

## PhD Thesis Defense

# Multiphysic Modeling of Second Generation Magnetolectric Materials: Application to Connected Objects

Tuan Anh DO

November 04, 2019

Thesis directors: Zhuoxiang Ren

Hakeim Talleb

Supervisor : Aurélie Gensbittel

## 1 Introduction

- Motivation

## 2 Modeling

- Static analysis
- Dynamic analysis

## 3 Laminate

- Laminate composite with circular section
- Laminate composite with rectangular section

## 4 Homogenization

- Context
- Fiber composite
- Particulate composite

## 5 Conclusion

## 1 Introduction

- Motivation

## 2 Modeling

- Static analysis
- Dynamic analysis

## 3 Laminate

- Laminate composite with circular section
- Laminate composite with rectangular section

## 4 Homogenization

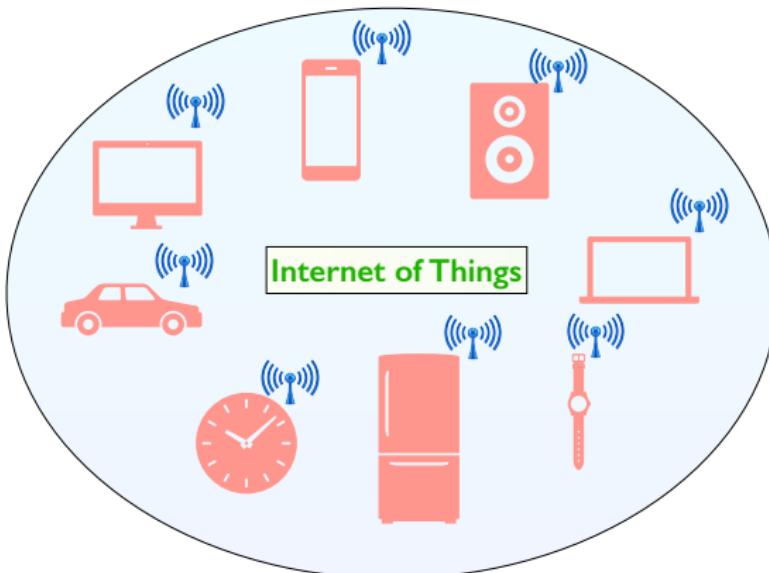
- Context
- Fiber composite
- Particulate composite

## 5 Conclusion

# Motivation

## Internet of Things

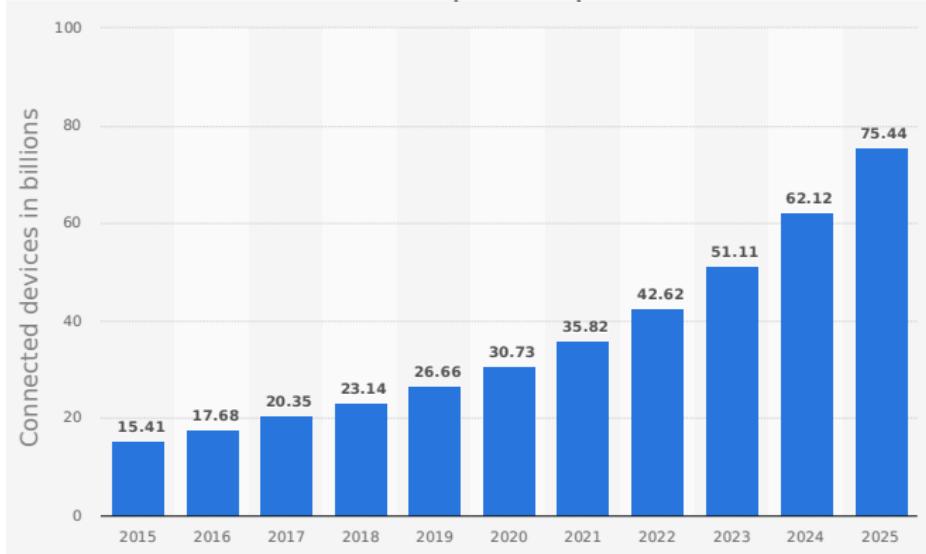
The internet doesn't just connect and distribute information, it can feel and intelligently respond.



- More efficient water supply
- Improved public safety
- Energy-efficient buildings
- Digitised healthcare system

# Motivation

## The evolution of IoTs



More devices



More power requirement

IHS forecast. *IoT platforms: enabling the Internet of Things.* March 2016.

## Battery as power

- Replacement difficulty.
- Need cable for charging.

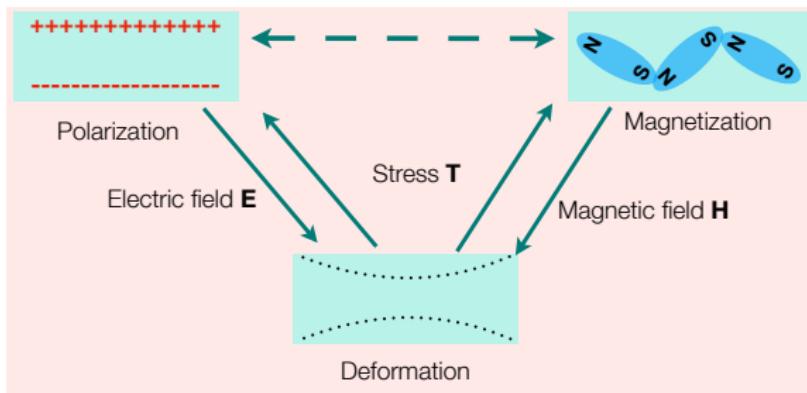
## Magnetoelectric materials

- Energy harvesting.
- Profit electromagnetic sources.

# Magnetoelectric (ME) effect

## Definition

Magnetization induced by an electric field or polarization induced by a magnetic field.



## ME coefficient

Static regime:

$$\alpha_V = \frac{V}{H}$$

Dynamic regime:

$$\tilde{\alpha}_V = \frac{\Delta V}{\Delta H}$$

## ME composite

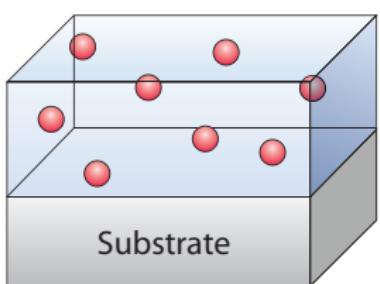
Magnetostrictive  
material



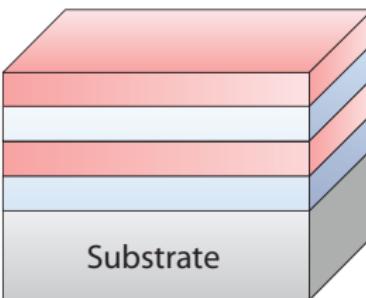
Piezoelectric material

# ME composite

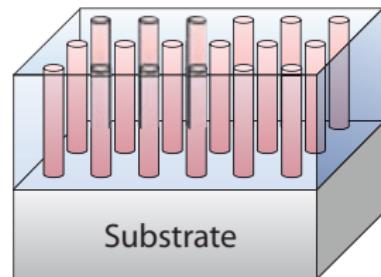
## Three type of ME composite



0 - 3 type particulate composite



2 - 2 type laminate composite

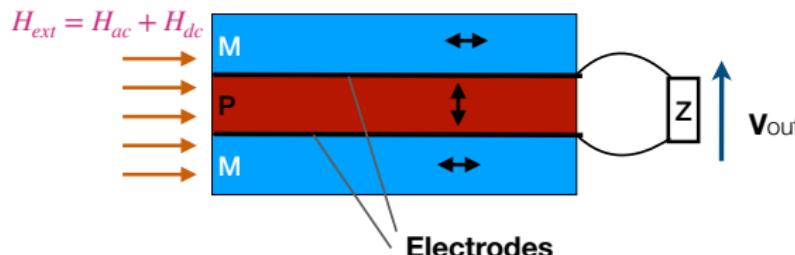


1 - 3 type fiber composite

Wang, Yao, et al. *Multiferroic magnetoelectric composite nanostructures*. NPG Asia Materials 2.2 (2010): 61.

