	153.71	154.84	1a
S577	0.00	12.80	7
S577	12.80	17.07	5b
S577	17.07	123.93	5a
S577	123.93	124.27	5c
S577	124.27	168.77	5a
S577	168.77	168.86	5b
S577	168.86	169.19	4a
S577	169.19	169.62	2
S577	169.62	173.13	1a
S578	0.00	13.72	7
S578	13.72	20.42	5a
S578	20.42	22.25	5b
S578	22.25	53.80	5a
S578	53.80	54.25	5c
S578	54.25	72.76	5a
S578	72.76	73.33	5c
S578	73.33	91.29	5a
S578	91.29	91.90	4a
S578	91.90	93.39	2
S578	93.39	94.79	1a
S579	0.00	15.50	7
S579	15.50	21.55	5b
S579	21.55	24.69	5a
S579	24.69	25.91	5b
S579	25.91	29.57	5a
S579	29.57	39.01	5b
S579	39.01	42.88	5d
S579	42.88	43.19	4b
S579	43.19	44.56	4a
S579	44.56	47.46	2
S579	47.46	48.77	1a
S580	0.00	17.98	7
S580	17.98	44.07	4a
S580	44.07	44.59	4b
S580	44.59	49.07	4a
S580	49.07	51.05	2
S580	51.05	53.34	1a
S581	0.00	41.15	7
S581	41.15	41.61	4b
S581	41.61	57.06	4a
S581	57.06	57.36	2
S581	57.36	57.61	1a
S590	0.00	35.97	7
S590	35.97	54.56	5b
S590	54.56	66.14	5d
S590	66.14	69.19	5c
S590	69.19	78.49	5a
S590	78.49	79.86	5b
S590	79.86	90.77	5a
S590	90.77	109.42	5b
S590	109.42	110.34	5a
S590	110.34	111.25	6a
S590	111.25	112.59	4a
S590	112.59	116.13	1a
S591	0.00	19.20	7
S591	19.20	21.18	4a
S591	21.18	22.10	4e
S591	22.10	23.62	4a
S591	23.62	24.69	4e
S591	24.69	29.57	4a
S591	29.57	35.66	2
S591	35.66	38.71	1a
S592	0.00	29.26	7
S592	29.26	29.72	4b
S592	29.72	32.46	4e
S592	32.46	36.18	4b
S592	36.18	42.67	2
S592	42.67	46.63	1a
S593	0.00	7.92	7
S593	7.92	12.80	4a
S593	12.80	16.15	2
S593	16.15	20.42	1a
S594	0.00	6.71	7
S594	6.71	14.33	4a
S594	14.33	15.85	2
S594	15.85	17.37	1a
S595	0.00	17.68	7
S595	17.68	37.67	4a
S595	37.67	38.95	2
S595	38.95	41.76	1a
S596	0.00	41.45	7
S596	41.45	57.61	5a
S596	57.61	59.74	5d
S596	59.74	61.87	4a
S596	61.87	65.84	2
S597	0.00	36.73	7
S597	36.73	75.53	5a
S597	75.53	76.50	4a
S597	76.50	78.94	2
S598	0.00	38.40	7
S598	38.40	80.77	5a
S598	80.77	81.99	4a
S598	81.99	83.52	2
S598	83.52	85.95	1a
S599	0.00	38.10	7
S599	38.10	41.45	1a
S607	0.00	17.98	7
S607	17.98	53.86	4a
S607	53.86	60.81	2
S607	60.81	64.92	1a
S608	0.00	46.63	7
S608	46.63	61.11	4a
S608	61.11	66.69	2
S608	66.69	69.49	1a
S609	0.00	27.13	7
S609	27.13	30.48	5a
S609	30.48	36.58	5d
S609	36.58	58.52	5b
S609	58.52	76.05	6a
S609	76.05	87.42	4a
S609	87.42	88.24	4b
S609	88.24	88.97	4a
S609	88.97	91.44	2
S610	0.00	45.42	7
S610	45.42	48.77	5b
S610	48.77	61.26	6a
S610	61.26	75.59	4a
S610	75.59	76.20	2
S611	0.00	47.24	7
S611	47.24	67.06	6a
S611	67.06	67.67	2
S611	67.67	69.19	1a
S612	0.00	21.34	7
S612	21.34	39.93	4a
S612	39.93	40.14	2
S612	40.14	44.81	1a
S613	0.00	26.21	7
S613	26.21	40.84	5b
S613	40.84	44.50	5a
S613	44.50	46.02	5d
S613	46.02	46.94	5a
S613	46.94	47.85	5d
S613	47.85	49.99	5a
S613	49.99	53.64	5b
S613	53.64	70.87	5a
S613	70.87	73.00	4a
S613	73.00	76.50	2
S613	76.50	78.03	1a
S614	0.00	25.00	7
S614	25.00	29.56	5b
S614	29.56	30.20	5d
S614	30.20	61.72	5b
S614	61.72	84.43	5a
S614	84.43	85.90	5c
S614	85.90	92.05	5b
S614	92.05	94.34	4a
S614	94.34	94.54	2
S614	94.54	94.94	4a
S614	94.94	95.16	2
S614	95.16	96.92	1a
S615	0.00	38.10	7
S615	38.10	42.67	5b
S615	42.67	43.59	5d
S615	43.59	48.16	5a
S615	48.16	50.00	5d
S615	50.00	80.00	5a
S615	80.00	82.60	4a
S615	82.60	82.90	1a
S616	0.00	21.43	7
S616	21.43	26.06	5b
S616	26.06	26.52	5d
S616	26.52	35.00	5b
S616	35.00	35.66	5d
S616	35.66	35.90	5b
S616	35.90	38.10	5d
S616	38.10	55.78	5b
S616	55.78	89.79	5a
S616	89.79	90.70	5b
S616	90.70	92.72	4a
S616	92.72	94.48	1a
S617	0.00	35.66	7
S617	35.66	41.45	5b
S617	41.45	43.83	5d
S617	43.83	46.33	5b
S617	46.33	52.73	5a
S617	52.73	55.47	5b
S617	55.47	81.77	5a
S617	81.77	83.15	5b
S617	83.15	84.67	4a
S617	84.67	85.04	2
S617	85.04	87.48	1a
S618	0.00	30.48	7
S618	30.48	54.49	5b
S618	54.49	57.79	5a
S618	57.79	63.89	4a
S618	63.89	65.83	1a
S619	0.00	24.69	7
S619	24.69	25.14	5c
S619	25.14	48.37	5b
S619	48.37	72.23	5a
S619	72.23	77.72	5b
S619	77.72	79.40	5a
S619	79.40	80.80	5b
S619	80.80	82.81	4a
S619	82.81	83.55	2
S619	83.55	85.64	1a
S620	0.00	18.75	7
S620	18.75	33.28	5a
S620	33.28	38.74	5b
S620	38.74	70.59	5a
S620	70.59	72.60	4a
S620	72.60	73.76	2
S620	73.76	74.00	1a
S621	0.00	39.93	7
S621	39.93	70.43	5b
S621	70.43	72.87	5c
S621	72.87	76.80	5b
S621	76.80	79.55	5a
S621	79.55	89.31	5b
S621	89.31	90.37	5d
S621	90.37	96.12	5c
S621	96.12	104.24	5b
S621	104.24	133.95	5a
S621	133.95	156.06	5b
S621	156.06	157.28	4a
S621	157.28	158.34	2
S621	158.34	160.02	4a
S621	160.02	160.36	2
S621	160.36	161.54	1a
S622	0.00	40.08	7
S622	40.08	65.07	5b
S622	65.07	65.99	5d
S622	65.99	81.23	5b
S622	81.23	84.58	5d
S622	84.58	91.89	5a
S622	91.89	99.97	5b
S622	99.97	100.88	5c
S622	100.88	102.72	5d
S622	102.72	142.34	5a
S622	142.34	148.44	4a
S622	148.44	149.66	2
S622	149.66	150.26	1a
S623	0.00	27.98	7
S623	27.98	50.23	5b
S623	50.23	78.33	5a
S624	0.00	30.78	7
S624	30.78	46.93	5b
S624	46.93	51.20	5a
S624	51.20	51.51	5b
S624	51.51	71.38	5a
S624	71.38	72.90	4a
S624	72.90	74.12	2
S624	74.12	78.02	1a
S625	0.00	26.21	7
S625	26.21	32.91	5c
S625	32.91	35.66	5d
S625	35.66	39.01	5b
S625	39.01	78.33	5d
S625	78.33	78.63	5c
S625	78.63	80.46	5b
S625	80.46	80.77	5c
S625	80.77	82.60	5b
S625	82.60	86.41	5c
S625	86.41	89.30	5b
S625	89.30	93.11	5a
S625	93.11	100.98	5b
S625	100.98	101.49	4a
S625	101.49	103.02	4a
S625	103.02	107.59	1a
S626	0.00	21.38	7
S626	21.38	47.32	5b
S626	47.32	49.09	5a
S626	49.09	69.23	5b
S626	69.23	83.14	5a
S626	83.14	84.78	5c
S626	84.78	115.56	5a
S626	115.56	117.03	5b

S626	117.03	120.41	4a
S626	120.41	121.36	2
S626	121.36	122.90	1a
S627	0.00	15.54	7
S627	15.54	44.07	5b
S627	44.07	44.95	5a
S627	44.95	56.99	5b
S627	56.99	73.45	5a
S627	73.45	78.18	5b
S627	78.18	79.85	5a
S627	79.85	82.02	5b
S627	82.02	84.06	4a
S627	84.06	87.47	1a
S628	0.00	25.95	7
S628	25.95	95.14	5b
S628	95.14	96.67	5c
S628	96.67	104.13	5b
S628	104.13	107.64	5c
S628	107.64	108.01	5b
S628	108.01	114.80	4a
S628	114.80	116.33	4c
S628	116.33	117.09	4a
S628	117.09	119.53	2
S628	119.53	121.61	1a
S629	0.00	31.08	7
S629	31.08	41.75	5b
S629	41.75	63.09	5a
S629	63.09	82.08	5b
S629	82.08	87.99	5c
S629	87.99	109.60	5b
S629	109.60	111.86	5d
S629	111.86	118.32	5b
S629	118.32	124.81	5c
S629	124.81	135.57	5b
S629	135.57	136.97	4a
S629	136.97	138.10	2
S629	138.10	139.29	1a
S630	0.00	37.79	7
S630	37.79	67.28	4a
S630	67.28	72.22	1a
S631	0.00	36.27	7
S631	36.27	64.66	4a
S631	64.66	65.27	2
S631	65.27	66.75	1a
S632	0.00	35.35	7
S632	35.35	68.45	4a
S632	68.45	72.24	1a
S633	0.00	36.71	7
S633	36.71	65.67	4a
S633	65.67	66.13	1a
S634	0.00	70.41	7
S634	70.41	78.72	4a
S634	78.72	80.48	1a
S635	0.00	88.66	7
S635	88.66	95.72	4a
S635	95.72	100.85	2
S635	100.85	102.07	1a
S636	0.00	32.18	7
S636	32.18	102.06	5a
S636	102.06	139.16	5b
S636	139.16	139.49	4c
S636	139.49	144.89	4a
S636	144.89	148.44	1a
S637	0.00	33.83	7
S637	33.83	38.71	5c
S637	38.71	39.47	5b
S637	39.47	47.59	5c
S637	47.59	92.05	6a
S637	92.05	94.18	4b
S637	94.18	112.93	4e
S637	112.93	117.26	1a
S638	0.00	46.65	7
S638	46.65	47.56	5c
S638	47.56	86.27	6a
S638	86.27	87.80	4a
S638	87.80	90.24	2
S638	90.24	91.59	1a
S639	0.00	25.29	7
S639	25.29	39.62	5a
S639	39.62	50.29	5b
S639	50.29	52.57	5a
S639	52.57	55.93	5b
S639	55.93	70.71	5a
S639	70.71	92.80	5d
S639	92.80	103.02	5a
S639	103.02	103.72	6a
S639	103.72	105.98	4a
S639	105.98	106.53	2
S639	106.53	107.31	1a
S640	0.00	32.89	7
S640	32.89	50.57	5b
S640	50.57	73.89	5a
S640	73.89	77.70	5b
S640	77.70	79.22	5c
S640	79.22	82.58	5b
S640	82.58	89.59	5a
S640	89.59	89.98	5b
S640	89.98	91.42	4a
S640	91.42	92.63	2
S640	92.63	93.86	1a
S641	0.00	39.21	7
S641	39.21	62.83	5b
S641	62.83	111.70	5a
S641	111.70	112.52	4a
S641	112.52	114.30	1a
S642	0.00	31.37	7
S642	31.37	41.40	4a
S642	41.40	43.04	2
S642	43.04	50.88	1a
S643	0.00	35.08	7
S643	35.08	54.43	5b
S643	54.43	77.42	5a
S644	0.00	31.54	7
S644	31.54	40.87	4a
S644	40.87	43.31	2
S644	43.31	44.80	1a
S645	0.00	32.61	7
S645	32.61	35.50	4a
S645	35.50	39.39	1a
S646	0.00	33.97	7
S646	33.97	42.06	4a
S646	42.06	45.72	1a
S647	0.00	27.48	7
S647	27.48	64.66	4a
S647	64.66	71.06	2
S647	71.06	71.93	1a
S648	0.00	28.02	7
S648	28.02	70.99	4a
S648	70.99	76.48	2
S648	76.48	78.33	1a
S649	0.00	27.74	7
S649	27.74	63.97	4a
S649	63.97	70.74	2
S649	70.74	73.45	1a
S650	0.00	25.76	7
S650	25.76	51.34	4a
S650	51.34	54.84	2
S651	0.00	27.98	7
S651	27.98	62.06	4a
S651	62.06	68.72	1a
S652	0.00	31.09	7
S652	31.09	44.84	4b
S652	44.84	78.06	4a
S652	78.06	82.94	2
S652	82.94	87.47	1a
S653	0.00	28.19	7
S653	28.19	70.44	4a
S653	70.44	76.39	2
S653	76.39	81.22	1a
S654	0.00	25.42	7
S654	25.42	57.97	4a
S654	57.97	59.49	2
S655	0.00	47.86	7
S655	47.86	49.99	5c
S655	49.99	66.15	5b
S655	66.15	75.29	6a
S655	75.29	76.81	4a
S655	76.81	80.47	2
S655	80.47	85.34	1a
S656	0.00	31.66	7
S656	31.66	60.01	5a
S656	60.01	62.45	5d
S656	62.45	72.21	5b
S656	72.21	84.40	5a
S656	84.40	87.45	5d
S656	87.45	103.60	5a
S656	103.60	105.74	5d
S656	105.74	107.90	6a
S656	107.90	121.07	5b
S656	121.07	123.47	4a
S656	123.47	127.10	1a
S657	0.00	38.53	7
S657	38.53	44.78	5c
S657	44.78	65.20	5b
S657	65.20	81.35	5a
S657	81.35	86.84	5c
S657	86.84	96.59	5a
S657	96.59	105.35	5d
S657	105.35	105.58	5b
S657	105.58	108.78	4a
S658	0.00	31.81	7
S658	31.81	35.32	4a
S658	35.32	38.55	1a
S659	0.00	33.79	7
S659	33.79	38.66	5b
S659	38.66	66.40	5a
S659	66.40	68.08	5c
S659	68.08	87.43	5a
S659	87.43	87.89	5b
S659	87.89	92.64	5c
S659	92.64	131.87	5a
S659	131.87	137.72	4a
S659	137.72	137.95	1a
S660	0.00	34.74	7
S660	34.74	68.57	5a
S660	68.57	75.28	5d
S660	75.28	76.49	5b
S660	76.49	93.10	5a
S660	93.10	97.83	5c
S660	97.83	130.44	5a
S660	130.44	134.86	6a
S660	134.86	140.44	4a
S660	140.44	140.94	1a
S661	0.00	41.12	7
S661	41.12	86.84	5a
S661	86.84	90.81	5c
S661	90.81	119.70	5a
S661	119.70	120.83	5c
S661	120.83	123.36	5a
S661	123.36	125.92	4a
S661	125.92	126.22	1a
S662	0.00	44.49	7
S662	44.49	49.36	5b
S662	49.36	64.30	5a
S662	64.30	65.82	5b
S662	65.82	86.03	5a
S662	86.03	91.43	5c
S662	91.43	118.55	5a
S662	118.55	123.43	4a
S662	123.43	125.74	4b
S662	125.74	126.32	4a
S662	126.32	136.04	1a
S663	0.00	36.53	7
S663	36.53	54.06	4a
S663	54.06	58.17	1a
S664	0.00	34.44	7
S664	34.44	57.62	4a
S664	57.62	59.29	2
S664	59.29	61.20	1a
S665	0.00	44.84	7
S665	44.84	63.36	5b
S666	0.00	41.42	7
S666	41.42	63.06	5b
S666	63.06	93.42	5a
S666	93.42	95.98	4a
S666	95.98	97.26	4b
S666	97.26	99.67	1a
S667	0.00	35.70	7
S667	35.70	41.49	5b
S667	41.49	70.14	5a
S667	70.14	72.28	4a
S667	72.28	75.02	2
S667	75.02	77.42	1a
S668	0.00	36.86	7
S668	36.86	68.71	4a
S668	68.71	70.38	2
S668	70.38	72.21	1a
S669	0.00	36.99	7
S669	36.99	66.71	4a
S669	66.71	69.14	1a
S670	0.00	35.97	7
S670	35.97	73.81	4a
S670	73.81	78.38	2
S670	78.38	81.38	1a
S671	0.00	36.73	7
S671	36.73	56.36	4a
S671	56.36	65.22	2
S672	0.00	32.29	7
S672	32.29	44.03	4a
S672	44.03	47.08	2
S672	47.08	49.07	1a
S673	0.00	64.01	7
S673	64.01	86.88	4a
S673	86.88	92.65	1a
S674	0.00	28.34	7
S674	28.34	58.82	4a
S674	58.82	61.56	1a
S675	0.00	30.48	7
S675	30.48	53.79	4a
S675	53.79	55.19	2
S675	55.19	57.91	1a
S676	0.00	37.80	7
S676	37.80	73.78	4a
S676	73.78	80.48	2
S676	80.48	81.38	1a
S677	0.00	75.25	7
S677	75.25	95.82	4a
S677	95.82	99.64	1a
S677A	0.00	1.00	
S678	0.00	32.31	7
S678	32.31	46.33	4a
S678	46.33	48.77	1a
S679	0.00	26.37	7
S679	26.37	39.05	4a
S679	39.05	42.06	1a
S680	0.00	1.00	
S681	0.00	43.89	7
S681	43.89	68.88	4b
S681	68.88	71.20	4a
S681	71.20	73.15	1
S682	0.00	1.00	
S683	0.00	49.00	7
S683	49.00	49.20	5b
S683	49.20	54.46	5a
S683	54.46	62.70	5d
S683	62.70	78.20	5a
S683	78.20	80.95	5c
S683	80.95	81.70	5b
S683	81.70	81.77	5c
S683	81.77	85.40	5b
S683	85.40	89.20	5c
S683	89.20	94.45	5a
S683	94.45	95.56	5b
S683	95.56	98.30	5c
S683	98.30	100.00	5b
S683	100.00	105.40	5a
S683	105.40	107.10	5c
S683	107.10	109.42	5b
S683	109.42	114.90	5a
S683	114.90	117.00	5b
S683	117.00	124.00	4a
S683	124.00	129.20	1a
S684	0.00	26.21	7
S684	26.21	38.76	4a
S684	38.76	40.28	2
S684	40.28	41.76	1a
S685	0.00	29.01	7
S685	29.01	36.32	5b
S685	36.32	51.56	5a
S685	51.56	52.78	5c
S685	52.78	56.43	5a
S685	56.43	58.26	5c
S685	58.26	60.55	5a
S685	60.55	66.04	5c

S685	66.04	68.12	2
S685	68.12	70.10	1a
S686	0.00	64.10	7
S686	64.10	70.41	5a
S686	70.41	71.63	5c
S686	71.63	74.68	5b
S686	74.68	78.64	4c
S686	78.64	80.62	4a
S686	80.62	84.43	1a
S687	0.00	22.56	7
S687	22.56	43.16	4a
S687	43.16	46.33	1a
S688	0.00	27.48	7
S688	27.48	68.93	5b
S688	68.93	77.47	5a
S688	77.47	96.98	5b
S688	96.98	99.48	5a
S688	99.48	104.78	4a
S688	104.78	105.21	2
S688	105.21	107.65	1a
S689	0.00	27.48	7
S689	27.48	32.97	5b
S689	32.97	48.82	5d
S689	48.82	62.84	5a
S689	62.84	70.46	5b
S689	70.46	72.29	5a
S689	72.29	74.12	5c
S689	74.12	77.23	5a
S689	77.23	79.72	4a
S689	79.72	83.67	1a
S690	0.00	42.95	7
S690	42.95	76.47	4a
S690	76.47	82.21	2
S690	82.21	84.70	1a
S691	0.00	71.76	7
S691	71.76	87.76	4a
S691	87.76	96.29	2
S691	96.29	98.43	1a
S692	0.00	67.62	7
S692	67.62	70.36	5b
S692	70.36	70.67	5d
S692	70.67	76.46	5b
S692	76.46	76.76	5d
S692	76.76	78.29	5b
S692	78.29	101.76	6a
S692	101.76	114.35	4a
S692	114.35	114.47	4c
S692	114.47	117.11	1a
S693	0.00	33.48	7
S693	33.48	64.58	4a
S693	64.58	76.16	1a
S694	0.00	36.57	7
S694	36.57	72.85	4a
S694	72.85	82.30	2
S694	82.30	85.34	1a
S695	0.00	41.71	7
S695	41.71	76.77	4a
S695	76.77	77.99	2
S695	77.99	82.86	1a
S696	0.00	41.75	7
S696	41.75	42.36	4a
S696	42.36	55.77	6a
S696	55.77	56.23	4a
S696	56.23	57.30	4c
S696	57.30	59.43	4a
S696	59.43	59.89	4c
S696	59.89	60.35	4a
S696	60.35	74.37	4c
S696	74.37	86.25	4a
S696	86.25	87.78	2
S696	87.78	91.74	1a
S697	0.00	39.62	7
S697	39.62	76.80	4a
S697	76.80	80.46	2
S697	80.46	81.38	1a
S698	0.00	83.51	7
S698	83.51	84.73	4a
S698	84.73	85.95	4c
S698	85.95	89.61	4a
S698	89.61	96.92	1a
S699	0.00	61.26	7
S699	61.26	72.23	4b
S699	72.23	87.47	4a
S699	87.47	92.04	2
S699	92.04	94.79	1a
S700	0.00	61.56	7
S700	61.56	79.85	4a
S700	79.85	88.39	2
S700	88.39	89.61	1a
S701	0.00	60.65	7
S701	60.65	79.85	4a
S701	79.85	80.77	2
S701	80.77	84.12	1a
S702	0.00	35.66	7
S702	35.66	75.59	4a
S702	75.59	77.42	1a
S703	0.00	52.12	7
S703	52.12	56.38	5b
S703	56.38	65.83	6a
S703	65.83	89.00	4a
S703	89.00	92.96	2
S703	92.96	94.18	1a
S704	0.00	71.62	7
S704	71.62	78.48	4a
S704	78.48	83.51	4c
S704	83.51	90.83	4a
S704	90.83	98.14	2
S704	98.14	98.75	1a
S705	0.00	30.48	7
S705	30.48	47.55	5b
S705	47.55	47.70	4c
S705	47.70	55.16	4a
S705	55.16	55.60	2
S705	55.60	60.35	1a
S706	0.00	27.43	7
S706	27.43	31.09	4a
S706	31.09	32.61	1a
S707	0.00	1.00	
S708	0.00	24.69	7
S708	24.69	25.75	5c
S708	25.75	53.03	5a
S708	53.03	64.61	4a
S708	64.61	69.19	2
S708	69.19	73.15	1a
S709	0.00	24.38	7
S709	24.38	97.84	5a
S709	97.84	99.67	5b
S709	99.67	99.82	5c
S709	99.82	99.97	5b
S709	99.97	101.19	4a
S709	101.19	103.63	1a
S710	0.00	19.51	7
S710	19.51	80.16	5a
S710	80.16	97.84	5a
S710	97.84	132.13	5a
S710	132.13	132.59	4a
S710	132.59	135.94	1a
S711	0.00	21.34	7
S711	21.34	175.56	5a
S711	175.56	176.78	5b
S711	176.78	176.81	4a
S711	176.81	181.66	1a
S712	0.00	46.94	7
S712	46.94	47.70	5c
S712	47.70	71.93	5a
S712	71.93	79.25	5b
S712	79.25	79.86	4c
S712	79.86	82.30	4a
S712	82.30	83.82	2
S712	83.82	87.17	1a
S713	0.00	15.85	7
S713	15.85	46.18	5b
S713	46.18	135.64	5a
S713	135.64	137.22	5b
S713	137.22	141.12	4a
S713	141.12	146.06	2
S713	146.06	151.18	1a
S714	0.00	18.29	7
S714	18.29	32.32	5b
S714	32.32	35.36	5d
S714	35.36	57.93	5b
S714	57.93	80.68	5a
S714	80.68	81.14	4c
S714	81.14	86.67	4d
S714	86.67	88.13	2
S714	88.13	93.27	1a
S715	0.00	25.60	7
S715	25.60	32.92	5b
S715	32.92	103.02	5a
S715	103.02	104.24	4c
S715	104.24	104.85	4a
S715	104.85	105.46	4c
S715	105.46	107.29	4a
S715	107.29	108.20	2
S715	108.20	112.78	1a
S716	0.00	28.96	7
S716	28.96	53.95	5b
S716	53.95	81.38	5a
S716	81.38	84.43	4a
S716	84.43	87.17	2
S716	87.17	89.12	1a
S717	0.00	1.00	
S718	0.00	40.87	7
S718	40.87	98.63	5b
S718	98.63	102.63	4a
S718	102.63	105.67	2
S718	105.67	108.50	1a
S720	0.00	30.48	7
S720	30.48	51.82	5b
S720	51.82	74.49	5a
S720	74.49	77.57	4a
S720	77.57	79.16	2
S720	79.16	81.87	1a
S723	0.00	62.79	7
S723	62.79	74.98	5b
S723	74.98	90.22	5d
S723	90.22	93.27	4a
S723	93.27	97.13	4c
S723	97.13	100.88	4a
S723	100.88	102.41	1a
S724	0.00	75.60	7
S724	75.60	78.03	5b
S724	78.03	100.13	6a
S724	100.13	100.89	4a
S724	100.89	102.41	4b
S724	102.41	106.98	4a
S724	106.98	110.39	4b
S724	110.39	111.25	2
S725	0.00	75.59	7
S725	75.59	92.66	4a
S725	92.66	103.63	2
S725	103.63	105.77	1a
S726	0.00	77.72	7
S726	77.72	101.50	4a
S726	101.50	103.63	2
S726	103.63	111.25	1a
S727	0.00	70.10	7
S727	70.10	89.61	5a
S727	89.61	105.46	5d
S727	105.46	105.61	4c
S727	105.61	111.71	4a
S727	111.71	114.60	2
S727	114.60	116.43	1a
S728	0.00	62.81	7
S728	62.81	87.14	5b
S728	87.14	100.50	6a
S728	100.50	101.90	4c
S728	101.90	104.90	4a
S728	104.90	108.53	1a
S729	0.00	41.46	7
S729	41.46	76.76	4a
S729	76.76	81.89	2
S729	81.89	84.14	1a
S730	0.00	62.80	7
S730	62.80	70.11	5b
S730	70.11	84.14	6a
S730	84.14	87.19	4a
S730	87.19	87.59	4c
S730	87.59	97.99	4a
S730	97.99	102.00	2
S730	102.00	103.65	1a
S731	0.00	56.00	7
S731	56.00	65.85	5b
S731	65.85	79.70	4a
S731	79.70	80.40	4c
S731	80.40	91.14	4a
S731	91.14	92.58	2
S731	92.58	96.23	1a
S732	0.00	55.50	7
S732	55.50	56.71	5b
S732	56.71	59.76	5d
S732	59.76	65.85	5a
S732	65.85	67.85	5b
S732	67.85	76.82	5d
S732	76.82	84.34	5a
S732	84.34	93.74	6a
S732	93.74	97.60	4a
S732	97.60	99.39	1a
S733	0.00	34.91	7
S733	34.91	76.20	4a
S733	76.20	76.70	2
S733	76.70	78.04	1a
S734	0.00	49.90	7
S734	49.90	51.70	5b
S734	51.70	105.48	5a
S734	105.48	117.68	5d
S734	117.68	142.40	5a
S734	142.40	145.30	4a
S734	145.30	146.00	4b
S734	146.00	149.50	4a
S734	149.50	151.83	2
S735	0.00	68.10	7
S735	68.10	99.90	5a
S735	99.90	113.18	5b
S735	113.18	117.68	6a
S735	117.68	128.20	4a
S735	128.20	128.48	2
S736	0.00	68.50	7
S736	68.50	70.00	5b
S736	70.00	76.30	5a
S736	76.30	93.29	6a
S736	93.29	103.03	4a
S736	103.03	104.87	1a
S737	0.00	64.24	7
S737	64.24	84.04	4a
S737	84.04	86.89	1a
S738	0.00	56.73	7
S738	56.73	84.14	5a
S738	84.14	91.00	5b
S738	91.00	102.11	5a
S738	102.11	108.53	6a
S738	108.53	112.38	4b
S738	112.38	114.02	2
S739	0.00	84.16	7
S739	84.16	93.68	4a
S739	93.68	95.42	1a
S740	0.00	68.39	7
S740	68.39	74.99	5b
S740	74.99	86.80	5a
S740	86.80	87.20	5b
S740	87.20	105.49	5a
S740	105.49	114.64	6a
S740	114.64	117.69	4a
S740	117.69	118.29	4c
S740	118.29	122.00	4a
S740	122.00	122.60	2
S740	122.60	123.79	1a
S801	0.00	6.34	7
S801	6.34	27.12	4a
S801	27.12	35.98	1a
S802	0.00	6.35	7
S802	6.35	25.30	4a
S802	25.30	28.96	2
S803	0.00	4.43	7
S803	4.43	13.09	4a
S803	13.09	15.63	2
S803	15.63	16.46	1a
S804	0.00	6.75	7
S804	6.75	38.80	4a
S804	38.80	40.20	2
S804	40.20	45.12	1a
S805	0.00	6.10	7
S805	6.10	37.15	4a
S805	37.15	37.30	2

S805	37.30	38.41	1a
S806	0.00	5.30	7
S806	5.30	19.05	4a
S806	19.05	19.45	2
S806	19.45	19.82	1a
S807	0.00	18.30	7
S807	18.30	31.85	4a
S807	31.85	34.65	2
S807	34.65	35.98	1a
S808	0.00	15.50	7
S808	15.50	31.58	4a
S808	31.58	33.35	2
S808	33.35	35.98	1a
S809	0.00	16.10	7
S809	16.10	32.93	4a
S811	0.00	5.65	7
S811	5.65	15.70	4a
S811	15.70	16.46	2
S811	16.46	19.51	1a
S812	0.00	6.10	7
S812	6.10	25.75	4a
S812	25.75	27.55	2
S812	27.55	29.88	1a
S813	0.00	6.40	7
S813	6.40	21.40	4a
S813	21.40	22.25	2
S813	22.25	24.39	1a
S814	0.00	36.90	7
S814	36.90	47.56	5a
S814	47.56	63.11	6
S814	63.11	66.60	4b
S814	66.60	66.75	4c
S814	66.75	67.90	4a
S814	67.90	68.12	4c
S814	68.12	69.16	4d
S814	69.16	70.68	4a
S814	70.68	73.17	2
S814	73.17	75.61	1a
S815	0.00	63.26	7
S815	63.26	64.31	5a
S815	64.31	81.40	6
S815	81.40	81.72	4c
S815	81.72	89.00	4a
S815	89.00	89.80	2
S815	89.80	92.99	1a
S816	0.00	54.88	7
S816	54.88	78.66	5a
S816	78.66	90.55	6
S816	90.55	94.20	4b
S816	94.20	94.56	4c
S816	94.56	100.74	4a
S816	100.74	101.20	2
S816	101.20	105.18	1a
S817	0.00	51.83	7
S817	51.83	114.02	5
S817	114.02	115.54	5c
S817	115.54	116.00	5
S817	116.00	124.40	4a
S817	124.40	132.10	2
S817	132.10	132.93	1a
S818	0.00	56.69	7
S818	56.69	76.70	5a
S818	76.70	78.10	7
S818	78.10	84.73	5a
S818	84.73	102.20	6b
S818	102.20	102.82	4b
S818	102.82	108.45	4a
S818	108.45	110.75	2
S818	110.75	112.17	1a
S819	0.00	79.59	7
S819	79.59	84.66	6b
S819	84.66	85.34	4b
S819	85.34	86.85	4d
S819	86.85	87.10	4a
S819	87.10	87.96	4e
S819	87.96	88.70	4a
S819	88.70	93.27	2
S820	0.00	102.72	7
S820	102.72	103.63	4a
S820	103.63	104.70	4d
S820	104.70	105.65	4a
S820	105.65	110.90	2
S820	110.90	114.91	1a
S821	0.00	52.23	7
S821	52.23	73.46	5a
S821	73.46	84.12	5d
S821	84.12	103.02	5a
S821	103.02	104.30	5c
S821	104.30	110.00	5a
S821	110.00	110.85	5d
S821	110.85	110.90	5b
S821	110.90	111.25	4a
S821	111.25	113.60	4d
S821	113.60	114.00	4a
S821	114.00	117.75	2
S821	117.75	121.31	1a
S822	0.00	69.49	7
S822	69.49	70.71	6
S822	70.71	71.93	4b
S822	71.93	72.15	6a
S822	72.15	72.54	4d
S822	72.54	80.75	4a
S822	80.75	82.85	2
S822	82.85	83.21	1a
S823	0.00	95.10	7
S823	95.10	96.05	4a
S823	96.05	103.50	2
S823	103.50	106.07	1a
S824	0.00	69.60	7
S824	69.60	70.90	4a
S824	70.90	71.63	1a
S825	0.00	59.13	7
S825	59.13	71.32	5a
S825	71.32	90.43	6a
S825	90.43	91.15	4d
S825	91.15	93.74	4a
S825	93.74	94.50	4d
S825	94.50	98.20	2
S825	98.20	101.19	1a
S826	0.00	46.94	7
S826	46.94	71.32	5a
S826	71.32	89.61	6a
S826A	0.00	85.65	7
S826A	85.65	100.35	5a
S826A	100.35	101.57	5d
S826A	101.57	102.41	5a
S826A	102.41	103.94	6a
S826A	103.94	103.99	4c
S826A	103.99	104.35	4d
S826A	104.35	105.77	4a
S827	0.00	77.72	7
S827	77.72	99.67	5a
S827	99.67	110.95	6a
S827	110.95	111.10	4c
S827	111.10	113.05	4d
S827	113.05	113.90	4a
S827	113.90	115.90	2
S827	115.90	123.75	1a
S828	0.00	64.31	7
S828	64.31	73.15	5a
S828	73.15	78.03	5a
S828	78.03	101.88	6a
S828	101.88	102.35	4c
S828	102.35	102.60	4a
S828	102.60	102.88	4c
S828	102.88	105.46	4d
S828	105.46	106.05	4a
S828	106.05	106.75	4d
S828	106.75	112.78	2
S828	112.78	117.04	1a
S829	0.00	112.06	7
S829	112.06	112.42	4c
S829	112.42	113.09	4d
S830	0.00	83.95	7
S830	83.95	84.12	4b
S830	84.12	84.22	4c
S830	84.22	90.70	4a
S830	90.70	96.32	1a
S831	0.00	54.86	7
S831	54.86	96.10	5a
S831	96.10	121.77	6a
S831	121.77	123.45	4d
S831	123.45	126.02	4a
S831	126.02	129.84	2
S831	129.84	134.42	1a
S832	0.00	45.42	7
S832	45.42	96.01	5a
S832	96.01	103.02	5d
S832	103.02	106.07	5a
S832A	0.00	43.89	7
S832A	43.89	95.71	5a
S832A	95.71	103.33	5d
S832A	103.33	120.70	5a
S832A	120.70	121.62	5d
S832A	121.62	125.58	5a
S832A	125.58	130.50	6a
S832A	130.50	130.95	4b
S832A	130.95	131.66	4d
S832A	131.66	132.55	4a
S832A	132.55	132.70	2
S832A	132.70	134.11	1a
S833	0.00	44.20	7
S833	44.20	73.15	5a
S833	73.15	79.25	5d
S833	79.25	85.34	5a
S833	85.34	97.23	5d
S833	97.23	112.78	5a
S833	112.78	116.13	6a
S833	116.13	116.44	4b
S833	116.44	118.40	4a
S833	118.40	119.20	2
S833	119.20	122.53	1a
S834	0.00	65.53	7
S834	65.53	78.64	5a
S834	78.64	80.77	5d
S834	80.77	86.56	5a
S834	86.56	100.28	5d
S834	100.28	111.95	5a
S834	111.95	113.50	6a
S834	113.50	114.15	4b
S834	114.15	114.68	4d
S834	114.68	116.65	4a
S834	116.65	120.09	1a
S835	0.00	64.62	7
S835	64.62	70.41	5a
S835	70.41	93.27	6a
S835	93.27	93.40	4b
S835	93.40	94.58	4d
S835	94.58	97.00	4a
S835	97.00	97.65	4d
S835	97.65	98.95	4a
S835	98.95	100.05	4d
S835	100.05	103.00	2
S835	103.00	106.98	1a
S836	0.00	45.26	7
S836	45.26	67.51	5
S836	67.51	76.50	5d
S836	76.50	93.27	5
S836	93.27	97.84	5d
S836	97.84	100.70	5
S836	100.70	100.80	6
S836	100.80	100.97	4c
S836	100.97	101.67	4d
S836	101.67	103.50	2
S836	103.50	106.98	1a
S837	0.00	49.07	7
S837	49.07	52.43	5
S837	52.43	72.46	6
S837	72.46	72.90	4d
S837	72.90	73.95	4c
S837	73.95	74.00	4a
S837	74.00	74.20	4d
S837	74.20	77.83	4d
S837	77.83	81.25	4a
S837	81.25	81.60	4d
S837	81.60	82.75	4a
S837	82.75	90.22	2
S838	0.00	21.34	7
S838A	0.00	54.90	7
S838A	54.90	67.60	4a
S838A	67.60	71.25	4d
S838A	71.25	74.98	1a
S839	0.00	41.15	7
S839	41.15	56.69	5
S839	56.69	61.57	5d
S839	61.57	81.08	5
S839	81.08	82.40	6
S839	82.40	82.87	4c
S839	82.87	83.50	4d
S839	83.50	85.70	4a
S839	85.70	86.50	2
S839	86.50	89.61	1a
S840	0.00	33.53	7
S840	33.53	104.04	5
S840	104.04	104.60	5c
S840	104.60	105.89	5
S840	105.89	106.24	4d
S840	106.24	107.23	4a
S840	107.23	107.94	2
S840	107.94	118.26	1a
S841	0.00	24.38	7
S841	24.38	100.00	5
S841	100.00	101.90	4a
S841	101.90	102.25	2
S841	102.25	115.52	1a
S842	0.00	35.36	7
S842	35.36	60.66	5
S842	60.66	70.40	5d
S842	70.40	90.73	5
S842	90.73	91.02	4d
S842	91.02	92.12	4a
S842	92.12	93.00	2
S842	93.00	102.41	1a
S843	0.00	59.74	7
S843	59.74	74.98	5
S843	74.98	78.10	5d
S843	78.10	79.93	5
S843	79.93	80.30	4c
S843	80.30	80.52	4d
S843	80.52	83.85	4a
S843	83.85	84.20	2
S843	84.20	86.87	1a
S844	0.00	68.70	7
S844	68.70	71.93	4a
S844	71.93	73.70	4d
S844	73.70	77.90	4a
S844	77.90	81.08	1a
S845	0.00	62.79	7
S845	62.79	63.00	4d
S845	63.00	72.85	4a
S845	72.85	76.20	1a
S846	0.00	69.20	7
S846	69.20	78.03	4d
S846	78.03	80.45	4a
S846	80.45	84.00	2
S846	84.00	87.17	1a
S847	0.00	44.50	7
S847	44.50	50.60	5
S847	50.60	52.12	5d
S847	52.12	60.96	5
S847	60.96	70.41	5d
S847	70.41	84.00	5
S847	84.00	102.41	5d
S847	102.41	104.20	5
S847	104.20	106.00	4a
S847	106.00	107.92	2
S847	107.92	111.56	1a
S848	0.00	70.90	7
S848	70.90	86.60	5
S848	86.60	88.85	5c
S848	88.85	90.35	4a
S848	90.35	90.70	2
S848	90.70	96.32	1a
S849	0.00	65.15	7
S849	65.15	66.80	4b
S849	66.80	80.95	4a
S849	80.95	83.75	2
S849	83.75	86.56	1a
S850A	0.00	70.10	7
S850A	70.10	74.37	5
S850A	74.37	96.93	5d
S850A	96.93	121.30	5
S850A	121.30	122.12	4d
S850A	122.12	122.65	4a

S850A	122.65	123.95	2
S850A	123.95	126.80	1a
S851	0.00	37.70	7
S851	37.70	65.47	4a
S851	65.47	68.41	2
S851	68.41	71.93	1a
S852	0.00	51.81	7
S852	51.81	56.69	5b
S852	56.69	65.83	6
S852	65.83	86.07	4a
S852	86.07	86.43	2
S852	86.43	90.22	1a
S853	0.00	30.69	7
S853	30.69	64.87	4a
S853	64.87	68.21	2
S853	68.21	71.32	1a
S854A	0.00	81.79	7
S854A	81.79	90.22	4a
S854A	90.22	95.63	2
S854A	95.63	96.31	1a
S855	0.00	62.50	7
S855	62.50	84.12	5a
S855	84.12	93.27	6
S855	93.27	104.20	6
S855	104.20	111.56	4a
S855	111.56	114.60	2
S856	0.00	58.21	7
S856	58.21	81.05	5a
S856	81.05	98.00	6
S856	98.00	98.45	4b
S856	98.45	100.15	4a
S856	100.15	102.41	1a
S857	0.00	44.19	7
S857	44.19	62.79	6
S857	62.79	65.84	4a
S857	65.84	69.38	4d
S857	69.38	70.13	4c
S857	70.13	72.33	4d
S857	72.33	74.80	4a
S857	74.80	76.01	4d
S857	76.01	81.07	4a
S858	0.00	62.51	7
S858	62.51	65.36	4c
S858	65.36	72.58	4d
S858	72.58	74.63	4a
S858	74.63	81.07	2
S859	0.00	43.20	7
S859	43.20	81.07	5
S859	81.07	82.11	4d
S859	82.11	84.65	4a
S859	84.65	92.96	1a
S860	0.00	73.10	7
S860	73.10	74.70	4d
S860	74.70	88.69	4a
S860	88.69	93.00	2
S860	93.00	96.32	1a
S861	0.00	42.67	7
S861	42.67	75.74	5
S861	75.74	84.12	5d
S861	84.12	109.65	5
S861	109.65	111.29	4d
S861	111.29	114.60	1a
S862	0.00	35.30	7
S862	35.30	45.78	5b
S862	45.78	48.70	4a
S862	48.70	50.40	2
S862	50.40	59.40	1b
S863	0.00	41.45	7
S863	41.45	76.00	5b
S863	76.00	77.75	4a
S863	77.75	110.90	1b
S864	0.00	30.48	7
S864	30.48	250.50	5a
S864	250.50	251.30	5c
S864	251.30	271.60	5a
S864	271.60	272.20	5c
S864	272.20	273.60	2
S864	273.60	282.20	1b
S865	0.00	25.00	7
S865	25.00	68.60	5b
S865	68.60	69.00	4a
S865	69.00	71.00	2
S865	71.00	74.70	3
S865	74.70	78.60	1b
S866	0.00	38.00	7
S866	38.00	65.80	5b
S866	65.80	68.00	4a
S866	68.00	75.00	2
S866	75.00	81.00	3
S867	0.00	30.80	7
S867	30.80	50.37	4a
S867	50.37	54.60	2
S867	54.60	58.22	1a
S868	0.00	30.60	7
S868	30.60	46.72	4a
S868	46.72	52.45	2
S868	52.45	56.08	1a
S869	0.00	29.57	7
S869	29.57	48.60	4a
S869	48.60	51.40	2
S869	51.40	55.78	1a
S870	0.00	28.00	7
S870	28.00	57.60	4a
S870	57.60	61.57	2
S871	0.00	26.20	7
S871	26.20	64.00	4a
S871	64.00	66.85	2
S871	66.85	68.58	1a
S872	0.00	27.99	7
S872	27.99	58.72	4a
S872	58.72	61.06	2
S872	61.06	65.84	1a
S873	0.00	44.51	7
S873	44.51	47.55	6
S873	47.55	48.55	4b
S873	48.55	63.00	4a
S873	63.00	67.30	4d
S873	67.30	75.88	4a
S873	75.88	76.19	2
S873	76.19	81.08	1a
S874	0.00	36.58	7
S874	36.58	52.07	4a
S874	52.07	56.05	4d
S874	56.05	66.82	4a
S874	66.82	70.60	2
S874	70.60	73.46	1a
S875	0.00	28.35	7
S875	28.35	50.00	4a
S875	50.00	61.00	4b
S875	61.00	63.80	2
S875	63.80	71.34	1a
S876	0.00	30.48	7
S876	30.48	69.02	4a
S876	69.02	71.22	2
S876	71.22	74.98	1a
S877	0.00	59.55	7
S877	59.55	61.80	4b
S877	61.80	63.60	4c
S877	63.60	66.35	4d
S877	66.35	77.25	4a
S877	77.25	81.61	2
S877	81.61	83.52	1a
S878	0.00	32.61	7
S878	32.61	66.30	4a
S878	66.30	71.93	2
S878	71.93	74.98	1a
S879	0.00	25.50	7
S879	25.50	54.20	4a
S879	54.20	57.91	2
S880	0.00	27.65	7
S880	27.65	68.35	4a
S880	68.35	75.75	2
S880	75.75	78.03	1a
S881	0.00	33.40	7
S881	33.40	45.55	4b
S881	45.55	77.05	4a
S881	77.05	81.55	2
S881	81.55	85.95	1a
S882	0.00	30.25	7
S882	30.25	68.60	4a
S882	68.60	72.85	2
S882	72.85	76.81	1a
S883	0.00	59.45	7
S883	59.45	62.65	4b
S883	62.65	63.30	4d
S883	63.30	64.57	4e
S883	64.57	66.75	4c
S883	66.75	73.20	4d
S883	73.20	89.00	4a
S883	89.00	90.25	2
S884	0.00	81.35	7
S884	81.35	81.60	4b
S884	81.60	92.40	4a
S884	92.40	97.45	2
S884	97.45	101.80	1a
S885	0.00	32.55	7
S885	32.55	74.65	4a
S885	74.65	79.40	2
S885	79.40	84.73	1a
S886	0.00	33.80	7
S886	33.80	72.70	4a
S886	72.70	73.20	2
S886	73.20	79.25	1a
S887	0.00	27.30	7
S887	27.30	55.45	4a
S887	55.45	62.35	2
S887	62.35	66.14	1a
S901	0.00	2.00	
S901	2.00	13.15	
S901	13.15	26.00	
S902	0.00	3.00	
S902	3.00	20.50	
S902	20.50	24.40	
S902	24.40	30.00	
S903	0.00	2.50	
S903	2.50	14.45	
S903	14.45	30.00	
S904	0.00	2.75	
S904	2.75	12.50	
S904	12.50	14.75	
S904	14.75	29.00	
S905	0.00	3.45	
S905	3.45	11.80	
S905	11.80	20.00	
S906	0.00	2.30	
S906	2.30	13.10	
S906	13.10	14.00	
S906	14.00	20.00	
S907	0.00	2.80	
S907	2.80	13.90	
S907	13.90	17.40	
S907	17.40	23.00	
S908	0.00	4.15	
S908	4.15	24.20	
S908	24.20	24.85	
S908	24.85	27.00	
S909	0.00	2.75	
S909	2.75	22.85	
S909	22.85	26.55	
S909	26.55	29.00	
S910	0.00	3.70	
S910	3.70	27.20	
S910	27.20	32.00	
S911	0.00	3.80	
S911	3.80	30.80	
S911	30.80	40.60	
S911	40.60	43.00	
S912	0.00	3.50	
S912	3.50	19.80	
S912	19.80	26.15	
S912	26.15	29.00	
S913	0.00	3.80	
S913	3.80	14.45	
S913	14.45	20.00	
S914	0.00	6.20	
S914	6.20	25.30	
S914	25.30	25.70	
S914	25.70	29.00	
S915	0.00	5.90	
S915	5.90	20.80	
S915	20.80	23.00	
S916	0.00	5.40	
S916	5.40	26.70	
S916	26.70	32.00	
S917	0.00	6.20	
S917	6.20	46.00	
S917	46.00	47.45	
S917	47.45	49.00	
S918	0.00	3.40	
S918	3.40	39.85	
S918	39.85	40.80	
S918	40.80	44.00	
S919	0.00	8.70	
S919	8.70	45.10	
S919	45.10	50.00	
S920	0.00	9.00	
S920	9.00	41.40	
S920	41.40	44.17	
S920	44.17	50.00	
S921	0.00	12.00	
S921	12.00	36.35	
S921	36.35	38.10	
S921	38.10	44.00	
S922	0.00	12.90	
S922	12.90	47.45	
S922	47.45	50.00	
S922	50.00	53.00	
S923	0.00	10.85	
S923	10.85	42.20	
S923	42.20	44.85	
S923	44.85	50.00	
S924	0.00	13.80	
S924	13.80	49.50	
S924	49.50	51.00	
S925	0.00	16.30	
S925	16.30	33.40	
S925	33.40	37.00	
S926	0.00	14.00	
S926	14.00	28.55	
S926	28.55	32.00	
S927	0.00	18.40	
S927	18.40	42.75	
S927	42.75	47.00	
S928	0.00	22.70	
S928	22.70	46.10	
S928	46.10	48.90	
S928	48.90	56.00	
S929	0.00	21.70	
S929	21.70	50.20	
S929	50.20	56.00	
S930	0.00	6.60	
S930	6.60	32.90	
S930	32.90	37.20	
S930	37.20	40.00	
S931	0.00	4.65	
S931	4.65	26.80	
S931	26.80	31.00	
S932	0.00	13.60	
S932	13.60	39.10	
S932	39.10	42.70	
S932	42.70	44.00	
S933	0.00	12.10	
S933	12.10	29.95	
S933	29.95	32.45	
S933	32.45	35.00	
S934	0.00	18.40	
S934	18.40	38.20	
S934	38.20	41.70	
S934	41.70	44.00	
S935	0.00	8.00	
S935	8.00	29.55	
S935	29.55	31.50	
S935	31.50	35.00	
S936	0.00	7.20	
S936	7.20	30.90	
S936	30.90	35.00	
S937	0.00	50.00	7
S938	0.00	58.50	7
S938	58.50	61.22	4
S938	61.22	62.90	2
S938	62.90	70.00	1
S939	0.00	45.00	7
S939	45.00	48.95	4
S939	48.95	50.60	2

S939	50.60	54.00	1
S940	0.00	44.60	7
S940	44.60	44.90	6
S940	44.90	57.20	5b
S940	57.20	66.30	5a
S940	66.30	76.25	5a
S940	76.25	78.88	5a
S940	78.88	83.95	4
S940	83.95	85.00	1
S941	0.00	50.00	7
S941	50.00	61.75	5b
S941	61.75	66.00	5a
S941	66.00	76.00	5a
S941	76.00	77.70	5c
S941	77.70	86.40	5a
S941	86.40	86.80	5c
S941	86.80	90.80	5a
S941	90.80	91.05	4
S941	91.05	91.60	2
S941	91.60	95.00	1
S942	0.00	22.70	7
S942	22.70	49.00	5b
S942	49.00	59.00	5d
S942	59.00	67.00	5b
S942	67.00	70.98	5a
S942	70.98	78.40	5b
S942	78.40	79.20	5b
S942	79.20	86.95	5a
S942	86.95	89.35	5b
S942	89.35	90.30	5b
S942	90.30	95.60	5b
S942	95.60	96.65	4
S942	96.65	97.00	1
S943	0.00	35.00	7
S943	35.00	55.80	5b
S943	55.80	57.10	5b
S943	57.10	58.80	5b
S943	58.80	64.80	4
S943	64.80	65.50	2
S943	65.50	68.00	1
S944	0.00	40.50	7
S944	40.50	41.00	5b
S944	41.00	50.00	5d
S944	50.00	51.95	6b
S944	51.95	54.85	4
S944	54.85	56.80	2
S944	56.80	57.30	4
S944	57.30	59.00	1
S945	0.00	31.20	7
S945	31.20	39.80	5b
S945	39.80	40.65	5c
S945	40.65	43.50	5b
S945	43.50	44.40	5d
S945	44.40	51.10	4
S945	51.10	53.00	1
S946	0.00	73.00	7
S946	73.00	77.00	6b
S946	77.00	84.08	4
S946	84.08	87.00	2
S947	0.00	17.40	7
S947	17.40	32.33	4
S947	32.33	37.00	1
S948	0.00	35.00	7
S948	35.00	38.60	4
S948	38.60	41.00	1
S949	0.00	56.00	7
S949	56.00	58.50	4
S949	58.50	58.65	2
S949	58.65	62.00	1
S950	0.00	23.00	7
S950	23.00	36.00	6a
S950	36.00	41.60	4
S950	41.60	49.60	2
S950	49.60	50.00	1
S951	0.00	23.00	7
S951	23.00	64.20	5b
S951	64.20	66.60	4
S951	66.60	67.90	2
S951	67.90	71.00	1
S952	0.00	20.50	7
S952	20.50	33.00	5b
S952	33.00	47.47	5a
S952	47.47	57.00	5a
S952	57.00	59.20	5a
S952	59.20	63.40	5a
S952	63.40	82.90	5a
S952	82.90	83.30	5c
S952	83.30	90.50	5a
S952	90.50	93.00	5b
S952	93.00	93.55	4
S952	93.55	94.10	2
S952	94.10	96.00	1
S953	0.00	32.00	7
S953	32.00	50.00	5b
S953	50.00	56.05	5c
S953	56.05	56.87	5a
S953	57.87	60.70	5c
S953	60.70	64.75	5b
S953	64.75	73.94	5a
S953	73.94	74.25	5c
S953	74.25	88.00	5a
S953	88.00	90.90	5b
S953	90.90	92.62	4
S953	92.62	93.70	2
S953	93.70	98.00	1
S954	0.00	17.50	7
S954	17.50	42.30	5b
S954	42.30	44.30	5c
S954	44.30	53.50	5b
S954	53.50	68.57	5a
S954	68.57	73.63	5c
S954	73.63	80.25	5a
S954	80.25	81.25	5b
S954	81.25	87.35	5c
S954	87.35	114.85	5a
S954	114.85	115.50	5c
S954	115.50	117.95	5b
S954	117.95	118.50	5c
S954	118.50	120.75	5b
S954	120.75	126.42	4
S954	126.42	128.00	2
S954	128.00	131.00	1
S955	0.00	19.90	7
S955	19.90	44.10	5b
S955	44.10	59.50	5a
S955	59.50	65.10	5c
S955	65.10	73.05	5a
S955	73.05	75.20	5c
S955	75.20	78.30	5a
S955	78.30	79.80	5c
S955	79.80	101.10	5a
S955	101.10	104.40	5a
S955	104.40	105.10	4c
S955	105.10	106.68	4
S955	106.68	108.50	2
S955	108.50	110.00	1
S956	0.00	19.90	7
S956	19.90	40.77	5b
S956	40.77	42.63	5c
S956	42.63	53.55	5b
S956	53.55	68.00	5a
S956	68.00	72.50	5c
S956	72.50	79.50	5a
S956	79.50	82.80	5c
S956	82.80	87.15	5c
S956	87.15	109.50	5a
S956	109.50	117.55	5a
S956	117.55	123.50	4
S956	123.50	124.75	2
S956	124.75	129.00	1
S957	0.00	26.00	7
S957	26.00	63.00	5b
S957	63.00	68.00	5c
S957	68.00	75.50	5b
S957	75.50	81.25	5c
S957	81.25	84.50	5a
S957	84.50	86.95	5c
S957	86.95	95.40	5a
S957	95.40	96.85	5c
S957	96.85	102.15	5a
S957	102.15	103.20	5b
S957	103.20	109.90	4
S957	109.90	113.00	2
S957	113.00	116.00	1
S958	0.00	24.50	7
S958	24.50	33.50	5b
S958	33.50	39.75	5c
S958	39.75	53.92	5b
S958	53.92	77.00	5a
S958	77.00	77.70	5c
S958	77.70	84.10	5a
S958	84.10	86.10	5b
S958	86.10	87.10	5c
S958	87.10	88.00	5b
S958	88.00	91.20	4
S958	91.20	93.00	2
S958	93.00	98.00	1
S959	0.00	38.00	7
S959	38.00	60.50	5b
S959	60.50	62.00	5c
S959	62.00	65.00	5b
S959	65.00	66.90	4
S959	67.90	72.50	2
S959	72.50	74.00	1
S960	0.00	28.70	7
S960	28.70	48.15	4
S960	48.15	53.00	1
S961	0.00	22.70	7
S961	22.70	51.15	5b
S961	51.15	61.15	4
S961	61.15	61.35	2
S961	61.35	65.00	1
S962	0.00	29.00	7
S962	29.00	48.00	6a
S962	48.00	59.50	5b
S962	62.35	71.70	4
S962	71.70	76.00	1
S963	0.00	17.00	7
S963	17.00	38.17	5b
S963	38.17	62.75	5a
S963	62.75	64.20	5c
S963	64.20	65.25	5b
S963	65.25	66.70	5b
S963	66.70	67.60	5c
S963	67.60	69.10	5b
S963	69.10	70.75	4
S963	70.75	72.35	2
S963	72.35	74.00	1
S964	0.00	23.00	7
S964	23.00	26.00	7b
S964	26.00	47.00	7b
S964	47.00	50.00	7d
S964	50.00	53.00	7d
S964	53.00	65.00	7b
S964	65.00	76.20	7b
S964	76.20	77.83	4
S964	77.83	78.50	2
S964	78.50	83.00	1
S965	0.00	44.00	7
S965	44.00	58.10	5b
S965	58.10	67.50	5c
S965	67.50	69.50	5b
S965	69.50	72.60	5a
S965	72.60	77.10	5b
S965	77.10	78.40	5d
S965	78.40	80.00	5c
S965	80.00	83.00	5d
S965	83.00	84.50	6a
S965	84.50	87.82	4
S965	87.82	92.00	1
S966	0.00	41.00	7
S966	41.00	53.00	5b
S966	53.00	60.20	5d
S966	60.20	61.80	4
S966	61.80	63.90	2
S966	63.90	65.00	1
U001	0.00	15.64	4a
U001	15.64	20.63	4b
U001	20.63	20.97	4c
U001	20.97	21.70	7
U002	0.00	8.59	4a
U002	8.59	10.79	4b
U002	10.79	10.91	4e
U002	10.91	11.34	4b
U002	11.34	12.30	4c
U002	12.30	12.49	4e
U002	12.49	12.62	4b
U002	12.62	13.26	4e
U002	13.26	13.56	4b
U002	13.56	14.54	4e
U002	14.54	14.63	4b
U003	0.00	4.42	4a
U003	4.42	11.89	4b
U003	11.89	13.50	4a
U003	13.50	21.24	4b
U003	21.24	21.64	4c
U003	21.64	28.53	4a
U003	28.53	31.94	4b
U004	0.00	8.72	4a
U004	8.72	19.53	4b
U004	19.53	21.33	7
U005	0.00	19.20	4a
U006	0.00	45.72	4a
U007	0.00	8.75	1a
U007	8.75	35.23	2
U007	35.23	43.10	4a
U008	0.00	2.44	1a
U008	2.44	13.72	4a
U008	13.72	14.33	4b
U008	14.33	36.88	7
U009	0.00	0.70	1a
U009	0.70	13.14	2
U009	13.14	42.06	4a
U010	0.00	3.38	2
U010	3.38	18.07	4a
U011	0.00	5.69	4a
U011	5.69	6.13	4c
U011	6.13	17.37	6a
U012	0.00	17.07	4a
U012	17.07	17.34	4c
U012	17.34	18.68	4b
U012	18.68	20.73	7
U013	0.00	3.05	2
U014	0.00	6.80	4a
U014	6.80	8.96	2
U015	0.00	17.68	4a
U016	0.00	4.45	4a
U016	4.45	8.99	2
U017	0.00	9.36	4a
U017	9.36	9.66	4e
U017	9.66	12.89	4a
U017	12.89	13.66	4e
U017	13.66	14.20	4a
U017	14.20	14.33	4e
U017	14.33	18.96	4a
U018	0.00	2.80	2
U018	2.80	4.79	1a
U019	0.00	0.18	1a
U019	0.18	24.11	4a
U019	24.11	24.29	7
U020	0.00	2.35	4a
U020	2.35	5.79	2
U020	5.79	7.28	1a
U021	0.00	24.56	4a
U021	24.56	24.69	7
U022	0.00	1.10	4a
U022	1.10	3.20	1a
U023	0.00	9.39	4a
U023	9.39	9.78	4e
U023	9.78	23.84	4a
U023	23.84	24.48	6a
U024	0.00	7.16	1a
U024	7.16	10.76	2
U024	10.76	16.28	4a
U024	16.28	16.64	4c
U024	16.64	17.77	4b
U024	17.77	18.65	4c
U024	18.65	19.81	7
U025	0.00	11.13	1a
U025	11.13	13.26	2
U025	13.26	13.66	4a
U025	13.66	15.24	4c
U025	15.24	16.76	7
U026	0.00	20.54	1a

U026	20.54	31.09	4a
U027	0.00	12.37	1a
U027	12.37	13.96	2
U027	13.96	25.09	4b
U027	25.09	26.49	6
U028	0.00	4.88	1a
U028	4.88	6.46	2
U028	6.46	14.66	4a
U028	14.66	15.42	4c
U028	15.42	15.73	4b
U028	15.73	16.76	6
U029	0.00	7.62	4a
U029	7.62	8.66	4c
U029	8.66	9.14	7
U030	0.00	1.52	2
U030	1.52	8.41	4a
U030	8.41	9.60	4c
U031	0.00	6.10	4a
U031	6.10	13.71	1a
U032	0.00	5.94	4a
U032	5.94	7.62	4b
U032	7.62	22.86	4a
U033	0.00	3.04	1a
U034	0.00	13.32	4a
U034	13.32	14.05	4c
U035	0.00	2.99	1a
U035	2.99	5.12	2
U035	5.12	5.64	4b
U035	5.64	8.23	4a
U035	8.23	8.53	7
U036	0.00	10.88	4a
U037	0.00	2.13	1a
U037	2.13	3.38	2
U037	3.38	20.36	4a
U037	20.36	20.79	4e
U037	20.79	22.56	4a
U037	22.56	23.20	4e
U037	23.20	24.84	4a
U037	24.84	25.30	4c
U037	25.30	25.40	4b
U037	25.40	25.63	4c
U037	25.63	26.21	4b
U037	26.21	27.43	7
U038	0.00	12.74	1a
U038	12.74	34.14	4a
U039	0.00	8.17	1a
U039	8.17	12.86	2
U039	12.86	38.10	4a
U040	0.00	3.29	1a
U040	3.29	8.53	2
U040	8.53	29.72	4a
U041	0.00	0.37	2
U041	0.37	7.66	4a
U041	7.66	7.92	4e
U041	7.92	31.67	4a
U041	31.67	32.00	7
U042	0.00	4.51	4a
U042	4.51	6.61	4c
U042	6.61	7.01	4a
U042	7.01	9.75	4b
U043	0.00	3.66	4a
U043	3.66	14.60	1a
U044	0.00	22.52	4a
U045	0.00	2.26	4a
U045	2.26	2.44	4e
U045	2.44	15.12	4a
U045	15.12	15.64	4c
U045	15.64	20.24	4a
U046	0.00	2.90	4a
U046	2.90	7.68	1a
U047	0.00	12.19	4a
U047	12.19	12.50	4b
U048	0.00	0.79	4a
U048	0.79	4.08	2
U048	4.08	11.58	1a
U049	0.00	19.72	4a
U050	0.00	4.20	4a
U050	4.20	7.22	1a
U051	0.00	3.84	4a
U051	3.84	4.42	4e
U051	4.42	22.22	4a
U051	22.22	22.86	7
U052	0.00	15.24	4a
U052	15.24	15.54	4e
U052	15.54	16.31	4b
U052	16.31	16.61	4e
U052	16.61	21.15	4a
U052	21.15	21.34	7
U053	0.00	1.89	4a
U053	1.89	4.88	1a
U054	0.00	18.29	4a
U054	18.29	18.62	4c
U054	18.62	19.81	4b
U055	0.00	11.58	2
U055	11.58	14.23	1a
U056	0.00	5.49	5a
U056	5.49	6.10	5c
U056	6.10	7.86	5b
U056	7.86	9.75	5c
U056	9.75	18.29	5a
U056	18.29	29.57	4a
U057	0.00	19.35	1a
U057	19.35	19.81	2
U057	19.81	25.30	4a
U057	25.30	30.78	5a
U058	0.00	15.69	1a
U058	15.69	17.68	2
U058	17.68	22.56	4a
U059	0.00	4.27	4a
U059	4.27	8.84	6a
U059	8.84	9.45	5b
U060	0.00	5.85	4a
U060	5.85	7.01	4b
U060	7.01	18.29	2
U061	0.00	3.96	4a
U061	3.96	6.09	4b
U061	6.09	11.28	6
U062	0.00	4.57	4a
U062	4.57	7.78	4d
U062	7.78	15.54	6
U063	0.00	38.40	4a
U064	0.00	16.00	1a
U064	16.00	38.40	2
U065	0.00	7.62	4a
U065	7.62	11.58	4a
U066	0.00	12.50	5b
U067	0.00	14.02	4a
U067	14.02	27.13	2
U067	27.13	35.66	1a
U068	0.00	3.69	4b
U068	3.69	14.32	4a
U069	0.00	6.09	4a
U069	6.09	12.19	4b
U069	12.19	18.29	4a
U070	0.00	22.25	4a
U071	0.00	23.65	4a
U071	23.65	25.91	7
U073	0.00	13.10	5a
U073	13.10	18.90	4a
U073	18.90	23.04	2
U073	23.04	28.04	1a
U074	0.00	10.05	1a
U074	10.05	11.58	4a
U074	11.58	13.72	5b
U075	0.00	8.40	1a
U075	8.40	13.65	4a
U075	13.65	16.64	4c
U075	16.64	16.95	4a
U075	16.95	17.07	5b
U076	0.00	9.14	4a
U076	9.14	9.91	4e
U076	9.91	11.79	4b
U076	11.79	12.13	4e
U076	12.13	13.87	4c
U076	13.87	18.59	4a
U076	18.59	19.20	4e
U076	19.20	40.23	4a
U077	0.00	4.20	4a
U077	4.20	5.51	4b
U077	5.51	6.09	4e
U077	6.09	24.99	4a
U077	24.99	25.90	4e
U077	25.90	31.39	4a
U077	31.39	39.01	4b
U077	39.01	39.62	4e
U078	0.00	18.28	4a
U078	18.28	22.68	4b
U078	22.68	30.48	4a
U079	0.00	31.05	4a
U079	31.05	35.05	1a
U080	0.00	9.14	4a
U080	9.14	9.90	4e
U080	9.90	10.61	4a
U080	10.61	13.08	2
U080	13.08	15.24	1a
U081	0.00	8.80	4a
U081	8.80	15.24	6a
U082	0.00	11.94	4a
U082	11.94	14.93	1a
U083	0.00	8.84	4a
U083	8.84	11.27	6a
U084	0.00	5.79	4a
U085	0.00	2.80	4a
U085	2.80	3.04	4e
U085	3.04	9.14	4a
U085	9.14	11.28	4e
U085	11.28	12.64	4a
U085	12.64	14.32	4e
U085	14.32	19.20	4b
U086	0.00	3.81	4a
U086	3.81	4.10	2
U086	4.10	7.62	1a
U087	0.00	28.34	4a
U088	0.00	7.62	1a
U088	7.62	11.30	2
U088	11.30	16.06	4a
U088	16.06	16.33	4c
U088	16.33	17.37	6a
U089	0.00	6.91	1a
U089	6.91	7.52	4e
U089	7.52	11.28	4a
U089	11.28	11.37	4e
U089	11.37	19.87	4a
U089	19.87	19.94	4b
U089	19.94	20.42	6
U090	0.00	15.39	1a
U090	15.39	22.56	4a
U091	0.00	2.56	4a
U091	2.56	3.05	4e
U091	3.05	12.77	4a
U091	12.77	13.41	4e
U091	13.41	14.23	4b
U091	14.23	14.94	4e
U091	14.94	15.85	4b
U091	15.85	17.68	4e
U092	0.00	2.47	4a
U092	2.47	2.74	4e
U092	2.74	26.67	4a
U092	26.67	27.73	4e
U092	27.73	30.78	4a
U093	0.00	25.90	4a
U093	25.90	29.87	2
U094	0.00	26.69	4a
U094	26.69	38.30	4b
U095	0.00	37.50	4a
U096	0.00	11.37	4a
U096	11.37	14.94	1a
U097	0.00	3.23	4a
U097	3.23	6.27	2
U097	6.27	33.53	4a
U098	0.00	0.24	4a
U098	0.24	21.03	1a
U099	0.00	12.19	4a
U099	12.19	13.72	4a
U099	13.72	14.81	4e
U099	14.81	18.28	4a
U099	18.28	18.71	4a
U099	18.71	20.17	4c
U099	20.17	20.48	4a
U099	20.48	23.77	4b
U100	0.00	2.44	4a
U100	2.44	9.14	1a
U101	0.00	3.05	4a
U101	3.05	4.57	4b
U101	4.57	33.52	4a
U101	33.52	33.68	4c
U101	33.68	34.42	4e
U101	34.42	37.79	4b
U102	0.00	27.43	4a
U102	27.43	27.79	4c
U102	27.79	31.09	4b
U103	0.00	22.25	4a
U104	0.00	16.49	2
U104	16.49	26.12	4a
U104	26.12	31.60	4b
U104	31.60	33.52	4a
U104	33.52	42.67	4a
U104	42.67	45.29	4c
U104	45.29	46.63	4b
U105	0.00	13.90	4a
U105	13.90	14.48	4e
U105	14.48	19.20	4a
U105	19.20	29.26	4b
U106	0.00	30.48	4a
U107	0.00	6.10	4a
U107	6.10	8.04	4a
U107	8.04	11.12	4b
U107	11.12	18.28	1a
U108	0.00	1.52	4a
U108	1.52	2.13	4b
U108	2.13	2.74	4c
U108	2.74	8.53	4b
U109	0.00	0.54	4b
U109	0.54	1.52	4a
U109	1.52	2.10	4e
U109	2.10	10.66	4a
U109	10.66	12.49	4b
U109	12.49	16.91	4c
U109	16.91	17.61	6a
U109	17.61	21.94	5c
U109	21.94	22.25	5b
U110	0.00	6.73	4a
U110	6.73	14.02	4b
U110	14.02	16.22	4e
U110	16.22	18.89	1a
U111	0.00	4.66	4a
U111	4.66	6.67	4c
U111	6.67	21.64	4a
U112	0.00	22.56	4a
U113	0.00	3.19	4a
U113	3.19	13.71	4b
U113	13.71	14.41	4e
U113	14.41	15.84	2
U113	15.84	18.28	1a
U114	0.00	10.97	1a
U114	10.97	11.27	2
U114	11.27	17.06	4a
U114	17.06	17.67	5a
U115	0.00	2.34	1a
U115	2.34	2.52	2
U115	2.52	6.70	4a
U116	0.00	5.46	1a
U116	5.46	6.79	4a
U116	6.79	8.32	4a
U116	8.32	10.02	4a
U116	10.02	11.89	5b
U117	0.00	3.38	1a
U117	3.38	7.47	2
U117	7.47	16.64	4a
U117	16.64	17.28	4c
U117	17.28	23.90	4a
U117	23.90	24.00	4c
U117	24.00	26.51	5b
U118	0.00	1.52	4a
U118	1.52	3.05	4c
U118	3.05	5.18	4b
U118	5.18	14.02	6
U119	0.00	3.41	1a
U119	3.41	21.34	4a
U120	0.00	21.34	4a
U120	21.34	22.56	4e
U120	22.56	24.38	4a
U121	0.00	24.38	4a
U121	24.38	25.30	7

