# DCMIP2016, Part 3: Idealized Tropical Cyclone

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**Abstract.** This paper discusses a new idealized test for atmospheric dynamical cores.

### 1 Introduction

The simplified tropical cyclone test case on a regular-size Earth is based on the work of Reed and Jablonowski (2012, 2011a, c, b). In this test an analytic vortex is initialized in a background environment which is tractable to a rapid intensification of tropical cyclones.

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Table 1. List of constants used for the Ideaized Tropical Cyclone test

| Constant       | Value                        | Description   |
|----------------|------------------------------|---|
| $\overline{X}$ | 1                            | small-planet scaling factor (regular-size Earth)              |
| $z_t$          | 15000 m                      | Tropopause height   |
| $q_0$          | 0.021 kg/kg                  | Maximum specific humidity amplitude                           |
| $q_t$          | $10^{-11} \text{ kg/kg}$     | Specific humidity in the upper atmosphere                     |
| $T_0$          | $302.15~{ m K}$              | Surface temperature of the air                                |
| $T_s$          | $302.15~{ m K}$              | Sea surface temperature (SST), 29 C°                          |
| $z_{q1}$       | 3000 m                       | Height related to the linear decrease of $q$ with height      |
| $z_{q2}$       | 8000 m                       | Height related to the quadratic decrease of $q$ with height   |
| Γ              | $0.007~{\rm K}~{\rm m}^{-1}$ | Virtual temperature lapse rate                                |
| $p_b$          | 1015 hPa                     | Background surface pressure                                   |
| $arphi_c$      | $\pi/18$                     | Initial latitude of vortex center (radians)                   |
| $\lambda_c$    | $\pi$                        | Initial longitude of vortex center (radians)                  |
| $\Delta p$     | 11.15 hPa                    | Pressure perturbation at vortex center                        |
| $r_p$          | 282000 m                     | Horizontal half-width of pressure perturbation                |
| $z_p$          | 7000 m                       | Height related to the vertical decay rate of $p$ perturbation |
| $\epsilon$     | $10^{-25}$                   | Small threshold value   |

### 1.1 Initialization

The background state consists of a prescribed specific humidity profile, virtual temperature and pressure profile. The initial profile is defined to be in approximate gradient wind balance. The vertical sounding is chosen to roughly match an observed tropical sounding documented in Jordan (1958). The background specific humidity profile  $\bar{q}(z)$  as a function of height z is

$$\overline{q}(z) = q_0 \exp\left(-\frac{z}{z_{q1}}\right) \exp\left[-\left(\frac{z}{z_{q2}}\right)^2\right] \quad \text{for } 0 \le z \le z_t$$

$$\overline{q}(z) = q_t \quad \text{for } z_t \le z \tag{1}$$

The background virtual temperature sounding  $\overline{T}_v(z)$  is split into two different representations for the lower and upper atmosphere. It is given by

$$\overline{T}_v(z) = T_{v0} - \Gamma z \qquad \text{for } 0 \le z \le z_t,$$

$$\overline{T}_v(z) = T_{vt} = T_{v0} - \Gamma z_t \quad \text{for } z_t < z,$$
(2)

with the virtual temperature at the surface  $T_{v0} = T_0(1 + 0.608 q_0)$  and the virtual temperature at the tropopause level  $T_{vt} = T_{v0} - \Gamma z_t$ . The background temperature profile can be obtained from (??).

The background vertical pressure profile  $\overline{p}(z)$  of the moist air is computed using the hydrostatic balance and (2). The profile is given by:

$$\overline{p}(z) = p_b \left(\frac{T_{v0} - \Gamma z}{T_{v0}}\right)^{g/R_d \Gamma} \quad \text{for } 0 \le z \le z_t, 
\overline{p}(z) = p_t \exp\left(\frac{g(z_t - z)}{R_d T_{vt}}\right) \quad \text{for } z_t < z.$$
(3)

The pressure at the tropopause level  $z_t$  is continuous and given by

$$p_t = p_b \left(\frac{T_{vt}}{T_{v0}}\right)^{\frac{g}{R_d\Gamma}},\tag{4}$$

which, for the given set of parameters, is approximately 130.5 hPa.