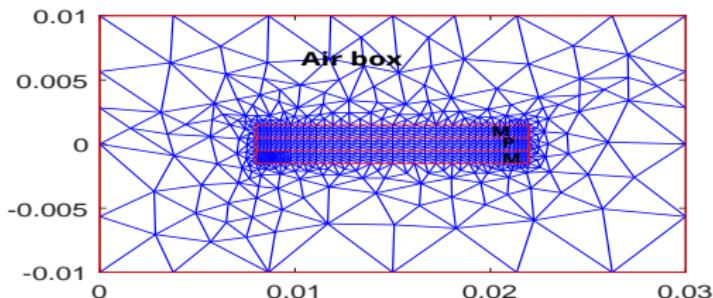
# Energy harvesting

## Working principle

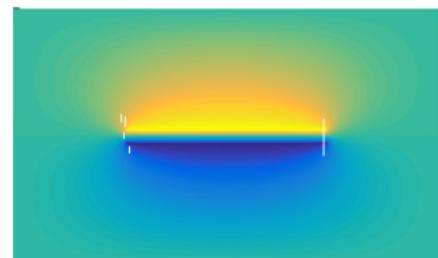


- Cochlear implant
- Artificial pacemaker
- Insulin pump

## 2D model

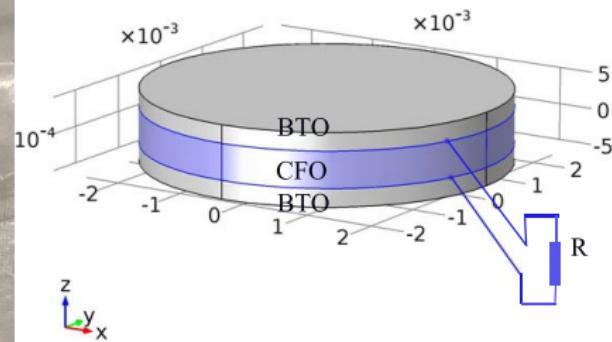


## Electric potential



*Condition: Laminate composites under the plane strain or stress state.*

3D model is needed



## Thesis works

- Develop a 3D FEM to consider complex structure.
- Analyze laminate composite( circular section, rectangular section), novel structure.
- Investigate different type: particulate composite and fiber composite.

## 1 Introduction

- Motivation

## 2 Modeling

- Static analysis
- Dynamic analysis

## 3 Laminate

- Laminate composite with circular section
- Laminate composite with rectangular section

## 4 Homogenization

- Context
- Fiber composite
- Particulate composite

## 5 Conclusion

# Problem description

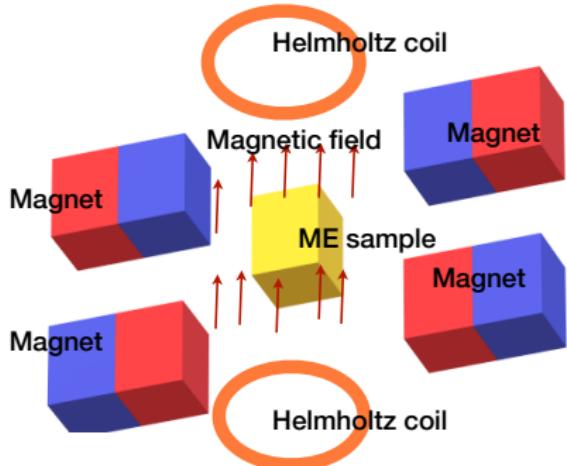
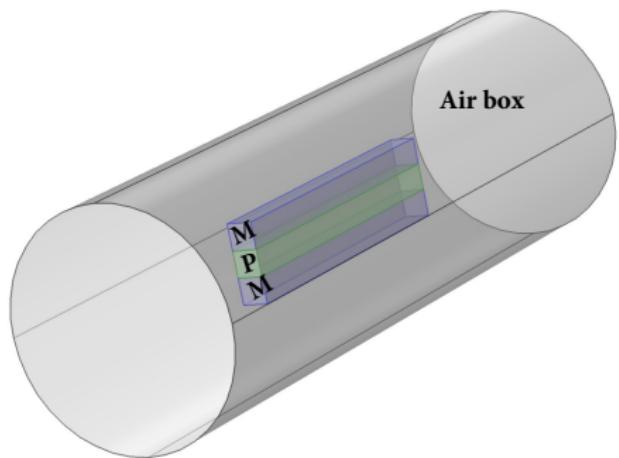


Illustration of ME measurement



3D model

Magnetic Field → Electric potential distribution

# General equations

## Physical equations

- Elastic equilibrium

$$\operatorname{div} \mathbf{T} + \mathbf{f} = 0$$

- Ampere's law

$$\operatorname{curl} \mathbf{H} = \mathbf{J}$$

- Gauss's law

$$\operatorname{div} \mathbf{D} = \rho_v$$

## Constitutive laws

$$\begin{cases} \mathbf{T} = c\mathbf{S} - e^t \mathbf{E} - h^t \mathbf{B} \\ \mathbf{H} = -h\mathbf{S} + \nu \mathbf{B} \\ \mathbf{D} = -e\mathbf{S} + \epsilon \mathbf{E} \end{cases}$$

## Introduce state variables

$$\begin{cases} \mathbf{S} = \frac{1}{2}(\nabla + \nabla^t) \mathbf{u} \\ \mathbf{B} = \nabla \times \mathbf{a} \\ \mathbf{E} = \nabla V \end{cases}$$

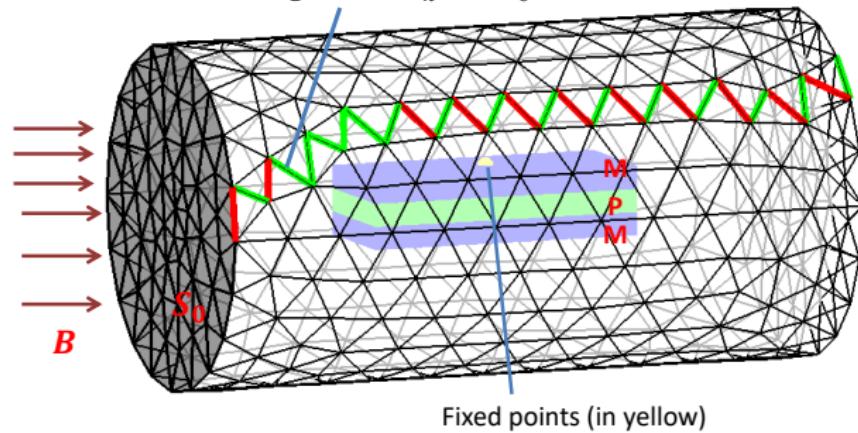
# Static analysis

$$[\mathbb{K}]\{X\} = [F]$$

- $[\mathbb{K}] = \begin{bmatrix} K_{uu} & -K_{au}^t & K_{vu}^t \\ -K_{au} & K_{aa} & 0 \\ K_{vu} & 0 & -K_{vv} \end{bmatrix}$
- $\{X\} = \{u, a, V\}^t$
- $[F] = \{0, \Sigma_k a_k, 0\}^t$