U122	0.00	0.64	1a
U122	0.64	23.16	4a
U123	0.00	21.64	4a
U123	21.64	22.00	7
U124	0.00	1.21	1a
U124	1.21	17.37	4a
U125	0.00	4.36	1a
U125	4.36	8.08	2
U125	8.08	25.18	4a
U125	25.18	27.43	7
U126	0.00	3.93	1a
U126	3.93	27.43	4a
U126	27.43	28.95	6a
U127	0.00	5.33	4a
U127	5.33	7.92	1a
U128	0.00	19.81	4a
U129	0.00	27.52	4a
U129	27.52	39.01	2
U130	0.00	6.27	4a
U130	6.27	9.14	1a
U131	0.00	9.44	4a
U131	9.44	13.10	1a
U132	0.00	8.53	1a
U133	0.00	6.10	1a
U135	0.00	15.24	1a
U137	0.00	1.00	4a
U137	1.00	14.57	4b
U139	0.00	14.63	4b
U140	0.00	1.52	4a
U140	1.52	24.38	4b
U141	0.00	6.10	4b
U141	6.10	6.70	4e
U141	6.70	7.01	4b
U141	7.01	7.62	4e
U141	7.62	8.53	4b
U141	8.53	9.14	4e
U141	9.14	19.20	4b
U143	0.00	19.53	4a
U143	19.53	22.86	4b
U143	22.86	23.92	4a
U143	23.92	24.38	4e
U143	24.38	25.60	4a
U143	25.60	25.90	4e
U143	25.90	27.88	4a
U143	27.88	31.39	4b
U143	31.39	32.16	4a
U143	32.16	44.20	6a
U144	0.00	24.38	4a
U144	24.38	25.30	7
U145	0.00	23.77	4a
U145	23.77	27.12	7
U146	0.00	23.47	4a
U146	23.47	23.77	7
U147	0.00	15.85	4a
U147	15.85	19.05	4e
U147	19.05	26.82	4a
U148	0.00	26.82	4a
U149	0.00	2.44	4a
U149	2.44	3.05	4e
U149	3.05	13.26	4a
U149	13.26	13.72	4e
U149	13.72	25.76	4a
U149	25.76	25.90	7
U150	0.00	0.76	2
U150	0.76	32.91	4a
U151	0.00	2.19	2
U151	2.19	19.35	4a
U151	19.35	19.81	4e
U151	19.81	24.38	4a
U152	0.00	1.92	4a
U152	1.92	9.42	4b
U152	9.42	13.23	4a
U152	13.23	15.73	4b
U152	15.73	16.82	4a
U152	16.82	18.71	4b
U152	18.71	25.42	4a
U152	25.42	26.57	4e
U152	26.57	31.80	4a
U152	31.80	32.30	4b
U153	0.00	3.47	4a
U153	3.47	8.30	4b
U153	8.30	13.90	4a
U153	13.90	19.81	4b
U154	0.00	2.31	4a
U154	2.31	9.14	4b
U154	9.14	13.78	4a
U154	13.78	18.29	4b
U154	18.29	24.38	4a
U155	0.00	3.05	4b
U155	3.05	4.88	4a
U155	4.88	11.52	4b
U155	11.52	12.68	4a
U155	12.68	19.35	4b
U155	19.35	36.12	4a
U155	36.12	36.72	4e
U155	36.72	37.64	4b
U155	37.64	38.56	4e
U155	38.56	40.78	4b
U155	40.78	42.67	4a
U156	0.00	6.85	4a
U156	6.85	8.47	4e
U156	8.47	10.09	4b
U156	10.09	17.89	4a
U156	17.89	18.29	4e
U156	18.29	32.00	4a
U157	0.00	12.64	4a
U157	12.64	13.71	4e
U157	13.71	18.10	4a
U157	18.10	24.38	2
U158	0.00	6.10	4a
U158	6.10	9.14	6a
U159	0.00	1.22	4a
U159	1.22	1.52	4e
U159	1.52	18.29	4a
U160	0.00	5.94	4a
U160	5.94	8.62	4e
U160	8.62	9.27	4b
U160	9.27	18.29	4a
U161	0.00	17.37	4a
U161	17.37	17.68	4b
U162	0.00	8.30	4a
U162	8.30	9.14	4e
U162	9.14	17.68	4a
U163	0.00	2.74	4c
U163	2.74	3.05	4e
U163	3.05	6.10	4c
U163	6.10	11.58	4b
U163	11.58	14.02	4c
U164	0.00	5.33	2
U164	5.33	23.77	4a
U165	0.00	2.74	1a
U165	2.74	19.81	4a
U165	19.81	21.34	6a
U166	0.00	12.19	4a
U166	12.19	13.25	4c
U166	13.25	14.17	4a
U166	14.17	15.24	6a
U167	0.00	25.15	4a
U167	25.15	25.90	4b
U167	25.90	29.32	4a
U168	0.00	32.00	4a
U169	0.00	4.11	4a
U169	4.11	4.57	4e
U169	4.57	18.29	4a
U169	18.29	24.38	4b
U169	24.38	25.15	4e
U169	25.15	39.16	4b
U169	39.16	39.93	4a
U169	39.93	41.45	4b
U170	0.00	6.10	4a
U171	0.00	8.60	4a
U171	8.60	10.12	4b
U171	10.12	19.20	6a
U172	0.00	7.16	4a
U173	0.00	14.17	4a
U173	14.17	15.24	4b
U173	15.24	15.69	4e
U173	15.69	17.22	4b
U173	17.22	17.76	4e
U173	17.76	18.74	4b
U173	18.74	21.34	4a
U174	0.00	13.32	4a
U174	13.32	14.48	4c
U174	14.48	16.76	6a
U175	0.00	26.52	4a
U176	0.00	7.62	4a
U176	7.62	10.67	4b
U176	10.67	26.37	4a
U176	26.37	28.65	4c
U176	28.65	35.05	6a
U177	0.00	1.25	1a
U177	1.25	8.00	4a
U177	8.00	8.38	4e
U177	8.38	8.79	4a
U177	8.79	9.14	4e
U177	9.14	39.14	4a
U177	39.14	40.84	6a
U178	0.00	33.53	4a
U178	33.53	40.84	4b
U179	0.00	38.40	4a
U180	0.00	29.57	4a
U180	29.57	30.00	7
U181	0.00	22.86	4a
U181	22.86	23.77	7
U182	0.00	40.23	2
U183	0.00	4.08	1a
U183	4.08	9.14	2
U183	9.14	20.24	4a
U183	20.24	20.54	4b
U183	20.54	32.00	4a
U184	0.00	2.13	4b
U184	2.13	5.51	4a
U184	5.51	7.55	4b
U184	7.55	10.94	4a
U184	10.94	17.06	4b
U185	0.00	21.64	4a
U186	0.00	43.59	4a
U186	43.59	45.72	4b
U187	0.00	16.40	4a
U187	16.40	35.35	2
U188	0.00	20.93	4a
U188	20.93	25.90	4b
U189	0.00	16.30	4a
U189	16.30	63.09	2
U190	0.00	23.31	4a
U190	23.31	28.95	4b
U190	28.95	32.30	7
U191	0.00	6.09	1a
U191	6.09	9.44	2
U191	9.44	39.93	4a
U192	0.00	4.87	1a
U192	4.87	13.10	4a
U192	13.10	16.15	6a
U193	0.00	19.20	4a
U194	0.00	14.14	1a
U194	14.14	15.63	4a
U194	15.63	16.30	4c
U194	16.30	16.45	4b
U194	16.45	19.20	7
U195	0.00	16.00	1a
U195	16.00	18.29	2
U195	18.29	20.11	4a
U195	20.11	20.72	4c
U195	20.72	23.16	6a
U196	0.00	27.43	1a
U196	27.43	29.32	4a
U196	29.32	30.24	4c
U196	30.24	32.30	6a
U197	0.00	0.30	4a
U197	0.30	2.59	4b
U197	2.59	2.86	4e
U197	2.86	7.62	4a
U197	7.62	7.77	4e
U197	7.77	8.20	4b
U197	8.20	8.35	4e
U197	8.35	8.53	4b
U197	8.53	8.84	4e
U197	8.84	12.80	4b
U197	12.80	14.78	4e
U197	14.78	15.84	4b
U198	0.00	0.69	4a
U198	0.69	1.00	4e
U198	1.00	4.14	4b
U198	4.14	9.14	4a
U199	0.00	13.11	4a
U199	13.11	16.30	4b
U199	16.30	31.40	4a
U200	0.00	6.40	2
U200	6.40	40.84	4a
U200	40.84	44.50	4b
U200	44.50	47.55	7
U201	0.00	47.24	2
U204	0.00	6.55	4a
U204	6.55	7.77	2
U204	7.77	11.60	1a
U205	0.00	24.69	4a
U206	0.00	37.79	4a
U208	0.00	31.09	1a
U209	0.00	23.16	4a
U210	0.00	5.03	4a
U210	5.03	23.47	2
U211	0.00	8.84	4a
U211	8.84	42.67	2
U212	0.00	23.13	4a
U212	23.13	27.43	4b
U213	0.00	25.00	4a
U213	25.00	27.74	4b
U213	27.74	30.78	7
U214	0.00	12.50	2
U214	12.50	15.24	1a
U215	0.00	27.52	4a
U215	27.52	29.26	7
U216	0.00	2.74	2
U216	2.74	23.90	4a
U216	23.90	24.68	4c
U216	24.68	26.51	4b
U217	0.00	5.80	2
U217	5.80	41.84	4a
U217	41.84	45.11	1a
U218	0.00	3.35	2
U218	3.35	5.79	4a
U218	5.79	12.49	4e
U218	12.49	20.97	4a
U218	20.97	21.94	4b
U218	21.94	25.30	4a
U218	25.30	39.01	4b
U220	0.00	2.43	1a
U220	2.43	3.81	2
U220	3.81	9.75	4a
U221	0.00	1.76	1a
U221	1.76	3.65	4a
U222	0.00	7.49	1a
U222	7.49	11.58	2
U222	11.58	16.45	4a
U222	16.45	16.77	4b
U222	16.77	19.20	6
U223	0.00	5.18	1a
U223	5.18	11.94	4a
U223	11.94	13.87	4b
U223	13.87	16.15	4a
U224	0.00	3.35	1a
U224	3.35	6.40	4a
U224	6.40	7.62	6a
U224	7.62	10.97	5b
U225	0.00	34.75	4a
U225	34.75	35.05	4c
U225	35.05	35.35	7
U226	0.00	21.33	4a
U226	21.33	21.64	4c
U226	21.64	22.56	4b
U226	22.56	24.69	7
U227	0.00	27.83	4a
U227	27.83	31.09	4b
U227	31.09	32.00	7
U228	0.00	18.89	4a
U228	18.89	19.35	4c
U228	19.35	20.11	4b
U228	20.11	24.38	6a
U229	0.00	9.75	4a
U229	9.75	11.58	4c
U229	11.58	13.10	4b
U229	13.10	14.32	4a
U229	14.32	16.46	4b
U230	0.00	5.18	4a

U230	5.18	5.48	4c
U230	5.48	10.97	4a
U231	0.00	7.13	4a
U231	7.13	7.68	4c
U231	7.68	7.92	7
U232	0.00	16.67	4a
U232	16.67	17.00	4c
U233	0.00	8.84	4a
U233	8.84	13.41	4b
U234	0.00	8.47	4a
U234	8.47	15.84	4b
U235	0.00	25.14	4a
U235	25.14	27.73	2
U235	27.73	28.65	1a
U236	0.00	19.20	4a
U236	19.20	23.40	4e
U236	23.40	27.58	4a
U236	27.58	29.60	7
U237	0.00	7.77	4a
U237	7.77	8.84	2
U237	8.84	10.67	1a
U238	0.00	6.10	4a
U238	6.10	7.77	4b
U238	7.77	7.92	4c
U239	0.00	38.40	4a
U239	38.40	38.70	7
U240	0.00	8.38	4a
U241	0.00	11.28	4a
U241	11.28	12.20	4c
U241	12.20	13.41	4b
U242	0.00	12.03	4a
U242	12.03	12.89	4b
U242	12.89	13.44	4a
U242	13.44	17.37	4b
U243	0.00	9.69	4a
U243	9.69	21.88	4b
U243	21.88	24.69	6a
U244	0.00	32.43	4a
U244	32.43	35.66	1a
U245	0.00	40.54	4a
U246	0.00	3.35	4a
U246	3.35	4.27	4c
U246	4.27	4.82	4b
U246	4.82	5.88	7
U247	0.00	7.01	4a
U247	7.01	10.67	4b
U248	0.00	25.30	4a
U248	25.30	25.91	7
U249	0.00	46.33	4a
U250	0.00	21.34	4a
U250	21.34	21.94	1a
U251	0.00	27.43	4a
U251	27.43	28.50	4c
U251	28.50	31.40	6a
U252	0.00	11.89	4a
U252	11.89	16.15	4b
U252	16.15	18.90	7
U253	0.00	6.10	1a
U253	6.10	12.64	4a
U253	12.64	14.33	4b
U253	14.33	16.15	7
U254	0.00	3.35	1a
U254	3.35	7.62	4a
U254	7.62	8.38	4c
U254	8.38	9.45	4b
U254	9.45	12.80	6a
U256?	0.00	10.30	4a
U256?	10.30	10.94	4b
U258	0.00	10.36	4a
U258	10.36	13.40	7
U259	0.00	22.56	4a
U259	22.56	23.16	7
U260	0.00	18.60	1a
U260	18.60	39.62	2
U261	0.00	11.73	1a
U261	11.73	14.60	4a
U261	14.60	16.15	1a
U261	16.15	32.77	2
U261	32.77	43.90	4a
U261	43.90	44.35	4c
U261	44.35	45.11	4a
U261	45.11	48.16	7
U262	0.00	11.40	2
U262	11.40	43.90	4a
U263	0.00	2.74	4a
U263	2.74	3.35	4b
U263	3.35	15.54	6a
U263	15.54	22.56	5b
U264	0.00	2.44	4a
U264	2.44	3.05	4b
U264	3.05	16.15	6a
U265	0.00	22.40	1a
U265	22.40	24.54	4a
U265	24.54	25.30	4c
U265	25.30	29.70	6a
U266	0.00	3.04	4a
U266	3.04	3.35	4b
U266	3.35	24.38	6a
U267	0.00	5.49	4a
U267	5.49	6.10	4e
U267	6.10	19.81	4a
U267	19.81	21.94	7
U268	0.00	5.80	4a
U268	5.80	7.16	4c
U268	7.16	11.00	7
U269	0.00	4.57	4a
U269	4.57	4.88	4e
U269	4.88	7.92	4a
U269	7.92	8.23	4e
U269	8.23	11.00	4a
U269	11.00	11.89	4e
U269	11.89	12.50	4c
U269	12.50	13.87	6a
U269	13.87	16.76	5b
U270	0.00	8.53	1a
U270	8.53	11.88	2
U270	11.88	16.02	4a
U270	16.02	18.57	5b
U270	18.57	30.48	5b
U271	0.00	4.41	1a
U271	4.41	6.09	2
U271	6.09	9.14	4a
U271	9.14	13.10	5b
U272	0.00	28.80	1a
U272	28.80	30.69	4a
U272	30.69	32.30	4c
U272	32.30	34.44	4a
U272	34.44	34.75	5b
U273	0.00	13.10	1a
U273	13.10	15.24	2
U273	15.24	16.76	4a
U273	16.76	17.06	5b
U274	0.00	17.67	1a
U274	17.67	21.33	4a
U274	21.33	25.29	5b
U275	0.00	6.25	1a
U275	6.25	8.38	2
U275	8.38	10.66	4a
U275	10.66	14.33	5b
U276	0.00	22.25	1a
U276	22.25	24.68	4a
U276	24.68	26.52	6a
U276	26.52	28.04	5b
U277	0.00	29.56	1a
U277	29.56	32.76	4a
U277	32.76	36.88	5b
U282	0.00	19.20	4a
U282	19.20	23.93	4b
U282	23.93	26.06	2
U282	26.06	27.43	1a
U283	0.00	3.66	4a
U283	3.66	4.82	4c
U283	4.82	18.89	6a
U285	0.00	0.76	4c
U285	0.76	6.10	6a
U286	0.00	0.61	1a
U286	0.61	1.22	4a
U286	1.22	5.18	2
U286	5.18	8.23	1a
U287	0.00	10.67	4a
U287	10.67	12.67	2
U287	12.67	15.48	1a
U288	0.00	1.46	2
U288	1.46	2.04	4a
U288	2.04	3.04	4b
U288	3.04	15.24	4a
U289	0.00	22.56	1a
U289	22.56	37.95	4a
U289	37.95	38.56	4e
U289	38.56	38.71	4c
U289	38.71	40.23	4b
U290	0.00	10.06	1a
U290	10.06	10.21	4e
U290	10.21	23.16	4a
U291	0.00	33.22	1a
U291	33.22	33.98	4a
U291	33.98	38.40	4e
U291	38.40	42.97	4a
U291	42.97	46.48	4e
U291	46.48	46.94	4c
U292	0.00	25.91	1a
U292	25.91	38.71	4b
U292	38.71	42.67	4e
U292	42.67	43.59	4c
U292	43.59	43.74	4e
U292	43.74	44.96	4b
U292	44.96	45.72	4e
U292	45.72	48.46	4b
U292	48.46	49.38	4e
U292	49.38	51.05	4b
U292	51.05	52.12	4e
U292	52.12	54.56	4b
U292	54.56	65.84	6a
U293	0.00	26.50	1a
U293	26.50	32.16	2
U293	32.16	35.36	4e
U293	35.36	36.11	4b
U293	36.11	36.73	4e
U293	36.73	43.28	4a
U293	43.28	44.81	4c
U293	44.81	49.68	5b
U294	0.00	27.19	1a
U294	27.19	45.29	4a
U294	45.29	46.02	4c
U294	46.02	49.38	4e
U294	49.38	49.62	4b
U294	49.62	54.25	6a
U295	0.00	11.58	1a
U295	11.58	13.11	2
U295	13.11	19.81	4a
U295	19.81	20.57	6a
U295	20.57	23.16	5b
U296	0.00	9.14	1a
U296	9.14	12.65	4a
U296	12.65	13.11	4c
U296	13.11	13.72	4e
U296	13.72	14.33	4b
U296	14.33	15.24	5b
U296	15.24	15.85	5d
U296	15.85	18.90	5b
U297	0.00	33.22	1a
U297	33.22	36.58	2
U297	36.58	42.06	4b
U297	42.06	42.37	4e
U297	42.37	44.81	4a
U297	44.81	45.42	4c
U297	45.42	53.65	5b
U298	0.00	21.95	1a
U298	21.95	31.70	4b
U298	31.70	32.61	4e
U298	32.61	38.71	4b
U298	38.71	46.02	4a
U298	46.02	51.21	6a
U299	0.00	34.44	1a
U299	34.44	39.78	4a
U299	39.78	40.54	4b
U299	40.54	40.90	4c
U299	40.90	42.98	6a
U299	42.98	43.59	5b
U299	43.59	44.20	5d
U299	44.20	50.29	5b
U301	0.00	16.46	1a
U304	0.00	28.04	4a
U305	0.00	7.47	2
U305	7.47	10.67	4a
U305	10.67	11.89	4e
U305	11.89	12.80	4a
U305	12.80	13.11	4e
U305	13.11	13.72	4a
U305	13.72	14.33	4e
U305	14.33	17.37	4a
U305	17.37	17.98	4e
U305	17.98	22.56	4a
U305	22.56	23.16	4e
U305	23.16	25.30	4a
U305	25.30	25.60	4e
U305	25.60	28.04	4a
U305	28.04	28.65	4e
U305	28.65	33.53	4a
U305	33.53	33.83	4e
U305	33.83	38.40	4a
U305	38.40	39.01	4e
U305	39.01	41.45	4a
U305	41.45	42.06	4e
U305	42.06	42.67	4a
U305	42.67	43.28	4e
U305	43.28	45.42	4a
U305	45.42	46.33	4e
U305	46.33	47.85	4a
U307	0.00	1.52	4a
U307	1.52	2.59	4c
U307	2.59	4.27	4b
U307	4.27	9.45	7
U309	0.00	2.74	4a
U309	2.74	3.96	4e
U309	3.96	4.27	4a
U309	4.27	4.88	4e
U309	4.88	42.67	4a
U310	0.00	0.91	4a
U310	0.91	8.84	2
U311	0.00	5.79	4a
U312	0.00	6.40	4a
U312	6.40	47.24	2
U314	0.00	31.58	1a
U314	31.58	41.45	4a
U314	41.45	41.97	4c
U314	41.97	43.89	4b
U314	43.89	48.77	7
U315	0.00	28.96	1a
U316	0.00	24.38	1a
U316	24.38	32.46	4b
U316	32.46	33.83	4e
U316	33.83	34.74	4b
U316	34.74	45.11	4a
U316	45.11	46.94	4c
U316	46.94	47.85	4b
U316	47.85	53.95	6
U317	0.00	24.38	1a
U317	24.38	25.60	4b
U317	25.60	26.21	4a
U317	26.21	27.43	4e
U317	27.43	34.75	4a
U317	34.75	35.20	4c
U317	35.20	39.93	4b
U318	0.00	19.96	1a
U318	19.96	37.80	4a
U318	37.80	42.06	4b
U318	42.06	42.67	6a
U319	0.00	22.86	4a
U320	0.00	8.69	4a
U320	8.69	9.57	4c
U320	9.57	16.76	7
U321	0.00	7.77	4a
U321	7.77	7.92	4c
U321	7.92	14.32	7
U322	0.00	8.44	4a
U322	8.44	8.53	4c
U322	8.53	12.41	7
U324	0.00	1.83	4a
U324	1.83	6.10	2
U325	0.00	7.01	4a
U325	7.01	7.07	4c
U325	7.07	15.54	6a
U326	0.00	6.40	4a

U326	6.40	6.46	4c
U326	6.46	12.80	6a
U330	0.00	2.44	4a
U330	2.44	4.27	4c
U330	4.27	5.94	4a
U330	5.94	7.37	4c
U330	7.37	13.72	6a
U331	0.00	0.61	4a
U331	0.61	2.74	4c
U331	2.74	3.66	4a
U331	3.66	6.10	4c
U331	6.10	7.93	4a
U332	0.00	1.37	4a
U332	1.37	7.62	4c
U333	0.00	10.80	4a
U334	0.00	30.48	4a
U334	30.48	34.74	6a
U336	0.00	9.14	1a
U336	9.14	13.41	2
U336	13.41	20.72	4a
U336	20.72	23.77	5b
U337	0.00	19.81	1a
U337	19.81	24.23	4a
U337	24.23	24.38	4c
U337	24.38	26.82	5b
U500	0.00	44.81	1a
U500	44.81	46.40	2
U500	46.40	50.10	4d
U500	50.10	51.60	4c
U500	51.60	51.85	4b
U500	51.85	60.66	5a
U501	0.00	15.26	1a
U501	15.26	16.30	4d
U501	16.30	18.95	4a
U501	18.95	22.14	4d
U501	22.14	23.30	4c
U501	23.30	25.30	7
U502	0.00	10.93	1a
U502	10.93	13.55	4d
U502	13.55	18.48	4a
U502	18.48	20.42	4d
U502	20.42	21.94	7
U503	0.00	35.35	1a
U503	35.35	39.35	2
U503	39.35	41.05	4d
U503	41.05	44.90	4a
U503	44.90	47.53	4d
U503	47.53	51.21	4a
U503	51.21	56.90	1a
U503	56.90	71.80	4d
U503	71.80	72.54	2
U504	0.00	9.30	1a
U504	9.30	11.95	2
U504	11.95	15.75	4d
U504	15.75	18.30	4a
U504	18.30	22.45	4d
U504	22.45	22.75	4c
U504	22.75	22.90	4b
U504	22.90	24.99	7
U505	0.00	7.39	1a
U505	7.39	8.72	2
U505	8.72	12.60	4d
U505	12.60	18.68	4a
U505	18.68	18.97	4d
U505	18.97	19.10	4c
U505	19.10	19.36	4b
U505	19.36	20.73	7
U506	0.00	18.40	1a
U506	18.40	26.90	2
U506	26.90	42.06	4a
U506	42.06	45.95	4c
U506	45.95	49.68	4a
U506	49.68	50.00	4d
U506	50.00	50.65	4c
U506	50.65	50.90	4d
U506	50.90	57.00	5d
U507	0.00	9.80	1a
U507	9.80	11.80	4d
U507	11.80	14.02	4a
U507	14.02	16.10	4d
U507	16.10	16.85	4c
U507	16.85	17.07	4b
U507	17.07	17.22	4a
U507	17.22	18.59	7
U508	0.00	5.60	4d
U508	5.60	12.28	4a
U508	12.28	14.40	4d
U508	14.40	20.93	4a
U508	20.93	22.05	4d
U508	22.05	22.86	4c
U508	22.86	27.43	7
U509	0.00	3.00	4d
U509	3.00	4.42	4a
U509	4.42	5.44	4d
U509	5.44	9.20	4a
U509	9.20	12.21	4d
U509	12.21	12.40	4c
U509	12.40	14.63	7
U510	0.00	1.58	4d
U510	1.58	9.68	4a
U510	9.68	11.02	4d
U510	11.02	11.58	4c
U510	11.58	13.11	4b
U510	13.11	14.63	7
U511	0.00	9.10	4a
U511	9.10	9.48	4d
U511	9.48	9.75	4c
U511	9.75	10.03	4b
U511	10.03	11.28	6b
U512	0.00	1.70	4d
U512	1.70	4.70	4a
U512	4.70	5.20	4d
U512	5.20	6.95	4c
U512	6.95	9.45	6a
U513	0.00	0.76	4d
U513	0.76	2.95	4a
U513	2.95	5.00	4d
U513	5.00	6.10	4c
U513	6.10	7.62	7
U514	0.00	0.40	4d
U514	0.40	5.05	4a
U514	5.05	5.60	4d
U514	5.60	8.70	4c
U514	8.70	11.28	7
U515	0.00	1.40	4a
U515	1.40	4.10	4d
U515	4.10	6.40	4c
U515	6.40	6.90	4b
U515	6.90	7.92	7
U516	0.00	1.05	4d
U516	1.05	5.50	4a
U516	5.50	6.70	4d
U516	6.70	8.10	4c
U516	8.10	9.15	4b
U516	9.15	9.75	7
U517	0.00	1.53	4a
U517	1.53	3.25	4d
U517	3.25	4.05	4c
U517	4.05	4.45	4b
U517	4.45	5.49	7
U518	0.00	1.10	1a
U518	1.10	2.95	4d
U518	2.95	20.02	4a
U518	20.02	26.83	4d
U518	26.83	28.26	4c
U518	28.26	30.18	7
U519	0.00	7.35	4d
U519	7.35	15.30	4a
U519	15.30	15.93	4d
U519	15.93	16.35	4c
U519	16.35	17.68	7
U520	0.00	9.25	4a
U520	9.25	22.40	4d
U520	22.40	22.65	4b
U520	22.65	25.60	7
U521	0.00	15.70	4a
U521	15.70	17.37	7
U522	0.00	2.60	4d
U522	2.60	8.75	4a
U522	8.75	9.44	4d
U522	9.44	10.30	4a
U522	10.30	14.60	4d
U522	14.60	15.75	4c
U522	15.75	17.98	7
U523	0.00	4.72	4a
U523	4.72	5.37	4c
U523	5.37	7.60	4b
U523	7.60	9.14	7
U524	0.00	3.05	4d
U524	3.05	10.75	4a
U524	10.75	13.27	4e
U524	13.27	13.72	4d
U524	13.72	15.64	4a
U524	15.64	16.76	4e
U524	16.76	17.36	4b
U524	17.36	19.81	7
U525	0.00	2.74	4a
U525	2.74	2.90	4b
U525	2.90	3.65	4d
U525	3.65	7.32	4b
U525	7.32	8.84	7
U526	0.00	11.28	4a
U526	11.28	13.32	4d
U526	13.32	17.13	4a
U526	17.13	17.25	4d
U526	17.25	17.30	4d
U526	17.30	18.90	7
U527	0.00	3.40	4a
U527	3.40	3.95	4d
U527	3.95	5.15	4a
U527	5.15	5.30	4d
U527	5.30	6.60	4a
U527	6.60	8.00	4d
U527	8.00	8.45	4a
U527	8.45	8.55	4b
U527	8.55	10.97	7
U528	0.00	4.77	4a
U528	4.77	5.05	4d
U528	5.05	5.70	4a
U528	5.70	7.14	4c
U528	7.14	8.71	4a
U528	8.71	9.10	4c
U528	9.10	10.06	7
U529	0.00	6.75	4a
U529	6.75	7.09	4d
U529	7.09	7.40	4c
U529	7.40	8.60	4a
U529	8.60	11.58	7
U530	0.00	0.30	2
U530	0.30	17.22	4a
U530	17.22	17.48	4d
U530	17.48	19.20	6a
U531	0.00	7.65	4a
U531	7.65	8.90	4c
U531	8.90	9.60	4a
U531	9.60	9.77	4c
U531	9.77	13.11	4b
U532	0.00	1.30	2
U532	1.30	15.31	4a
U532	15.31	15.46	4d
U532	15.46	15.55	4b
U532	15.55	17.37	6a
U533	0.00	4.95	4a
U533	4.95	5.56	4d
U533	5.56	6.08	4c
U533	6.08	9.65	4a
U533	9.65	9.78	4c
U533	9.78	11.90	4a
U533	11.90	12.32	4d
U533	12.32	13.30	4c
U533	13.30	14.50	4b
U533	14.50	16.76	6a
U534	0.00	5.46	4a
U534	5.46	6.82	4c
U534	6.82	7.78	4d
U534	7.78	26.10	4a
U534	26.10	26.35	4c
U534	26.35	28.04	4b
U534	28.04	30.18	6a
U535	0.00	25.91	4a
U535	25.91	27.43	7
U536	0.00	7.25	4a
U536	7.25	10.50	4d
U536	10.50	11.15	4e
U536	11.15	11.58	4b
U536	11.58	13.11	7
U537	0.00	6.85	4a
U537	6.85	7.20	4d
U537	7.20	9.00	4c
U537	9.00	9.30	4b
U537	9.30	11.28	6a
U538	0.00	15.55	4a
U538	15.55	16.00	4c
U538	16.00	16.15	4b
U538	16.15	17.68	6a
U539	0.00	5.45	4a
U539	5.45	6.05	4d
U539	6.05	8.23	6a
U540	0.00	14.70	4a
U540	14.70	18.45	4c
U540	18.45	19.51	6a
U541	0.00	6.80	4a
U541	6.80	7.40	4d
U541	7.40	9.14	6a
U542	0.00	11.15	4a
U542	11.15	12.20	4d
U542	12.20	12.72	4c
U542	12.72	14.02	6a
U543	0.00	2.20	2
U543	2.20	8.53	4a
U543	8.53	9.35	4e
U543	9.35	10.06	4a
U544	0.00	0.45	2
U544	0.45	8.10	4a
U544	8.10	9.60	4d
U544	9.60	12.46	4a
U544	12.46	12.50	4c
U544	12.50	14.02	6a
U545	0.00	4.65	4a
U545	4.65	5.50	4c
U545	5.50	8.23	6a
U546	0.00	4.65	4a
U546	4.65	5.35	4d
U546	5.35	6.20	4c
U546	6.20	7.88	4e
U546	7.88	8.53	4d
U546	8.53	8.83	4b
U546	8.83	10.06	6a
U547	0.00	3.88	4a
U547	3.88	4.23	4c
U547	4.23	6.71	6a
U548	0.00	7.85	4a
U548	7.85	8.38	4d
U548	8.38	8.87	4c
U548	8.87	11.58	6a
U549	0.00	7.95	4a
U549	7.95	8.37	4d
U549	8.37	10.05	4c
U549	10.05	11.89	6a
U550	0.00	5.89	4a
U550	5.89	6.01	4c
U550	6.01	8.54	6a
U551	0.00	8.23	4a
U551	8.23	8.48	4d
U551	8.48	9.76	6a
U552	0.00	1.00	4d
U552	1.00	3.05	4a
U552	3.05	4.28	4d
U552	4.28	5.37	4c
U552	5.37	5.67	4b
U552	5.67	6.10	6a
U553	0.00	4.10	4a
U553	4.10	4.41	4d
U553	4.41	4.78	4b
U553	4.78	5.49	6a
U554	0.00	5.00	4a
U554	5.00	5.15	4c
U554	5.15	9.60	4a
U554	9.60	12.62	4d
U554	12.62	15.24	6a
U555	0.00	3.85	4a
U555	3.85	4.65	4d
U555	4.65	5.61	4a
U555	5.61	6.71	4c

U555	6.71	6.90	4b
U555	6.90	8.23	6a
U556	0.00	17.38	4a
U556	17.38	17.70	4c
U556	17.70	18.45	4a
U556	18.45	33.45	4b
U556	33.45	35.06	6
U557	0.00	4.85	4a
U557	4.85	6.05	4d
U557	6.05	6.75	4a
U557	6.75	7.35	4b
U557	7.35	9.45	6
U558	0.00	25.84	4a
U558	25.84	27.01	4d
U558	27.01	39.62	4b
U558	39.62	41.45	6b
U559	0.00	20.40	4a
U559	20.40	21.34	4c
U559	21.34	22.87	6
U560	0.00	7.93	1a
U560	7.93	13.80	2
U560	13.80	30.95	4a
U560	30.95	31.70	4d
U560	31.70	35.37	4b
U561	0.00	9.80	2
U561	9.80	33.05	4a
U561	33.05	34.60	4b
U561	34.60	36.58	6b
U562	0.00	24.45	1a
U562	24.45	44.25	4a
U562	44.25	49.65	4b
U562	49.65	52.13	6
U563	0.00	13.41	2
U563	13.41	34.86	4a
U563	34.86	42.07	4b
U563	42.07	42.99	6
U564	0.00	31.18	2
U564	31.18	49.52	4a
U564	49.52	50.01	4c
U564	50.01	51.80	4b
U564	51.80	53.96	6
U565	0.00	45.48	1a
U565	45.48	54.26	2
U565	54.26	67.01	4a
U565	67.01	70.12	4b
U566	0.00	34.00	1a
U566	34.00	59.67	4a
U566	59.67	61.59	6
U567	0.00	22.65	1a
U567	22.65	58.20	4a
U567	58.20	58.60	4b
U567	58.60	60.98	6
U568	0.00	12.10	1a
U568	12.10	28.35	4a
U568	28.35	28.61	4d
U568	28.61	28.90	4c
U568	28.90	30.49	6
U569	0.00	8.53	1a
U569	8.53	12.50	4a
U569	12.50	13.00	4d
U569	13.00	29.75	4a
U569	29.75	29.95	4b
U569	29.95	31.70	6
U570	0.00	3.35	1a
U570	3.35	19.18	4a
U570	19.18	19.89	4d
U570	19.89	20.11	4c
U570	20.11	21.10	4a
U570	21.10	24.08	6
U571	0.00	1.55	1a
U571	1.55	9.77	4a
U571	9.77	10.61	4d
U571	10.61	17.59	4a
U571	17.59	19.13	4b
U571	19.13	21.34	6
U572	0.00	0.25	2
U572	0.25	12.40	4a
U572	12.40	13.05	4d
U572	13.05	13.40	4c
U572	13.40	13.55	4b
U572	13.55	14.94	6
U573	0.00	24.50	1a
U573	24.50	37.90	2
U573	37.90	39.40	4a
U573	39.40	42.82	4d
U573	42.82	45.42	6a
U574	0.00	15.34	1a
U574	15.34	24.90	2
U574	24.90	39.40	4a
U574	39.40	42.06	6a
U575	0.00	18.37	1a
U575	18.37	28.35	2
U575	28.35	31.50	4a
U575	31.50	34.00	4d
U575	34.00	35.97	6a
U576	0.00	12.80	1a
U576	12.80	15.90	2
U576	15.90	30.65	4a
U576	30.65	30.75	4b
U576	30.75	32.00	6
U577	0.00	36.50	1a
U577	36.50	45.90	2
U577	45.90	53.30	4a
U577	53.30	53.60	4b
U577	53.60	55.17	6
U578	0.00	26.40	1a
U578	26.40	39.59	4a
U578	39.59	39.75	4b
U578	39.75	41.76	6
U579	0.00	17.06	1a
U579	17.06	17.20	2
U579	17.20	29.80	4a
U579	29.80	30.30	4d
U579	30.30	35.15	4a
U579	35.15	35.85	4b
U579	35.85	37.49	6
U583	0.00	4.15	4a
U583	4.15	6.18	4d
U583	6.18	6.60	4c
U583	6.60	8.23	6
U584	0.00	3.95	4a
U584	3.95	4.70	4d
U584	4.70	4.80	4b
U584	4.80	4.95	4c
U584	4.95	5.05	4b
U584	5.05	6.10	6
U585	0.00	4.40	4a
U585	4.40	5.70	4d
U585	5.70	12.19	4a
U585	12.19	13.72	6
U586	0.00	8.65	4a
U586	8.65	9.75	6
U587	0.00	9.00	4a
U587	9.00	9.50	4d
U587	9.50	9.87	4c
U587	9.87	10.00	4b
U587	10.00	11.28	6
U588	0.00	7.35	4a
U588	7.35	7.85	4b
U588	7.85	9.14	6
U589	0.00	4.55	4a
U589	4.55	5.22	4c
U589	5.22	6.71	6
U590	0.00	1.00	4a
U590	1.00	1.85	4d
U590	1.85	2.15	4c
U590	2.15	3.96	6
U591	0.00	25.40	1a
U591	25.40	37.05	2
U591	37.05	42.55	4a
U591	42.55	46.80	4d
U591	46.80	47.85	4a
U591	47.85	53.20	4a
U591	53.20	61.05	4a
U591	61.05	61.40	4c
U591	61.40	62.33	4d
U591	62.33	65.53	6a
U592	0.00	2.25	2
U592	2.25	8.60	4a
U592	8.60	9.53	4d
U592	9.53	34.10	4a
U592	34.10	34.55	4d
U592	34.55	36.58	6a
U593	0.00	13.63	2
U593	13.63	36.58	4a
U593	36.58	36.85	4d
U593	36.85	38.00	4c
U593	38.00	40.23	6a
U594	0.00	4.85	2
U594	4.85	6.95	4a
U594	6.95	7.43	4d
U594	7.43	24.41	4a
U594	24.41	24.80	4b
U594	24.80	27.13	6a
U595	0.00	8.84	1a
U595	8.84	12.23	2
U595	12.23	26.67	4a
U595	26.67	26.72	4d
U595	26.72	29.87	6a
U596	0.00	12.85	1a
U596	12.85	20.95	4a
U596	20.95	26.00	4b
U596	26.00	28.96	6a
U597	0.00	3.66	1a
U597	3.66	14.94	2
U597	14.94	20.00	4a
U597	20.00	20.95	4c
U597	20.95	23.47	6a
U598	0.00	1.83	1a
U598	1.83	8.03	2
U598	8.03	10.35	4a
U598	10.35	10.50	4b
U598	10.50	12.50	6a
U599	0.00	6.10	1a
U599	6.10	9.30	2
U599	9.30	12.00	4a
U599	12.00	12.19	4c
U599	12.19	13.95	4a
U599	13.95	14.30	4b
U599	14.30	16.76	6a
U600	0.00	3.35	1a
U600	3.35	4.70	2
U600	4.70	6.95	4a
U600	6.95	7.10	4b
U600	7.10	9.45	6a
U601	0.00	40.10	1a
U601	40.10	42.40	2
U601	42.40	52.37	4a
U601	52.37	56.00	4d
U601	56.00	57.00	4a
U601	57.00	57.20	4b
U601	57.20	59.74	6a
U602	0.00	15.00	1a
U602	15.00	42.00	4a
U602	42.00	46.00	4b
U602	46.00	48.77	6a
U603	0.00	24.38	1a
U603	24.38	33.83	2
U603	33.83	44.35	1a
U603	44.35	46.80	2
U603	46.80	51.30	4a
U603	51.30	52.70	4d
U603	52.70	65.86	4a
U603	65.86	66.35	4d
U603	66.35	67.40	4b
U603	67.40	69.80	6a
U604	0.00	14.16	2
U604	14.16	51.20	4a
U605	0.00	14.63	1a
U605	14.63	26.01	2
U605	26.01	44.50	4a
U605	44.50	46.24	4d
U605	46.24	60.40	4a
U605	60.40	61.87	6a
U606	0.00	8.01	1a
U606	8.01	16.58	2
U606	16.58	26.00	4a
U606	26.00	26.85	6a
U607	0.00	17.12	1a
U607	17.12	30.35	2
U607	30.35	32.31	4a
U607	32.31	35.07	4d
U607	35.07	36.88	6a
U608	0.00	13.72	1a
U608	13.72	19.93	2
U608	19.93	31.28	4a
U608	31.28	32.61	6a
U609	0.00	32.21	1a
U609	32.21	33.21	2
U609	33.21	38.10	4a
U609	38.10	41.00	4a
U609	41.00	44.19	6a
U610	0.00	13.98	1a
U610	13.98	30.22	2
U610	30.22	32.50	4a
U610	32.50	36.83	4d
U610	36.83	36.88	4c
U610	36.88	38.40	6a
U611	0.00	41.77	1a
U611	41.77	46.02	4a
U611	46.02	47.50	4d
U611	47.50	48.20	4b
U611	48.20	50.59	6a
U612	0.00	17.05	1a
U612	17.05	27.53	2
U612	27.53	39.93	4a
U612	39.93	41.45	6a
U613A	0.00	38.40	1a
U613A	38.40	40.60	4a
U613A	40.60	42.00	4d
U613A	42.00	42.10	4b
U613A	42.10	44.15	6a
U614	0.00	16.49	1a
U614	16.49	21.95	2
U614	21.95	40.08	4a
U614	40.08	40.43	4b
U614	40.43	41.76	6a
U615	0.00	36.63	1a
U615	36.63	42.98	4a
U615	42.98	45.65	4d
U615	45.65	53.85	4a
U615	53.85	54.71	4d
U615	54.71	61.26	4a
U615	61.26	61.95	4d
U615	61.95	64.31	4a
U615	64.31	65.20	4d
U615	65.20	67.36	6
U616	0.00	42.98	1a
U616	42.98	49.35	2
U616	49.35	77.33	4a
U616	77.33	78.40	4b
U616	78.40	82.30	6
U617	0.00	25.05	1a
U617	25.05	26.53	2
U617	26.53	28.75	4a
U617	28.75	29.80	4d
U617	29.80	30.20	4c
U617	30.20	32.31	6
U618	0.00	8.80	1a
U618	8.80	13.55	2
U618	13.55	15.05	4a
U618	15.05	15.53	4d
U618	15.53	16.35	4a
U618	16.35	18.29	6
U619	0.00	23.17	1a
U619	23.17	29.15	2
U619	29.15	29.80	4a
U619	29.80	30.07	4d
U619	30.07	30.30	4a
U619	30.30	30.40	4b
U619	30.40	32.48	6
U619	32.48	35.37	5b
U620	0.00	12.68	1a
U620	12.68	18.52	2
U620	18.52	20.98	4a
U620	20.98	21.72	4d
U620	21.72	22.70	4c
U620	22.70	26.22	6
U621	0.00	32.38	1a
U621	32.38	34.50	2
U621	34.50	36.72	4a
U621	36.72	38.26	4d
U621	38.26	39.88	4a
U621	39.88	42.35	4c

U621	42.35	45.72	6a
U622	0.00	18.96	1a
U622	18.96	22.20	2
U622	22.20	23.80	4d
U622	23.80	24.77	4a
U622	24.77	25.50	4d
U622	25.50	26.96	4c
U622	26.96	29.26	6a
U623	0.00	37.40	1a
U623	37.40	47.90	2
U623	47.90	48.93	4a
U623	48.93	49.63	4d
U623	49.63	49.84	4c
U623	49.84	53.34	6a
U624	0.00	22.72	1a
U624	22.72	27.15	2
U624	27.15	28.54	4a
U624	28.54	29.36	4d
U624	29.36	31.09	4a
U624	31.09	31.67	4d
U624	31.67	32.07	4c
U624	32.07	35.05	6a
U625	0.00	33.28	1a
U625	33.28	40.70	2
U625	40.70	41.37	4a
U625	41.37	41.89	4d
U625	41.89	42.13	4c
U625	42.13	46.33	6
U626	0.00	25.05	1a
U626	25.05	30.00	2
U626	30.00	33.02	4a
U626	33.02	33.72	4c
U626	33.72	36.59	6
U627	0.00	16.63	1a
U627	16.63	25.16	2
U627	25.16	25.60	4a
U627	25.60	26.15	4d
U627	26.15	26.44	4e
U627	26.44	27.46	4a
U627	27.46	30.48	6
U628	0.00	8.91	1a
U628	8.91	14.54	2
U628	14.54	17.91	4d
U628	17.91	18.65	4c
U628	18.65	21.34	6
U629	0.00	24.62	1a
U629	24.62	27.01	2
U629	27.01	29.45	4a
U629	29.45	32.01	6
U630	0.00	9.50	1a
U630	9.50	14.63	2
U630	14.63	15.80	4d
U630	15.80	16.04	1a
U630	16.04	17.68	4a
U630	17.68	18.76	4c
U630	18.76	21.34	6
U631	0.00	41.80	1a
U631	41.80	42.20	2
U631	42.20	42.65	4a
U631	42.65	43.00	4d
U631	43.00	43.04	4c
U631	43.04	43.32	4b
U631	43.32	46.64	6
U632	0.00	24.15	1a
U632	24.15	24.90	2
U632	24.90	25.45	4a
U632	25.45	26.09	4d
U632	26.09	26.66	4c
U632	26.66	29.27	4b
U633	0.00	45.60	1a
U633	45.60	46.70	4d
U633	46.70	46.79	4c
U633	46.79	48.78	4b
U634	0.00	27.75	1a
U634	27.75	27.92	2
U634	27.92	28.51	4a
U634	28.51	29.14	4d
U634	29.14	29.23	4c
U634	29.23	29.38	4b
U635	0.00	43.28	1a
U635	43.28	50.20	2
U635	50.20	53.11	4a
U635	53.11	53.50	4c
U635	53.50	55.17	6
U636	0.00	96.15	1a
U636	96.15	98.10	4a
U636	98.10	98.42	4b
U636	98.42	101.50	6
U637	0.00	66.35	1a
U637	66.35	68.77	4d
U637	68.77	71.32	6
U638	0.00	63.67	1a
U638	63.67	64.28	4d
U638	64.28	64.83	4a
U638	64.83	65.30	4b
U638	65.30	65.64	4c
U638	65.64	67.67	6
U639	0.00	36.50	1a
U639	36.50	45.00	2
U639	45.00	46.60	4d
U639	46.60	47.35	4c
U639	47.35	49.09	6
U640	0.00	29.60	1a
U640	29.60	31.13	2
U640	31.13	32.85	4a
U640	32.85	33.82	4d
U640	33.82	34.52	4c
U640	34.52	37.19	6
U641	0.00	21.85	1a
U641	21.85	29.00	2
U641	29.00	38.85	4b
U641	38.85	40.54	6
U642	0.00	7.28	1a
U642	7.28	8.20	2
U642	8.20	12.80	4a
U642	12.80	13.56	4d
U642	13.56	15.60	4a
U642	15.60	16.40	4d
U642	16.40	32.43	4a
U642	32.43	33.53	4d
U642	33.53	37.59	4a
U642	37.59	40.54	6
U643	0.00	2.50	1a
U643	2.50	10.70	4a
U643	10.70	12.05	4d
U643	12.05	15.00	4a
U643	15.00	16.10	4b
U643	16.10	19.20	6
U644	0.00	10.06	1a
U644	10.06	15.14	2
U644	15.14	21.42	4a
U644	21.42	25.06	4d
U644	25.06	25.30	4c
U644	25.30	26.40	4b
U644	26.40	28.04	6
U645	0.00	32.90	1a
U645	32.90	33.70	4a
U645	33.70	34.62	4d
U645	34.62	35.16	4c
U645	35.16	36.26	4b
U645	36.26	37.49	6
U646	0.00	33.17	1a
U646	33.17	34.35	2
U646	34.35	34.99	4a
U646	34.99	35.62	4d
U646	35.62	35.78	5
U646	35.78	36.25	4a
U646	36.25	36.80	4b
U646	36.80	38.71	6
U647	0.00	35.10	1a
U647	35.10	36.38	2
U647	36.38	36.90	4a
U647	36.90	37.40	4d
U647	37.40	37.80	4a
U647	37.80	38.08	4b
U647	38.08	41.76	6
U648	0.00	33.15	1a
U648	33.15	34.75	2
U648	34.75	35.35	4d
U648	35.35	36.12	4c
U648	36.12	36.26	4a
U648	36.26	36.60	4b
U648	36.60	39.62	6
U649	0.00	32.50	1a
U649	32.50	35.80	2
U649	35.80	36.35	4d
U649	36.35	36.72	4a
U649	36.72	36.90	4b
U649	36.90	38.10	6
U650	0.00	42.20	1a
U650	42.20	42.38	4a
U650	42.38	43.06	4c
U650	43.06	43.32	4e
U650	43.32	43.42	4c
U650	43.42	45.11	6
U651	0.00	0.96	2
U651	0.96	2.90	4d
U651	2.90	3.52	4c
U651	3.52	3.70	4b
U651	3.70	9.14	6
U804R1H	0.00	13.11	4a
U804R1H	13.11	15.55	6
U804R1H	15.55	21.00	5b
U804R1H	0.00	9.15	4a
U804R1H	9.15	13.72	6
U804R1H	13.72	19.50	5b
U804R1H	0.00	8.23	4a
U804R1H	8.23	12.80	6
U804R1H	12.80	17.40	5b
U804R1H	0.00	6.71	4a
U804R1H	6.71	13.72	6
U804R1H	13.72	16.16	5b
U804R1H	16.16	16.77	5d
U804R1H	16.77	18.90	4d
U804R1H	0.00	6.71	4a
U804R1H	6.71	13.72	6
U804R1H	13.72	22.90	5b
U804R2H	0.00	18.29	4a
U804R2H	18.29	19.51	6
U804R2H	19.51	24.10	5b
U804R2H	0.00	13.72	4a
U804R2H	13.72	15.85	6
U804R2H	15.85	20.40	5b
U804R2H	0.00	12.80	4a
U804R2H	12.80	17.38	6
U804R2H	17.38	18.90	5b
U804R2H	18.90	21.34	6
U804R2H	21.34	24.70	5b
U804R2H	0.00	12.20	4a
U804R2H	12.20	17.68	6
U804R2H	17.68	21.95	5b
U804R2H	21.95	25.00	5d
U804R2H	25.00	28.30	5b
U804R2H	0.00	13.72	6
U804R2H	13.72	16.46	5b
U804R2H	16.46	17.38	5d
U804R2H	17.38	20.70	5b
U804R3H	0.00	11.28	4a
U804R3H	11.28	15.24	6
U804R3H	15.24	21.30	5b
U804R3H	0.00	10.67	4a
U804R3H	10.67	12.20	6
U804R3H	12.20	16.80	5b
U808R1H	0.00	14.02	1a
U808R1H	14.02	15.85	4a
U808R1H	15.85	20.43	6
U808R1H	20.43	30.49	5b
U808R2H	0.00	11.59	1a
U808R2H	11.59	12.80	4a
U808R2H	12.80	19.51	6
U808R2H	19.51	19.82	5b
U808R2H	0.00	10.98	1a
U808R2H	10.98	11.59	4a
U808R2H	11.59	20.43	6
U808R2H	20.43	23.78	5b
U808R3H	0.00	10.89	1a
U808R3H	10.89	11.89	4a
U808R3H	11.89	16.16	6
U808R3H	0.00	8.84	1a
U808R3H	8.84	9.76	4a
U808R3H	9.76	10.67	6
U808R3H	10.67	12.50	5b
U808R3H	12.50	15.85	5d
U808R3H	15.85	17.38	5b
U808R3H	0.00	7.62	1a
U808R3H	7.62	7.93	4a
U808R3H	7.93	11.28	6
U808R3H	11.28	14.33	5b
U808R3H	0.00	6.10	1a
U808R3H	6.10	6.71	4a
U808R3H	6.71	9.45	6
U808R3H	9.45	11.28	5b
U808R3H	0.00	4.27	1a
U808R3H	4.27	5.49	4a
U808R3H	5.49	7.32	6
U808R3H	7.32	9.76	5b
U808R4H	0.00	9.45	1a
U808R4H	9.45	10.06	4a
U808R4H	10.06	16.77	6
U808R4H	16.77	20.73	5b
U808R4H	0.00	8.54	1a
U808R4H	8.54	8.84	4a
U808R4H	8.84	14.02	6
U808R4H	14.02	17.07	5b

Assays

Hole	From	To (m)	%Zn	%Pb
S001	0	1.98	0.7	1
S001	1.98	6.1	0	0
S003	3.15	7.72	0.2	0
S004	1.62	8.63	0.16	0
S005	5.18	7.01	0.5	0
S005	7.01	8.53	2.5	0.4
S006	3.05	10.06	1.28	0.08
S007	8.23	35.66	0	0
S008	3.05	9.14	1.4	0.07
S009	1.22	7.62	0.6	0
S009	7.62	12.8	0.5	0
S010	2.74	5.79	0	0
S011	7.01	28.96	0	0
S012	1.22	7.01	0.85	0.23
S012	7.01	10.67	1.7	0.17
S012	10.67	14.02	0	0.06
S013	16.46	37.8	0	0
S014	1.52	7.62	1.1	0
S015	1.52	5.33	1.26	0.39
S016	2.44	6.4	0.6	0
S017	20.12	20.88	0	0.64
S018	1.83	7.01	0.5	0
S018	7.01	15.24	1.6	0
S018	15.24	19.2	0.25	0
S019	3.05	10.06	0.3	0
S019	10.06	17.68	2.3	0
S019	17.71	20.45	1.4	0
S021	7.62	10.06	0.7	0.35
S021	10.06	13.11	3.25	5.95
S021	13.11	14.02	0.7	0.61
S022	3.05	9.75	1.9	0
S023	13.56	15.54	1.7	0
S023	15.54	18.29	3.75	0.55
S024	6.71	9.14	1.8	0
S024	9.14	14.02	0	0
S024	14.02	15.54	4.75	2.4
S024	15.54	17.22	1.4	0.38
S025	8.53	11.58	1.66	0.26
S026	3.35	4.57	0.15	0.32
S027	14.33	14.63	3.42	0
S028	8.84	24.99	0	0
S030	10.36	11.58	0	0.96
S030	11.58	18.29	0.85	0.24
S031	15.24	17.37	0.7	0
S031	17.37	19.81	0.35	0
S031	19.81	21.49	0.26	0
S032	15.6	20.79	1.7	0
S033	3.05	20.42	0	0
S034	2.74	20.73	0	0
S035	25.91	29.87	12.05	0.78
S036	9.75	26.21	0	0
S037	13.41	19.51	0	0
S038	16.46	17.98	1.86	0
S038	17.98	22.71	3.52	1.2
S040	2.74	35.36	0	0
S041	11.89	23.77	0	0
S042	14.02	17.83	0.6	0.64
S043	17.98	36.58	0	0
S044	25.6	41.76	0	0
S045	23.16	28.96	0	0
S046	22.86	24.38	1.6	0
S046	24.38	26.52	0.5	0
S046	26.53	28.97	0	0
S048	25.6	29.87	0.75	0
S048	29.87	32.61	1.35	0
S049	42.98	43.59	1.8	0
S049	43.59	45.11	0	0
S049	45.11	46.02	1.8	0
S049	46.02	47.82	1.6	0
S049	47.82	49.68	2.2	0
S049	49.68	53.04	1.8	0
S049	53.04	59.13	2.5	0
S050	46.02	49.62	0.4	0
S050	49.62	50.6	0.9	16
S050	50.6	52.12	2.2	0
S050	52.12	55.78	2.2	0
S050	55.78	61.26	2.2	0
S050	61.26	64.92	5.4	0
S050	64.92	69.95	2.6	0
S051	39.93	42.37	0.6	0
S051	42.37	45.72	1	0
S051	45.72	48.77	3	0
S051	48.77	53.34	0.7	0
S052	37.19	77.72	0	0
S054	35.97	39.62	1.5	0
S054	39.62	53.04	0.13	0
S054	53.04	57	0.45	0
S054	57	60.05	0.25	0
S055	39.93	43.28	0.1	0
S055	43.28	43.89	0.3	1.41
S055	43.89	47.55	0	0.07
S055	47.55	57.61	0.3	0
S055	57.61	59.44	0.8	1.6
S055	59.44	60.96	0.8	1.94
S055	60.96	62.79	1.75	0
S055	62.79	68.28	1.6	0
S055	68.28	71.32	6.15	0
S055	71.32	72.54	2.6	0
S055	72.54	74.07	0.5	0
S055	74.07	74.98	3.65	0
S055	74.98	79.55	0.2	0
S056	60.96	106.07	0	0
S057	63.09	67.06	0.1	0
S057	67.06	69.19	1	0.2
S057	69.19	70.41	0.3	0
S057	70.41	74.52	0.8	0
S057	74.52	80.16	0.3	0
S057	80.16	81.08	0.95	1.3
S058	90.22	90.98	0.9	0
S058	90.98	91.9	3.1	0
S058	91.9	95.4	1	0
S058	95.4	99.06	3.2	0
S058	99.06	100.89	1	0
S060	34.44	35.66	0.5	0
S060	35.66	37.64	4.1	0
S060	37.64	39.93	1.4	0
S060	39.93	42.67	0.35	0
S061	36.58	38.4	0.7	0
S061	38.4	41	1.6	0
S061	41	46.94	0.4	0
S061	46.94	48.92	2.4	0
S061	48.92	50.44	0.7	0
S061	50.44	53.34	1.1	0.4
S061	53.34	55.78	3.3	1
S061	55.78	58.83	1.8	11.3
S061	58.83	60.66	0.4	1.6
S062	43.59	48.77	0.4	0
S062	48.77	52.58	0.5	0
S063	92.25	93.93	3.1	0
S063	93.93	94.85	9.1	0.1
S063	94.85	99.87	0.3	0
S064	94.49	121.01	0	0
S065	61.26	62.79	0	0.9
S065	62.79	64.62	0.4	0
S065	64.62	66.45	0.7	0
S065	66.45	67.97	1.6	0
S065	67.97	68.73	0.2	0
S065	68.73	71.32	1.2	0
S065	71.32	72.24	0.25	0
S065	72.24	73.46	3.65	0
S065	73.46	76.81	0.2	0
S069	71.93	73.76	0.32	0.1
S069	73.76	75.59	0.71	0.01
S071	36.58	38.1	0.8	0.01
S071	38.1	39.62	2.45	0.01
S071	39.62	41.15	4.04	1.1
S071	41.15	42.67	2.4	7.51
S071	42.67	44.2	0.98	2.31
S071	44.2	45.72	2.65	0.81
S071	45.72	47.24	2.78	0
S071	47.24	48.77	1.99	0
S071	48.77	50.29	1.49	0
S071	50.29	51.82	0.4	0.1
S071	51.82	53.34	0.4	0.1
S071	53.34	54.86	0.18	0
S071	54.86	56.39	1.91	0.06
S071	56.39	57.91	0.67	0
S071	57.91	59.44	0.09	0
S071	59.44	60.96	0.07	0
S071	60.96	62.03	0.01	0
S072	87.48	96.93	0.02	0
S072	96.93	99.06	0.04	0.04
S072	99.06	100.28	0	0
S072	100.28	101.8	0	0
S072	101.8	102.41	0	0
S072	102.41	103.63	0	0
S072	103.63	104.85	0	0
S072	104.85	105.77	0	0
S074	34.44	78.64	0	0
S075	0	0	0	0
S076	36.58	38.1	0.15	0
S076	38.1	39.62	0.8	0.03
S076	39.62	41.15	0.04	0.03
S076	41.15	42.98	0.03	0.15
S076	42.98	44.2	0.03	0.87
S077	36.58	38.1	0.1	0
S077	38.1	39.93	0	0
S077	39.93	41.45	0.1	0
S077	41.45	42.67	0	0
S077	42.67	46.94	0.55	0.01
S077	46.94	48.46	0	0
S077	48.46	49.99	0.6	0
S077	49.99	51.51	0	0
S077	51.51	53.04	0.18	0.01
S077	53.04	54.56	0	0
S077	54.56	56.08	0.1	0.05
S077	56.08	57.61	0	0
S077	57.61	59.13	0.03	0.03
S078	0	0	0	0
S080	69.49	72.54	0.12	0.01
S080	72.54	77.11	0	0
S080	77.11	78.64	0.18	0.03
S080	78.64	86.56	0	0
S080	86.56	88.09	0	0
S080	88.09	89.31	0	0
S080	89.31	90.83	0.02	0
S081	61.87	63.4	0	0
S082	34.75	37.49	0.02	0.01
S082	37.49	40.23	0.02	0.01
S082	40.23	42.67	0.04	0
S082	42.67	45.11	0.05	0
S082	45.11	46.02	0	0
S082	46.02	46.33	0.03	0
S082	46.33	48.16	0.09	0
S082	48.16	49.99	0.15	0
S082	49.99	50.29	0.04	0
S082	50.29	51.66	0.86	0
S082	51.66	52.18	2.99	0.12
S082	52.18	53.64	2.85	1.85
S082	53.64	54.25	1.76	0
S082	54.25	56.51	1.62	0
S082	56.51	59.74	1.03	0
S082	59.74	60.35	4.58	0
S082	60.35	61.87	0.25	0
S082	61.87	63.4	0	0
S082	63.4	64.62	0	0
S084	22.86	28.04	0	0
S085	36.88	38.1	0.03	0.03
S085	38.1	40.08	0.03	0.01
S085	40.08	42.37	0.01	0.02
S085	42.37	45.11	0.1	0
S085	45.11	46.02	0.08	0
S085	46.02	48.16	0.04	0
S085	48.16	49.68	0.02	0
S085	49.68	51.82	0.01	0
S085	51.82	52.88	0.02	0
S085	52.88	54.86	0.51	0
S085	54.86	56.08	0.4	0
S085	56.08	58.52	0.35	0
S085	58.52	60.96	2.35	0
S085	60.96	61.87	1.27	0
S085	61.87	62.64	0.4	0.06
S085	62.64	63.7	2.11	0.02
S085	63.7	65.23	1.02	0
S085	65.23	66.9	4.37	0.02
S085	66.9	69.19	1	0
S085	69.19	71.63	0.01	0
S086	53.64	75.29	0	0
S087	62.79	64.16	0.02	0.95
S087	64.16	64.47	0.03	0.25
S087	64.47	64.92	0.02	0.96
S087	64.92	65.23	0.1	26.4
S087	65.23	66.75	0.22	2.28
S087	66.75	68.28	0.13	0.68
S087	68.28	69.8	0	0.16
S087	69.8	71.32	0.03	0.09
S087	71.32	71.63	8.6	0.85
S087	71.63	73.15	0.73	0.13
S087	73.15	74.16	0.4	0.29
S087	74.16	74.68	2.17	2.05
S087	74.68	76.2	2.24	0
S088	41.45	43.28	0.04	0.05
S088	43.28	44.5	1.52	0.08
S088	44.5	45.72	11.8	0.58
S088	45.72	47.85	4.44	0.12
S088	47.85	49.07	1.09	0.05
S089	19.81	20.12	0.02	0
S090	31.4	32.93	0.07	0
S090	32.93	38.72	0	0
S090	38.72	40.24	0.14	0
S090	40.24	46.03	0	0
S090	46.03	47.56	0.42	0
S091	83.21	84.12	2.59	0.29
S091	84.12	84.73	6.21	1.68
S091	84.73	86.26	0.58	0.09
S093	148.74	150.27	1.1	1.11
S093	150.27	151.18	1.31	0.69
S093	151.18	152.25	1.28	3.27
S093	152.25	153.92	0.32	0.74
S093	153.92	155.3	4.39	4.92
S094	30.94	32.46	0.06	0.02
S094	32.46	35.66	0.13	0
S094	35.66	37.19	0.14	0
S094	37.19	38.71	0.22	0
S094	38.71	40.54	0.54	0
S094	40.54	42.06	1.81	0
S094	42.06	43.59	0.72	0
S094	43.59	44.81	0.5	2.57
S094	44.81	46.02	0.11	1.81
S094	46.02	47.24	0.1	1.21
S094	47.24	48.92	1.16	1.8
S094	48.92	50.29	2.5	4.05
S094	50.29	51.82	1.68	7.19
S094	51.82	53.19	2.63	1.22
S094	53.19	54.41	1.99	0.06
S094	54.41	55.78	4.82	4.13
S094	55.78	56.08	4.15	5.2
S094	56.08	56.85	2.19	7.58
S094	56.85	58.22	0.57	9.61
S094	58.22	59.74	0.01	0.05
S096	32.61	34.14	0.04	0.05
S096	34.14	36.88	0	0
S096	36.88	38.71	0.1	0
S096	38.71	40.39	0.3	0
S096	40.39	42.37	1.08	0
S096	42.37	44.2	0	0
S096	44.2	45.72	0.49	0
S096	45.72	50.6	0	0
S096	50.6	51.82	0.63	0.03
S096	51.82	53.04	0.87	0.02
S096	53.04	54.1	0.39	0
S096	54.1	54.86	0.69	0
S097	162.15	162.46	1.95	1.25
S098	111.71	112.17	0.01	3.97
S099	127.25	128.63	1.3	1.8
S099	128.63	130.15	0.73	2.19
S099	130.15	131.67	0.67	2.3