# 1.1.1 Axisymmetric Vortex

The pressure equation p(r,z) for the moist air is comprised of the background pressure profile (3) plus a 2D pressure perturbation p'(r,z),

$$p(r,z) = \overline{p}(z) + p'(r,z), \tag{5}$$

where r symbolizes the radial distance (or radius) to the center of the prescribed vortex. On the sphere r is defined using the great circle distance

$$r = a\arccos(\sin\varphi_c\sin\varphi + \cos\varphi_c\cos\varphi\cos(\lambda - \lambda_c)). \tag{6}$$

15 The perturbation pressure is defined as

$$p'(r,z) = -\Delta p \exp\left[-\left(\frac{r}{r_p}\right)^{3/2} - \left(\frac{z}{z_p}\right)^2\right] \left(\frac{T_{v0} - \Gamma z}{T_{v0}}\right)^{\frac{g}{R_d \Gamma}}$$
 for  $0 \le z \le z_t$ ,
$$p'(r,z) = 0$$
 for  $z_t < z$ . (7)

The pressure perturbation depends on the pressure difference  $\Delta p$  between the background surface pressure  $p_b$  and the pressure at the center of the initial vortex, the pressure change in the radial direction  $r_p$  and the pressure decay with height within the vortex  $z_p$ . The moist surface pressure  $p_s(r)$  is computed by setting z = 0 m in (5), which gives

$$p_s(r) = p_b - \Delta p \exp\left[-\left(\frac{r}{r_p}\right)^{3/2}\right]. \tag{8}$$

The axisymmetric virtual temperature  $T_v(r,z)$  is computed using the hydrostatic equation and ideal gas law

$$T_v(r,z) = -\frac{gp(r,z)}{R_d} \left(\frac{\partial p(r,z)}{\partial z}\right)^{-1}.$$
(9)

Again it can be written as a sum of the background state and a perturbation,

$$T_v(r,z) = \overline{T}_v(z) + T_v'(r,z), \tag{10}$$

where the virtual temperature perturbation is defined as

The axisymmetric specific humidity q(r,z) is set to the background profile everywhere

$$q(r,z) = \overline{q}(z). \tag{12}$$

Consequently, the temperature can be written as

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$$T(r,z) = \overline{T}(z) + T'(r,z),$$
 (13)

with the temperature perturbation

$$T'(r,z) = \frac{T_{v0} - \Gamma z}{1 + 0.608\overline{q}(z)} \left\{ \left[ 1 + \frac{2R_d(T_{v0} - \Gamma z)z}{gz_p^2 \left[ 1 - \frac{p_b}{\Delta p} \exp\left(\left(\frac{r}{r_p}\right)^{3/2} + \left(\frac{z}{z_p}\right)^2\right) \right]} \right]^{-1} - 1 \right\}$$
 for  $0 \le z \le z_t$ ,
$$T'(r,z) = 0$$
 for  $z_t < z$ . (14)

Due to the small specific humidity value in the upper atmosphere ( $10^{-11}$  kg/kg for  $z > z_t$ ) the virtual temperature equals the temperature to a very good approximation in this region. The formulation presented here is equivalent to the one presented in Reed and Jablonowski (2012).

If the density of the moist air needs to be initialized its formulation is based on the ideal gas law

$$\rho(r,z) = \frac{p(r,z)}{R_d T_v(r,z)} \tag{15}$$

which utilizes the moist pressure (5) and virtual temperature (10). The surface elevation  $z_s$  and thereby the surface geopotential  $\Phi_s = gz_s$  are set to zero.

Finally, the tangential velocity field  $v_T(r,z)$  of the axisymmetric vortex is defined by utilizing the gradient-wind balance, which depends on the pressure (5) and the virtual temperature (11). The tangential velocity is given by

$$v_T(r,z) = -\frac{f_c r}{2} + \sqrt{\frac{f_c^2 r^2}{4} + \frac{R_d T_v(r,z) r}{p(r,z)} \frac{\partial p(r,z)}{\partial r}},$$
(16)

where  $f_c = 2\Omega\sin(\varphi_c)$  is the Coriolis parameter at the constant latitude  $\varphi_c$ . Substituting  $T_v(r,z)$  and p(r,z) into (16) gives

$$v_{T}(r,z) = -\frac{f_{c}r}{2} + \sqrt{\frac{f_{c}^{2}r^{2}}{4} - \frac{\frac{3}{2}\left(\frac{r}{r_{p}}\right)^{3/2}(T_{v0} - \Gamma z)R_{d}}{1 + \frac{2R_{d}(T_{v0} - \Gamma z)z}{gz_{p}^{2}} - \frac{p_{b}}{\Delta p}\exp\left(\left(\frac{r}{r_{p}}\right)^{3/2} + \left(\frac{z}{z_{p}}\right)^{2}\right)}}$$
 for  $0 \le z \le z_{t}$ ,
$$v_{T}(r,z) = 0$$
 for  $z_{t} < z$ . (17)