Nonzero edge values  $a_k = B \cdot S_0$

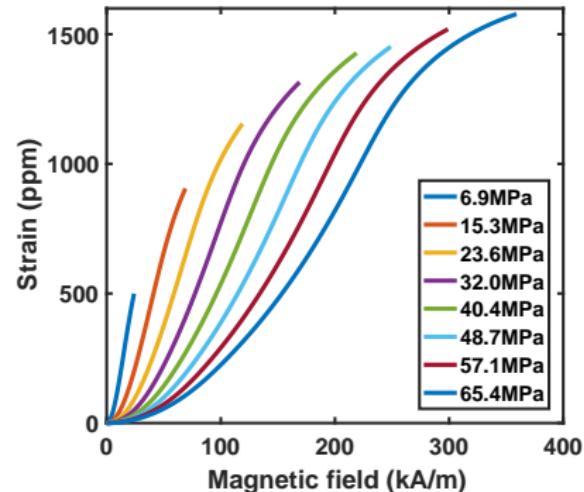
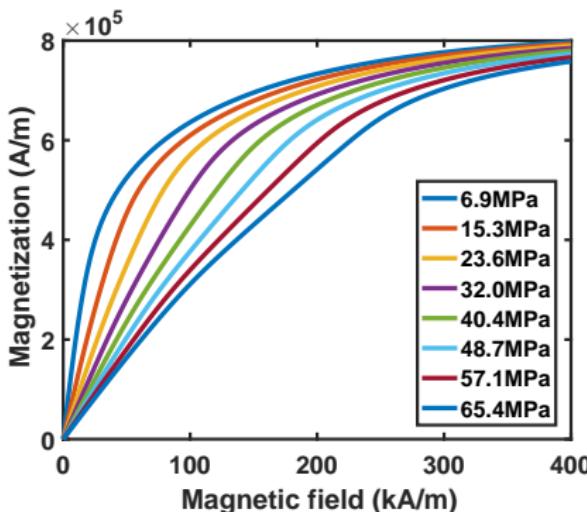
Boundary condition



Fixed points (in yellow)

# Nonlinear magnetostriiction

Describe the nonlinear behavior by multiscale model



Compute material Jacobian

$$\zeta = \begin{bmatrix} \mu^S = \frac{\partial B}{\partial H}(H_0, T_0) & d = \frac{\partial B}{\partial T}(H_0, T_0) \\ d^t = \frac{\partial S}{\partial H}(H_0, T_0) & s^H = \frac{\partial S}{\partial T}(H_0, T_0) \end{bmatrix}$$

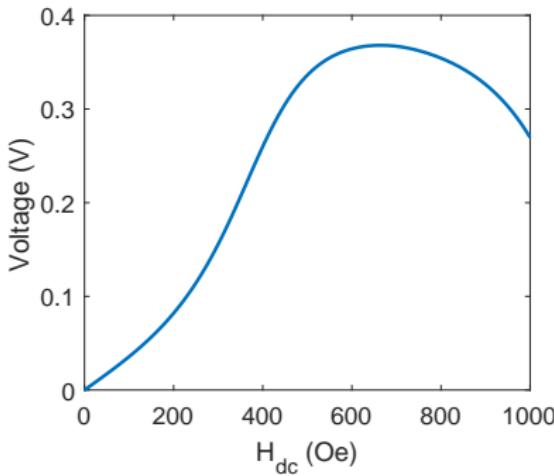
Chakrabarti, S. and Dapino, M. J. (2012). *Fully coupled discrete energy-averaged model for Terfenol-D* Journal of Applied Physics, 111(5), 054505.

# Piesewise linear procedure

Under small deviations

$$\begin{bmatrix} \Delta H \\ \Delta T \end{bmatrix} = \zeta^{-1} \begin{bmatrix} \Delta B \\ \Delta S \end{bmatrix}$$

Choose  $\Delta H$ ,  $N = \frac{H_{max}}{\Delta H}$



Repeat  $N$  times

$[\mu, h, c] = DEAM\_model(\mathbf{H}, \mathbf{T})$

Assemble matrix  
 $\mathbf{K}_{uu}, \mathbf{K}_{ua}, \mathbf{K}_{aa}, \Delta \mathbf{F}$

Solve equation  
 $[\Delta \mathbf{U}, \Delta \mathbf{A}, \Delta \mathbf{V}] = mat\_UAV \backslash \Delta \mathbf{F}$

$[\Delta S, \Delta B, \Delta E] = state\_eq([\Delta \mathbf{U}, \Delta \mathbf{A}, \Delta \mathbf{V}])$   
 $[\Delta H, \Delta T] = const.law(\Delta B, \Delta S)$

update  $\mathbf{H}, \mathbf{T}$

## 1 Introduction

- Motivation

## 2 Modeling

- Static analysis
- Dynamic analysis

## 3 Laminate

- Laminate composite with circular section
- Laminate composite with rectangular section

## 4 Homogenization

- Context
- Fiber composite
- Particulate composite

## 5 Conclusion

# Dynamic analysis

- **Elastic equilibrium**

$$\operatorname{div} \boldsymbol{T} + \boldsymbol{f} = \rho \frac{d^2 \boldsymbol{u}}{dt^2}$$

$\rho$ : masse volumique kg/m<sup>3</sup>

- **Ampere's law**

$$\begin{cases} \operatorname{curl} \boldsymbol{H} = \boldsymbol{J}_c \\ \operatorname{div} \boldsymbol{J}_c = 0 \end{cases} \quad \boldsymbol{J}_c = \sigma_c \boldsymbol{E}: \text{eddy currents}$$

Introduce time primitive of electric potential

$$\boldsymbol{E} = - \frac{d(\boldsymbol{a} + \operatorname{grad} \psi)}{dt} \quad \text{with } V = \frac{d\psi}{dt}$$

- **Gauss's law**

$$\frac{d(\operatorname{div} \boldsymbol{D})}{dt} = 0 \quad \text{for the symmetry of the system}$$

# Linear harmonic analysis

$$[\mathbb{K}]\{X\} = [F]$$

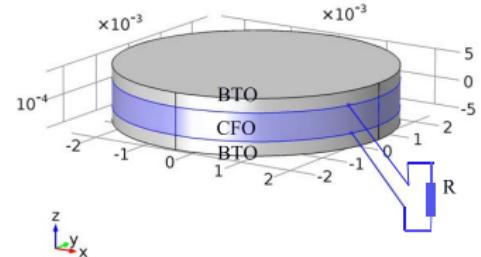
with:

- 

$$[\mathbb{K}] = \begin{bmatrix} -\omega^2 M_{uu} + j\omega C_{uu} + K_{uu} & -K_{ua} & j\omega K_{u\psi} & 0 \\ -K_{ua}^t & j\omega C_{aa} + K_{aa} & j\omega C_{a\psi} & 0 \\ j\omega K_{u\psi}^t & j\omega C_{a\psi}^t & j\omega C_{\psi\psi} + \omega^2 K_{\psi\psi} & -j\omega K_{\psi q} \\ 0 & 0 & -j\omega K_{\psi q}^t & j\omega Z \end{bmatrix}$$

- $\{X\} = \{u, a, \psi, Z\}^t$ .

$Z$  : Electrical charge connecting two electrodes.