S099	131.67	132.44	2.04	4.57
S099	132.44	133.5	5.42	17.5
S099	133.5	134.72	2.29	11.6
S100	37.19	38.71	0.05	0.01
S100	38.71	41.76	0	0
S100	41.76	43.59	0.15	0.03
S100	43.59	46.33	0	0
S100	46.33	47.85	0.08	0.02
S100	47.85	49.38	0.06	0
S100	49.38	51.21	0	0
S100	51.21	52.73	0.53	0
S100	52.73	54.86	0.34	0.23
S100	54.86	56.39	0.43	0.02
S100	56.39	57.91	1.04	0.01
S100	57.91	59.44	2.11	0
S100	59.44	60.96	0.13	0.28
S100	60.96	61.87	0.03	0.07
S100	61.87	63.4	0.2	0.94
S100	63.4	65.23	0.2	0.08
S106	43.59	45.11	0.13	0.03
S106	45.11	49.99	0	0
S106	49.99	51.51	0.07	0
S106	51.51	59.44	0	0
S106	59.44	60.96	0.46	0.04
S106	60.96	64.92	0	0
S106	64.92	66.45	0.26	0.14
S106	66.45	69.49	0	0
S106	69.49	71.02	0.82	0.03
S106	71.02	72.54	0.65	0.04
S106	72.54	74.07	1.34	0.56
S106	74.07	75.59	0.59	1.31
S106	75.59	77.11	0.54	0.51
S106	77.11	77.42	0	0
S106	77.42	78.64	0.55	0.26
S106	78.64	81.84	0	0
S106	81.84	83.36	0.06	0.01
S107	117.71	118.93	2.28	2.41
S107	118.93	120.46	3.87	1.59
S110	70.71	72.39	39.8	20.2
S110	72.39	73.76	15.7	8.48
S110	73.76	75.74	3.74	3.07
S111	66.26	67.36	0	0
S111	109.73	110.95	0.33	0
S111	110.95	112.47	0.01	0
S112	89.76	90.83	0.06	0.29
S112	90.83	92.66	0.38	0.06
S112	92.66	96.16	0	0
S112	96.16	97.23	0.02	0.01
S114	63.4	64.92	0.04	2.95
S114	64.92	65.53	1.75	24
S114	65.53	66.9	0.31	19.6
S114	66.9	67.21	1.55	5.82
S114	67.21	68.58	2.36	21.3
S114	68.58	68.61	1.59	36.7
S114	68.61	70.14	6.05	3.06
S114	70.14	70.6	9.94	0.16
S114	70.6	71.36	3.25	0.06
S114	71.36	72.88	7.92	6.21
S114	72.88	74.41	1.04	5.82
S114	74.41	75.93	0.97	5.28
S114	75.93	77.45	1.17	6.6
S114	77.45	78.98	2.33	1.61
S114	78.98	80.2	1.55	1.78
S114	80.2	81.42	0.3	0.03
S114	81.42	82.48	0	0
S115	28.35	30.78	0.82	0.22
S115	30.78	33.83	0	0
S115	33.83	35.66	0.03	0.15
S115	35.66	37.19	1.49	0.51
S115	37.19	38.25	10.6	0.16
S115	38.25	39.78	3.34	0.04
S115	39.78	40.54	8.25	0.23
S115	40.54	41.45	2.07	0.05
S115	41.45	42.52	0.16	0.08
S115	42.52	43.43	5.33	0.02
S115	43.43	44.2	2.49	0.03
S115	44.2	45.57	1.68	0.04
S117	80.16	80.77	21.8	28.6
S117	80.77	81.99	2.33	9.16
S117	81.99	82.6	0.34	3.86
S119	97.69	98.76	0.02	0.28

S120	32	33.83	0.07	0.04
S120	33.83	35.96	0.09	0.03
S120	35.96	42.05	0	0
S120	42.05	43.58	0.17	0.03
S120	43.58	44.49	1.59	0.03
S120	44.49	46.62	0	0
S120	46.62	48.15	0.13	0.01
S120	48.15	49.67	0	0
S120	49.67	51.2	0.61	0.01
S120	51.2	53.94	0	0
S120	53.94	55.46	0.14	0
S120	55.46	57.29	0.15	0
S120	57.29	58.82	0.09	0.02
S120	58.82	59.73	0	0
S120	59.73	60.65	0	0.18
S120	60.65	62.17	0.02	0.07
S120	62.17	64.91	0	0
S120	64.91	66.44	0.11	0.13
S120	66.44	67.96	0.25	0.14
S120	67.96	68.57	0	0
S120	68.57	70.09	0.02	0.03
S121	81.69	81.99	0.57	0.24
S121	81.99	82.6	0	0
S121	82.6	83.21	0.35	0.47
S121	83.21	83.82	1.19	1.68
S121	83.82	84.43	0.04	0.27
S121	84.43	85.65	0	0
S121	85.65	86.2	3.27	1.13
S121	86.2	86.75	3.85	9.54
S123	51.21	52.73	0.51	2.76
S123	52.73	54.25	1.86	0.08
S123	54.25	55.78	1.66	0.22
S124	41.45	42.98	0.8	0.08
S124	42.98	43.89	3.54	6.28
S124	43.89	45.42	2.2	0.16
S124	45.42	46.33	1.45	0.53
S124	46.33	47.85	0.34	2.21
S124	47.85	49.38	0.51	4.09
S124	49.38	50.9	0.47	1.57
S124	50.9	52.43	0.04	1.55
S125	65.23	65.53	0.8	0.05
S125	65.53	66.6	2.27	1.28
S126	28.96	30.48	0.24	0
S126	30.48	33.68	0	0
S126	33.68	35.2	0.48	0
S126	35.2	38.25	0	0
S126	38.25	39.78	0.45	0
S126	39.78	44.81	0	0
S126	44.81	46.33	0.49	0.02
S127	52.43	52.73	4.23	1.68
S127	52.73	53.64	16.9	7.09
S127	53.64	54.25	10.6	7.14
S127	54.25	55.17	10.4	2.97
S127	55.17	56.24	6.19	2.04
S127	56.24	57.76	0.94	0.78
S128	28.19	29.72	0.71	0
S128	29.72	31.09	0	0
S128	31.09	32.61	0.33	0
S131	42.67	46.33	0.17	0.05
S131	46.33	46.94	3.21	20.6
S131	46.94	47.85	6.83	0.56
S131	47.85	49.38	1.23	0.43
S131	49.38	50.14	0.43	0.02
S131	50.14	50.75	1.58	0.07
S131	50.75	52.27	1.86	0.13
S131	52.27	53.04	5.57	0.22
S131	53.04	53.49	27.4	5.81
S131	53.49	54.1	32.2	4.09
S131	54.1	54.71	29.1	34.3
S131	54.71	55.47	27.4	31
S131	55.47	55.78	26.8	8.52
S131	55.78	56.08	13.9	6.5
S131	56.08	56.84	8.57	3.66
S131	56.84	56.99	15.9	4.92
S131	56.99	57.6	17.8	4.07
S131	57.6	58.21	7.31	0.07
S131	58.21	58.66	8.02	4.28
S131	58.66	60.19	5.06	0.62
S131	60.19	61.71	1.71	0.09
S131	61.71	63.24	0.8	1.74
S131	63.24	64.76	1.01	2.25

S131	64.76	66.28	1.29	0.3
S133	34.75	36.27	0.07	0.03
S133	36.27	38.4	0.66	0.05
S133	38.4	39.31	0.02	0.01
S133	39.31	40.53	0.62	0.03
S133	40.53	41.29	0.25	0.03
S133	41.29	42.36	0.03	0.04
S133	42.36	43.58	2.06	6.88
S133	43.58	45.1	0.52	0.14
S133	45.1	47.08	4.63	1.75
S133	47.08	47.84	7.69	5.94
S133	47.84	49.36	6.31	4.06
S133	49.36	50.88	4.76	13.6
S133	50.88	51.8	4.87	12
S133	51.8	52.41	3.3	7.88
S133	52.41	53.93	2.99	2.69
S133	53.93	55.15	0.21	0.06
S133	55.15	56.67	0.1	0
S137	30.48	32	0.55	0.08
S137	32	44.2	0	0
S137	44.2	45.72	0.44	0.02
S138	0	0	0	0
S140	29.26	30.78	0.96	0
S140	30.78	32	1.29	0.12
S140	32	32.92	0.88	0
S140	32.92	33.83	1.2	0
S140	33.83	35.36	0.31	0.01
S140	35.36	36.88	0.07	0
S141	163.22	164.13	0.44	0.88
S147	152.25	152.55	0.05	0.6
S147	152.55	153.77	0.81	6.64
S147	153.77	154.53	0.02	0.15
S147	154.53	154.84	0.58	4.64
S147	154.84	156.06	0.06	0.1
S147	156.06	157.58	0.07	0.16
S147	157.58	159.11	0.05	0.7
S148	121.31	121.62	0.61	1.24
S148	121.62	121.92	0.51	3.31
S148	121.92	123.14	1.59	0.25
S148	123.14	124.66	2.16	3.81
S148	124.66	125.27	0.2	0.81
S148	125.27	126.19	0.01	0.02
S149	101.5	101.8	8.95	7.25
S149	101.8	102.72	3.48	6.24
S149	102.72	103.94	2.62	3.88
S149	103.94	104.39	1.29	2.95
S149	104.39	104.7	0.56	2.94
S149	104.7	105.77	0.08	0.36
S150	24.38	25.15	3.77	0.02
S150	25.15	26.67	1.87	0.04
S150	25.3	26.21	0.13	0
S150	26.67	28.35	1.78	0.05
S150	28.35	29.57	1.21	0.15
S150	29.57	29.87	1.19	0.4
S150	29.87	30.33	3.11	1.12
S150	30.33	30.94	1.27	0.03
S150	30.94	31.24	1.11	1.35
S150	31.24	31.7	3.14	1.44
S150	31.7	32.77	0.98	0.04
S150	32.77	33.83	0.37	0.01
S150	33.83	34.44	1.15	0.02
S150	34.44	34.75	0.82	0.01
S151	25.3	26.21	0.13	0
S151	26.21	26.52	2.38	0
S151	26.52	28.04	0.25	0
S151	28.04	29.87	0.01	0
S151	29.87	31.39	0	0
S152	41.45	42.67	1.93	0
S152	42.67	44.2	5.74	0
S152	44.2	45.42	3.07	0
S152	45.42	46.02	0.13	0.02
S153	56.69	57.91	2.78	0.24
S153	57.91	58.98	7.12	0.2
S153	58.98	60.35	8.11	8.04
S153	60.35	61.11	1.04	1.43
S153	61.11	62.64	0.92	2.05
S153	62.64	63.09	0.22	1.25
S154	99.21	99.67	2.47	1.38
S154	99.67	100.28	6.67	7.24
S154	100.28	101.5	5.42	11.7
S154	101.5	102.11	4.01	5.48

S162	30.18	31.7	0.4	2.27
S162	31.7	33.22	0.33	0.17
S163	32.61	34.14	2.34	0.02
S163	34.14	35.66	1.46	0.07
S163	35.66	37.19	0.17	2.84
S163	37.19	38.4	0.73	0.57
S163	38.4	39.93	1.61	0
S163	39.93	40.84	1.68	0.09
S163	40.84	42.37	0.76	0.14
S163	42.37	43.28	0.24	0.02
S163	43.28	44.5	1.01	0.1
S163	44.5	45.11	1.14	0
S163	45.11	46.63	7	0.41
S163	46.63	47.85	0.84	1.44
S163	47.85	49.07	0.92	11.4
S163	49.07	49.68	0.13	2.5
S163	49.68	50.9	1.57	11.5
S163	50.9	51.51	1.27	2.72
S163	51.51	52.73	1.63	7.9
S163	52.73	54.25	1.96	1.62
S163A	28.81	29.47	0.02	0.03
S163A	29.47	30.33	0.01	0.01
S163A	30.33	31.85	0.26	0.02
S163A	31.85	33.38	2.05	0
S163A	33.38	34.75	1.26	0.1
S163A	34.75	36.27	1.03	2.5
S163A	36.27	37.8	0.57	0.22
S163A	37.8	39.01	1.11	0
S163A	39.01	40.45	3.59	0
S163A	40.45	41.76	0.63	0.81
S163A	41.76	43.13	0.16	0.29
S163A	43.13	44.5	0.31	0.09
S163A	44.5	46.02	1.15	0
S163A	46.02	47.4	1.8	0
S163A	47.4	48.77	1.43	0.8
S163A	48.77	50.14	1.93	1.6
S163A	50.14	51.36	1.52	1.41
S163A	51.36	52.73	0.93	1.23
S163A	52.73	54.1	0.02	0
S163A	54.1	55.47	0.02	0
S163A	55.47	56.85	0	0
S163A	56.85	58.37	0	0
S163A	58.37	58.73	0	0
S163B	29.41	30.94	0.04	0
S163B	30.94	32.31	0.35	0
S163B	32.31	33.53	0.5	0
S163B	33.53	35.05	1.51	0
S163B	35.05	36.12	1.87	0.02
S163B	36.12	36.88	0.5	1.23
S163B	36.88	37.49	0.48	0.46
S163B	37.49	38.1	0.34	0.18
S163B	38.1	39.62	1.18	0.01
S163B	39.62	40.84	1.94	0.01
S163B	40.84	41.91	2.69	0.02
S163B	41.91	42.98	1.56	0.15
S163B	42.98	44.04	0.35	0.09
S163B	44.04	44.81	0.15	0
S163B	44.81	45.72	3.06	0.02
S163B	45.72	46.63	3.4	1.18
S163B	46.63	48.16	2	5.13
S163B	48.16	49.68	1.1	19.8
S163B	49.68	50.6	1.24	19.3
S163B	50.6	51.66	1.61	11.2
S163B	51.66	53.04	0.55	4.49
S163B	53.04	54.56	1.69	2.18
S163B	54.56	56.08	0.71	0.38
S164	42.67	44.2	1.16	0.08
S164	44.2	45.72	0.87	0.01
S164	45.72	46.63	1.69	0.06
S164	46.63	47.55	1.35	6.46
S164	47.55	49.07	1.1	0.03
S164	49.07	50.29	1.55	0.06
S164	50.29	51.21	1.5	1.44
S164	51.21	52.58	0.48	2.38
S164	52.58	54.1	0.06	4.07
S164	54.1	54.56	2.09	1.75
S170	74.52	74.98	3.14	46.1
S170	74.98	75.9	3.03	1.35
S170	75.9	77.11	4.26	0.09
S170	77.11	77.88	3.45	1.16
S170	77.88	78.64	11.2	4.73

S170	78.64	80.16	2.66	1.13	S180	61.42	62.64	0.55	0.03	S195	19.81	21.34	4.03	0	S198	53.34	53.95	1.78	0.07
S170	80.16	81.69	1.08	0.58	S180	62.64	63.09	1.83	0.15	S195	21.34	22.86	2.15	0	S198	53.95	55.47	2.42	0.03
S170	81.69	83.21	1.16	0.3	S180	63.09	64.01	2.49	0.17	S195	22.86	23.77	1.52	0	S198	55.47	57	5.88	0.08
S170	83.21	84.43	0.93	0.67	S180	64.01	64.62	1.04	2.17	S195	23.77	24.38	1.64	0	S198	57	58.52	1.95	1.23
S171	28.04	28.96	2.07	0	S180	64.62	65.23	0.45	0.35	S195	24.38	25.91	1.11	0	S198	58.52	60.05	1.38	1.77
S171	28.96	29.87	3.33	0.02	S181	56.69	57	0.76	0.02	S195	25.91	27.43	0.22	0	S198	60.05	60.35	3.24	2.3
S171	29.87	31.39	1.18	0.04	S181	57	58.06	0.33	0.03	S195	27.43	28.19	0.11	0	S198	60.35	61.87	4.03	2.85
S171	31.39	32.92	1.78	0	S181	58.06	59.59	2.92	0	S195	28.19	28.8	0.14	0.02	S198	61.87	62.48	11.2	5.08
S171	32.92	34.44	0.72	0	S181	59.59	61.42	1.06	0	S196	17.37	18.9	1.11	0.02	S198	62.48	63.4	4.34	1.28
S171	34.44	35.51	0.94	0	S181	61.42	62.64	0.14	0.01	S196	18.9	20.42	1.42	0.03	S198	63.4	64.62	9.57	1.83
S171	35.51	36.88	1.15	0	S181	62.64	63.7	0.84	0	S196	20.42	22.1	1.43	0.1	S198	64.62	66.14	0.24	0.03
S171	36.88	38.4	0.71	0	S181	63.7	64.62	4.49	0	S196	22.1	23.62	0.53	0.19	S198	66.14	67.36	2.65	0.4
S171	38.4	39.32	0.65	0	S181	64.62	65.84	0.67	0	S196	23.62	25.15	0.7	0.02	S199	74.68	75.44	42.4	13.1
S171	39.32	39.93	0.29	0	S181	65.84	67.36	0.87	0	S196	25.15	26.67	2.05	0.67	S199	75.44	76.5	12.9	1.37
S171	39.93	41.45	0.28	0	S181	67.36	68.58	0.67	0	S196	26.67	28.19	2.94	0.93	S199	76.5	78.03	12.1	4.03
S171	41.45	42.98	0.1	0	S181	68.58	70.1	1.55	0	S196	28.19	29.72	1.82	1.18	S199	78.03	78.33	2.83	0.43
S171	42.98	43.59	0.23	0	S181	70.1	71.32	1.12	0	S196	29.72	31.09	4.91	6.14	S199	78.33	78.82	0.77	0.22
S171	43.59	44.35	1.92	0	S181	71.32	71.93	3.81	0	S196	31.09	32	10.5	1.97	S202	94.18	94.95	0.69	0.93
S171	44.35	45.87	0.87	0	S181	71.93	73.46	0.67	0	S196	32	32.31	0.12	0.05	S202	94.95	95.71	0.22	0.75
S171	45.87	47.4	1.3	0.15	S182	81.99	82.6	2.63	0.66	S196	32.31	33.83	2.44	0.06	S204	188.37	188.61	0.23	1.19
S171	47.4	47.85	1.18	0	S182	82.6	83.52	3.18	0.98	S196	33.83	35.36	0.88	0	S204	188.61	189.13	11.6	5.57
S171	47.85	48.46	0.33	0	S182	83.52	84.43	0.14	0.15	S196A	16.34	17.1	0.26	0.04	S204	189.13	189.43	0.04	0.3
S171	48.46	49.38	0.39	0	S182	84.43	85.65	1.43	0.12	S196A	17.1	18.62	2.52	0.19	S204	189.43	190.96	10.1	7.35
S171	49.38	49.99	0.04	0	S182	85.65	87.17	9.69	0.4	S196A	18.62	20.15	1.82	0	S204	190.96	191.72	11.3	9.39
S171	49.99	51.51	0	0	S182	87.17	88.7	7.25	4.59	S196A	20.15	21.55	1.4	0.31	S204	191.72	192.63	9.04	6.42
S172	22.79	24.01	0.04	0.23	S182	88.7	90.22	8.9	2.24	S196A	21.55	23.07	0.62	0.29	S204	192.63	193.55	1.48	2.58
S174	133.5	134.26	0.13	0.48	S182	90.22	91.44	11.9	3.55	S196A	23.07	24.6	1.18	0.24	S204	193.55	194.01	8.17	1
S174	134.26	134.57	9.61	5.46	S182	91.44	92.96	4.76	2.95	S196A	24.6	25.88	3.99	0.39	S206	150.72	151.03	15.4	47.2
S174	134.57	134.87	8.95	9.13	S183	110.03	110.34	5.77	4.81	S196A	25.88	27.16	1.47	0.41	S206	151.03	151.49	2.67	13.2
S174	134.87	135.18	1.2	0.28	S183	110.34	110.64	2.76	6.55	S196A	27.16	28.62	3.07	0.22	S206	151.49	152.1	1.09	1.38
S174	135.18	136.55	7.37	1.76	S183	110.64	110.86	5.09	8.63	S196A	28.62	29.9	9.07	0.04	S206	152.1	152.4	1.06	5.79
S174	136.55	137.16	6.05	0.74	S183	110.86	111.25	0.71	1.78	S196A	29.9	31.42	1.14	0.01	S208	79.86	80.16	0.34	0.02
S176	57.3	58.22	0.02	0.03	S185	103.94	104.24	49.3	16.8	S196A	31.42	32.95	0.64	0	S208	80.16	80.47	8.62	0.41
S176	58.22	58.83	0.03	0.04	S185	104.24	104.85	12.5	4.78	S196A	32.95	34.02	0.48	0	S208	80.47	80.77	0.62	0
S176	58.83	60.35	0	0	S185	104.85	106.07	2.32	0.28	S196A	34.02	35.54	0.96	0	S208	80.77	81.38	17.77	9.3
S176	60.35	61.26	3.03	2.42	S185	106.07	107.59	0.92	0.09	S196A	35.54	36.48	1.23	0	S208	81.38	82.6	6.2	2.61
S176	61.26	62.79	1.48	0.62	S185	107.59	109.12	0.7	0.03	S196B	18.22	18.9	4.17	0.04	S208	82.6	83.21	1.99	1.88
S176	62.79	63.7	6.88	1.87	S185	109.12	110.64	1.8	0.03	S196B	18.9	19.5	1.29	0.01	S208	83.21	83.67	4.3	0.61
S176	63.7	65.07	2.29	0.14	S185	110.64	110.95	1.21	0.05	S196B	19.5	20.75	2.78	0.12	S209	34.75	36.27	1.12	0.46
S176	65.07	65.84	0.04	0.01	S186	152.86	153.31	0.01	0.28	S196B	20.75	21.97	1.03	0.09	S209	36.27	37.8	0.58	0.12
S176	65.84	66.6	2.95	0.98	S186	153.31	153.92	0	2.29	S196B	21.97	22.89	1.28	0.01	S209	37.8	39.32	1.48	0.06
S176	66.6	67.06	4.68	2.88	S187	121.92	122.22	4.06	0.82	S196B	22.89	23.47	1.5	0.03	S209	39.32	40.54	1.32	0.03
S177	36.12	37.49	0.49	0	S187	122.22	122.74	16.2	56.2	S196B	23.47	24.99	3.74	0.72	S210	35.14	35.84	0.71	0
S177	37.49	38.25	0.89	0	S187	122.74	123.23	7.38	13.5	S196B	24.99	26.52	1.56	0.51	S210	35.84	36.58	4.27	0
S177	38.25	38.86	1.47	0	S187	123.23	123.99	3.36	1.34	S196B	26.52	27.8	2.99	1	S210	36.58	38.1	1.36	0.29
S177	38.86	39.47	0.11	0	S187	123.99	124.72	1.09	3.26	S196B	27.8	29.32	0.9	0.02	S210	38.1	39.62	0.53	0
S177	39.47	41	0.4	0.01	S187	124.72	125.88	1.2	1.48	S196B	29.32	30.84	0.14	0	S210	39.62	41.09	0.49	0
S177	41	42.52	0.16	0.01	S188	89.61	89.95	9.59	0.1	S196B	30.84	32.36	0.93	0.02	S210	41.09	42.67	0.6	0
S177	42.52	43.43	0.35	0.02	S188	89.95	90.62	45.2	0.02	S196B	32.36	33.31	1.81	0.01	S210	42.67	44.14	0.34	0
S177	43.43	44.96	0.07	0.01	S188	90.62	91.35	19.3	1.72	S196B	33.31	34.84	0.36	0.01	S210	44.14	45.57	0.14	0
S177	44.96	46.48	0.22	0.02	S189	35.36	36.88	0.21	0	S196B	34.84	36.36	0.91	0.01	S210	45.57	47.03	0.09	0.01
S177	46.48	47.55	0.37	0.02	S189	36.88	37.49	0.04	0.01	S196B	36.36	37.88	1.33	0	S210	47.03	48.46	0.03	0
S177	47.55	49.07	0.08	0.05	S189	37.49	39.01	0.47	0	S196B	37.88	38.86	0.15	0.01	S210	48.46	49.47	0	0
S177	49.07	50.6	0.25	0.04	S189	39.01	40.54	0.34	0	S196B	38.86	40.35	0.43	0.01	S211	30.63	32.16	0.14	0
S177	50.6	52.12	0.17	0.04	S189	40.54	42.06	0.31	0	S197	21.95	23.77	1.28	0.54	S211	32.16	33.83	0.08	0.01
S177	52.12	53.64	0.04	0	S189	42.06	43.59	0.39	0	S197	23.77	25.3	0.3	0.45	S212	92.66	93.21	0.91	0.07
S177	53.64	55.17	0.07	0.06	S189	43.59	44.5	0.36	0	S197	25.3	25.91	1.13	0	S212	93.21	94.43	2.25	0.51
S177	55.17	56.69	0.43	0.05	S189	44.5	45.72	0.25	0	S197	25.91	26.97	0.97	0.05	S212	94.43	95.19	2.74	0.18
S178	88.7	89	22.5	1.66	S189	45.72	47.09	0.01	0.01	S197	26.97	28.35	0.38	0	S212	95.19	96.87	2.52	0.26
S178	89	89.31	15.9	0.17	S189	47.09	48.62	0.03	0	S197	28.35	29.87	0.55	0.18	S212	96.87	97.81	9.35	3.11
S178	89.31	89.61	23.3	0.03	S189	48.62	50.14	0.03	0	S197	29.87	30.78	0.08	0.02	S212	97.81	99.06	6.55	7.89
S178	89.61	90.53	14.3	10.1	S189	50.14	51.66	0.16	0	S197	30.78	31.7	0.05	0.05	S212	99.06	100.58	10.3	4.69
S178	90.53	90.83	19.6	6.45	S189	51.66	52.43	0.15	0	S197	31.7	33.22	0.09	0.2	S212	100.58	101.96	8.19	3.22
S178	90.83	91.14	2.3	0.04	S189	52.43	53.95	0.37	0	S197	33.22	34.75	0.46	0.02	S213	134.72	135.79	0.12	2.98
S178	91.14	91.74	18.4	1.43	S189	53.95	55.63	0.56	0	S197	34.75	36.27	0.88	0.03	S216	44.44	45.23	0.45	0
S178	91.74	93.27	2.56	4.15	S189	55.63	57.3	1.03	0	S197	36.27	37.8	0.68	0.17	S216	45.23	46.02	1.99	0.01
S178	93.27	94.79	3.61	2.64	S189	57.3	58.83	0.92	0.01	S197	37.8	39.01	0.22	0.42	S216	46.02	47.09	0.44	0.06
S178	94.79	96.32	1.76	1.84	S189	58.83	60.35	1.75	0	S197	39.01	40.54	0.09	0.09	S216	47.09	48.46	0.11	0
S178	96.32	97.84	2.63	8.94	S189	60.35	61.87	1.54	0	S197	40.54	42.06	1.25	0.55	S216	48.46	49.07	0.15	0.06
S178	97.84	99.36	2.54	1.02	S189	61.87	63.34	4.77	0	S197	42.06	43.59	0.04	0.19	S216	49.07	50.6	0.02	0.11
S179	100.28	100.58	14.9	7.94	S189	63.34	64.77	4.47	0	S197	43.59	45.11	0.32	0.2	S216	50.6	52.12	0	0.02
S179	100.58	100.89	47.4	6.82	S189	64.77	66.14	3.84	0	S197	45.11	46.02	1.36	0	S216	52.12	53.64	0.07	0.13
S179	100.89	101.19	23.8	4.71	S189	66.14	67.67	0.65	0	S197	46.02	47.24	4.24	0	S216	53.64	54.86	0.26	0.06
S179	101.19	102.41	3.56	2.25	S193	98.15	98.76	0.08	0.13	S197	47.24	48.77	3.89	0	S216	54.86	56.39	0.99	0.03
S179	102.41	103.48	0.26	0.06	S193	98.76	99.97	0.42	0.24	S197	48.77	49.99	0.37	0.54	S216	56.39	57.91	0.69	1.4
S179	103.48	103.78	7.64	11.3	S193	99.97	101.5	4.76	6.56	S197	49.99	51.51	0.04	0.48	S216	57.91	59.44	0.04	0.25
S179	103.78	104.55	0.98	3.66	S193	101.5	103.02	2.53	8.62	S197	51.51	53.04	0	0.17	S216	59.44	60.23	0.01	0.15
S180	56.69	57.91	0.1	0.5	S193	103.02	104.55	0.14	0.27	S198	47.24	48.77	3.37	0.8	S216	60.23	61.2	0.07	0.54
S180	57.91	58.83	0.56	0.6	S193	104.55	105.46	0.05	0.21	S198	48.77	50.29	1.41	0.03	S216	61.2	61.87	1.61	7.85
S180	58.83	60.05	2.95	0	S195	16.76	18.29	3.25	0	S198	50.29	51.82	0.28	0.02	S216	61.87	62.79	0.94	1.2
S180	60.05	61.42	5.34	0.05	S195	18.29	19.81	3.32	0	S198	51.82	53.34	0.65	0.3	S216	62.79	64.31	0.84	0.83

S217	73.91	74.22	1.3	0.05	S225	90.23	90.83	11.1	3.21	S239	166.73	168.25	0.12	0.01	S258	22.56	23.47	1.66	0
S217	74.22	74.46	0.92	0.02	S226	67.97	69.19	2.02	1.43	S239	168.25	168.8	4.49	0.01	S258	23.47	24.38	1.04	0
S217	74.46	75.99	1.64	0.01	S226	69.19	69.8	1.9	0.43	S239	168.8	169.41	1.12	0.02	S258	24.38	25.3	0.16	0
S217	75.99	77.51	0.74	0	S226	69.8	71.32	0.04	2.86	S240	173.22	173.37	6.35	28.4	S258	25.3	26.21	0.1	0
S217	77.51	78.49	0.83	0	S226	71.32	72.85	0.01	2.48	S240	173.37	173.55	1.59	11.1	S258	26.21	27.13	0.13	0
S217	78.49	79.86	0.45	0	S226	72.85	74.37	0.25	1.38	S240	173.55	174.19	7.47	25.8	S258	27.13	28.35	0.78	0
S218	103.33	104.85	1.06	0.84	S227	60.96	61.57	9.23	69.2	S240	174.19	175.5	2.8	15.8	S259	16.76	17.68	3.56	0.01
S220	35.36	36.58	4	4.96	S227	61.57	62.33	6.69	20.7	S241	150.91	151.39	3.73	1.74	S259	17.68	18.59	3.43	0
S220	36.58	37.8	10.1	10.9	S227	62.33	63.4	0.75	4.49	S243	36.58	39.01	0.57	0.03	S259	18.59	19.51	2.36	0
S220	37.8	39.32	5.69	0.03	S227	63.4	64.31	0.61	3.76	S243	39.01	40.54	0.41	0	S259	19.51	20.73	3.5	0
S220	39.32	40.54	1.2	0	S228	87.33	88.85	0.78	18.4	S243	40.54	42.06	0.87	0	S259	20.73	21.64	1.4	0
S220	40.54	41.61	3.51	0	S228	88.85	89.31	1.81	0.68	S243	42.06	43.59	0.37	0	S259	21.64	22.86	1.34	0
S220	41.61	42.67	2.55	0	S229	108.51	109.12	0.01	0.12	S243	43.59	45.11	0.16	0	S259	22.86	23.77	1.32	0
S220	42.67	44.04	3.36	0	S229	109.12	110.03	0.07	7.55	S243	45.11	46.63	0.03	0	S259	23.77	24.99	2.13	0
S220	44.04	45.11	2.89	0	S229	110.03	110.95	0.03	0.35	S243	46.63	48.16	0.48	0	S266	37.8	39.32	0.23	0.05
S220	45.11	46.63	3.55	0.02	S229	110.95	111.81	0	0.17	S243	48.16	49.38	2.13	0	S266	39.32	40.66	1.08	0
S220	46.63	47.85	0.71	0.02	S231	130.45	131.22	0.97	0.24	S243	49.38	49.8	4.5	0	S266	40.66	41.06	1.06	0
S220	47.85	48.46	0.6	0	S231	131.22	131.98	1.42	0.15	S243	49.8	51.21	1.4	0	S266	41.06	41.7	3.26	0
S220	48.46	49.68	0.87	0	S231	131.98	132.59	0.79	0.03	S245	189.89	190.65	0.29	0.33	S266	41.7	43.22	1.2	0
S220	49.68	50.9	0.15	0	S231	132.59	134.11	3.88	0.01	S246	222.5	222.75	2.09	7.63	S266	43.22	43.59	0.43	0
S220	50.9	51.82	0.15	0	S231	134.11	135.64	0.91	0.14	S246	222.75	222.99	0.75	6.3	S266	43.59	45.05	0.45	0.02
S220	51.82	53.34	0.09	0	S231	135.64	137.16	0.23	0.43	S250	145.42	145.69	9.05	2.08	S266	45.05	46.57	0.3	0.01
S220	53.34	54.86	0.04	0	S231	137.16	138.38	0.06	0.01	S251	105.77	106.22	2.89	0.26	S266	46.57	47.27	0.54	0
S220	54.86	56.39	0.07	0	S232	60.56	60.87	0.59	0.79	S251	106.22	107.02	2.22	0.07	S266	47.27	48.01	0.62	0
S220	56.39	57.91	0.01	0	S232	60.87	61.63	1.97	0.13	S251	107.02	108.02	7.16	0.05	S266	48.01	49.53	1.16	0.11
S220	57.91	58.83	0.07	0	S232	61.63	62.7	2.95	0.08	S251	108.02	108.51	0.78	0.05	S266	49.53	51.05	0.16	0
S220	58.83	59.74	0.29	0	S234	169.62	170.84	3.16	1.15	S251	108.51	109.12	1.38	0.27	S266	51.05	52.58	0.1	0.02
S220	59.74	60.96	0.19	0	S234	170.84	172.36	0.28	0.6	S252	64.01	64.25	12.1	1.64	S266	52.58	54.1	0.74	0
S220	60.96	61.57	0.18	0	S234	172.36	173.58	1.32	0.37	S252	64.25	66.03	6.16	0.55	S266	54.1	55.63	1.06	0
S220	61.57	63.09	0.43	0	S234	173.58	175.11	2.44	1.25	S255	66.45	67.97	1.11	0.03	S266	55.63	57.12	1.97	0.02
S220	63.09	64.01	0.44	0.01	S234	175.11	175.87	1.16	0.45	S255	67.97	68.58	38.2	0.03	S266	57.12	58.64	0.61	0
S220	64.01	64.62	0.03	0.08	S235	28.35	29.11	1.34	0.49	S255	68.58	70.1	1.4	0.37	S266	58.64	60.17	1.57	0
S222	40.84	42.06	0.87	0.01	S235	29.11	30.63	0.11	0.02	S255	70.1	71.63	2.43	0.04	S266	60.17	61.69	1.29	0
S222	42.06	42.98	0.83	0	S235	30.63	32.16	0.15	0.01	S255	71.63	72.54	2.46	0.05	S266	61.69	63.22	2.2	0.01
S222	42.98	44.5	1.63	0	S235	32.16	33.53	0.46	0.01	S255	72.54	73.15	1.03	0.95	S266	63.22	64.74	0.76	0.08
S222	44.5	45.72	1.12	0	S235	33.53	35.05	0.91	0.01	S255	73.15	74.68	0.98	1.17	S266	64.74	66.26	0.5	0
S222	45.72	46.94	1.09	0	S235	35.05	36.58	1.96	0	S255	74.68	76.2	0.05	1.1	S267	33.83	44.5	0	0
S222	46.94	47.85	1.16	0	S235	36.58	36.88	4.12	0	S255	76.2	77.72	0	0.53	S268	73.23	73.84	46.6	3.38
S222	47.85	48.77	1.84	0	S235	36.88	37.49	0.75	0.01	S255	77.72	79.25	0	0.17	S268	73.84	74.15	19.8	0.45
S222	48.77	50.29	1.67	0	S235	37.49	39.01	2.58	0	S255	79.25	80.16	0	0.14	S268	74.15	75.31	8.55	0.2
S222	50.29	51.82	1.97	0	S235	39.01	40.54	5.88	0.19	S255	80.16	81.38	2.17	1.79	S268	75.31	76.77	4.12	0.05
S222	51.82	53.34	1.05	0.03	S235	40.54	42.06	11.7	0	S255	81.38	82.3	0.05	0.28	S268	76.77	78.29	4.58	0.06
S222	53.34	54.86	0.35	0	S235	42.06	43.59	7.76	2.4	S256	17.68	19.2	0.47	0.03	S268	78.29	79.82	2.07	0.06
S222	54.86	56.39	0.13	0.03	S235	43.59	43.89	10.9	0	S256	19.2	20.73	0.65	0.02	S268	79.82	81.34	3.21	0.43
S222	56.39	57.61	0.04	0	S235	43.89	45.42	1.29	0	S256	20.73	22.25	0.09	0.03	S268	81.34	82.47	4.56	1.49
S222	57.61	58.83	0.26	0	S235	45.42	46.94	0.66	0.03	S256	22.25	23.77	1.52	0.02	S268	82.47	82.93	1.64	1.91
S222	58.83	59.59	0.3	0.01	S235	46.94	48.46	1.89	0.01	S256	23.77	25.15	0.73	0.27	S268	82.93	84.36	2.09	1.38
S222	59.59	60.66	0.82	0.05	S235	48.46	49.99	2.42	0.06	S256	25.15	26.52	0.23	0	S268	84.36	85.85	4.25	1.02
S222	60.66	61.26	0.67	0.02	S235	49.99	51.51	2.76	0.03	S256	26.52	28.04	0.76	0.26	S268	85.85	86.61	4.7	0.16
S222	61.26	62.48	0.2	0.12	S235	51.51	51.82	10.8	0	S256	28.04	29.57	0.57	0.19	S268	86.66	88.05	0.74	0.85
S222	62.48	63.09	0.16	0.13	S235	51.82	53.34	2.33	0.02	S256	29.57	31.09	0.02	0.02	S268	88.05	89.57	0.96	0.18
S223	41.91	43.43	0.62	0.02	S235	53.34	54.25	2.91	0.02	S256	31.09	32	0.02	0	S268	89.57	90.85	0.24	0.39
S223	43.43	44.96	0.58	0	S235	54.25	55.78	1.84	0.59	S256	32	33.22	0.93	0.02	S268	90.85	92.37	0.7	0.12
S223	44.96	46.48	1.76	0	S235	55.78	57	0.46	2.86	S256	33.22	34.75	2.84	0.27	S281	49.53	50.29	1.74	0.11
S223	46.48	48.01	1.98	0.02	S235	57	57.91	0.42	3.72	S256	34.75	36.27	3.98	0.06	S281	50.29	51.82	2.71	0.41
S223	48.01	49.53	2.3	0.01	S235	57.91	59.13	0.05	1.49	S256	36.27	37.8	2.67	0.13	S281	51.82	53.04	1.04	0
S223	49.53	50.29	0.99	0.02	S235	59.13	60.66	0.06	3.63	S256	37.8	39.32	4.47	0.43	S281	53.04	53.86	0.65	0.04
S223	50.29	50.9	0	0	S235	60.66	61.87	0.06	1.78	S256	39.32	40.54	4.29	0.02	S281	53.86	55.38	2.72	0.62
S223	50.9	51.97	1.7	0.01	S237	30.18	31.3	0.37	0.33	S256	40.54	42.06	0.49	0.16	S281	55.38	56.91	3.42	0.58
S223	51.97	53.04	2.58	0.03	S237	31.3	32.77	0.26	0.73	S256	42.06	42.98	0.53	0.04	S281	56.91	58	0.5	0.02
S223	53.04	53.64	0	0	S237	32.77	33.22	2.71	2.06	S256	42.98	43.89	0.21	0.13	S281	58	59.59	0.74	0.02
S223	53.64	55.17	1.42	0.01	S237	33.22	34.14	2.32	0.58	S256	43.89	45.42	0.69	0.01	S281	59.59	61.11	0.64	0
S223	55.17	56.69	0.7	0.02	S237	34.14	34.53	7.49	0.17	S256	45.42	46.94	0.76	0.01	S281	61.11	62.64	0.54	0
S223	56.69	58.22	0.67	0	S237	34.53	35.97	3.09	0.6	S256	46.94	48.46	0.53	0	S281	62.64	63.4	0.29	0.03
S223	58.22	59.74	0.86	0	S237	35.97	36.39	7.68	2.75	S257	12.8	14.33	1.65	0.07	S281	63.4	64.62	0.39	0.05
S223	59.74	61.26	1.75	0.02	S237	36.39	37.86	4.08	1.07	S257	14.33	15.85	1.53	0.1	S281	64.62	66.14	0.39	1.69
S223	61.26	62.79	1.98	0	S237	37.86	39.17	3.24	3.71	S257	15.85	17.37	1.69	0.08	S281	66.14	67.67	2.4	3.04
S223	62.79	63.7	5.03	1.76	S237	39.17	40.14	15.3	4	S257	17.37	18.9	1.09	0.04	S281	67.67	68.49	3.77	1.46
S223	63.7	64.31	0	0	S237	40.14	40.84	0.26	2.33	S257	18.9	20.42	0.07	0.02	S281	68.49	70.01	0.88	0.05
S223	64.31	65.84	4.48	0.76	S237	40.84	41.61	0.62	4.41	S257	20.42	21.95	0.21	0.02	S282	36.41	37.94	0.53	0.02
S223	65.84	67.36	1.28	0.01	S237	41.61	41.82	0	0	S257	21.95	23.47	0.78	0	S282	37.94	39.46	2.32	0.02
S223	67.36	68.88	1.17	0	S237	41.82	42.67	4.27	0.44	S257	23.47	24.08	2.11	0	S282	39.46	40.99	1.1	0.18
S223	68.88	70.41	2.61	0.74	S237	42.67	44.2	3.14	0.29	S257	24.08	24.54	3.35	0	S282	40.99	42.05	3.09	0.03
S223	70.41	71.93	2.61	0.78	S237	44.2	44.81	0.21	0.17	S258	14.94	15.85	1.15	0	S282	42.05	42.72	2.83	0.16
S223	71.93	73.46	3.34	0.15	S237	44.81	46.33	2.76	1.35	S258	15.85	17.37	2.01	0	S282	42.72	43.79	4.15	0
S223	73.46	74.98	2.5	0.08	S237	46.33	47.85	1.21	1.06	S258	17.37	18.59	2.45	0	S282	43.79	45.31	2.05	0.06
S223	74.98	76.5	6.23	0.01	S238	146.36	147.43	11.9	0.83	S258	18.59	18.9	1.19	0	S282	45.31	46.11	3.06	0
S223	76.5	78.03	2.32	0.15	S239	164.96	165.05	0.92	0.24	S258	18.9	19.81	1.53	0	S283	62.84	63.24	4.56	0.03
S223	78.03	78.94	2.27	0.07	S239	165.05	165.14	9.25	0.42	S258	19.81	20.73	3.59	0	S283	63.24	63.45	0	0
S223	78.94	80.01	0.29	0.22	S239	165.14	165.2	1.22	0	S258	20.73	21.64	1.56	0	S283	63.45	64.18	21.3	0.06
S225	89.62	90.23	5.6	8.55	S239	165.2	166.73	1.79	0.02	S258	21.64	22.56	1.96	0	S283	64.18	65.67	0.75	0.4

S283	65.67	67.11	0.79	0.93	S295	128.04	128.65	0.99	0.18	S307	33.57	33.84	1.77	0.59	S329	136.41	136.47	22.8	10.2
S283	67.11	68.33	2.62	0.14	S296	30.48	32	0.71	0.01	S307	33.84	33.93	8.36	45.5	S329	136.47	136.8	1.39	0.05
S283	68.33	69.85	3.2	0.39	S296	32	33.83	2.31	0.02	S307	33.93	34.94	18.5	8.69	S330	151.84	152.91	0.06	0.66
S283	69.85	70.28	5.96	0.24	S296	33.83	35.66	1.51	0	S307	34.94	36.4	2.54	0.39	S330	152.91	153.3	1.09	10.8
S283	70.28	71.74	0.5	0.13	S296	35.66	37.19	0.65	0	S307	36.4	37.93	2.15	0.73	S332	37.24	38.76	0.46	0
S283	71.74	73.2	1.99	0.17	S296	37.19	38.71	0.58	0.02	S307	37.93	39.45	2.06	1.33	S332	38.76	40.28	1.59	0
S283	73.2	74.73	4.12	1.28	S296	38.71	40.23	0.2	0	S307	39.45	40.97	4.18	0.08	S332	40.28	40.89	0.51	0
S283	74.73	75.24	0.67	0.13	S296	40.23	41.76	0.01	0.01	S307	40.97	41.65	3.48	0	S332	40.89	41.66	3.69	0.01
S284	80	80.52	0.02	0.02	S296	41.76	43.28	0.03	0.03	S307	41.65	42.1	4.55	0	S332	41.66	42.72	0.44	0
S284	80.52	81.34	9.35	31.1	S296	43.28	44.81	0.23	0.01	S307	42.1	43.63	4.8	0.01	S332	42.72	44.25	0.18	0
S284	81.34	81.68	2.82	2.77	S296	44.81	46.33	0.24	0.01	S307	43.63	44.08	7.32	0.02	S333	49.27	50.18	1.15	0
S284	81.68	82.01	7.99	36	S296	46.33	47.85	0.39	0	S307	44.08	45.15	1.63	0.03	S333	50.18	51.98	1.32	0
S284	82.01	82.38	8.55	1.65	S296	47.85	49.38	0.53	0	S307	45.15	46.67	0.46	0.01	S333	51.98	53.23	1.29	0
S284	82.38	83.2	0.77	0.76	S296	49.38	50.9	0.07	0.01	S307	46.67	48.2	0.45	0.03	S333	53.23	54.6	1.09	0
S285	106.1	107.17	8.71	8.07	S296	50.9	52.43	0.16	0.02	S308	132.44	132.95	0	0.9	S333	54.6	55.67	1.94	0
S286	75.94	76.82	0.31	0.11	S296	52.43	53.95	0.24	0.03	S308	132.95	133.5	0	5.62	S333	55.67	56.73	0.9	0
S286	76.82	77.55	29.4	35.5	S296	53.95	55.78	0.2	0.01	S309	76.14	76.47	1.54	0.07	S333	56.73	57.49	0.34	0
S286	77.55	79.01	50	1.36	S296	55.78	57	0.96	0	S309	76.47	76.87	17.1	15.9	S333	57.49	58.87	0.26	0
S286	79.01	79.9	11.5	0.05	S296	57	57.3	0.04	0	S309	76.87	77.6	5.66	7.15	S333	58.87	59.93	0.45	0
S286	79.9	80.26	2.33	0.05	S296	57.3	59.13	1.62	0	S309	77.6	78.09	5.48	15.3	S334	74.01	74.23	1.05	10.7
S286	80.26	80.81	3.63	0.12	S296	59.13	60.14	0.45	0	S309	78.09	78.33	7.2	2.66	S334	74.23	74.47	2.81	2.23
S287	43.63	45.15	0.02	0	S296	60.14	60.53	1.53	0	S309	78.33	79.49	1.01	1.66	S334	74.47	75.51	1.38	0.32
S287	45.15	46.67	0	0	S296	60.53	61.97	0.44	0	S310	70.62	71.11	2.05	0.26	S334	75.51	75.66	0.72	0.04
S287	46.67	48.2	0	0	S297	31.29	31.72	0.86	0.16	S310	71.11	72.18	6.59	0	S335	80.49	81.28	1.46	0.13
S287	48.2	48.5	0	0	S297	31.72	34.19	7.2	0.94	S310	72.18	73.43	4.81	0	S335	81.28	81.92	2.47	2.36
S287	48.5	50.03	0	0	S297	34.19	36.05	3.33	0.07	S310	73.43	74.61	2.98	0.09	S335	81.92	82.47	0.74	0.4
S287	50.03	50.64	0	0	S297	36.05	37.39	1.85	0	S310	74.61	75.62	1.42	0.52	S336	104.44	104.81	0.49	0.46
S287	50.64	51.25	0	0	S297	37.39	38.61	2.97	0.01	S311	48.46	49.99	0.07	0.02	S336	104.81	105.75	0.02	0.05
S287	51.25	52.77	0	0	S297	38.61	40.74	0.94	0	S311	49.99	51.51	0.13	0.16	S336	105.75	106.97	6.09	5.07
S287	52.77	54.29	0	0	S297	40.74	42.42	2.3	0.02	S311	51.51	53.04	0.05	0.03	S336	106.97	108.16	2.76	3.57
S287	54.29	54.9	0	0	S297	42.42	44.55	0.95	0	S311	53.04	54.56	0.03	0.02	S337	115.54	128.32	0	0
S287	54.9	56.43	0	0	S297	44.55	46.68	0.06	0	S311	54.56	56.08	0.04	0	S339	24.72	25.94	2.1	0
S287	56.43	57.95	0	0.01	S297	46.68	49.12	0.14	0	S311	56.08	57.61	0.09	0	S339	25.94	26.7	2.55	0.11
S287	57.95	59.48	0	0	S297	49.12	51.93	0.18	0	S311	57.61	58.22	0.16	0.01	S339	26.7	28.07	1.18	0
S287	59.48	61	0	0.01	S297	51.93	52.26	11.3	0	S311	58.22	58.98	0.56	0.25	S339	28.07	29.6	1.72	0
S287	61	62.52	0	0	S297	52.26	54.61	1.24	0	S311	58.98	60.35	0.07	0.01	S339	29.6	30.51	1.09	0.02
S287	62.52	64.05	0	0	S297	54.61	56.74	0.9	0	S312	114.98	115.22	1.22	3.69	S339	30.51	32.03	2.5	0
S287	64.05	65.57	0	0	S297	56.74	59.61	1.19	0	S312	115.22	115.99	2.91	3.36	S339	32.03	33.41	0.73	0
S287	65.57	67.1	0	0	S297	59.61	61.01	0.43	0	S312	115.99	116.75	0.43	0.31	S340	0	93.88	0	0
S287	67.1	68.08	0	0	S297	61.01	62.29	0.55	0	S312	116.75	118.42	0.05	0.18	S341	44.79	45.94	1.96	0
S287	68.08	69.53	0	0	S297	62.29	64.18	0.74	0.06	S313	139.17	139.63	1.84	0.02	S342	19.37	19.62	0.87	0
S287	69.53	70.75	0.06	0.02	S297	64.18	66.4	0.04	0.05	S314	147.5	147.66	0.06	0.51	S342	19.62	20.65	2.01	0
S287	70.75	71.36	52.8	0.26	S297	66.4	67.78	0.82	0.02	S314	147.66	148.75	2.47	5.69	S342	20.65	22.03	2.14	0
S287	71.36	71.82	8.42	2.78	S298	67.85	68.06	0.08	0	S314	148.75	150.28	2.84	4.02	S342	22.03	22.3	0.53	0
S287	71.82	73.13	7.69	9.98	S298	68.06	68.7	1.78	0	S315	152.56	152.84	1.46	1.22	S342	22.3	23.55	0.43	0
S287	73.13	73.89	1.84	3.33	S298	68.7	69.31	5.29	0	S316	114.6	115.07	0.79	0.55	S342	23.55	25.04	2.71	0
S287	73.89	75.2	2.4	2.99	S299	81.57	82.58	3.85	2.45	S317	6.1	68.56	0	0	S342	25.04	26.26	0.7	0
S287	75.2	75.94	0.7	0.81	S299	82.58	83.19	0.04	0.04	S318	29.25	29.86	1.42	0.04	S342	26.26	27.45	0.77	0
S288	93.53	94.14	0.09	0.02	S300	48.16	61.57	0	0	S318	29.86	31.08	0.67	0	S342	27.45	27.76	1.33	0
S288	94.14	94.81	0.35	0.17	S301	78.64	79.24	46	16.4	S318	31.08	31.84	1.81	0	S342	27.76	28.55	0.18	0
S288	94.81	96.49	4.51	0.12	S301	79.24	79.85	0.25	0.18	S319	10.06	12.19	0	0	S342	28.55	28.85	5.48	0
S288	96.49	96.64	10.5	0.1	S301	79.85	80.21	46.3	0.01	S320	93.89	95.41	2.06	0.62	S342	28.85	29.8	0.46	0
S288	96.64	97.56	3.29	4.12	S301	80.21	80.91	17.7	0.04	S321	50.28	51.65	0.37	0.08	S343	6.1	14.59	0	0
S288	97.56	98.17	5.51	0.67	S301	80.91	81.65	2.63	0.05	S321	51.65	52.51	2.08	0.03	S344	49.55	50.37	0.52	0
S288	98.17	99.66	1	1.2	S301	81.65	83.17	1.5	0.05	S321	52.51	53.94	1.31	0.01	S344	50.37	50.62	1.45	0
S289	114.44	115.87	0.14	0.06	S301	83.17	84.24	4.94	1.79	S321	53.94	55.46	0.21	0.02	S346	149.05	153.92	0	0
S289	115.87	116.42	29.9	2.33	S302	112.38	113.17	0.93	1.61	S321	55.46	56.99	2.83	0.1	S347	24.32	25.12	0	0
S289	116.42	117.61	10.3	0	S302	113.17	113.54	1.82	4.63	S321	56.99	58.51	2.12	0.01	S348	54.25	54.96	0.13	0.6
S289	117.61	118.16	0.9	0.03	S302	113.54	113.96	1.35	24.8	S321	58.51	60.04	1.21	0	S349	79.11	80.17	0.36	0.58
S290	125.03	126.8	0.2	0.11	S302	113.96	114.7	1.64	0.88	S321	60.04	61.56	1.5	0	S349	80.17	80.84	0.12	0.64
S290	126.8	128.32	8.5	4.34	S302	114.7	116.16	0.31	0.7	S321	61.56	63.84	2.01	0	S349	80.84	81.7	0.16	3.18
S290	128.32	128.56	3.13	1.09	S302	116.16	116.77	5.07	10	S321	63.84	64.21	1.39	0.01	S349	81.7	82.61	1.16	2.2
S290	128.56	129.63	2.31	0.15	S303	125.27	126.08	2.85	4.86	S321	64.61	65.52	1.05	0	S349	82.61	83.27	0.97	1.49
S290	129.63	130.45	4.34	0.8	S303	126.08	126.38	0.02	0.12	S321	65.52	66.44	0.62	0	S349	83.27	83.68	2.19	0.81
S290	130.45	131.98	10.8	2.09	S303	126.38	126.75	0.85	5.31	S321	66.44	67.29	1.34	0	S349	83.68	84.35	3.93	1.45
S290	131.98	133.5	1.55	0.09	S304	87.29	88.36	3.22	0.25	S321	67.29	67.96	0.8	0	S349	84.35	85.05	0.82	1.02
S290	133.5	134.72	0.14	0.01	S304	88.36	89.03	5.4	0.2	S321	67.96	69.48	0.41	0.05	S350	161.44	161.63	4.99	3.38
S290	134.72	135.64	7.32	0.49	S304	89.03	89.73	2.34	0.73	S321	69.48	70.09	0.12	0.38	S350	161.63	161.93	4.64	5.86
S290	135.64	136.89	3.4	0.01	S304	89.73	90.4	0.91	1.43	S322	30.18	57.91	0	0	S351	129.47	130.14	4.08	3.67
S290	136.89	137.34	7.65	0	S304	90.4	91.5	3.35	4.21	S323	26.21	44.81	0	0	S351	130.14	130.75	1.03	1.32
S291	26.52	138.38	0	0	S304	91.5	91.71	1.91	0.67	S324	22.56	67.36	0	0	S352	109.2	109.32	0.2	0.17
S292	137.8	138.17	0.18	2.12	S304	91.71	91.99	4.78	1.45	S325	39.62	59.71	0	0	S352	109.32	109.41	34.3	8.49
S292	138.17	138.71	0.02	0.13	S306	63.98	64.83	9.36	0.14	S326	36.58	63.36	0	0	S352	109.41	109.87	3.62	0.04
S292	138.71	140.24	0.23	0.32	S306	64.83	65.72	3.92	0.19	S328	111.7	111.85	2.25	2.34	S352	109.87	110.02	55.5	0.39
S292	140.24	140.39	0.02	0.45	S306	65.72	65.96	12	3.05	S328	111.85	113.34	0.34	0.03	S352	110.02	110.33	15	4.14
S292	140.39	140.63	0.01	1.47	S306	65.96	66.23	2.66	0.42	S328	113.34	114.17	1.01	0.02	S352	110.33	110.75	2.19	0.33
S293	179.83	179.98	4.14	0.97	S306	66.23	66.54	0.07	0.15	S328	114.17	115.05	0.79	0.14	S353	96.18	96.82	0.29	0.06
S295	120.11	120.42	0.08	1.12	S306	66.54	67.33	3.54	1.22	S328	115.05	115.97	4.94	0	S353	96.82	97.19	10.8	0
S295	120.42	126.51	0	0	S307	29.91	31.43	0.64	0.4	S328	115.97	116.27	1.04	0	S353	97.19	97.65	5.63	0
S295	126.51	126.97	0.24	2.03	S307	31.43	32.96	0.39	0.62	S329	124.7	124.73	0.03	0.02	S353	97.65	98.1	5.14	4.47
S295	126.97	128.04	3.56	2.59	S307	32.96	33.57	1.37	0.36	S329	124.73	136.41	0	0	S354	67.56	67.78	0.9	0.02

S354	67.78	68.3	0.54	0.03	S372	268.58	286.51	0	0	S393	25.84	26.99	0.38	0.83	S416	31.44	32.66	1.36	0
S354	68.3	69.15	0.37	0.02	S374	71.48	71.63	0	0	S393	26.99	29.4	0.42	0.08	S416	32.66	34.19	0.51	0
S354	69.15	69.36	0.68	0.01	S374	77.11	77.72	0	0	S393	29.4	31.57	0.4	0.31	S417	26.87	27.21	1.83	0.01
S354	69.36	69.88	0.18	0.03	S377	111.1	111.4	0.02	0.02	S393	31.57	32.3	1.4	0.04	S417	27.21	27.57	0	0
S354	69.88	70.52	1.88	0	S377	111.4	112.26	0	0.03	S393	32.3	33.82	4.96	0.77	S417	27.57	28.4	0.35	0.01
S354	70.52	70.98	8.64	1.52	S377	112.26	113.78	0	0	S393	33.82	34.95	1.24	0.56	S417	28.4	29.19	0.37	0.01
S354	70.98	71.5	6.02	0.08	S377	116.74	117.04	0	0	S393	34.95	36.32	1.99	0.46	S417	29.19	30.04	0.53	0
S354	71.5	72.11	14.4	0.41	S377	117.96	119.48	0	0	S394	23.1	25.6	0	0	S417	30.04	31.44	1.61	0
S354	72.11	72.26	0.46	0.03	S379	150.16	151.64	0	0	S395	24.38	25.91	0	0	S417	31.44	32.66	1.34	0
S354	72.26	72.75	2.52	0	S379	151.64	151.84	20.5	16.8	S396	16.46	18.29	0	0	S417	32.66	34.19	0.24	0
S354	72.75	73.29	0.08	0	S379	151.84	152.15	8.67	4.42	S397	16.76	24.69	0	0	S420	53.09	53.73	0.41	0.75
S354	73.29	73.72	2.6	0	S379	152.15	153.67	0.08	0.08	S398	87.28	87.83	1.24	0.04	S420	53.73	54.7	0.33	0.51
S354	73.72	74.33	1.16	0	S380	25.35	25.84	2.63	0	S398	87.83	88.29	2.95	0.66	S420	54.7	55.4	0.59	0.14
S355	38.25	38.5	3.07	0.01	S380	25.84	26.45	1.37	0	S398	88.29	89.84	0.58	0.98	S420	55.4	55.62	0.45	0.75
S355	38.5	38.68	0.27	0	S380	26.45	26.72	2.22	0	S398	89.84	90.73	2.8	2.09	S420	55.62	55.83	0.19	0.19
S355	38.68	39.44	3.47	0	S380	26.72	28.55	3.73	0	S400	24.22	26.35	0.31	0	S420	55.83	57.96	0	0
S355	39.44	40.29	2.82	0	S380	28.55	29.34	4.62	0	S400	26.35	27.88	0.51	0	S420	57.96	59.49	7.65	0.03
S355	40.29	40.87	2.46	0	S380	29.34	29.77	0.58	0	S400	27.88	29.4	0.22	0	S420	59.49	61.01	14.6	0.04
S355	40.87	41.48	0.9	0	S380	29.77	30.1	3.67	0	S400	29.4	30.93	0.45	0	S420	61.01	62.38	8.33	0.03
S355	41.48	42.06	0.63	0	S380	30.1	30.9	0.75	0	S400	30.93	31.35	0.23	0.12	S420	62.38	62.84	0.22	0.02
S356	29.12	29.61	0.85	0.03	S380	30.9	31.38	0.27	0	S400	31.35	31.6	0.76	2.51	S420	62.84	63.88	5.27	0.56
S356	29.61	29.91	2.13	0.01	S380	31.38	32.97	0.52	0	S400	31.6	32.05	0.07	0.05	S420	63.88	64.06	0.12	0.05
S356	29.91	30.18	0.56	0	S380	32.97	34.49	0.49	0	S401	16.3	40.89	0	0	S420	64.06	65.28	2.8	2.15
S356	30.18	30.55	1.74	0	S380	34.49	35.86	0.48	0	S402	23.67	51.44	0	0	S420	65.28	66.04	0.59	0.71
S356	30.55	31.56	0.38	0	S380	35.86	37.54	0.13	0	S404	40.89	41.35	2.69	2.78	S420	66.04	66.47	0.83	4.04
S356	31.56	32.01	0.37	0	S380	37.54	39.06	0.18	0	S404	41.35	42.81	0.9	0.42	S420	66.47	66.86	0.05	0.09
S356	32.01	32.2	1.89	0	S380	39.06	40.59	0.95	0	S404	42.81	44.34	1.78	0.69	S420	66.86	68.33	2.32	4.99
S356	32.2	33.72	0.18	0	S380	40.59	42.11	0.48	0	S404	44.34	44.86	1.95	0.03	S420	68.33	68.51	1.31	1.97
S356	33.72	35.24	0.13	0	S380	42.11	43.21	0.3	0	S404	44.86	46.38	1.9	0.05	S420	68.51	69.33	0.02	0.03
S356	35.24	36.77	0.13	0	S380	43.21	44.73	1.07	0	S404	46.38	47.54	1.89	0.24	S420	69.33	70.09	0.67	3.15
S356	36.77	37.68	0.11	0	S380	44.73	46.78	0.07	0	S404	47.54	47.78	2.46	0.12	S420	70.09	70.79	0.16	0.03
S356	37.68	38.2	0.54	0	S381	156.75	157.75	0.34	1	S404	47.78	48.45	4.29	0.27	S421	29.01	29.31	2.74	0
S356	38.2	38.44	0.03	0.02	S382	198.47	199.08	0.7	1.82	S404	48.45	49.43	1.83	0.11	S421	29.31	32.63	0	0
S356	38.44	38.75	0.84	0	S383	195.73	196.28	2.11	0.88	S404	49.43	49.58	1.47	0.93	S421	32.63	32.82	0.23	0
S356	38.75	39.21	3.11	0	S383	196.28	196.86	0.03	0.03	S404	49.58	50.49	2.87	0.46	S421	32.82	33.88	1.46	0
S356	39.21	39.6	1.31	0	S384	133.95	134.1	1.24	0.2	S404	50.49	52.02	3.3	0.05	S421	33.88	35.1	0.83	0
S358	105.92	106.1	1.38	0.32	S384	134.1	135.14	5.23	0.02	S404	52.02	53.54	2.65	0.08	S421	35.1	36.63	0.78	0
S358	106.1	106.62	0.15	0.05	S384	135.14	136.3	0.11	0.02	S404	53.54	54.09	0.97	0	S422	27.13	34.14	0	0
S358	106.62	107.47	0.72	0.09	S384	136.3	136.78	3.39	0.1	S410	103.38	106.12	0	0	S423	125.11	126.12	15.6	4.81
S358	107.47	108.29	0.02	0.02	S385	130.5	130.81	0	0	S411	83.53	84.24	1.26	0.01	S423	126.12	126.91	2.61	0.03
S358	108.29	109	1.37	0.04	S386	149.17	149.46	36.3	29.7	S411	84.24	84.54	3.21	0.01	S423	126.91	127.64	2.48	7.43
S358	109	109.91	0.69	0.7	S386	149.46	149.89	2.5	0.29	S411	84.54	84.95	0.7	0	S423	127.64	128.04	10.2	4.4
S359	132.3	132.58	14.5	57.8	S387	149.19	149.8	3.6	4	S411	84.95	85.1	1.64	0	S423	128.04	128.65	0	0
S359	132.58	132.76	47.1	11.4	S388	109.93	111.09	7.3	3.03	S412	89.97	90.73	8.58	3.07	S423	128.65	129.68	14.2	7.69
S359	132.76	133.07	3.66	0.11	S388	111.09	112.22	1.68	0.04	S412	90.73	91.49	11.9	1.49	S423	129.68	130.99	13	8.14
S359	133.07	134.59	3.26	0.04	S388	112.22	113.74	5.27	3.2	S412	91.49	92.71	5.38	1.14	S423	130.99	131.88	7.22	9.89
S360	124.84	125.6	0	0.03	S389	68.93	70.15	0.88	0.13	S412	92.71	93.72	2.88	0.11	S423	131.88	133.37	0.35	0.58
S360	125.6	126.21	0	4	S389	70.18	70.46	0.24	0.08	S413	98.76	99.97	1.1	0.3	S423	133.37	133.67	0.3	0.28
S360	126.21	127.12	0	0.96	S389	70.46	71.37	0.79	0.31	S413	99.97	100.58	3.13	4.17	S425	139.04	140.56	0.61	0.19
S362	116.14	116.75	0.26	1.36	S389	71.37	71.83	0.99	0.2	S413	100.58	101.96	2.42	1.65	S425	140.56	142.09	0.88	0.3
S362	116.75	117.91	0.3	0.18	S389	71.83	73.26	5.73	1.61	S413	101.96	103.02	0.31	0.34	S425	142.09	142.85	1.42	0.62
S363	98.31	98.67	0.46	0.52	S389	73.26	74.73	0.56	0.55	S413	103.02	103.94	0.04	0.44	S425	142.85	144.22	4.3	0.59
S363	98.67	99.83	2.17	2.88	S389	74.73	75.4	3.43	4.86	S413	103.94	104.33	8.7	29.9	S425	144.22	144.98	4.18	4.87
S364	114.5	115.26	3.43	4.87	S389	75.4	76.25	2.26	0.77	S413	104.33	105.34	1.87	5.52	S425	144.98	146.02	0.6	1.82
S365	118.9	119.25	0.59	0.22	S389	76.25	77.5	1.7	0.34	S413	105.34	106.07	1.41	1.96	S425	146.02	146.23	0.74	0.26
S365	119.25	120.25	6.88	1.41	S389	77.5	78.57	6.04	7.11	S413	106.07	107.52	3.05	4.34	S425	146.23	146.87	0.04	1.04
S365	120.25	120.56	1.35	3.13	S389	78.57	79.36	5.04	3.35	S413	107.52	108.13	0.26	0.23	S425	146.87	147.27	1.18	3.42
S365	120.56	122.27	0.09	0.04	S389	79.36	80.27	0.29	0.53	S414	68.33	69.54	1.29	0.46	S426	135.08	136.45	0.17	0.12
S365	122.27	123.33	5.67	8.53	S390	45.47	46.38	4.55	0.04	S414	69.54	70.15	0.28	0.04	S426	136.45	137.27	0.25	0.47
S365	123.33	124.28	3.07	8.43	S390	46.38	47.9	8.79	0.06	S414	70.15	71.68	2.22	0	S427	48.03	48.27	2.49	0.04
S367	100.19	101.64	6.48	9	S390	47.9	48.91	3.1	0.03	S414	71.68	72.47	0.47	0	S427	48.27	48.36	0.55	0.11
S367	101.64	102.07	22.9	17.4	S390	48.91	50.34	2.22	0.06	S414	72.47	73.26	1.93	0	S427	48.36	48.82	2.23	0.01
S367	102.07	103.62	1.6	2.31	S390	50.34	50.95	8.77	0.48	S414	73.26	74.12	3.31	0	S427	48.82	49.67	2.05	1.1
S367	103.62	104.84	8.61	1.82	S390	50.95	51.84	8.12	4.85	S414	74.12	74.57	1.12	0	S427	49.67	50.49	3.37	2.92
S367	104.84	106.03	9.41	5.06	S390	51.84	52.87	2.62	0.41	S415	29.01	30.53	5.41	0	S427	50.49	51.32	6.12	6.57
S367	106.03	106.64	7.86	9.06	S390	52.87	53.21	2.05	0.49	S415	30.53	32.05	1.25	0.01	S427	51.32	51.87	6.47	0.31
S367	106.64	107.71	4.22	1.79	S390	53.21	53.79	2.7	0.32	S415	32.05	33.58	2.73	0	S427	51.87	53.39	0.07	0.01
S367	107.71	109.35	1.74	1.33	S390	53.79	55.07	2.1	0.17	S415	33.58	33.88	1.95	0	S428	57.96	58.27	5.22	1.11
S367	109.35	110.05	8.72	18.3	S391	138.58	138.83	12.8	0.1	S415	33.88	35.41	1.55	0	S428	58.27	58.57	6.07	0.82
S367	110.05	110.42	3.4	2.91	S391	138.83	139.89	0.77	0.1	S415	35.41	36.93	1.15	0	S428	58.57	59.49	3.38	4.59
S368	79.9	81.42	2.31	0.06	S391	139.89	140.17	14.2	0	S415	36.93	37.97	1.16	0	S428	59.49	60.43	4.78	3.39
S368	81.42	82.95	1.92	0.09	S392	113.95	115.42	5.46	0.83	S415	37.97	39.37	1.16	0	S428	60.43	61.62	1.25	0.83
S368	82.95	83.8	6.1	4	S392	115.42	116.85	3.94	0.1	S415	39.37	40.44	0.06	0.13	S428	61.62	63.14	1.42	2.54
S368	83.8	83.98	5.84	1.26	S392	116.85	118.62	14.5	4.95	S415	40.44	41.21	0.03	0.03	S429	81.07	82.59	0.02	0.02
S368	83.98	84.77	8.08	0.13	S392	118.62	120.14	0.08	0.04	S415	41.21	42.36	0.03	0.08	S429	82.59	83.26	16.9	10.8
S368	84.77	86.3	3.52	0	S392	120.14	120.29	31	1.96	S415	42.36	43.64	0.02	0.03	S429	83.26	83.63	1.16	0.05
S368	86.3	87.52	3.17	0	S392	120.29	121.73	4.41	1.5	S415	43.64	45.16	0	0	S429	83.63	84.54	5.42	2.54
S368	87.52	88.74	3.36	0.07	S392	121.73	123.34	2.53	0.34	S416	27.18	28.7	1.2	0	S429	84.54	85.03	5.25	2.7
S368	88.74	90.26	0.06	0.34	S393	21.39	22.91	1.8	0.06	S416	28.7	29.31	1.86	0	S429	85.03	85.45	1.34	2.1
S369	18.6	39.36	0	0	S393	22.91	24.74	1.76	0.06	S416	29.31	30.04	2.21	0	S429	85.45	85.58	14	2.28
S370	134.4	191.07	0	0	S393	24.74	25.84	3.52	0.77	S416	30.04	31.44	2.25	0	S429	85.58	85.77	7.56	10.4

