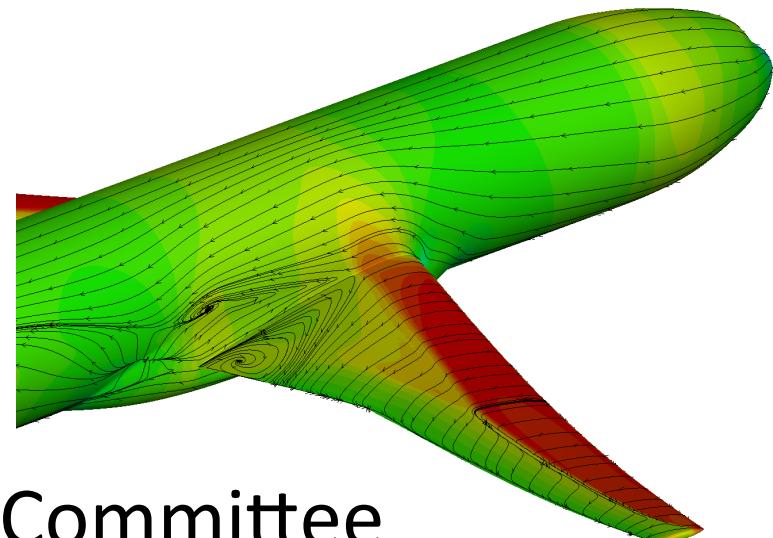


DPW 5 Summary of Participant Data

Ed Tinoco,
David Levy,
Olaf Brodersen,
and the DPW Organizing Committee



24 June 2012



Outline:

- Participant Data
- Case 1: Grid Convergence
- Case 2: Buffet Study
- Pressure Data
- Side of Body Separation
- Trailing Edge Separation
- Conclusions



Participant Data:

- **54 Data Total Data Submittals**
- **22 Teams/Organizations**
 - 10 N. America, 5 Europe, 6 Asia, 1 S. America
 - 8 Government, 5 Industry, 6 Academia, 2 Commercial, 1 Unknown
 - 1 for Case 3 only
- **Grid Types:**
 - 5 Overset (4 Teams)
 - 7 Structured Multi-block (5 Teams)
 - 25 Unstructured (13 teams)
(14 Hex, 7 Hybrid, 4 Prism)
 - 16 Custom (all types)
- **Turbulence Models:**
 - 34 SA (all types), 12 SST, 4 k-e-RT, 1 EARSM, 1 Lag-RST



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Team	ID	Name	Organization	File Name	Code	Misc Solver	Grid Type	Turbulence Model
1	A	Sclafani	Boeing (Huntington)	SclafaniT-CommonOverset-SAla-1	OVERFLOW v2.2c	Central	Overset	SA-la —————
	B	Sclafani	Boeing (Huntington)	SclafaniT-CommonOverset-SARC-1	OVERFLOW v2.2c	Central	Overset	SA-la w/ RC - - - -
	C	Sclafani	Boeing (Huntington)	SclafaniT-CustomOverset-SAla-1	OVERFLOW v2.2c	Central	Custom (Overset)	SA-la —————
	D	Sclafani	Boeing (Huntington)	SclafaniT-CustomOverset-SAla-2	OVERFLOW v2.2c	Central / QCR	Custom (Overset)	SA-la —————
	E	Sclafani	Boeing (Huntington)	SclafaniT-CustomOverset-SARC-1	OVERFLOW v2.2c	Central	Custom (Overset)	SA-la w/ RC - - - -
	F	Sclafani	Boeing (Huntington)	SclafaniT-CustomOverset-SARC-2	OVERFLOW v2.2c	Central / QCR	Custom (Overset)	SA-la w/ RC - - - -
	G	Sclafani	Boeing (Huntington)	SclafaniT-CustomOverset-SARC-3	OVERFLOW v2.2c	Central	Custom (Overset)	SA-la w/ RC - - - -
	H	Sclafani	Boeing (Huntington)	SclafaniT-CustomOverset-SARC-4	OVERFLOW v2.2c	Central / QCR	Custom (Overset)	SA-la w/ RC - - - -
2	I	Chen	Mianyang City, China	Chen-CommonHex-SA-1	MFlow	Upwind	Hex - - - -	SA —————
	J	Chen	Mianyang City, China	Chen-CommonHex-SA-1	MFlow	Upwind	Hybrid —————	SA —————
3	K	GariÉpy	EcolePolytechMontreal	GariepyM-CommonPrism-SA-1	Fluent V13	Upwind	Prism - - - -	SA —————
	L	GariÉpy	EcolePolytechMontreal	GariepyM-Custom-SA-1	Fluent V13	Upwind	Custom (Hex)	SA —————
4	M	Scalabrin	Embraer	ScalabrinL-CommonHex-RT-1	CFD++	Upwind	Hex - - - -	k-e-RT
	N	Scalabrin	Embraer	ScalabrinL-CommonHex-SST-1	CFD++	Upwind	Hex - - - -	SST
	O	Scalabrin	Embraer	ScalabrinL-CommonHybrid-RT-1	CFD++	Upwind	Hybrid —————	k-e-RT
	P	Scalabrin	Embraer	ScalabrinL-CommonHybrid-SST-1	CFD++	Upwind	Hybrid —————	SST
	Q	Scalabrin	Embraer	ScalabrinL-CommonPrism-RT-1	CFD++	Upwind	Prism - - - -	k-e-RT
	R	Scalabrin	Embraer	ScalabrinL-CommonPrism-SST-1	CFD++	Upwind	Prism - - - -	SST
	S	Scalabrin	Embraer	ScalabrinL-CommonCustom-RT-1	CFD++	Upwind	Custom (Hybrid)	k-e-RT
	T	Scalabrin	Embraer	ScalabrinL-CommonCustom-SST-1	CFD++	Upwind	Custom (Hybrid)	SST
5	U	Eliasson	FOI	EliassonP-CommonHex-EARSM-1	EDGE		Hex - - - -	EARSM
	V	Eliasson	FOI	EliassonP-CommonHex-SA-1	EDGE		Hex - - - -	SA —————
	W	Eliasson	FOI	EliassonP-CommonHex-SST-1	EDGE		Hex - - - -	SST
6	X	Powell	Gulfstream	PowellIN-CommonHybrid-SA-1	FUN3D		Hybrid —————	SA —————
7	Y	Balakrishnan	Indian Inst. Science	BalakrishnanN-CommonHex-SA-1	HiFUN	Upwind	Hex - - - -	SA —————
8	Z	Hashimoto	JAXA	Hashimoto-CommonHex-SA-1	FaSTAR	Upwind	Hex - - - -	SA-noft2-R - - - -
	2	Hashimoto	JAXA	Hashimoto-Custom-SA-1	FaSTAR	Upwind	Custom (Hex)	SA-noft2-R - - - - 4



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Team	ID	Name	Organization	File Name	Code	Misc Solver	Grid Type	Turbulence Model
9	3	Yamamoto	JAXA	YamamotoK-CommonMB-SA-noft2-R-1	UPACS	Upwind	Multi-block	SA-noft2-R (Crot=1)
	4	Yamamoto	JAXA	YamamotoK-CommonMB-SST-V-1	UPACS	Upwind	Multi-block	SST-V
10	5	Olson	NASA Ames	Olsen-CommonOverset-LagRST-1	overflow2.2e_LRS	Central/matrix	Overset	Lag RST
11	6	Park	NASA Langley	ParkM-CommonHybrid-SA-1	FUN3D v12.2	Upwind Roe	Hybrid	SA
	7	Park	NASA Langley	ParkM-CommonMB-SA-1	CFL3D v6.6	Upwind Roe	Multi-block	SA
12	8	Cai	NPU China	CaiJ-CommonOverset-SST-1	ExStream	Upwind	Overset	SST
13	9	Hue	ONERA	HueD_CommonMB_SA_1	elsA	Central	Multi-block	SA
14	a	Coder	Penn St. U	CoderJ-CommonOverset-SA-fv3-1	OVERFLOW 2.2c	Upwind	Overset	SA-fv3
15	b	Osusky	U. Toronto	OsuskyM-CommonMB-SA-1	Diablo	Scalar	Multi-block	SA
	d	Osusky	U. Toronto	OsuskyM-CommonMB-SA-2	Diablo	Matrix	Multi-block	SA
16	e	Levy	Cessna Aircraft Co.	LevyD-CommonHybrid-SA-1	NSU3D	Central/matrix	Hybrid	SA
	f	Levy	Cessna Aircraft Co.	LevyD-CommonHybrid-SA-2	FUN3D	Upwind Roe	Hybrid	SA
17	g	Crippa	DLR	DLR_CrippaS-CommonHex-SA-1	TAU	Matrix	Hex	SA
	h	Crippa	DLR	DLR_CrippaS-CommonHex-SST-1	TAU	Matrix	Hex	SST
18	k	Moitra	CRL_INDIA	CRL_INDIA_MoitraA	CFD++	Upwind	Prism	SA-RC
19	m	Winkler	Boeing (St. Louis)	BCFD-CommonHex-SA-1	BCFD	Upwind HLLE	Hex	SA
	n	Winkler	Boeing (St. Louis)	BCFD-CommonHex-SSTV-1	BCFD	Upwind HLLE	Hex	SST-V
	q	Winkler	Boeing (St. Louis)	BCFD-CommonHex-SA-2	BCFD	Upwind HLLE	Hex	SA
	r	Winkler	Boeing (St. Louis)	BCFD-CommonHex-SSTV-2	BCFD	Upwind HLLE	Hex	SST-V
20	t	Temmerman	NUMECA	DPW-V-NUMECA	FINE/Open	Cell Centered	Multi-block	SA
21	α	Brodersen	DLR	DLR_BrodersenO_Cust1_SA_D1	TAU	Diss 1	Custom (Hybrid)	SA
	β	Brodersen	DLR	DLR_BrodersenO_Cust1_SA_D3	TAU	Diss 3	Custom (Hybrid)	SA
	δ	Brodersen	DLR	DLR_BrodersenO_Cust2_SA_D1	TAU	Diss 1	Custom (Hyb w/ Hex-Wake)	SA
	γ	Brodersen	DLR	DLR_BrodersenO_Cust2_SA_D3	TAU	Diss 3	Custom (Hyb w/ Hex-Wake)	SA
	λ	Brodersen	DLR	DLR_BrodersenO_Cust2_SST_D1	TAU	Diss 1	Custom (Hyb w/ Hex-Wake)	Menter SST
	π	Brodersen	DLR	DLR_BrodersenO_Cust2_SST_D3	TAU	Diss 3	Custom (Hyb w/ Hex-Wake)	Menter SST

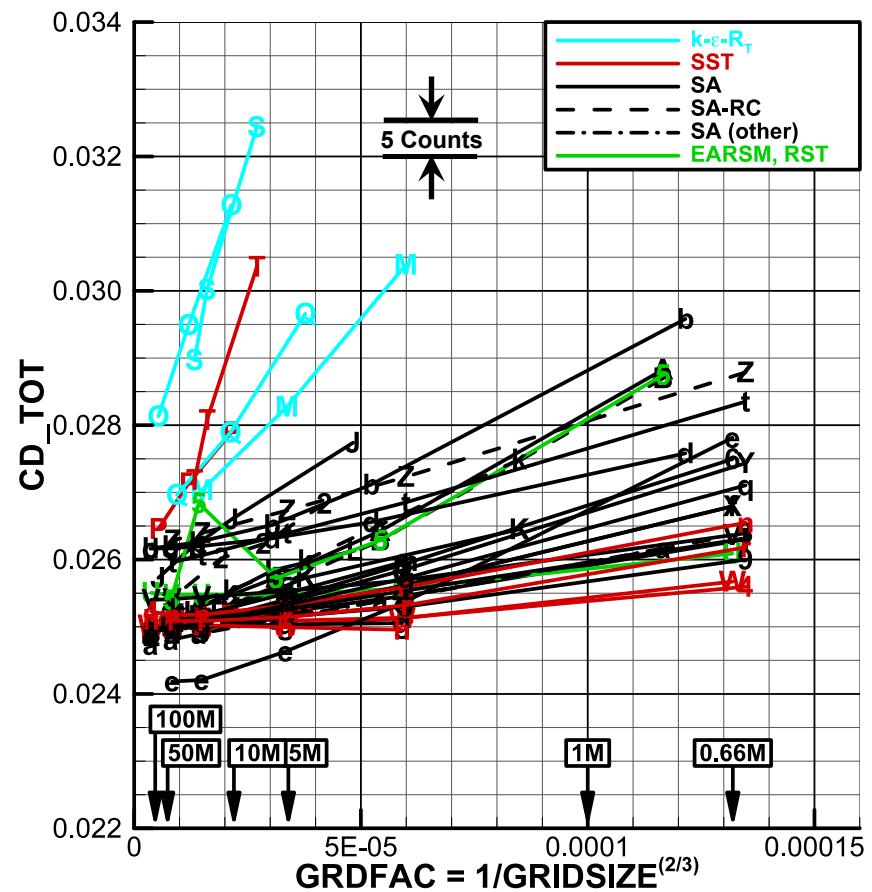
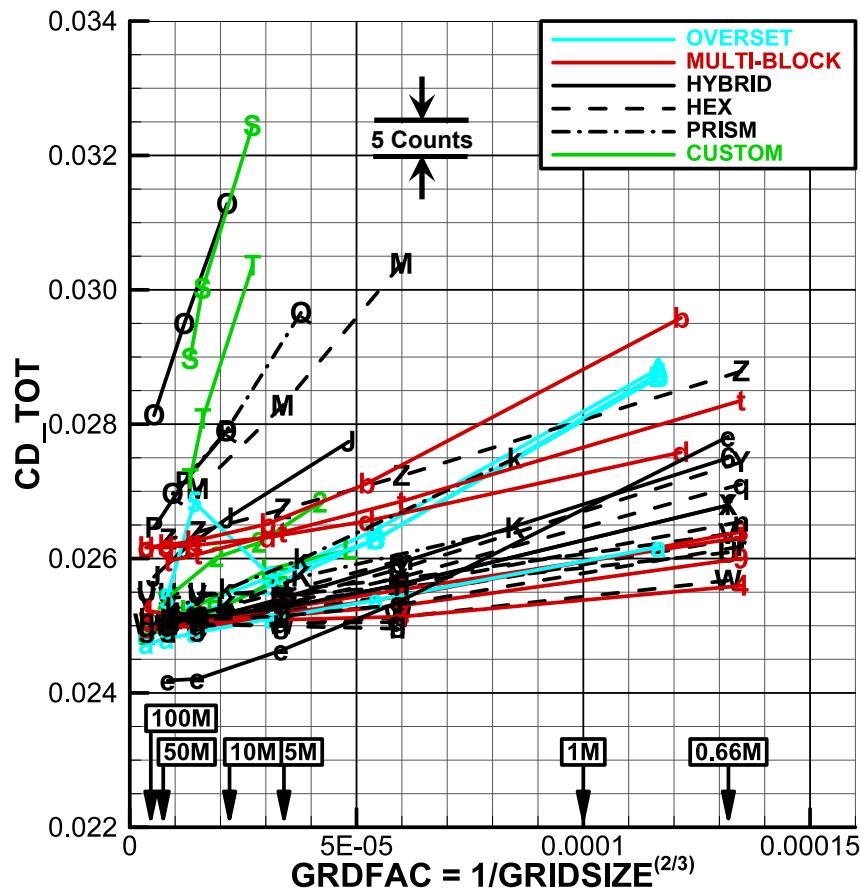
Case 1: Grid Convergence Study