## 1 Introduction

- Motivation

## 2 Modeling

- Static analysis
- Dynamic analysis

## 3 Laminate

- Laminate composite with circular section
- Laminate composite with rectangular section

## 4 Homogenization

- Context
- Fiber composite
- Particulate composite

## 5 Conclusion

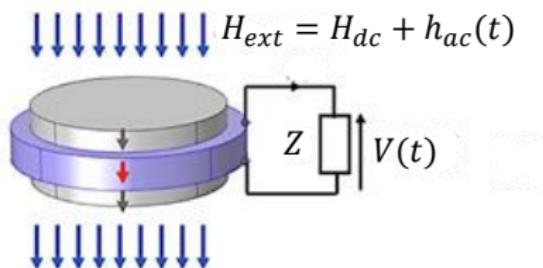
# Geometry

## Why laminate composite?

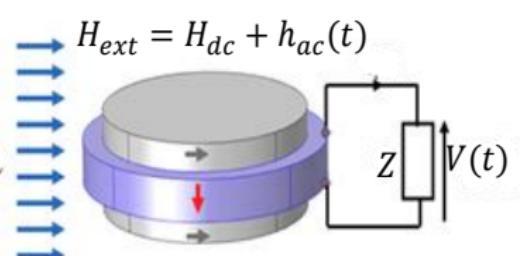
- Good coupling can be obtained at the ferroelectric and ferromagnetic interfaces.
- Higher resonance response in a wide frequency range

Wang, Lei, et al. *Effect of load resistance on magnetostrictive properties in FeGa/BaTiO<sub>3</sub>/FeGa laminate composites*. Journal of Alloys and Compounds 509.30 (2011): 7870-7873.

Mode TT



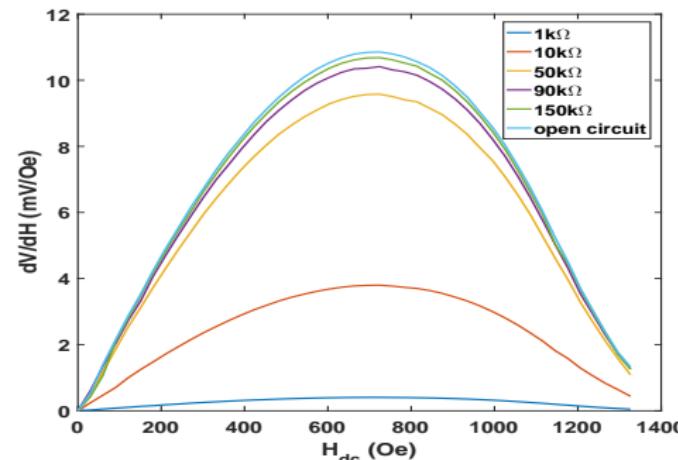
Mode LT



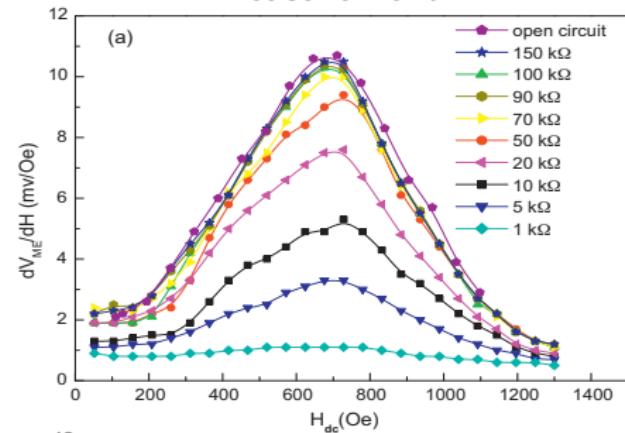
BaTiO<sub>3</sub> (gray layer): Thickness 1.5mm, diameter 12mm  
 FeGa (magenta layer): Thickness 1mm, diameter 10mm

# DC magnetic field dependence

Simulation result



Measurement

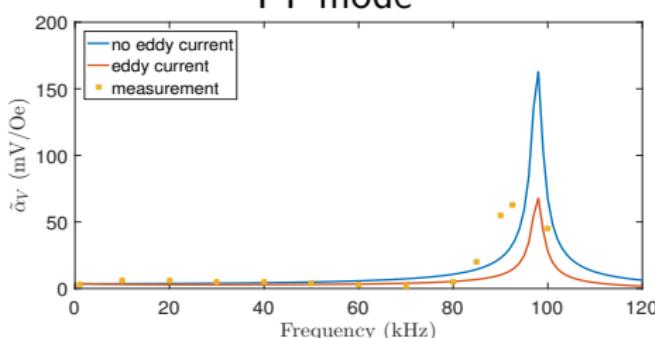


- ME voltage coefficient as a function of DC magnetic field under various electrical resistance load values and external magnetic field:  $H_{ac} = 1$  (Oe),  $f = 1$  (kHz)
- In concordance with

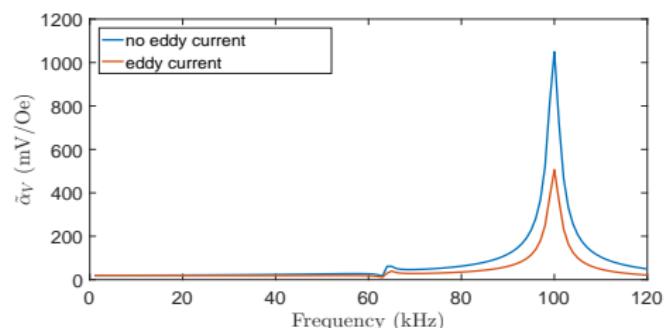
Wang, Lei, et al. 2011. *Effect of load resistance on magnetoelectric properties in FeGa/BaTiO<sub>3</sub>/FeGa laminate composites*. Journal of Alloys and Compounds

# Eddy current effect

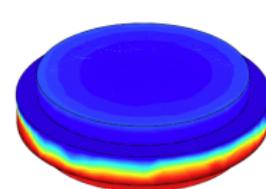
TT mode



LT mode



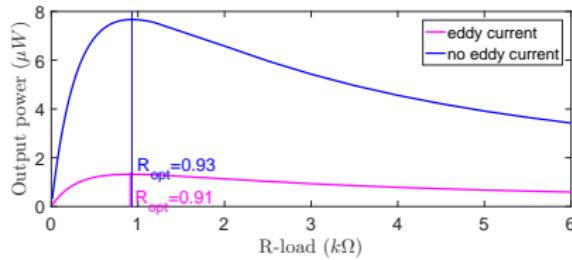
- The magnetic external field:  $H_{ac} = 1$  (Oe)
- The result with effect of eddy current in TT mode in concordance with measurement
- The quality factor decrease under eddy current effect.