S429	85.77	86.87	0.18	0.17
S430	71.07	71.56	20.2	26.9
S430	71.56	72.44	22.6	49.3
S430	72.44	72.69	24.9	1.86
S430	72.69	73.46	3.53	1.53
S431	47.45	48.82	0.36	0.09
S431	48.82	49.73	0.85	0.03
S431	49.73	51.2	1.33	0.01
S431	51.2	51.38	6.39	0.04
S431	51.38	52.78	0.87	0.06
S431	52.78	54.3	0.88	0.05
S431	54.3	55.1	0.9	0.02
S431	55.1	56.13	0.58	0.01
S431	56.13	57.66	1.64	0.03
S431	57.66	58.57	2.56	0
S431	58.57	59.79	2.36	0.01
S431	59.79	61.25	2.01	0
S431	61.25	62.53	3.5	0
S431	62.53	63.75	2.92	0
S431	63.75	65.12	3.45	0.02
S431	65.12	65.89	3.2	0.34
S431	65.89	66.19	1.36	0.1
S431	66.19	67.41	3.62	1.07
S431	67.41	68.93	2.54	1.69
S431	68.93	70.15	1.2	0.19
S431	70.15	71.37	1.86	1.5
S431	71.37	72.59	4.07	1.09
S431	72.59	72.96	10.1	1.99
S431	72.96	74.48	3.1	1.56
S431	74.48	74.67	11.4	15.8
S431	74.67	75.91	0.08	0.1
S431	75.91	76.04	4.86	1.52
S431	76.04	76.65	0.07	0.11
S431	76.65	77.47	1.7	3.85
S431	77.47	77.93	0.04	0.05
S431	77.93	78.38	0.02	0.01
S431	78.38	79.3	0.32	0.03
S431	79.3	80.4	4.67	0.01
S431	80.4	81.19	0.2	0
S431	81.19	82.65	0.59	0.04
S432	32.97	34.49	2.04	0.9
S432	34.49	36.02	1.39	0.07
S432	36.02	37.39	1.24	0.02
S432	37.39	38.45	1.32	0
S432	38.45	39.67	2.08	0
S432	39.67	41.2	2.61	0
S432	41.2	42.72	2.67	0
S432	42.72	43.64	0.42	0
S432	43.64	44.55	0.13	0
S433	26.63	27.91	0.18	0.03
S433	27.91	29.22	0.2	0.01
S433	29.22	29.52	0.01	0.01
S433	29.52	29.8	0.01	0.01
S433	29.8	30.93	2.2	0
S433	30.93	32.45	0.02	0
S433	32.45	33.97	0.01	0
S433	33.97	35.04	0.01	0
S434	27.43	28.96	0	0
S435	14.63	17.68	0	0
S436	4.57	6.1	0	0
S437	7.67	19.56	0	0
S438	6.15	23.52	0	0
S439	11.33	17.42	0	0
S440	111	111.18	1.09	0.11
S440	111.18	111.7	12.8	4.22
S440	111.7	112.77	1.67	5.36
S440	112.77	113.74	1.93	3.77
S440	113.74	115.26	1.49	4.47
S445	85.09	90.73	0	0
S446	33.03	34.55	1.13	0.13
S446	34.55	35.86	0.08	0.01
S446	35.86	37.69	3.63	0.22
S446	37.69	39.16	1.19	0.32
S447	12.85	13.77	2.08	0.59
S447	13.77	14.83	1.49	0.89
S447	14.83	15.29	3.36	2.26
S447	15.29	15.72	2.67	2.21
S447	15.72	17.03	1.96	0.65
S447	17.03	18.34	2.23	0.77
S447	18.34	19.86	0.6	0.57
S447	19.86	21.08	0.04	0.03

S447	21.08	22.61	0.22	0.04
S447	22.61	24.13	1.54	0.09
S447	24.13	25.35	2.07	1.1
S447	25.35	26.26	1.56	2.65
S447	26.26	27.48	0.63	11.3
S447	27.48	28.7	3.57	5.12
S447	28.7	29.4	2.4	0.05
S447	29.4	30.29	1.87	0.02
S448	13.92	15.29	1.38	0.02
S448	15.29	16.51	2.38	0.01
S449	18.34	34.95	0	0
S450	108.96	110.48	0.01	0.01
S450	110.48	110.94	4.01	7.5
S450	110.94	111.24	3.75	14
S450	111.24	111.39	3.62	9.42
S450	111.39	111.79	0.24	3.2
S450	111.79	113.22	0.44	22.8
S450	113.22	113.74	0.06	7.24
S450	113.74	115.26	0	0.07
S451	26.26	26.96	0	0
S452	32.92	35.97	0	0
S453	53.69	53.85	4.32	0.02
S453	53.85	54.12	0.23	0.06
S453	54.12	55.34	4.09	0.58
S453	55.34	56.19	0.74	0.01
S453	56.19	57.35	0.22	0.03
S454	99.96	100.12	7.11	0.01
S454	100.12	100.73	18.9	0.01
S454	100.73	100.85	0	0
S454	100.85	101.03	10.7	0.04
S454	101.03	101.43	6.87	0.03
S454	101.43	102.57	0.06	0.01
S454	102.57	103.02	0.02	0
S455	135.69	137.21	0	0
S455	137.21	137.85	3.63	0.04
S455	137.85	139.37	0.06	0.01
S456	26.29	27.73	2.2	0.05
S456	27.73	27.97	2.68	0.02
S456	27.97	28.21	0.12	0.01
S456	28.21	28.91	1.05	0.01
S456	28.91	29.22	0.74	0.04
S456	29.22	29.92	0.14	0.01
S456	29.92	30.41	1.05	0.01
S456	30.41	30.87	0.05	0.01
S456	30.87	31.66	1.42	0.02
S456	31.66	32.97	0.39	0.06
S456	32.97	33.58	0.02	0.02
S456	33.58	35.1	0.38	0.03
S456	35.1	35.86	1.65	0.34
S457	93.38	93.93	0.35	0.05
S457	93.93	95.45	3.36	0.23
S457	95.45	95.79	0.46	0.06
S458	158.73	160.25	0.01	0
S458	160.25	160.56	53.7	2.14
S458	160.56	160.8	8.54	0.03
S458	160.8	161.78	0.55	0.02
S458	161.78	162.76	2.23	0.03
S458	162.76	163.98	0.23	0.25
S459	158.39	159.77	0	0
S460	36.02	62.63	0	0
S461	102.46	103.38	0.69	0
S461	103.38	104.6	7.19	0.57
S461	104.6	106.12	1	0.02
S462	57.05	58.57	0.72	0.04
S462	58.57	59.18	2.29	0.24
S462	59.18	60.1	0.86	0.07
S462	60.1	60.4	1.71	0.37
S462	60.4	61.25	0.89	0.25
S462	61.25	62.72	0.25	0.01
S462	62.72	63.45	0.05	0.01
S463	77.47	78.02	0.47	0.06
S463	78.02	78.63	0.41	0.06
S463	78.63	78.87	0.87	0.11
S463	78.87	80.09	1.2	0.59
S463	80.09	81.52	8.3	1.11
S463	81.52	82.8	1.17	0.04
S464	21.75	22.76	0.81	0.1
S464	22.76	24.25	0.52	0.05
S464	24.25	24.4	0.38	0.02
S464	24.4	24.65	1.66	0.01
S464	24.65	25.68	3.89	0

S464	25.68	27.21	3.14	0
S464	27.21	28.73	0.91	0
S464	28.73	29.52	1.55	0
S464	29.52	31.05	12.5	0.14
S464	31.05	31.57	3.89	0
S464	31.57	33.09	2.81	0
S464	33.09	34.55	1.05	0.02
S464	34.55	35.83	1.53	0
S464	35.83	37.36	9.07	0
S464	37.36	38.88	10.8	0
S464	38.88	39.73	8.45	0
S464	39.73	41.23	4.97	0
S464	41.23	41.38	3.64	0
S464	41.38	42.36	3.22	0
S464	42.36	43.79	6.34	0
S464	43.79	45.31	12.2	0
S464	45.31	46.11	5.18	0
S464	46.11	47.63	3.06	0
S464	47.63	49.15	3.06	0.09
S464	49.15	49.37	2.08	0.01
S464	49.37	50.43	0.99	0.04
S464	50.43	51.87	2.56	0.54
S464	51.87	53.39	3.66	0.09
S464	53.39	53.6	1.21	0
S464	53.6	55.13	3.01	0.08
S464	55.13	56.47	2.78	0.04
S464	56.47	57.99	2.58	0.04
S464	57.99	59.52	2.7	0.02
S464	59.52	60.74	3.49	0.06
S464	60.74	61.22	2	0.02
S464	61.22	62.59	1.23	2.01
S464	62.59	62.96	1.03	11.6
S464	62.96	63.14	0.24	0.45
S464	63.14	64.48	0.23	0.03
S465	18.34	19.13	0.89	0.15
S465	19.13	20.65	0.71	0.01
S465	20.65	26.32	0	0
S465	26.32	27.85	0.36	0
S465	27.85	29.31	1.34	0
S465	29.31	30.53	0.95	0
S465	30.53	30.93	1.77	0.01
S465	30.93	32.05	2.46	0
S465	32.05	32.72	13.1	0.26
S465	32.72	33.4	5.94	0.02
S465	33.4	34	6.04	0.01
S465	34	35.13	4.65	0.23
S465	35.13	36.26	1.86	0.05
S465	36.26	37.14	2.26	0.25
S465	37.14	38.15	0.73	0.08
S465	38.15	38.7	0.4	0.11
S465	38.7	39.77	2.38	0.31
S465	39.77	40.59	0.72	0.01
S465	40.59	41.81	1.35	0.03
S465	41.81	43	1.27	0.01
S465	43	44.52	0.57	0.04
S465	44.52	48.09	0	0
S465	48.09	49.12	1.36	0
S465	49.12	49.61	3.58	1.46
S465	49.61	51.1	0.14	0.06
S465	51.1	51.26	0.57	0.44
S465	51.26	52.17	0.82	0.71
S465	52.17	52.99	1.56	0.48
S466	30.23	31.75	0.03	0.14
S466	31.75	32.97	8.54	0.02
S466	32.97	34.07	12.9	0.01
S466	34.07	35.59	5.88	0.87
S466	35.59	36.5	3.75	0.41
S466	36.5	38.03	4.47	1.65
S466	38.03	39.55	2.62	2.99
S466	39.55	41.08	3.3	4.08
S466	41.08	41.69	5.8	5.56
S466	41.69	42.6	2.61	1.95
S466	42.6	43.45	2.95	1.56
S466	43.45	44.86	3.42	1.76
S466	44.86	46.38	1.75	1.96
S466	46.38	47.9	2.37	2.31
S466	47.9	49.18	2.65	2.13
S466	49.18	50.49	1.7	3.66
S467	84.48	86	0.03	0.53
S467	86	86.43	0.92	0.95
S467	86.43	87.07	4.57	1.03

S467	87.07	87.53	0.95	0.83
S468	37.8	50.6	0	0
S470	42.42	42.9	0.63	0.05
S470	42.9	44.37	0.71	0.01
S470	44.37	45.1	1.41	0
S470	45.1	46.59	1.48	0
S470	46.59	47.93	0.33	0
S470	47.93	48.67	0.3	0
S470	48.67	49.58	0.17	0
S470	49.58	50.98	1.53	0
S470	50.98	52.48	0.66	0
S470	52.48	54	0.89	0
S470	54	55.22	0.22	0
S470	55.22	56.44	0.25	0
S470	56.44	57.66	0.17	0.01
S470	57.66	59.09	0.15	0
S470	59.09	60.28	0.43	0
S470	60.28	61.62	0.96	0
S470	61.62	62.32	1.13	0
S470	62.32	63.33	1.59	0
S470	63.33	64.82	0.47	0
S470	64.82	66.19	1.5	0
S470	66.19	67.47	2.35	0.07
S470	67.47	68.26	1.33	0
S470	68.26	69.54	0.03	0
S470	69.54	71.07	0	0
S470	71.07	71.86	1.2	0.32
S470	71.86	72.47	1.08	0.07
S470	72.47	73.66	0.1	0.18
S470	73.66	75.18	0.01	0.27
S471	29.01	31.9	0	0
S472	34.64	36.02	0.99	0
S472	36.02	37.54	1.32	0
S472	37.54	38.36	0.98	0
S472	38.36	39.25	0.8	0
S472	39.25	40.59	0.53	0
S472	40.59	42.1	0.42	0
S472	42.1	43.45	0.94	0
S472	43.45	44.98	0.29	0
S472	44.98	57.66	0	0
S472	57.66	58.33	0.49	0
S472	58.33	59.79	0.43	0
S472	59.79	61.01	0.71	0
S473	67.11	67.53	3.91	0.03
S473	67.53	67.78	4.45	0
S473	67.78	68.81	1.38	0.02
S473	68.81	70	1.63	0
S473	70	70.82	0.37	0
S473	70.82	71.83	0.7	0.1
S473	71.83	72.53	2.72	0.02
S473	72.53	72.65	3.55	4.72
S473	72.65	74.12	2.14	0.03
S473	74.12	74.73	0.51	0.3
S473	74.73	75.46	0.26	0.31
S473	75.46	75.82	0.72	1.04
S473	75.82	76.55	7.71	4.16
S473	76.55	78.08	8.42	4.02
S473	78.08	78.78	1.44	0.13
S473	78.78	80.03	1.22	0.01
S475	108.86	109.14	0.01	0.03
S475	109.14	110.2	0	0
S475	110.2	111.36	0	0
S475	111.36	112.28	3.59	2.68
S475	112.28	112.49	9.83	0.19
S475	112.49	112.73	2.8	0.95
S475	112.73	113.37	1.66	0.15
S475	113.37	113.59	4.61	0.22
S475	113.59	113.8	1.03	0.06
S475	113.8	115.42	0.03	0.02
S475	115.42	116.89	0.01	0
S475	116.89	117.96	0.01	0
S476	43.21	44.06	0.84	0.07
S476	44.06	45.37	0.53	0.03
S476	45.37	45.71	0.19	0.05
S476	45.71	46.14	0.98	0.04
S476	46.14	47.66	0.22	0.04
S476	47.66	49.18	0.31	0.06
S476	49.18	50.62	0.83	0.15
S476	50.62	50.86	0.97	0.17
S476	50.86	52.38	1.26	0.15
S476	52.38	53.6	2.38	0.04

S476	53.6	55.13	0.77	0.09
S476	55.13	56.65	1.1	0
S476	56.65	58.18	1.06	0.05
S476	58.18	59.06	0.72	0.01
S476	59.06	60.58	0.85	0.12
S476	60.58	62.11	1.19	0.05
S476	62.11	63.63	1.96	0.04
S476	63.63	65.16	2.12	0.01
S476	65.16	65.73	2.44	0
S476	65.73	67.26	0.58	0.02
S476	67.26	68.33	0.51	0.01
S476	68.33	69.85	0.59	0.25
S476	69.85	71.16	1.32	0.02
S476	71.16	72.47	1.66	0.04
S476	72.47	73.45	1.44	0.28
S476	73.45	74.97	2.43	0.3
S476	74.97	76.49	1.2	0.46
S476	76.49	78.02	0.52	0.46
S476	78.02	79.51	4.51	0.63
S476	79.51	80.58	0.57	1.03
S476	80.58	80.85	0.17	0.01
S479	89.36	89.66	0.07	0.06
S479	89.66	89.84	6.8	0.98
S479	89.84	90.39	46.4	22.3
S479	90.39	91.19	54.3	10.51
S479	91.19	92.89	1.26	1.59
S479	92.89	94.32	4.78	1.11
S479	94.32	95.73	4.65	0.69
S479	95.73	97.25	5.46	2.37
S479	97.25	98.77	2.38	1.1
S480	181.5	182.47	0	0.27
S480	182.47	183.48	0.11	3.36
S480	183.48	185	0.01	0.01
S486	200.25	200.44	0.01	0.06
S486	200.44	200.86	0.01	0.02
S490	79.76	80.82	0.03	0.05
S490	80.82	82.22	0	0.02
S490	82.22	82.71	0.47	0.14
S490	82.71	83.9	0.02	0.02
S490	83.9	85.3	0.05	0.02
S490	85.3	86.83	0.14	0.03
S490	86.83	87.38	0	0
S491	59.64	79.76	0	0
S492	33.73	69.24	0	0
S493	37.54	39.06	6.38	0.02
S493	39.06	40.28	0.2	0.01
S493	40.28	41.5	0.03	0.01
S494	33.58	34.64	4.08	0.04
S494	34.64	36.02	1.68	1.3
S494	36.02	37.24	2.69	0.12
S494	37.24	38.45	0.26	0
S494	38.45	39.83	0.21	0
S494	39.83	40.59	2.51	0
S494	40.59	41.5	0.88	0.02
S494	41.5	42.11	0.41	0
S494	42.11	43.64	1.97	0
S494	43.64	45.16	1.93	0
S494	45.16	46.68	0.93	0
S494	46.68	48.21	0.96	0.02
S495	29.92	55.89	0	0
S496	28.21	29.49	2.32	0
S496	29.49	30.07	3.35	0
S496	30.07	31.6	4.02	0
S496	31.6	33.12	1.99	0
S496	33.12	34.64	2.2	0
S496	34.64	35.86	0.78	0
S496	35.86	37.39	1.02	0
S497	48.7	50.22	0.01	0.1
S497	50.22	50.95	0.01	0.38
S497	50.95	51.71	0.02	0.03
S497	51.71	52.66	1.44	0.01
S497	52.66	53.18	1.22	0
S497	53.18	54	0.37	0
S497	54	54.88	0.47	0.05
S497	54.88	55.92	0.31	0.07
S497	55.92	56.44	0.08	0.04
S497	56.44	57.72	0.91	0.04
S497	57.72	58.57	1.25	0.99
S497	58.57	60.03	0.29	0.17
S498	58.57	66.04	0	0
S499	34.74	35.41	0.17	0.13

S499	35.41	35.86	0.91	0.06
S499	35.86	36.32	6.58	0.07
S499	36.32	37.85	0.44	0.06
S499	37.85	38.45	0.46	0.13
S499	38.45	38.64	4.2	1.23
S499	38.64	38.94	2.98	0.01
S499	38.94	40.19	18.7	1.46
S499	40.19	40.65	11.7	15.9
S499	40.65	41.5	2.9	0.09
S499	41.5	42.11	2.86	0.09
S499	42.11	42.97	2.34	0.1
S499	42.97	44.09	1.26	0.89
S499	44.09	44.43	2.2	0.39
S499	44.43	44.7	2.95	0.22
S499	44.7	45.7	0.33	0.07
S499	46.01	46.32	0.33	0.03
S499	46.32	47.6	0.89	0.14
S499	47.6	48.06	0.08	0.24
S499	48.06	49.43	0.65	1.47
S499	49.43	50.89	1.73	0.81
S499	50.89	51.5	1.15	8.34
S499	51.5	51.74	0.05	0.7
S499	51.74	52.11	7.97	11.7
S499	52.11	52.29	1.88	0.02
S499	52.29	53.6	4.33	1.03
S499	53.6	54	0.58	3.18
S499	54	54.09	2.8	0.75
S499	54.09	54.67	0.16	0.12
S499	54.67	54.76	4.86	0.02
S499	54.76	55.16	0.02	0
S499	55.16	55.34	0.53	0.39
S499	55.34	56.74	0.01	0
S500	117.7	118.46	5.06	7.75
S500	118.46	119.68	0.63	4.53
S501	58.27	60.71	0	0
S502	45.28	45.47	1.58	0.08
S502	45.47	46.38	1.06	0.04
S502	46.38	47.48	2.54	0.18
S502	47.48	48.51	0.05	0.05
S502	48.51	50.04	4.22	0.03
S502	50.04	51.26	1.73	0.78
S502	51.26	52.78	0.52	0.45
S502	52.78	53.54	0.3	0.32
S503	21.39	22.3	1.55	0.01
S503	22.3	23.52	0.61	0
S503	23.52	24.13	0.66	0
S503	24.13	24.89	0.95	0
S503	24.89	26.87	0.34	0
S503	26.87	27.79	0.61	0
S503	27.79	28.09	0.55	0
S503	28.09	29.62	0.7	0
S503	29.62	31.44	0.46	0
S503	31.44	32.97	0.47	0
S503	32.97	34.34	2.16	0
S504	21.34	22.71	0	0
S505	78.38	80.82	0	0
S506	77.87	79.39	0.02	0
S506	79.39	80.91	0.03	0.02
S506	80.91	82.13	0.13	0.06
S506	82.13	83.26	0.59	0.03
S506	83.26	84.42	0.55	0.04
S506	84.42	85.24	1.8	0.17
S506	85.24	85.76	0.71	0.04
S506	85.76	86.31	3.48	0.3
S506	86.31	87.83	1.53	0.2
S506	87.83	88.78	1.13	0.1
S506	88.78	90.12	0.7	0.04
S506	90.12	90.88	0.83	0.04
S506	90.88	91.31	0.01	0
S506	91.31	92.4	0.25	0.03
S506	92.4	93.32	0.49	0.01
S506	93.32	94.84	0.7	0
S506	94.84	95.97	0.59	0.02
S506	95.97	96.67	0.16	0.02
S506	96.67	98.2	0.02	0
S506	98.2	99.72	0.01	0
S506	99.72	113.04	0	0
S506	113.04	114.56	0	0
S506	114.56	114.9	0.22	0.01
S506	114.9	115.97	0.25	0.01
S506	115.97	116.79	0.05	0.01

S506	116.79	117.86	0.08	0.01
S506	117.86	119.23	0.15	0.03
S506	119.23	120.75	0.19	0.03
S506	120.75	122.27	0.22	0.06
S506	122.27	122.88	0.25	0.04
S506	122.88	123.95	0.39	0.07
S506	123.95	124.16	0.09	0
S506	124.16	124.87	0.13	0.05
S506	124.87	125.93	0.88	0
S506	125.93	126.76	0.87	0.01
S506	126.76	128.07	0.2	0.01
S507	108.56	109.14	30.54	30.66
S507	109.14	109.47	5.52	0.37
S507	109.47	110.14	3.38	0.31
S508	116.03	117.55	0	0
S508	117.55	117.76	7.4	15.3
S508	117.76	119.29	0.11	0.09
S509	29.62	30.53	0.87	0.38
S509	30.53	31.9	0.34	0.19
S509	31.9	32.36	0.1	0.03
S509	32.36	33.88	0	0.01
S509	33.88	34.34	0.1	0.04
S509	34.34	35.71	0.11	0.01
S509	35.71	37.24	0.37	0
S509	37.24	38.76	0.41	0.07
S509	38.76	39.8	0.52	0.1
S509	39.8	40.95	0.14	0
S510	11.72	13.16	0	0
S511	11.58	14.33	0	0
S512	9.75	11.28	0	0
S513	7.92	11.28	0	0
S514	13.47	14.81	0.01	0
S521	39.62	40.84	0	0
S522	30.48	33.83	0	0
S523	25.91	27.74	0	0
S525	86.92	87.53	0	0
S526	45.16	46.07	0.73	3.01
S526	46.07	46.84	0.13	0.7
S526	46.84	47.75	0.36	1.18
S526	47.75	49.12	2.6	0.91
S526	49.12	50.65	4.01	0.52
S526	50.65	52.17	4.29	0.45
S526	52.17	53.39	2.47	0.69
S526	53.39	54.61	4.66	1.12
S526	54.61	56.13	6.08	1.98
S526	56.13	57.66	5.63	2.05
S526	57.66	59.18	2.35	0.31
S526	59.18	60.71	1.81	0.02
S526	60.71	61.62	0.85	0
S527	20.17	21.39	3.53	0.09
S527	21.39	22.15	2.95	0.59
S527	22.15	23.52	1.62	0.16
S527	23.52	24.43	1.39	0.08
S527	24.43	25.65	3.29	0.12
S527	25.65	27.18	1.03	0.02
S527	27.18	28.09	0.64	0
S527	28.09	29.62	0.54	0.14
S527	29.62	30.53	1.02	0.07
S527	30.53	32.05	1.35	0.03
S527	32.05	33.58	0.62	0.06
S527	33.58	34.86	2.36	0.27
S527	34.86	35.47	0.12	0.02
S527	35.47	35.71	12.2	22.9
S527	35.71	36.5	3.85	1.67
S527	36.5	37.54	3.76	0.02
S527	37.54	38.52	2.29	0.01
S527	38.52	39.37	1.67	0
S527	39.37	40.89	2.14	0.03
S527	40.89	41.81	0.9	0
S527	41.81	43.33	0.66	0
S527	43.33	44.76	0.51	0
S527	44.76	45.43	5.44	0
S527	45.43	45.74	0.12	0
S527	45.74	45.92	2.01	0
S527	45.92	46.9	1.59	0
S527	46.9	48.21	0.21	0
S527	48.21	48.51	0.15	0
S527	48.51	49.24	0.46	0
S528	19.86	21.14	1.16	0
S528	21.14	22	1.64	0.07
S528	22	22.18	0.16	0.18

S528	22.18	22.61	0.5	0.05
S528	22.61	22.82	0.04	0.01
S528	22.82	23.82	0.27	0.09
S528	23.82	24.92	0.11	0.03
S528	24.92	25.96	0.23	0.06
S528	25.96	26.14	0.06	0.01
S528	26.14	27.48	0.2	0.01
S528	27.48	29.01	0	0
S528	29.01	30.04	0.2	0
S532	69.54	76.43	0	0
S533	62.84	63.75	0.16	0.05
S533	63.75	63.94	0.15	0.07
S533	63.94	65.46	0.14	0.07
S533	65.46	65.89	0.2	0.01
S534	80.21	81.13	0.02	0.01
S535	64.89	65.53	0	0
S536	65.89	68.97	0	0
S537	98.32	106.97	0	0
S539	17.58	19.1	4.89	0.02
S539	19.1	20.62	1.6	0.03
S540	41.66	42.54	6.95	1.36
S540	42.54	43.42	33.6	2.06
S540	43.42	44.25	6.51	0.01
S540	44.25	45.07	0.68	0
S540	45.07	46.5	0.45	0.01
S540	46.5	47.9	2.83	0.01
S540	47.9	48.18	14.8	0.01
S540	48.18	49	6.34	0
S540	49	49.61	1.07	0.06
S540	49.61	50.34	3.07	0.01
S540	50.34	50.95	8.19	0.48
S540	50.95	51.93	3.18	1.21
S540	51.93	52.78	5.51	0.52
S540	52.78	53.79	11.3	5.78
S540	53.79	54.33	8.38	10.1
S540	54.33	55.83	3.09	1.25
S540	55.83	56.74	7.09	6.76
S540	56.74	57.66	2	0.83
S540	57.66	58.39	7.25	2.21
S540	58.39	58.66	0.18	0.09
S540	58.66	59.18	6.23	10.9
S540	59.18	60.1	0.13	0.5
S540	60.1	61.62	0.53	0.82
S540	61.62	63.02	0.39	2.9
S540	63.02	64.55	0.02	0.03
S541	54	54.91	33.9	0
S541	54.91	56.01	55.1	0.68
S541	56.01	57.26	19.8	0.47
S541	57.26	58.57	11.3	0.24
S541	58.57	59.36	4.64	0.05
S541	59.36	60.89	9.28	9.68
S541	60.89	62.23	9.44	6.22
S541	62.23	62.78	20.3	21.4
S541	62.78	64.3	12.9	17.4
S541	64.3	65.16	7.43	5.07
S542	70.21	70.86	42.9	5.14
S542	70.86	71.4	6.97	0.88
S542	71.4	72.93	3.37	0.76
S542	72.93	74.42	3.27	2.83
S542	74.42	75.95	1.59	0.68
S542	75.95	77.47	0.94	1.15
S542	77.47	79.05	1.35	1.16
S542	79.05	79.97	4.42	3.47
S542	79.97	80.55	0.22	0.17
S542	80.55	81.43	10.3	2.04
S542	81.43	83.2	3.48	0.16
S542	83.2	84.78	0.07	0.06
S543	78.26	78.6	0.25	0.39
S543	78.6	79.91	0.11	0.16
S543	79.91	80.85	5.02	4.22
S543	80.85	81.98	0.26	0.22
S543	81.98	82.16	1.41	1.73
S543	82.16	82.65	1.72	17.4
S543	82.65	83.26	6.07	2.3
S543	83.26	84.02	2.6	2.46
S543	84.02	84.48	1.85	0.23
S543	84.48	85.55	1.71	2.33
S543	85.55	85.85	1	0.62
S544	44.86	45.98	0.93	0
S544	45.98	47.51	1.8	0
S544	47.51	48.51	0.74	0

S544	48.51	49.64	0.66	0
S544	49.64	50.34	0.19	0.03
S544	50.34	51.04	0.02	0
S544	51.04	52.57	0.05	0.01
S545	44.55	46.07	3.15	0.04
S545	46.07	47.29	2.25	0
S545	47.29	48.76	1.91	0
S545	48.76	50.22	3.32	0
S545	50.22	52.48	1.2	0.02
S545	52.48	54	0.11	0.07
S545	54	55.52	0.27	0
S545	55.52	57.05	0.13	0
S545	57.05	58.57	0.45	0
S545	58.57	60.1	0.9	0.01
S545	60.1	61.62	1.03	0.13
S545	61.62	63.14	0.43	0.01
S545	63.14	64.67	0.36	0.02
S545	64.67	65.95	0.68	0.03
S545	65.95	66.59	0.74	0.09
S546	42.57	43.21	3.7	0.02
S546	43.21	44.25	6.29	0.01
S546	44.25	45.92	2.02	0.01
S546	45.92	47.45	2.24	0.02
S546	47.45	49.03	2.05	0.02
S546	49.03	50.34	1.83	0.01
S546	50.34	51.71	1.02	0.03
S546	51.71	52.78	1.06	0.05
S546	52.78	54.3	0.32	0.01
S546	54.3	57.05	0.57	0.19
S546	57.05	58.57	0.19	0.02
S546	58.57	60.1	0.12	0.08
S546	60.1	61.62	0.21	0.02
S546	61.62	63.14	0.17	0.02
S546	63.14	64.67	0.14	0.05
S546	64.67	66.19	0.54	0
S546	66.19	67.72	1.27	0
S546	67.72	69.24	0.2	0.04
S546	69.24	70.76	0.74	0.1
S546	70.76	71.74	1.25	0.12
S546	71.74	73.2	1	0.29
S546	73.2	74.73	1.15	0.01
S546	74.73	76.25	1.17	0.03
S546	76.25	77.77	1.64	0.29
S546	77.77	78.54	0.91	0.23
S546	78.54	78.69	2.57	0.91
S546	78.69	80.21	1.42	0.76
S546	80.21	81.74	1.76	0.97
S546	81.74	82.04	1.34	0.32
S546	82.04	82.19	0.22	0
S546	82.19	83.72	1.32	0.41
S546	83.72	84.48	0.6	0.14
S547	42.72	42.87	2.91	0.85
S547	42.87	44.15	0	0
S547	44.15	44.92	2.1	1.07
S547	44.92	45.47	0	0
S547	45.47	46.53	4.55	8.78
S547	46.53	47.9	0.85	2.09
S547	47.9	49.43	1.43	0.97
S547	49.43	50.95	0.78	1.24
S547	50.95	52.48	2.86	2.23
S547	52.48	54.61	0	0
S547	54.61	55.37	7.84	7.71
S547	55.37	56.13	6.22	1.7
S547	56.13	57.5	3.88	2.21
S547	57.5	59.91	0	0
S547	59.91	61.62	1.31	0.38
S547	61.62	63.14	0.97	0.04
S547	63.14	64.67	1.31	0.22
S547	64.67	66.19	0.62	0.01
S547	66.19	67.72	2.21	0.06
S547	67.72	69.24	3.19	0.01
S547	69.24	70.31	4.99	0.03
S547	70.31	71.83	4.1	0
S547	71.83	73.35	3.49	0.09
S547	73.35	74.88	1.54	0.01
S547	74.88	75.95	1.04	0.02
S547	75.95	77.47	2.12	0.29
S547	77.47	78.84	5.54	0.01
S547	78.84	80.21	3.36	0.01
S547	80.21	81.74	4.31	0.66
S547	81.74	83.26	2.29	0.86

S547	83.26	84.78	2.25	0.3
S547	84.78	86.31	0.19	0.81
S547	86.31	87.83	1.37	0.51
S547	87.83	88.44	1.93	0.85
S547	88.44	89.36	0.47	0.15
S547	89.36	90.88	1.64	0.15
S547	90.88	91.49	0.45	0.78
S548	87.83	88.09	29.1	37.9
S548	88.09	88.7	20.3	0.74
S549	90.42	90.88	21	0.08
S549	90.88	91.83	4.26	0.23
S549	91.83	92.71	5.45	0.03
S549	92.71	93.14	1.2	1.06
S549	93.14	94.26	0.65	0.07
S549	94.26	95.67	1.58	4.01
S549	95.67	96.37	5.56	4.33
S549	96.37	97.46	3.02	0.37
S549	97.46	98.41	6.2	7.14
S549	98.41	99.72	2.3	1.34
S549	99.72	101.24	1.04	1.84
S551	124.1	125.2	0	0
S552	165.86	166.59	0	0
S554	94.6	95.04	1.23	0.05
S554	95.04	95.71	0.18	0
S554	95.71	96.77	0.89	0
S555	102.31	102.81	21.3	40.1
S555	102.81	103.94	3.58	1.92
S556	41.81	43.33	0.82	0.36
S556	43.33	44.86	1.36	1.02
S556	44.86	46.38	1.07	1.52
S556	46.38	47.9	2.46	0.84
S556	47.9	49.43	2.2	0.24
S556	49.43	50.95	2.73	0.29
S556	50.95	52.48	1.16	0.18
S556	52.48	54	1.09	0.01
S556	54	55.52	0.43	0.05
S556	55.52	56.44	0.97	0.04
S556	56.44	58.27	3.72	0.12
S556	58.27	59.27	16.3	30.5
S556	59.27	61.92	0	0
S556	61.92	63.45	4.87	3.51
S556	63.45	64.67	3.24	4.94
S556	64.67	65.59	1.4	0.35
S556	65.59	66.5	1.53	0.07
S556	66.5	67.72	0.67	0.01
S556	67.72	68.93	0.6	0.02
S556	68.93	70.15	1.58	0.01
S556	70.15	71.37	3.91	0.01
S556	71.37	72.9	3.77	0
S556	72.9	74.12	3.49	0
S556	74.12	75.64	0.47	0.11
S556	75.64	77.16	1.24	0
S556	77.16	78.69	2.75	0
S556	78.69	80.21	2.58	0
S556	80.21	81.28	1.96	0
S556	81.28	82.35	0.52	0
S556	82.35	83.26	1.39	0
S557	75.64	77.07	24.9	27.7
S557	77.07	78.26	10.2	0.12
S557	78.26	79.82	2.76	0.02
S557	79.82	81.19	3.11	0
S557	81.19	82.68	3.16	0
S557	82.68	83.57	1.69	0
S557	83.57	83.9	0.26	0.05
S557	83.9	85.24	4.22	0.05
S557	85.24	85.49	14.1	0.63
S557	85.49	86.31	3.49	0.13
S557	86.31	87.38	3.99	0.76
S557	87.38	88.08	3.22	2.81
S557	88.08	90.09	0.88	0.2
S557	90.09	90.76	6.71	0.12
S558	37.78	41.66	0.61	0.2
S558	41.66	43.18	0.92	0.5
S558	43.18	44.7	0.8	0.43
S558	44.7	45.31	0.06	0.01
S558	45.31	46.07	2.81	0.3
S558	46.07	46.99	1.01	0.47
S558	46.99	48.21	1.14	0.64
S558	48.21	49.43	0.7	0.71
S558	49.43	50.95	0.25	0.25
S558	50.95	52.17	3.39	0.05

S558	52.17	53.33	4.61	0.81
S558	53.33	54.55	3.95	1.57
S558	54.55	55.77	9.15	0.52
S558	55.77	57.29	0.8	0.11
S558	57.29	58.82	0.6	0.25
S558	58.82	60.58	0.57	0.1
S560	46.68	47.02	0.11	0.14
S560	47.02	47.51	0.37	0.13
S560	47.51	47.9	29.1	38.6
S560	47.9	48.79	4.09	0.77
S560	48.79	49.28	2.83	1.11
S560	49.28	50.8	3.27	2.09
S560	50.8	51.44	2.62	2.28
S560	51.44	52.11	2.98	1.08
S561	64.97	65.92	3.7	8.54
S561	65.92	66.77	2.89	1.76
S561	66.77	67.41	0.74	5.6
S561	67.41	67.87	0.7	2.31
S562	14.99	35.25	0	0
S563	14.38	27.73	0	0
S564	14.07	28.7	0	0
S565	36.02	36.17	30.4	11.4
S565	36.17	37.69	1.93	0.03
S565	37.69	39.37	0.17	0.53
S565	39.37	39.52	13.6	21.5
S565	39.52	41.35	2.54	0.1
S565	41.35	41.5	20.1	0.01
S565	41.5	41.96	3.34	0.01
S565	41.96	43.48	1.39	0.07
S565	43.48	44.09	5.99	1.05
S565	44.09	46.53	0.71	0.41
S565	46.53	46.99	8.17	0.98
S565	46.99	48.51	11.3	5.92
S565	48.51	48.97	11.4	8.72
S565	48.97	49.23	2.91	2.23
S565	49.23	50.6	13.3	4
S566	23.52	23.73	1.68	0.03
S566	23.73	25.04	1.81	0.65
S566	25.04	26.57	0.41	0.4
S566	26.57	28.09	0.31	0.11
S566	28.09	28.7	1.33	0.04
S566	28.7	30.23	0.74	0.01
S566	30.23	31.75	0.17	0.19
S566	31.75	33.27	0.49	0.05
S566	33.27	34.8	0.52	0.02
S566	34.8	36.32	0.61	0.02
S566	36.32	37.85	0.97	0.03
S566	37.85	39.37	0.72	0.02
S566	39.37	40.89	0.51	0.02
S566	40.89	42.42	0.6	0.2
S566	42.42	43.94	4.62	0.12
S566	43.94	44.37	1.53	0.08
S566	44.37	45.92	0.8	0.49
S566	45.92	46.84	1.14	0.41
S566	46.84	47.29	1.18	0.34
S566	47.29	48.82	0.93	0.18
S566	48.82	50.04	4.28	2.21
S566	50.04	51.2	3.63	1
S567	17.73	19.86	0.25	0.04
S567	19.86	21.39	0.24	0.02
S567	21.39	22.91	0.02	0.02
S567	22.91	24.43	0.03	0.04
S567	24.43	25.96	0.25	0.03
S567	25.96	27.48	2.34	0.22
S567	27.48	29.01	2.84	0
S567	29.01	29.62	4.38	0
S567	29.62	31.14	0.72	0.01
S567	31.14	32.66	0.37	0
S567	32.66	33.27	0.42	0.01
S567	33.27	34.8	2.17	0.21
S567	34.8	36.32	0.78	0.07
S567	36.32	37.85	1.24	0.01
S567	37.85	38.76	4.23	0.12
S567	38.76	39.37	0.63	0.01
S567	39.37	40.89	14.1	3.91
S567	40.89	42.42	2.72	0.1
S567	42.42	43.94	0.86	0.14
S567	43.94	45.47	5.36	3.16
S567	45.47	46.99	8.13	0.64
S567	46.99	48.51	8.94	0.09
S567	48.51	50.04	7.4	2.12

S567	50.04	51.56	1.44	0.25
S567	51.56	52.48	1.49	0.39
S567	52.48	54.15	0.53	0.94
S568	68.93	69.39	8.52	0.5
S568	69.39	70.92	2.6	2.31
S568	70.92	72.44	1.87	14.7
S569	28.24	28.7	0.26	0.03
S569	28.7	29.62	0	0
S569	29.62	29.83	0.09	0
S570	14.02	14.63	0.52	0.03
S570	14.63	16.06	0.54	0.02
S570	16.06	17.53	1.56	0.01
S570	17.53	17.78	0.24	0.01
S570	17.78	20.3	0.23	0.01
S570	20.3	20.76	1.11	0.06
S570	20.76	21.34	1.11	0
S570	21.34	22.1	0.21	0
S570	22.1	22.77	0.38	0
S570	22.77	23.77	1.68	0
S570	23.77	24.54	3.48	0
S570	24.54	25.21	6.41	0
S570	25.21	25.97	0.89	0
S570	25.97	26.91	1.52	0.01
S571	62.79	63.61	2.49	0
S573	111.67	112.22	1.39	0.18
S573	112.22	113.74	0.11	0.07
S573	113.74	114.81	0.13	0.05
S574	188.42	189.94	0.09	0.01
S574	189.94	191.46	0.02	0
S574	191.46	192.99	0.24	0.13
S574	192.99	194.51	0.52	0.57
S574	194.51	196.04	2.15	0.73
S574	196.04	196.86	2.5	2.77
S574	196.86	197.01	13.5	10.5
S574	197.01	197.32	0.15	1.03
S574	197.32	197.56	2.74	25
S575	196.81	197.82	0.08	1.07
S576	151.49	152.74	0.04	0
S576	152.74	153.01	1.54	0.12
S576	153.01	153.44	0.12	0.04
S576	153.44	153.71	2.64	0.01
S577	168.86	169.16	2.49	1.77
S577	169.16	169.62	0.73	0.06
S578	91.29	91.9	0.67	0
S578	91.9	93.39	1.03	0.01
S579	35.97	37.49	0.1	0.02
S579	37.49	39.01	0.1	0.05
S580	31.81	32.76	2.31	0.8
S580	32.76	37.08	0	0
S580	37.08	38.61	1.52	0.44
S580	38.61	39	0.91	0.07
S580	39	39.37	1.67	0.01
S580	39.37	39.67	3.48	0.04
S580	39.67	41.2	0.62	0.05
S580	41.2	42.72	1.23	0.14
S580	42.72	44.12	0.71	0.3
S580	44.12	44.64	1.11	0.04
S580	44.64	44.86	4.09	0.04
S580	44.86	46.38	1.2	0.23
S580	46.38	47.9	1.17	0.19
S580	47.9	49.12	1.63	0.18
S581	41.66	42.42	10.6	0
S581	42.42	43.03	1.93	0
S581	43.03	43.33	8.3	0
S581	43.33	44.86	1.9	0
S581	44.86	45.62	1.14	0
S581	45.62	47.14	5.22	0
S581	47.14	49.06	4.61	0.17
S581	49.06	50.65	7.57	5.72
S581	50.65	51.56	2.59	2.43
S581	51.56	53.57	2.53	7.38
S581	53.57	54	2.15	1.46
S581	54	54.3	1.97	3.81
S581	54.3	56.59	5.07	4.59
S581	56.59	57.11	1.6	0.18
S581	57.11	57.41	1.46	0.62
S607	40.89	42.42	0.32	0.01
S607	42.42	43.94	5.28	0.13
S607	43.94	45.47	3.87	2.81
S607	45.47	46.32	7.94	0.49
S607	46.32	47.84	0.01	0.56

S608	46.68	48.15	0.02	0.06
S608	48.15	48.51	12	38.8
S608	48.51	49.28	6.33	0.02
S608	49.28	50.8	0.07	0.02
S608	50.8	52.32	0.07	0.02
S608	52.32	53.85	0.58	0.01
S608	53.85	54.91	1.58	0.01
S608	54.91	55.28	1.2	0.09
S608	55.28	56.8	2.63	1.22
S608	56.8	58.33	7.44	2.68
S608	58.33	58.66	8.27	10.8
S608	58.66	59.64	3.21	0.06
S608	59.64	61.16	2.62	1.82
S609	77.38	77.77	1.82	0.64
S609	77.77	79.3	1.08	0.09
S609	79.3	80.82	1.34	0.7
S609	80.82	82.22	3.43	2.95
S609	82.22	83.69	2.63	2.59
S609	83.69	84.81	2.58	2.37
S609	84.81	86.74	1.46	2.62
S609	86.74	88.14	2.04	4.48
S609	88.14	89.45	1.34	1.65
S610	61.31	61.92	8.68	26.5
S610	61.92	63.45	0.18	0.11
S610	63.45	65.12	0.18	0.02
S610	65.12	65.95	0.3	0.04
S610	65.95	67.23	0.62	0.46
S610	67.23	68.17	2.1	0.02
S610	68.17	69.54	0.21	0.43
S610	69.54	71.04	2.4	0.87
S610	71.04	72.41	4.72	2.15
S610	72.41	73.93	3.29	2.2
S610	73.93	75.46	2.09	0.88
S610	75.46	75.82	2.09	0.54
S611	47.24	69.19	0	0
S613	70.87	71.38	25.34	20.56
S613	71.38	73	0.68	10.11
S613	73	73.33	0.25	0.63
S613	73.33	74.07	0.12	2.51
S613	74.07	75.59	0.22	2.27
S613	75.59	76.5	0.14	1.06
S614	94.34	95.16	0	1.89
S615	80.1	81.38	1.57	4.72
S615	81.38	82.6	3.31	5.39
S615	82.6	82.9	0.78	4.67
S616	90.7	92.72	2.36	2.75
S617	83.15	84.67	6.67	4.19
S617	84.67	85.04	1.46	0.92
S617	85.04	86.29	0.5	0.15
S618	57.79	59.31	2.14	9.71
S618	59.31	60.83	1.5	7.76
S618	60.83	62.36	0.96	8.09
S618	62.36	63.89	1.48	3.89
S619	80.8	81.08	0.02	0.35
S619	81.08	82.81	0.02	7.27
S619	82.81	83.55	0.01	3.24
S620	70.59	72.6	0.36	10.34
S620	72.6	73.76	0.04	14.17
S621	156.07	157.28	1.02	0.38
S621	157.28	158.34	0.14	0.62
S621	158.34	160.02	1.07	15.5
S621	160.02	160.36	0.58	8.86
S622	142.34	143.86	0.31	0.58
S622	143.86	145.38	0.68	3.58
S622	145.38	146.54	0.55	0.2
S622	146.54	148.44	1.97	0.56
S622	148.44	148.7	0.52	0.4
S622	148.7	149.66	0.03	0.09
S624	71.43	72.95	1.4	14.9
S624	72.95	74.17	0.4	12.8
S624	74.17	74.9	0.2	1.02
S625	101.03	101.54	0.02	0.02
S625	101.54	103.07	0.52	3.16
S626	117.95	119.17	0.12	0.54
S626	119.17	119.66	0.52	3.94
S626	119.66	120.36	0.26	1.9
S626	120.36	121.31	1.06	1.74
S626	121.31	122.83	0.22	0.48
S628	114.76	116.28	22.5	54.3
S628	116.28	116.79	2.04	0.16
S628	116.79	117.04	0.82	0.06
S628	117.04	117.65	1.09	0.05
S628	117.65	118.87	0.41	0.3
S629	136.48	136.97	4.58	0.27
S629	136.97	137.28	1.22	2.44
S629	137.28	138.1	0.07	0.01
S630	37.8	39.62	0.14	0.04
S630	39.62	40.53	0.44	0.1
S630	40.53	42.06	1.04	0.06
S630	42.06	43.58	0.4	0
S630	43.58	45.56	0.44	0.04
S630	45.56	46.63	1.04	0.02
S630	46.63	48.55	1.8	1.82
S630	48.55	50.9	0.46	0.1
S630	50.9	53.12	1.58	0.02
S630	53.12	55.32	0.62	0.02
S630	55.32	56.84	2.28	0.02
S630	56.84	58.52	1.02	0.02
S630	58.52	61.26	2.58	0.04
S630	61.26	63.09	2.96	0.04
S630	63.09	64.62	1.22	0.02
S630	64.62	66.39	3.28	0.12
S630	66.39	67.29	0.4	0.08
S631	36.27	38.55	1.74	0.01
S631	38.55	39.77	0.31	0.01
S631	39.77	41.91	2.12	0.01
S631	41.91	44.05	0.39	0.01
S631	44.05	47.1	1.2	0.01
S631	47.1	50.15	0.08	0.01
S631	50.15	51.67	0.03	0.01
S631	51.67	52.89	0.04	0.01
S631	52.89	55.02	1.16	0.01
S631	55.02	58.07	3.14	0.01
S631	58.07	60.05	1.61	0.01
S631	60.05	62.03	1.51	0.03
S631	62.03	64.63	0.36	0.28
S631	64.63	65.24	0.04	0.04
S631	65.24	66.75	0.01	0.01
S632	35.35	38.4	1.94	0
S632	38.4	41.14	0.4	0
S632	41.14	42.06	1.82	0.18
S632	42.06	43.13	0.64	0.02
S632	43.13	44.19	0.06	0.02
S632	44.19	47.24	0.26	0.01
S632	47.24	49.23	0.28	0.01
S632	49.23	49.99	1.76	1.68
S632	49.99	51.2	0.66	0.04
S632	51.2	52.73	2.11	0.32
S632	52.73	53.6	3.4	2.8
S632	53.6	56.52	4.32	0.48
S632	56.52	58.2	7.96	0
S632	58.2	59.11	0.78	0.01
S632	59.11	61.4	3.42	0.01
S632	61.4	62.46	0.58	0.02
S632	62.46	64.9	0.06	0.04
S632	64.9	67.64	0.42	0.06
S632	67.64	68.41	2.34	2.58
S633	36.72	39.62	0.68	0.02
S633	39.62	42.67	0.3	0.02
S633	42.67	45.41	0.3	0.02
S633	45.41	48.31	0.06	0
S633	48.31	49.83	0.58	0.04
S633	49.83	52.18	0.16	0.02
S633	52.18	53.94	0.04	0.16
S633	53.94	56.99	0.03	0.12
S633	56.99	60.04	0.02	0.09
S634	70.41	71.17	0	0.48
S634	71.17	72.69	6.72	1.33
S634	72.69	75.74	3.55	10.7
S634	75.74	78.33	1.44	5.33
S634	78.33	78.7	0.03	0.28
S634	78.7	80.76	0.02	0.07
S635	88.7	90.52	7.25	2.36
S635	90.52	91.74	9.9	2.39
S635	91.74	93.2	3.26	0.51
S635	93.2	94.18	7.46	3.18
S635	94.18	95.76	0.14	3.62
S635	95.76	98.29	0.02	0.04
S635	98.29	99.06	0.42	5.42
S635	99.06	100.88	0.09	0.02
S636	136.25	137.53	0.39	0.03
S636	137.53	139.21	3.3	1.96
S636	139.21	140.73	14.4	6.44
S636	140.73	142.24	1.96	0.5
S636	142.24	143.61	0.06	0.07
S636	143.61	144.92	3.66	0.25
S636	144.93	146.45	0.86	0.04
S638	86.25	87.78	1.88	2.66
S638	87.78	90.22	5.8	2.68
S639	103.02	103.72	0.03	0.02
S639	103.72	105.98	10.9	7.8
S639	105.98	106.53	1.66	3.72
S640	90	91.43	5.54	0.36
S640	91.43	92.65	0.52	0.42
S641	108.2	111.7	0.05	0.12
S641	111.7	112.47	1.36	4.02
S642	31.37	32.89	0.06	0.44
S642	32.89	34.42	0.13	0.13
S642	34.42	35.94	0.16	2.52
S642	35.94	37.47	0.24	5.25
S642	37.47	38.99	0.06	0.96
S642	38.99	39.75	0.27	0.83
S642	39.75	41.4	0.1	0.03
S642	41.4	43.04	0.52	0.05
S645	32.61	34.14	0.23	0.01
S645	34.14	34.9	0.05	0.01
S645	34.9	35.51	0.01	0.01
S647	27.43	28.95	0.11	0.09
S647	28.95	30.48	0.19	0.05
S647	30.48	32	0.2	0.01
S647	32	33.52	0.58	0.02
S647	33.52	35.04	1.24	0.01
S647	35.04	36.56	0.48	0.02
S647	36.56	37.41	4.46	0.01
S647	37.41	38.69	6.2	0.01
S647	38.69	40.21	2.74	0.02
S647	40.21	40.94	0.8	0.01
S647	40.94	41.73	0.64	0.04
S647	41.73	43.26	1.1	0.03
S647	43.26	44.78	0.31	0.3
S647	44.78	46.3	6.04	0.79
S647	46.3	47.83	6.44	1.12
S647	47.83	49.36	1.22	0.02
S647	49.36	50.88	1.44	0.46
S647	50.88	52.4	0.19	1.5
S647	52.4	53.93	0.68	8.25
S647	53.93	55.09	1.24	2.76
S647	55.09	55.45	0.47	0.01
S647	55.45	56.98	0.2	0.01
S647	56.98	58.5	0.57	0.04
S648	28.04	29.57	0.03	0.08
S648	29.57	31.09	0.14	0.02
S648	31.09	32.61	0.29	0.1
S648	32.61	34.14	0.58	0.08
S648	34.14	35.66	1.22	0.01
S648	35.66	36.73	2.02	0.02
S648	36.73	40.23	3.04	0.01
S648	40.23	41.76	1.42	0.01
S648	43.28	44.81	1.12	0.02
S648	44.81	46.33	1.86	0.01
S648	46.33	47.85	5.2	0.01
S648	47.85	49.38	6.4	1.96
S648	49.38	50.9	0.92	7.04
S648	50.9	52.43	1.07	1
S648	52.43	53.95	2.84	3.28
S648	53.95	55.47	0.49	0.33
S648	55.47	57	1.12	0.38
S648	57	58.52	0.35	0.25
S648	58.52	60.05	0.02	0.01
S648	60.05	61.57	0.05	0.02
S648	61.57	63.09	0.16	0.18
S648	63.09	64.62	0.04	0.02
S648	64.62	66.14	0.01	0.07
S649	27.74	29.26	1.2	0.03
S649	29.26	30.79	3.62	0.01
S649	30.79	32.31	1.48	0
S649	32.31	33.53	2.64	0
S649	33.53	35.05	1.2	0
S649	35.05	36.57	5.68	0
S649	38.86	40.23	2.56	0.02
S649	40.23	41.76	7.6	0.03
S649	41.76	43.28	0.66	0
S649	43.28	44.81	3.1	0
S649	44.81	46.33	4.04	0
S649	46.33	47.85	0.9	0
S649	47.85	49.38	2.28	0
S649	49.38	50.9	2.36	0.06
S649	50.9	52.43	1.18	2.14
S649	52.43	53.19	0.85	1.62
S649	53.19	53.95	0.88	0.69
S649	53.95	55.47	0.88	0.69
S649	55.47	57	0.9	0.19
S649	57	58.52	0	0.01
S649	58.52	59.38	0.26	0.84
S649	59.38	62.36	0.03	0.32
S649	62.36	63.7	0.21	0.08
S649	63.7	63.95	0	0
S649	63.95	64.62	0.12	0.32
S650	25.78	28.83	0.1	0.02
S650	28.83	30.35	0.42	0.01
S650	30.35	33.37	0.6	0.01
S650	33.37	34.68	0.21	0.01
S650	34.68	37.73	1.94	0.12
S650	37.73	39.83	0.45	0.01
S650	39.83	43.58	0.94	0.02
S650	43.58	44.37	0.05	0.14
S650	44.37	45.26	0.7	8.18
S650	45.26	45.87	0.04	0.96
S650	45.87	46.75	0.29	0.68
S650	46.75	49.46	0.02	0.25
S650	49.46	51.35	0.44	1.98
S651	27.98	29.57	0.06	0.05
S651	29.57	30.78	1.18	0.01
S651	30.78	32.19	2.38	0
S651	32.19	33.89	2.16	0.01
S651	33.89	35.42	2.1	0.01
S651	35.42	36.88	3.72	0
S651	36.88	38.4	1.22	0
S651	38.4	40.23	1.18	0.02
S651	40.23	41.76	0.26	0.01
S651	41.76	44.81	0.21	0
S651	44.81	47.85	1.1	1.12
S651	47.85	50.9	0.46	0.27
S651	50.9	53.95	0.07	1.11
S651	53.95	57	0	0.1
S651	57	60.05	0.02	0
S651	60.05	62.03	0.02	0.02
S651	62.03	63.8	0	0
S651	63.8	65.53	0	0.01
S652	31.09	32.61	0.08	0.03
S652	32.61	35.66	0.01	0.01
S652	35.66	38.71	0.02	0.01
S652	38.71	41.76	0.04	0.04
S652	41.76	44.81	0.03	0.08
S652	44.81	47.85	0.44	0.06
S652	47.85	49.38	1.74	0.02
S652	49.38	50.9	5.46	0.01
S652	50.9	52.43	6.6	0.01
S652	52.43	53.95	3.34	0.02
S652	53.95	55.47	3.5	0.01
S652	55.47	57	1.66	0.02
S652	57	58.52	2.38	0.03
S652	58.52	60.05	0.98	0.22
S652	60.05	61.57	0.72	1.04
S652	61.57	63.1	2.3	3.4
S652	63.1	63.68	4.45	19.1
S652	63.68	64.9	1.18	2.86
S652	64.9	66.29	1.29	0.84
S652	66.29	67.67	0.52	1.94
S652	67.67	69.19	1.36	1.96
S652	69.19	70.71	2.32	1.94
S652	70.71	72.24	0.21	1.78
S652	72.24	73.76	0.03	0.01
S652	73.76	75.29	0	0
S652	75.29	76.5	0.06	0.11
S652	76.5	78.03	0.03	0.03
S652	78.03	79.4	0.01	0.01
S652	79.4	81.38	0	0
S652	81.38	82.91	0	0
S653	28.2	29.12	0.07	0.02
S653	29.12	29.63	0.08	0.02
S653	29.63	32.68	0.21	0.01
S653	32.68	35.73	0.28	0.01
S653	35.73	38.78	0.44	0.01

S653	38.78	40.79	0.78	0.01
S653	40.79	41.62	2.02	0.01
S653	41.62	44.51	0.72	0.01
S653	44.51	47.56	0.37	0.01
S653	47.56	50.3	0.7	0.03
S653	50.3	53.81	0.34	0.01
S653	53.81	54.57	0.67	0.01
S653	54.57	57.56	0.19	0.54
S653	57.56	58.35	0.01	0.59
S653	58.35	59.54	0.01	0.76
S653	59.54	60.43	0.01	4.2
S653	60.43	62.59	0.01	0.99
S653	62.59	64.94	0.01	0.96
S653	64.94	65.91	0.34	0.83
S653	65.91	67.68	0.98	3.66
S653	67.68	70.46	0.21	0.56
S653	70.46	71.8	0.01	0.01
S653	71.8	74.85	0.01	0.01
S653	74.85	76.37	0.01	0.01
S655	75.28	76.8	5.88	5.22
S655	76.8	79.55	1.02	6.84
S655	79.55	80.46	0.03	0.01
S656	121.12	122	2.74	2.12
S656	122	123.52	5.3	9.75
S657	109.58	112.78	0.41	0.07
S659	131.92	133.29	0.86	0.29
S659	133.29	134.72	0.47	0.04
S659	134.72	136.34	0.51	0.03
S659	136.34	136.7	0.3	0.02
S659	136.7	137.76	7.08	0.02
S659	137.76	139.29	0.29	0.01
S660	134.87	136.39	0.57	1.77
S660	136.39	138.37	0.1	0.03
S660	138.37	138.98	3.35	2.64
S661	123.38	125.94	2.62	0.17
S662	118.56	120.39	0.98	0.05
S662	120.39	121.92	2.15	0.21
S662	121.92	123.44	9.15	1.46
S662	123.44	125.72	3.3	0.07
S662	125.72	126.33	19.1	0.02
S662	126.33	128.02	0.8	0.03
S663	38.1	39.01	1.16	0.01
S663	39.01	40.54	5.92	0.01
S663	40.54	42.06	2.26	0
S663	42.06	42.67	3.01	0.14
S663	42.67	45.11	1.14	0.46
S663	45.11	46.48	2.04	0.42
S663	46.48	48	4.58	0.95
S663	48	49.53	7.3	7.38
S663	49.53	51.05	2.96	1.28
S663	51.05	52.58	4.72	2.36
S663	52.58	54.1	4.38	0.62
S663	54.1	55.63	0	0.01
S664	34.44	35.97	0.44	0.02
S664	35.97	37.49	0.37	0
S664	37.49	39.01	0.34	0.01
S664	39.01	40.54	0.42	0.02
S664	40.54	42.06	1.06	0.14
S664	42.06	43.59	0.04	0.01
S664	43.59	45.57	0.9	0.02
S664	45.57	46.79	1.33	0.07
S664	46.79	48.31	2.74	0.92
S664	48.31	49.83	1.52	0.13
S664	49.83	51.56	3.82	0.17
S664	51.56	52.88	2.02	0.98
S664	52.88	54.41	1.78	0.39
S664	54.41	55.93	1.65	0.63
S664	55.93	57.61	2.28	0.74
S664	57.61	59.28	1.44	0.13
S666	91.35	93.42	0.84	0.12
S666	93.42	95.1	0.51	0.11
S666	95.1	96.01	2.84	0.07
S666	96.01	97.29	0.79	0.15
S666	97.29	99.67	1.18	0.05
S667	70.1	72.24	2.36	0.07
S667	72.24	74.98	2.08	0.01
S668	36.88	38.4	2.64	0.01
S668	38.4	39.93	2.66	0.01
S668	39.93	41.45	1.82	0.01
S668	41.45	42.97	2.52	0.01
S668	42.97	44.5	2.26	0.11
S668	44.5	46.02	3.18	0.02
S668	46.02	47.54	1.42	0.07
S668	47.54	49.07	0.36	0.01
S668	49.07	50.69	0.89	0.01
S668	50.69	52.22	0.33	0
S668	52.22	53.74	0.94	0
S668	53.74	55.27	0.02	0.02
S668	55.27	56.79	0.07	0.02
S668	56.79	58.32	0	0.06
S668	58.32	59.84	0.03	0.11
S668	59.84	61.37	0.09	0.04
S668	61.37	62.89	0.1	0.12
S668	62.89	64.42	0	0.05
S668	64.42	65.94	0.01	0.04
S668	65.94	67.46	0	0.03
S669	38.71	41.75	1.05	0.01
S669	41.75	44.8	0.82	0.01
S669	44.8	47.85	0.36	0.01
S669	47.85	50.9	0.64	0.01
S669	50.9	53.94	0.19	0.01
S669	53.94	56.99	0.48	0.01
S670	35.97	37.49	1.54	0.01
S670	37.49	39.01	1.96	0.01
S670	39.01	40.53	2.02	0
S670	40.53	42.06	2.76	0
S670	42.06	43.58	2.38	0.16
S670	43.58	45.11	1.99	0.01
S670	45.11	46.63	2.62	0
S670	46.63	48.15	1.44	0.02
S670	48.15	49.68	1.02	0.07
S670	49.68	51.2	0.51	0.04
S670	51.2	52.12	0.7	0.01
S671	36.73	38.25	1.58	0.02
S671	38.25	39.77	0.41	0.08
S671	39.77	40.78	0.43	0.01
S671	40.78	42.36	0.4	0.01
S671	42.36	43.73	2.34	0.01
S671	43.73	45.26	1.72	0.02
S671	45.26	46.93	0.59	0.08
S671	46.93	48.15	0.19	0.03
S671	48.15	49.68	0.56	0.02
S671	49.68	51.2	1.47	0.21
S671	51.2	52.88	1.28	0.25
S671	52.88	54.4	0.7	0.01
S671	54.4	55.56	1.74	0.01
S671	55.56	56.26	5.04	0.01
S671	56.26	57.85	1.42	0.01
S671	57.85	59.52	1.29	0.01
S671	59.52	61.35	0.52	0.02
S672	32.36	33.88	2.03	0.01
S672	33.88	35.41	1.22	0.01
S672	35.41	36.93	0.63	0.01
S672	36.93	38.45	0.79	0.01
S673	64.01	66.69	1.68	16.7
S673	66.69	68.12	7.8	21.7
S673	68.12	69.49	12.1	5.4
S673	69.49	71.01	7.15	0.11
S673	71.01	72.54	7.5	1.32
S673	72.54	74.06	8.45	3.28
S673	74.06	75.43	3.88	0.36
S673	75.43	77.41	0.07	0.02
S673	77.41	78.85	3.64	0.31
S673	78.85	80.16	0.11	0.08
S673	80.16	81.68	0.09	0.03
S673	81.68	83.21	0	0.03
S673	83.21	84.73	0	0.01
S673	84.73	86.86	0	0
S674	28.34	30.48	0.29	0.01
S674	30.48	32.61	1.07	0.02
S674	32.61	34.13	2.04	0.02
S674	34.13	35.66	2.1	0.01
S674	35.66	37.18	1.24	0.01
S674	37.18	38.7	1.04	0.01
S674	38.7	40.23	2.54	0.03
S674	40.23	41.75	0.9	0.06
S674	41.75	43.28	0.61	0.07
S674	43.28	44.8	0.1	0.02
S674	44.8	47.85	0.38	0.16
S674	47.85	50.9	1.46	1.37
S674	50.9	52.42	0.69	0.01
S674	52.42	53.94	0.8	0.1
S674	53.94	55.47	0.41	0.13
S674	55.47	56.99	0.73	0.43
S674	56.99	58.82	0.74	0.25
S675	30.48	33.52	0.69	0.05
S675	33.52	35.66	1.7	0.01
S675	35.66	37.18	1.98	0.01
S675	37.18	38.7	0.89	0.32
S675	38.7	39.77	3.48	0.08
S675	39.77	42.82	2.02	2.54
S675	42.82	44.34	1.18	0.16
S675	44.34	47.34	0.8	0.16
S675	47.34	48.1	1.03	0.31
S675	48.1	49.63	1.96	1.01
S675	49.63	51.15	4.18	2.65
S675	51.15	52.68	5.1	6.18
S675	52.68	53.71	2.26	0.68
S675	53.71	55.24	0.27	0.5
S676	37.79	38.7	2.33	1.38
S676	38.7	41.75	2.42	0.55
S676	41.75	44.8	1.72	0.22
S676	44.8	46.63	0.83	0.78
S676	46.63	47.85	1.65	0.55
S676	47.85	50.9	0.99	2.88
S676	50.9	53.95	0.43	0.16
S676	53.95	56.99	0.61	0.11
S676	56.99	60.04	0.59	0.08
S676	60.04	61.56	0.96	0.01
S676	61.56	64.62	0.69	0.02
S676	64.62	67.05	2.16	0.02
S676	67.05	68.58	1.34	0.03
S676	68.58	69.49	6.12	0.05
S676	69.49	72.23	1.03	0.37
S676	72.23	73.76	1.12	0.47
S676	73.76	75.28	0.16	0.7
S676	75.28	78.33	0.51	0.58
S676	78.33	80.46	0.27	0.72
S677	75.28	78.33	3.24	1.38
S677	78.33	81.38	3.06	1.52
S677	81.38	87.47	1.16	0.37
S677	87.47	90.52	17.6	0.65
S677	90.52	93.57	13.7	0.51
S677	93.57	94.48	3.87	6.95
S677	94.48	95.85	0.86	1.83
S678	31.09	31.7	0.84	2.1
S678	31.7	32.31	0	0
S678	32.31	33.22	0.99	0.31
S678	33.22	35.66	1.93	1.14
S678	35.66	37.95	1.62	0.48
S678	37.95	39.62	1.98	1.46
S678	39.62	41.15	1.92	4.26
S678	41.15	42.67	2.55	6.65
S678	42.67	43.59	0.89	1.86
S678	43.59	44.81	0.37	0.85
S678	44.81	46.33	0.62	1.36
S679	26.37	27.43	0.8	0.18
S679	27.43	28.95	0.33	0.22
S679	28.95	32	1.48	0.45
S679	32	35.05	1.18	1.61
S679	35.05	36.36	0.81	0.66
S679	36.36	37.18	0.67	0.05
S679	37.18	39.01	0.13	0.07
S681	67.36	68.88	4.76	0.38
S681	68.88	71.17	4.7	2.91
S684	26.21	26.82	2.94	0.45
S684	26.82	29.87	0.53	0.01
S684	29.87	32.91	0.32	0.03
S684	32.91	34.74	0.09	0.19
S684	34.74	35.81	0.17	0.08
S684	35.81	37.18	0.32	0.01
S684	37.18	38.71	0.03	0.04
S685	60.5	62.03	1.04	0.06
S685	62.03	63.86	0.6	0.02
S685	63.86	65.99	2.85	0.05
S685	65.99	67.06	3.58	0.05
S686	74.68	76.2	28.1	45.8
S686	76.2	77.72	45.7	17.9
S686	77.72	78.64	19.3	46.3
S686	78.64	79.85	7.44	2.34
S686	79.85	80.62	6.78	1.16
S687	22.56	25.6	0.42	0.41
S687	25.6	26.67	2.44	0.02
S687	26.67	29.71	1.88	0.46
S687	29.71	32.76	1.53	0.39
S687	32.76	33.68	0.6	0.09
S687	33.68	35.66	2.2	1.19
S687	35.66	37.19	0.53	0.09
S687	37.19	39.01	0.21	0.11
S688	99.43	100.94	0.14	0.41
S688	100.94	102.63	0.42	0.23
S688	102.63	104.73	2.52	2.24
S688	104.73	105.16	0.53	1.92
S689	76.63	77.23	0	0
S689	77.23	79.67	9.7	0.06
S690	42.97	44.5	2.24	0.65
S690	44.5	46.02	2.03	1.27
S690	46.02	47.54	1.07	0.53
S690	47.54	49.07	0.91	1.12
S690	49.07	50.59	0.8	0.98
S690	50.59	52.12	1.44	0.96
S690	52.12	53.64	3.72	0.34
S690	53.64	55.16	4.55	0.15
S690	55.16	56.69	2.13	0.18
S690	56.69	57.6	11.7	0.09
S690	57.6	58.52	25.6	2.74
S690	58.52	60.04	22.6	46.2
S690	60.04	60.96	43.8	19.8
S690	60.96	61.56	10.8	0.12
S690	61.56	63.09	48.2	2.98
S690	63.09	64	45.6	1.72
S690	64	65.53	14.2	0.47
S690	65.53	67.05	10.7	1.87
S690	67.05	68.58	15.8	0.5
S690	68.58	70.1	4.56	3.46
S690	70.1	71.62	3.26	0.75
S690	71.62	73.15	1.58	2.52
S690	73.15	74.67	1.79	2.21
S690	74.67	76.5	1.44	2.34
S691	71.78	73.15	8.9	0.46
S691	73.15	74.06	24.9	1.93
S691	74.06	76.2	43.2	0.8
S691	76.2	78.18	11.6	0.41
S691	78.18	79.55	9.15	0.13
S691	79.55	81.07	2.31	0.08
S691	81.07	82.29	5.34	1.51
S691	82.29	83.81	2.88	2.15
S691	83.81	85.33	1.76	2.78
S691	85.33	86.86	2.13	6.24
S691	86.86	87.47	3.02	4.68
S691	87.47	89.3	0.43	0.89
S692	101.8	102.26	0.55	0.36
S692	102.26	103.62	13.1	11.7
S692	103.62	104.08	3.16	2.11
S692	104.08	105.46	0.13	0.49
S692	105.46	107.44	0.67	1.48
S692	107.44	109.72	0.06	0.07
S692	109.72	112.77	0.2	0.66
S692	112.77	114.39	0.36	0.81
S692	114.39	114.51	4.13	59.3
S693	33.52	35.05	1.04	0.39
S693	35.05	36.57	1.98	0.26
S693	36.57	39.62	1.73	0.04
S693	39.62	41.14	1.34	0.11
S693	41.14	42.67	0.72	0.12
S693	42.67	44.19	3.92	3.16
S693	44.19	45.72	0.98	0.26
S693	45.72	48.76	0.87	1.39
S693	48.76	51.81	0.54	0.06
S693	51.81	54.86	1.33	0.16
S693	54.86	57.91	0.97	0.16
S693	57.91	60.96	1.12	0.29
S693	60.96	62.48	1.65	0.03
S693	62.48	64.61	4.54	0.01
S694	36.57	38.86	0.56	0.47
S694	38.86	41.3	1.14	0.25
S694	41.3	43.43	4.52	1.76
S694	43.43	45.41	3.54	0.72
S694	45.41	46.93	1.31	0.33
S694	46.93	48.4	1.38	0.87
S694	48.4	50.23	2.66	1.04
S694	50.23	51.75	1.82	0.13
S694	51.75	53.28	0.59	0.11
S694	53.28	54.8	0.52	0.08