The last step is to split the tangential velocity (17) into its zonal and meridional wind components  $u(\lambda, \varphi, z)$  and  $v(\lambda, \varphi, z)$ . Similar to Nair and Jablonowski (2008) these are computed using the following expressions,

$$d_1 = \sin \varphi_c \cos \varphi - \cos \varphi_c \sin \varphi \cos(\lambda - \lambda_c) \tag{18}$$

$$d_2 = \cos \varphi_c \sin(\lambda - \lambda_c) \tag{19}$$

$$d = \max\left(\epsilon, \sqrt{d_1^2 + d_2^2}\right),\tag{20}$$

10 which are utilized in the projections

$$u(\lambda, \varphi, z) = \frac{v_T(\lambda, \varphi, z) d_1}{d} \tag{21}$$

$$v(\lambda, \varphi, z) = \frac{v_T(\lambda, \varphi, z) d_2}{d}. \tag{22}$$

A small  $\epsilon=10^{-25}$  value avoids divisions by zero. The vertical velocity is set to zero.

**Note:** We are currently investigating a test case specification that places the idealized tropical cyclone on an f-plane. This configuration would remove issues associated with  $\beta$  drift of the cyclone and allow for a more direct intercomparison of the simulated storm.

# 1.2 Grid spacings, simulation time, output and diagnostics

- Moist simulations should be performed at 0.5° resolution with 30 vertical levels for 10 days.
- Plots of minimum surface pressure over the duration of the simulation.
- Experiments could address the coupling frequency between the dynamics and physics.
- A variable resolution simulation should be performed that (a) studies the effect of the tropical cyclone transitioning from fine resolution to coarse resolution and (b) high resolution simulations down to 0.125° over the tropical cyclone.

### 2 Conclusions

**TEXT** 

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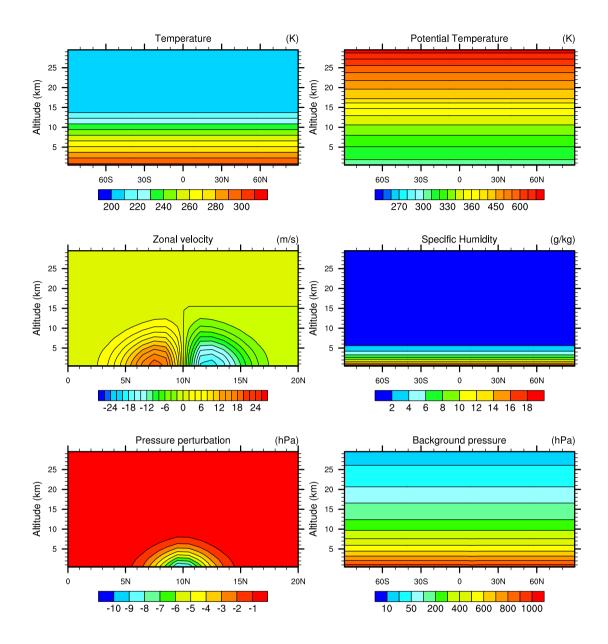


Figure 1. Initial state for the tropical cyclone test.

## Appendix A: Alternative Planetary Boundary Layer for Tropical Cyclone Test

An alternative approach for boundary layer mixing has been proposed using a K-profile parameterization formulation for the tropical cyclone test described in Section ??. The implementation only impacts the manner in which the eddy diffusivity coefficients are calculated. In particular the calculation of  $K_m$  in (??) is replaced with

$$K_m = \kappa u^* z \left(1 - \frac{z}{h}\right)^2 \quad \text{for } z \le h$$

$$K_m = 0 \qquad \qquad \text{for } z > h,$$
(A1)

where  $\kappa = 0.4$ ,  $u^* = \sqrt{C_d} |v_a|$  and h = 1 km.  $K_E$  in (??) is then defined as

$$K_E = \kappa e^* z \left(1 - \frac{z}{h}\right)^2 \quad \text{for } z \le h$$

$$K_E = 0 \qquad \text{for } z > h,$$
(A2)

where  $e^* = \sqrt{C_E} |v_a|$ . This implementation will be used in supplemental simulations of the tropical cyclone test.

10 Author contributions. TEXT

Acknowledgements. [Include a complete list of DCMIP2016 student participants here along with sponsors]

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