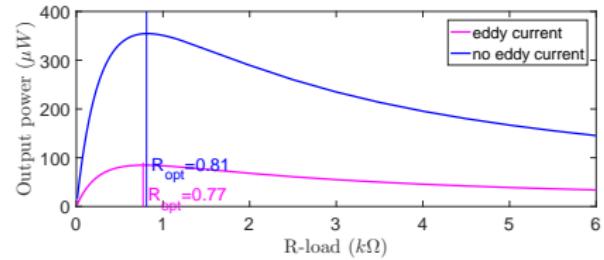
Electrical potential distribution

# Performance

TT mode



LT mode



- Output power  $P = V^2/R$  (post processing)
- The eddy current decrease the performance of material.
- Measurement with  $P_{max} = 2.75(\mu W)$   $R_{opt} = 0.6k\Omega$

## 1 Introduction

- Motivation

## 2 Modeling

- Static analysis
- Dynamic analysis

## 3 Laminate

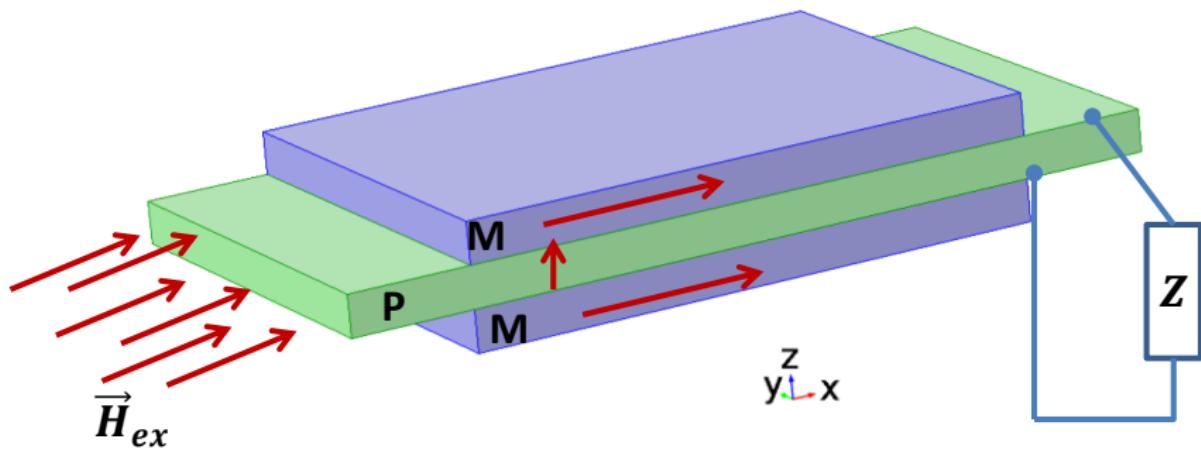
- Laminate composite with circular section
- Laminate composite with rectangular section

## 4 Homogenization

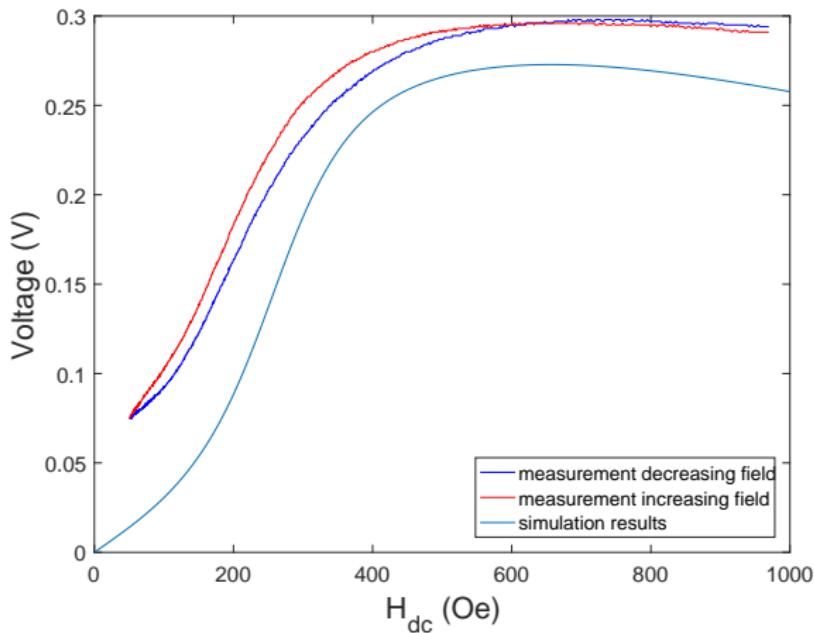
- Context
- Fiber composite
- Particulate composite