S694	54.8	55.71	0.59	0.04
S694	55.71	57.85	3.32	0.02
S694	57.85	59.37	4.76	0.03
S694	59.37	60.9	1.87	0.02
S694	60.9	62.42	3.48	0.03
S694	62.42	63.94	12.7	0.05
S694	63.94	65.47	9.75	0.14
S694	65.47	66.99	4.2	0.15
S694	66.99	68.52	2.92	0.05
S694	68.52	70.04	2.88	0.53
S694	70.04	71.56	1.06	0.09
S694	71.56	72.78	1.12	0.41
S694	72.78	74.61	0.76	0.69
S694	74.61	76.14	1.73	1.64
S694	76.14	77.66	1.64	2.26
S694	77.66	79.18	1.03	0.89
S694	79.18	80.71	1.72	2.68
S694	80.71	82.23	0.63	1.36
S695	41.75	43.28	4	0.48
S695	43.28	44.8	4.04	0.86
S695	44.8	46.32	4.06	2.72
S695	46.32	47.85	1.36	0.64
S695	47.85	49.37	3.54	0
S695	49.37	50.9	2.56	0.06
S695	50.9	52.42	2.84	0.66
S695	52.42	53.94	3.62	0.12
S695	53.94	55.47	5.34	0.02
S695	55.47	56.99	7.42	0.06
S695	56.99	58.52	8.12	0.02
S695	58.52	60.04	6.9	0.06
S695	60.04	61.56	3.12	0.01
S695	61.56	63.09	6.48	0.02
S695	63.09	64.61	11.7	0.18
S695	64.61	66.75	4.84	0.01
S695	66.75	67.66	0.96	0.26
S695	67.66	69.18	2.92	0.52
S695	69.18	70.71	0.67	0.18
S695	70.71	71.93	2.58	1.02
S695	71.93	73.76	8.32	6.52
S695	73.76	75.43	6.54	7.42
S695	75.43	76.8	1.25	1.42
S695	76.8	78.02	0.87	1.74
S696	41.75	42.36	0.42	0.77
S696	54.56	55.78	3.7	7.76
S696	55.78	56.24	1.6	10.8
S696	56.24	57.3	6.15	41.8
S696	57.3	59.44	2.84	6.96
S696	59.44	59.89	3.95	52.1
S696	59.89	60.35	5.36	6.08
S696	60.35	61.87	27.5	21.1
S696	61.87	63.4	38.5	23.2
S696	63.4	64.92	50.5	12.1
S696	64.92	66.45	46.8	7.06
S696	66.45	67.97	56.2	0.21
S696	67.97	69.49	37	18.2
S696	69.49	71.01	27	53.1
S696	71.01	72.54	39.5	20.2
S696	72.54	74.37	34.1	33.6
S696	74.37	75.9	5.96	0.02
S696	75.9	77.42	12.6	0.78
S696	77.42	78.94	7	1.22
S696	78.94	80.47	3.96	1.78
S696	80.47	81.99	4.18	0.76
S696	81.99	83.36	2.38	2.1
S696	83.36	84.43	2.3	1.4
S696	84.43	86.26	0.44	2.4
S696	86.26	87.78	1.56	1.34
S697	39.62	41.14	0.91	0.02
S697	41.14	42.67	2.68	0.13
S697	42.67	44.19	1.66	0.01
S697	44.19	45.72	3.64	0.01
S697	45.72	46.93	2.85	0.01
S697	46.93	48.46	3.28	4.28
S697	48.46	49.98	3.36	0.48
S697	49.98	51.2	1.74	4.36
S697	51.2	54.25	0.52	0.23
S697	54.25	57.3	0.41	0.1
S697	57.3	60.35	0.07	0.05
S697	60.35	63.39	0.26	0.03
S697	63.39	64.92	0.21	0.07
S697	64.92	66.44	2.52	0.47

S697	66.44	67.97	4.19	1.27
S697	67.97	69.49	0.69	0.25
S697	69.49	71.01	0.31	0.02
S697	71.01	72.23	0.28	0.05
S697	72.23	75.28	1.73	0.17
S697	75.28	76.8	1.41	0.35
S697	76.8	80.46	0.03	0.04
S698	83.51	84.73	24.5	0.72
S698	84.73	85.95	48.5	5.28
S698	85.95	87.47	21.4	4.04
S698	87.47	88.39	15.4	9.56
S698	88.39	89.61	3.4	1.44
S698	89.61	91.44	1.06	0.66
S698	91.44	94.48	1.66	0.9
S698	94.48	96.92	2.68	0.58
S699	72.23	74.98	1.2	0.2
S699	74.98	76.5	0.52	0.16
S699	76.5	78.02	0.56	1.2
S699	78.02	79.55	2.34	0.48
S699	79.55	81.07	6.7	1.1
S699	81.07	83.05	5.38	1.12
S699	83.05	85.34	0.46	0.56
S699	85.34	87.47	5.26	2
S699	87.47	88.39	0.08	0.12
S699	88.39	90.52	3.78	3.22
S699	90.52	92.04	0.6	0.24
S700	61.56	61.87	1.13	0.47
S700	61.87	62.78	2.64	1.09
S700	62.78	64.31	0.93	0.08
S700	64.31	65.83	1.68	0.17
S700	65.83	67.36	1.86	0.55
S700	67.36	68.88	1.47	0.24
S700	68.88	70.4	2.24	0.02
S700	70.4	71.93	3.2	0.27
S700	71.93	73.45	5.18	0.95
S700	73.45	74.98	4.56	1.81
S700	74.98	76.5	3.24	1.28
S700	76.5	78.02	1.64	0.47
S700	78.02	79.85	1.04	0.63
S700	79.85	81.38	0.74	2.76
S700	81.38	82.29	0.98	3.22
S701	60.65	62.48	0.57	0.12
S701	62.48	64	0.69	0.08
S701	64	65.53	0.76	0.09
S701	65.53	67.05	0.43	0.16
S701	67.05	68.58	2.08	0.73
S701	68.58	70.1	1.61	0.04
S701	70.1	71.62	0.43	0.43
S701	71.62	73.15	0.19	0.51
S701	73.15	74.67	0.3	0.35
S701	74.67	76.2	0.12	0.08
S701	76.2	77.11	0.21	0.05
S701	77.11	78.63	1.36	0.06
S701	78.63	79.85	1.88	0.15
S701	79.85	80.76	1.79	0.03
S702	35.66	36.88	0.9	0.02
S702	36.88	38.4	1.34	0.01
S702	38.4	39.92	2.02	0.01
S702	39.92	41.45	2.74	0.04
S702	41.45	42.97	1.96	0.01
S702	42.97	44.5	3.26	0.04
S702	44.5	46.02	2.36	0.06
S702	46.02	47.54	1.14	0.02
S702	47.54	49.07	2.28	0.02
S702	49.07	50.59	3.28	0.01
S702	50.59	52.12	1.68	0.04
S702	52.12	53.64	0.78	0.02
S702	53.64	55.16	0.36	0.01
S702	55.16	56.69	0.5	0.01
S702	56.69	58.21	0.24	0.01
S702	58.21	59.43	0.62	0.01
S702	59.43	60.96	2.66	0.02
S702	60.96	62.48	1.07	0.01
S702	62.48	64	1.52	0.01
S702	64	65.53	1.55	0.03
S702	65.53	67.05	0.93	0.01
S702	67.05	68.58	2.5	0.55
S702	68.58	70.1	1.36	1.06
S702	70.1	71.62	0.13	0.31
S702	71.62	73.15	0.59	0.49
S702	73.15	74.67	0.68	0.26

S702	74.67	75.59	0.6	0.06
S703	75.59	76.5	0.21	0.26
S703	76.5	78.03	4.76	0.23
S703	78.03	79.55	3.95	0.95
S703	79.55	81.08	4.28	0.05
S703	81.08	82.6	1.39	0.04
S703	82.6	84.12	1.17	2.36
S703	84.12	85.64	1.28	1.64
S703	85.64	87.17	2.06	2.1
S703	87.17	89	2.56	2.18
S703	89	91.13	0.05	5.72
S704	71.62	73.45	1.08	0.96
S704	73.45	74.98	2.52	0.26
S704	74.98	76.5	1.84	0.22
S704	76.5	78.02	0.32	0.62
S704	78.02	78.48	12.8	1.38
S704	78.48	79.55	49	20.4
S704	79.55	81.07	53	12.8
S704	81.07	82.6	54	14.7
S704	82.6	83.51	0	0
S704	83.51	84.12	13.2	2.42
S704	84.12	85.64	1.76	0.62
S704	85.64	87.17	3.76	2.76
S704	87.17	88.69	6.2	4.96
S704	88.69	90.22	2.22	3.36
S704	90.22	90.98	1.12	0.68
S704	90.98	92.65	0.32	0.1
S704	92.65	94.18	0.36	0.06
S704	94.18	95.7	1.34	1.22
S705	47.55	47.7	16.6	35.6
S705	47.7	50.59	2.68	0.09
S705	50.59	53.64	1.76	0.28
S705	53.64	55.16	0.46	0.07
S708	53.03	56.08	0.14	0.05
S708	56.08	57.91	0.46	0.22
S708	57.91	59.43	1.07	0.21
S708	59.43	60.65	0.74	0.05
S708	60.65	62.17	9.14	0.3
S708	62.17	63.09	5.06	0.42
S708	63.09	64.61	1.32	0.72
S708	64.61	66.44	1.66	0.32
S708	66.44	69.18	0.4	0.37
S709	100.28	101.5	2.53	0.04
S710	132.13	132.59	4.18	0.04
S712	79.25	79.86	32.2	17.4
S712	79.86	81.08	8.12	7.16
S712	81.08	82.3	4.24	1.23
S712	82.3	83.82	1.21	2.59
S713	137.22	137.65	3.62	10.2
S713	137.65	139.17	0.19	0.11
S713	139.17	141.12	0.42	0.51
S713	141.12	142.49	1.68	1.32
S713	142.49	144.72	3.86	1.79
S713	144.72	145.45	2.52	0.49
S713	145.45	146.06	1.24	0.11
S713	146.06	147.68	0.19	0.46
S714	75.29	77.21	0.25	0.63
S714	77.21	79.68	0.21	0.31
S714	79.68	80.68	2.04	0.84
S714	80.68	81.14	55.6	0.54
S714	81.14	81.87	19.8	3.42
S714	81.87	83.72	4.28	0.35
S714	83.72	85.3	1.28	0.27
S714	85.3	86.67	8.74	1.73
S714	86.67	88.13	3.28	2.26
S715	103.02	104.24	60.3	0.01
S715	104.24	104.85	24.8	0.05
S715	104.85	105.46	54.8	2.8
S715	105.46	107.29	8.18	2.58
S715	107.29	108.2	2.6	0.21
S716	81.38	82.45	27.4	26.3
S716	82.45	84.43	11.8	4.6
S716	84.43	85.65	5.68	3.02
S716	85.65	87.17	3.52	3.2
S718	98.63	99.97	16.4	10.8
S718	99.97	102.62	6.36	7.68
S718	102.62	103.66	1.7	0.52
S718	103.66	105.67	3.74	0.63
S718	105.67	106.19	1.35	0.79
S720	74.49	75.68	0.09	0.15
S720	75.68	77.57	3.08	0.84

S720	77.57	79.16	0.67	0.92
S723	93.27	94.27	22.1	55.6
S723	94.27	96.74	45.2	18.1
S723	96.74	97.14	12.6	60.9
S723	97.14	98.42	5.92	3.52
S723	98.42	99.06	2.03	1.07
S723	99.06	100.89	1.92	0.89
S724	100.13	100.59	10.7	3.22
S724	100.59	100.9	23.7	7.78
S724	100.9	102.42	5.86	1.04
S724	102.42	103.95	6.76	5.44
S724	103.95	104.56	6.1	0.56
S724	104.56	105.47	2	2.8
S724	105.47	106.99	1.48	0.26
S724	106.99	108.52	0.9	2.58
S724	108.52	110.35	0.28	0.52
S725	75.59	77.11	0.62	0.22
S725	77.11	78.64	0.98	0.06
S725	78.64	80.16	2.26	0.18
S725	80.16	81.69	0.8	0.04
S725	81.69	83.21	1	0.02
S725	83.21	84.74	0.16	0.02
S725	84.74	86.26	2.86	0
S725	86.26	87.79	1.1	0.08
S725	87.79	89.31	2.88	0.36
S725	89.31	90.84	3.72	0.62
S725	90.84	92.67	1.08	0.06
S726	77.72	83.82	2.73	1.01
S726	83.82	85.34	18.6	1
S726	85.34	86.87	9.85	0.03
S726	86.87	87.87	3.06	0.1
S726	87.87	89.52	8.15	0.66
S726	89.52	92.81	2.76	0.26
S726	92.81	95.86	0.53	0.24
S726	95.86	98.91	1.88	0.47
S726	98.91	101.35	1.12	0.32
S726	101.35	103.48	0.05	0.37
S727	105.46	105.61	30.4	26.2
S727	105.61	107.9	3.02	2.91
S727	107.9	109.42	1.6	3.32
S727	109.42	111.71	2.28	3.28
S727	111.71	113.08	0.83	0.7
S727	113.08	113.69	5.1	1.29
S727	113.69	115.22	1.21	0.66
S728	100.5	101.9	32.6	31.2
S728	101.9	103.1	8.88	11.1
S728	103.1	103.5	12.9	32.8
S728	103.5	104.9	2.97	1.17
S729	41.46	44.51	2.6	1.38
S729	44.51	46.36	2.63	0.08
S729	46.36	47.56	3.38	0.89
S729	47.56	50.61	0.85	0.13
S729	50.61	52.61	0.62	0.04
S729	52.61	53.66	1.02	0.1
S729	53.66	55.16	1.93	0.12
S729	55.16	56.71	2.98	0.02
S729	56.71	59.66	0.33	0.03
S729	59.66	62.81	0.31	0.01
S729	62.81	65.56	2.13	0.05
S729	65.56	68.41	0.54	0.03
S729	68.41	71.46	3.87	2.42
S729	71.46	74.75	2.16	0.35
S729	74.75	76.76	3.12	1.96
S729	76.76	78.75	1.92	2.09
S729	78.75	79.8	0.22	0.39
S729	79.8	81.89	0.79	0.56
S730	84.14	87.19	0.71	0.41
S730	87.19	87.59	29.6	10.3
S730	87.59	89.59	7.82	0.56
S730	89.59	91.09	1.67	0.05
S730	91.09	91.79	3.6	0.09
S730	91.79	94.49	8.66	1.03
S730	94.49	95.49	2.06	3.72
S730	95.49	97.99	2.79	2.38
S730	97.99	98.74	2.76	0.11
S730	98.74	99.9	0.26	0.5
S730	99.9	102	0.31	0.22
S731	65.85	69.5	0.46	0.59
S731	69.5	71.94	0.38	0.91
S731	71.94	79.7	0.63	0.35
S731	79.7	80.4	34	15

S731	80.4	81.09	16.7	0.91
S731	81.09	82.59	3.46	0.21
S731	82.59	84.09	2.29	0.06
S731	84.09	85.59	14.3	0.53
S731	85.59	87.09	1.82	0.28
S731	87.09	88.99	3.52	0.84
S731	88.99	91.14	7.12	3.52
S731	91.14	92.58	1.98	0.59
S732	93.74	94.05	13.2	11.4
S732	94.05	95.5	3.86	3.14
S732	95.5	97.6	2.06	3.18
S733	34.91	38.11	0.17	0.02
S733	38.11	41.16	0.15	0.01
S733	41.16	44.51	0.1	0.1
S733	44.51	50.58	0.15	0.03
S733	50.58	59.78	0.24	0.04
S733	59.78	68.89	0.65	0.06
S733	68.89	71.94	0.92	0.01
S733	71.94	74.99	0.03	0.02
S733	74.99	76.2	0.05	0.01
S734	142.4	144.2	0.9	0.79
S734	144.2	144.7	1.23	0.5
S734	144.7	145.3	1.02	12.8
S734	145.3	146	5.02	3.66
S734	146	148.78	9.06	4.82
S734	148.78	149.5	0.24	8.34
S734	149.5	150.5	0.04	0.43
S734	150.5	151.83	0.22	0.21
S735	117.68	119.23	0.91	0.41
S735	119.23	121.93	11.3	3.64
S735	121.93	124.58	3.27	0.69
S735	124.58	126	6.35	3.62
S735	126	128.2	1.26	0.79
S735	128.2	128.98	3.22	8.35
S736	93.29	94.74	3.68	2.76
S736	94.74	96.64	0.27	0.16
S736	96.64	99.38	0.19	0.12
S736	99.38	102.2	0.07	0.22
S736	102.2	102.43	0.7	14.2
S736	102.43	103.03	0.09	1.62
S737	64.24	65.24	0.54	0.84
S737	65.24	68.29	0.87	0.29
S737	68.29	69.39	0.62	0.12
S737	69.39	71.39	0.58	0.03
S737	71.39	74.39	0.45	0.08
S737	74.39	77.44	0.6	0.2
S737	77.44	80.49	0.17	0.64
S737	80.49	83.54	1.56	0.16
S737	83.54	84.04	1.38	0.23
S738	108.53	112.38	5.18	0.27
S738	112.38	114.02	0.88	0.35
S739	84.16	85.97	2.92	0.46
S739	85.97	87.8	0.33	0.29
S739	87.8	89	3.02	4.36
S739	89	91.48	2.32	7.16
S739	91.48	93.68	2.29	3.56
S740	114.64	117.69	1.37	0.11
S740	117.69	118.29	53.1	9.85
S740	118.29	120.74	11.2	2.52
S740	120.74	122	4.43	2.56
S740	122	122.6	2.52	2.09
S801	6.34	7.24	2.47	0.1
S801	7.24	8.54	1.48	0.06
S801	8.54	10.06	2.93	0.01
S801	10.06	11.59	2.57	0.01
S801	11.59	13.09	1.78	0.01
S801	13.09	14.63	0.51	0.01
S801	14.63	16	0.55	0.01
S801	16	17.68	0.33	0.01
S801	17.68	19	0.02	0.01
S801	19	20	0.03	0.01
S802	6.35	7	0.25	0.03
S802	7	8.54	1.67	0.01
S802	8.54	10.04	2.22	0.01
S802	10.04	11.59	2.66	0.01
S802	11.59	12.3	3.94	0.01
S802	12.3	13.09	2.37	0.01
S802	13.09	14.63	0.48	0.05
S802	14.63	16	0.24	0.02
S802	16	17.68	0.38	0.02
S802	17.68	19	0.38	0.01

S802	19	20.5	0.08	0.01
S802	20.5	21.3	0.23	0.01
S803	4.43	5.49	3.34	0.04
S803	5.49	6.8	4.88	0.02
S803	6.8	7.49	1.9	0.02
S803	7.49	8.54	1.63	0.02
S803	8.54	10.06	0.9	0.01
S803	10.06	10.75	2.2	0.01
S803	10.75	11.59	0.5	0.01
S803	11.59	13.09	0.7	0.01
S804	6.75	8.54	0.12	0.04
S804	8.54	10.06	0.01	0.01
S804	10.06	11.59	0.3	0.14
S804	11.59	13.1	1.08	0.02
S804	13.1	14.63	2.4	0.02
S804	14.63	15.45	2.85	0.02
S804	15.45	16.4	2.51	0.01
S804	16.4	17.1	0.65	0.01
S804	17.1	18.15	0.34	0.01
S804	20.38	21.3	0.38	0.01
S804	21.3	21.6	1.41	0.01
S804	21.6	22.6	0.22	0.01
S805	6.1	7.62	0.13	0.04
S805	7.62	9.15	0.32	0.02
S805	9.15	10.67	0.3	0.01
S805	10.67	11.65	0.09	0.1
S805	11.65	12.2	0.01	0.12
S805	12.2	13.72	0.2	0.03
S805	13.72	15.25	0.29	0.02
S805	15.25	16.57	1.58	0.01
S805	16.57	17.45	0.93	0.01
S805	17.45	18.3	0.32	0.01
S805	18.3	19.82	0.36	0.02
S805	19.82	21.35	0.12	0.02
S805	21.35	22.87	0.05	0.01
S805	22.87	24.6	0.02	0.01
S805	24.6	26.22	0.01	0.01
S805	26.22	27.75	0.21	0.01
S805	27.75	29.27	0.34	0.02
S805	29.27	30.8	0.1	0.02
S805	30.8	32.32	0.13	0.01
S805	32.32	33.2	0.03	0.01
S805	33.2	34.2	0.01	0.02
S805	34.2	35.37	0.01	0.02
S805	35.37	37.3	0.04	0.02
S806	5.3	7.01	2.17	0.01
S806	7.01	8	4.23	0.36
S806	8	8.53	2.6	0.8
S806	8.53	10.06	1.41	0.17
S806	10.06	11.67	1.48	0.01
S806	11.67	12.87	2.63	0.15
S806	12.87	13.26	1.3	0.18
S806	13.26	15	0.21	0.02
S806	15	16.16	1.35	0.01
S806	16.16	18	0.75	0.01
S806	18	19.05	0.27	0.01
S807	18.3	19.04	2.17	0.03
S807	19.04	20.73	2.56	0.01
S807	20.73	22.56	2.91	0.01
S807	22.56	24.8	1.52	0.03
S807	24.8	25.2	3.83	0.01
S807	25.2	25.61	1.96	0.01
S807	25.61	26.83	1.6	0.03
S807	26.83	27.35	2.15	0.01
S807	27.35	28.35	0.98	0.01
S807	28.35	29.2	1.01	0.01
S807	29.2	30.2	1.32	0.01
S807	30.2	31.25	2.35	0.01
S807	31.25	31.85	2.13	0.01
S808	15.5	16.77	0.16	0.05
S808	16.77	18.25	0.56	0.02
S808	18.25	19.81	1.9	0.02
S808	19.81	21.49	2.13	0.42
S808	21.49	23	0.39	0.01
S808	23	24.5	0.08	0.01
S808	24.5	25.5	0.15	0.01
S808	25.5	26.7	0.18	0.01
S809	16.1	17.23	1.06	0.02
S809	17.23	17.68	2.39	0.02
S809	17.68	18.6	2.28	0.02
S809	18.6	19.2	0.56	0.06

S809	19.2	20.53	3.12	0.45
S809	20.53	21.55	1.53	0.02
S809	21.55	22.05	1.83	0.01
S809	22.05	22.95	2.85	0.01
S809	22.95	24.4	4.33	0.01
S809	24.4	25.92	0.23	0.02
S809	25.92	27.5	0.37	0.01
S809	27.5	28.15	2.95	0.01
S809	28.15	29.35	2.28	0.01
S809	29.35	30.55	1.12	0.01
S811	5.65	6.1	6.35	0.01
S811	6.1	7.35	4.16	0.01
S811	7.35	8.54	1.7	0.08
S811	8.54	9	1.07	0.04
S811	9	10.06	0.52	0.01
S811	10.06	11.59	1.89	0.01
S811	11.59	13.11	0.64	0.09
S811	13.11	14.63	1.17	0.05
S811	14.63	15.7	0.24	0.05
S812	6.1	7.85	1.76	0.02
S812	7.85	10.8	3.41	0.01
S812	10.8	11.2	3.62	0.01
S812	11.2	12.5	1.85	0.01
S812	12.5	14.63	0.96	0.01
S812	14.63	16	0.28	0.01
S812	16	17.5	0.08	0.01
S812	17.5	19	0.04	0.01
S812	19	20.4	0.05	0.01
S812	20.4	21.5	0.02	0.01
S813	6.4	6.8	4.31	0.01
S813	6.8	7.9	3.22	0.01
S813	7.9	9.6	2.5	0.02
S813	9.6	11.59	1.25	0.01
S813	11.59	13.1	0.92	0.01
S813	13.1	14.63	0.41	0.01
S813	14.63	16	0.16	0.01
S813	16	17.68	0.08	0.01
S813	17.68	18.5	0.14	0.01
S813	18.5	20.73	0.16	0.01
S813	20.73	21.4	0.01	0.01
S814	63.11	64.63	1.46	0.03
S814	64.63	66.6	0.1	0.01
S814	66.6	66.75	8.9	26.8
S814	66.75	67.9	6.1	8.9
S814	67.9	68.12	33.1	1.91
S814	68.12	69.16	8.2	0.25
S814	69.16	70.68	3.24	0.03
S814	70.68	71.31	2.63	0.15
S815	81.4	81.72	14.8	33.9
S815	81.72	82.41	4.8	2.95
S815	82.41	83.62	2.27	0.23
S815	83.62	84.45	3.64	0.01
S815	84.45	85.95	3.34	0.06
S815	85.95	87.5	1.46	0.01
S816	90.55	94.2	0.48	0.06
S816	94.2	94.56	10.7	2.9
S816	94.56	96.65	1.43	0.32
S816	96.65	97.75	0.94	0.01
S817	116	117.07	0.57	0.41
S817	117.07	118.4	0.5	0.06
S817	118.4	119.24	0.66	0.04
S817	119.24	120.12	0.82	0.22
S817	120.12	121.7	0.07	0.32
S817	121.7	123.17	0.61	0.12
S817	123.17	124.37	0.19	0.97
S818	102.2	102.82	0.04	0.03
S818	102.82	104.5	5.8	1.23
S818	104.5	106	4	1.02
S818	106	107.11	2.55	0.01
S818	107.11	108.45	1.35	0.01
S819	85.34	86.85	2.4	0.89
S819	86.85	87.1	0.78	0.19
S819	87.96	88.7	0.53	0.05
S820	102.72	103.63	1.35	0.1
S820	103.63	104.7	15	1.5
S820	104.7	105.65	3.68	0.6
S821	110.9	111.25	1.3	1.87
S821	111.25	112.17	7.14	0.55
S821	112.17	112.92	8.1	0.04
S821	112.92	113.6	5.27	0.02
S821	113.6	114	1.62	0.02

S821	114	115.05	2.8	0.02
S824	69.6	70.9	3.15	0.4
S825	90.43	91.15	10.4	0.15
S825	91.15	92.66	3.1	2
S825	92.66	93.74	4.73	2.22
S825	93.74	94.5	4.34	19.5
S826A	103.94	104.35	5.06	14.1
S826A	104.35	105.1	1.45	0.56
S826A	105.1	105.77	3.02	0.22
S827	110.95	111.45	14.4	23.4
S827	111.45	113.05	6.38	0.16
S827	113.05	113.9	3.53	0.38
S828	101.88	102.88	25.7	27.3
S828	102.88	103.95	21.9	0.54
S828	103.95	105.46	9.3	0.36
S828	105.46	106.05	5.1	0.49
S828	106.05	106.75	8.2	2.69
S829	112.06	113.09	23.2	3.54
S830	84.12	84.72	11.8	0.77
S830	84.72	86.88	2.3	0.22
S830	86.88	88.05	2.4	0.75
S830	88.05	90.22	3.6	2.37
S830	90.22	90.7	0.9	2.6
S831	121.77	123.45	16.6	7.75
S831	123.45	124.85	4.94	6.95
S831	124.85	126.02	2.45	5.04
S832A	130.5	130.95	0.13	0.52
S832A	130.95	131.66	11.5	6.65
S832A	131.66	132.7	4.73	1.17
S833	116.44	118.4	3.8	1.96
S834	113.5	114.15	0.55	0.57
S834	114.15	114.68	9.6	3.14
S834	114.68	116.65	2.9	2.74
S835	93.4	94.58	12	1.1
S835	94.58	97	2.1	1.98
S835	97	97.65	9.4	9.1
S835	97.65	98.95	9.1	1.94
S835	98.95	100.05	8.9	4.2
S836	100.8	100.97	24	3.92
S836	100.97	101.67	8.4	1.38
S836	101.67	103.5	0.55	0.42
S837	72.46	73	15.1	0.03
S837	73	74	4.93	0.13
S837	74	75.47	3.97	7.35
S837	75.47	76.67	3	2.59
S837	76.67	77.83	2.8	2.77
S837	77.83	79.55	2.13	2.34
S837	79.55	81.25	1.4	2.66
S837	81.25	81.6	1.85	17
S837	81.6	82.75	1.38	2.52
S837	82.75	84.12	2.4	4.96
S838A	54.9	56.2	0.6	0.16
S838A	60.58	62.79	1.08	0.5
S838A	62.79	64.7	1.9	0.52
S838A	66.95	67.6	0.35	0.16
S838A	67.6	68.49	5.89	8.3
S838A	68.49	69.65	9.1	2.98
S838A	69.65	71.25	4.5	1.25
S839	82.4	82.87	14.4	42.2
S839	82.87	83.5	5.39	1.88
S839	83.5	84.12	2.75	0.22
S839	84.12	85.7	2.6	0.65
S840	104.04	105.89	0.01	0.19
S840	105.89	106.24	3.35	15.4
S840	106.24	107.23	3.15	5.63
S840	107.23	107.94	1.6	1.58
S841	100	101.2	0.03	3.48
S841	101.2	102.25	0.06	2.66
S842	90.73	92.12	3.05	0.68
S843	79.93	80.52	14.3	16.3
S843	80.52	81.6	3.4	2.58
S843	81.6	82.25	3.9	3.27
S843	82.25	83.85	3.4	1.76
S844	68.7	71	0.6	0.07
S844	71	71.93	3.84	0.01
S844	71.93	72.8	9	0.01
S844	72.8	73.7	4.12	0.04
S844	73.7	74.98	3.72	0.11
S844	74.98	76.4	1.05	0.06
S844	76.4	77.9	0.1	0.24
S845	62.79	63.55	9.6	0.01

S845	63.55	64.25	0.27	0.01
S845	64.25	70.45	0	0
S845	70.45	71.45	3.4	0.56
S845	71.45	71.93	0	0
S845	71.93	72.1	0.11	0.98
S846	69.2	70.55	6.61	0.02
S846	70.55	72	4.2	0.01
S846	72	73.5	5.98	0.22
S846	73.5	74.98	2.8	0.3
S846	74.98	76.4	3.8	1.02
S846	76.4	78.03	4.25	1.34
S846	78.03	79.25	4.05	0.02
S846	79.25	80.45	2.8	0.03
S847	104.2	105.46	1.81	1.34
S847	105.46	106	0.29	0.47
S848	86.6	88.85	0.03	0.02
S848	88.85	90.35	2.2	0.57
S848	90.35	90.7	1.15	0.86
S849	73.4	74.1	1.08	0.13
S849	74.1	76.8	1.5	0.31
S849	76.8	78.03	0.52	0.05
S850A	121.3	122.12	3.8	4.52
S850A	122.12	122.65	0.35	0.44
S850A	122.65	123.4	0.03	0.05
S851	58.34	58.84	0.2	0.01
S851	58.84	59.74	6.37	0.01
S851	59.74	60.59	2.5	0.01
S852	71.93	72.73	0.34	0.08
S852	72.73	73.23	0.2	0.04
S852	73.23	75.53	0.07	0.06
S852	75.53	76.98	0.02	0.04
S852	76.98	78.42	0.16	0.13
S852	78.42	79.9	0.17	0.38
S852	79.9	81.32	0.57	1.2
S852	81.32	82.79	0.54	2.58
S852	82.79	84.12	0.06	0.47
S852	84.12	85.63	0.18	0.11
S852	85.63	86.07	0.01	0.02
S852	86.07	86.43	0.01	0.01
S853	30.69	32.07	0.25	0.04
S853	32.07	33.81	0.49	0.01
S853	33.81	34.87	0.64	0.01
S853	34.87	36.6	1.35	0.01
S853	36.6	37.75	0.51	0.01
S853	37.75	39.16	0.6	0.01
S853	39.16	40.62	0.36	0.01
S853	40.62	42.04	1.1	0.01
S853	42.04	43.68	0.08	0.01
S853	43.68	45.1	0.36	0.01
S853	45.1	46.5	0.5	0.01
S853	46.5	47.9	1.09	0.01
S853	47.9	49.27	0.5	0.01
S853	49.27	50.71	1.35	0.01
S853	50.71	52.2	0.55	0.01
S853	52.2	53.64	0.48	0.01
S853	53.64	55.08	1.4	0.01
S853	55.08	56.6	2.2	0.01
S853	56.6	57.99	2.3	0.01
S853	57.99	59.47	0.75	0.01
S853	59.47	60.92	0.6	0.04
S853	60.92	62.39	0.42	0.02
S853	62.39	63.78	0.5	0.06
S853	63.78	65.2	0.42	0.2
S853	65.2	66.64	0.04	0.07
S853	66.64	68.21	0.01	0.07
S854A	86.15	86.75	0.01	0.1
S854A	86.75	89.2	0.46	0.02
S854A	89.2	90.43	0.02	0.03
S855	104.2	105.46	0.07	0.01
S855	105.46	106.98	0.2	0.08
S855	106.98	108.51	0.04	0.13
S855	108.51	110.03	0.01	0.25
S855	110.03	111.56	0.1	0.12
S856	98	98.45	0.01	0.02
S856	98.45	100.15	0.09	0.16
S857	65.2	65.84	0.08	2.39
S857	65.84	66.84	0.05	16.9
S857	66.84	67	0.05	11.2
S857	67	67.96	0.11	6.06
S857	67.96	69.38	4.2	12.7
S857	69.38	70.13	2.01	48.2

S857	70.13	71.6	2.4	14.7
S857	71.6	72.33	0.3	2.13
S857	72.33	74.8	2.32	0.4
S857	74.8	76.01	5.28	17.3
S857	76.01	77.23	1.32	0.21
S857	77.23	78.67	1	0.04
S857	78.67	80.16	3.24	0.49
S857	80.16	81.07	1.6	0.05
S858	62.51	62.79	0.04	5.33
S858	62.79	63.41	0.09	10.4
S858	63.41	65.36	2.2	8.4
S858	65.36	65.83	3.1	1.24
S858	65.83	66.4	0.09	0.56
S858	66.4	66.76	0.12	2.01
S858	66.76	68.3	3.1	0.7
S858	68.3	68.88	10.5	0.05
S858	68.88	69.78	2.98	0.03
S858	69.78	71.16	0.11	0.01
S858	71.16	72.58	0.16	0.01
S858	72.58	73.28	0.04	0.01
S859	81.07	81.85	0.21	0.06
S859	81.85	82.11	13.7	6.94
S859	82.11	84.12	2.24	1.88
S859	84.12	84.65	1.68	1.29
S860	74.7	76.51	0.24	0.77
S860	76.51	78.03	0.01	0.21
S860	78.03	81.85	0	0
S860	81.85	82.6	0.13	0.05
S860	82.6	83.4	0.56	0.75
S860	83.4	83.77	3.2	1.09
S860	83.77	84.59	1.04	0.04
S860	84.59	85	3.6	0.37
S860	85	86	1.4	0.53
S860	86	86.83	2.5	4.23
S860	86.83	88.64	0.25	1.34
S861	109.65	110.65	8	10.5
S861	110.65	111.29	5.2	6.32
S862	46.25	46.75	0.11	0.09
S862	46.75	47.3	0.03	0.04
S862	47.3	48	0.08	0.06
S862	48	48.6	0.06	0.05
S862	48.6	48.8	0.02	0.01
S862	48.8	50	0.01	0.01
S862	50	50.6	0.01	0.01
S862	50.6	52	0.01	0.01
S863	76	77.5	0.06	0.02
S863	77.5	77.75	0.02	0.02
S863	77.75	78	0.01	0.01
S863	78	79	0.01	0.01
S863	88.7	89.3	0.01	0.01
S863	89.3	90.3	0.01	0.01
S863	90.3	90.8	0.01	0.01
S863	102.4	103	0.01	0.01
S864	250	250.5	0.01	0.01
S864	250.5	251.3	0.01	0.01
S864	251.3	251.9	0.01	0.01
S864	271.6	272.2	0.03	0.01
S864	272.2	272.6	0.12	0.07
S864	272.6	273	0.14	0.1
S864	273	273.6	0.02	0.01
S864	275.4	276	0.02	0.01
S864	278.6	279.2	0.01	0.01
S864	279.2	280	0.01	0.01
S867	38.1	38.7	0.5	0.63
S867	38.7	40.45	0.66	0.3
S867	40.45	41.27	0.28	2.73
S867	41.27	42.8	0.98	0.78
S867	42.8	43.9	2.2	0.03
S867	43.9	44.5	1.2	0.02
S867	44.5	46.02	1.24	0.01
S867	46.02	47.55	1.04	0.01
S867	47.55	48.85	0.96	0.01
S867	48.85	50.37	1.56	0.16
S867	50.6	51.65	0.8	4.04
S867	51.65	52.03	3.28	20.5
S868	34.7	35.36	0.96	0.26
S868	35.36	36	1.2	0.08
S868	36	37	0.6	1.24
S868	37	38.2	0.85	0.39
S868	38.2	39.93	2	0.04
S868	39.93	41.45	2.5	0.01

S868	41.45	41.85	1.67	0.02
S868	41.85	42.7	0.8	0.04
S868	47.07	47.73	2.95	0.02
S868	47.73	48.7	2.4	0.48
S868	48.7	49.2	0.61	0.28
S868	50.38	50.9	1.4	9.2
S868	51.5	52.45	0.82	1.82
S869	29.57	32.05	0.24	0.04
S869	32.05	33.82	2.2	0.16
S869	33.82	34.6	0.88	1.27
S869	34.6	35.6	0.12	3.72
S869	35.6	36.6	0.18	1.2
S869	36.6	37	0.06	1.34
S869	37	38.6	1.24	0.03
S869	38.6	39.92	2.25	0.3
S869	39.92	41.45	0.44	0.26
S869	41.45	42.97	0.12	0.01
S869	42.97	44.13	1.15	0.01
S869	44.13	45.4	4.53	0.01
S869	45.4	46.9	4.67	0.01
S869	46.9	48.6	2.82	0.01
S869	49.3	49.67	0.81	0.2
S869	50.8	51.4	0.18	0.01
S870	33.2	34.7	0.52	0.01
S870	34.7	35.7	1.04	0.01
S870	35.7	36.4	0.87	0.01
S870	36.4	38.17	1.97	0.12
S870	38.17	38.97	0.32	4.3
S870	38.97	40.4	1.16	1.4
S870	40.4	42.2	1.15	1.03
S870	42.2	44.5	0.95	0.09
S870	44.5	45.3	0.65	0.52
S870	45.3	47.2	2.4	5.5
S870	47.2	49.6	2.4	0.48
S870	49.6	51.58	2.05	1.86
S870	51.58	53.65	2.1	1.52
S870	53.65	55.25	3.08	0.78
S870	55.25	57.6	0.36	1.04
S871	41.65	42.7	0.84	0.03
S871	42.7	44.5	0.48	0.02
S871	44.5	46.05	0.92	0.02
S871	46.05	47	1.4	0.49
S871	47	47.55	2.7	0.02
S871	47.55	48.06	8.2	0.67
S871	48.06	49.58	6.39	0.05
S871	49.58	51.5	1.95	0.08
S871	51.5	52.85	2.45	0.03
S871	52.85	53.65	7.89	3.4
S871	53.65	55.1	1.48	0.03
S871	55.1	56.97	1.72	0.01
S871	56.97	57.67	2.84	2.07
S871	57.67	58.57	3.77	5.96
S871	58.57	59.2	4.12	0.16
S871	59.2	60.65	1.24	0.05
S872	40.2	41.45	1.24	0.02
S872	41.45	43	1.06	0.15
S872	43	44.5	0.66	0.01
S872	44.5	45.15	2.03	0.01
S872	50.6	51.1	0.81	0.03
S872	51.1	52.07	1.44	0.01
S872	52.07	53.65	4.03	0.12
S872	53.65	55.1	1.78	1.06
S872	55.1	56.7	0.19	0.41
S872	56.7	57.66	0.18	0.58
S872	57.66	58.63	0.04	0.03
S872	58.63	58.72	0.01	0.01
S872	60.03	61.06	0.01	0.01
S873	54.97	55.52	1.32	0.01
S873	55.52	56.7	4.17	0.01
S873	56.7	57.5	4.58	0.04
S873	61.13	62.07	0.16	0.01
S873	62.07	62.8	1.33	0.01
S873	62.8	64.61	7.49	0.69
S873	64.61	65.85	6.6	5.88
S873	65.85	66.45	2.26	1.96
S873	66.45	67.3	0.35	0.04
S874	41.45	42.45	0.88	0.01
S874	44	45.44	4.16	0.01
S874	45.44	46.5	3.52	0.01
S874	46.5	47.97	1.84	0.01
S874	47.97	49.45	0.4	0.01

S874	49.45	50.6	1.12	0.01
S874	50.6	51.47	0.9	0.01
S874	51.47	52.07	1.9	0.03
S874	52.07	53.64	7.04	0.08
S874	53.64	54.88	1.85	0.77
S874	54.88	56.05	1.4	10.85
S874	56.05	57.04	1.75	0.66
S874	57.04	58.14	8.1	0.16
S874	58.14	59.59	1.95	0.03
S874	59.59	61.85	1.6	0.02
S874	61.85	62.64	0.52	0.87
S874	62.64	63.63	0.44	0.02
S874	63.63	65.13	0.04	0.01
S875	35.75	37.4	4.02	0.02
S875	37.4	38.96	1.7	0.01
S875	45.83	47.56	0.68	0.89
S875	47.56	49.06	0.3	0.72
S875	49.06	50.61	0.62	0.94
S875	50.61	51.78	0.34	0.83
S875	51.78	53.2	0.62	4.24
S875	53.2	53.66	4.53	0.63
S875	53.66	55.16	0.46	0.31
S875	55.16	56.71	0.06	0.63
S875	56.71	58.22	0.74	1.07
S875	58.22	59.76	0.7	0.74
S875	59.76	61	0.44	0.7
S876	40.09	41.57	0.6	0.02
S876	41.57	42.88	2.9	0.01
S876	42.88	44.23	2.15	0.01
S876	44.23	46.2	2.1	0.01
S876	46.2	48.3	3.2	0.01
S876	48.3	51.37	3.42	0.01
S876	51.37	51.95	3.19	0.01
S876	51.95	52.85	1.2	0.04
S876	52.85	54.52	1.16	0.01
S876	54.52	57.7	1.36	0.02
S876	57.7	59	3.61	0.01
S876	59	60.01	1.64	0.01
S876	60.01	60.85	1.92	0.01
S876	60.85	62.64	1.85	0.52
S876	62.64	63.32	3.9	0.06
S876	63.32	65.3	1.36	0.56
S876	65.3	67.2	0.42	0.8
S876	67.2	69.02	0.12	0.01
S877	61.8	63.6	0.9	34.9
S877	63.6	64.67	6.24	1.29
S877	64.67	65.23	8.4	6.64
S877	65.23	66.35	4.12	0.1
S877	66.35	67.3	9.52	0.06
S877	67.3	68.4	1.02	0.01
S877	68.4	69.01	3	0.01
S877	69.01	71.83	0.68	0.12
S877	71.83	74.46	0.6	0.02
S877	74.46	75.51	0.08	0.23
S877	75.51	77.25	0.87	0.48
S878	35.36	36.05	1.24	0.01
S878	36.05	37.6	1.44	0.01
S878	37.6	39.93	2.3	0.01
S878	39.93	41.7	0.84	0.01
S878	41.7	42.6	0.9	0.06
S878	42.6	42.86	1.68	1.74
S878	42.86	43.55	1.08	0.03
S878	47.55	48.3	1.36	0.02
S878	48.3	49.55	10.7	0.01
S878	49.55	50.92	4.42	0.01
S878	50.92	51.75	2.3	0.01
S878	51.75	53.65	0.26	0.01
S878	53.65	55.17	0.96	0.04
S878	55.17	56.9	0.08	0.05
S878	56.9	57.45	2.3	0.18
S878	57.45	58.23	1.05	0.01
S878	58.23	59.75	1.4	0.12
S878	59.75	61.27	1.48	0.14
S878	61.27	62.79	0.84	0.09
S878	62.79	64.32	1.24	0.12
S879	28.9	29.6	0.66	0.01
S879	29.6	31.2	1.32	0.01
S879	31.2	32.38	0.93	0.01
S879	32.38	33.5	1.54	0.01
S879	33.5	35.35	0.48	0.01
S879	50.6	52.12	0.11	0.02

S879	52.12	54.2	0.08	0.01
S880	33.85	35.7	0.19	0.01
S880	35.7	37.15	2.15	0.01
S880	37.15	38.4	4.92	0.01
S880	38.4	39.52	3.4	0.01
S880	39.52	40.7	3.25	0.01
S880	40.7	41.45	0.84	0.01
S880	41.45	42.97	0.38	0.02
S880	42.97	44.5	1.2	0.02
S880	44.5	46.03	1.35	0.01
S880	46.03	47.55	0.96	0.01
S880	47.55	49.07	2.15	0.01
S880	49.07	49.9	2.1	0.12
S880	49.9	50.85	1.56	0.68
S880	50.85	51.4	5.54	0.99
S880	51.4	51.91	2.76	20.8
S880	51.91	52.65	1.45	9.4
S880	52.65	53.65	1.48	4.5
S880	53.65	54.3	0.6	2.85
S880	54.3	55.9	0.69	0.55
S880	55.9	57.15	0.28	4.44
S880	57.15	58.22	0.05	0.1
S880	58.22	59.74	0.01	0.01
S881	44.5	45.55	0.42	0.06
S881	45.55	47.55	0.85	0.02
S881	47.55	49.07	0.65	0.01
S881	49.07	50.75	0.24	0.01
S881	50.75	52.5	4.95	0.01
S881	52.5	52.83	8.51	0.01
S881	52.83	55.17	1.1	0.04
S881	55.17	56.7	2.2	2.33
S881	56.7	57.55	0.9	0.45
S881	57.55	58.23	1.95	8.46
S881	58.23	59.65	1.4	0.31
S881	59.65	61.27	0.05	0.01
S881	61.27	62.8	1.4	0.31
S882	36.1	36.75	1.8	0.01
S882	36.75	38.95	2.8	0.01
S882	38.95	41.45	1.88	0.01
S882	41.45	43	1.8	0.01
S882	43	44.5	3.96	0.07
S882	44.5	46.03	3.2	0.01
S882	46.03	47.55	4.08	0.01
S882	47.55	49.08	2.68	0.02
S882	49.08	50.25	2.52	1.76
S882	50.25	50.8	2.39	1.62
S882	50.8	52.1	3.51	1.45
S882	52.1	53.8	1.4	0.83
S882	53.8	54.45	0.6	4.72
S882	54.45	55.17	0.78	10.2
S882	55.17	56.15	2.57	1.92
S882	56.15	58.2	0.76	0.28
S882	58.2	59.1	4.26	0.23
S882	59.1	60.1	2.93	0.02
S882	60.1	61.45	0.16	0.01
S882	61.45	62.8	0.01	0.01
S883	62.65	63.3	0.02	4.08
S883	64.57	65.45	1.24	39.6
S883	65.45	66.75	5.2	33.4
S883	66.75	68.9	9.57	2.47
S883	68.9	70.43	11.6	1.61
S883	70.43	71.95	7.96	5.33
S883	71.95	73.2	16.1	2.54
S883	73.2	74.4	4.13	0.31
S883	74.4	76.2	0.52	0.21
S883	76.2	78.15	3.23	0.56
S883	78.15	79.7	0.07	0.03
S884	84.13	85.6	0.05	0.05
S884	85.6	86.75	0.2	0.32
S884	86.75	87.4	3.15	1.52
S884	87.4	88.1	3.61	1.34
S884	88.1	89.5	0.04	0.07
S885	39	39.65	1.02	0.01
S885	39.65	40.05	2.44	0.01
S885	40.05	40.6	0.73	0.01
S885	53.65	54.2	0.15	0.01
S885	54.2	55.18	1.07	0.01
S885	55.18	56.7	0.93	0.01
S885	56.7	58.75	1.26	0.01
S885	58.75	60.4	2.66	0.01
S885	60.4	61.6	0.08	0.01

S885	61.6	62.8	0.23	0.03
S885	62.8	64.5	0.11	0.29
S885	64.5	65.85	0.1	1.45
S885	65.85	67.35	0.01	1.15
S885	67.35	68.88	0.21	1.14
S885	68.88	70.4	0.05	0.68
S885	70.4	72.1	0.21	0.3
S885	72.1	73.45	0.29	0.89
S885	73.45	74.65	0.1	0.14
S886	42.7	43.2	0.25	0.01
S886	43.2	43.6	0.81	0.01
S886	43.6	44	0.37	0.01
S886	52.55	53.15	0.16	0.01
S886	53.15	53.55	3.17	0.01
S886	53.55	54.2	0.2	0.01
S886	54.2	54.75	1.09	0.01
S886	54.75	56	0.72	0.01
S886	56	56.7	0.23	0.02
S886	60.5	62.8	0.65	0.04
S886	68.9	70.42	0.07	0.4
S886	70.42	71.95	0.06	0.52
S886	71.95	72.7	0.04	0.3
S887	32.3	32.75	0.6	0.02
S887	32.75	34.4	2.3	0.01
S887	34.4	35.35	0.56	0.02
S887	45.2	47.95	1.1	0.08
S887	47.95	48.5	1.3	0.01
S887	48.5	49.1	0.18	0.01
S887	49.1	50.6	0.64	0.01
S887	50.6	52.13	0.6	0.01
S887	52.13	54.05	0.26	0.01
S901	3.2	4.4	1.68	1.1
S901	4.4	5.6	1.12	0.79
S901	5.6	6.8	0.48	0.22
S901	6.8	8	1.3	1.14
S901	8	9.3	1.48	1.04
S901	9.3	10.6	0.65	0.37
S901	10.6	12	0.47	0.12
S901	12	13.15	0.46	0.01
S902	3	4.5	1.47	0.69
S902	4.5	6	1.66	0.82
S902	6	7.25	2.21	0.62
S902	7.25	8.65	4.08	1.39
S902	8.65	10	2.7	0.63
S902	10	11.35	0.53	0.31
S902	11.35	12.7	0.12	0.05
S902	12.7	14	0.21	0.04
S902	16.5	18	0.52	0.01
S902	18	19.6	0.66	0.01
S902	19.6	20.5	0.4	0.01
S903	2.5	4.05	0.96	0.14
S903	4.05	5.65	1.47	0.04
S903	5.65	6.6	2.53	1.82
S903	6.6	7.6	1.86	1.72
S903	7.6	9	0.94	0.26
S903	9	10.4	0.15	0.05
S903	10.4	11.8	0.56	0.16
S903	11.8	13.2	0.77	0.01
S903	13.2	14.45	0.48	0.28
S904	2.75	3.75	1.45	0.05
S904	3.75	4.75	0.88	0.01
S904	4.75	5.85	1	0.01
S904	5.85	7.3	1.9	0.01
S904	7.3	8.7	0.41	0.13
S904	8.7	10	0.04	0.09
S904	10	11.3	0.09	0.02
S904	11.3	12.5	0.39	0
S905	3.45	4.75	1.88	0.01
S905	4.75	6.05	0.6	0.07
S905	6.05	7.35	3	0.13
S905	7.35	8.65	1.56	0.03
S905	8.65	9.7	0.19	0.02
S905	9.7	10.75	0.19	0.02
S905	10.75	11.8	0.97	0.27
S906	2.3	3	2.34	0.01
S906	3.7	4.7	1.96	0.02
S906	4.7	5.6	1.52	0.03
S906	5.6	6.9	1.76	0.58
S906	6.9	8.2	2.02	0.04
S906	8.2	9.4	5.38	0.16
S906	9.4	10.6	1.12	0.01

S906	10.6	11.8	0.41	0.01
S906	11.8	13.1	0.47	0.01
S907	2.8	4.2	3.45	0.04
S907	4.2	5.6	2.74	0.02
S907	5.6	7	1.35	0.02
S907	7	8.4	0.41	0.01
S907	8.4	9.85	0.42	0.02
S907	9.85	11.3	0.7	0.02
S907	11.3	12.6	0.31	0.01
S907	12.6	13.9	0.48	0.01
S908	4.15	5.6	0	0
S908	5.6	7	0.24	0.04
S908	7	8.4	0.99	0.01
S908	8.4	9.8	1.04	0.01
S908	9.8	10.9	1.42	0.01
S908	10.9	12	1.22	0.01
S908	12	13.3	0.18	0.05
S908	13.3	14.6	0.24	0.01
S908	14.6	15.9	0.15	0.01
S908	15.9	17.2	0.13	0.01
S908	17.2	18.5	0.02	0.01
S908	18.5	19.8	0.03	0.01
S908	19.8	21.2	0.17	0.01
S908	21.2	22.7	0.15	0.01
S908	22.7	24.2	0.01	0.01
S909	2.75	3.9	0.93	0.15
S909	3.9	5	1.57	0.05
S909	5	6.1	2.75	0.04
S909	6.1	7	2.68	0.14
S909	7	8.2	3.8	0.71
S909	8.2	9.4	4.12	0.55
S909	9.4	10.55	1.58	0.21
S909	10.55	11.9	0.31	0.16
S909	11.9	13.4	0.15	0.16
S909	13.4	14.9	0.5	0.51
S909	14.9	15.8	3	3.06
S909	15.8	16.6	1.98	2.75
S909	16.6	18	3.25	0.06
S909	18	19.3	4.69	0.17
S909	19.3	20.5	2.38	0.02
S909	20.5	21.7	0.24	0.01
S909	21.7	22.85	0.29	0.01
S910	3.7	4.95	2.98	1.01
S910	4.95	6.2	1.15	0.31
S910	6.2	7.45	0.3	0.2
S910	7.45	8.7	0.48	0.14
S910	8.7	9.9	0.2	0.11
S910	9.9	11.2	0.16	0.06
S910	11.2	12.5	0.67	0.1
S910	12.5	13.8	0.02	0.03
S910	13.8	15.1	0.05	0.06
S910	15.1	16.4	0.08	0.07
S910	16.4	17.7	0.7	0.08
S910	17.7	19	1.8	1.41
S910	19	20.45	0.92	0.15
S910	20.45	21.9	0.53	0.15
S910	21.9	23.35	0.07	0.06
S910	23.35	24.8	0.01	0.04
S910	24.8	26.2	0.01	0.04
S910	26.2	27.2	0.02	0.13
S911	3.8	5.15	3.55	0.62
S911	5.15	6.4	5.13	2.67
S911	6.4	7.65	0.98	0.29
S911	7.65	8.9	0.71	0.16
S911	8.9	10.15	1.8	0.12
S911	10.15	11.4	1.86	2.25
S911	11.4	12.65	1.31	0.45
S911	12.65	13.9	0.73	1.68
S911	13.9	15.3	1.02	0.27
S911	15.3	16.1	1.92	7.48
S911	16.1	16.9	3.73	11.36
S911	16.9	18.15	1.07	0.19
S911	18.15	19.4	2	0.27
S911	19.4	20.65	4.74	1.83
S911	20.65	21.9	3.51	0.37
S911	21.9	23.15	3.48	2.05
S911	23.15	24.45	1.15	0.02
S911	24.45	25.7	2.01	0.02
S911	25.7	27	3.44	0.01
S911	27	28.3	3.6	0.02
S911	28.3	29.6	2.47	0.05

S911	29.6	30.8	3.37	0.03
S911	30.8	32.1	0.03	0.06
S911	32.1	33.4	0.06	0.01
S911	33.4	34.8	0	0.01
S912	3.5	4.9	2.37	0.26
S912	4.9	6.3	3.52	0.21
S912	6.3	7.5	1.29	0.11
S912	7.5	8.7	2.78	0.29
S912	8.7	9.9	3.16	1.77
S912	9.9	11	0.64	0.45
S912	11	12.25	0.15	0.05
S912	12.25	13.5	0.18	0.03
S912	13.5	14.75	0.11	0.08
S912	14.75	16	0.18	0.06
S912	16	17.25	0.48	0.19
S912	17.25	18.5	0.56	0.18
S912	18.5	19.8	0.53	0.14
S913	3.8	5	1.01	0.16
S913	5	6.3	1.86	0.96
S913	6.3	7.6	2.16	0.34
S913	7.6	8.75	2.44	1.84
S913	8.75	9.9	1	1.16
S913	9.9	11.1	0.85	0.44
S913	11.1	12.3	0.94	0.74
S913	12.3	13.4	0.85	1.31
S913	13.4	14.45	5.13	4.4
S914	6.2	7.7	2.72	0.03
S914	7.7	9.2	1.23	0.02
S914	9.2	10.75	1.67	0.01
S914	10.75	11.9	1	0.01
S914	11.9	13.2	0.79	0.01
S914	13.2	14.3	1.22	0.02
S914	14.3	15.4	0.41	0.01
S914	15.4	16.5	0.1	0.02
S914	16.5	17.65	0.02	0.02
S914	17.65	19.1	0.06	0.01
S914	19.1	20.55	0.16	0.01
S914	20.55	21.7	0.09	0.01
S914	21.7	22.9	0.21	0.01
S914	22.9	24.1	0.12	0.01
S914	24.1	25.3	0.01	0.04
S915	5.9	7.1	1.27	0.03
S915	7.1	8.3	2.1	0.01
S915	8.3	9.5	1.44	0.01
S915	9.5	10.7	1.37	0.01
S915	10.7	11.9	0.94	0.05
S915	11.9	13.1	1.04	0.01
S915	13.1	14.3	0.3	0.02
S915	14.3	16.7	0.1	0.01
S915	16.7	17.9	0.7	0.01
S915	17.9	19	0.27	0.01
S915	19	19.9	0.16	0.01
S915	19.9	20.8	0.01	0.01
S916	5.4	6.4	0.21	0.02
S916	6.4	7.4	0.31	0.01
S916	7.4	8.5	0.8	0.05
S916	8.5	9.6	1.68	0.04
S916	9.6	10.7	2.8	0.02
S916	10.7	11.9	2.17	0.01
S916	11.9	13.1	1.13	0
S916	13.1	14.3	1.48	0.01
S916	14.3	15.5	1.38	0.01
S916	15.5	16.8	0.38	0.01
S916	16.8	18.1	0.03	0.01
S916	18.1	19.4	0.03	0.01
S916	19.4	20.7	0.15	0.01
S916	20.7	22	0.2	0.01
S916	22	23.2	0.05	0.01
S916	23.2	24.4	0.08	0.01
S916	24.4	25.6	0.02	0.04
S916	25.6	26.7	0.01	0.01
S917	6.2	7.7	0.03	0.05
S917	7.7	8.8	0.01	0.08
S917	8.8	9.9	0.07	0.02
S917	9.9	10.95	0.17	0.01
S917	10.95	12.2	0.32	0.03
S917	12.2	13.5	0.03	0.05
S917	13.5	14.8	0.12	0.05
S917	14.8	16.1	0.32	0.01
S917	16.1	17.3	0.69	0.01
S917	17.3	18.5	0.93	0.01