- NASA Common Research Model, Wing-Body
- Mach=0.85, $C_L = 0.500 \pm 0.001$
- Grid Resolution Level:
 - 1) Tiny 2) Coarse 3) Medium,
 - 4) Fine 5) Extra-Fine 6) Super-Fine
- Chord Reynolds Number: 5×10^6

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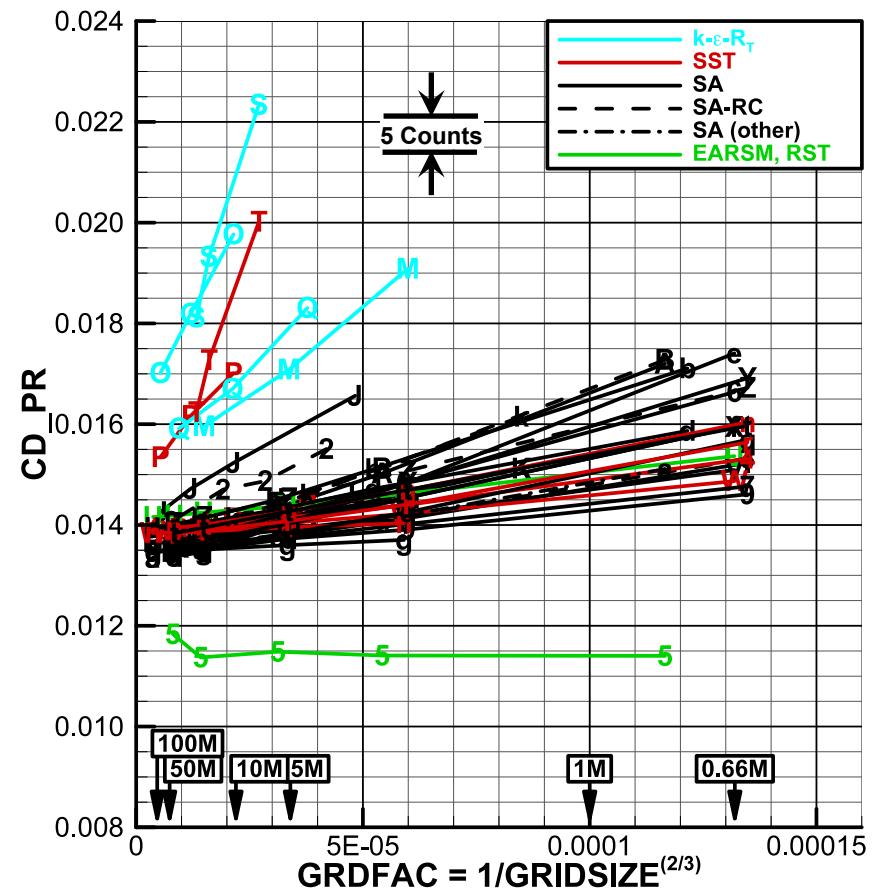
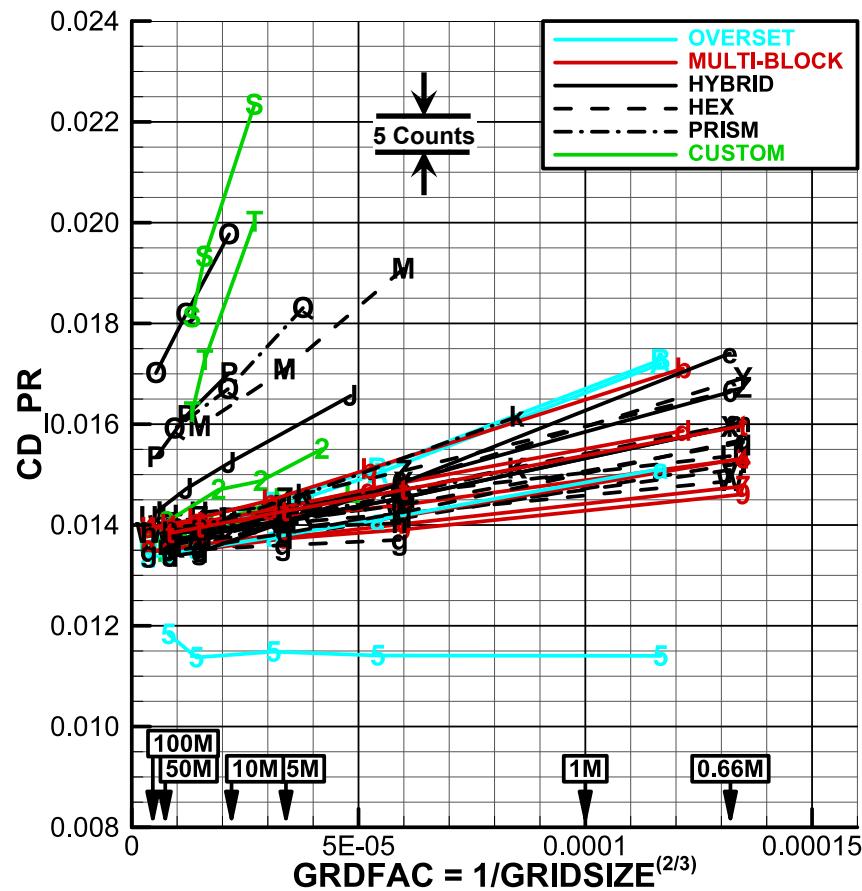
Case 1: CD_TOT - All Solutions by Grid Type and Turbulence Model



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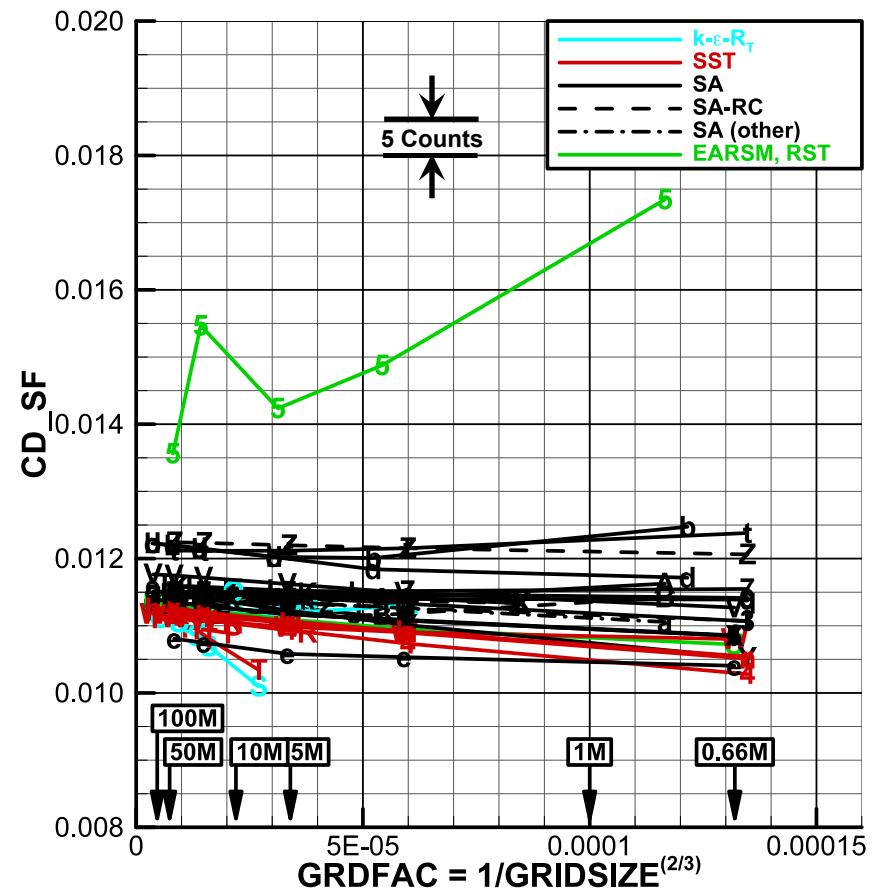
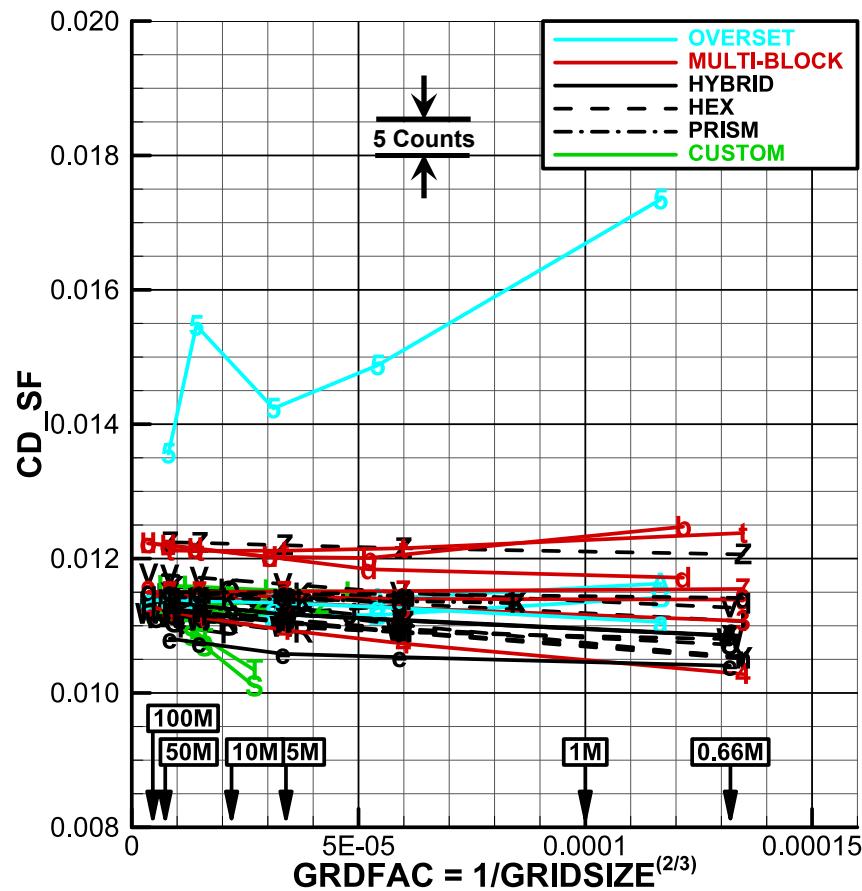
Case 1: CD_PR - All Solutions by Grid Type and Turbulence Model



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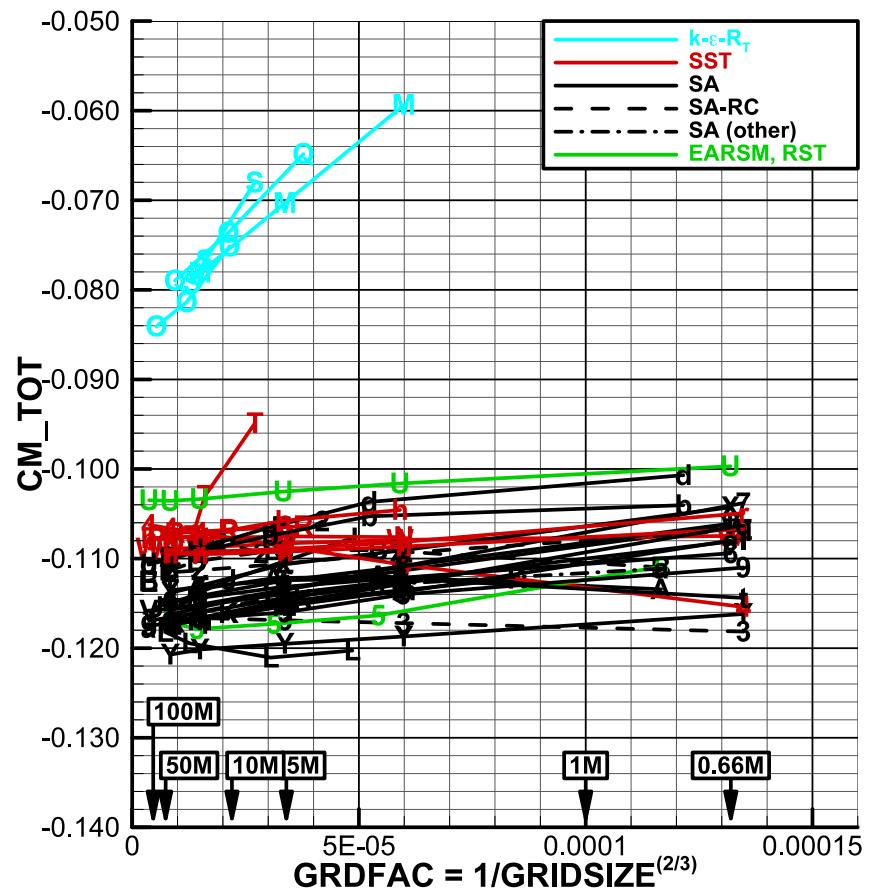
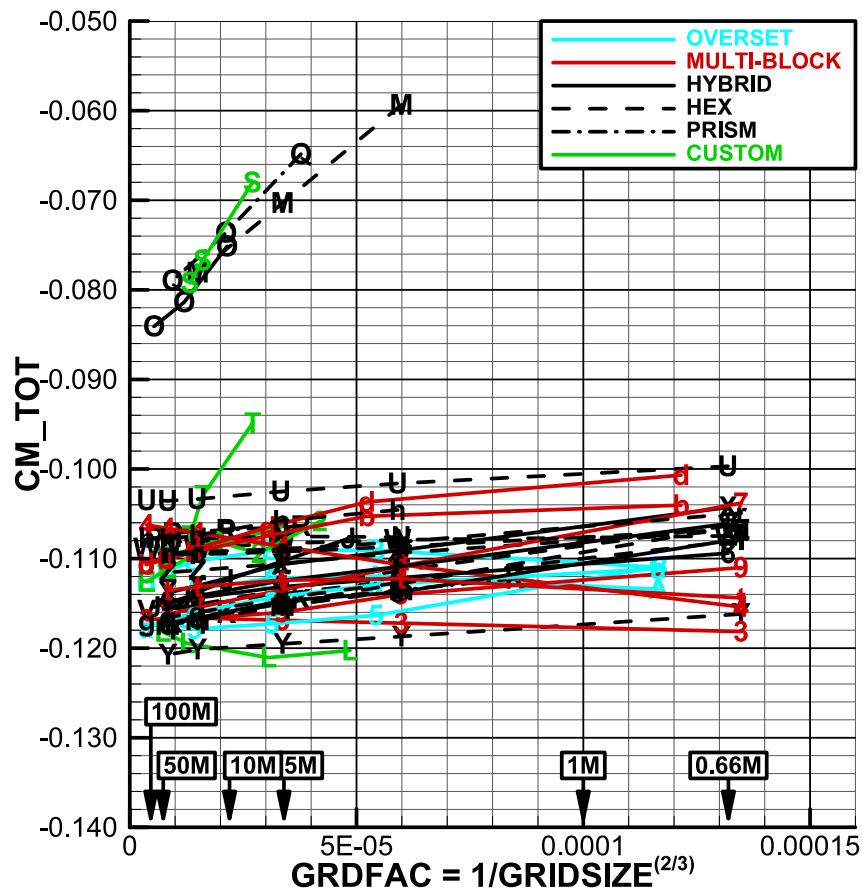
Case 1: CD_SF - All Solutions by Grid Type and Turbulence Model