## 5 Conclusion

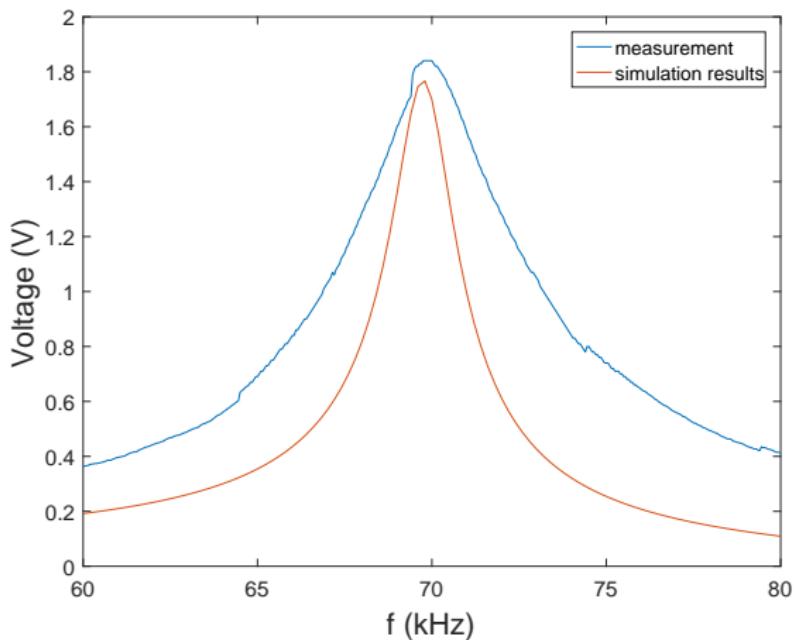
# Geometry



# DC magnetic field dependency

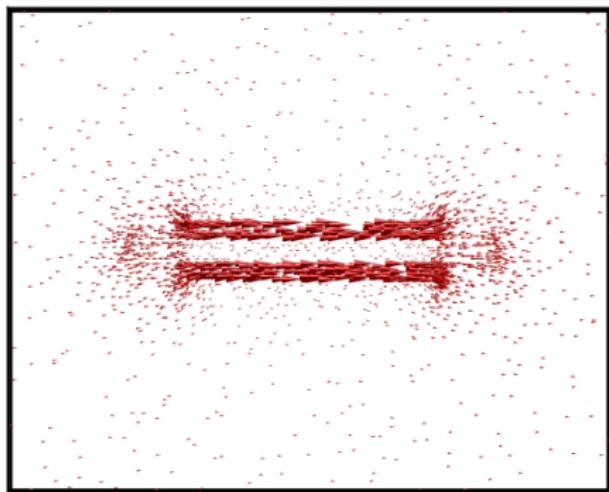


# Frequency dependency

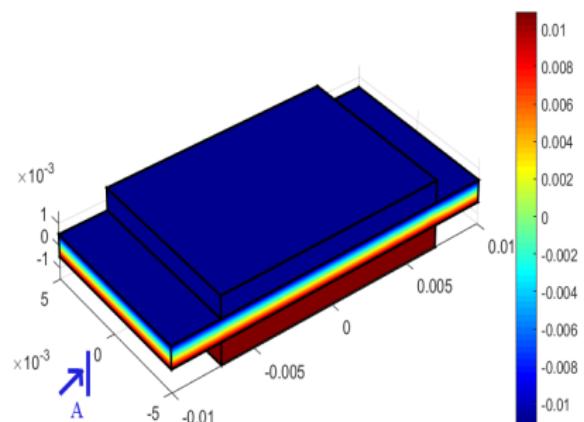


# Field distribution

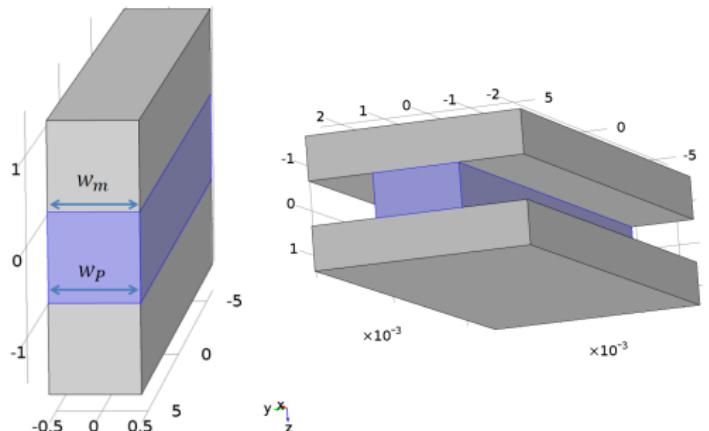
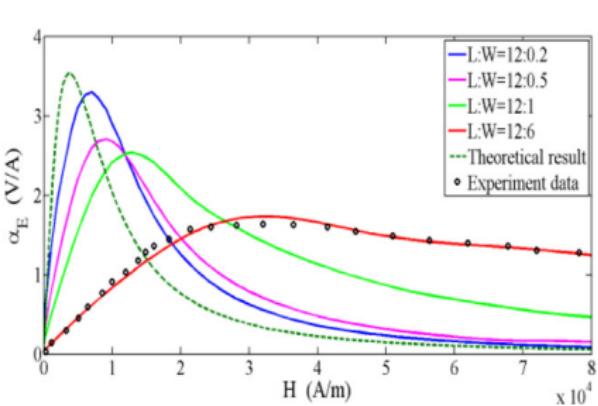
Magnetic induction distribution



Electric potential distribution



# Geometry

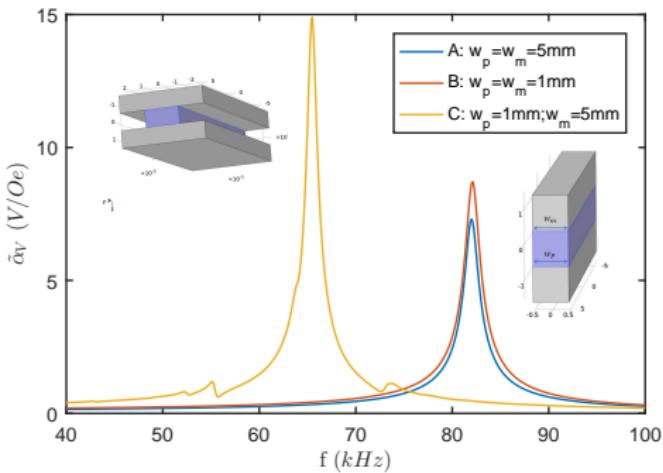


Three configurations are examined

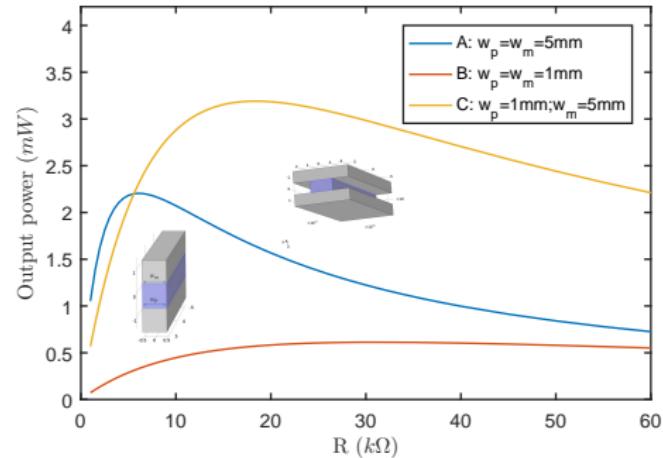
- A. Width of 5mm for all layers.
- B. Width of 1mm for all layers.
- C. Width of 5mm for magnetostrictive layer and width of 1mm for piezoelectric layer.

# Performance

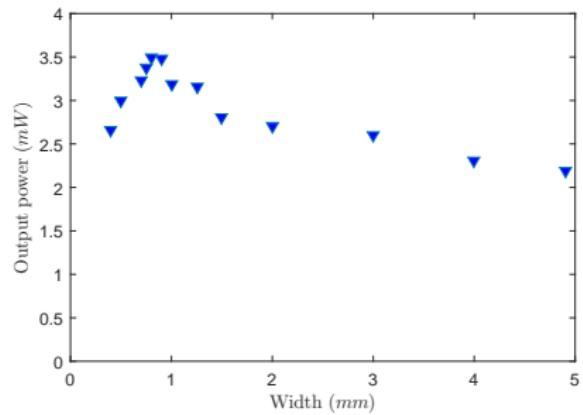
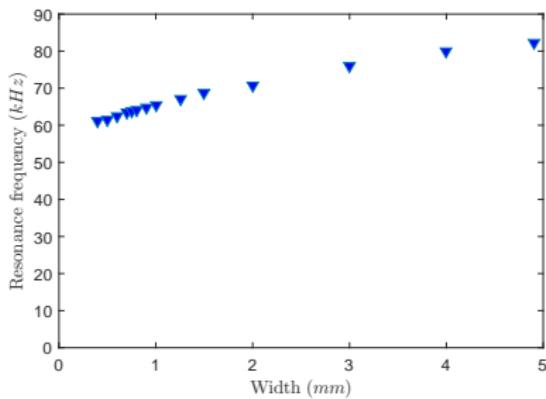
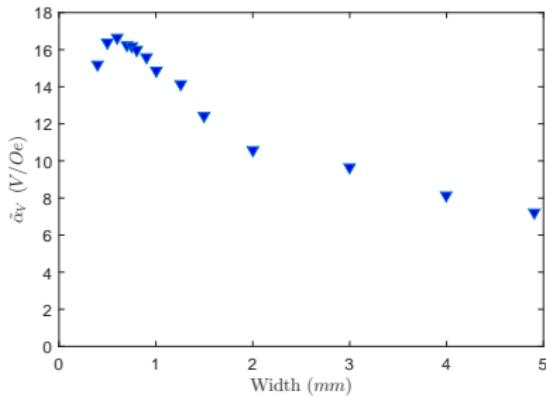
## Voltage



## Output power



# Parametric study



- a
- b
- c

## 1 Introduction

- Motivation

## 2 Modeling

- Static analysis
- Dynamic analysis

## 3 Laminate

- Laminate composite with circular section
- Laminate composite with rectangular section

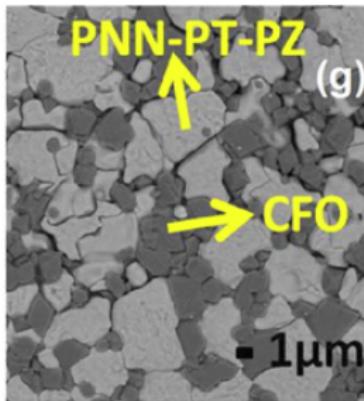
## 4 Homogenization

- Context
- Fiber composite
- Particulate composite

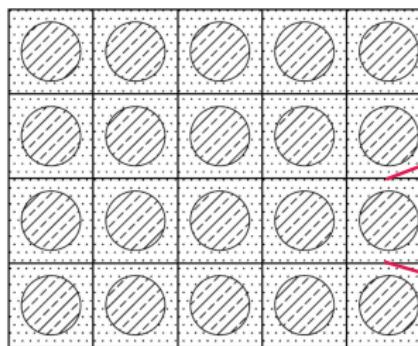
## 5 Conclusion

# 0-3 type and 1-3 type ME composite

- ✓ 3D FEM is useful to study the behavior of ME laminate composite
- ✗ It is difficult to apply for fiber composite and particulate composite

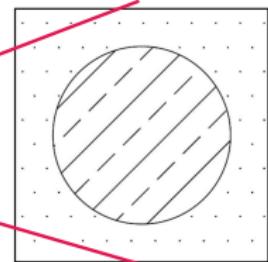


- a
- b



Square periodic structure

REV



Analytical method → Simple structure  
(Fiber composite)

Vadla, S. et al. (2016)  
Magnetoelectric coupling in  
0.5 Pb (Ni<sub>1/3</sub>Nb<sub>2/3</sub>) O<sub>3</sub>-0.35  
PbTiO<sub>3</sub>-0.15 PbZrO<sub>3</sub> and  
CoFe<sub>2</sub>O<sub>4</sub> based particulate  
composites. Scripta Materialia

Corcolle, R. et al., 2008 Generic formalism for homogenization of coupled behavior: Application to magneto-electroelastic behavior. Physical Review B.