S917	18.5	19.8	0.36	0.01
S917	19.8	21.1	0.05	0.01
S917	21.1	22.4	0.12	0.01
S917	22.4	23.7	0.11	0.01
S917	23.7	25	0.23	0.01
S917	25	26.3	0.2	0
S917	26.3	27.6	0.06	0.01
S917	27.6	28.7	0.3	0.01
S917	28.7	29.7	0.24	0.01
S917	29.7	30.9	0.13	0
S917	30.9	32.1	0.05	0.01
S917	32.1	33.3	0.15	0.01
S917	33.3	34.5	0.18	0.01
S917	34.5	35.7	0.16	0.01
S917	35.7	36.9	0.11	0.01
S917	36.9	38.1	0.05	0
S917	38.1	39.2	1.13	0.01
S917	39.2	40.2	0.64	0.02
S917	40.2	41.3	0.16	0.01
S917	41.3	42.2	0.02	0.01
S917	42.2	43.1	0.01	0.01
S917	43.1	44.6	0.01	0.01
S917	44.6	46	0.01	0.01
S918	7.5	8.8	0.03	0.06
S918	8.8	10.1	0.49	0.02
S918	10.1	11.35	0.17	0
S918	11.35	12.55	0.09	0.02
S918	12.55	13.75	0.01	0.3
S918	13.75	14.9	0.01	0.08
S918	14.9	16.3	0.14	0.02
S918	16.3	17.7	0.9	0.01
S918	17.7	19	0.53	0.01
S918	19	20.35	0.18	0.01
S918	20.35	21.6	0.04	0.02
S918	21.6	22.9	0.13	0.01
S918	22.9	24.2	0.06	0.01
S918	24.2	25.5	0.16	0.01
S918	25.5	26.75	0.01	0.01
S918	26.75	28	0.05	0.01
S918	28	29.25	0.15	0.01
S918	29.25	30.5	0.11	0.01
S918	30.5	31.7	0.15	0.01
S918	31.7	32.9	0.12	0.01
S918	32.9	34.1	0.1	0.01
S918	34.1	35.3	0.14	0.01
S918	35.3	36.5	0.02	0.01
S918	36.5	37.6	0.01	0.02
S918	37.6	38.7	0.01	0.01
S918	38.7	39.85	0.01	0.01
S919	8.7	10.1	0.03	0.05
S919	10.1	11.5	0.08	0.02
S919	11.5	12.95	0.11	0.02
S919	12.95	14.3	0.01	0.02
S919	14.3	15.65	0.02	0.09
S919	15.65	17	0.01	0.04
S919	17	18.35	0.41	0.04
S919	18.35	19.7	0.76	0.01
S919	19.7	21.1	1.15	0.01
S919	21.1	22.25	0.28	0.01
S919	22.25	23.45	0.05	0.01
S919	23.45	24.7	0.02	0.01
S919	24.7	25.95	0.03	0.01
S919	25.95	27.2	0.01	0.01
S919	27.2	28.4	0.18	0.01
S919	28.4	29.7	0.11	0.01
S919	29.7	31	0.04	0.01
S919	31	32.3	0.06	0.01
S919	32.3	33.6	0.03	0.01
S919	33.6	34.9	0.11	0.01
S919	34.9	36.2	0.02	0.01
S919	36.2	37.5	0.1	0.01
S919	37.5	38.9	0.01	0.01
S919	38.9	40.45	0.01	0.01
S919	40.45	41.6	0	0.01
S919	41.6	42.8	0	0.01
S919	42.8	44	0	0.01
S919	44	45.1	0	0.01
S920	9	10.1	0.02	0.02
S920	10.1	11.25	0.29	0.02
S920	11.25	12.6	2.47	0.01
S920	12.6	14.1	1.24	0.01
S920	14.1	15.6	1.53	0.01
S920	15.6	17.1	0.71	0.01
S920	17.1	18.6	0.5	0.01
S920	18.6	20.1	0.57	0.01
S920	20.1	21.6	0.22	0.01
S920	21.6	23.1	0.04	0.01
S920	23.1	24.6	0.01	0.01
S920	24.6	26.1	0.04	0.01
S920	26.1	27.5	0.06	0.01
S920	27.5	28.8	0.8	0.01
S920	28.8	30	0.64	0.01
S920	30	31.2	0.33	0.01
S920	31.2	32.4	0.24	0.02
S920	32.4	33.6	0.19	0.01
S920	33.6	34.9	0.12	0.01
S920	34.9	36.2	0.19	0.02
S920	36.2	37.5	0.35	0.01
S920	37.5	38.8	0.5	0
S920	38.8	40.1	0.01	0.02
S920	40.1	41.4	0.01	0.01
S921	12	13.6	0.14	0.01
S921	13.6	15.1	0.4	0.01
S921	15.1	16.2	0.45	0.01
S921	16.2	17.25	0.49	0.01
S921	17.25	18.6	0.42	0.01
S921	18.6	19.95	0.07	0.01
S921	19.95	21.3	0.03	0.01
S921	21.3	22.65	0.04	0.01
S921	22.65	24	0.02	0.01
S921	24	25.4	0.01	0.01
S921	25.4	26.8	0.08	0.01
S921	26.8	28.2	0.09	0
S921	28.2	29.6	0.21	0.01
S921	29.6	31	0.12	0.01
S921	31	32.3	0.07	0.01
S921	32.3	33.65	0.06	0.01
S921	33.65	35	0	0.01
S921	35	36.35	0	0.01
S922	12.9	14.4	1.13	0.01
S922	14.4	15.8	3.49	0.01
S922	15.8	17.15	4.91	0.01
S922	17.15	18.6	4.11	0.01
S922	18.6	19.9	1.3	0.01
S922	19.9	21.2	0.68	0.01
S922	21.2	22.5	0.34	0.01
S922	22.5	23.7	0.38	0.01
S922	23.7	24.9	1.16	0.01
S922	24.9	26.2	3.39	0.02
S922	26.2	27.5	1.8	0.01
S922	27.5	28.8	1.02	0.01
S922	28.8	30.2	0.6	0.01
S922	30.2	31.5	0.58	0.01
S922	31.5	32.9	0.46	0.01
S922	32.9	34.3	1.5	0.01
S922	34.3	35.7	0.79	0.01
S922	35.7	37.1	0.72	0.01
S922	37.1	38.5	1.01	0.01
S922	38.5	39.9	0.66	0.01
S922	39.9	41.3	0.17	0.01
S922	41.3	42.6	0.18	0.01
S922	42.6	43.9	0.59	0.03
S922	43.9	45.3	0.19	0.01
S922	45.3	46.4	0.04	0.01
S922	46.4	47.45	0.01	0.01
S923	10.85	12.3	1.81	0.01
S923	12.3	13.7	2.3	0
S923	13.7	15.1	2.73	0.01
S923	15.1	16.2	0.86	0.01
S923	16.2	17.2	2.34	0.01
S923	17.2	18.2	1.43	0.01
S923	18.2	19.7	0.12	0.01
S923	19.7	21.2	0.26	0.01
S923	21.2	22.7	0.32	0.01
S923	22.7	24.2	0.17	0.01
S923	24.2	25.7	0.32	0.01
S923	25.7	27.2	0.66	0.01
S923	27.2	28.7	0.18	0.01
S923	28.7	30.2	0.28	0.01
S923	30.2	31.7	0.13	0
S923	31.7	33.2	0.08	0.01
S923	33.2	34.7	0.31	0.01
S923	34.7	36.1	0.24	0.01
S923	36.1	37.4	0.19	0.01
S923	37.4	38.7	0.66	0.01
S923	38.7	39.9	2.38	0.01
S923	39.9	41.1	1.66	0.14
S923	41.1	42.2	0.21	0.02
S924	13.8	15	0.16	0.01
S924	15	16.2	0.37	0.01
S924	16.2	17.5	1.07	0.01
S924	17.5	18.8	3.83	0.01
S924	18.8	19.7	6.6	0.01
S924	19.7	20.7	7.42	0.01
S924	20.7	22	1.5	0.01
S924	22	23.35	1.3	0.01
S924	23.35	24.45	1.31	0.01
S924	24.45	25.65	0.3	0.01
S924	25.65	26.85	0.88	0.01
S924	26.85	28.2	0.25	0.01
S924	28.2	29.6	0.61	0.01
S924	29.6	31	0.35	0.01
S924	31	32.4	0.35	0
S924	32.4	33.7	0.29	0.01
S924	33.7	35	0.37	0.01
S924	35	36.3	0.48	0.01
S924	36.3	37.6	0.22	0.01
S924	37.6	38.9	0.47	0.01
S924	38.9	40.1	0.5	0.01
S924	40.1	41.3	0.45	0.01
S924	41.3	42.4	0.78	0.01
S924	42.4	43.5	1.3	0.01
S924	43.5	44.55	0.96	0.01
S924	44.55	45.8	0.12	0.02
S924	45.8	47.1	0.02	0.01
S924	47.1	48.3	0.01	0.01
S924	48.3	49.5	0.01	0.01
S924	49.5	51	0.01	0
S925	16.3	17.3	0.5	0.01
S925	17.3	18.4	0.01	0.01
S925	18.4	19.7	0.4	0.03
S925	19.7	21	4.09	0.01
S925	21	22.3	4.27	0.01
S925	22.3	23.6	3.8	0.01
S925	23.6	24.9	0.99	0.01
S925	24.9	26.2	1.62	0.01
S925	26.2	27.5	1.46	0.01
S925	27.5	28.9	0.25	0.01
S925	28.9	30.35	0.19	0.01
S925	30.35	31.85	0.15	0.01
S925	31.85	33.4	0.17	0.01
S926	14	15.5	0.12	0.4
S926	15.5	17	0.24	0.02
S926	17	18.4	0.98	0.02
S926	18.4	19.9	2.82	0.01
S926	19.9	21.4	3.27	0.01
S926	21.4	22.4	1.14	0.01
S926	22.4	23.3	1.13	0.01
S926	23.3	24.2	0.95	0.01
S926	24.2	25	1.07	0.01
S926	25	26.2	0.39	0.01
S926	26.2	27.4	0.19	0.01
S926	27.4	28.55	0.06	0.01
S927	18.4	19.9	0.08	0.09
S927	19.9	21.4	0.14	0.08
S927	21.4	22.85	0.22	0.03
S927	22.85	24.35	0.1	0.21
S927	24.35	25.85	0.36	0.01
S927	25.85	26.9	0.33	0.09
S927	26.9	28	0.8	0.01
S927	28	29.1	0.95	0.01
S927	29.1	30.2	0.27	0.01
S927	30.2	31.4	0.52	0.01
S927	31.4	32.6	0.62	0.01
S927	32.6	33.8	0.44	0.01
S927	33.8	35	0.46	0.01
S927	35	36.3	0.46	0.01
S927	36.3	37.7	0.09	0.01
S927	37.7	39.1	0.57	0.02
S927	39.1	40.5	0.51	0.01
S927	40.5	41.6	0.64	0.21
S927	41.6	42.75	1	0.02
S928	22.7	23.9	0.33	0.3
S928	23.9	25.2	0.07	0.02
S928	25.2	26.5	0.08	0.16
S928	26.5	27.6	0.77	0.23
S928	27.6	28.6	1.49	0.02
S928	28.6	29.6	2.05	0.08
S928	29.6	30.7	3.89	0.89
S928	30.7	31.8	2.06	0.03
S928	31.8	33	1.45	0.07
S928	33	34.1	0.88	0.01
S928	34.1	35.1	1.11	0.01
S928	35.1	36.1	1.99	0
S928	36.1	37.5	1.86	0.01
S928	37.5	39	0.75	0
S928	39	40.4	0.86	0
S928	40.4	41.8	1.34	0
S928	41.8	43.1	2.44	0.01
S928	43.1	44.1	3.09	0.01
S928	44.1	45.1	2.55	0.01
S928	45.1	46.1	2.3	0.01
S929	21.7	23	0.5	0.04
S929	23	24.3	1.09	0.08
S929	24.3	25.5	0.6	0.03
S929	25.5	26.7	0.73	0.02
S929	26.7	27.8	1.88	0.01
S929	27.8	28.8	0.93	0.01
S929	28.8	29.8	1.29	0.01
S929	29.8	31	0.18	0.02
S929	31	32.2	0.69	0.06
S929	32.2	33.4	0.59	0.02
S929	33.4	34.6	0.57	0.02
S929	34.6	35.9	0.44	0.04
S929	35.9	37.2	0.23	0.1
S929	37.2	38.5	0.29	0.08
S929	38.5	39.8	0.32	0.02
S929	39.8	41.1	1.6	0.02
S929	41.1	42.5	0.56	0.01
S929	42.5	43.9	1	0.06
S929	43.9	45.2	0.28	0.02
S929	45.2	46.5	1.45	0.1
S929	46.5	47.8	1.77	0.01
S929	47.8	49.1	1.13	0.01
S929	49.1	50.2	2.32	0.01
S929	50.2	51.7	1.42	0.01
S930	6.6	7.9	2.42	1.03
S930	7.9	9.3	1.55	0.77
S930	9.3	10.7	2.45	2.06
S930	10.7	12.1	0.8	0.25
S930	12.1	13.5	1.14	0.18
S930	13.5	15	0.66	2.45
S930	15	16.4	0.58	0.62
S930	16.4	17.8	0.27	0.1
S930	17.8	19.1	0.51	0.07
S930	19.1	20.4	0.14	0.11
S930	20.4	21.7	0.26	0.06
S930	21.7	23	0.16	0.02
S930	23	24.3	0.33	0.02
S930	24.3	25.6	1.63	0.03
S930	25.6	26.9	1.4	0.05
S930	26.9	28	1.54	0.02
S930	28	29.1	2.26	0.06
S930	29.1	30.1	5.27	0.01
S930	30.1	31.5	0.39	0.02
S930	31.5	32.9	0.26	0.01
S931	4.65	5.9	1.85	0.04
S931	5.9	7.1	1.18	0.22
S931	7.1	8.3	1.22	1.39
S931	8.3	9.5	3.17	2.65
S931	9.5	10.9	3.23	0.09
S931	10.9	12.3	1.37	0.11
S931	12.3	13.6	0.3	0.03
S931	13.6	14.9	0.13	0.07
S931	14.9	16.2	0.63	0.01
S931	16.2	17.5	0.69	0.02
S931	17.5	18.7	0.04	0.02
S931	18.7	19.9	0.23	0.21
S931	19.9	21.1	0.25	0.05
S931	21.1	22.25	0.6	0.02
S931	22.25	23.8	1.1	0.07
S931	23.8	25.3	0.7	0.01
S931	25.3	26.8	0.69	0.02
S932	13.6	14.8	1.09	0.4

S932	14.8	16.1	1.35	0.06
S932	16.1	17.4	2.02	0.27
S932	17.4	18.7	1.57	0.03
S932	18.7	19.8	0.38	0.11
S932	19.8	20.8	0.02	0.07
S932	20.8	21.8	0.06	0.04
S932	21.8	22.8	0.91	0.53
S932	22.8	23.9	1.35	0.02
S932	23.9	25.1	0.17	0.06
S932	25.1	26.3	0.04	0.14
S932	26.3	27.5	0.02	0.08
S932	27.5	28.7	0.01	0.15
S932	28.7	30	0.01	0.03
S932	30	31.3	0.01	0.02
S932	31.3	32.6	0.85	0.05
S932	32.6	33.9	0.4	0.08
S932	33.9	35.2	0.02	0.02
S932	35.2	36.5	0.02	0.05
S932	36.5	37.8	0.22	0.1
S932	37.8	39.1	0.19	0.11
S933	12.1	13.6	1.4	0.01
S933	13.6	14.9	2.78	0.01
S933	14.9	16.2	2.25	0.03
S933	16.2	17.5	2.42	0.27
S933	17.5	18.8	0.55	1.6
S933	18.8	20.1	0.7	0.89
S933	20.1	21.5	0.02	0.03
S933	21.5	22.9	0.05	0.02
S933	22.9	24.2	0.01	0.02
S933	24.2	25.5	0.02	0.02
S933	25.5	26.8	0.3	0.01
S933	26.8	27.9	0.89	0
S933	27.9	28.9	1.47	0.01
S933	28.9	29.95	3.05	0.01
S934	18.4	19.5	2.55	0.01
S934	19.5	20.6	2.38	0.01
S934	20.6	21.8	2.34	0.67
S934	21.8	23	0.36	0.03
S934	23	24.2	0.03	0.02
S934	24.2	25.5	0.4	0.06
S934	25.5	26.8	0.02	0.03
S934	26.8	28.2	0.05	0.02
S934	28.2	29.7	0.02	0.02
S934	29.7	31.1	0.09	0.01
S934	31.1	32.3	0.82	0.01
S934	32.3	33.5	0.55	0.02
S934	33.5	34.7	0.15	0.02
S934	34.7	35.9	0.46	0.01
S934	35.9	37.1	1.52	0.01
S934	37.1	38.2	1.66	0
S935	8	9.4	1.08	0
S935	9.4	10.7	2.31	0.01
S935	10.7	12.05	1.41	0.01
S935	12.05	13.2	1.43	0.01
S935	13.2	14.3	1.58	0.01
S935	14.3	15.5	1.17	0.01
S935	15.5	16.9	0.43	0.07
S935	16.9	18.3	0.24	0.16
S935	18.3	19.7	0.21	0.01
S935	19.7	21.15	0.58	0.01
S935	21.15	22.4	0.55	0.01
S935	22.4	23.7	0.58	0
S935	23.7	24.9	0.38	0.01
S935	24.9	25.8	0.44	0
S935	25.8	26.65	0.03	0.01
S935	26.65	28.1	0.04	0.01
S935	28.1	29.55	0.06	0.01
S936	7.2	8.5	1.76	0.01
S936	8.5	9.8	3.73	0.01
S936	9.8	11	2.4	0.01
S936	11	12.2	1.02	0.01
S936	12.2	13.4	1.73	0.01
S936	13.4	14.6	0.63	0
S936	14.6	15.7	0.82	0.01
S936	15.7	17.2	0.14	0
S936	17.2	18.7	0.02	0.01
S936	18.7	20.2	0.23	0.01
S936	20.2	21.7	0.4	0
S936	21.7	23.2	0.12	0.01
S936	23.2	24.5	0.45	0.01
S936	24.5	25.8	1.32	0.01

S936	25.8	27	0.38	0.01
S936	27	28.3	0.18	0.01
S936	28.3	29.6	0.21	0.01
S936	29.6	30.9	0.02	0.01
S938	58.74	59.74	17.47	5.3
S938	59.74	61.22	4.2	0.5
S938	61.22	62.22	1.72	0.6
S939	45	46.2	0.05	0.08
S939	46.2	47.2	7.07	9.37
S939	47.2	48.95	2.98	0.81
S939	48.95	50.6	1.37	0.06
S940	78.88	80	0.09	0.04
S940	80	81	0.81	0.08
S940	81	82	1.12	0.06
S940	82	82.95	1.03	0.11
S941	75.5	76	0.25	1.14
S941	76	77.7	0.02	0.01
S941	77.7	78.75	0.39	0.43
S941	78.75	79.75	0.07	0.1
S941	86.4	86.8	0.08	0.02
S941	90.8	91.05	0.91	0.09
S941	91.05	91.6	0.7	0.06
S942	89.35	90.3	0.67	0.61
S942	95.6	96.05	0.66	2.01
S943	58.8	60	5.38	1.29
S943	60	60.75	9.85	0.84
S943	60.75	62	7.56	2.63
S943	62	63	3.16	5.7
S943	63	64	4.03	5.04
S943	64	64.8	4.58	3.62
S943	64.8	65.5	2.55	1.71
S944	51.95	52.45	29.94	0.78
S944	52.45	53.45	3.25	0.09
S944	53.45	54.85	7.4	0.13
S944	56.8	57.3	2.94	0.33
S945	44.4	46.4	0.12	0.06
S945	46.4	48.4	0.4	0.17
S945	48.4	49.65	0.11	0.11
S945	50	51.1	0.09	1.19
S946	77	78.5	1.15	0.28
S946	78.5	78.7	5.5	10.27
S946	78.7	80.35	0.34	0.4
S946	80.35	82	1.71	0.93
S946	82	84.08	1.04	0.9
S947	17.4	19.4	0.24	0.01
S947	19.4	21.4	0.25	1.03
S947	21.4	23.4	0.22	0.1
S947	23.4	24.1	2.15	0.22
S947	24.1	26.1	0.48	0.04
S947	26.1	28.1	0.51	0.04
S947	28.1	30.1	1.14	0.07
S947	30.1	32.3	0.24	0.17
S948	35	35.65	0.17	0.19
S948	36.1	37.2	1.38	0.05
S948	37.2	38.46	0.59	0.01
S949	56.45	57.45	5.39	0.21
S949	57.45	58.5	3.4	0.65
S950	30.8	32.8	0.35	0.65
S950	32.8	35	1.79	2.08
S950	35	36	0.98	1.58
S950	36	37.15	5.2	3.02
S950	37.15	38.25	17.37	1.07
S950	38.25	38.95	2.33	0.11
S950	38.95	40.5	1.76	0.08
S950	40.5	41.6	1.01	0.02
S951	64.2	64.85	0.02	0.06
S951	64.85	65.85	4.63	0.47
S951	65.85	66.6	5.17	4.79
S952	93	93.55	2.45	4.18
S952	93.55	94.1	1.31	2.52
S953	90.9	91.8	29.59	30.49
S953	91.8	92.65	4.41	7.34
S953	92.65	93	1.96	1.58
S953	117.95	118.5	0.1	0.24
S954	120.75	122.75	0.29	0.32
S954	122.75	124.75	0.21	0.14
S954	124.75	125.4	0.74	0.45
S954	125.4	126.42	2.03	1.84
S954	126.42	126.92	1.35	3.54
S955	104.4	105.1	36.81	23.95
S955	105.1	106.68	6.19	1

S956	117.55	118.33	20.97	26.41
S956	118.33	119.33	16.39	9.75
S956	119.33	120.33	14.33	7.98
S956	120.33	121.33	13.38	8.63
S956	121.33	122.33	4.2	4.49
S956	122.33	123.5	5.13	0.87
S956	123.5	124.75	1.87	1.02
S957	103.2	103.8	1.07	1.34
S957	103.8	104.8	9.37	1.38
S957	104.8	105.5	3.99	0.51
S957	105.5	106.5	0.88	0.09
S957	106.5	107.92	0.46	0.04
S957	107.92	109.15	1.93	0.33
S957	109.15	110.15	5.58	1.07
S957	111.35	111.7	4.48	4.35
S958	65	65.75	22.78	5.87
S958	65.75	66.9	7.36	1.08
S958	66.9	67.9	4.45	0.54
S958	67.9	69.5	2.21	0.09
S958	69.5	70.45	3.37	0.52
S958	88	88.45	5.83	5.75
S958	88.45	89.8	13.93	5.31
S958	89.8	91.2	2.58	0.63
S958	91.2	93	0.93	1.33
S960	28.7	30.7	1.58	0.04
S960	30.7	32.7	2.36	0.18
S960	32.7	34.7	3.18	2.84
S960	34.7	36.7	1.32	1.96
S960	37.7	38.7	1.73	0.27
S960	38.7	40.7	1.89	0.56
S960	40.7	42.7	1.56	0.05
S960	42.7	44.7	2.55	0.57
S960	44.7	46.7	2.07	0.36
S960	46.7	48.15	0.93	0.01
S961	51.15	51.5	10.32	1.19
S961	51.5	52.4	0.73	0.06
S961	52.4	53.4	1.71	2.14
S961	53.4	54.32	12.6	4.05
S961	55.35	55.95	0.15	0.02
S961	55.95	57	32.36	0.09
S961	57	58	15.92	0.18
S961	58	59.8	3.08	0.19
S961	59.8	61.15	1.2	0.22
S962	62.35	63.9	3.68	1.32
S962	63.9	65.57	8.13	0.08
S962	65.57	66.2	21.07	9.56
S962	66.2	67.2	6.58	1.08
S962	67.2	68.5	6.09	0.96
S962	68.5	69.85	4.27	0.6
S962	69.85	70.4	1.33	0.09
S962	70.4	71.7	4.18	0.2
S963	62.75	64.2	0.3	0.44
S963	69.1	69.6	7.93	0.36
S963	69.6	70.75	3.39	0.64
S963	70.75	72	2.76	1.01
S964	76.2	77	13.48	34.07
S964	77	77.83	4.01	2.5
S964	77.83	78.5	0.63	0.29
S965	83	83.55	1.65	3.74
S965	84.5	84.8	0.97	0.22
S965	84.8	86.3	2.29	3.05
S965	86.3	87.82	2.91	2.65
S966	60.2	61.3	2.39	0.21
S966	61.3	61.8	1.53	0.05
S966	62.5	63.9	1.05	0.13
U003	0	1.07	2.74	7.78
U003	1.07	3.9	1.15	0.04
U003	3.9	5.12	0.49	2.72
U003	5.12	6.19	0.32	0.18
U003	6.19	7.8	0.59	0.14
U003	7.8	9.27	1.3	1.12
U003	9.27	11.43	0.93	0.42
U003	11.43	13.29	4.29	2.39
U003	13.29	15.15	1.32	1.49
U003	15.15	16.46	6.15	1.03
U003	16.46	17.98	5.66	0.56
U003	17.98	19.87	2.51	0.29
U003	19.87	21.21	0.54	1.32
U003	21.21	22.52	25.8	0.01
U003	22.52	23.56	1.11	0.02
U003	23.56	25.15	1.32	0.01

U003	25.15	27.19	3.35	0.05
U003	27.19	28.47	1.1	0.62
U003	28.47	30.78	0.1	0.09
U003	30.78	31.94	1.52	0.06
U005	4.63	5.64	2.2	0.05
U005	5.64	7.16	1.85	0.11
U005	7.16	8.69	0.49	0.21
U005	8.69	9.3	0.16	0.23
U005	9.3	10.82	1.9	0.36
U005	10.82	12.34	1.46	0.34
U005	12.34	13.69	2.3	2.23
U005	13.69	15.24	0.35	0.3
U006	0	1.46	1.52	0.06
U006	1.46	2.83	0.93	0
U006	2.83	3.9	1.39	0
U006	3.9	5.18	0.66	0
U006	5.18	6.61	0.96	0
U006	6.61	8.81	1.28	0.01
U006	8.81	10.21	1.61	0
U006	10.21	11.52	1.22	0.03
U006	11.52	12.31	1.91	0
U006	12.31	14.2	2.93	0
U006	14.2	16.03	3.03	1.08
U006	16.03	18.01	1.63	0.58
U006	18.01	19.32	15.9	0.84
U006	19.32	20.7	0.78	0.03
U006	20.7	21.95	2.96	0.02
U006	21.95	23.07	1.81	0.02
U006	23.07	24.51	2.75	0.15
U006	24.51	25.97	2.91	0.02
U006	25.97	27.74	2.82	0.01
U006	27.74	28.93	3.17	0.01
U006	28.93	30.42	0.58	0.02
U006	30.42	31.94	2.15	0.02
U006	31.94	33.16	1.46	0
U006	33.16	34.38	0.91	0
U006	34.38	35.78	0.22	0.01
U006	35.78	37.19	0.41	0.01
U006	37.19	38.77	0.6	0
U006	38.77	40.33	0.55	0.02
U006	40.33	41.15	0.7	0.05
U006	41.15	42.06	2.4	0.12
U006	42.06	43.68	1.93	0.11
U006	43.68	44.53	4.57	0.14
U006	44.53	45.72	3.95	1.69
U008	3.02	3.75	1.44	1.52
U008	3.75	4.82	0.12	3.37
U008	4.82	6.31	0.77	0.72
U008	6.31	6.89	9.45	0.07
U008	6.89	8.75	0.28	0.62
U008	8.75	10.24	7.98	8.63
U008	10.24	11.46	6.11	1.53
U008	11.46	12.92	5.36	0.15
U008	12.92	14.3	21.6	0.17
U009	3.99	5.39	0.4	3.2
U009	5.39	6.71	0.03	2.31
U009	6.71	7.22	0.13	1.98
U009	7.22	8.63	0.3	1.55
U009	8.63	9.75	0.21	0.31
U009	9.75	11.37	0.91	1.71
U009	11.37	14.54	1.13	0.22
U009	14.54	15.94	0.51	0.02
U009	15.94	17.65	0.93	0.51
U009	17.65	18.9	1.21	0.63
U009	18.9	20.6	2.47	0.18
U009	20.6	21.76	1.33	0.09
U009	21.76	22.71	8.76	0.53
U009	22.71	24.14	2.86	0.06
U009	24.23	24.93	2.57	0.09
U009	24.93	25.54	0.54	0.35
U009	25.54	26.27	4.07	0.1
U009	26.27	27.86	2.16	0.2
U009	27.86	29.26	1.57	1.64
U009	29.26	30.63	5.02	0.05
U009	30.63	32.67	8.4	0.1
U009	32.67	33.13	8.26	0.01
U009	33.13	34.72	4.41	0.35
U009	34.72	36.03	0.91	0.07
U009	36.03	37.25	3.67	0.01
U009	37.25	38.1	1.74	0.2
U010	5.97	7.22	0.55	0.05

U010	7.22	7.83	11.6	0.01
U010	7.83	8.75	4.89	0.08
U010	8.75	10.42	5.3	0.58
U010	10.42	11.95	1.51	2.27
U010	11.95	13.26	3.12	2.26
U010	13.26	14.54	7.31	0.09
U010	14.54	16.34	3.56	0.06
U010	16.34	18.07	6.72	0.01
U011	0	1.4	6.31	0.16
U011	1.4	2.74	1.56	0.01
U011	2.74	4.14	5.98	0.02
U011	4.14	5.7	23.9	0
U011	5.7	6.13	50.2	0.12
U012	0	0.91	8.76	0.53
U012	0.91	2.32	1.21	0.11
U012	2.32	3.99	4.74	0.09
U012	3.99	5.06	1.79	0.01
U012	5.06	6.8	1.59	0.01
U012	6.8	8.47	1.78	0.2
U012	8.47	14.05	0.89	0.01
U012	14.05	15.48	5.99	0.48
U012	15.48	16.31	11.7	0.01
U012	16.31	17.43	18.4	0.71
U019	6.8	8.23	0.33	0.44
U019	8.23	8.99	1.74	2.56
U019	8.99	10.45	2.14	0.34
U019	10.45	11.89	0.77	0.4
U019	19.29	21.15	1.87	1.22
U019	21.15	22.65	3.84	0.6
U019	22.65	24.11	1.24	0.14
U021	0	2.23	0.18	0.07
U021	2.23	3.75	0.2	0.03
U021	3.75	5.06	3.34	0
U021	5.06	6.64	2.46	0.04
U021	6.64	8.14	5	6.03
U021	8.14	9.72	0.15	0.03
U021	9.72	11.25	0.16	0.28
U021	11.25	12.77	0.17	0.03
U021	12.77	14.3	0.16	0.05
U021	14.3	15.7	0.93	0.05
U021	15.7	17.19	0.45	0.04
U021	22.86	24.56	0.38	0.13
U023	0	1.49	2.16	1.47
U023	1.49	2.9	4.67	1.07
U023	2.9	4.66	2.61	0.16
U023	4.66	6.22	0.34	0.03
U023	6.22	7.77	1.23	2.01
U023	7.77	9.39	2.56	0.57
U023	9.78	11.43	2.11	0.62
U023	11.43	12.56	1.06	0.18
U023	12.56	13.99	0.98	0.37
U023	13.99	14.9	0.39	0.14
U023	14.9	16.46	0.2	0.08
U023	16.46	17.98	0.19	0.02
U023	17.98	19.57	0.96	0.01
U023	19.57	21.03	0.46	0.75
U023	21.03	22.86	0.3	0.1
U023	22.86	24.48	0.7	0.08
U024	9.14	10.76	1.45	1.39
U024	10.76	11.31	2.78	1.49
U024	11.31	12.5	5.22	8.54
U024	12.5	13.53	7.26	1.09
U024	13.53	14.17	1.12	0.06
U024	14.17	14.94	6.91	0.13
U024	14.94	16.28	8.78	0.22
U024	16.28	16.64	43.8	0.94
U024	16.64	17.77	16.3	0
U024	17.77	18.65	47.6	0
U025	10.39	11.61	2.66	2.51
U025	11.61	13.14	5.55	2.08
U025	13.14	13.65	14.3	5.44
U025	13.65	15.24	39.4	11
U026	20.54	22.16	12.4	12.4
U026	22.16	23.77	2.29	0.13
U026	23.77	24.17	11.8	1.01
U026	24.17	25.69	3.47	0.02
U026	25.69	26.7	1.96	0.04
U026	26.7	28.22	4.08	0
U026	28.22	29.72	3.95	0.04
U026	29.72	31.09	5.21	0
U027	15.7	16.12	4.43	1.87
U027	16.12	17.59	1.62	6.06
U027	17.59	18.68	1.45	3.14
U027	18.68	20.51	5.81	4.38
U027	20.51	22.04	8.3	2.5
U027	22.04	23.56	8.28	0.09
U027	23.56	25.09	4.18	0.24
U027	25.09	26.49	1.55	0.03
U028	6.46	7.01	5.31	0.04
U028	7.01	8.29	6.62	0.45
U028	8.29	9.97	8.86	0.29
U028	9.97	11.49	2.26	0.25
U028	11.49	13.14	1.04	0.16
U028	13.14	14.66	26.7	0.08
U028	14.66	15.42	23.2	0.17
U028	15.42	15.73	2.41	0.72
U029	0.27	1.22	8.02	0.01
U029	1.22	1.92	1.55	0.14
U029	1.92	2.77	0.42	0.13
U029	2.77	4.3	2.27	0.23
U029	4.3	4.57	14.7	0.07
U029	4.57	6.1	1.28	0.85
U029	6.1	7.62	5.84	4.8
U029	7.62	8.66	6.59	11
U030	0	1.52	9.32	1.53
U030	1.52	3.05	0.67	0.26
U030	3.05	4.57	1.28	0.25
U030	4.57	6.1	0.41	0.04
U030	6.1	7.62	0.29	0.12
U030	7.62	8.41	0.37	0.02
U030	8.41	9.6	20.3	6.86
U032	0	1.52	2.4	0.48
U032	1.52	3.05	4.22	1.76
U032	3.05	4.57	0.24	1.38
U032	4.57	4.87	0.17	0.58
U032	4.87	5.94	0.16	1.49
U032	5.94	7.62	8.61	3.05
U032	7.62	9.3	0.66	2.08
U032	9.3	10.73	1.04	1.12
U032	10.73	12.8	2.23	0.43
U032	12.8	15.09	12.7	0.51
U032	15.09	16.95	3.56	0.31
U032	16.95	17.98	18.5	0.98
U032	17.98	19.51	2.01	1.1
U032	19.51	21.03	3.62	1.54
U032	21.03	22.86	2.07	1.31
U034	0	0.3	5.95	0
U034	0.3	1.01	3.93	0.69
U034	1.01	1.62	5.03	0.38
U034	1.62	2.29	5.21	0.93
U034	2.29	3.81	0.31	0.16
U034	3.81	5.33	0.11	0.2
U034	5.33	6.86	0.55	0.09
U034	6.86	8.38	0.15	0.18
U034	8.38	10.61	1.85	0.11
U034	10.61	10.82	14.6	0.01
U034	10.82	11.73	1.3	0.12
U034	11.73	13.32	16.4	0
U034	13.32	14.05	24.1	9.62
U035	2.99	5.12	0.99	0.8
U035	5.12	5.64	3.88	1.39
U035	5.64	6.55	5.22	0.75
U035	6.55	8.23	6.96	0.38
U036	0	1.52	0.48	0.48
U036	1.52	3.05	0.22	0.35
U036	3.05	3.66	8.2	4.64
U036	3.66	4.57	1.12	0.35
U036	4.57	6.1	3.18	0.02
U036	6.1	7.68	3.27	0.79
U036	7.68	9.2	4.39	0.34
U036	9.2	10.88	2.78	0.07
U037	3.38	4.3	3.69	1.19
U037	4.3	5.79	0.14	0.22
U037	5.79	6.92	0.36	0.63
U037	6.92	7.86	2.51	0.59
U037	7.86	9.75	2.4	0.72
U037	9.75	10.61	2.13	0.2
U037	10.61	12.19	3.21	0.43
U037	12.19	13.17	5.2	0
U037	13.17	14.69	0.3	0.07
U037	14.69	16.67	2.03	0.35
U037	16.67	18.2	1.83	0.11
U037	18.2	19.72	1.76	0
U037	19.72	20.36	0.45	0.01
U037	20.79	22.56	4.53	0.01
U037	23.2	24.11	6.44	0
U037	24.11	24.84	6.61	0.01
U037	24.84	25.63	24.9	36
U038	13.78	15.3	2.26	1.61
U038	15.3	16.82	4.54	3.14
U038	16.82	17.68	5.08	1.02
U038	17.68	19.2	0.58	0.04
U038	19.2	20.73	0.63	0.09
U038	20.73	22.16	2.17	0.09
U038	22.16	23.62	2.56	0.28
U038	23.62	25.15	0.78	0
U039	12.86	14.39	0.81	0
U039	14.39	15.91	0.64	0
U039	15.91	17.43	2.15	0.08
U039	17.43	19.39	0.59	0.01
U039	19.39	20.79	8.75	0.42
U039	20.79	21.95	2.48	0.07
U039	21.95	22.4	6.08	0.24
U039	22.4	23.93	1.13	0
U039	23.93	25.18	0.34	0
U039	25.18	25.69	5.36	0
U039	25.69	27.22	0.39	0
U039	27.22	28.74	0.17	0
U040	8.02	8.56	1.15	0
U040	8.56	10.09	1.32	0
U040	10.09	11.64	1.85	0
U040	11.64	12.28	12.8	0
U040	12.28	13.47	1.41	0
U040	13.47	14.33	0.36	0
U041	0	0.61	12.6	4.29
U041	0.61	1.89	2.48	0.01
U041	1.89	3.41	0.62	0.03
U041	3.41	4.94	0.84	0.01
U041	4.94	6.37	0.47	0.14
U041	6.37	7.62	1.48	0.51
U042	0	1.52	3.08	0
U042	1.52	2.29	0.44	0
U042	2.29	3.81	3.19	0
U042	3.81	5.33	0.32	0.01
U042	5.33	5.64	18.9	0
U042	5.64	7.16	3.63	0.01
U043	0	1.95	1.81	0.2
U043	1.95	3.66	5.44	1.87
U043	3.66	4.3	0.06	0.28
U043	4.3	5.61	2.43	3.18
U043	5.61	6.95	1.44	2.1
U043	6.95	7.71	5	4.22
U043	7.71	8.96	1.12	0.79
U043	8.96	11.16	0.56	0.91
U043	11.16	11.83	2.42	3.94
U044	0	1.28	0.87	0.07
U044	1.28	2.8	1.27	0.08
U044	2.8	4.33	2	0
U044	4.33	5.3	1.5	0
U044	5.3	7.01	0.79	0.26
U044	7.01	8.02	3.4	7.12
U044	8.02	9.14	3.01	0.86
U044	9.14	10.06	8.05	0
U044	10.06	11.58	2.31	0.01
U044	11.58	12.56	2.93	0.06
U044	12.56	13.9	2.57	0.01
U045	9.3	10.82	2.19	0.7
U045	10.82	12.34	2.74	0.4
U045	12.34	13.87	3.96	0.37
U045	13.87	15.12	3.52	0.4
U045	15.12	15.64	21.5	3.46
U045	15.64	17.16	5.65	1.66
U045	17.16	18.17	3.98	2.18
U045	18.17	18.56	6.98	0.85
U045	18.56	20.24	2.11	0.01
U047	0	0.61	2.3	6.42
U047	0.61	1.95	2.39	3.67
U047	1.95	3.29	6.22	1.17
U047	3.29	3.96	15.9	0
U047	3.96	5.49	3.36	0
U047	5.49	5.88	13.8	0
U047	5.88	6.8	3.48	0.36
U047	6.8	8.32	5.89	0.01
U047	8.32	9.85	3.57	0
U047	9.85	11.37	2.73	0
U047	11.37	12.19	3.5	0
U048	0.79	1.4	5.83	2.42
U048	1.4	2.93	0.55	0.27
U048	2.93	4.08	0.89	0.08
U051	7.86	9.39	1.87	4.96
U051	9.39	10.91	1.12	0.16
U051	10.91	12.44	0.67	0.05
U051	12.44	14.11	0.54	0.13
U051	14.11	15.64	1.09	1
U051	15.64	17.47	2.49	1.96
U051	17.47	18.99	2.14	0.33
U051	18.99	20.51	0.89	0
U051	20.51	21.34	1.65	0
U051	21.34	22.22	6.54	0.05
U052	7.71	9.39	0.58	0.61
U052	9.39	11.16	1.31	0.27
U052	11.16	12.28	1.92	0.98
U052	12.28	12.89	0.08	0.38
U052	12.89	13.72	1.78	0.42
U052	13.72	15.24	3.18	1.09
U052	15.24	16.76	2.82	0.74
U052	16.76	18.29	1.95	0.65
U052	18.29	19.63	1.46	1.04
U052	19.63	21.15	1.62	0.17
U054	0	0.64	1.88	0.03
U054	0.64	1.71	0.59	0.03
U054	1.71	3.23	0.67	0.05
U054	3.23	4.75	1.18	0.46
U054	4.75	6.28	0.29	0.8
U054	6.28	7.44	0.83	0.09
U054	7.44	9.36	8.21	1.73
U054	9.36	10.88	1.22	0.29
U054	10.88	13.01	0.48	0.14
U054	13.01	14.39	0.59	0.05
U054	14.39	16.37	2.6	0.09
U054	16.37	17.89	2.33	0.01
U054	17.89	18.29	2.9	0.02
U054	18.29	18.62	15.2	54
U054	18.62	19.81	3.18	0.26
U055	0.43	1.55	2.8	3.11
U055	1.55	2.19	1.78	1.08
U055	2.19	3.08	1.38	0.97
U055	3.08	4.82	0.03	0.04
U055	4.82	5.15	1.8	0.94
U055	5.15	5.91	0.07	0.09
U055	5.91	7.92	0.9	0.66
U055	7.92	9.75	0.4	1.96
U055	9.75	11.58	0.14	2.05
U056	19.81	21.34	1.58	4.97
U056	21.34	22.86	1.61	0.32
U056	22.86	24.38	3.73	0.5
U056	24.38	25.91	1.41	2.48
U056	25.91	27.43	1.45	0.39
U056	27.43	28.96	1.06	0.18
U056	28.96	29.57	0.02	0.09
U057	19.35	19.81	0.39	0.11
U057	19.81	20.09	0.48	0.28
U057	20.09	21.34	3.85	2.41
U057	21.34	22.86	1.75	0.49
U057	22.86	24.38	3.99	0.49
U057	24.38	25.3	6.4	16.48
U058	15.69	16.67	1.63	2.69
U058	16.67	17.68	4.45	4.86
U058	17.68	18.29	5.39	2.61
U058	18.29	19.81	5	3.75
U058	19.81	21.34	5.64	2.47
U058	21.34	21.88	4.83	0.06
U058	21.88	22.56	30.52	0.05
U059	0	1.52	3.06	0.07
U059	1.52	3.05	1.16	0.11
U059	3.05	4.27	4.41	0.05
U060	0	0.82	0.53	0.37
U060	0.82	1.52	1.68	2.66
U060	1.52	2.29	1.56	0.26
U060	2.29	3.35	3.25	1.02
U060	3.35	4.45	1.35	0.03
U060	4.45	5.85	7.27	0.19
U060	5.85	7.01	1.89	0.13
U060	7.01	7.62	0.04	0.02

U060	7.62	8.84	1.39	0.62
U060	8.84	9.42	10.96	0.04
U060	9.42	10.67	1.39	0.12
U060	10.67	12.19	2.2	0.43
U061	0	1.52	1.03	0.75
U061	1.52	3.05	0.64	0.05
U061	3.05	3.96	1.34	0.57
U061	3.96	4.57	1.28	0.13
U061	4.57	6.1	1.27	0.11
U062	0	1.52	5.1	0
U062	1.52	3.05	5.42	0.06
U062	3.05	4.57	5.49	0.06
U062	4.57	6.1	4.56	7.07
U062	6.1	7.62	11.1	35.46
U062	7.62	7.78	10.92	2.17
U063	13.72	14.78	0.23	0.02
U063	14.78	15.24	1.78	0.01
U063	15.24	17.52	1.26	0
U063	17.52	19.81	3.17	0.76
U063	19.81	21.34	1.47	0.08
U063	21.34	22.86	1.06	0.11
U063	22.86	24.38	2.21	0.1
U063	24.38	25.9	0.84	0.08
U063	25.9	26.51	3.37	0.1
U063	26.51	27.12	5.83	0.4
U063	27.12	28.95	1.37	0.85
U063	28.95	30.48	1.42	0.5
U063	30.48	32.92	2.95	0.38
U063	32.92	33.52	3.12	0.06
U063	33.52	33.98	6.12	0.42
U063	33.98	36.05	3.07	1.09
U063	36.05	38.4	0.41	0.4
U064	16.76	18.29	0.2	0.02
U064	18.29	19.81	1.62	0
U064	19.81	20.73	1.6	0
U064	20.73	21.24	12.75	1.33
U064	21.24	22.95	1.42	0.44
U064	22.95	23.92	0.65	0.15
U064	23.92	25.29	3.41	0.43
U064	25.29	26.82	2.49	0.35
U064	26.82	28.34	0.04	0.01
U064	28.34	30.17	0.03	1.25
U064	30.17	30.93	4.35	2.2
U064	31.3	33.38	0.3	0.05
U064	33.38	33.68	3.95	2.42
U064	33.68	37.03	0.4	0.33
U064	37.03	38.25	2.37	3.72
U064	38.25	38.4	0.03	0.04
U065	0	1.52	2.24	0.38
U065	1.52	3.05	0.47	0.08
U065	3.05	3.96	0.93	0.42
U065	3.96	4.57	1.38	0.69
U065	4.57	6.1	0.76	0.03
U065	6.1	7.62	0.48	0.01
U067	0	1.52	1.03	20.64
U067	1.52	3.05	1.87	10.41
U067	3.05	4.57	5.99	9.74
U067	4.57	6.25	2.49	11.94
U067	6.25	7.62	0.49	3.71
U067	7.62	9.14	0.08	3.4
U067	9.14	10.67	8.18	0.94
U067	10.67	12.19	3.25	2.48
U067	12.19	14.02	6.57	7
U067	14.02	15.24	0.64	0.68
U067	15.24	16.61	0.1	0.11
U067	16.61	18.29	0.17	7.22
U067	18.29	19.81	4.05	6.5
U067	19.81	20.63	5.57	7.41
U067	20.63	21.34	0.15	0.16
U067	21.34	22.86	0.11	0.06
U067	22.86	24.38	2.62	1.86
U067	24.38	25.91	1.13	12.35
U067	25.91	27.13	2.51	8.94
U067	27.13	28.65	0.08	0.05
U068	0	1.52	0.34	0.06
U068	3.69	5.21	0.14	0.02
U069	0	1.01	1.24	0
U069	1.01	2.53	1.92	0
U069	2.53	4.05	1.88	0
U069	4.05	5.58	2.61	0
U069	5.58	6.1	0.66	0.12

U069	6.1	7.62	0.03	0.01
U069	7.62	9.14	0.05	0.01
U069	9.14	10.67	0.14	0.35
U069	10.67	12.19	0.3	0.08
U070	0	1.52	0.09	0.08
U070	1.52	3.04	1.73	0.14
U070	3.04	3.84	2.94	0.01
U070	3.84	4.97	0.81	0
U070	4.97	6.1	0.55	0.02
U070	6.1	7.62	0.35	0.01
U070	7.62	9.14	2.29	0
U070	9.14	10.67	3.21	0
U070	10.67	12.19	1.33	0.02
U070	12.19	13.72	1.49	0.01
U070	13.72	15.24	0.38	0.07
U071	0	1.52	1.67	0
U071	1.52	3.04	1.64	0
U071	3.04	4.57	9.8	0.01
U071	4.57	6.1	3.01	0
U071	6.1	7.6	2.48	0.06
U071	7.6	9.14	4.13	0.01
U071	9.14	10.67	3.32	0.03
U071	22.86	23.47	3.48	0.47
U071	23.47	23.65	7.42	11.45
U071	23.65	25.91	1.62	0.06
U073	13.1	14.02	9.24	12.18
U073	14.02	14.87	3.76	0.48
U073	14.87	15.54	5.48	0.49
U073	15.54	17.07	5.78	0.39
U073	17.07	17.98	3.94	0.7
U073	17.98	18.9	2.63	0.78
U073	18.9	20.42	1.69	0.33
U073	20.42	21.95	0.05	0.01
U073	21.95	23.04	0.44	0.08
U074	9.14	10.06	1.28	2.2
U074	10.06	11.58	0.92	13.52
U075	10.67	11.43	0.41	0.33
U075	11.43	11.83	0.77	2.79
U075	11.83	12.19	16.97	15.76
U075	12.19	13.72	3.46	4.84
U075	13.72	14.81	10.22	6.78
U075	14.81	15.12	20.46	5.4
U075	15.12	15.24	16.04	0.34
U075	15.24	17.07	0.65	1.56
U076	0	1.52	8.65	0.38
U076	1.52	2.26	22.56	33.88
U076	2.26	3.78	5.47	2.02
U076	3.78	5.43	4.27	5.92
U076	5.43	6.52	6.89	6.48
U076	6.52	6.98	16.35	41.25
U076	6.98	8.63	5.29	20.39
U076	8.63	9.91	2.62	0.5
U076	9.91	11.8	2.24	0.25
U076	12.13	13.87	8.83	71.56
U076	13.87	14.17	5.14	3.33
U076	14.17	14.75	18.13	46.43
U076	14.75	16.38	5.54	13.64
U076	16.38	17.47	0.91	0.08
U076	17.47	18.6	4.68	0.11
U076	19.2	20.21	8.91	3.35
U076	20.21	21.34	0.91	0.04
U076	21.34	23.26	0.33	0.08
U076	23.26	24.81	2.49	0.01
U076	24.81	25.97	1.96	0.04
U076	25.97	27.43	0.48	0.01
U076	27.43	28.96	2.94	0.03
U076	28.96	30.48	2.53	0.03
U076	30.48	32	3.06	0.03
U076	32	33.53	2.38	0
U076	33.53	35.05	2.62	0.02
U076	35.05	36.58	3.57	0.01
U076	36.58	37.83	1.33	0
U076	37.83	39.08	2.86	0.01
U076	39.08	40.23	2.76	0.01
U077	0	1.52	4.63	0.17
U077	1.52	2.07	4.89	0.48
U077	2.07	4.21	1.81	0.24
U077	4.21	5.52	2.56	0.24
U077	6.1	7.62	3.17	0.49
U077	7.62	8.53	2.24	0.18
U077	8.53	9.05	2.64	0.18

U077	9.05	10.67	2.46	0.31
U077	10.67	12.19	15.43	15.06
U077	12.19	13.72	2.5	0.12
U077	13.72	15.24	2.91	0.02
U077	15.24	16.76	3.2	0
U077	16.76	18.29	7.02	0.01
U077	18.29	19.81	3.57	0.03
U077	19.81	21.34	0.88	0.03
U077	21.34	22.59	1.19	0
U077	22.59	24.38	1.74	0.02
U077	24.38	25	2.76	0
U077	25.91	27.43	2.01	0.01
U077	27.43	28.96	2.47	0.01
U077	28.96	30.48	3.07	0.01
U077	30.48	31.4	3.03	0
U077	31.4	33.53	2.66	0.01
U077	33.53	35.05	3.13	0.01
U077	35.05	36.58	1.83	0
U077	36.58	38.1	2.2	0.02
U077	38.1	39.01	2.2	0
U078	0	1.52	3.3	0.41
U078	1.52	2.74	2.83	0.04
U078	2.74	3.41	3.26	3.22
U078	3.41	5.27	0.76	0.02
U078	5.27	6.1	0.35	0
U078	6.1	7.62	3.95	0.01
U078	7.62	9.14	8.73	0.02
U078	9.14	10.67	4.07	0.03
U078	10.67	12.2	3.12	0
U078	12.2	13.72	2.85	0
U078	13.72	15.24	2.15	0.02
U078	15.24	16.76	2.86	0.1
U078	16.76	18.29	3.69	0.02
U078	18.29	19.81	3.13	0.02
U078	19.81	21.34	3.11	0.01
U078	21.34	22.86	2.65	0.04
U079	0	1.52	0.23	0.01
U079	1.52	3.05	0.59	0.07
U079	3.05	4.57	0.58	0
U079	4.57	6.1	0.25	0
U079	6.1	7.62	0.4	0
U079	7.62	9.14	0.19	0
U079	9.14	10.67	0.19	0
U079	10.67	12.19	0.19	0
U079	12.19	13.29	0.16	0
U079	13.29	14.57	0.18	0
U079	14.57	16.76	0.14	0
U079	16.76	18.29	0.19	0
U079	18.29	19.63	0.42	0.01
U079	19.63	19.81	0.02	0
U079	19.81	21.34	0.2	0.01
U079	21.34	22.86	0.12	0.07
U079	22.86	23.53	0.04	0.09
U079	23.53	24.38	0	1.12
U079	24.38	25.91	0	0.57
U079	25.91	27.43	0	0.13
U079	27.43	28.96	0	0
U079	28.96	30.48	0	0
U079	30.48	31.06	0	0
U080	0	1.52	0.77	0.01
U080	1.52	2.6	0.19	0.09
U080	2.6	3.44	0.58	0
U080	3.44	5.33	0.76	0.16
U080	5.33	5.73	0.2	0
U080	5.73	6.1	0.2	0
U080	6.1	7.74	0.23	0.08
U080	7.74	8.6	0.03	0.07
U080	8.6	9.14	0.05	0.21
U080	9.14	10.61	0.03	0.25
U080	11.27	13.08	0	0.02
U081	0	1.52	1.94	0.15
U081	1.52	1.79	1.08	0.02
U081	1.79	2.43	3.97	2
U081	2.43	3.05	0.08	0.15
U081	3.05	3.77	0.98	1.26
U081	3.77	4.57	0.3	0.07
U081	4.57	6.1	0.18	0.18
U081	6.1	7.8	0.01	0.13
U081	7.8	8.81	0.02	0.05
U082	0	1.52	1.51	0.11
U082	1.52	3.05	5.86	0.12

U082	3.05	4.57	0.44	0.04
U082	4.57	6.1	0.66	0.06
U082	6.1	6.4	3.67	1.22
U082	6.4	7.62	0.38	0.07
U082	7.62	9.14	0.59	0.43
U082	9.14	10.67	0.18	0.02
U082	10.67	11.95	0.17	0.32
U083	0	1.52	0.78	0.09
U083	1.52	3.05	2.26	0.05
U083	3.05	4.57	3.54	0.22
U083	4.57	6.1	3.88	0.22
U083	6.1	7.62	0.85	0.1
U083	7.62	8.84	1.08	0.1
U084	0	3.05	1.18	0.03
U084	3.05	5.79	1.16	0.03
U085	0	0.76	4.02	0.08
U085	0.76	1.52	1.01	0.03
U085	1.52	2.8	3.1	0.01
U085	3.04	3.87	10.17	0.01
U085	3.87	6.09	1.31	0.01
U085	6.09	8.22	0.76	0
U085	8.22	9.14	18.49	0.08
U085	11.28	12.64	15.02	5.14
U085	14.32	19.2	0.37	0.25
U086	0	1.52	0.35	1.61
U086	1.52	3.81	0.03	0.15
U086	3.81	4.36	0.01	0
U087	0	1.52	1.66	0.02
U087	1.52	3.04	1.32	0.03
U087	3.04	4.57	2.78	0.11
U087	4.57	6.1	1.41	0.01
U087	6.1	7.62	4.52	0.01
U087	7.62	9.54	1.88	0
U087	9.54	12.19	0.45	0
U087	12.19	13.01	1.8	0.01
U087	13.01	15.24	0.36	0.02
U088	7.62	7.98	5.37	0
U088	8.32	9.14	4.4	0.99
U088	9.14	9.54	9.33	1.58
U088	9.54	10.57	0.07	0.01
U088	10.57	10.66	3.59	0.01
U088	10.66	11.3	0.06	0.01
U088	11.3	12.98	4.62	0.1
U088	12.98	14.66	16.41	0.4
U088	14.66	16.06	9.7	0.04
U088	16.06	16.33	38.84	21.36
U089	7.52	9.14	1.72	1
U089	9.14	10.06	2.2	0.79
U089	10.06	10.67	11.22	1.31
U089	10.67	11.28	6.36	4.77
U089	11.37	12.19	5.75	0.27
U089	12.19	13.72	6.35	0.08
U089	13.72	15.24	3.99	0.14
U089	15.24	16.76	3.95	0.18
U089	16.76	17.56	5.89	0.04
U089	17.56	18.29	11.58	0.02
U089	18.29	18.68	8.97	0
U089	18.68	19.32	4.05	0.02
U089	19.32	19.87	8.37	0
U089	19.87	19.94	3.08	0.14
U090	15.39	16.55	0.1	0.05
U090	16.55	16.76	0.08	0.48
U090	16.76	18.29	0.2	0.3
U090	18.29	19.81	0.43	0.11
U090	19.81	21.34	0.37	0.17
U090	21.34	22.56	0.1	0
U091	0	1.22	1.91	1.8
U091	1.22	1.52	0.65	2.27
U091	1.52	2.56	3.9	2.69
U091	3.05	4.57	3.96	0.12
U091	4.57	6.1	5.98	0
U091	6.1	7.62	8.86	0
U091	7.62	9.14	4.17	0
U091	9.14	10.67	0.91	0
U091	10.67	12.19	1.4	0
U091	12.19	12.77	1.16	0
U091	13.41	14.23	0.39	0
U091	14.94	15.85	0.1	0
U092	0	3.05	1.56	1.63
U092	3.05	6.1	1.19	2.65
U092	6.1	9.14	2.98	3.26

U092	9.14	12.19	1.6	1.81
U092	12.19	15.24	3.18	1.77
U092	15.24	18.29	2.55	4.05
U092	18.29	21.34	1.18	1.14
U092	21.34	24.38	1.74	0.53
U092	24.38	26.67	4.2	0.6
U092	27.74	30.78	2.55	0.66
U093	0	3.05	0.39	1.32
U093	3.05	6.1	3.39	2.72
U093	6.1	9.14	1.79	4.81
U093	9.14	12.19	2.2	2.24
U093	12.19	15.24	1.4	3.36
U093	15.24	18.29	2.8	3.37
U093	18.29	21.34	2.79	1.86
U093	21.34	24.38	1.07	4.29
U093	24.38	25.91	0.38	3.85
U093	25.91	26.43	0.17	9
U093	26.43	27.43	0.06	0.11
U093	27.43	29.87	0.18	1.64
U094	0	2.42	1.14	0.81
U094	2.42	4.56	1.15	0.42
U094	4.56	6.88	1.09	0.57
U094	6.88	9.12	0.83	0.13
U094	9.12	11.24	1.13	0.87
U094	11.24	13.68	1.09	1.98
U094	13.68	15.9	1.13	5.17
U094	15.9	18.24	5.2	1.75
U094	18.24	20.56	0.45	2.64
U094	20.56	22.28	0.86	3.81
U094	22.28	24.32	5	0.31
U094	24.32	26.69	5.34	0.73
U094	26.69	27.36	0.22	0.05
U095	0	2.29	1.32	2.16
U095	2.29	4.59	1.66	0.68
U095	4.59	6.1	0.57	1.1
U095	6.1	8.38	1.61	6.09
U095	8.38	10.67	3.4	8.8
U095	10.67	12.95	0.95	1.5
U095	12.95	15.24	0.99	2.76
U095	15.24	17.53	2.29	2.82
U095	17.53	19.81	1.17	5.46
U095	19.81	22.1	1.73	7.71
U095	22.1	24.38	0.78	1.79
U095	24.38	26.67	1.05	1.4
U095	26.67	28.96	2.05	5.96
U095	28.96	31.24	0.76	2.2
U095	31.24	33.53	2.54	1.82
U095	33.53	37.49	0.7	1.05
U096	0	1.52	1.08	1.39
U096	1.52	3.05	1.04	1.65
U096	3.05	4.57	1.14	2.02
U096	4.57	6.1	1.35	5.13
U096	6.1	7.01	1.82	5.96
U096	7.01	8.3	0.78	2.72
U096	8.3	9.14	1.07	2.5
U096	9.14	10.67	1.66	4.79
U096	10.67	11.37	0.37	1.48
U097	0	1.52	0.01	0.04
U097	1.52	3.23	0.2	0.43
U097	6.27	7.62	0.08	0.15
U097	7.62	9.14	0.03	0
U097	9.14	10.67	0.21	0.02
U097	10.67	12.19	0.39	0.02
U097	12.19	13.72	0.39	2.8
U097	13.72	15.24	0.44	3.03
U097	15.24	16.76	0.18	9.47
U097	16.76	18.29	0.39	6.09
U097	18.29	19.81	0.99	23.64
U097	19.81	21.34	0.37	2.29
U097	21.34	22.86	0.25	1.85
U097	22.86	24.38	0.4	3.29
U097	24.38	25.91	0.23	4.5
U097	25.91	27.43	0.4	1.8
U097	27.43	29.26	0.56	0.29
U097	29.26	30.48	2.25	0.42
U097	30.48	33.53	0.22	0.23
U099	0	0.61	0.18	1.03
U099	0.61	0.79	0.09	0.83
U099	0.79	1.52	0.34	4.47
U099	1.52	2.38	0.59	8.2
U099	2.38	2.65	0.95	4.19
U099	2.65	4.57	1.52	6.86
U099	4.57	6.1	2.39	1.69
U099	6.1	7.8	0.98	0.82
U099	7.8	8.14	0.43	8.33
U099	8.14	8.93	0.37	2.21
U099	8.93	9.08	2.89	8.85
U099	9.08	10.67	0.4	1.24
U099	10.67	12.19	0.79	1.26
U099	12.19	13.11	0.39	0.8
U099	13.11	13.72	1.16	0.04
U099	14.81	15.24	1.62	0.03
U099	15.24	18.28	2.52	0.09
U099	18.28	18.71	16.88	0.35
U099	18.71	20.17	35.46	40
U099	20.17	20.48	3.73	11.74
U099	20.48	23.77	0.34	0.62
U100	0	2.44	0.14	0.23
U101	0	3.05	0.02	0.01
U101	3.05	4.57	0.05	0.01
U101	4.57	6.86	0.08	0.24
U101	6.86	9.14	0.24	2.33
U101	9.14	10.06	0.91	0.65
U101	10.06	12.19	3.46	2.08
U101	12.19	14.48	2.77	2.96
U101	14.48	16.76	2.13	2.71
U101	16.76	18.29	4.24	1.93
U101	18.29	20.57	1.61	5
U101	20.57	22.86	1.17	1.34
U101	22.86	25.15	0.77	0.42
U101	25.15	27.43	1.15	0
U101	27.43	29.72	1.74	0
U101	29.72	32	0.58	0.03
U101	32	33.53	4.97	0
U101	33.53	33.68	51.72	0
U101	34.44	37.8	0.1	0.05
U102	0	2.35	0.79	0.74
U102	2.35	4.57	0.55	0.9
U102	4.57	6.1	0.17	0.08
U102	6.1	7.62	0.16	0.2
U102	7.62	9.14	0.36	0.18
U102	9.14	10.67	0.38	0.01
U102	10.67	12.2	0.28	0.62
U102	12.2	13.72	0.39	0.86
U102	13.72	15.24	0.58	0.3
U102	15.24	16.76	0.21	0.02
U102	16.76	18.29	0.27	0.02
U102	18.29	20.57	1.16	0.25
U102	20.57	22.86	0.2	0.08
U102	22.86	25.3	0.48	0.06
U102	25.3	27.43	4.44	0
U102	27.43	27.8	37.54	0.08
U102	27.8	31.09	4.02	0.35
U103	0	2.16	2.39	1.18
U103	2.16	4.57	1.15	0.13
U103	4.57	6.8	0.43	0.01
U103	6.8	9.14	0.19	0.1
U103	9.14	11.43	0.55	0.23
U103	11.43	13.72	0.19	1.18
U103	13.72	16	0.39	0.46
U103	16	18.29	0.38	0
U103	18.29	22.25	1.69	0
U104	0	0.79	0.04	0.24
U104	9.29	9.75	0.04	0.51
U104	16.49	18.28	0.95	5.32
U104	18.28	20.57	0.38	5.29
U104	20.57	22.86	1.15	2.31
U104	22.86	24.38	0.96	7.1
U104	24.38	26.12	1.39	5.94
U104	26.12	28.19	5.96	16.02
U104	28.19	30.69	1.21	3.79
U104	30.69	31.6	4.73	0.67
U104	31.6	33.52	6.21	0.48
U104	33.52	35.81	5.08	1.02
U104	35.81	38.1	3.8	0.2
U104	38.1	39.62	9.4	0.28
U104	39.62	41.14	2.04	0.48
U104	41.14	42.67	12.36	1.1
U104	42.67	45.29	43.22	16.95
U104	45.29	46.63	5.05	0.92
U105	0	1.52	2.49	0.58
U105	1.52	3.05	1.57	0.3
U105	3.05	6.1	1.06	0.1
U105	6.1	13.9	0.56	0.1
U105	14.48	18.28	0.39	0.02
U105	18.28	19.2	0.18	0.04
U105	19.2	29.26	0.01	0
U106	0	1.52	0.58	0.34
U106	1.52	3.04	2.19	0.32
U106	3.04	4.57	2.94	0.01
U106	4.57	5.79	12.93	0.47
U106	5.79	9.14	2.72	1.17
U106	9.14	10.66	1.15	1.31
U106	10.66	12.19	1.61	0.03
U106	12.19	13.71	1.38	0.09
U106	13.71	15.24	3.19	0.08
U106	15.24	16.76	4.04	1.67
U106	16.76	18.28	1.55	0.76
U106	18.28	19.81	0.19	0.26
U106	19.81	21.33	0.59	0.02
U106	21.33	22.86	1.39	0.06
U106	22.86	24.38	1.29	0.9
U106	24.38	25.9	0.8	0.06
U106	25.9	27.43	0.49	0.03
U106	27.43	28.95	0.6	0.03
U106	28.95	30.48	0.58	0.08
U107	0	1.88	0.37	0.76
U107	1.88	3.05	4.54	0.55
U107	3.05	4.57	4.57	0.66
U107	4.57	6.09	0.36	0.29
U107	6.09	8.04	0.51	0.05
U108	0	1.52	1.29	0
U108	1.52	2.13	12.43	0
U108	2.13	2.74	40.48	20.64
U109	0	3.04	2.6	0.01
U109	3.04	6.09	4.45	0.01
U109	6.09	9.14	4.89	0.04
U109	9.14	10.66	3.36	0.06
U109	10.66	12.49	1.91	0.16
U109	12.49	15.24	38.67	3.68
U109	15.24	16.91	33.45	0.27
U110	0	6.73	0.6	0.06
U110	6.73	14.02	5.43	0.36
U110	14.02	16.22	4.65	3.79
U110	16.22	18.89	0.57	0.37
U111	0	3.04	0.38	0.03
U111	3.04	4.66	1.71	0.04
U111	4.66	6.67	31.8	0.18
U111	6.67	9.14	5.28	0.26
U111	9.14	12.19	2	0.01
U111	12.19	15.24	3.89	0.07
U111	15.24	18.28	0.19	0.33
U111	18.28	21.64	0.4	0.04
U112	0	0.51	1.19	0.02
U112	0.51	3.04	0.4	0.02
U112	3.04	6.09	0.7	0.11
U112	6.09	9.14	1.27	0.75
U112	9.14	11.34	1.59	5.25
U112	11.34	13.72	1.17	0.09
U112	13.72	16.76	0.99	0.78
U113	0	3.04	1.3	8.18
U113	3.04	6.09	0.55	0.16
U113	6.09	9.14	0.19	1.21
U113	9.14	12.19	1.37	1.24
U113	12.19	13.71	1.77	0.2
U113	13.71	14.02	0.61	0.04
U114	10.97	11.27	2.8	0.04
U114	11.27	12.46	0.59	0.2
U114	12.46	13.71	16.1	0.5
U114	13.71	15.24	3.19	0.01
U114	15.24	17.06	15	0.03
U115	2.34	2.52	14.09	2.78
U115	2.52	4.57	10	0.06
U115	4.57	6.7	8.95	0.03
U116	5.46	6.79	10.5	0.02
U117	3.38	7.04	1.57	0.06
U117	7.04	9.14	6.23	1.88
U117	9.14	10.66	7.93	9.44
U117	10.66	11.3	0.77	0.23
U117	11.3	12.19	17.92	0.89
U117	12.19	15.24	15.47	0.04
U117	15.24	16	15	0.08
U117	16	16.64	33.82	0.03
U117	16.64	17.28	39.81	9.16
U117	17.28	18.28	9.46	0.12
U117	18.28	21.33	3.46	0.03
U117	21.33	23.9	4.15	0.03
U117	23.9	24	5.56	26.39
U118	0	1.52	6.47	9.98
U118	1.52	3.04	3	77.22
U119	3.41	6.09	0.22	0.02
U119	6.09	9.14	0.11	0.01
U119	9.14	12.19	0.01	0.02
U119	12.19	15.24	0.08	0.01
U119	15.24	18.29	0.19	0
U119	18.29	21.34	0.09	0
U120	0	3.05	0.39	0
U120	3.05	4.57	1.2	0
U120	4.57	6.09	0.19	0
U120	6.09	9.14	1.82	0
U120	9.14	12.19	0.56	0
U120	12.19	15.24	0.06	0
U120	15.24	18.29	0.37	0
U120	18.29	21.34	0.7	0.22
U120	22.56	24.38	1.29	0
U121	0	3.04	0.11	0
U121	3.04	6.09	1.16	0
U121	6.09	9.14	0.64	0
U121	9.14	12.19	0.45	0
U121	12.19	15.24	0.35	0
U121	15.24	18.28	0.36	0
U121	18.28	21.33	1.8	0
U121	21.33	24.38	0.71	0
U122	0.64	1.83	0.24	0
U122	1.83	4.57	0.88	0
U122	4.57	6.55	0.68	0
U122	6.55	9.14	0.62	0.02
U122	9.14	12.19	0.37	0
U122	12.19	15.24	0.51	0.43
U122	15.24	18.28	0.91	0
U122	18.28	21.33	0.97	0
U122	21.33	23.16	0.8	0
U123	0.39	3.04	0.38	0
U123	3.04	4.69	0.67	0
U123	4.69	7.62	0.54	0.01
U123	7.62	10.67	0.3	0
U123	10.67	13.76	0.12	0.02
U123	13.76	16.76	1	0.16
U123	16.76	19.81	0.86	0.18
U123	19.81	21.64	0.81	0
U124	1.21	3.04	1.15	0
U124	3.04	6.09	0.59	0
U124	6.09	9.14	0.21	0.05
U124	9.14	12.19	0.17	0
U124	12.19	15.24	0.88	0
U124	15.24	17.37	0.4	0
U125	4.36	4.72	0.13	0.02
U125	4.72	7.71	0.56	0.59
U125	8.08	10.66	0.22	0.06
U125	10.66	13.71	0.38	0.15
U125	13.71	16.76	0.6	1.67
U125	16.76	19.81	0.91	0.89
U125	19.81	22.86	0.97	0.88
U125	22.86	25.18	0.77	0
U126	3.93	6.09	0.85	0
U126	6.09	9.14	0.44	0
U126	9.14	12.19	0.69	0
U126	12.19	15.24	0.12	0.03
U126	15.24	18.28	0.43	0.11
U126	18.28	19.81	0.6	0.07
U126	19.81	22.86	1.4	0.21
U126	22.86	25.9	0.19	0
U126	25.9	27.43	0.59	0
U127	0	3.04	2.54	1.69
U127	3.04	5.33	0.74	0.13
U128	0	3.04	0.36	0.26
U128	3.04	6.09	0.41	0.6
U128	6.09	9.14	0.56	7.45
U128	9.14	10.82	1.5	5.29
U128	10.82	13.72	4.54	1.85
U128	13.72	16.76	0.1	0.23
U128	16.76	19.81	0.11	0.19
U129	0	3.04	3.15	2.11
U129	3.04	6.09	1.31	1.32