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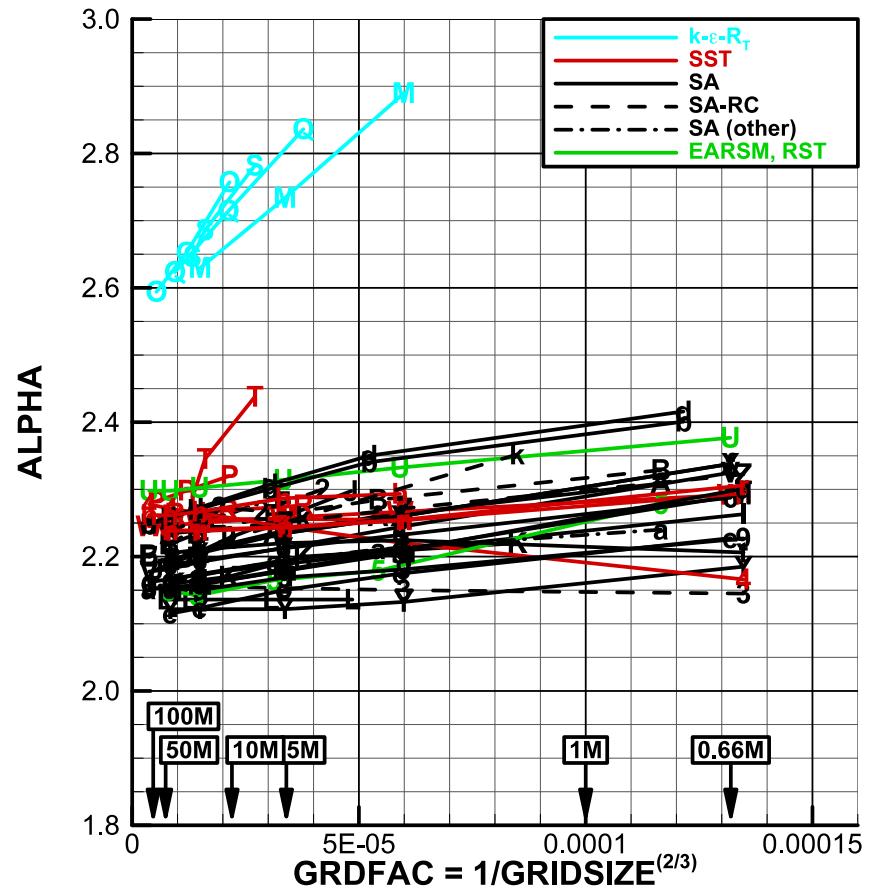
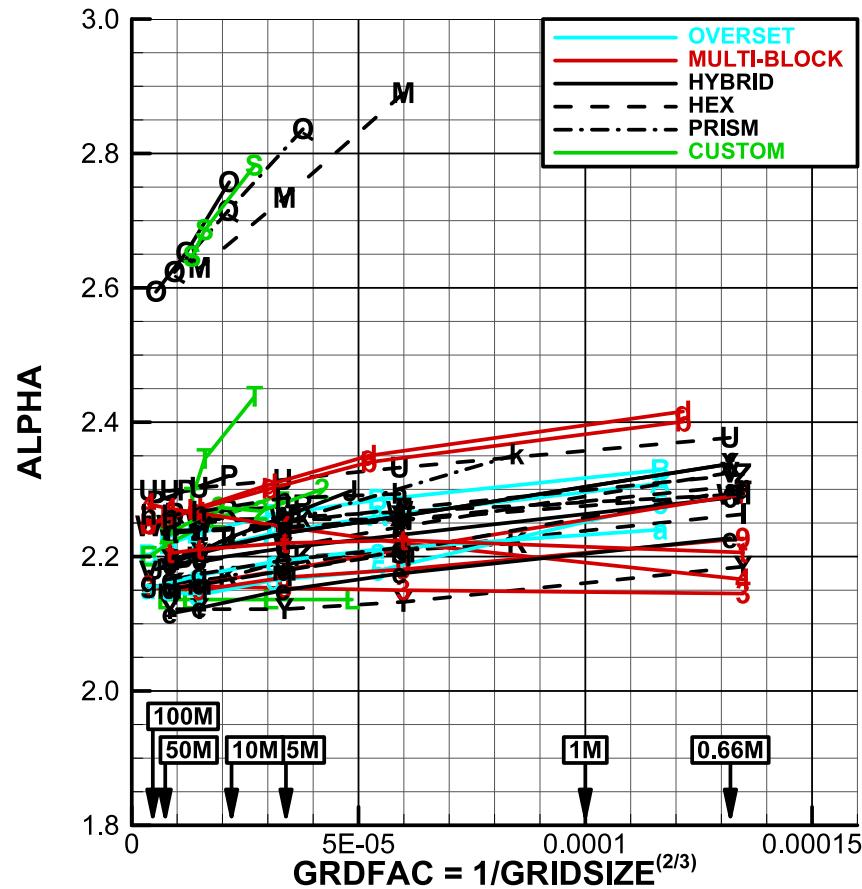
Case 1: CM_TOT - All Solutions by Grid Type and Turbulence Model



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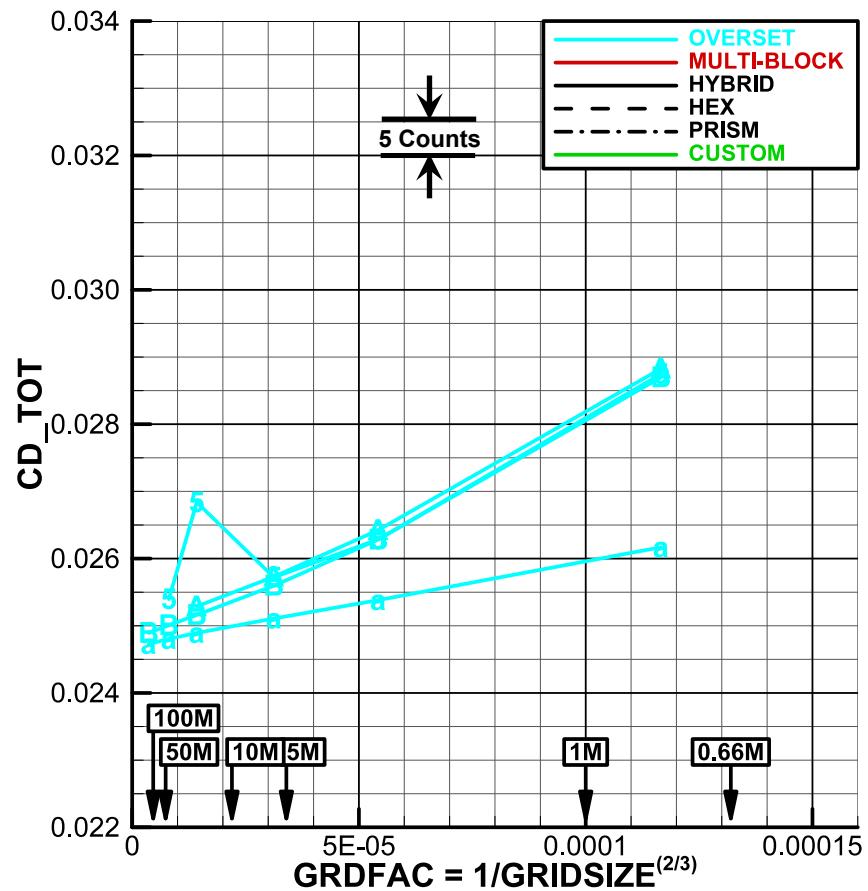
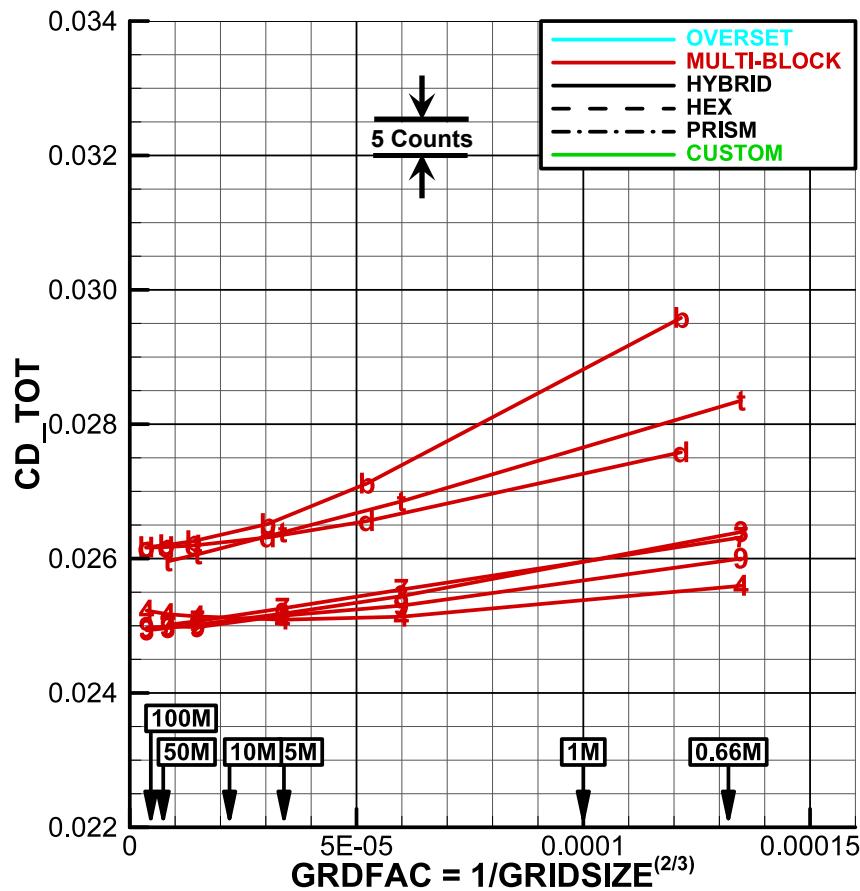
Case 1: ALPHA - All Solutions by Grid Type



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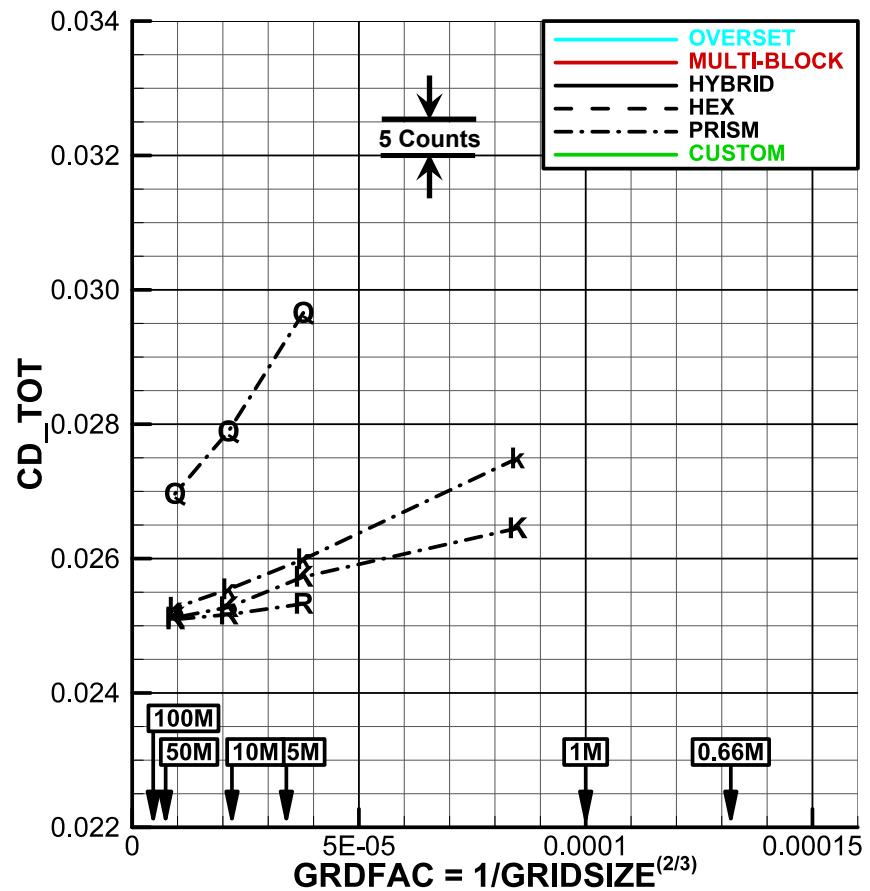
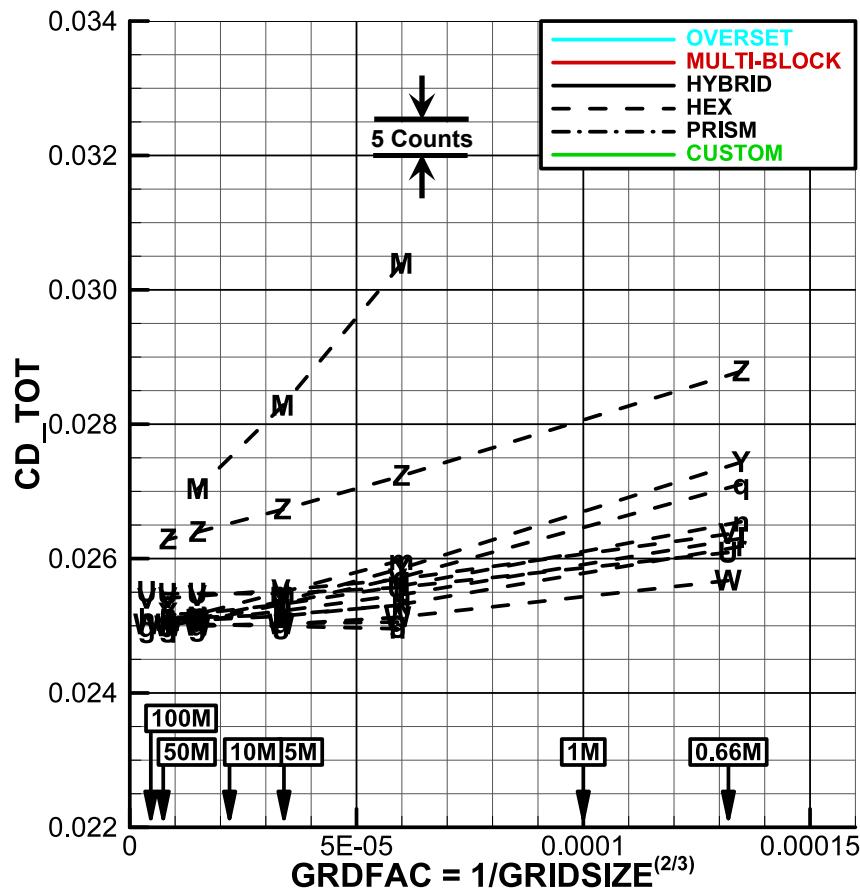
Case 1: CD_TOT – Multi-block and Overset Grids