# Boundary condition

- a
- b

Point:  $k_i + d_i, k_i$

Edge:  $(k_{i1} + d_i, k_{i2} + d_i), (k_{i1}, k_{i2})$

## Mechanics

$$u_j(k_i + d_i) = u_j(k_i) + \bar{S}_{ij}d_i$$

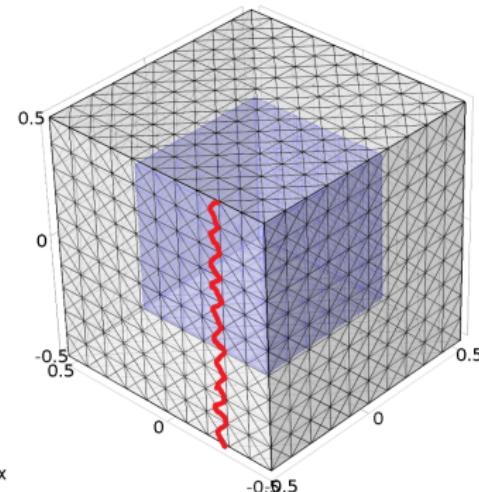
## Electric

$$V(k_i + d_i) = V(k_i) + \bar{E}_i d_i$$

## Magnetic

$$a(k_{i1} + d_i, k_{i2} + d_i) = a(k_{i1}, k_{i2}) + c_j \phi_j + c_k \phi_k$$

$$\begin{cases} c_j = 1 / -1 & \text{for the red edges} \\ c_0 = 0 & \text{for the others} \end{cases}$$



$$\phi_j = \int \mathbf{B}_j dA$$

A : the perpendicular surface

# Effective coefficients

Solve equation

$$[K]\{X\} = [F]$$



State variable  $\{X\} = \{u \quad a \quad V\}^t$

$$S = 1/2(\mathbf{grad} + \mathbf{grad}^t)u$$

$$B = \mathbf{curl} \, a$$

$$E = -\mathbf{grad} \, V$$



Local field

$$S, \quad B, \quad E$$

$$T = cS - e^t E - h^t B$$

$$H = -hS + \nu B$$

$$D = -eS + \varepsilon E$$



Local field

$$T, \quad H, \quad D$$

Local constitutive laws



Material coefficients

$$\begin{bmatrix} \bar{T} \\ \bar{H} \\ \bar{D} \end{bmatrix} = \begin{bmatrix} \tilde{C} & -\tilde{h}^t & -\tilde{e}^t \\ \tilde{h} & \tilde{\nu} & \tilde{\alpha}_H^t \\ \tilde{e} & \tilde{\alpha}_H & \tilde{\varepsilon} \end{bmatrix} \begin{bmatrix} \bar{S} \\ \bar{B} \\ \bar{E} \end{bmatrix}$$

$$\begin{cases} \bar{T} = 1/V \int T dV \\ \bar{H} = 1/V \int H dV \\ \bar{D} = 1/V \int D dV \end{cases}$$

## 1 Introduction

- Motivation

## 2 Modeling

- Static analysis
- Dynamic analysis

## 3 Laminate

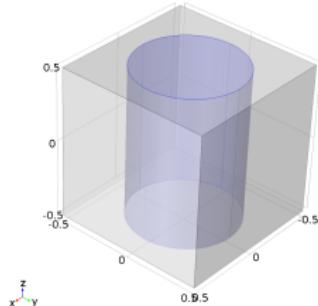
- Laminate composite with circular section
- Laminate composite with rectangular section

## 4 Homogenization

- Context
- Fiber composite
- Particulate composite

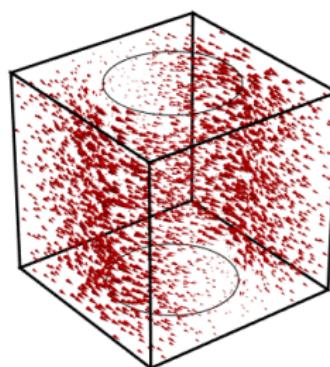
## 5 Conclusion

# Apply of magnetic field

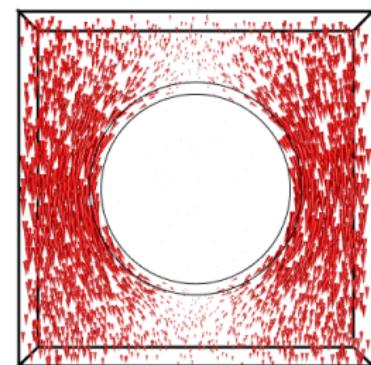


- Magnetostrictive matrix ( $\text{CoFe}_2\text{O}_4$ ) reinforced by fiber piezoelectric ( $\text{BaTiO}_3$ ).
- The volume fraction is  $f = 0$  to  $f = 0.8$ .

Example:  
Magnetic field is  
applied

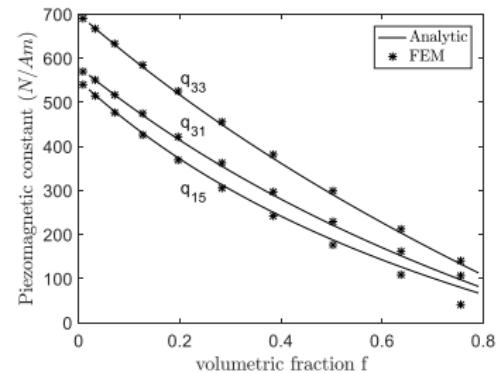
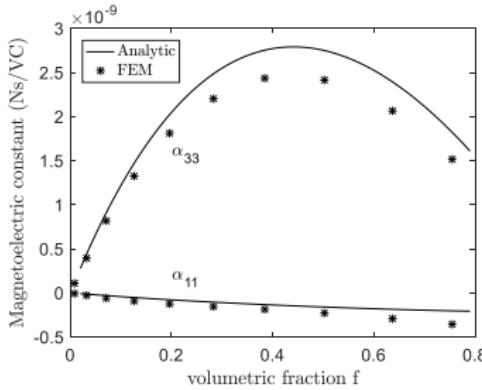
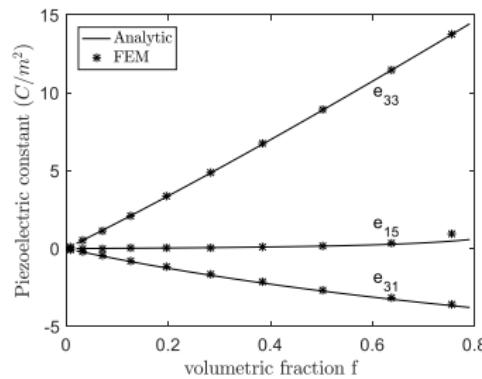