U129	6.09	9.14	0.77	0.99
U129	9.14	12.19	2.18	1.6
U129	12.19	15.24	1.75	2.17
U129	15.24	18.28	1.32	3.78
U129	18.28	21.33	1.79	5.17
U129	21.33	24.38	0.38	4.62
U129	24.38	27.52	0.2	5.1
U129	28.8	32	0.72	3.25
U129	32	35.05	0.8	4.39
U129	35.05	39.01	0.18	6.99
U130	0	3.04	0.55	0.47
U130	3.04	6.27	0.25	0.04
U131	0	1.52	1.98	1.18
U131	1.52	3.04	1.38	1.46
U131	3.04	4.57	1.48	1.92
U131	4.57	6.09	0.82	0.9
U131	6.09	7.62	1.88	1.68
U131	7.62	9.44	1.08	3.06
U143	0	3.04	1.86	8.12
U143	3.04	6.09	1.72	3.02
U143	6.09	9.14	6.08	4.96
U143	9.14	10.39	2.98	6.66
U143	10.39	11.88	1.68	1.44
U143	11.88	12.19	1.74	3.7
U143	12.19	15.24	2.08	2.6
U143	15.24	18.28	1.6	0.48
U143	18.28	19.53	1.58	0.16
U143	19.53	22.86	2.1	0.08
U143	22.86	23.92	2.28	0.58
U143	24.38	25.9	1.16	0.12
U143	25.9	27.88	1.92	0.04
U143	27.88	30.48	0.66	0.1
U143	30.48	31.39	1.06	0.04
U143	31.39	32.15	18.3	0.02
U144	0	3.04	0.27	0.1
U144	3.04	6.09	0.07	0.11
U144	6.09	9.14	0.09	0.04
U144	9.14	12.19	0.49	0.12
U144	12.19	15.24	1.36	0.41
U144	15.24	18.28	0.87	0.08
U144	18.28	21.33	0.37	0.06
U144	21.33	24.38	0.65	0.01
U145	0	1.52	0.72	0.02
U145	1.52	3.04	0.02	0.14
U145	3.04	4.57	0.11	0.14
U145	4.57	6.09	0.12	0.16
U145	6.09	7.62	0.12	0.04
U145	7.62	9.14	0.28	0.03
U145	9.14	10.42	0.95	0.01
U145	10.42	12.19	0.2	0.04
U145	12.19	15.24	0.09	0.13
U145	15.24	18.28	0.67	0.12
U145	18.28	19.81	0.51	0.12
U145	19.81	21.34	0.43	0.07
U145	21.34	23.77	0.64	0.08
U146	0	1.52	2.04	0.06
U146	1.52	3.04	1.09	0.2
U146	3.04	4.57	0.44	0.03
U146	4.57	6.09	1.24	0.01
U146	6.09	7.62	0.76	0.01
U146	7.62	9.14	0.83	0.01
U146	9.14	10.67	0.61	0.01
U146	10.67	12.19	0.3	0.01
U147	0	1.52	2.74	0.56
U147	1.52	3.04	1.6	0.04
U147	3.04	4.57	1.18	0.06
U147	4.57	9.14	0.7	0.02
U147	9.14	10.67	0.66	0.32
U147	10.67	12.19	1.08	0.74
U147	12.19	13.72	2.92	10.9
U147	13.72	15.85	3.1	1.78
U148	0	1.52	1.94	0.02
U148	1.52	3.04	0.48	0.01
U148	3.04	4.57	0.48	0.24
U148	4.57	6.09	0.78	0.05
U148	6.09	7.62	2.11	0.24
U148	7.62	9.14	0.65	0.03
U148	9.14	10.67	0.68	0.02
U148	10.67	12.19	0.1	0.06
U148	12.19	14.17	0.35	0.1
U148	14.17	16	2.62	0.56

U148	16	17.34	1.73	1.14
U148	17.34	18.29	0.56	0.85
U148	18.29	21.34	0.53	0.42
U148	21.34	24.39	0.89	0.26
U148	24.39	26.82	1.38	0.86
U149	0	0.79	5.4	2.62
U149	0.79	3.05	0.32	0.14
U149	3.05	4.57	2.62	0.04
U149	4.57	6.1	0.96	0.18
U149	6.1	7.32	1.54	0.29
U149	7.32	9.14	0.28	0.22
U149	9.14	13.26	0.55	0.03
U150	0	2.28	2.54	0.04
U150	2.28	3.04	0.93	0.01
U150	3.04	6.09	0.58	0.04
U150	6.09	9.14	0.4	0.03
U150	9.14	12.19	0.08	0.03
U150	12.19	15.24	0.32	0.01
U150	15.24	18.28	0.3	0.09
U150	18.28	21.33	0.14	0.14
U150	21.33	23.77	0.23	0.28
U150	23.77	27.43	0.44	0.07
U150	27.43	30.48	0.4	0.35
U151	0	2.19	0.05	0.03
U151	2.19	3.04	0.4	0.24
U151	3.04	6.09	0.3	0.2
U151	6.09	10.1	0.26	0.01
U151	10.1	12.19	0.85	0.03
U151	12.19	15.24	0.27	0.01
U151	15.24	19.35	0.18	0.14
U151	19.81	22.86	0.1	0.01
U151	22.86	24.38	0.79	1.06
U152	0	1.92	1.84	0.92
U152	1.92	2.59	0.14	0.16
U152	2.59	4.57	12.2	2.22
U152	4.57	6.09	1.24	12.4
U152	6.09	7.62	4.32	0.06
U152	7.62	9.41	5.88	0.5
U152	9.41	10.67	1.28	0.1
U152	10.67	13.22	0.16	0.1
U152	13.22	15.72	3.32	0.08
U152	15.72	16.82	0.06	0.08
U152	16.82	18.71	3.14	0.16
U152	18.71	21.33	3.14	0.18
U152	21.33	24.38	2.64	0.06
U152	24.38	25.42	0.48	0.1
U152	26.57	28.95	1.24	0.1
U152	28.95	31.79	1.8	0.46
U152	31.79	32.3	4.84	0.06
U153	0	2.25	1.58	0.28
U153	2.25	3.47	11.8	3.12
U153	3.47	4.81	4.96	9.28
U153	4.81	6.3	0.36	0.5
U153	6.3	8.29	8.1	1.72
U153	8.29	9.44	4.06	0.3
U153	9.44	12.19	0.34	0.26
U153	12.19	13.89	1.8	0.2
U153	13.89	16.76	0.88	0.09
U153	16.76	19.81	1.68	0.22
U154	0	1.52	5.74	1.14
U154	1.52	2.31	0.24	0.14
U154	2.31	3.04	12.88	8.22
U154	3.04	4.57	11.9	13.3
U154	4.57	6.3	9.34	4.76
U154	6.3	7.62	4.06	2.98
U154	7.62	9.14	2.74	0.28
U154	9.14	10.85	2.32	0.14
U154	10.85	12.19	1.14	0.02
U154	12.19	13.77	0.12	0.14
U154	13.77	15.24	1.32	0.06
U154	15.24	17.06	1.86	0.04
U154	17.06	18.28	1.42	0.04
U154	18.28	19.81	0.62	0.28
U154	19.81	21.33	2.4	0.09
U154	21.33	22.86	1.98	0.52
U154	22.86	24.38	5.66	2.54
U155	0	1.34	0.06	0.28
U155	1.34	3.04	8.16	14.3
U155	3.04	4.87	0.63	0.32
U155	4.87	6.55	11.7	0.04
U155	6.55	7.62	3.48	0.02

U155	7.62	9.14	1.28	0.07
U155	9.14	11.52	3.06	0.12
U155	11.52	12.67	0.46	0.08
U155	12.67	14.63	0.3	0.04
U155	14.63	16.76	4.14	0.11
U155	16.76	18.28	4.06	0.22
U155	18.28	19.35	2.36	0.14
U155	19.35	21.33	0.52	0.06
U155	21.33	22.86	0.86	0.05
U155	22.86	24.38	1.35	0.24
U155	24.38	25.9	2.92	0.16
U155	25.9	27.43	1.04	0.09
U155	27.43	28.95	1.92	0.04
U155	28.95	29.87	1.12	0.02
U155	29.87	30.48	4.36	0.01
U155	30.48	32	0.74	0.02
U155	32	33.53	2.72	0.01
U155	33.53	35.05	1.68	0.12
U155	35.05	36.12	0.22	0.02
U155	36.72	37.64	1.46	0.08
U156	0	1.28	1	0.08
U156	1.28	3.04	0.46	0.18
U156	3.04	4.57	0.48	0.34
U156	4.57	6.09	0.58	0.34
U156	6.09	6.85	1.96	0.72
U156	8.47	10.09	4.16	1.14
U156	10.09	12.19	7.28	5.5
U156	12.19	15.24	8.78	0.38
U156	15.24	15.84	0.2	0.12
U156	15.84	17.89	3.08	0.32
U156	18.28	21.33	13.1	0.04
U156	21.33	22.86	4.96	0.4
U156	22.86	24.38	0.04	0.04
U156	24.38	32	0.66	0.66
U157	0	1.24	1.44	0.02
U157	1.24	3.04	2.64	0.01
U157	3.04	4.57	5.62	0.01
U157	4.57	6.09	7.46	0.04
U157	6.09	9.14	2.4	0.01
U157	9.14	12.64	1.32	0.08
U157	13.71	15.24	0.62	0.36
U157	15.24	18.1	0.98	0.14
U157	19.35	19.96	2.76	0.12
U159	12.19	15.24	1.52	0.64
U159	15.24	18.29	2.26	0.02
U160	0	3.04	1.14	0.08
U160	3.04	5.18	0.46	0.06
U160	5.18	5.94	2.18	0.3
U160	5.94	8.62	3.92	0.08
U160	8.62	9.27	4.04	0.64
U160	9.27	12.19	4.84	1.36
U160	12.19	15.24	5.16	0.36
U160	15.24	16.76	5.08	0.02
U160	16.76	18.29	2.94	0.02
U161	0	3.04	2.14	0.48
U161	3.04	6.09	0.96	1.28
U161	6.09	9.14	0.82	0.44
U161	9.14	12.19	0.7	0.3
U161	12.19	17.37	0.96	0.92
U161	17.37	17.68	4.3	1.1
U162	0	0.73	1.23	0.04
U162	0.73	1.52	0.36	0.02
U162	1.52	3.04	0.58	0.01
U162	3.04	6.09	0.4	0.01
U162	6.09	8.3	3.24	0.01
U162	9.14	10.66	0.95	0.02
U162	10.66	12.19	0.82	0.02
U162	12.19	13.71	0.73	0.01
U162	13.71	15.24	0.5	0.04
U162	15.24	17.68	0.4	0.04
U163	0	2.74	48	0.12
U163	3.05	4.26	62.1	2.6
U163	4.26	6.09	18.9	63.3
U163	6.09	11.58	24.7	0.44
U163	11.58	14.02	26.4	23
U164	0	3.1	0.08	0.04
U164	3.1	4.45	0.02	0.16
U164	5.33	8.38	0.12	0.02
U164	8.38	11.43	0.18	0.01
U164	11.43	14.47	0.16	0.02
U164	14.47	17.52	0.04	0.02

U164	17.52	18.89	0.32	0.12
U164	18.89	23.77	0.64	0.02
U165	0	3.04	0.04	0.04
U165	3.04	6.09	0.48	0.46
U165	6.09	9.14	0.02	0.04
U166	0	0.79	1.23	0.12
U166	0.79	3.04	2.52	0.14
U166	3.04	6.09	2.14	0.07
U166	6.09	9.14	4.36	0.06
U166	9.14	10.66	5.42	0.04
U166	10.66	12.19	12.8	0.04
U166	12.19	13.25	30.8	27.1
U166	13.25	13.41	18.4	3.55
U166	13.41	14.17	2.92	0.39
U167	0	2.71	0.6	0.32
U167	2.71	3.16	1.38	0.64
U167	3.16	7.1	0.08	0.06
U167	7.1	8.07	0.36	0.04
U167	8.07	11.12	0.36	0.02
U167	11.12	12.31	0.12	0.2
U167	12.31	13.01	0.4	0.02
U167	13.01	14.53	0.22	0.02
U167	14.53	17.58	0.02	0.02
U167	17.58	21.33	0.04	0.04
U167	21.33	24.38	0.02	0.02
U167	24.38	25.14	0.04	0.02
U167	25.9	29.32	0.04	0.02
U168	0	1.52	0.04	0.68
U168	1.52	3.04	0.08	1.26
U168	3.04	6.09	0.08	1.24
U168	6.09	7.62	0.1	0.6
U168	7.62	9.14	0.46	0.24
U168	9.14	12.19	1.08	1.62
U168	12.19	15.24	0.24	0.1
U168	15.24	18.28	0.22	0.02
U168	18.28	21.33	0.22	0.1
U168	21.33	24.38	0.44	0.02
U168	24.38	26.21	0.3	0.01
U168	26.21	28.95	0.18	0.01
U168	28.95	32	0.16	0.01
U169	0	1.52	0.86	3.22
U169	1.52	3.04	1.2	0.12
U169	3.04	4.11	0.62	0.12
U169	4.57	6.09	0.3	0.08
U169	6.09	7.62	0.08	0.04
U169	7.62	9.14	0.08	0.02
U169	9.14	12.19	0.18	0.04
U169	12.19	15.24	0.44	0.06
U169	15.24	18.28	0.6	0.02
U169	18.28	21.33	0.44	0.02
U169	21.33	22.86	0.72	0.02
U169	22.86	24.38	0.64	0.02
U169	25.15	25.9	1.02	0.02
U169	25.9	28.9	3.64	0.02
U169	28.9	31.02	4.24	0.02
U169	31.02	33.52	6.52	0.02
U169	33.52	36.57	7.04	0.02
U169	36.57	39.16	4.78	0.02
U169	39.16	39.92	3.22	0.02
U169	39.92	41.45	1.08	0.02
U170	0	1.52	3.68	5.08
U170	1.52	3.04	0.54	0.86
U170	3.04	4.57	1.54	8.04
U170	4.57	6.09	2.64	6.78
U171	0	1.52	1.08	2.06
U171	1.52	3.04	1.74	2.5
U171	3.04	4.57	1.2	1.68
U171	4.57	6.09	0.6	0.06
U171	6.09	7.62	0.72	0.04
U171	7.62	8.59	0.2	0.1
U171	8.59	9.14	1.74	8
U171	9.14	10.12	1.94	0.18
U172	0	1.52	2.06	4.6
U172	1.52	3.04	1.26	4.68
U172	3.04	4.57	0.54	2.24
U172	4.57	6.09	2.88	8.16
U172	6.09	7.16	2.84	7.64
U173	0	1.52	0.68	0.12
U173	1.52	3.04	0.56	0.68
U173	3.04	4.57	1.58	1.02
U173	4.57	6.09	2.08	0.2

U173	6.09	7.62	0.98	0.1
U173	7.62	9.14	1.72	0.12
U173	9.14	10.66	1.32	1.54
U173	10.66	12.19	2.18	2.64
U173	12.19	14.17	1.42	2.16
U173	14.17	15.24	1.16	0.34
U173	15.69	17.22	1.72	0.6
U173	17.76	18.74	0.54	0.18
U173	18.74	21.34	0.88	0.68
U174	0	1.52	0.26	0.1
U174	1.52	2.31	1.32	1.1
U174	2.31	4.57	3.16	0.88
U174	4.57	7.62	2.88	0.02
U174	7.62	10.66	2.08	0.02
U174	10.66	12.19	0.4	0.02
U174	12.19	13.32	8.52	5.92
U174	13.32	14.48	16.4	42.8
U175	0	3.04	0.18	0.04
U175	3.04	6.09	0.34	0.02
U175	6.09	9.14	0.06	0.04
U175	9.14	12.19	0.04	0.02
U175	12.19	15.24	0.12	0.01
U175	15.24	18.28	0.1	0.01
U175	18.28	21.33	0.44	0.02
U175	21.33	22.86	1.12	0.04
U175	22.86	24.38	2.24	0.02
U175	24.38	26.52	0.96	0.02
U176	0	1.52	0.32	0.6
U176	1.52	3.04	0.2	1.3
U176	3.04	4.57	0.28	0.42
U176	4.57	6.09	1.16	0.42
U176	6.09	7.62	1.2	0.06
U176	7.62	9.14	1.68	0.02
U176	9.14	10.66	2.28	0.06
U176	10.66	12.19	4.28	0.58
U176	12.19	13.71	2.87	0.42
U176	13.71	15.24	2.24	0.06
U176	15.24	16.76	4.32	0.06
U176	16.76	18.28	4.06	0.02
U176	18.28	19.81	4.78	0.02
U176	19.81	21.33	2.48	0.04
U176	21.33	21.64	0.76	0.06
U176	21.64	22.86	8.88	0.1
U176	22.86	24.38	10.9	0.02
U176	24.38	25.9	8.98	0.01
U176	25.9	26.37	5.46	0.02
U176	26.37	28.65	48.7	0.04
U176	28.65	29.93	51.7	0.08
U177	1.25	2.68	1.5	0.46
U177	2.68	3.68	0.13	1.04
U177	3.68	4.57	0.04	0.18
U177	4.57	6.09	0.07	0.09
U177	6.09	7.62	0.02	0.02
U177	7.62	9.14	0.02	0.02
U177	9.14	10.66	0.13	0.16
U177	10.66	12.19	0.44	0.06
U177	12.19	13.71	0.02	0.02
U177	13.71	15.24	1.74	0.02
U177	15.24	16.76	1.86	0.02
U177	16.76	18.28	0.04	0.02
U177	18.28	19.81	0.06	0.16
U177	19.81	21.33	0.26	0.52
U177	21.33	22.86	2.57	0.64
U177	22.86	24.38	1.86	3.04
U177	24.38	25.9	0.58	1.3
U177	25.9	27.43	1.36	0.98
U177	27.43	28.95	3.02	2.12
U177	28.95	30.48	2.3	1.66
U177	30.48	32	0.8	0.68
U177	32	33.52	1.74	3.86
U177	33.52	35.05	0.92	2.62
U177	35.05	36.57	2.36	5.76
U177	36.57	38.1	4.64	1.76
U177	38.1	39.14	1.76	1.06
U178	0	2.37	0.48	0.04
U178	2.37	3.04	0.52	0.01
U178	3.04	6.09	1.38	0.36
U178	6.09	9.14	0.96	0.3
U178	9.14	12.19	3.6	0.02
U178	12.19	15.24	3.18	0.1
U179	6.09	7.62	0.12	0.01

U179	7.62	9.14	0.68	0.01
U179	9.14	10.66	1.98	0.01
U179	10.66	12.19	1.74	0.01
U179	12.19	13.71	1.92	0.02
U179	13.71	15.24	1.1	0.04
U179	15.24	16.76	1.42	0.54
U179	16.76	18.28	1.44	0.42
U179	18.28	19.81	1.48	0.58
U179	19.81	21.33	1.4	0.68
U179	21.33	22.86	0.76	0.16
U179	22.86	24.38	0.22	0.26
U179	24.38	25.9	0.18	0.42
U179	25.9	27.43	0.84	0.32
U179	27.43	28.95	1	0.08
U179	28.95	30.48	1.26	0.2
U179	30.48	32	2.76	0.06
U179	32	33.52	2.86	0.06
U179	33.52	35.05	1.76	0.12
U179	35.05	36.57	1.86	0.1
U179	36.57	38.4	1.44	0.06
U180	0	1.52	1.46	0.02
U180	1.52	3.04	0.52	0.02
U180	3.04	4.57	0.78	0.02
U180	4.57	6.09	1.18	0.02
U180	6.09	7.62	0.74	0.02
U180	7.62	9.14	0.22	0.04
U180	9.14	10.66	0.23	0.24
U180	10.66	12.19	0.48	0.53
U180	12.19	13.71	0.26	0.22
U180	13.71	15.24	0.38	0.32
U180	15.24	16.76	0.76	0.56
U180	16.76	18.28	0.48	0.28
U180	18.28	19.81	0.44	0.24
U180	19.81	21.33	0.16	0.06
U180	21.33	22.86	0.3	0.22
U180	22.86	24.38	0.58	0.54
U180	24.38	25.59	2.76	0.78
U180	25.59	27.43	5.28	0.22
U180	27.43	28.95	4.88	0.14
U180	28.95	29.56	4.74	0.5
U181	0	1.52	0.58	0.02
U181	1.52	3.62	0.94	0.02
U181	3.62	5.79	0.82	0.02
U181	5.79	7.31	1.34	0.1
U181	7.31	8.38	1.84	0.6
U181	8.38	9.9	0.2	0.06
U181	9.9	10.82	0.44	0.08
U181	10.82	11.88	0.54	0.06
U181	11.88	13.28	1.22	0.08
U181	13.28	14.78	0.78	0.16
U181	14.78	16.15	0.58	0.02
U181	16.15	17.67	0.26	0.04
U181	17.67	19.2	1.82	0.02
U181	19.2	20.72	2.06	0.06
U181	20.72	21.94	3.28	0.28
U181	21.94	22.86	1.64	0.04
U182	1.52	3.05	0.84	0.1
U182	10.82	12.34	0.27	0.02
U182	12.34	13.41	0.1	0.18
U182	13.41	14.93	0.04	0.02
U183	4.08	7.28	0.02	0.02
U183	7.28	9.14	0.02	0.02
U183	9.14	9.99	0.02	0.02
U183	9.99	11.97	0.22	0.02
U183	11.97	13.71	0.3	0.02
U183	13.71	16.76	0.14	0.02
U183	16.76	20.23	0.18	0.02
U183	20.23	20.54	0.14	0.1
U183	20.54	21.21	2.18	0.02
U183	21.21	22.03	0.36	0.02
U183	22.03	24.38	0.74	0.02
U183	24.38	25.9	0.48	0.02
U183	25.9	28.8	0.32	0.02
U183	28.8	30.32	1.78	0.02
U183	30.32	32	0.32	0.04
U184	0	2.13	3.16	0.94
U184	2.13	3.81	0.8	0.22
U184	3.81	5.51	0.34	0.34
U184	5.51	7.55	0.24	1.6
U184	7.55	9.14	0.46	1.45
U184	9.14	10.94	0.14	0.28

U184	10.94	13.41	0.26	0.34
U184	13.41	17.06	0.06	0.14
U185	0	1.52	0.2	0.1
U185	1.52	3.04	0.14	0.02
U185	3.04	4.57	0.2	0.06
U185	4.57	6.09	0.38	0.52
U185	6.09	7.62	1	1.64
U185	7.62	9.14	1.08	1.82
U185	9.14	10.66	0.16	1
U185	10.66	12.19	0.4	0.28
U185	12.19	13.71	0.26	0.14
U185	13.71	15.24	1.72	0.62
U185	15.24	16.76	0.94	0.42
U185	16.76	18.28	2.96	0.02
U185	18.28	19.81	0.66	0.42
U185	19.81	21.64	0.3	0.02
U186	0	1.52	1.26	0.08
U186	1.52	3.04	1.06	0.06
U186	3.04	4.57	0.18	0.08
U186	4.57	6.09	0.22	0.18
U186	6.09	7.62	0.36	0.06
U186	7.62	9.14	1.18	0.16
U186	9.14	11.58	0.94	0.06
U186	11.58	13.31	5.4	0.86
U186	13.31	13.99	1.54	1.34
U186	13.99	15.51	0.92	0.92
U186	15.51	17.83	1.48	1.02
U186	17.83	19.35	0.94	0.48
U186	19.35	20.87	1.44	0.44
U186	20.87	22.4	2.06	0.1
U186	22.4	23.92	2.02	0.6
U186	23.92	25.29	1.88	0.08
U186	25.29	27.27	0.94	0.02
U186	27.27	28.34	0.54	0.08
U186	28.34	29.87	0.32	0.14
U186	29.87	31.39	1.76	0.02
U186	31.39	32.91	1.18	0.2
U186	32.91	34.01	0.66	0.34
U186	34.01	36.45	2.36	0.44
U186	36.45	38.49	0.68	0.4
U186	38.49	39.92	0.26	0.22
U186	39.92	41.45	0.18	0.48
U186	41.45	43.59	0.68	0.24
U187	0	1.18	0.2	0.38
U187	1.18	3.04	0.92	0.02
U187	3.04	4.57	1.76	0.02
U187	4.57	5.48	1.88	0.02
U187	5.48	7.62	0.48	0.24
U187	7.62	9.14	0.94	0.2
U187	9.14	10.24	1.94	0.04
U187	10.24	12.03	1.3	0.16
U187	12.03	12.95	3.06	0.84
U187	12.95	14.17	0.66	0.34
U187	14.17	16.39	0.68	0.9
U187	17.92	19.35	0.86	0.16
U187	19.35	20.9	2.36	0.14
U187	20.9	22.43	1.16	0.28
U187	22.43	23.95	1.22	0.16
U187	23.95	25.48	0.32	0.12
U187	25.48	26.6	0.12	0.18
U187	26.6	28.55	0.56	0.38
U187	31.94	33.52	0.04	0.12
U187	33.52	35.35	0.02	0.12
U188	0	1.52	2.44	0.02
U188	1.52	3.04	2.04	0.06
U188	3.04	4.57	0.78	0.06
U188	4.57	6.09	0.74	1.39
U188	6.09	7.62	1.06	0.1
U188	7.62	9.14	0.06	0.02
U188	9.14	10.66	0.69	0.04
U188	10.66	12.49	0.68	0.06
U188	12.49	13.71	1.1	0.04
U188	13.71	15.24	0.64	0.14
U188	15.24	16.76	0.52	0.12
U188	16.76	18.59	1.48	0.02
U188	18.59	20.11	1.26	0.38
U188	20.11	20.93	2.48	1.82
U188	20.93	21.94	1.3	0.44
U188	21.94	25.9	0.84	0.08
U189	0	1.52	0.44	0.08
U189	1.52	3.04	3.52	0.06

U189	3.04	4.57	1.12	0.02
U189	4.57	5.24	1.02	0.04
U189	5.24	6.4	0.62	0.04
U189	6.4	9.14	0.78	0.04
U189	9.14	12.19	0.54	0.04
U189	12.19	14.93	0.68	0.3
U189	14.93	16.3	0.2	0.28
U189	16.3	18.89	1.28	3.28
U189	18.89	20.42	4.06	1
U189	20.42	21.94	4.36	0.56
U189	21.94	23.46	2.84	0.66
U189	23.46	24.99	2.48	0.9
U189	24.99	27.76	4.18	1.04
U189	27.76	28.46	1.94	0.16
U189	28.46	29.01	5.14	0.02
U189	29.01	29.26	1.46	0.12
U189	29.26	30.57	2.64	0.16
U189	33.52	34.68	2.42	0.08
U189	34.68	36.6	18.4	0.15
U189	36.6	37.94	4.4	0.06
U189	37.94	39.62	0.26	0.1
U189	39.62	41.3	6.4	0.22
U189	41.3	43.43	0.5	0.05
U189	43.43	44.98	2.05	0.4
U189	44.98	46.51	4.2	0.4
U189	46.51	48.03	4.2	0.1
U189	48.03	49.56	3.6	0.04
U189	49.56	50.9	3.6	0.62
U189	50.9	52.42	2.54	0.14
U189	52.42	53.95	1.95	0.22
U189	53.95	55.47	2.9	0.28
U189	55.47	57	1.59	0.17
U189	57	58.52	17.8	1.5
U189	58.52	60.04	14.4	3.28
U189	60.04	61.56	2.96	0.92
U189	61.56	63.09	3.6	0.18
U190	0	3.04	0.72	0.06
U190	3.04	6.09	0.4	0.02
U190	6.09	9.14	0.32	0.02
U190	9.14	12.19	0.24	0.02
U190	12.19	15.24	0.48	0.04
U190	15.24	18.28	0.5	0.14
U190	18.28	22.09	1.14	0.16
U190	22.09	23.31	0.48	0.06
U190	23.31	28.95	0.76	0.36
U190	28.95	32.3	0.38	0.24
U191	9.44	12.19	1.22	0.02
U191	12.19	15.24	0.92	0.02
U191	15.24	17.67	1.62	0.06
U191	17.67	19.5	0.62	0.02
U191	19.5	20.72	0.44	0.08
U191	20.72	22.12	0.82	0.18
U191	22.12	23.95	1.68	0.44
U191	23.95	26.51	0.18	0.48
U191	26.51	29.56	0.98	0.1
U191	29.56	32.61	1.28	0.14
U191	32.61	34.74	3.98	0.22
U191	34.74	36.27	3.24	0.2
U191	36.27	38.4	1.96	0.06
U191	38.4	39.93	4.62	0.14
U192	4.87	7.31	0.36	0.06
U192	7.31	10.36	0.96	0.06
U192	10.36	13.1	0.28	0.02
U193	0	1.52	0.3	0.3
U193	1.52	3.04	0.1	0.06
U193	3.04	4.57	0.12	0.22
U193	4.57	6.09	0.14	0.02
U193	6.09	7.62	0.04	0.02
U193	7.62	8.83	0.02	0.02
U193	8.83	10.36	0.06	0.06
U193	10.36	11.88	0.02	0.03
U193	11.88	13.41	0.14	0.1
U193	13.41	14.93	0.02	0.02
U193	14.93	16.76	0.04	0.04
U193	16.76	18.28	0.06	0.05
U193	18.28	19.2	0.14	0.02
U194	13.1	14.14	0.06	0.18
U194	14.14	15.63	1.57	3.42
U194	15.63	16.3	16.2	8.58
U195	11.27	13.71	0.52	0.66
U195	13.71	15.24	0.06	0.04

U195	15.24	16	0.02	0.06
U195	16	18.29	2.78	0.08
U195	18.29	20.06	6.06	1.96
U195	20.06	20.72	41.6	16.2
U195	20.72	21.03	0.27	0.31
U196	26.6	27.43	1.38	0.2
U196	27.43	29.32	4.9	0.12
U196	29.32	30.24	49.6	4.54
U197	0	2.59	0.26	0.12
U197	2.86	5.48	0.24	0.36
U197	5.48	8.53	1.72	0.36
U197	8.83	12.8	0.88	0.14
U197	14.78	15.84	0.14	0.02
U198	0	0.6	0.34	0.94
U198	1	4.14	0.74	1.32
U198	4.14	7.31	1.64	0.8
U198	7.31	9.14	0.76	0.36
U199	0	3.04	0.9	0
U199	3.04	6.09	0.86	0.1
U199	6.09	9.14	0.3	0
U199	9.14	12.19	0.46	0.46
U199	12.19	13.1	1.04	0.3
U199	13.1	14.63	0.24	0.96
U199	14.63	16.3	2.08	1.02
U199	16.3	20.11	1.78	0.16
U199	20.11	21.33	0.46	0
U199	21.33	24.38	0.6	0
U199	24.38	27.43	0.25	0.14
U199	27.43	31.4	0.68	0
U200	0	2.43	0.06	0.02
U200	2.43	4.72	0.48	0.01
U200	4.72	6.4	0.48	0.01
U200	6.4	9.14	1.54	0.01
U200	9.14	12.19	0.6	0.04
U200	12.19	15.24	0.1	0.08
U200	15.24	17.92	0.48	0.01
U200	17.92	19.87	0.66	0.01
U200	19.87	21.64	0.3	0.08
U200	21.64	24.38	0.46	0.2
U200	24.38	25.9	0.26	0.2
U200	25.9	27.43	0.8	0.01
U200	27.43	30.48	0.98	0.12
U200	30.48	32	0.44	0.02
U200	32	33.68	0.2	0.02
U200	33.68	37.18	0.88	0.08
U200	37.18	39.01	0.48	0.02
U200	39.01	40.84	0.36	0.02
U200	40.84	44.5	1.02	0.76
U201	0	0.85	0.16	0.04
U201	0.85	2.49	0.62	0.12
U201	2.49	4.63	0.03	0.01
U201	4.63	6.09	0.22	0.38
U201	6.09	7.77	0.02	0.01
U201	7.77	10.66	0.06	0.01
U201	10.66	13.71	0.02	0.01
U201	13.71	16.76	0.08	0.01
U201	16.76	18.28	0.06	0.01
U201	18.28	20.11	0.04	0.02
U201	20.11	22.15	0.02	0.01
U201	22.15	23.22	0.06	0.1
U201	23.22	24.38	0.02	0.06
U201	24.38	27.43	0.02	0.02
U201	27.43	30.48	0.04	0.04
U201	39.19	42.55	0.84	0.05
U201	42.55	44.19	0.92	0.06
U201	44.19	47.24	0.16	0.06
U204	0	1.37	0	0
U204	1.37	2.89	0	0
U204	2.99	3.65	0	0
U204	3.65	6.55	0	0
U204	6.55	7.77	0	0
U205	0	3.04	0.17	0.1
U205	3.04	5.79	0.38	0.03
U205	5.79	8.83	0.28	0.02
U205	8.83	11.88	0.37	0.01
U205	11.88	14.93	0.14	0.01
U205	14.93	17.06	0.4	0.27
U205	17.06	18.59	0.44	0.8
U205	18.59	21.64	0.6	0.1
U205	21.64	22.86	0.51	0.49
U205	22.86	24.69	0.71	1.12

U206	0	3.35	0.56	0.34
U206	3.35	5.94	1.48	0.62
U206	5.94	8.07	2.54	2.32
U206	8.07	11.12	1.56	6.28
U206	11.12	12.64	2.92	7.86
U206	12.64	14.41	1.34	1.72
U206	14.41	16.46	1.94	3.88
U206	16.46	18.71	3.1	1.74
U206	18.71	21.64	3.86	3.76
U206	21.64	24.68	3.72	4.94
U206	24.68	26.35	2.64	3.62
U206	26.35	28.95	2.22	9.14
U206	28.95	29.71	1.36	4.2
U206	29.71	33.22	2.44	7.44
U206	33.22	36.27	3.02	2.76
U206	36.27	37.79	1.96	1.36
U209	0	3.04	0.18	0.06
U209	3.04	6.09	0.79	0.2
U209	6.09	9.14	0.4	0.04
U209	9.14	12.19	0.24	0.01
U209	12.19	15.24	0.06	0.01
U209	15.24	18.28	0.12	0.01
U209	18.28	21.33	0.03	0.02
U209	21.33	23.16	0.06	0.38
U210	0	1.52	0.78	0.24
U210	1.52	3.04	0.26	0.34
U210	3.04	5.02	0.29	0.88
U210	5.02	5.48	0.01	0.03
U210	5.48	6.7	0.02	0.16
U210	6.7	8.22	0.13	0.12
U210	8.22	9.44	0.01	0.01
U210	9.44	10.36	0.74	0.24
U210	10.36	10.66	0.03	0.02
U210	10.66	11.58	1.52	0.01
U210	11.58	12.61	0.08	0.08
U210	12.61	12.92	0.01	0.07
U210	12.92	13.41	0.02	0.82
U210	13.41	15.24	0.42	0.92
U210	15.24	17.06	0.08	0.09
U210	17.06	17.28	0.18	0.03
U210	17.28	20.11	0.26	0.01
U210	20.11	23.47	0.34	0.07
U211	0	1.7	0.56	0.1
U211	1.7	2.89	0.26	0.56
U211	2.89	5.97	0.43	1
U211	5.97	8.83	0.14	0.69
U211	8.83	11.76	0.23	0.74
U211	11.76	14.59	0.49	0.5
U211	14.59	15.66	0.16	0.04
U211	15.66	16.76	0.05	0.02
U211	16.76	19.11	0.58	0.55
U211	19.11	22.34	0.16	0.27
U211	22.34	25.35	0.29	0.48
U211	25.35	28.34	0.46	0.18
U211	28.34	31.69	0.78	0.13
U211	31.69	33.83	0.28	0.08
U211	33.83	36.57	0.33	0.06
U211	36.57	38.1	0.16	0.2
U211	38.1	40.23	0.1	0.1
U211	40.23	42.67	0.21	0.26
U212	0	2.13	1.14	0.01
U212	2.13	5.18	1.6	0.01
U212	5.18	6.24	1.56	0.01
U212	6.24	8.53	2.02	0.09
U212	8.53	11.58	2.16	0.06
U212	11.58	14.02	2.2	0.08
U212	14.02	17.37	2.78	0.05
U212	17.37	20.42	0.96	0.1
U212	20.42	21.94	1.4	0.4
U212	21.94	22.34	1.38	0.28
U212	22.34	22.73	1.62	0.05
U212	22.73	23.13	2.14	0.03
U212	23.13	23.46	6.24	2.22
U212	23.46	27.43	3.68	1.54
U213	0	1.52	1.04	0.02
U213	1.52	1.82	6.04	0.02
U213	1.82	3.35	1.08	0
U213	3.35	5.18	2.26	0.34
U213	5.18	8.22	1.44	0.3
U213	8.22	10.82	1.22	0.08
U213	10.82	10.97	4.2	8.54

U213	10.97	11.97	2.54	0.02
U213	11.97	12.8	0.24	0.04
U213	12.8	14.32	3.7	0.1
U213	14.32	15.24	2.6	0.02
U213	15.24	16.45	0.86	0.01
U213	16.45	17.06	5.74	1.1
U213	17.06	18.59	0.54	0.01
U213	18.59	21.03	0.68	0.02
U213	21.03	22.55	1.64	0.04
U213	22.55	24.07	2.46	0.12
U213	24.07	24.99	4.08	0.42
U213	24.99	27.73	1.68	0.76
U214	0	2.43	0.22	0.02
U214	2.43	5.79	0.48	0.08
U214	5.79	8.22	0.17	0.16
U214	8.22	9.75	0.34	0.2
U214	9.75	12.49	0.2	0.06
U214	12.49	15.24	0.01	0.01
U215	0	1.12	0.64	0.02
U215	1.12	1.52	0.56	0.01
U215	1.52	2.59	0.92	0.01
U215	2.59	3.04	0.1	0.08
U215	3.04	4.81	0.38	0.01
U215	4.81	5.42	1.16	0.01
U215	5.42	7.62	0.22	0.01
U215	7.62	9.14	0.36	0.01
U215	9.14	10.66	0.3	0.01
U215	10.66	12.19	0.26	0.01
U215	12.19	13.71	0.18	0.01
U215	13.71	15.24	0.34	0.01
U215	15.24	16.67	0.28	0.08
U215	16.67	16.96	0.86	0.16
U215	16.97	18.59	1.02	0.12
U215	18.59	20.51	0.94	0.28
U215	20.51	23.4	0.62	0.16
U215	23.4	24.38	3.22	0.9
U215	24.38	26.3	2.98	0.82
U215	26.3	26.91	6.3	1.84
U215	26.91	27.52	8.63	0.04
U216	0	1.06	0.18	0.42
U216	1.06	2.74	1.64	0.1
U216	2.74	5.79	0.56	0.02
U216	5.79	8.83	0.68	0.01
U216	8.83	10.36	1.12	0.01
U216	10.36	13.61	1.82	0.38
U216	13.61	13.71	6.4	23
U216	13.71	17.06	4.14	0.26
U216	17.06	18.28	5.06	0.7
U216	18.28	18.59	2.68	1.92
U216	18.59	21.12	1.78	0.04
U216	21.12	22.79	0	0
U216	22.79	23.46	16.7	3.3
U216	23.46	23.89	3.88	1.76
U216	23.89	24.68	8.45	54.3
U216	24.68	26.51	4.24	5.54
U217	0	1.98	0.07	0.08
U217	1.98	3.38	0.12	0.03
U217	3.38	4.96	0.22	0.17
U217	4.96	5.79	0.03	0.02
U217	5.79	7.01	0.82	0.39
U217	7.01	9.75	0.56	0.11
U217	9.75	11.88	1.75	0.12
U217	11.88	14.23	0.4	0.02
U217	14.23	15.75	0.58	0.03
U217	15.75	17.16	0.66	0.06
U217	17.16	18.68	0.56	0.14
U217	18.68	20.02	0.57	0.63
U217	20.02	21.85	1.87	0.77
U217	21.85	23.37	1.16	0.02
U217	23.37	24.81	1.96	0.02
U217	24.81	26.33	7.42	0.96
U217	26.33	27.85	4.96	4.48
U217	27.85	29.38	2.44	1.94
U217	29.38	30.69	2.96	0.8
U217	30.69	32.06	2.66	0.35
U217	32.06	33.64	3.36	1.7
U217	33.64	35.11	4.56	0.47
U217	35.11	36.63	2.34	1.21
U217	36.63	37.85	0.98	0.24
U217	37.85	39.34	1.24	1.72
U217	39.34	41.08	1.03	0.06

U217	41.08	41.84	1.76	0.18
U217	41.84	45.11	0.01	0.01
U218	0	1.82	0.29	0.2
U218	1.82	3.35	0.03	0.07
U218	3.35	5.18	0.3	0.06
U218	12.49	13.38	0.28	0.12
U218	13.38	14.93	11.4	0.12
U218	14.93	16.45	2.2	0.03
U218	16.45	17.37	4.72	0.12
U218	17.37	20.42	4.68	0.76
U218	20.42	20.97	8.9	1.68
U218	20.97	21.94	6.38	1.34
U218	21.94	24.08	3.82	2.6
U218	24.08	24.37	2.38	13.2
U218	24.38	25.29	5.12	1.64
U218	25.29	26.82	0.92	0.03
U218	26.82	27.43	0.78	0.07
U218	27.43	29.26	2.24	0.43
U218	29.26	31.08	1.94	0.01
U218	31.08	34.13	1.96	0.01
U218	34.13	35.66	0.72	0.09
U218	35.66	39.01	0.18	0.14
U220	2.43	3.81	1.58	0.6
U220	3.81	6.09	2.28	0.56
U220	6.09	9.75	6.56	0.2
U221	1.76	3.65	6.2	0.48
U222	7.49	10.36	1.72	0.28
U222	10.36	11.58	3.2	0.8
U222	11.58	12.19	0.12	11.2
U222	12.19	13.71	1.52	1.04
U222	13.71	16.45	4.62	0.27
U222	16.45	16.77	6.34	0.34
U223	5.18	7.31	2.09	0.31
U223	7.31	10.05	2.74	1.86
U223	10.05	11.94	6.76	5.78
U223	11.94	13.87	1.92	3.42
U224	2.74	3.35	0.88	4.74
U224	3.35	5.18	2.42	3.92
U224	5.18	6.4	21.9	43.6
U225	0	1.09	2.36	0.2
U225	1.09	2.74	0.74	0.36
U225	2.74	6.09	0.94	0.03
U225	6.09	8.53	0.98	0.82
U225	8.53	11.43	2.02	0.46
U225	11.43	13.04	1.56	0.32
U225	13.04	15.08	2.32	5.06
U225	15.08	17.37	0.98	1
U225	17.37	20.27	3.06	3.62
U225	20.27	22.86	2.36	0.34
U225	22.86	24.68	4.85	2.12
U225	24.68	27.12	4.34	1.48
U225	27.12	30.17	6.62	4.4
U225	30.17	33.22	7.48	2.14
U225	33.22	34.75	14.7	1.9
U225	34.75	35.05	32.7	32.9
U226	0	3.04	0.74	0.14
U226	3.04	6.09	3.9	2.42
U226	6.09	8.71	1.04	0.56
U226	8.71	10.24	0.3	0.09
U226	10.24	11.21	2.28	0.88
U226	11.21	13.86	2.82	1.66
U226	13.86	16.61	2.04	0.58
U226	16.61	18.44	0.76	0.12
U226	18.44	21.33	0.94	0.68
U226	21.33	21.64	6.15	11.5
U226	21.64	22.56	0.56	0.4
U227	0	1.52	1.18	0.21
U227	1.52	3.04	1.18	0.05
U227	3.04	4.57	1.44	0.15
U227	4.57	6.09	0.83	0.11
U227	6.09	7.92	0.46	0.1
U227	7.92	8.83	4.86	0.01
U227	8.83	10.66	1.28	0.02
U227	10.66	13.56	1.12	0.04
U227	13.56	15.24	1.7	0.02
U227	15.24	17.37	0.68	0.02
U227	17.37	18.89	1.34	0.01
U227	18.89	21.33	0.68	0.01
U227	21.33	22.86	1.02	0.05
U227	22.86	24.14	0.48	0.01
U227	24.14	25.42	2.06	0.01

U227	25.42	27.12	2.42	0.09
U227	27.12	27.82	2.68	0.01
U227	27.82	29.26	2.1	1.42
U227	29.26	31.09	0.78	0.84
U228	0	4.57	1.16	1.38
U228	4.57	5.79	2.86	0.46
U228	5.79	7.01	5.34	0.02
U228	7.01	9.14	0.17	0.1
U228	9.14	13.41	0.58	0.14
U228	13.41	15.24	1.18	0.5
U228	15.24	17.89	11.3	4.9
U228	17.89	18.89	6.68	1.04
U228	18.89	19.35	56.2	5.18
U228	19.35	20.11	3.04	0.1
U229	0	3.04	2.54	1.64
U229	3.04	6.09	3.38	0.98
U229	6.09	9.14	4.88	0.18
U229	9.14	9.75	9.96	0.1
U229	9.75	11.58	40.8	17
U229	11.58	16.46	0.21	0
U230	0	3.04	3.28	3.12
U230	3.04	5.18	4.44	1.62
U230	5.18	5.48	31.9	26.7
U230	5.48	9.14	0.06	0.08
U230	9.14	10.97	0.01	0.01
U231	0	3.04	2.32	0.25
U231	3.04	6.09	0.76	0.12
U231	6.09	7.13	8.85	1.18
U231	7.13	7.68	37.4	12.8
U231	7.68	7.92	1.75	1
U232	0	3.04	2.88	4.14
U232	3.04	6.09	1.8	1.01
U232	6.09	9.14	7.2	0.86
U232	9.14	12.19	4.16	0.09
U232	12.19	15.24	6.8	0.31
U232	15.24	16.67	6.7	0.31
U232	16.67	17.06	18.1	56.8
U233	0	3.04	0.68	0.05
U233	3.04	6.09	0.74	0.04
U233	6.09	8.83	0.8	0.03
U233	8.83	11.27	1.22	0.42
U233	11.27	13.41	0.42	0.21
U234	0	3.04	0.36	0.02
U234	3.04	6.09	0.3	0.02
U234	6.09	7.16	0.27	0.14
U234	7.16	8.47	0.64	0.3
U234	8.47	8.83	2.7	0.17
U234	8.83	12.8	4.26	0.49
U234	12.8	15.84	0.95	0.82
U235	0	3.04	0.25	0.19
U235	3.04	6.09	0.2	0.12
U235	6.09	10.36	0.11	0.06
U235	10.36	13.41	0.07	0.12
U235	13.41	16.45	0.12	0.02
U235	16.45	20.42	0.19	0.02
U235	20.42	22.86	2.08	0.01
U236	0	3.04	0.34	0.13
U236	3.04	6.09	0.64	0.2
U236	6.09	7.92	0.82	0.18
U236	7.92	10.97	0.06	0.07
U236	10.97	13.41	0.42	0.34
U236	13.41	16.15	0.9	0.58
U236	16.15	19.2	1.98	0.18
U236	19.2	19.81	2.38	0.05
U236	19.81	20.42	2.13	0.07
U236	20.42	26.51	2.04	0.08
U236	26.51	27.58	1.66	0.52
U237	0	2.43	0.38	0.1
U237	2.43	4.57	0.84	0.2
U237	4.57	6.7	1.72	0.01
U237	6.7	7.77	0.78	0.01
U237	7.77	8.84	0.03	0.03
U238	0	3.04	3.26	3.32
U238	3.04	6.09	3.52	3.8
U238	6.09	7.77	10.3	5.96
U238	7.77	7.92	21.5	25.9
U239	0	3.04	0.47	0.05
U239	3.04	6.09	0.84	0.13
U239	6.09	9.14	0.86	0.05
U239	9.14	12.19	0.47	0.03
U239	12.19	15.24	1.36	0.18
U239	15.24	18.28	0.41	0.11
U239	18.28	21.33	0.22	0.27
U239	21.33	24.38	0.2	0.07
U239	24.38	27.43	0.2	0.2
U239	27.43	30.48	0.56	1.74
U239	30.48	33.52	0.16	0.16
U239	33.52	36.57	0.07	0.17
U239	36.57	38.4	0.54	0.16
U240	0	3.04	3.84	0.2
U240	3.04	6.09	3.68	0.39
U240	6.09	7.62	0.35	0.65
U240	7.62	8.38	13.8	2.78
U241	0	3.04	3.02	0.7
U241	3.04	6.09	4.06	0.33
U241	6.09	9.14	9.04	0.87
U241	9.14	11.28	5.92	0.76
U241	11.28	12.19	44	13.4
U241	12.19	13.41	0.64	0.86
U242	3.04	6.09	7.72	1.05
U242	6.09	9.14	1.26	0.1
U242	9.14	12.04	1.82	0.03
U242	12.04	12.9	2.06	0.07
U242	12.9	13.44	4.56	0.14
U242	13.44	16.48	5.48	2.08
U242	16.48	17.37	4.34	1.54
U243	0	3.04	3.92	0.34
U243	3.04	6.09	3.54	0.04
U243	6.09	9.14	3.88	0.55
U243	9.14	9.69	2.04	0.93
U243	9.69	12.74	0.58	0.36
U243	12.74	15.78	1.78	0.41
U243	15.78	18.83	0.66	1.12
U243	18.83	21.88	0.34	0.26
U243	21.88	22.78	0.81	0.7
U244	0	1.82	1.96	0.01
U244	1.82	4.87	0.52	0.01
U244	4.87	7.31	2.46	0.01
U244	7.31	10.36	1.52	0.01
U244	10.36	13.41	0.76	0.01
U244	13.41	16.45	0.72	0.03
U244	16.45	19.5	1.32	0.01
U244	19.5	22.55	2.34	0.07
U244	22.55	25.6	2.3	0.31
U244	25.6	28.65	1.58	0.25
U244	28.65	31.69	0.87	0.74
U244	31.69	32.43	0.21	0.35
U245	0	3.04	2.88	1
U245	3.04	6.09	2.94	1.28
U245	6.09	9.14	0.18	0.35
U245	9.14	10.05	0.88	0.25
U245	10.05	12.19	14.8	3.18
U245	12.19	13.1	0.05	0.29
U245	13.1	16.15	6.05	1.46
U245	16.15	19.2	1.98	1.13
U245	19.2	22.25	1.56	2.78
U245	22.25	25.29	1.36	10.1
U245	25.29	28.34	4.64	1.19
U245	28.34	31.39	0.36	0.64
U245	31.39	34.44	0.07	0.28
U245	34.44	37.49	0.62	0.84
U245	37.49	40.54	3.52	6.04
U246	0	1.82	5.94	5.42
U246	1.82	3.35	5.76	5.48
U246	3.35	4.27	2.65	76.6
U246	4.27	4.82	1.42	1.2
U246	4.82	5.88	1.84	3.02
U247	0	1.52	2.26	2.97
U247	1.52	4.57	7.88	0.73
U247	4.57	7.01	6.16	0.1
U247	7.01	10.05	0.61	0.45
U247	10.05	10.67	0.42	0.2
U248	0	3.05	2.96	0.07
U248	3.05	6.1	2.7	0.12
U248	6.1	9.14	2.4	0.67
U248	9.14	12.19	4.52	0.31
U248	12.19	15.24	2.7	0.04
U248	15.24	18.29	1.42	0.02
U248	18.29	21.34	0.54	0.07
U248	21.34	24.38	1.84	0.02
U248	24.38	25.3	1.84	0.15
U249	0	3.04	0.83	0.82
U249	3.04	6.09	0.48	0.18
U249	6.09	9.14	0.32	0.13
U249	9.14	12.19	0.18	0.04
U249	12.19	15.24	0.14	0.06
U249	15.24	18.28	0.22	0.04
U249	18.28	20.02	1.36	0.16
U249	20.02	21.33	0.19	0.35
U249	21.33	24.38	0.16	0.2
U249	24.38	27.43	0.14	0.03
U249	27.43	30.48	0.58	0.03
U249	30.48	33.52	0.42	0.04
U249	33.52	34.19	0.39	0.01
U249	34.19	36.57	0.04	0.01
U249	36.57	39.62	0.2	0.01
U249	39.62	42.67	0.03	0.01
U249	42.67	45.72	0.08	0.05
U249	45.72	46.33	0.02	0.05
U250	0	1.37	3.54	0.68
U250	1.37	3.35	6.16	11
U250	3.35	6.4	4.54	2.48
U250	6.4	9.14	6.38	5.95
U250	9.14	12.19	0.66	0.43
U250	12.19	15.24	2.76	1.02
U250	15.24	18.28	1.9	0.65
U250	18.28	21.34	0.03	0.03
U250	21.34	21.94	0.04	0.02
U251	0	3.04	1.94	0.34
U251	3.04	6.09	1.56	0.36
U251	6.09	9.14	1.38	1.26
U251	9.14	12.19	1.3	0.29
U251	12.19	15.24	2.66	0.36
U251	15.24	18.28	0.35	0.06
U251	18.28	21.33	1.12	0.01
U251	21.33	24.38	1.98	0.02
U251	24.38	27.43	3.88	0.04
U251	27.43	28.5	28.3	6.34
U251	28.5	31.4	0.11	0.06
U252	0	3.04	2.28	0.29
U252	3.04	6.09	0.81	0.04
U252	6.09	9.14	1	0.27
U252	9.14	11.89	0.66	0.04
U252	11.89	14.93	0.26	0.11
U252	14.93	16.15	0.76	0.87
U252	16.15	18.9	0.11	0.06
U253	0	3.04	0.32	0.35
U253	3.04	6.09	0.17	0.05
U253	6.09	7.92	1.78	0.89
U253	7.92	9.6	5.06	2.26
U253	9.6	12.64	10.2	0.29
U253	12.64	14.32	0.64	0.96
U253	14.32	16.15	0.84	0.18
U254	0	1.52	1.78	0.39
U254	1.52	2.74	2.02	4.14
U254	2.74	3.35	0.8	0.09
U254	3.35	6.09	3.72	0.5
U254	6.09	7.62	8.1	0.69
U254	7.62	8.38	51.8	5.5
U254	8.38	9.26	0.76	0.12
U256?	0	2.74	10.7	0.2
U256?	2.74	5.79	0.44	0.02
U256?	5.79	8.84	0.09	0
U256?	8.84	9.57	0.34	0.22
U256?	9.57	10.3	1.28	0.08
U256?	10.3	10.94	0.29	0.01
U258	0	3.04	0.8	0.2
U258	3.04	6.09	0.21	0.81
U258	6.09	7.62	1.97	1.88
U258	7.62	10.36	3.12	3.32
U259	0	3.04	0.68	0.31
U259	3.04	6.09	1.78	0.35
U259	6.09	9.14	0.6	0.11
U259	9.14	12.19	0.09	0.09
U259	12.19	15.24	0.28	0.71
U259	15.24	18.28	3.38	7.4
U259	18.28	21.33	1.78	4.82
U259	21.33	22.55	2.86	2.52
U259	22.55	23.16	0.24	0.61
U260	21.79	23.01	0.03	0.42
U260	23.01	24.08	0.06	0.62
U260	24.08	25.45	1.22	0.22
U260	25.45	27.43	0.02	0.05
U260	27.43	28.35	0.01	0.06
U260	28.35	29.14	0.11	0.06
U260	29.14	31.4	0.01	0.01
U260	31.4	34.44	1.72	0.02
U260	34.44	35	0.54	0.03
U260	35	35.6	0.01	0.03
U260	35.6	36.27	0.02	0.18
U260	36.27	38.4	0.14	0.01
U260	38.4	39.62	0.01	0.01
U261	11.73	14.63	0.34	0.12
U261	14.63	16.15	0	0.02
U261	16.15	16.76	0.1	2.28
U261	16.76	19.5	0.64	0.42
U261	19.5	21.73	1.58	0.24
U261	21.73	22.13	0.02	0
U261	22.13	23.47	0.59	0.24
U261	23.47	24.99	1.02	0.46
U261	24.99	27.34	0.86	0.54
U261	27.34	28.04	0.36	0.74
U261	28.04	29.57	1.36	1.15
U261	29.57	31.24	0.12	0.31
U261	31.24	32.77	0.04	0.19
U261	32.77	34.13	1.8	1.38
U261	34.13	36.27	3.01	6.4
U261	36.27	39.31	2.06	4.8
U261	39.31	42.36	2.36	2.48
U261	42.36	43.9	1.8	0.46
U261	43.9	44.35	8.76	47.4
U261	44.35	45.11	2.26	0.06
U262	6.4	7.37	0.06	0.03
U262	7.37	9.75	0.04	0.04
U262	9.75	11.39	0.04	0.01
U262	11.39	13.35	0.07	0.01
U262	13.35	16.39	0.67	0.01
U262	16.39	19.44	1.26	0.01
U262	19.44	21.51	0.49	0.11
U262	21.51	23.28	0.42	0.18
U262	23.28	24.68	0.45	0.01
U262	24.68	27.73	1.62	0.02
U262	27.73	30.78	1.38	0.01
U262	30.78	33.83	3.5	0.03
U262	33.83	36.88	1.14	0.04
U262	36.88	38.19	1.06	0.02
U262	38.19	39.92	1.71	0.03
U262	39.92	41.81	5.3	0.6
U262	41.81	42.85	0.84	0.29
U262	42.85	43.89	7.85	0.33
U265	22.4	24.53	5.2	1.4
U265	24.53	25.3	51.5	6.3
U267	0	3.04	0.59	0.02
U267	3.04	5.48	0.68	0.02
U267	6.09	7.31	1.38	0.01
U267	7.31	10.36	5.56	0.01
U267	10.36	13.41	1.96	0.01
U267	13.41	15.69	3.16	0.01
U267	15.69	18.44	3.04	0.01
U267	18.44	19.81	0.74	0.05
U268	0	3.04	1.29	0.09
U268	3.04	5.02	0.94	0.13
U268	5.02	5.79	5.62	0.01
U268	5.79	7.16	47.2	0.02
U269	0	1.67	3.2	0.04
U269	1.67	2.74	1.72	0.02
U269	2.74	4.87	5.7	0.01
U269	4.87	8.22	3.74	0.07
U269	8.22	11.88	3.86	0.31
U269	11.88	12.49	40.5	8.04
U269	12.49	16.76	0.28	0.13
U270	8.53	9.75	0.88	0.12
U270	9.75	11.88	2.4	0.1
U270	11.88	14.28	3.7	0.2
U270	14.28	16.02	1.14	0.28
U270	16.02	18.59	0.68	0.24
U270	18.59	21.64	0.02	0.1
U270	21.64	27.73	0.01	0.12
U271	4.41	6.09	4	0.12
U271	6.09	7.01	3	1.25
U271	7.01	9.14	18.6	3.9
U272	28.8	30.69	1.94	0.46
U272	30.69	31.85	50	0.68
U272	31.85	32.3	10.9	63

U272	32.3	34.44	0.22	0.82
U273	13.1	15.24	1.86	0.04
U273	15.24	16.76	13.4	0.06
U273	16.76	17.06	0.06	0.02
U274	17.67	19.51	7.6	0.02
U274	19.51	21.33	3.9	0.02
U275	6.25	8.38	0.74	0.05
U275	8.38	10.66	10.2	0.07
U275	10.66	11.28	3.04	15.9
U275	11.28	12.8	0.34	2.54
U275	12.8	14.33	0.3	0.07
U276	22.25	22.56	0.56	1.26
U276	22.56	23.32	2.06	0.07
U276	23.32	26.52	0.96	0.48
U276	26.52	28.04	0.24	0.22
U277	29.56	30.48	12.3	0.03
U277	30.48	32.46	4.56	0.25
U277	32.46	32.76	1.08	2.9
U277	32.76	34.14	0.02	0.2
U277	34.14	35.05	0.01	0.2
U277	35.05	36.88	0.12	0.26
U282	0	1.86	6.95	2.38
U282	1.86	3.72	8.1	6.3
U282	3.72	5.58	6.9	9.45
U282	5.58	7.44	3.28	5.65
U282	7.44	11.16	1.86	7.12
U282	11.16	13.01	5.15	9.1
U282	13.01	14.87	3.4	9.75
U282	14.87	16.73	1.65	8.05
U282	16.73	18.59	2.95	17.8
U282	18.59	20.45	0.34	2.16
U282	20.45	22.31	1.42	2.14
U282	22.31	24.17	2.46	6.16
U283	0	0.91	4.45	12
U283	0.91	2.44	8.35	8.8
U283	2.44	3.66	7.05	8.6
U283	3.66	4.82	18.3	16.6
U285	0	0.76	30.4	36.1
U285	0.76	3.05	0.21	0.23
U286	0	0.61	0.04	0.07
U286	0.61	1.22	12.3	11.5
U286	1.22	2.13	0.02	0.66
U286	2.13	2.74	0.09	0.14
U286	2.74	3.65	6.12	0.82
U286	3.65	3.96	0.1	0.11
U286	3.96	5.18	5.76	6.05
U286	5.18	8.23	0.14	0.12
U287	0	1.21	4.46	2.36
U287	1.21	1.82	7.04	3.66
U287	1.82	2.74	4.82	7.48
U287	2.74	3.96	9.2	4.26
U287	3.96	4.26	8.38	2.5
U287	4.26	5.79	8.96	1.98
U287	5.79	7.62	1.92	11.1
U287	7.62	10.05	2.76	13.9
U287	10.05	10.67	3.32	6.52
U287	10.67	11.58	0.22	3.24
U287	11.58	12.67	0.74	2.88
U287	12.67	14.32	0.33	0.85
U287	14.32	15.48	0.16	0.13
U288	0	1.16	8.55	10.8
U288	1.16	1.46	0.18	0.67
U288	1.46	2.04	7.2	1.48
U288	2.04	3.04	1.52	0.77
U288	3.04	4.57	2.18	0.66
U288	4.57	7.31	2.26	0.95
U288	7.31	9.44	12.8	25.2
U288	9.44	10.66	3.82	3.52
U288	10.66	12.19	3.58	0.54
U288	12.19	13.71	12.2	3.48
U288	13.71	15.24	4.95	3.44
U289	22.56	24.69	2.56	3.32
U289	24.69	26.82	0.88	7.5
U289	26.82	27.43	1.08	12.8
U289	27.43	30.48	0.45	6.54
U289	30.48	33.83	0.52	2.78
U289	33.83	35.66	0.68	2.18
U289	35.66	38.56	1.7	2.76
U289	38.56	38.71	3.25	79.5
U289	38.71	40.23	0.04	0.19
U290	10.21	10.97	1.15	5.5
U290	10.97	11.58	4.26	5.96
U290	11.58	14.33	4.1	7.7
U290	14.33	14.94	1.18	1.82
U290	14.94	17.98	3.32	4.08
U290	17.98	21.03	2.88	2.23
U290	21.03	23.16	4.08	2.62
U291	33.22	33.99	1.78	0.17
U291	33.99	38.4	1.74	0.05
U291	38.4	40.23	1.88	0.16
U291	40.23	46.48	8.85	0.05
U291	46.48	46.94	35.6	0.04
U292	28.35	30.18	3.6	0.1
U292	30.18	33.22	2.04	0.07
U292	33.22	36.58	2.42	0.04
U292	36.58	38.71	2.4	0.02
U292	42.67	43.59	39.8	22.2
U293	26.5	29.26	0.88	0.03
U293	29.26	31.7	0.75	0.01
U293	31.7	35.36	1.52	0.09
U293	35.36	36.73	4.65	0.24
U293	36.73	38.1	6.1	0.05
U293	38.1	39.62	3.76	0.12
U293	39.62	41.76	10.2	0.06
U293	41.76	43.28	5.9	0.07
U293	43.28	44.81	42.5	21.8
U293	44.81	49.68	0.11	0.12
U294	27.19	29.02	4.42	3.18
U294	29.02	32.07	2.96	1.37
U294	32.07	34.5	3.25	1.6
U294	34.5	36.73	2.02	1.62
U294	36.73	40.54	3.04	0.65
U294	40.54	41.21	8.75	1.51
U294	41.21	43.89	2.92	0.32
U294	43.89	45.29	4.4	0.08
U294	45.29	46.02	47.8	1.17
U294	46.02	49.38	0	0
U294	49.38	49.62	0.24	0.06
U295	11.58	13.11	1.28	0.04
U295	13.11	15.24	2.26	0.01
U295	15.24	16.76	5.46	0.54
U295	16.76	17.68	14.6	2.94
U295	17.68	18.29	0.82	0.69
U295	18.29	19.81	0.11	0.12
U296	9.14	12.04	8.05	0.13
U296	12.65	13.11	57.8	0.59
U296	13.72	14.33	1.02	2.04
U297	33.22	34.14	1.16	0.77
U297	36.58	39.62	3.54	4.22
U297	39.62	42.06	2.04	0.51
U297	42.37	43.43	7.68	0.38
U297	43.43	44.81	18.1	0.02
U297	44.81	45.42	41.7	16.3
U297	45.42	46.94	0.14	0.16
U298	24.38	26.82	0.6	0.52
U298	26.82	30.33	5.42	0.69
U298	30.33	31.7	4.76	3.32
U298	32.61	34.59	4.14	2.17
U298	34.59	36.27	6.22	4.4
U298	36.27	38.86	8.84	2.54
U298	38.86	40.39	4.38	0.23
U298	40.39	43.43	4.68	0.61
U298	43.43	46.02	3.62	0.1
U299	34.44	35.97	0.16	0.07
U299	35.97	37.49	0.62	0.08
U299	37.49	39.78	1.16	0.05
U299	39.78	40.54	2.29	0.03
U299	40.54	40.9	23	0.03
U305	30.48	32.61	1.26	0.02
U305	32.61	33.53	7.05	0.07
U305	33.83	36.58	2.36	0.02
U305	36.58	37.8	4.94	0.01
U305	37.8	39.01	4.1	0.03
U305	39.01	41.45	7.22	0.1
U307	0	1.52	7.8	1.33
U307	1.52	2.59	7.75	34.2
U309	0	3.96	2.84	0.94
U309	3.96	5.79	0.44	0.07
U309	5.79	7.62	2.06	0.06
U309	7.62	9.14	3.6	0.35
U309	9.14	10.67	6.43	1.86
U309	10.67	12.19	4.24	3.18
U309	12.19	14.33	4.32	0.84
U309	14.33	16.46	2.64	0.44
U309	16.46	18.29	2.98	4.24
U309	18.29	20.73	2.96	1.16
U309	20.73	22.86	7.54	2.56
U309	22.86	24.38	1.96	0.27
U309	24.38	26.52	2.78	1.19
U309	26.52	29.87	2.96	2.14
U309	29.87	31.7	0.54	0.68
U309	31.7	34.75	3.82	1.16
U309	34.75	37.8	9.9	1.01
U309	37.8	39.62	9.3	5.25
U309	39.62	42.67	2.84	1.21
U310	0	0.91	0.69	1.61
U310	0.91	2.74	0.19	2.44
U310	2.74	3.96	0.06	3.51
U310	3.96	5.49	0.37	5.18
U310	5.49	7.32	2.32	7.16
U310	7.32	8.53	0.32	8.53
U311	0	2.74	2.22	0.13
U311	2.74	5.79	1.34	0.1
U314	31.58	33.1	2.44	0.91
U314	33.1	34.63	3.36	3.87
U314	34.63	36.15	1.92	4.22
U314	36.15	37.67	5	7.2
U314	37.67	39.2	5.6	4.78
U314	39.2	40.72	5.8	2.47
U314	40.72	41.45	11.2	0.11
U314	41.45	41.97	47.4	0.45
U314	41.97	43.89	2.74	0.55
U316	24.38	27.43	1.1	0.06
U316	27.43	30.48	2.84	0.15
U316	30.48	33.83	1.2	0.15
U316	33.83	34.75	1.02	1.1
U316	34.75	37.49	1.41	0.07
U316	37.49	40.54	2.59	0.01
U316	40.54	43.59	3.98	0.01
U316	43.59	45.11	8.44	0.01
U316	45.11	46.94	41	21.7
U316	46.94	47.86	0.31	0.73
U316	47.86	49.48	0	0
U316	49.48	50.6	0.04	0.03
U317	16.46	17.68	0.01	0.01
U317	18.29	20.12	0.01	0.01
U317	21.34	22.56	0.01	0.01
U317	24.38	25.6	1.23	4.78
U317	25.6	26.21	2.24	8.65
U317	27.43	30.48	1.68	3.76
U317	30.48	33.53	2.64	4.28
U317	33.53	34.75	7.48	0.73
U317	34.75	35.2	44.7	8.48
U317	35.2	36.27	7.74	0.81
U317	36.27	37.8	0.11	0.15
U318	19.96	21.03	1.26	4.52
U318	21.03	24.08	0.64	2.94
U318	24.08	27.13	0.52	4.34
U318	27.13	29.26	0.84	1.49
U318	29.26	31.39	4.56	0.17
U318	31.39	34.33	3.02	0.01
U318	34.33	37.8	2.24	0.14
U318	37.8	39.32	1.28	0.46
U318	39.32	42.06	0.01	0.02
U319	0	3.05	2.94	2.82
U319	3.05	5.79	3.22	0.42
U319	5.79	8.84	2.38	0.07
U319	8.84	11.89	1.18	0.02
U319	11.89	14.02	1.52	0.03
U319	14.02	15.54	1.46	0.01
U319	15.54	17.07	1.98	0.55
U319	17.07	19.81	1.06	0.2
U319	19.81	22.86	0.86	1.32
U320	7.74	8.69	2.08	11.1
U320	8.69	9.57	2.35	76.1
U321	0	2.13	4.4	1.29
U321	2.13	3.66	4.72	1.95
U321	3.66	5.18	4.6	0.4
U321	5.18	7.77	3.02	0.77
U321	7.77	7.92	5.9	47.7
U322	0	3.05	5.06	2.6
U322	3.05	5.79	2.98	1.54
U322	5.79	7.31	2.44	0.15
U322	7.31	8.44	2.99	0.22
U322	8.44	8.53	17.5	34.2
U324	0	1.83	1.69	1.69
U324	1.83	3.96	1.98	2.34
U324	3.96	4.57	0.03	0.01
U324	4.57	6.1	0.13	0.07
U325	0	0.91	4.22	0.33
U325	0.91	2.44	2.02	0.09
U325	2.44	5.49	1.72	0.15
U325	5.49	7.01	3.54	0.72
U325	7.01	7.07	21.4	23.9
U326	0	2.44	3.52	0.21
U326	2.44	5.49	9.2	0.59
U326	5.49	6.4	11.1	1.28
U326	6.4	6.46	21.7	20.9
U330	0	1.21	8.92	0.04
U330	1.21	2.44	16.6	0.23
U330	2.44	4.27	21.9	34.34
U330	4.27	5.94	6	1.25
U330	5.94	7.37	12	44.8
U331	0	0.61	18.2	11.7
U331	0.61	2.74	25.4	30.6
U331	2.74	3.66	4.42	0.35
U331	3.66	6.1	31	16.4
U331	6.1	7.93	0.84	0.36
U332	0	0.76	1.77	0.44
U332	0.76	1.37	17.4	0.28
U332	1.37	6.1	26.8	5.5
U332	6.1	7.62	14.7	31.3
U334	0	3.05	1.61	0.03
U334	3.05	5.49	1.02	0
U334	5.49	9.14	0.72	0.01
U334	9.14	12.8	0.71	0.04
U334	12.8	15.24	0.82	0.04
U334	15.24	18.29	0.97	0.09
U334	18.29	21.34	3.92	0.04
U334	21.34	24.38	2.47	0.02
U334	24.38	28.96	2.4	0.14
U334	28.96	30.48	2.38	0.24
U336	13.41	15.24	5.94	0.06
U336	15.24	16.76	5.2	0.07
U336	16.76	18.29	7.44	0.11
U336	18.29	20.72	0.29	0.27
U337	19.81	21.34	11.8	1.26
U337	21.34	22.86	10.9	3.3
U337	22.86	24.23	11.2	0.11
U337	24.23	24.38	30.8	10.9
U500	44.81	45.83	1.9	4.6
U500	46.4	47	2.05	5.8
U500	47	47.85	2.35	13.6
U500	47.85	48.77	1.8	12.8
U500	48.77	50.1	2.9	8.6
U500	50.1	51.6	22.8	39.6
U500	51.6	51.85	7.8	4.6
U501	15.26	16.3	2.85	11.2
U501	16.3	17.45	1.33	3.9
U501	17.45	18.2	1.5	1.42
U501	18.2	18.95	2.05	2.02
U501	18.95	19.87	4.25	9.8
U501	19.87	21	6.9	3.6
U501	21	22.14	8.8	1.32
U501	22.14	23.3	40.6	9
U502	10.93	11.14	2.2	3.1
U502	11.14	12.31	2.9	27
U502	12.31	13.55	3	4.6
U502	13.55	14.51	2.4	3
U502	14.51	15.92	1.85	5
U502	15.92	16.92	3.45	2.1
U502	16.92	18.48	4.8	1.72
U502	18.48	19.24	7.68	0.14
U502	19.24	20.42	9.94	0.52
U503	35.35	37.35	1.4	1.32
U503	37.35	39.35	1.02	1.8
U503	39.35	40.35	2.8	6.9
U503	40.35	41.05	2.9	4.55
U503	41.05	41.65	2.55	1.92
U503	41.65	42.25	1.68	0.96
U503	42.25	44.03	4.15	0.72
U503	44.03	44.9	4.1	2.14
U503	44.9	46.32	3.63	6.1
U503	46.32	47.53	2.6	7.1