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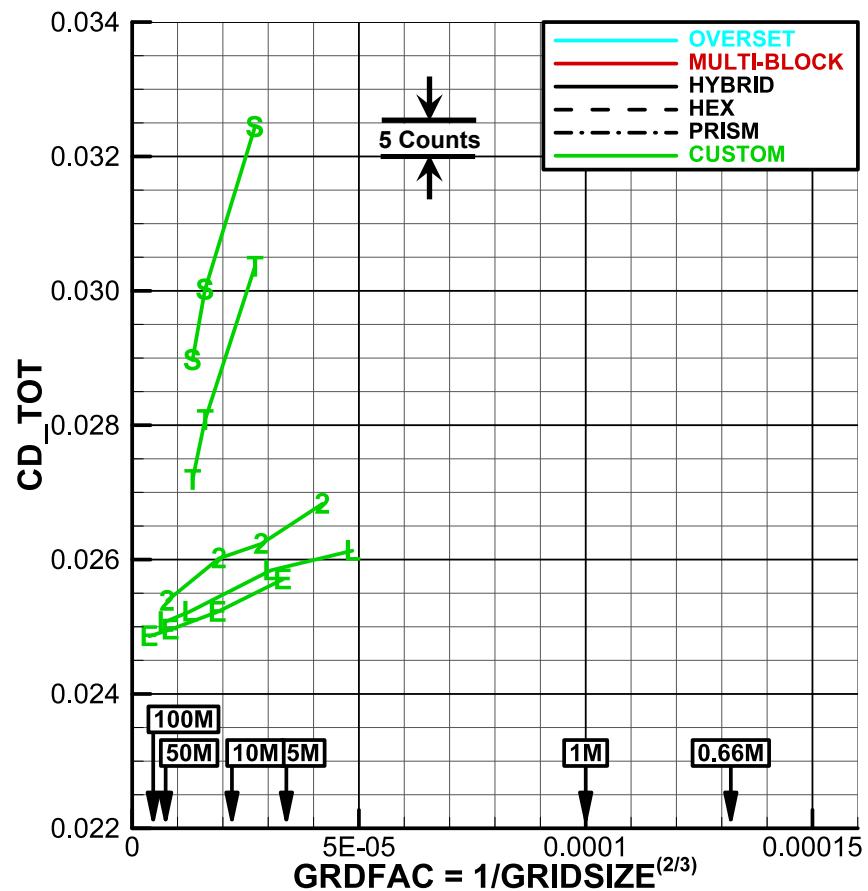
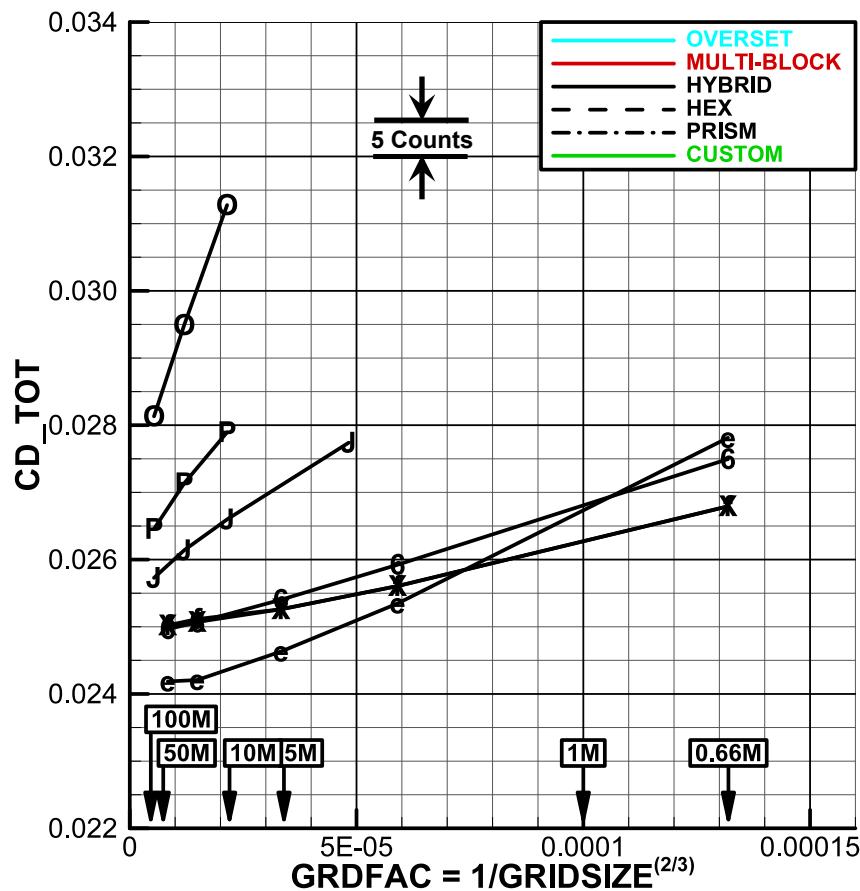
Case 1: CD_TOT – Unstructured Hexahedral and Prismatic Grids



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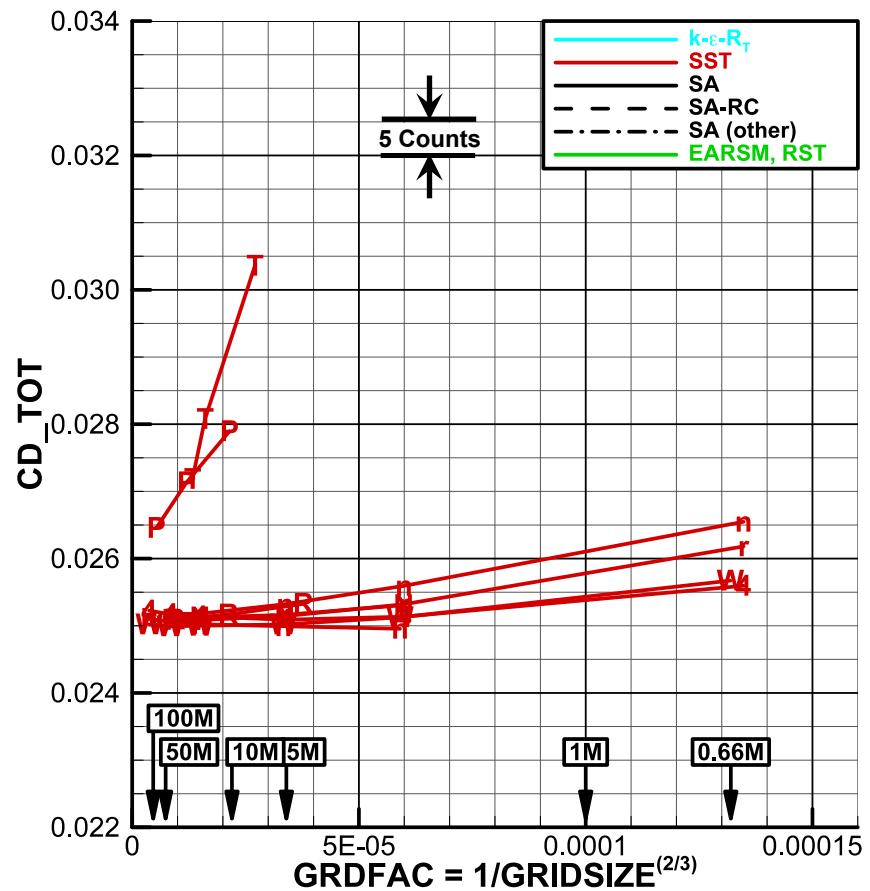
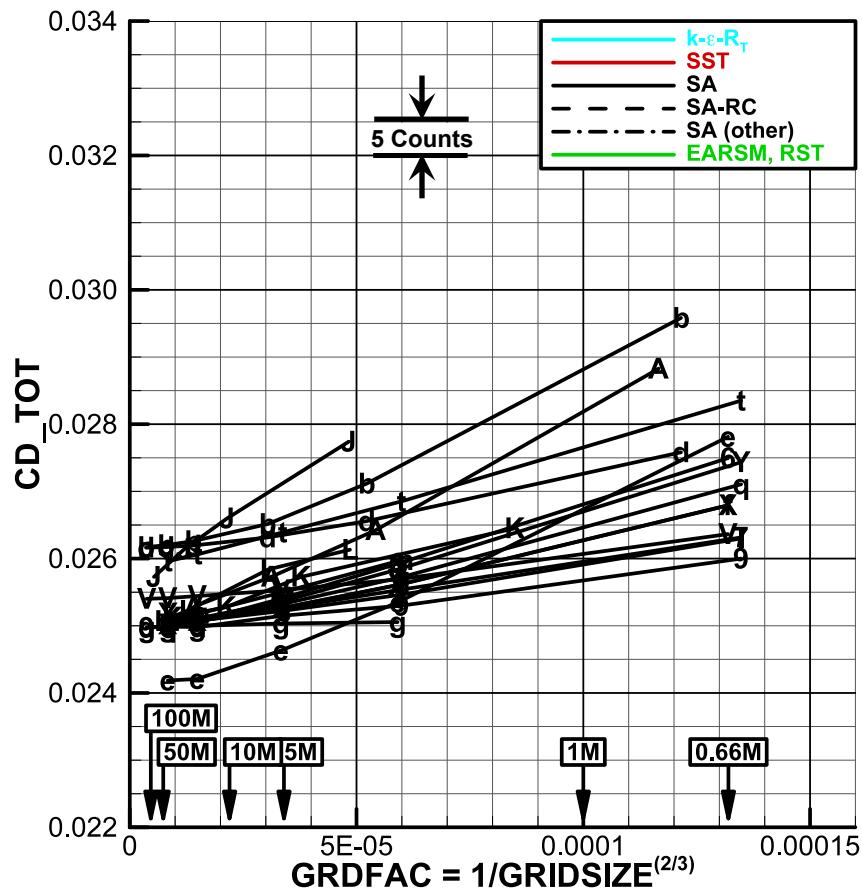
Case 1: CD_TOT – Unstructured Hybrid and all Custom Grids



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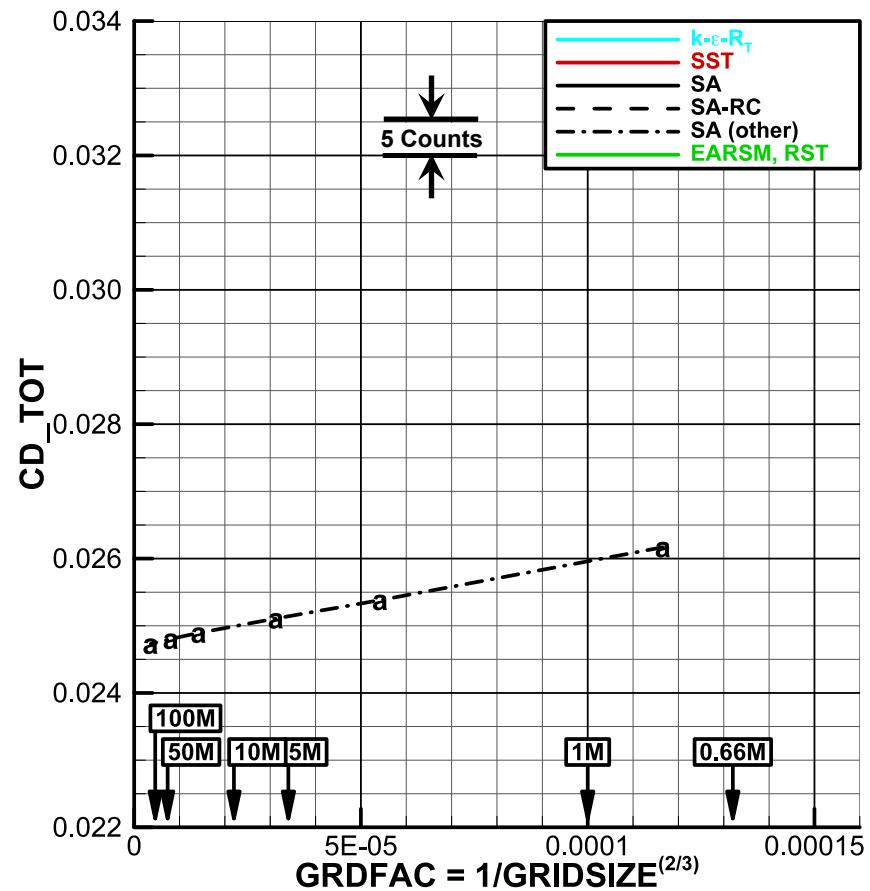
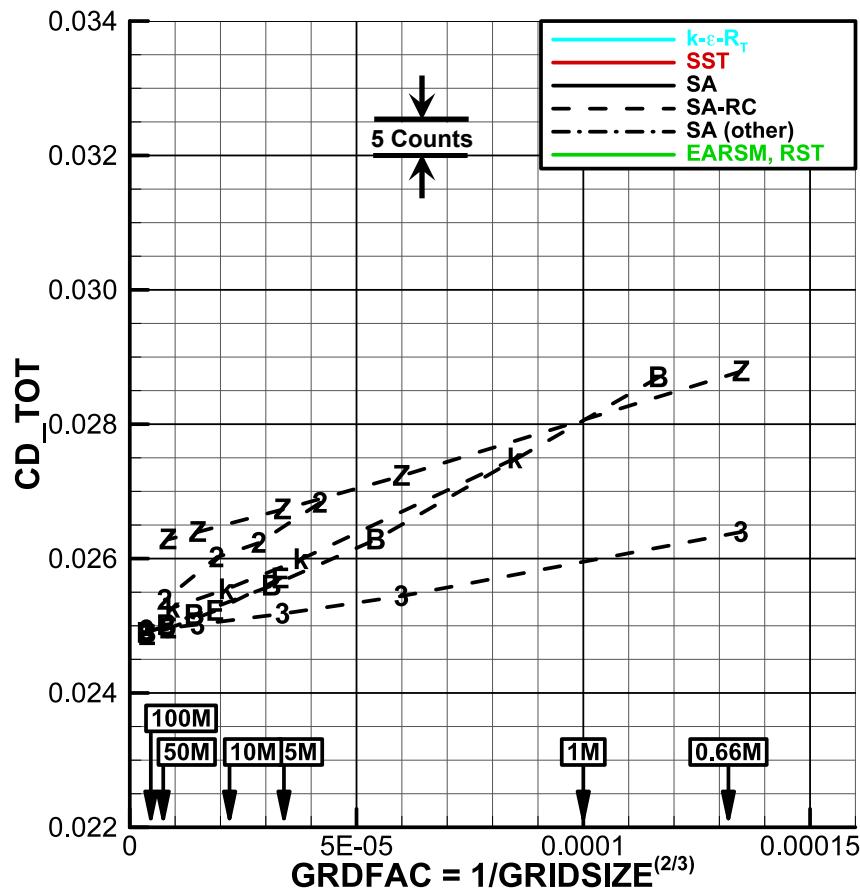
Case 1: CD_TOT – Spalart Allmaras and Shear Stress Transport Turb. Models