3D view



Top view

# Effective coefficient



## 1 Introduction

- Motivation

## 2 Modeling

- Static analysis
- Dynamic analysis

## 3 Laminate

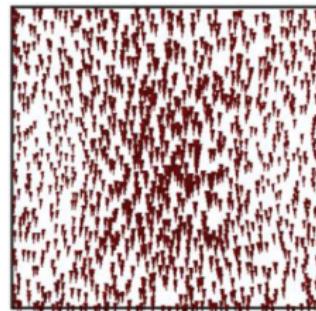
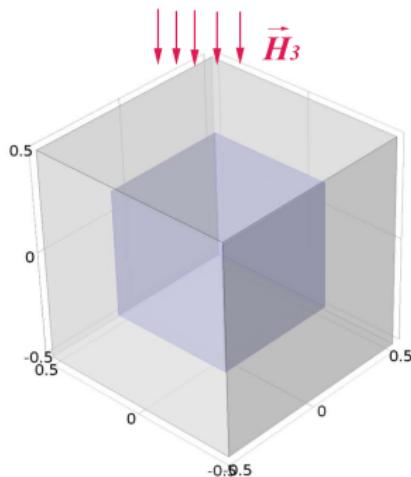
- Laminate composite with circular section
- Laminate composite with rectangular section

## 4 Homogenization

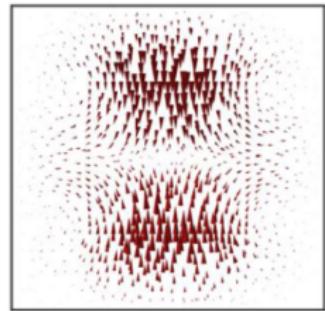
- Context
- Fiber composite
- Particulate composite

## 5 Conclusion

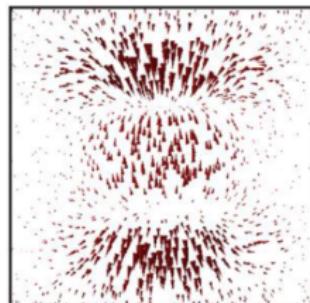
# Field distribution



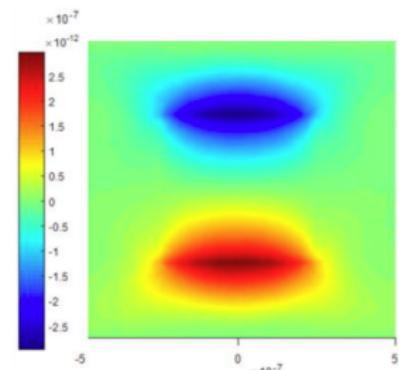
(a)



(b)



(c)

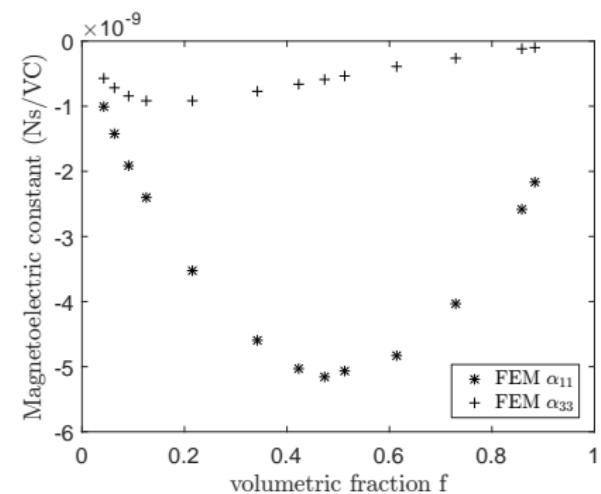
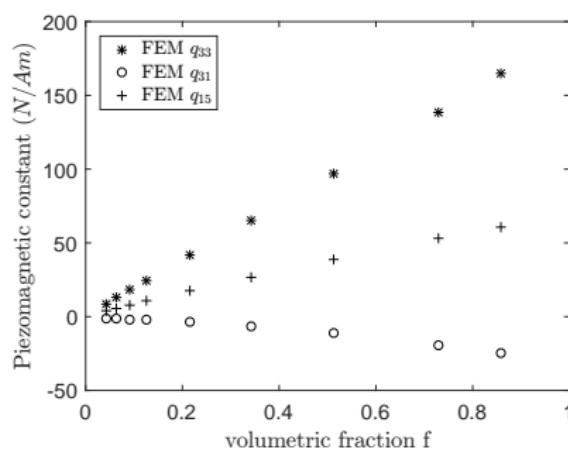


(d)

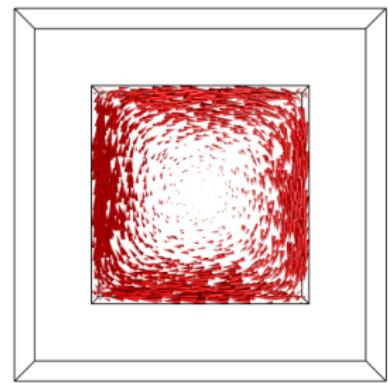
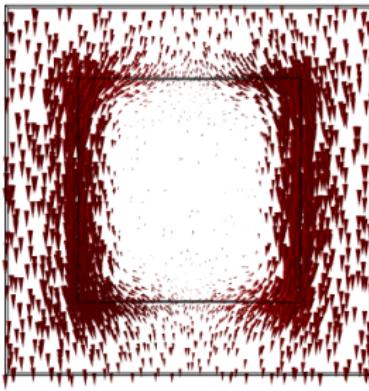
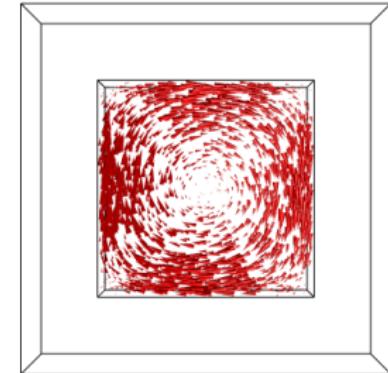
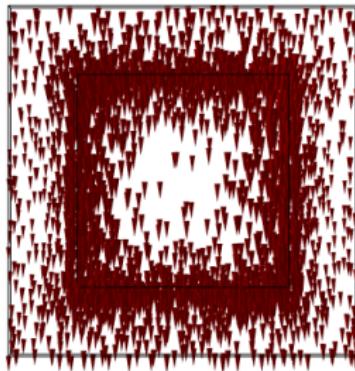
Magnetic field is applied

- (a) Magnetic field
- (b) Displacement field
- (c) Electric field
- (d) Electric potential

# Effective coefficient



# Dynamic analysis



# Conclusion and perspectives

## Conclusion

Completed FEM of circular tri-laminated ME composite has been presented.

The effect of eddy current is included.

The 3D analysis provides a useful tool to study ME composite of various geometries for energy transducer.

## Perspectives

Optimization geometry can be performed by this model.

Investigation under large signal of magnetic field

Time reduction for computation is needed.

# Publication

Homogenization of Magnetolectric 0–3 Type Composites by 3-D Multiphysics Finite-Element Modeling. *IEEE Transactions on Magnetics* 2019.

3-D Finite Element Analysis of Magnetolectric Composites Accounting for Material Non-linearity and Eddy Currents. *IEEE Transactions on Magnetics* 2019.

3D FEM modeling and study of novel structure of magnetoelectric composites. *International Journal of Numerical Modelling: Electronic Networks, Devices and Fields* 2019.

**THANK YOU FOR YOUR  
ATTENTION**