U503	47.53	48	3.65	1.12
U503	48	49.5	2.35	2.52
U503	49.5	50.7	3.15	1.92
U503	50.7	51.21	1.98	4.85
U503	51.21	52.15	2.45	8.05
U503	56.9	58.83	1.7	9.2
U503	58.83	60.1	2.7	9.5
U503	60.1	60.75	1.8	7.9
U503	60.75	61.87	1.55	12.4
U503	61.87	63.4	2.9	14.4
U503	63.4	64.92	3.1	13
U503	64.92	65.5	0.14	7.6
U503	65.5	67.1	1.17	9.9
U503	67.1	67.97	1.33	6.9
U503	67.97	69.15	0.21	9.2
U503	69.15	69.95	0.26	27
U503	69.95	71.02	1.08	8.9
U503	71.02	71.8	0.64	3.14
U504	11.95	12.5	1.2	5.4
U504	12.5	13.05	1.25	9.6
U504	13.05	14.02	0.87	26.1
U504	14.02	14.85	4.7	16
U504	14.85	15.75	2.1	10.9
U504	15.75	17.07	1.75	3.6
U504	17.07	18.3	3.1	2.9
U504	18.3	19.3	3.25	7.4
U504	19.3	20.73	6.2	3.95
U504	20.73	21.65	5.3	1.78
U504	21.65	22.45	7.3	2.1
U504	22.45	22.75	35	0.16
U505	8.72	9.7	6.1	22.8
U505	9.7	10.66	5.1	30.4
U505	10.66	11.6	1.62	7.5
U505	11.6	12.6	1.7	9.1
U505	12.6	13.6	2.25	1.96
U505	13.6	14.6	2.2	1.28
U505	14.6	15.4	6.1	2.64
U505	15.4	16.65	2.15	2.08
U505	16.65	17.65	3.55	1.48
U505	17.65	18.68	2.75	0.4
U505	18.68	18.97	11.2	4.88
U505	18.97	19.1	0.09	72.8
U506	26.9	28.35	1.53	1.52
U506	28.35	29.33	1.25	12
U506	29.33	30.49	2.55	0.43
U506	30.49	31.82	4.3	0.66
U506	31.82	32.35	6.86	1.24
U506	32.35	33.28	4	0.82
U506	33.28	34.44	2.6	2.6
U506	34.44	35.97	4.2	1.18
U506	35.97	37	3.5	3
U506	37	37.74	0.88	0.64
U506	37.74	39.18	4.15	11.4
U506	39.18	40.1	1.65	0.54
U506	40.1	40.92	3.6	0.22
U506	40.92	42.06	3.25	0.12
U506	42.06	42.65	17.5	0.06
U506	42.65	43.1	33.44	13
U506	43.1	43.59	28.14	1.56
U506	43.59	44.4	27.1	16.4
U506	44.4	45.11	30.22	15.2
U506	45.11	45.95	13.36	0.36
U506	45.95	47.2	2.4	0.1
U506	47.2	48.16	2.3	0.04
U506	48.16	49.68	2.6	0.04
U506	49.68	50	21.96	0.04
U506	50	50.65	56.48	0.06
U506	50.65	50.9	37.94	0.06
U507	9.8	10.55	6.36	5.6
U507	10.55	10.97	0.6	15
U507	10.97	11.8	4.7	15.4
U507	11.8	12.55	2.05	1.9
U507	12.55	12.8	2.35	10.6
U507	12.8	14.02	2.5	4.6
U507	14.02	15	5.3	3.2
U507	15	15.54	6.18	3.1
U507	15.54	16.1	11.32	0.44
U507	16.1	16.85	47.42	7
U507	16.85	17.07	1.75	0.52
U507	17.07	17.22	10	1.9
U508	0	0.8	1.5	29.8
U508	0.8	1.92	2	22.8
U508	1.92	2.98	2.2	11.6
U508	2.98	4.07	2.45	13.2
U508	4.07	4.7	3.2	17.8
U508	4.7	5.6	2.4	18.2
U508	5.6	7.62	0.8	5.9
U508	7.62	8.05	0.93	5.4
U508	8.05	9.1	3.1	9.6
U508	9.1	10.1	4.3	4.9
U508	10.1	11.18	4.8	2.9
U508	11.18	11.55	2.9	2.74
U508	11.55	12.28	5.1	2.34
U508	12.28	13.3	11.2	10.2
U508	13.3	14.4	2.25	5.95
U508	14.4	15.24	1.93	10.4
U508	15.24	15.64	1.34	0.68
U508	15.64	17.5	1.75	5.2
U508	17.5	18.29	0.8	3.6
U508	18.29	19.38	8.6	13
U508	19.38	20.08	5.1	2.52
U508	20.08	20.93	5.7	2.88
U508	20.93	21.34	6.8	1.51
U508	21.34	22.05	13	4
U508	22.05	22.86	27.8	29.8
U509	0	0.74	3.4	8.6
U509	0.74	2.13	5.5	15.6
U509	2.13	3	5.6	18.8
U509	3	4.42	1.95	9
U509	4.42	5.54	6.3	7.3
U509	5.54	7.01	5.7	4.5
U509	7.01	8.5	6.4	2.95
U509	8.5	9.2	1.9	0.78
U509	9.2	9.85	6.1	1.73
U509	9.85	10.75	4.9	0.66
U509	10.75	11.75	6.1	0.18
U509	11.75	12.21	8.6	0.24
U509	12.21	12.4	56.4	0.22
U509	12.4	14.63	0	0
U510	0	1.58	6.75	7.4
U510	1.58	3.02	2.05	0.64
U510	3.02	4.42	3.3	0.17
U510	4.42	5.94	1.9	0.37
U510	5.94	7.36	1.78	1.16
U510	7.36	8.14	3.35	1.22
U510	8.14	9.68	4.9	1.04
U510	9.68	11.02	9.5	2.6
U510	11.02	11.58	25.2	38.4
U510	11.58	14.63	0	0
U511	0	1.75	2.25	1.2
U511	1.75	3	1.15	0.33
U511	3	4.6	1.7	0.06
U511	4.6	6.03	0.93	0.03
U511	6.03	7.44	2.65	0.04
U511	7.44	9.1	2.55	0.1
U511	9.1	9.48	5.7	0.44
U511	9.48	9.75	58.2	0.82
U511	9.75	11.28	0	0
U512	0	1.7	5.8	0.06
U512	1.7	2.06	2.05	0.04
U512	2.06	2.85	4.6	1
U512	2.85	3.8	2.15	0.29
U512	3.8	4.7	4.3	0.09
U512	4.7	5.2	11.4	0.1
U512	5.2	6.27	51.6	7.2
U512	6.27	6.95	3.9	67.6
U512	6.95	9.45	0	0
U513	0	0.76	9.2	3.9
U513	0.76	1.7	1.7	0.3
U513	1.7	2.95	2.85	0.08
U513	2.95	3.77	21.4	0.37
U513	3.77	5	8.7	0.17
U513	5	6.1	42.8	22.8
U513	6.1	7.62	0	0
U514	0	0.4	6.4	0.98
U514	0.4	2.5	2.3	0.14
U514	2.5	4.45	5	0.04
U514	4.45	5.05	4.7	0.03
U514	5.05	5.6	18.4	0.01
U514	5.6	6.8	56.8	0.68
U514	6.8	8	56.2	0.32
U514	8	8.2	42.6	1.04
U514	8.2	8.7	30.2	17.2
U514	8.7	11.28	0	0
U515	0	1.4	3.4	0.26
U515	1.4	2.8	17.8	0.09
U515	2.8	4.1	9.4	0.51
U515	4.1	5.7	55.4	0.08
U515	5.7	6.4	36.4	19.2
U515	6.4	7.92	0	0
U516	0	1.05	5.15	6.6
U516	1.05	2.55	2.13	2.3
U516	2.55	4	2.05	0.66
U516	4	5.5	5.8	1.78
U516	5.5	6.7	4.15	12.4
U516	6.7	8.1	36.8	18.8
U516	8.1	9.75	0	0
U517	0	1.53	0.33	0.72
U517	1.53	3.25	8	3.35
U517	3.25	4.05	29.4	0.06
U517	4.05	5.49	0	0
U518	0	1.1	0	0
U518	1.1	2.95	4.1	1.58
U518	2.95	4.91	3.4	2.32
U518	4.91	5.79	2.7	9.6
U518	5.79	7.32	1.68	1.26
U518	7.32	7.85	4.85	4.5
U518	7.85	9.07	3.9	1.47
U518	9.07	10.36	5.15	2.96
U518	10.36	11.5	5.05	1.36
U518	11.5	12.2	9.2	2.32
U518	12.2	13.41	10.8	3.85
U518	13.41	14.94	3.4	3.28
U518	14.94	16.93	4.7	2.96
U518	16.93	17.53	4.6	0.56
U518	17.53	17.98	8.2	1.75
U518	17.98	19.51	3.6	1.36
U518	19.51	20.02	2.9	0.95
U518	20.02	20.75	4.5	2.08
U518	20.75	22.56	5.35	2.52
U518	22.56	24.08	5.9	0.1
U518	24.08	25.6	5.15	0.08
U518	25.6	26.5	4.14	0.2
U518	26.5	26.83	15.8	0.06
U518	26.83	28.26	35.6	21.2
U518	28.26	30.18	0	0
U519	0	0.91	5.45	3.1
U519	0.91	2	2.75	3.1
U519	2	2.6	14.6	3.65
U519	2.6	3.96	2.93	0.69
U519	3.96	5.49	3.33	0.74
U519	5.49	7.35	2.8	1.61
U519	7.35	8.53	2.15	0.02
U519	8.53	10.06	2.03	0.07
U519	10.06	11.58	0.08	0.04
U519	11.58	13.11	0.03	0.1
U519	13.11	14.63	0.05	0.14
U519	14.63	15.3	0.18	0.96
U519	15.3	15.93	11	0.52
U519	15.93	16.35	28.4	37.6
U519	16.35	17.68	0	0
U520	0	1.22	1.6	1.26
U520	1.22	2.74	5.8	2.8
U520	2.74	4.27	2.5	8.2
U520	4.27	5.79	2.45	1.48
U520	5.79	7.32	2.3	2.06
U520	7.32	7.85	6.2	2.6
U520	7.85	9.25	5.9	1.74
U520	9.25	10.36	3	6.2
U520	10.36	11.89	1.8	1.44
U520	11.89	13.41	6.3	2.6
U520	13.41	15.2	7.5	8.8
U520	15.2	16.46	5.86	6.2
U520	16.46	18.75	7.1	1.68
U520	18.75	20	8.6	1.86
U520	20	21.95	9.8	1.16
U520	21.95	22.23	4.56	0.24
U520	22.23	22.4	41.4	0.34
U520	22.4	25.6	0	0
U521	0	1.52	2.1	0.32
U521	1.52	2.95	2.23	1.66
U521	2.95	3.66	7.4	2.36
U521	3.66	5.05	1.78	0.32
U521	5.05	5.98	3.35	0.81
U521	5.98	11.75	0	0
U521	11.75	12.8	1.26	0.04
U521	12.8	14.48	1.46	0.01
U521	14.48	15.1	1.16	0.02
U521	15.1	15.7	4.25	0.01
U521	15.7	17.37	0	0
U522	0	1.22	6.2	0.22
U522	1.22	2.6	2.95	1.4
U522	2.6	3.27	1.2	0.08
U522	3.27	4.72	1.45	0.04
U522	4.72	5.23	3.45	0.01
U522	5.23	6.35	2.92	0.48
U522	6.35	7.32	1.78	0.13
U522	7.32	8.75	2.95	0.02
U522	8.75	9.44	16.6	0.04
U522	9.44	10.3	5.9	0.01
U522	10.3	10.5	37.6	0.01
U522	10.5	12.4	5.6	0.01
U522	12.4	13.41	14.2	0.01
U522	13.41	14.6	12.6	0.01
U522	14.6	15.75	50	0.01
U522	15.75	17.98	0	0
U523	0	1.2	3.75	0.02
U523	1.2	3.05	1.23	0.01
U523	3.05	4.72	3.9	0.01
U523	4.72	5.37	41.6	0.01
U523	5.37	5.78	6.6	0.02
U523	5.78	9.14	0	0
U524	0	1.77	3.1	1.74
U524	1.77	2.17	6.2	9.8
U524	2.17	3.05	19.6	1.88
U524	3.05	4.57	1.08	0.16
U524	4.57	6.42	1.3	0.02
U524	6.42	8.03	1.72	0.17
U524	8.03	8.8	1.88	0.01
U524	8.8	9.64	0.87	0.04
U524	9.64	10.05	6.7	1.11
U524	10.05	10.75	11	1.1
U524	10.75	13.27	0	0
U524	13.27	13.72	28.4	0.6
U524	13.72	19.81	0	0
U525	0	1.15	7.2	2.72
U525	1.15	2	6.9	0.18
U525	2	2.9	6.8	0.03
U525	2.9	3.1	17.4	0.02
U525	3.1	3.65	6.2	0.01
U525	3.65	8.84	0	0
U526	0	0.61	1.64	0.29
U526	0.61	2.5	1.02	0.22
U526	2.5	3.4	3.95	0.16
U526	3.4	3.85	7.2	0.02
U526	3.85	5.18	3.4	0.04
U526	5.18	6.71	2.65	0.01
U526	6.71	7.8	5.15	0.02
U526	7.8	8.5	12.1	0.02
U526	8.5	9.75	2.35	0.01
U526	9.75	11.28	1.3	0.02
U526	11.28	12.35	18.3	0.78
U526	12.35	13.32	11.7	0.3
U526	13.32	14.33	0.8	0.28
U526	14.33	15.4	0.8	0.24
U526	15.4	15.85	0.64	1.24
U526	15.85	17.13	6.9	0.36
U526	17.13	17.25	21.6	0.04
U526	17.25	18.9	0	0
U527	0	1.83	1.7	0.12
U527	1.83	3.4	2.75	0.12
U527	3.4	3.95	11	0.92
U527	3.95	5.15	4.7	0.02
U527	5.15	5.3	11.8	0.01
U527	5.3	6.25	8.2	0.04
U527	6.25	6.6	5.8	0.06
U527	6.6	7.28	10.6	0.02
U527	7.28	8	19.2	1.28
U527	8	8.45	4.2	0.24
U527	8.45	10.97	0	0
U528	0	0.91	2.6	0.04
U528	0.91	2.2	1.9	0.02
U528	2.2	3.1	5.32	0.02
U528	3.1	3.45	3.85	0.01

U528	3.45	4	10.9	0.4
U528	4	4.77	13.3	2.16
U528	4.77	5.05	24	0.24
U528	5.05	5.7	0.24	0.07
U528	5.7	7.14	27.7	12.8
U528	7.14	8.71	6.7	0.28
U528	8.71	9.1	36.3	1.88
U528	9.1	10.06	0	0
U529	0	0.91	1.55	0.26
U529	0.91	2.44	4.45	0.58
U529	2.44	3.96	3.4	0.12
U529	3.96	5.49	2.85	0.1
U529	5.49	6.33	2.85	0.02
U529	6.33	6.75	11.9	0.02
U529	6.75	7.09	21.6	0.01
U529	7.09	7.4	57.7	0.01
U529	7.4	11.58	0	0
U530	0	0.3	0	0
U530	0.3	1.1	12.6	0.46
U530	1.1	2.9	6	0.24
U530	2.9	3.96	3.15	1.3
U530	3.96	6.1	2.15	2.57
U530	6.1	7.3	5.4	0.28
U530	7.3	8.12	7	0.64
U530	8.12	8.85	5.7	0.08
U530	8.85	10.06	3.8	0.18
U530	10.06	11.58	2.05	0.05
U530	11.58	13.11	2.55	0.3
U530	13.11	14.63	3.45	0.07
U530	14.63	16.15	5.1	0.6
U530	16.15	17.22	5.4	2.56
U530	17.22	17.48	8	44.4
U530	17.48	19.2	0	0
U531	0	1	0.4	1.5
U531	1	2.44	0.79	0.66
U531	2.44	3.96	0.55	0.3
U531	3.96	5.49	1.35	0.64
U531	5.49	7.01	1.28	1.1
U531	7.01	7.65	13.2	3.6
U531	7.65	8.9	27.5	30.8
U531	8.9	9.6	1.8	1.88
U531	9.6	9.77	20.8	21.6
U531	9.77	10.15	3.35	0.92
U531	10.15	13.11	0	0
U532	0	1.3	0	0
U532	1.3	2.6	4.08	0.44
U532	2.6	3.66	0.25	0.17
U532	3.66	5.18	0.98	0.08
U532	5.18	6	8.2	0.7
U532	6	6.5	5.56	2.16
U532	6.5	8.23	3.8	0.94
U532	8.23	9.75	2.08	0.03
U532	9.75	11.28	0.1	0.26
U532	11.28	12.5	1.8	0.34
U532	12.5	14.02	4.12	0.02
U532	14.02	15.31	4.02	1.58
U532	15.31	15.46	1.98	7
U532	15.46	17.37	0	0
U533	0	1.83	0.61	0.38
U533	1.83	3.35	1.1	0.56
U533	3.35	4.95	2.95	2.24
U533	4.95	5.56	26.4	2.56
U533	5.56	6.08	8.1	53.6
U533	6.08	7.92	2.18	2.24
U533	7.92	9.65	2.95	0.52
U533	9.65	9.78	46.8	2.4
U533	9.78	10.15	5.6	1.52
U533	10.15	11.9	4.65	0.52
U533	11.9	12.32	5.12	1.56
U533	12.32	13.3	7.8	44.4
U533	13.3	14.02	3.8	7.4
U533	14.02	14.5	0.45	1.88
U533	14.5	16.76	0	0
U534	0	2.13	1.4	0.1
U534	2.13	3.66	2.3	0.27
U534	3.66	5.46	2.8	0.38
U534	5.46	6.82	20.8	33.6
U534	6.82	7.78	11.4	2.48
U534	7.78	8.23	0.98	0.31
U534	8.23	9.75	4.45	1.14
U534	9.75	11.28	3.25	0.57

U534	11.28	12.8	1.45	0.28
U534	12.8	14.33	3.15	0.02
U534	14.33	15.54	3.25	0.01
U534	15.54	17.07	3.75	0.09
U534	17.07	18.59	6.2	0.6
U534	18.59	20.12	3.62	1.76
U534	20.12	21.64	1.7	0.38
U534	21.64	23.47	3.45	0.77
U534	23.47	24.69	1.1	0.05
U534	24.69	26.1	1.95	1.22
U534	26.1	26.35	5.35	31.6
U534	26.35	28.04	0.24	1.14
U534	28.04	30.18	0	0
U535	0	1.52	2.05	0.18
U535	1.52	3.05	1.01	0.18
U535	3.05	4.57	0.95	0.06
U535	4.57	5.1	1.5	0.04
U535	5.1	7.35	8.3	0.24
U535	7.35	9.14	1.45	0.03
U535	9.14	10.67	1.35	0.02
U535	10.67	12.19	1.32	0.08
U535	12.19	13.72	0.79	0.02
U535	13.72	15.24	0.4	0.01
U535	15.24	16.76	0.16	0.04
U535	16.76	18.29	0.14	0.11
U535	18.29	19.81	0.34	0.22
U535	19.81	21.34	1.25	0.02
U535	21.34	22.86	2.75	0.2
U535	22.86	24.38	0.98	0.44
U535	24.38	27.43	0	0
U536	0	1	1.45	0.16
U536	1	2.44	0.68	0.34
U536	2.44	3.96	1.7	0.03
U536	3.96	5.49	1.55	0.4
U536	5.49	6.4	0.93	0.24
U536	6.4	7.25	7.5	0.08
U536	7.25	8.33	1.25	0.28
U536	8.33	10.06	11.4	0.74
U536	10.06	10.5	1.43	0.24
U536	10.5	13.11	0	0
U537	0	2.13	1.8	0.4
U537	2.13	3.66	0.68	0.18
U537	3.66	5.3	1.4	0.14
U537	5.3	6.05	9.8	0.1
U537	6.05	6.85	1.95	0.46
U537	6.85	7.2	22.5	5.8
U537	7.2	9	7.3	49.6
U537	9	11.28	0	0
U538	0	2.44	1.6	1.08
U538	2.44	4.35	2.25	0.7
U538	4.35	5.49	1.13	0.22
U538	5.49	7	1.86	0.48
U538	7	8.53	2.75	0.43
U538	8.53	9.9	4.98	0.48
U538	9.9	10.95	5.15	0.52
U538	10.95	12.55	4.18	3.4
U538	12.55	14	1.89	0.21
U538	14	15.12	0.6	0.62
U538	15.12	15.55	5.26	4.4
U538	15.55	16	7.2	57.2
U538	16	17.68	0	0
U539	0	2.9	2.55	0.82
U539	2.9	4.12	1.9	1.1
U539	4.12	5.45	5.8	0.98
U539	5.45	6.05	12.5	8
U539	6.05	8.23	0	0
U540	0	2.13	0.83	0.26
U540	2.13	3.66	1.13	0.44
U540	3.66	5.18	2.45	0.22
U540	5.18	7.05	1.95	0.46
U540	7.05	8.23	1.73	0.47
U540	8.23	9.75	4.9	0.26
U540	9.75	11.28	5.9	4.1
U540	11.28	12.8	4.5	1.1
U540	12.8	14.33	3.15	0.42
U540	14.33	14.7	8.7	0.3
U540	14.7	15.85	7.4	50
U540	15.85	17.37	2.8	67.6
U540	17.37	18.45	4.1	66
U540	18.45	19.51	0	0
U541	0	1.52	2.3	1.84

U541	1.52	3.05	1.7	1.86
U541	3.05	4.57	4.5	6.2
U541	4.57	6.1	3.98	2.44
U541	6.1	6.8	0.7	0.28
U541	6.8	7.4	12.7	6.2
U541	7.4	9.14	0	0
U542	0	1.7	2.45	0.64
U542	1.7	3.8	1.95	0.88
U542	3.8	4.75	4.6	0.48
U542	4.75	6.4	1.25	0.34
U542	6.4	8.4	2.5	0.86
U542	8.4	9.45	6.8	0.83
U542	9.45	11.15	6.4	2.4
U542	11.15	12.2	5.05	2.16
U542	12.2	12.72	5.1	50.4
U542	12.72	14.02	0	0
U543	0	2.2	0	0
U543	2.2	3.96	1.47	0.76
U543	3.96	5.35	2.2	0.96
U543	5.35	6.65	1.8	0.28
U543	6.65	8.53	4.4	0.6
U543	8.53	9.35	0	0
U543	9.35	10.06	2.28	0.03
U544	0	0.45	0	0
U544	0.45	1.83	0.5	0.32
U544	1.83	3.35	1.55	0.28
U544	3.35	4.88	2.25	0.54
U544	4.88	6.4	1.85	0.52
U544	6.4	8.1	2.85	0.93
U544	8.1	8.95	5.1	0.12
U544	8.95	9.6	7.9	0.31
U544	9.6	10.97	4.8	0.55
U544	10.97	12.5	6.1	0.36
U544	12.5	14.02	0	0
U545	0	2.13	2.48	0.54
U545	2.13	3.95	4.6	0.4
U545	3.95	4.65	8.2	1.52
U545	4.65	5.5	8	54.8
U545	5.5	8.23	0	0
U546	0	1.6	7.4	0.6
U546	1.6	2.44	2.95	0.2
U546	2.44	3.96	2.2	0.06
U546	3.96	4.65	8.4	0.04
U546	4.65	5.35	25	0.03
U546	5.35	6.2	44.8	6.2
U546	6.2	7.88	0	0
U546	7.88	8.53	6.4	5
U546	8.53	10.06	0	0
U547	0	0.75	5.4	0.98
U547	0.75	2.25	1.68	0.12
U547	2.25	2.95	4.6	0.02
U547	2.95	3.88	12	0.04
U547	3.88	4.23	28.5	0.34
U547	4.23	6.71	0	0
U548	0	1.8	1	0.18
U548	1.8	3.25	2.35	0.1
U548	3.25	4.25	6	0.02
U548	4.25	5.75	6.2	0.04
U548	5.75	7.01	3.53	0.04
U548	7.01	7.85	4.6	0.01
U548	7.85	8.38	14.2	2.6
U548	8.38	8.87	22.8	46.8
U548	8.87	11.58	0	0
U549	0	1.6	3.95	0.78
U549	1.6	2.74	5.6	0.7
U549	2.74	4.27	4.15	0.04
U549	4.27	5.79	3.35	0.2
U549	5.79	7.32	5.4	0.04
U549	7.32	7.95	9	0.03
U549	7.95	8.37	26.2	1.18
U549	8.37	9	48.8	15.2
U549	9	10.05	2.6	72.4
U549	10.05	11.89	0	0
U550	0	1.8	2.64	0.21
U550	1.8	2.44	1.57	0.01
U550	2.44	3.96	2.7	0.01
U550	3.96	4.8	1.74	0.02
U550	4.8	5.8	4.24	0.04
U550	5.8	6.01	34.6	0.75
U550	6.01	8.54	0	0
U551	0	1.07	2.25	0.01

U551	1.07	2.43	3.19	0.02
U551	2.43	3.65	1.74	0.02
U551	3.65	5.18	1.82	0.08
U551	5.18	6.7	2.04	0.06
U551	6.7	8.23	2.42	0.14
U551	8.23	8.48	21.3	2.7
U551	8.48	9.76	0	0
U552	0	1	15.4	10.3
U552	1	3.05	4.95	0.36
U552	3.05	4.28	11.4	0.1
U552	4.28	5.38	24.5	40
U552	5.38	5.67	4.06	0.68
U552	5.67	6.1	0	0
U553	0	1.52	1.18	1.67
U553	1.52	2.7	5.43	1.71
U553	2.7	4.1	5.1	0.06
U553	4.1	4.41	18.6	1.43
U553	4.41	4.78	0.3	0.04
U553	4.78	5.49	0	0
U554	0	1.15	6	1.7
U554	1.15	3.4	6.6	1.32
U554	3.4	4.15	6.8	1.08
U554	4.15	5	7.6	0.86
U554	5	5.15	16.2	34.8
U554	5.15	6.1	6.8	0.58
U554	6.1	7.8	6	0.38
U554	7.8	8.85	7.8	0.62
U554	8.85	9.6	5.2	0.22
U554	9.6	10.1	17.6	16.8
U554	10.1	11.23	14.4	4.45
U554	11.23	12.19	14	14
U554	12.19	13.72	12	12.2
U554	13.72	15.24	0	0
U555	0	1.6	2.4	1.17
U555	1.6	2.25	3.3	7.1
U555	2.25	3.3	5.36	0.84
U555	3.3	3.85	3.84	0.24
U555	3.85	4.65	12.4	11.8
U555	4.65	5.61	7.5	3.97
U555	5.61	6.71	49.9	10.6
U555	6.71	8.23	0	0
U556	0	4.82	0	0
U556	4.82	5.49	0.12	0.02
U556	5.49	6.05	4.8	0.01
U556	6.05	6.6	2.04	0.09
U556	6.6	7.65	4.52	0.02
U556	7.65	8.62	1.33	0.02
U556	8.62	13.6	0	0
U556	13.6	15.43	2.85	0.31
U556	15.43	16.95	0.61	0.03
U556	16.95	17.38	5.48	1.02
U556	17.38	17.7	8.8	35.5
U556	17.7	18.45	0.04	1.94
U556	18.45	19	0.04	0.47
U556	19	35.06	0	0
U557	0	3.35	0	0
U557	3.35	3.95	0.38	0.06
U557	3.95	4.85	2.65	0.06
U557	4.85	5.43	14.4	3.51
U557	5.43	6.05	4.5	0.06
U557	6.05	6.75	3.35	0.46
U557	6.75	9.45	0	0
U558	0	17.3	0	0
U558	17.3	18.35	1.1	0.37
U558	18.35	19.8	1.95	0.03
U558	19.8	21.21	0.99	0.07
U558	21.21	22.9	1.1	0.03
U558	22.9	24.64	1.08	0.02
U558	24.64	25.84	5.55	0.26
U558	25.84	27.01	13.5	12
U558	27.01	27.43	4.36	0.06
U558	27.43	41.45	0	0
U559	0	6.5	0	0
U559	6.5	8.21	1.08	0.01
U559	8.21	9.7	4.5	0.02
U559	9.7	10.23	9.6	0.01
U559	10.23	11.06	0.69	0.01
U559	11.06	12	5.25	0.01
U559	12	13.55	7.5	0.01
U559	13.55	15.05	8.5	0.03
U559	15.05	15.87	4.56	0.06

U559	15.87	16.77	0.65	0.01
U559	16.77	19.05	2.41	0.22
U559	19.05	19.8	1	0.09
U559	19.8	20.4	5.34	1.62
U559	20.4	21.34	9.7	34.5
U559	21.34	22.87	0	0
U560	0	26.75	0	0
U560	26.75	27.58	1.21	0.01
U560	27.58	28.5	3.3	0.05
U560	28.5	29.2	0.65	0.02
U560	29.2	30.15	0	0
U560	30.15	30.95	0.6	0.27
U560	30.95	31.7	1.55	8.75
U560	31.7	37.5	0	0
U562	0	33.54	0	0
U562	33.54	35.06	0.55	0.02
U562	35.06	36.59	0.55	0.01
U562	36.59	38.61	0.61	0.01
U562	38.61	39.63	1.12	0.07
U562	39.63	43.7	0.05	0.19
U562	43.7	44.25	1.75	1.36
U562	44.25	52.13	0	0
U563	0	32	0	0
U563	32	33.54	0.33	0.13
U563	33.54	34.86	1.36	0.03
U563	34.86	36.59	0.06	0.01
U563	36.59	42.99	0	0
U564	0	44.36	0	0
U564	44.36	45.12	1.31	0.1
U564	45.12	46.47	1.73	0.04
U564	46.47	47.24	0.24	0.06
U564	47.24	47.87	2.95	0.03
U564	47.87	49.52	3.48	0.1
U564	49.52	50.01	5.91	0.33
U564	50.01	50.91	1.5	0.02
U564	50.91	51.8	0.5	0.49
U564	51.8	53.96	0	0
U565	0	58.55	0	0
U565	58.55	59.94	1.68	0.01
U565	59.94	61.89	1.39	0.14
U565	61.89	63.41	0.18	0.19
U565	63.41	64.94	2.13	0.04
U565	64.94	67.01	2.88	0.31
U565	67.01	67.99	2.14	0.12
U565	67.99	70.12	0.2	0.11
U566	0	58.23	0	0
U566	58.23	59.24	1.07	0.2
U566	59.24	59.67	1.95	1.18
U566	59.67	61.59	0	0
U567	0	34.73	0	0
U567	34.73	35.5	0.13	0.01
U567	35.5	36.59	1.25	0.01
U567	36.59	38	2.22	0.01
U567	38	39.63	7.48	0.01
U567	39.63	41.3	3.46	0.01
U567	41.3	42.25	0.73	0.01
U567	42.25	43.27	1.55	0.01
U567	43.27	48.78	0	0
U567	48.78	49.4	1.18	0.01
U567	49.4	50.25	1.7	0.01
U567	50.25	51.05	0.37	0.01
U567	51.05	56.4	0	0
U567	56.4	58.2	0.22	0.01
U567	58.2	60.98	0	0
U568	0	14.35	0	0
U568	14.35	14.94	1.9	0.33
U568	14.94	16.2	3.25	0.94
U568	16.2	17.2	2.05	0.34
U568	17.2	17.7	4.05	4.3
U568	17.7	18.45	1.5	0.88
U568	18.45	20.9	0	0
U568	20.9	23.3	0.85	0.24
U568	23.3	24.85	1.6	0.1
U568	24.85	25.6	0.32	0.04
U568	25.6	26.85	1.6	0.02
U568	26.85	28.35	6.56	0.44
U568	28.35	28.61	27.6	0.12
U568	28.61	28.9	50.8	4
U568	28.9	30.49	0	0
U569	0	8.53	0	0
U569	8.53	9.95	0.29	1.14
U569	9.95	11.59	1.95	0.66
U569	11.59	12.5	0.15	2.84
U569	12.5	13	4.8	10.2
U569	13	13.5	1.45	0.95
U569	13.5	14.45	0.6	0.24
U569	14.45	16.4	0.66	0.44
U569	16.4	18.8	0.85	0.31
U569	18.8	19.9	0.9	0.44
U569	19.9	22.25	0.6	0.34
U569	22.25	23.1	0.82	2.02
U569	23.1	25	1.4	0.26
U569	25	26.05	1.31	0.16
U569	26.05	27.13	2.2	0.01
U569	27.13	28.65	0.64	0.04
U569	28.65	29.75	1.1	0.07
U569	29.75	31.7	0	0
U570	0	6.4	0	0
U570	6.4	7.55	0.39	0.39
U570	7.55	8.5	0.64	0.52
U570	8.5	10.37	2.6	1.39
U570	10.37	11.89	3.45	2.09
U570	11.89	12.99	1.45	1.74
U570	12.99	14.94	4.33	2.44
U570	14.94	16.46	3.2	0.09
U570	16.46	18.2	1.58	0.2
U570	18.2	19.18	6.4	0.12
U570	19.18	19.89	19.7	0.01
U570	19.89	20.11	40.7	0.01
U570	20.11	20.69	10.8	0.02
U570	20.69	21.03	3.05	0.11
U570	21.03	24.08	0	0
U571	0	3.9	0	0
U571	3.9	5.38	0.39	1.89
U571	5.38	6.54	0.61	0.37
U571	6.54	7.62	0.92	0.29
U571	7.62	8.82	1.8	0.42
U571	8.82	9.77	3.51	0.9
U571	9.77	10.72	7.6	0.08
U571	10.72	11.77	1.76	0.07
U571	11.77	13.72	0.2	0.01
U571	13.72	14.77	0.67	0.01
U571	14.77	15.35	4.85	1.33
U571	15.35	16.03	0.5	0.12
U571	16.03	16.76	3.8	0.01
U571	16.76	17.59	2.1	0.03
U571	17.59	19.13	0.9	0.1
U571	19.13	21.34	0	0
U572	0	0.25	0	0
U572	0.25	2.2	1.6	1.04
U572	2.2	2.9	5.1	8.2
U572	2.9	4	2.34	1.42
U572	4	4.7	5.22	6.5
U572	4.7	6.1	4.91	0.48
U572	6.1	7.62	3.73	0.31
U572	7.62	9.15	4.39	0.73
U572	9.15	11.75	1.73	0.06
U572	11.75	12.4	2.17	0.04
U572	12.4	13.05	4.11	0.1
U572	13.05	13.4	36.4	14.4
U572	13.4	14.94	0	0
U573	0	36.5	0	0
U573	36.5	37.9	1	0.05
U573	37.9	39.4	0.8	3.64
U573	39.4	40.3	6.3	9
U573	40.3	41.85	1.88	0.31
U573	41.85	42.82	11.9	9.3
U573	42.82	43.15	2.3	0.36
U573	43.15	45.42	0	0
U574	0	24.9	0	0
U574	24.9	27	0.21	0.68
U574	27	29.5	0.88	0.02
U574	29.5	32	4.3	0.33
U574	32	34.15	0.99	0.09
U574	34.15	36	0.47	0.23
U574	36	37.5	0.32	0.17
U574	37.5	39.4	0.39	0.94
U574	39.4	42.06	0	0
U575	0	26.88	0	0
U575	26.88	27.65	0.65	3.55
U575	27.65	28.35	0.17	0.38
U575	28.35	29.15	1.94	0.63
U575	29.15	30.79	2.47	0.36
U575	30.79	31.5	3.89	3.24
U575	31.5	32.61	5.61	11.3
U575	32.61	34	0.81	0.72
U575	34	35.97	0	0
U576	0	22.86	0	0
U576	22.86	24.2	0.42	0.04
U576	24.2	25.05	2	0.06
U576	25.05	25.91	0.5	0.48
U576	25.91	26.4	2.15	0.47
U576	26.4	27.43	0.35	0.55
U576	27.43	28.75	0.41	0.39
U576	28.75	29.15	1.38	1.9
U576	29.15	30.65	0.18	0.2
U576	30.65	32	0	0
U577	0	45.9	0	0
U577	45.9	46.9	0.33	1.73
U577	46.9	48.5	0.65	1.59
U577	48.5	50.05	1.9	0.68
U577	50.05	51.4	1.65	0.06
U577	51.4	52.5	3.16	0.12
U577	52.5	53.3	1.55	0.06
U577	53.3	55.17	0	0
U578	0	26.4	0	0
U578	26.4	27.85	3.76	0.05
U578	27.85	29.45	0.6	0.01
U578	29.45	30.35	0.81	0.13
U578	30.35	31.5	0.9	0.09
U578	31.5	33.15	1.1	0.33
U578	33.15	34.7	1.55	0.06
U578	34.7	36	4.88	0.49
U578	36	37	3.93	0.44
U578	37	37.9	1.17	0.49
U578	37.9	39.59	2	0.65
U578	39.59	41.76	0	0
U579	0	18	0	0
U579	18	18.59	0.75	0.01
U579	18.59	19.05	1.6	0.01
U579	19.05	19.9	1.38	0.05
U579	19.9	20.4	3	0.31
U579	20.4	22.35	0.75	0.01
U579	22.35	23.2	5.16	0.01
U579	23.2	24.4	2.5	0.01
U579	24.4	24.99	0.75	0.01
U579	24.99	29.3	0	0
U579	29.3	29.8	0.8	0.01
U579	29.8	30.3	8.6	0.01
U579	30.3	32.3	2.3	0.66
U579	32.3	33.65	0	0
U579	33.65	34.44	1.45	0.39
U579	34.44	35.15	2.28	0.7
U579	35.15	37.49	0	0
U583	0	1.25	1.15	0.1
U583	1.25	2.35	2.32	0.03
U583	2.35	3.05	2.7	0.06
U583	3.05	3.7	8	0.15
U583	3.7	4.15	1.98	0.32
U583	4.15	5.18	6.5	0.1
U583	5.18	6.18	9.4	0.08
U583	6.18	6.6	47.8	12.7
U583	6.6	8.23	0	0
U584	0	1.52	1.95	0.14
U584	1.52	3.05	1.72	0.25
U584	3.05	3.95	4.84	0.04
U584	3.95	4.7	9.8	0.2
U584	4.7	5.05	28.4	3.85
U584	5.05	6.1	0	0
U585	0	2.85	0	0
U585	2.85	3.35	1.82	2.26
U585	3.35	4.4	3.35	0.7
U585	4.4	5.7	6.2	2.06
U585	5.7	6.5	0.78	0.18
U585	6.5	9.14	0	0
U585	9.14	10.66	2.55	0.03
U585	10.66	12.19	4.08	1.1
U585	12.19	13.72	0	0
U586	0	3.35	0	0
U586	3.35	5.4	1.95	0.15
U586	5.4	7.6	0	0
U586	7.6	8.65	2.7	0.28
U586	8.65	9.75	0	0
U587	0	3	0	0
U587	3	3.66	1.1	0.18
U587	3.66	4.15	1.97	7.1
U587	4.15	4.55	1.12	0.31
U587	4.55	5.65	7.8	0.88
U587	5.65	6.2	1.58	0.06
U587	6.2	7.75	0	0
U587	7.75	8.45	0.9	0.1
U587	8.45	9	3.35	0.18
U587	9	9.5	17.8	1.4
U587	9.5	9.87	38.2	28.1
U587	9.87	11.28	0	0
U588	0	0.9	2.1	0.05
U588	0.9	1.5	1.28	0.05
U588	1.5	4.5	0	0
U588	4.5	5.1	2.4	0.04
U588	5.1	6.1	1.88	0.04
U588	6.1	7.35	2.8	0.15
U588	7.35	9.14	0	0
U589	0	1.15	2.3	0.1
U589	1.15	2.35	1.1	0.09
U589	2.35	3.75	1.38	0.18
U589	3.75	4.55	5.7	5.53
U589	4.55	5.22	32.6	20.1
U589	5.22	6.71	0	0
U590	0	0.55	6.6	4.24
U590	0.55	1	2.5	0.82
U590	1	1.85	11.2	0.39
U590	1.85	2.15	41	12.2
U590	2.15	3.96	0	0
U591	0	37.05	0	0
U591	37.05	38.4	2.1	0.16
U591	38.4	41.65	0	0
U591	41.65	42.55	1.19	0.04
U591	42.55	43.15	3.2	0.87
U591	43.15	45.05	6.6	7
U591	45.05	46.3	4.74	2.4
U591	46.3	46.81	4.6	0.31
U591	46.81	47.85	1.95	0.14
U591	47.85	49.2	4.47	0.29
U591	49.2	49.95	3.1	0.4
U591	49.95	51.5	1	0.05
U591	51.5	53.2	5.44	1.21
U591	53.2	53.95	4.85	0.15
U591	53.95	55.47	3.2	0.01
U591	55.47	57	4.67	0.04
U591	57	58.52	4.46	0.04
U591	58.52	60.05	2.4	0.24
U591	60.05	61.05	5.51	0.11
U591	61.05	61.4	39.9	0.38
U591	61.4	62.33	24.2	0.32
U591	62.33	65.53	0	0
U592	0	2.25	0	0
U592	2.25	3.3	1.1	0.37
U592	3.3	6.9	0	0
U592	6.9	7.62	1.2	0.27
U592	7.62	8.6	2.35	0.23
U592	8.6	9.53	2.97	1.01
U592	9.53	10.67	0.6	0.03
U592	10.67	25.07	0	0
U592	25.07	25.9	4.27	0.01
U592	25.9	27.35	2.85	0.02
U592	27.35	28.85	0	0
U592	28.85	29.7	1.98	0.01
U592	29.7	31.05	0	0
U592	31.05	32	1.35	0.01
U592	32	32.85	2.55	0.01
U592	32.85	34.1	6.7	0.11
U592	34.1	34.55	1.8	0.03
U592	34.55	36.58	0	0
U593	0	18	0	0
U593	18	18.9	3.84	1.6
U593	18.9	21.03	0	0
U593	21.03	22.1	0.5	0.06
U593	22.1	23.5	3.1	3.96
U593	23.5	24.44	2.45	0.1
U593	24.44	26.4	1.65	0.02
U593	26.4	32.78	0	0
U593	32.78	33.53	1.6	0.06
U593	33.53	35.05	1.25	0.13
U593	35.05	36.58	7.12	0.06

U593	36.58	36.85	14.35	0.01
U593	36.85	38	57.4	1.03
U593	38	40.23	0	0
U594	0	4.85	0	0
U594	4.85	6.3	1.3	0.01
U594	6.3	6.95	3.09	0.01
U594	6.95	7.43	15.3	5.58
U594	7.43	8.48	8.3	0.81
U594	8.48	9	0.75	0.01
U594	9	9.75	8.2	0.01
U594	9.75	11.05	0.48	0.01
U594	11.05	11.8	7.8	0.09
U594	11.8	12.7	0.42	0.04
U594	12.7	21.95	0	0
U594	21.95	23.95	2.38	0.16
U594	23.95	24.41	3.22	0.15
U594	24.41	27.13	0	0
U595	0	12.23	0	0
U595	12.23	13.05	5.53	0.73
U595	13.05	13.55	0.6	0.07
U595	13.55	18.1	0	0
U595	18.1	19.1	0.65	0.31
U595	19.1	20.73	4.27	0.09
U595	20.73	22.25	5.01	0.15
U595	22.25	24.45	2.81	0.34
U595	24.45	26.35	1.25	0.41
U595	26.35	26.72	2.87	4.44
U595	26.72	29.87	0	0
U596	0	12.85	0	0
U596	12.85	13.75	2.78	0.12
U596	13.75	14.6	3.7	0.02
U596	14.6	15.42	0.26	0.01
U596	15.42	16.05	7.8	0.73
U596	16.05	16.75	1.18	0.18
U596	16.75	17.05	12.7	0.11
U596	17.05	18.29	1.95	0.27
U596	18.29	19.05	3.24	2.01
U596	19.05	20.95	2.8	0.52
U596	20.95	28.96	0	0
U597	0	14.94	0	0
U597	14.94	16.45	0.75	1.2
U597	16.45	17.37	5.36	1.14
U597	17.37	19.1	2.75	0.28
U597	19.1	20	0.95	3.98
U597	20	20.95	29.4	33.6
U597	20.95	23.47	0	0
U598	0	8.03	0	0
U598	8.03	9.45	4.92	1.79
U598	9.45	10.35	8.8	0.84
U598	10.35	12.5	0	0
U599	0	9.3	0	0
U599	9.3	9.85	3.5	0.92
U599	9.85	11.05	7.14	4.18
U599	11.05	12	6.5	1.96
U599	12	12.7	9.7	4.96
U599	12.7	13.95	3.8	2.02
U599	13.95	14.3	6.95	2.12
U599	14.3	16.76	0	0
U600	0	4.7	0	0
U600	4.7	5.95	3.5	2.84
U600	5.95	6.95	7.1	2.43
U600	6.95	9.45	0	0
U601	0	42.98	0	0
U601	42.98	43.95	3.15	3.18
U601	43.95	45.75	1.95	2.14
U601	45.75	47.5	2.15	0.8
U601	47.5	49.25	1.57	2.44
U601	49.25	50.85	1.97	2.63
U601	50.85	52.37	9.8	0.82
U601	52.37	53.64	5.5	0.84
U601	53.64	54.65	14.6	0.84
U601	54.65	56	9.6	0.45
U601	56	57	6.27	0.33
U601	57	59.74	0	0
U602	0	22.77	0	0
U602	22.77	23.77	3	0.02
U602	23.77	25.11	2.35	0.02
U602	25.11	26.1	2.75	0.01
U602	26.1	26.7	1.05	0.01
U602	26.7	48.77	0	0
U603	0	47.55	0	0

U603	47.55	48.65	2.2	1.2
U603	48.65	49.4	1.38	1.49
U603	49.4	50.65	2.25	2.06
U603	50.65	51.3	2.15	6.84
U603	51.3	52.7	9.6	21.3
U603	52.7	53.5	2.8	7.58
U603	53.5	55.37	1.39	6.28
U603	55.37	56.75	3.5	8
U603	56.75	58.22	1.9	3.93
U603	58.22	59.64	5.26	4.05
U603	59.64	60.75	4.53	0.29
U603	60.75	62.58	2.7	3.1
U603	62.58	63.55	1.18	0.16
U603	63.55	65.86	5.33	0.63
U603	65.86	66.35	8	6.92
U603	66.35	67.4	2.4	3.09
U603	67.4	69.8	0	0
U604	0	16.46	0	0
U604	16.46	16.81	1	0.14
U604	16.81	17.81	3.22	0.33
U604	17.81	18.29	0.8	0.03
U604	18.29	46	0	0
U604	46	46.48	0.27	0.58
U604	46.48	47.01	1.18	0.39
U604	47.01	47.59	0.18	0.12
U604	47.59	51.2	0	0
U605	0	33.8	0	0
U605	33.8	35.35	3.82	0.08
U605	35.35	36.75	8.15	0.4
U605	36.75	38.4	4.74	0.1
U605	38.4	39.75	2	0.07
U605	39.75	41.45	2.12	0.06
U605	41.45	42.8	2.35	0.02
U605	42.8	44.3	0.6	0.1
U605	44.3	45.5	0.82	0.06
U605	45.5	46.24	2.35	3.48
U605	46.24	47.55	1.98	0.54
U605	47.55	49.68	3.5	0.05
U605	49.68	50.9	1.53	0.23
U605	50.9	51.75	0.95	0.02
U605	51.75	53.4	0.35	0.03
U605	53.4	54.65	0.19	0.04
U605	54.65	56.17	0.13	0.04
U605	56.17	57.3	0.03	0.07
U605	57.3	59.75	0.85	0.04
U605	59.75	60.35	1.08	0.07
U605	60.35	61.87	0	0
U606	0	16.58	0	0
U606	16.58	18.31	2.05	0.02
U606	18.31	19.7	1.75	0.17
U606	19.7	20.73	1.25	0.01
U606	20.73	22.55	1.23	0.04
U606	22.55	24.05	1.2	0.04
U606	24.05	25.6	0.69	0.12
U606	25.6	26	2.4	0.25
U606	26	26.85	0	0
U607	0	29.26	0	0
U607	29.26	30.35	1.38	2.81
U607	30.35	30.98	0.19	0.75
U607	30.98	32.31	3.2	0.64
U607	32.31	33.83	23.8	6.39
U607	33.83	35.07	10.3	0.14
U607	35.07	36.88	0	0
U608	0	19.93	0	0
U608	19.93	21.33	0.43	0.03
U608	21.33	22.86	2.1	0.02
U608	22.86	24.69	1.4	0.01
U608	24.69	26.21	1.48	0.12
U608	26.21	27.74	1.1	0.56
U608	27.74	29.26	1.5	0.79
U608	29.26	30.78	4.65	0.45
U608	30.78	31.28	11.7	2.06
U608	31.28	32.61	0	0
U609	0	32.21	0	0
U609	32.21	33.21	4.94	0.29
U609	33.21	35.05	2.15	0.18
U609	35.05	36.07	1.22	0.95
U609	36.07	37.5	4.69	0.36
U609	37.5	38.1	5.4	0.43
U609	38.1	38.88	12.2	0.09
U609	38.88	40.9	11.5	0.51

U609	40.9	41	26.6	2.85
U609	41	44.19	0	0
U610	0	30.22	0	0
U610	30.22	31.5	1.8	0.12
U610	31.5	32.5	2.7	0.12
U610	32.5	33.83	2.84	0.13
U610	33.83	35	4.54	0.12
U610	35	36.5	5	0.05
U610	36.5	36.88	13	9.4
U610	36.88	38.4	0	0
U611	0	41.77	0	0
U611	41.77	42.97	1.98	0.35
U611	42.97	44.27	5.51	0.99
U611	44.27	45.52	7.6	0.2
U611	45.52	46.02	9.8	0.64
U611	46.02	46.92	10.8	0.27
U611	46.92	48.2	9.8	5.6
U611	48.2	50.59	0	0
U612	0	27.53	0	0
U612	27.53	28.95	1.03	0.02
U612	28.95	30.17	0.63	0.03
U612	30.17	32	1.08	0.44
U612	32	33.15	0.88	0.15
U612	33.15	34.75	0.8	0.04
U612	34.75	36.07	0.73	0.01
U612	36.07	37.79	0.75	0.01
U612	37.79	39.33	1.56	0.04
U612	39.33	39.93	0.72	0.36
U612	39.93	41.45	0	0
U613A	0	38.4	0	0
U613A	38.4	39.7	2.11	0.08
U613A	39.7	40.6	1.13	0.12
U613A	40.6	42	11.8	1.02
U613A	42	44.5	0	0
U614	0	21.95	0	0
U614	21.95	23.4	1.98	0.53
U614	23.4	24.99	2.15	0.05
U614	24.99	26.29	3.74	0.35
U614	26.29	27.6	1.54	0.14
U614	27.6	29.06	2.53	0.01
U614	29.06	30.4	2.9	0.02
U614	30.4	31.82	1.6	0.01
U614	31.82	33.38	0.95	0.07
U614	33.38	34.78	1.15	0.01
U614	34.78	36.25	0.4	0.04
U614	36.25	37.63	0.24	0.12
U614	37.63	40.23	0.56	0.04
U614	40.23	40.43	1.38	0.08
U614	40.43	41.76	0	0
U615	0	40.7	0	0
U615	40.7	41.3	1.75	0.03
U615	41.3	42.98	1.5	0.57
U615	42.98	43.78	4.8	7.6
U615	43.78	45.65	4.2	3.48
U615	45.65	46.8	0.78	0.36
U615	46.8	48.62	4.1	1.94
U615	48.62	49.33	0.62	0.06
U615	49.33	53.2	0	0
U615	53.2	53.85	1.08	0.01
U615	53.85	54.71	9.7	5.98
U615	54.71	55.47	0.68	0.08
U615	55.47	59.8	0	0
U615	59.8	61.26	2	0.08
U615	61.26	61.95	7.3	0.08
U615	61.95	64.31	0.68	0.02
U615	64.31	65.2	14.1	0.87
U615	65.2	67.36	0	0
U616	0	49.35	0	0
U616	49.35	50.6	0.55	1.57
U616	50.6	52.12	0.6	1
U616	52.12	53.1	1.85	0.04
U616	53.1	53.64	0.58	0.34
U616	53.64	55.1	0	0
U616	55.1	56.5	1.32	2.52
U616	56.5	59.74	0	0
U616	59.74	60.35	5.52	2.23
U616	60.35	61	4.1	0.45
U616	61	61.75	3.8	3.51
U616	61.75	62.79	3.9	0.92
U616	62.79	63.9	6.37	4.66
U616	63.9	64.55	1.03	0.47

U616	64.55	67.44	0	0
U616	67.44	67.85	8.3	1.61
U616	67.85	70.7	0	0
U616	70.7	71.3	1.22	10.1
U616	71.3	74.98	0	0
U616	74.98	77.33	0.93	0.28
U616	77.33	78.4	0.89	0.17
U616	78.4	82.3	0	0
U617	0	26.53	0	0
U617	26.53	27.03	0.6	0.16
U617	27.03	28.75	4.65	0.06
U617	28.75	29.8	12.2	1.44
U617	29.8	30.2	24.8	2.86
U617	30.2	32.31	0	0
U618	0	13.55	0	0
U618	13.55	15.05	9.2	0.57
U618	15.05	15.53	22.9	0.54
U618	15.53	16.35	4.92	0.1
U618	16.35	18.29	0	0
U619	0	29.2	0	0
U619	29.2	29.78	2.2	0.28
U619	29.78	30.07	10.4	1.68
U619	30.07	30.4	0.92	3.64
U619	30.4	35.37	0	0
U620	0	12.5	0	0
U620	12.5	13.35	0.13	0.05
U620	13.35	14.55	0.02	0.15
U620	14.55	14.94	1.06	27.1
U620	14.94	15.24	0.48	3.68
U620	15.24	17.43	0	0
U620	17.43	18.03	0.04	0.08
U620	18.03	18.52	0.92	0.12
U620	18.52	19.3	3.4	0.42
U620	19.3	20.11	6.27	0.16
U620	20.11	20.98	6.76	5.26
U620	20.98	21.3	15.6	0.57
U620	21.3	21.72	32.1	2.67
U620	21.72	22.2	51	8.75
U620	22.2	22.7	19.6	52
U620	22.7	26.22	1.8	3.14
U621	0	34.5	0	0
U621	34.5	35.5	3.3	0.33
U621	35.5	36.72	2.8	0.42
U621	36.72	38.26	4.24	0.32
U621	38.26	39.88	3.3	0.52
U621	39.88	40.3	9.8	69.5
U621	40.3	41.05	49	15.1
U621	41.05	42.35	12.1	66.7
U621	42.35	45.72	0	0
U622	0	21.1	0	0
U622	21.1	22.2	0.97	2.7
U622	22.2	23.8	3.3	14.2
U622	23.8	24.77	2.55	0.62
U622	24.77	25.5	11.7	1.02
U622	25.5	26.96	51.3	9.8
U622	26.96	29.26	0	0
U623	0	47.9	0	0
U623	47.9	48.93	6.53	2.82
U623	48.93	49.63	10.4	9.54
U623	49.63	49.84	39.5	12.8
U623	49.84	53.34	0	0
U624	0	26.5	0	0
U624	26.5	27.15	1.12	1.54
U624	27.15	28.54	4.01	4.74
U624	28.54	29.36	4.55	8.1
U624	29.36	31.09	1.96	2.54
U624	31.09	31.67	8.3	0.5
U624	31.67	32.07	32.6	27.7
U624	32.07	35.05	0	0
U625	0	35.9	0	0
U625	35.9	37.42	0.48	4.12
U625	37.42	37.98	0.06	0.16
U625	37.98	39.28	0.68	1.51
U625	39.28	40.7	0.03	0.05
U625	40.7	41.37	3.18	1.04
U625	41.37	41.89	5.96	6.48
U625	41.89	42.13	14.3	24.1
U625	42.13	46.33	0	0
U626	0	28.95	0	0
U626	28.95	29.25	3.63	2.22
U626	29.25	30	0.5	0.47

U626	30	30.32	3.9	8.6
U626	30.32	31.4	3.42	3.84
U626	31.4	31.93	8.3	14.6
U626	31.93	32.39	10.8	4.24
U626	32.39	33.02	3.53	1.03
U626	33.02	33.72	22	30.5
U626	33.72	36.59	0	0
U627	0	23.55	0	0
U627	23.55	24.15	1.69	2.16
U627	24.15	25.16	1.31	1.31
U627	25.16	25.6	1.76	1.27
U627	25.6	26.15	7.45	10.2
U627	26.15	26.44	0.01	0.01
U627	26.44	27.46	1.5	6.76
U627	27.46	30.48	0	0
U628	0	12	0	0
U628	12	13.39	0.9	1.38
U628	13.39	14.54	0.95	0.92
U628	14.54	15.8	3.85	1.32
U628	15.8	16.31	8.3	5.56
U628	16.31	17.13	4.4	2.54
U628	17.13	17.91	7.6	11
U628	17.91	18.65	13.6	58.4
U628	18.65	21.34	0	0
U629	0	27.01	0	0
U629	27.01	28.18	1.8	4.08
U629	28.18	28.84	3.77	2.2
U629	28.84	29.45	4.2	1.96
U629	29.45	32.01	0	0
U630	0	12.25	0	0
U630	12.25	13.45	0.75	1.08
U630	13.45	14.63	0.85	0.95
U630	14.63	16	4.13	2.71
U630	16	17.68	4.31	1.7
U630	17.68	18.76	8.4	69.2
U630	18.76	21.34	0	0
U631	0	41.8	0	0
U631	41.8	42.2	0.65	1.55
U631	42.2	42.65	3.04	2.02
U631	42.65	43.04	11.1	5.18
U631	43.04	43.32	0.48	0.31
U631	43.32	46.64	0	0
U632	0	24.7	0	0
U632	24.7	25.45	5.87	3.62
U632	25.45	26.09	13.3	0.93
U632	26.09	26.66	23.2	40.4
U632	26.66	29.27	0	0
U633	0	45.6	0	0
U633	45.6	46.79	7.24	5.48
U633	46.79	48.78	0.88	0.98
U634	0	26.85	0	0
U634	26.85	27.75	1.44	2.85
U634	27.75	28.51	2.5	0.15
U634	28.51	29.23	19.4	0.87
U634	29.23	29.38	0.84	0.19
U635	0	50.2	0	0
U635	50.2	52.12	4.04	1.35
U635	52.12	52.53	0.25	0.11
U635	52.53	53.11	7.27	7.28
U635	53.11	53.5	27.2	46.3
U635	53.5	55.17	0	0
U636	0	96.15	0	0
U636	96.15	98.42	0.12	0.27
U636	98.42	101.5	0	0
U637	0	66.35	0	0
U637	66.35	67.2	5.42	11.9
U637	67.2	68.28	6	4.48
U637	68.28	68.77	3.4	21.4
U637	68.77	71.32	0	0
U638	0	63.67	0	0
U638	63.67	64.28	4.4	11.5
U638	64.28	64.83	0.75	0.95
U638	64.83	65.3	9.29	6.9
U638	65.3	65.64	5.4	52.3
U638	65.64	67.67	0	0
U639	0	45	0	0
U639	45	46.6	6	2.5
U639	46.6	47.35	35	35
U639	47.35	49.09	0	0
U640	0	31.13	0	0
U640	31.13	32.85	3.88	1.73
U640	32.85	33.82	4.75	2.32
U640	33.82	34.52	49.3	3.17
U640	34.52	37.19	0	0
U641	0	29	0	0
U641	29	30	3.26	1.02
U641	30	31	1.2	0.4
U641	31	31.8	3.38	0.3
U641	31.8	32.45	7.56	3.26
U641	32.45	33	3.26	0.19
U641	33	34	3.61	0.49
U641	34	35	3.45	0.37
U641	35	36	5.88	2.54
U641	36	37.1	1.9	0.6
U641	37.1	38.85	3.2	4.32
U641	38.85	40.54	0	0
U642	0	7.28	0	0
U642	7.28	8.2	1.33	0.18
U642	8.2	9.02	2.03	0.65
U642	9.02	10.6	0.83	0.51
U642	10.6	12.46	1.5	0.78
U642	12.46	12.8	0	0
U642	12.8	13.56	4.18	2.12
U642	13.56	15.6	0.18	0.43
U642	15.6	16.4	0.74	2.12
U642	16.4	18.4	0.77	1.87
U642	18.4	20.4	1.27	11.5
U642	20.4	22.4	1.48	2.64
U642	22.4	23.87	0.64	1.3
U642	23.87	24.78	1.19	1.47
U642	24.78	26.85	0.1	0.52
U642	26.85	29.2	0.11	0.45
U642	29.2	31.6	0.03	0.15
U642	31.6	32.43	0.03	0.73
U642	32.43	33.53	1.03	2.66
U642	33.53	34.45	0.04	0.17
U642	34.45	40.54	0	0
U643	0	2.5	0	0
U643	2.5	3.35	3.53	13.1
U643	3.35	4	2.4	3.76
U643	4	5	2.28	4.82
U643	5	6	2.1	2.66
U643	6	7	2.5	1.65
U643	7	8	2.57	0.25
U643	8	9	1.9	0.45
U643	9	10	1.6	0.09
U643	10	10.7	3.36	1.15
U643	10.7	12.05	11	10.1
U643	12.05	13	0.32	1.27
U643	13	14	0.95	0.21
U643	14	15	3.33	0.48
U643	15	19.2	0	0
U644	0	10.5	0	0
U644	10.5	12.25	1.81	2.43
U644	12.25	13.02	0.89	3.08
U644	13.02	13.96	0	0
U644	13.96	15.14	0.61	4.28
U644	15.14	16.74	0.74	2.8
U644	16.74	18.8	2.38	2.47
U644	18.8	20.12	2.5	1.75
U644	20.12	20.46	3.9	3.12
U644	20.46	20.73	5.06	11.39
U644	20.73	21.42	3	2.8
U644	21.42	21.95	10	4.23
U644	21.95	23.9	9.1	15.15
U644	23.9	25.06	8.92	14.74
U644	25.06	25.3	12.7	9.8
U644	25.3	26.4	2.48	1.04
U644	26.4	28.04	0	0
U645	0	32.9	0	0
U645	32.9	33.7	2.22	1.5
U645	33.7	34.62	14.02	10.05
U645	34.62	35.16	39.2	0.97
U645	35.16	37.49	0	0
U646	0	34.35	0	0
U646	34.35	34.99	5.07	0.76
U646	34.99	35.62	17.44	1.46
U646	35.62	36.25	0.54	0.23
U646	36.25	38.71	0	0
U647	0	36.38	0	0
U647	36.38	36.9	3.24	0.39
U647	36.9	37.4	17	6.54
U647	37.4	37.8	4.36	5.52
U647	37.8	41.76	0	0
U648	0	34.75	0	0
U648	34.75	35.35	11.04	1.85
U648	35.35	36.26	16.54	14.09
U648	36.26	39.62	0	0
U649	0	35.8	0	0
U649	35.8	36.35	11.2	5.72
U649	36.35	36.72	4.48	8.66
U649	36.72	38.1	0	0
U650	0	42.2	0	0
U650	42.2	43.32	21.34	8.21
U650	43.32	45.11	0	0
U651	0	0.96	2	2.04
U651	0.96	2.9	5.14	5.7
U651	2.9	3.52	18.36	14.04
U651	3.52	9.14	0	0