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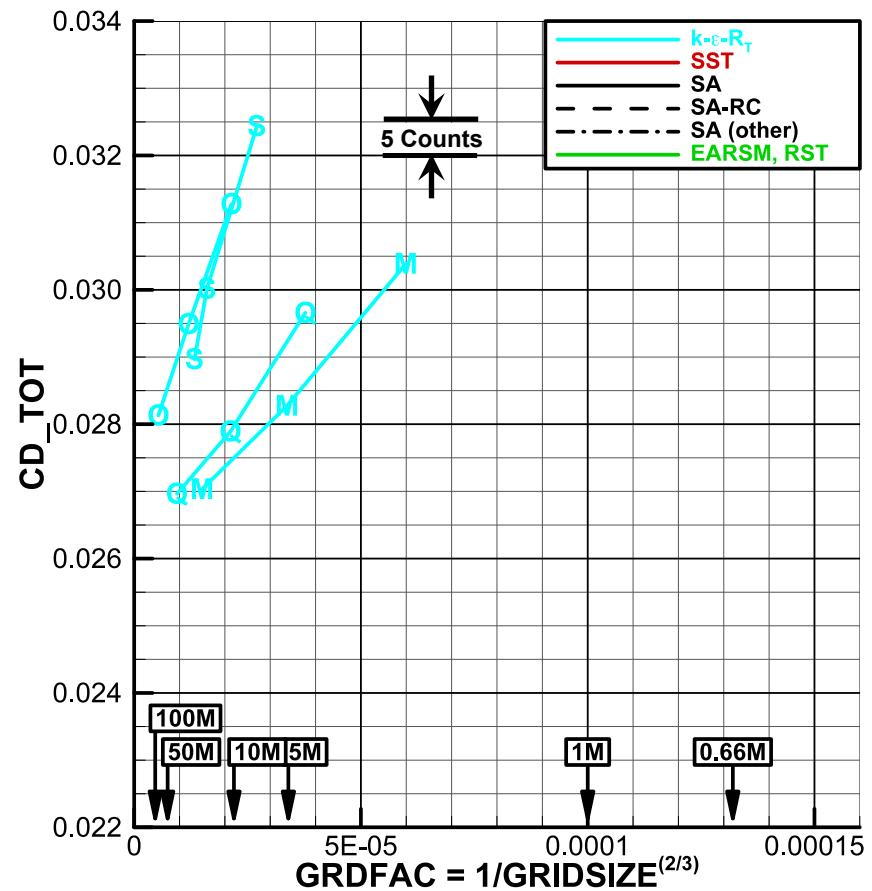
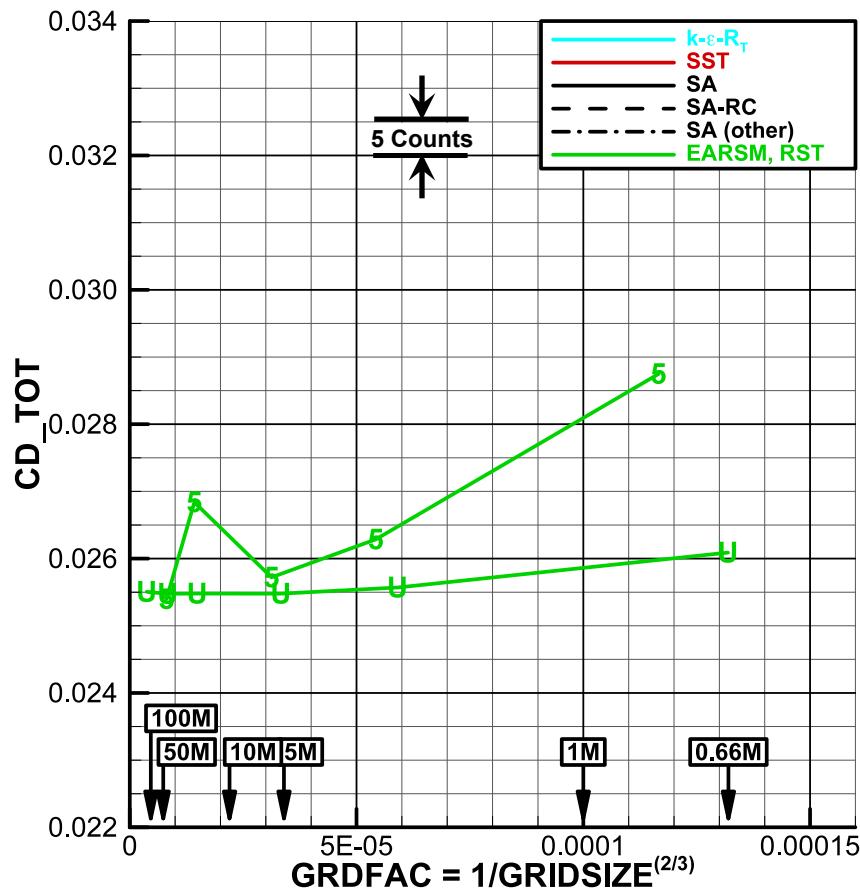
Case 1: CD_TOT – SA w/ Rotation Correction and SA other Turb. Models



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Case 1: CD_TOT – k- ε -RT and EARSM,RST Turbulence Models



Should we Compare to Wind Tunnel?

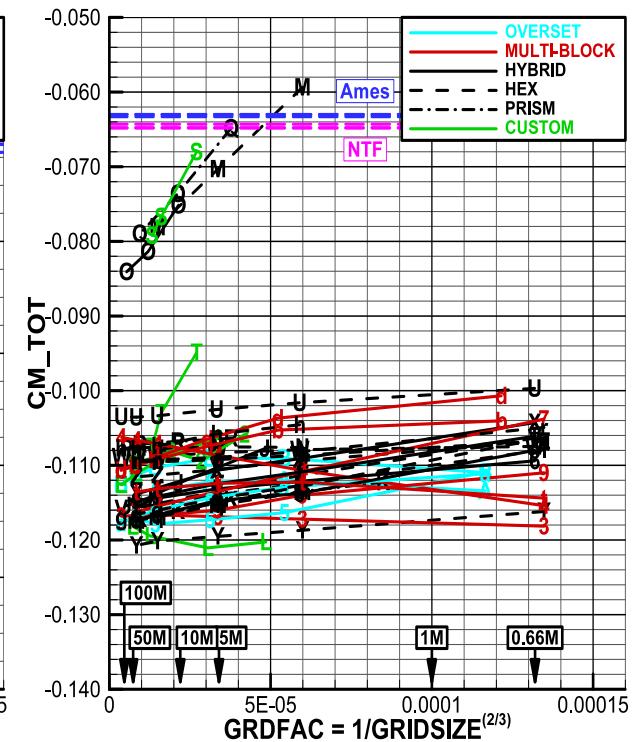
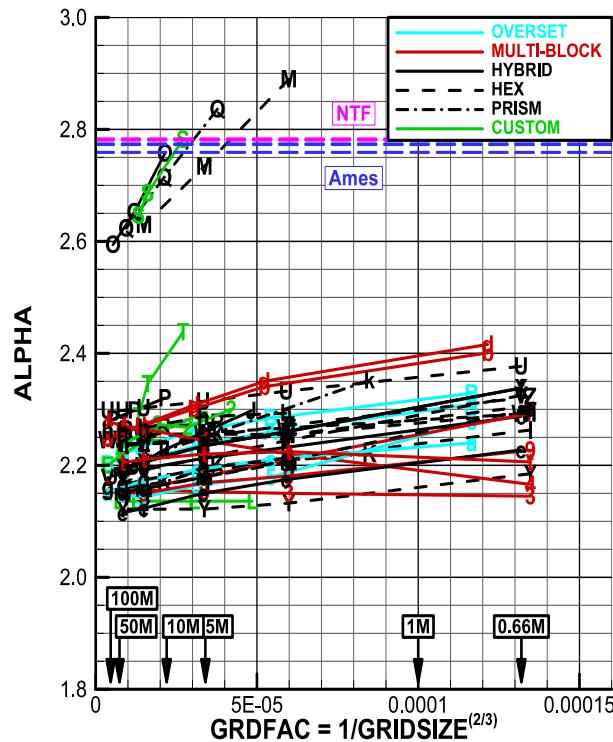
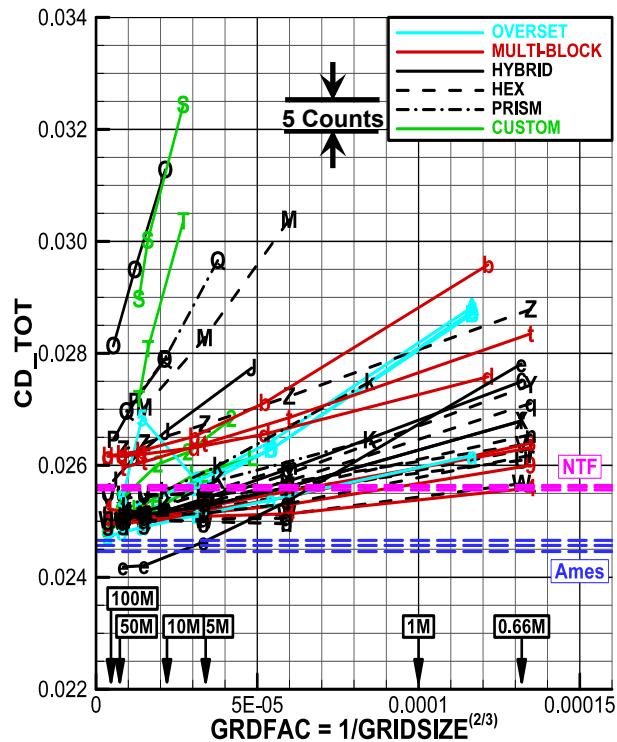
Wind Tunnel	CFD
Walls	Free Air
Support System (Sting)	Free Air
Laminar/Turbulent (Tripped)	“Fully” Turbulent (usually)
Aeroelastic Deformation	Rigid 1g Shape
Measurement Uncertainty	Numerical Uncertainty & Error
Corrections for known effects	No Corrections

- Wind Tunnel and CFD measure/compute different things!
- Data are included for reference only!

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Case 1: CD_TOT, ALPHA, and CM_TOT with Wind Tunnel Results



Wind Tunnel Results shown for Reference Only



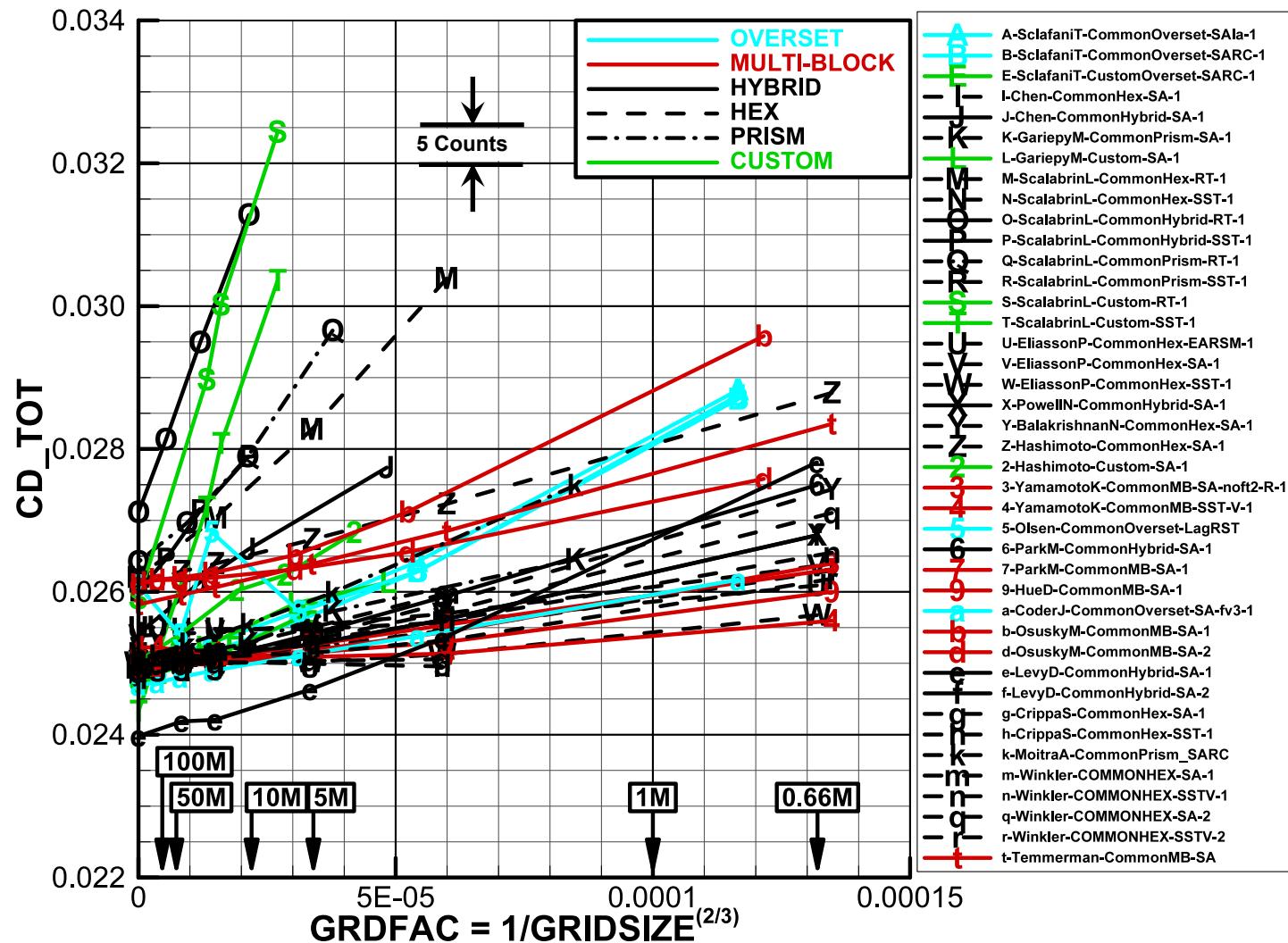
Richardson Extrapolation:

- Standard 2nd order least squares fit (Excel)
- For 2nd order codes, should be linear vs.
 $\text{Grid_Factor} = N^{-2/3}$
- Y-intercept estimates theoretical infinite resolution (continuum) result

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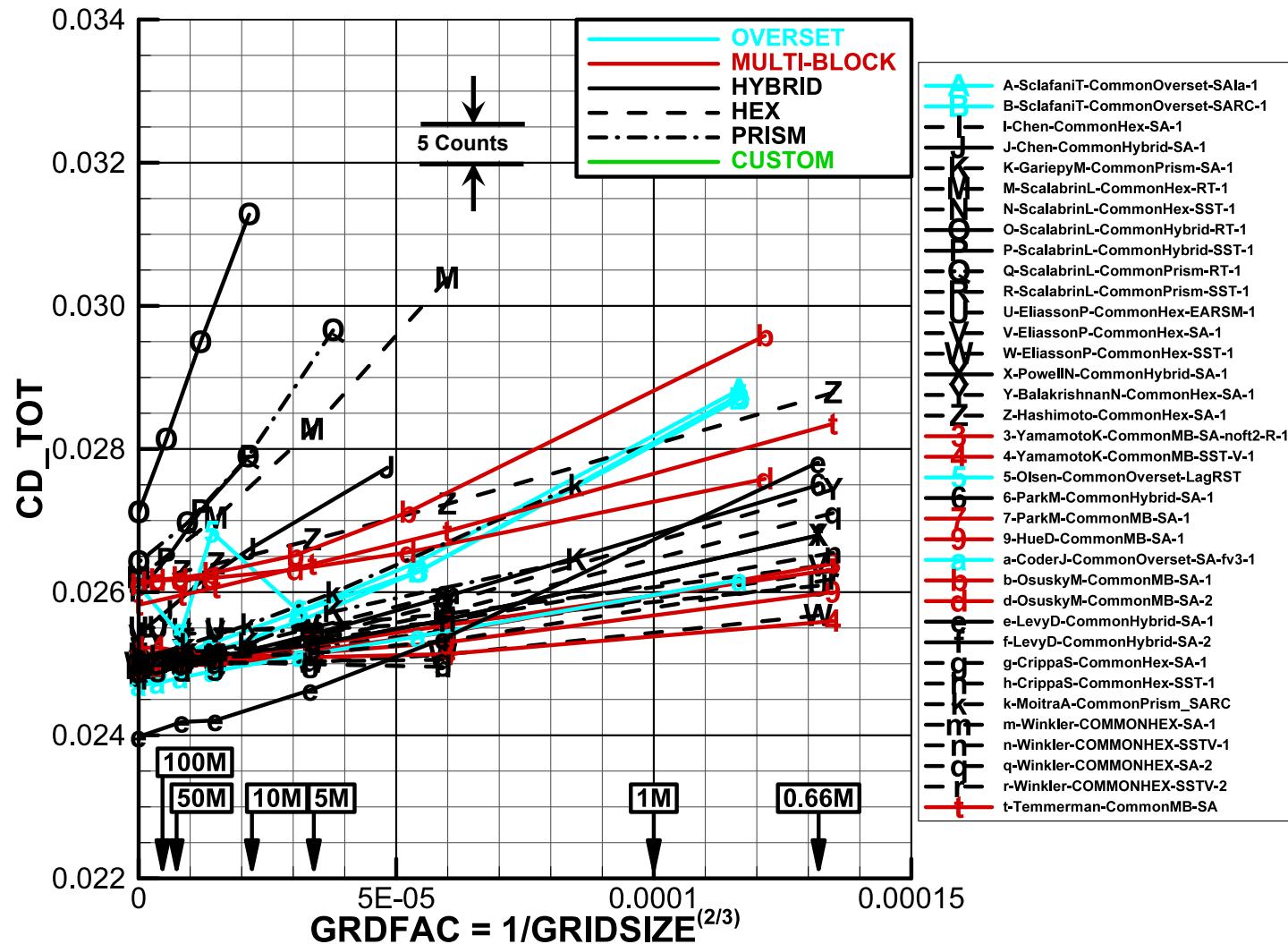
Case 1: Extrapolated CD_TOT by Grid Type



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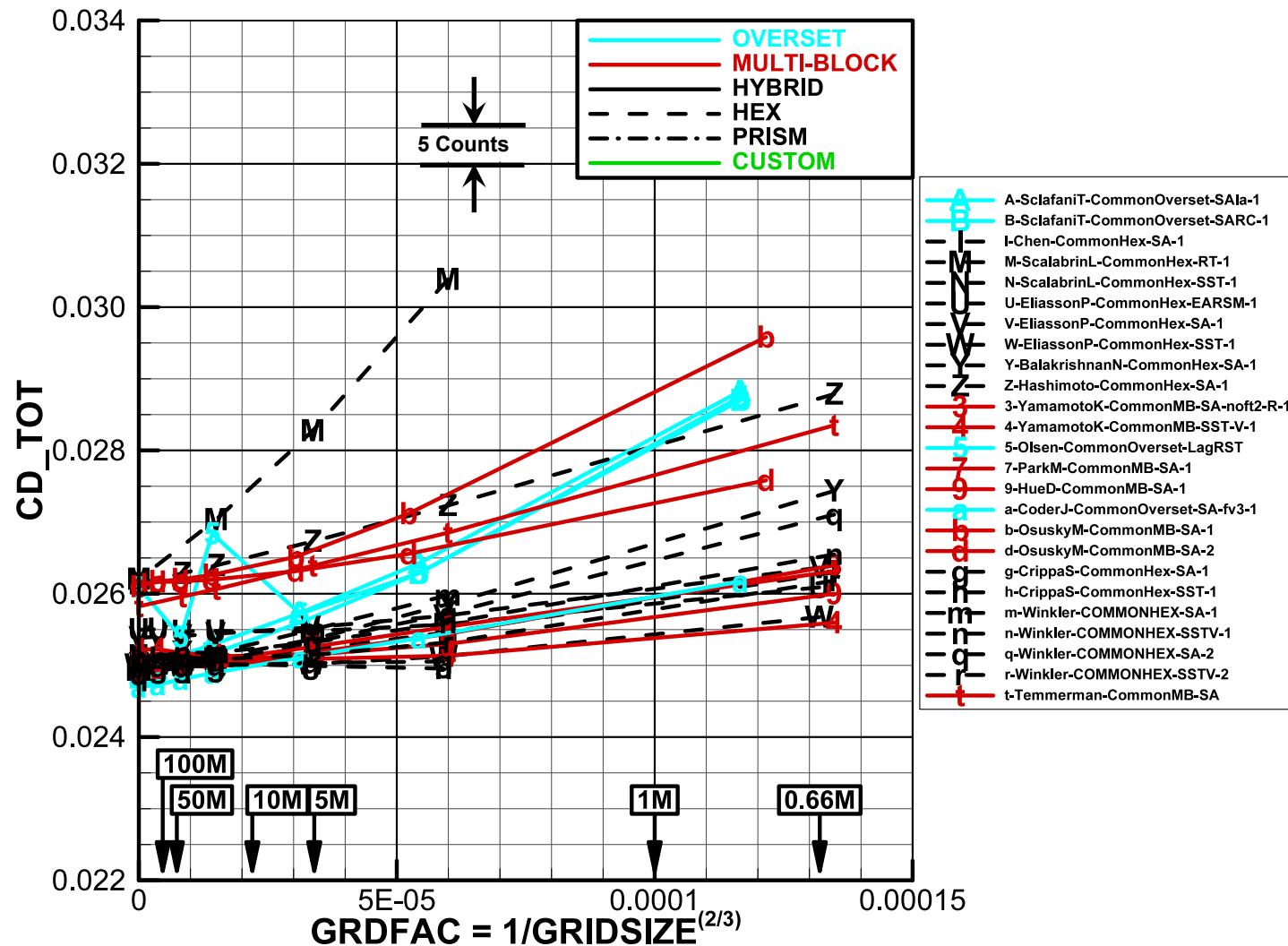
Case 1: Extrapolated CD_TOT by Grid Type (Common Grids Only)



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Case 1: Extrapolated CD_TOT by Grid Type (Common Hex Grids Only)





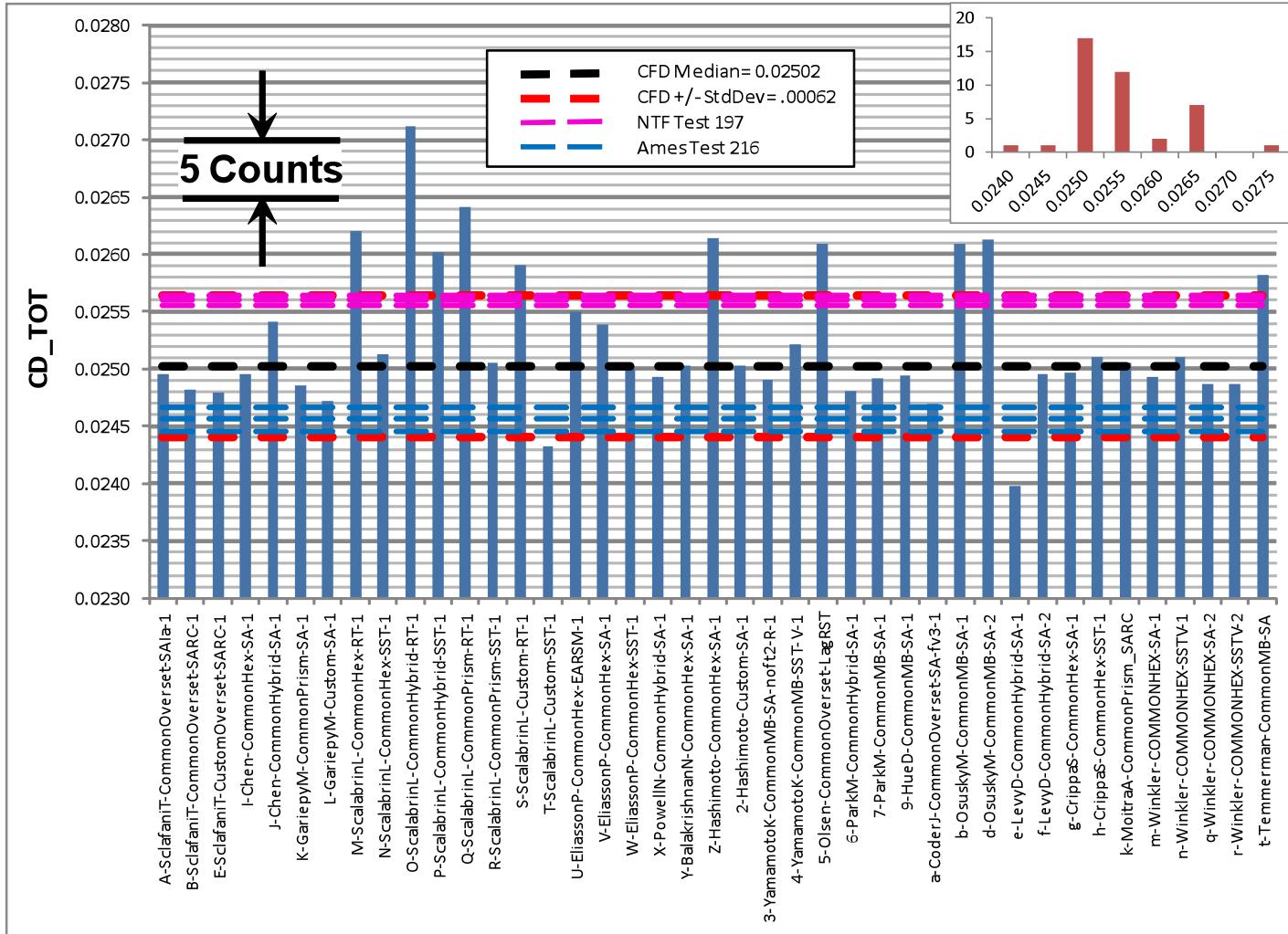
Conclusions from Richardson Extrapolation:

- Most results are monotonically decreasing
- Some are nonlinear
 - Convergence issues
 - Possible flow-feature changes (SOB or TE Separation)
- No clear break-outs with grid type or turbulence model (except for some outliers)
- Scatter is reduced somewhat for Common Grids
 - Scatter still large for coarser grids
 - Best for Hex-based, including Structured, Overset, and Unstructured

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Case 1: Extrapolated CD_TOT Statistics





Conclusions from Case 1 Results:

- Still a lot of scatter!
 - Less than DPW4 (was $\sigma=8.1$ for tail on). Are we getting better?
- No clear break-outs with grid type or turbulence model
 - Some Turb. Models are outliers
 - Trends are still hard to isolate due to small sample sizes
- Agreement with experiment on CD_TOT is better than for ALPHA and CM_TOT
 - Wing aeroelastic effects are likely part of this
 - Spread in CD_TOT is similar between wind tunnel and CFD scatter
- Scatter is reduced somewhat for Common Grids
 - Statistics did not change significantly
 - Best for Hex-based, including Structured, Overset, and Unstructured
 - Discretization and Turbulence Modeling is still a major contributor

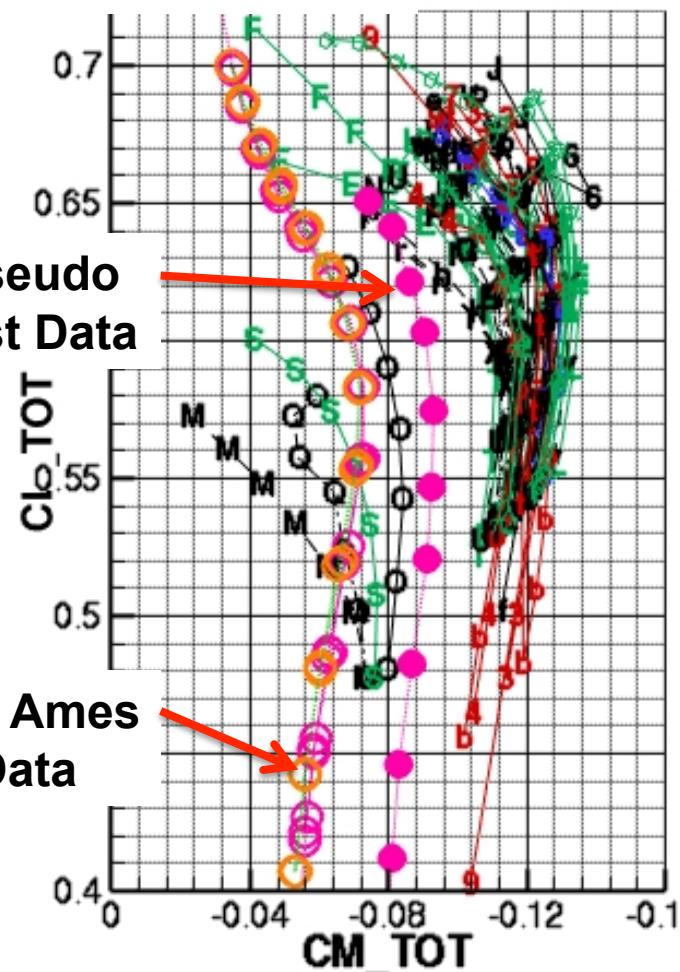
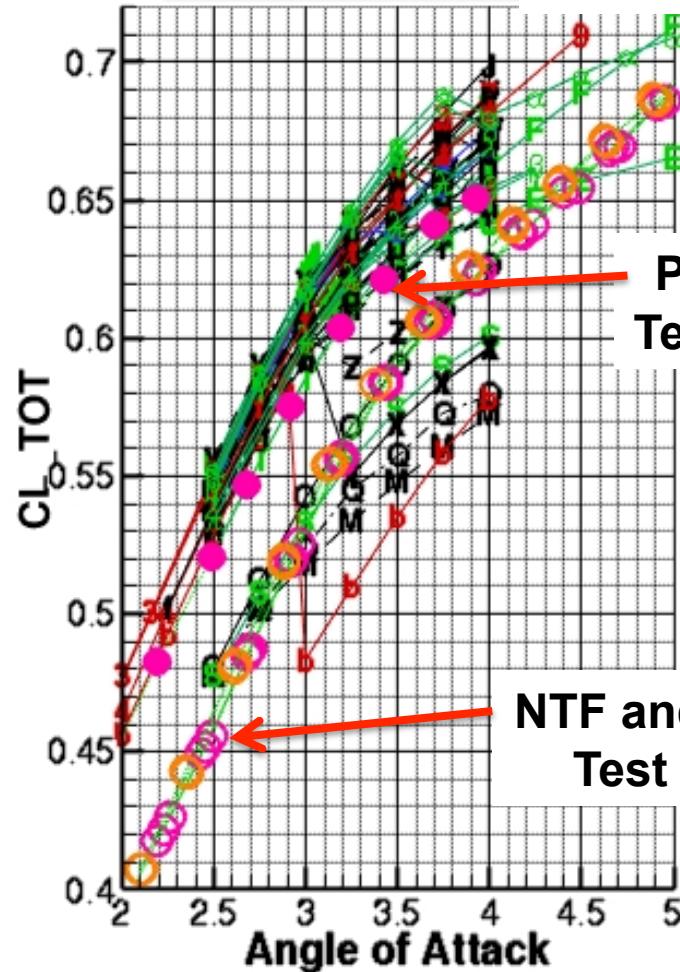
Case 2 Buffet Study:

- NASA Common Research Model, Wing-Body
- Mach=0.85:
 - $\alpha=2.50^\circ, 2.75^\circ, 3.00^\circ, 3.25^\circ, 3.50^\circ, 3.75^\circ, 4.00^\circ$
- Grid Resolution Level:
 - 3) Medium,
- Chord Reynolds Number: 5×10^6

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Case 2 – All Solutions



Pseudo Test data based on NTF test data modified by results from AIAA-2012-3209

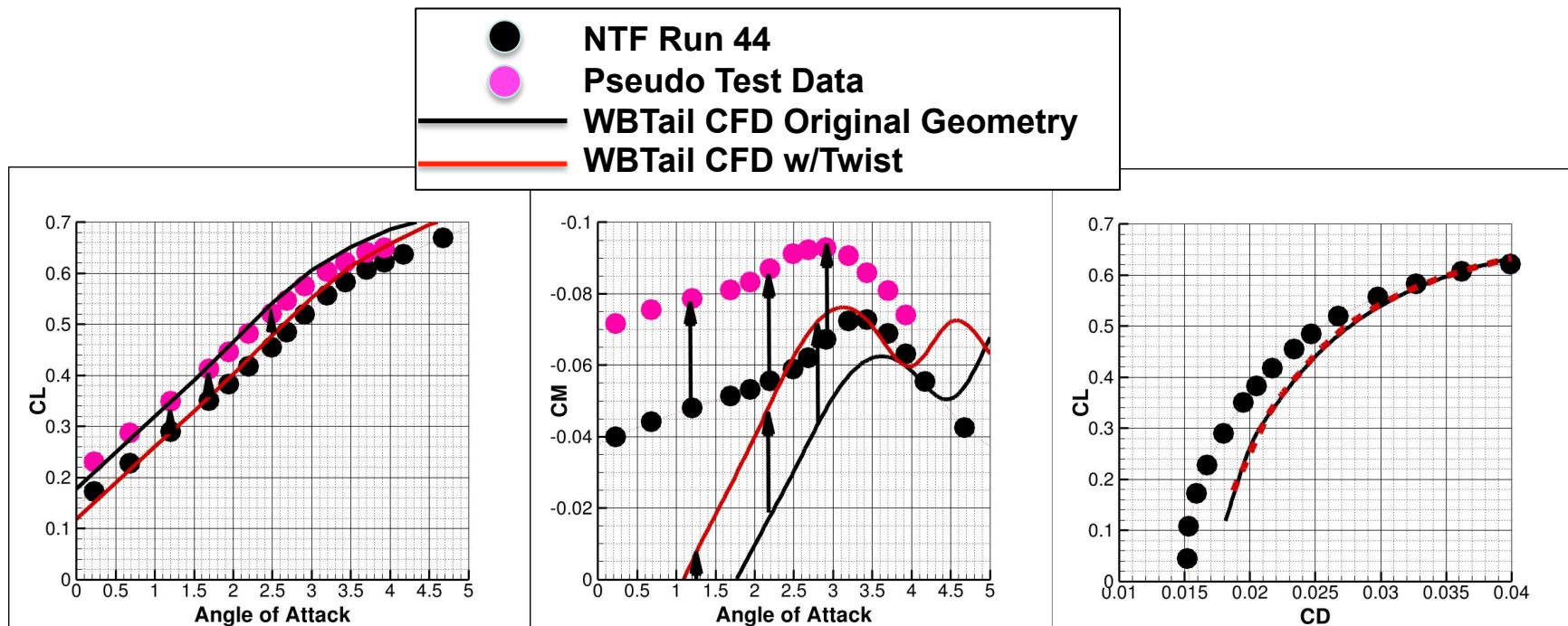
C	Overset
P	Overset
F	Overset
G	Overset
H	Overset
I	Overset
J	Unstruc1
M	Unstruc1
N	Unstruc1
O	Unstruc1
P	Unstruc1
Q	Unstruc1
R	Unstruc1
S	Unstruc1
T	Unstruc1
U	Unstruc1
V	Unstruc1
W	Unstruc1
X	Unstruc1
Y	Unstruc1
Z	Unstruc1
1	Unstruc1
2	Unstruc1
3	Struc1
4	Struc1
5	Overset
6	Unstruc1
7	Struc1
8	Unstruc1
9	Overset
a	Struc1
b	Struc1
c	Unstruc1
d	Unstruc1
e	Unstruc1
f	Unstruc1
g	Unstruc1
h	Unstruc1
i	Unstruc1
j	Unstruc1
k	Unstruc1
m	Unstruc1
o	Unstruc1
q	Unstruc1
r	Unstruc1
t	Struc1
u	Unstruc1
v	Unstruc1
w	Unstruc1
x	Unstruc1
y	Unstruc1
z	Unstruc1
1	Unstruc1
2	Pseudo Test
3	NTF Test

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CREATION OF “PSEUDO TEST DATA”

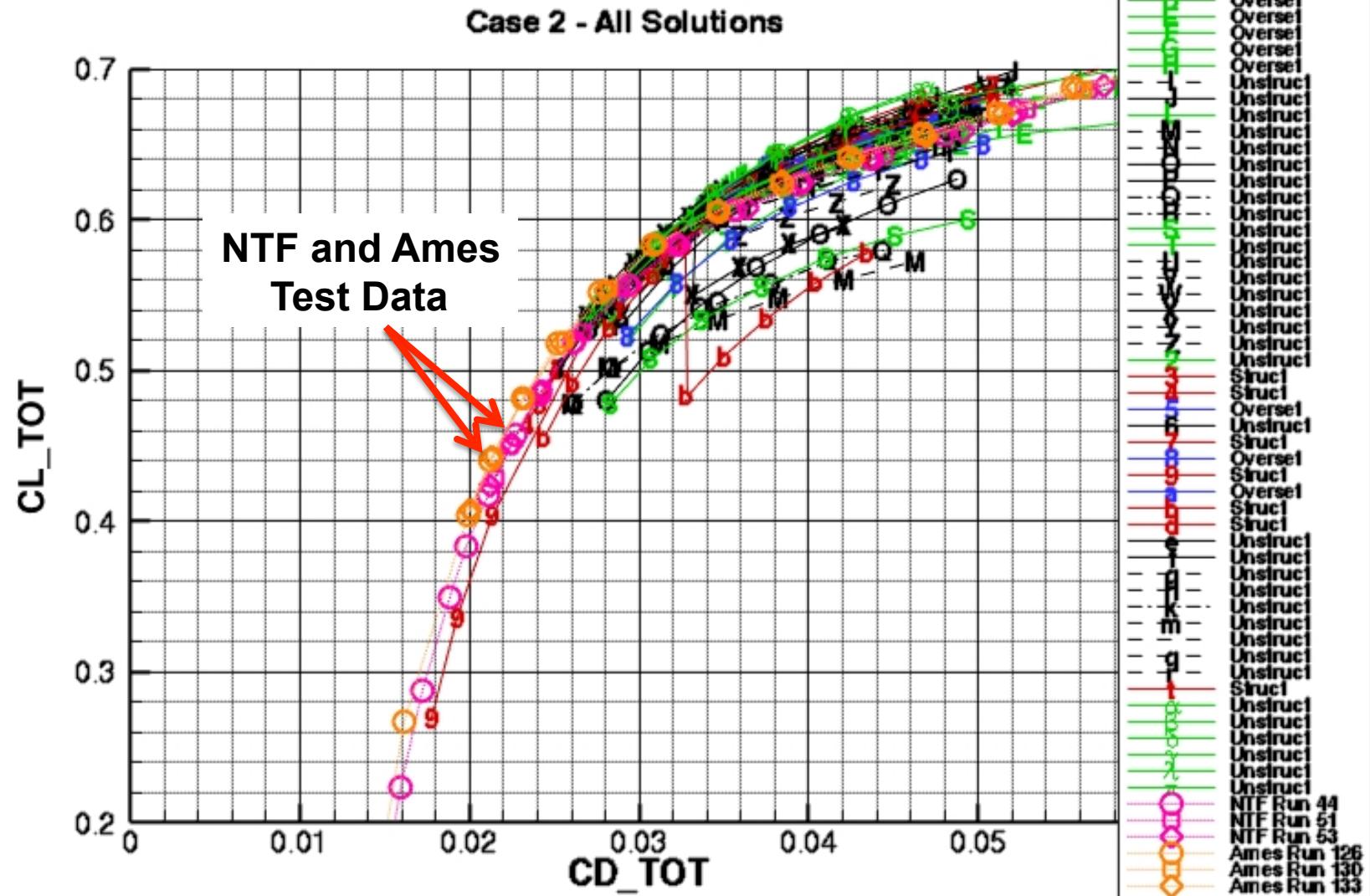
- The CRM geometry used for DPW5 was that of the wind tunnel model definition
- AIAA-2012-3209 details recent CFD analyses to account for the wing aeroelastic twist at Mach=0.85, CL=0.50, and for additional wind tunnel mounting system effects.
- “Pseudo Test Data” were created from the NTF data and CFD analyses to reflect what the test data might look like for the wing without the “CL=0.50 aeroelastic” twist.



- No corrections were applied to drag data

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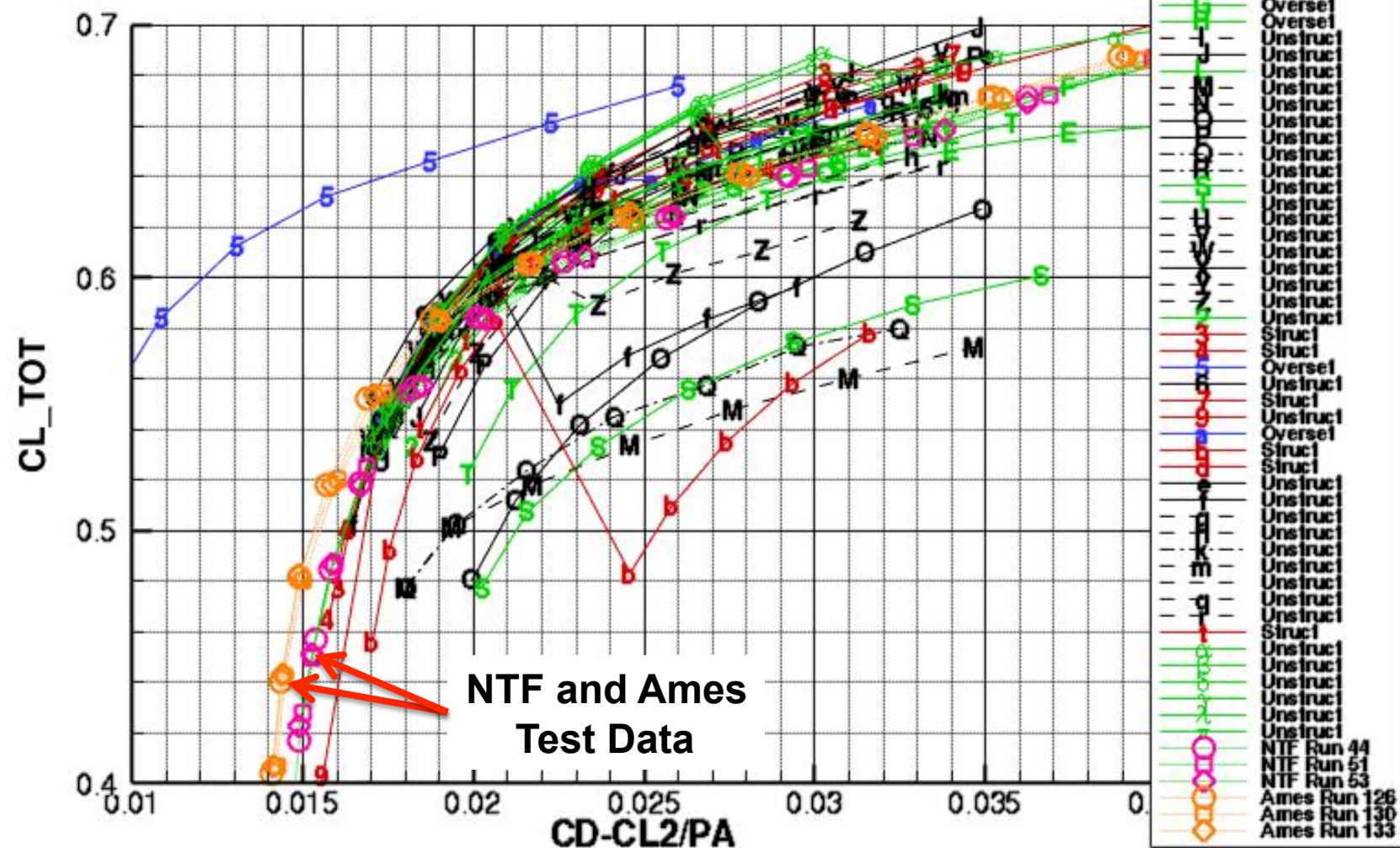
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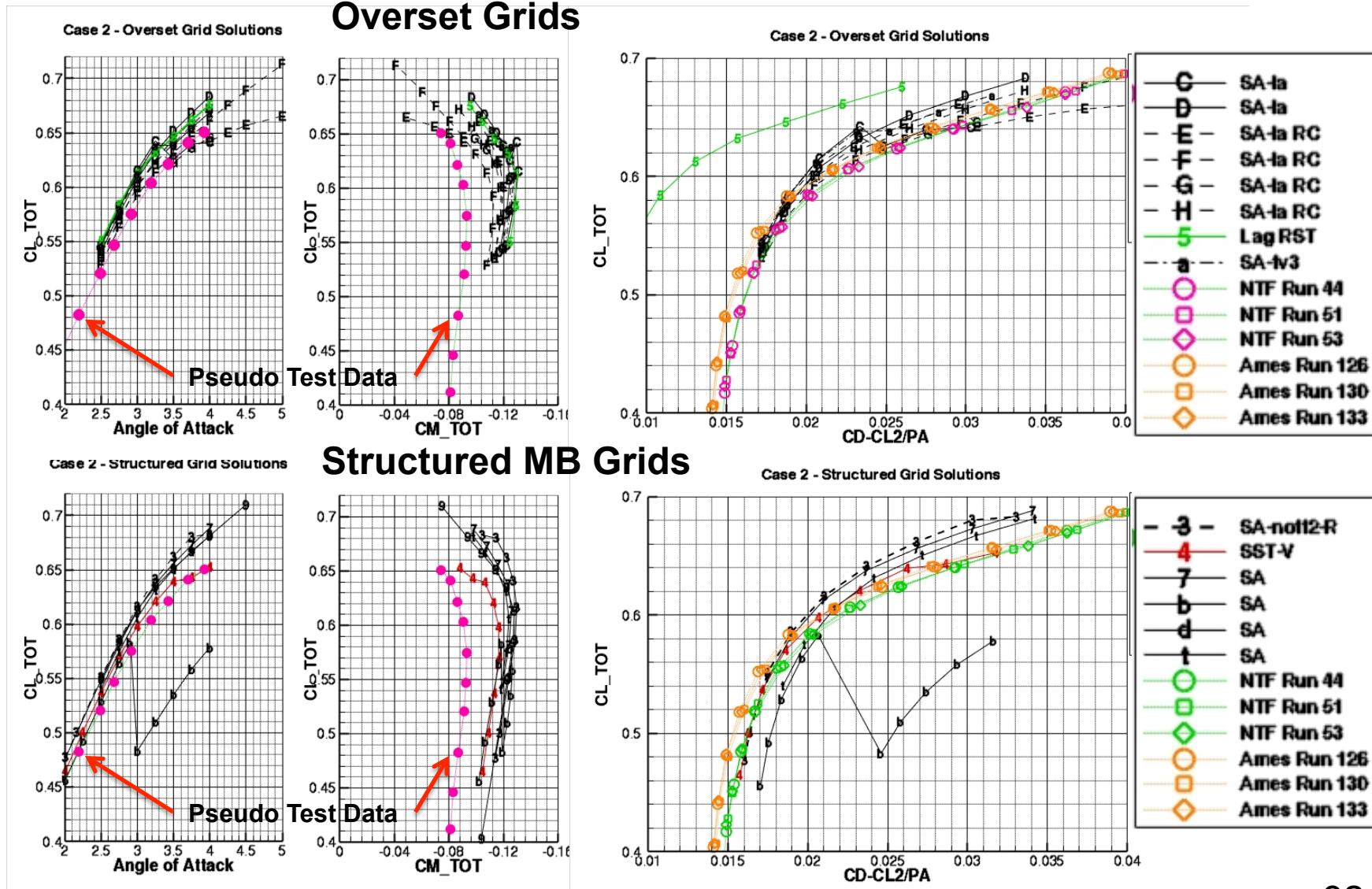
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Case 2 – All Solutions



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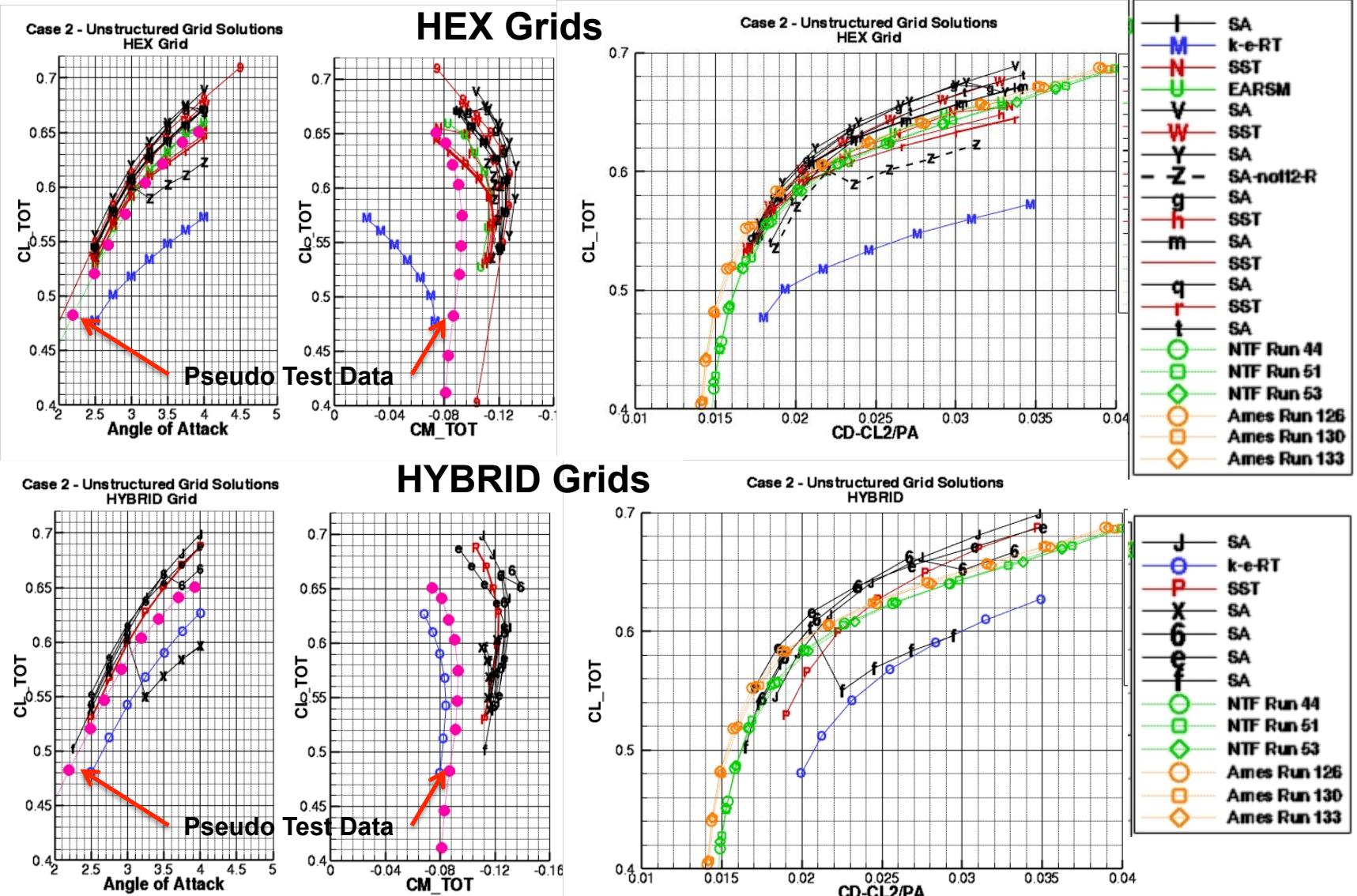
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Pseudo Test data based on NTF test data modified by results from AIAA-2012-3209

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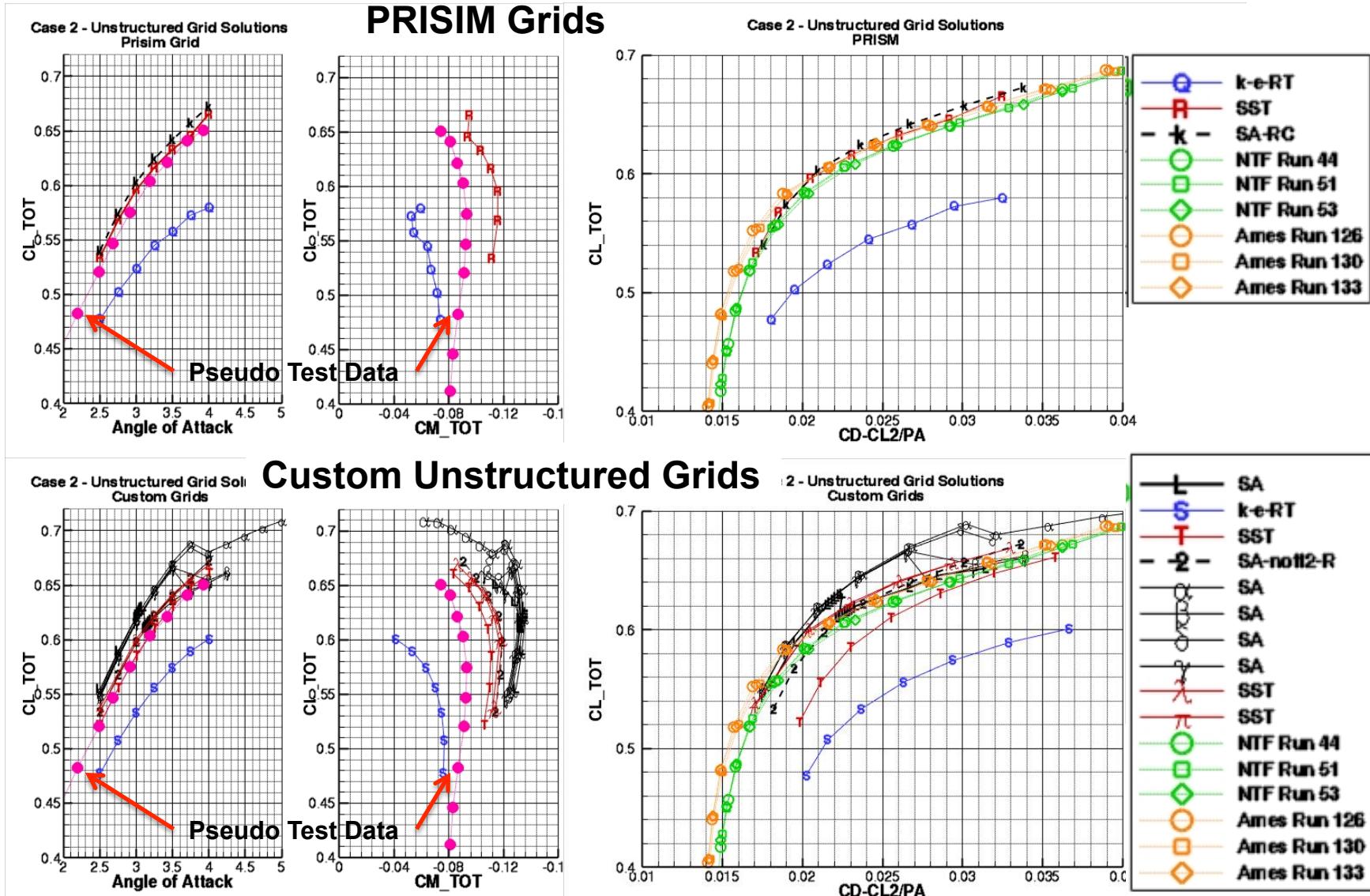
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Pseudo Test data based on NTF test data modified by results from AIAA-2012-3209

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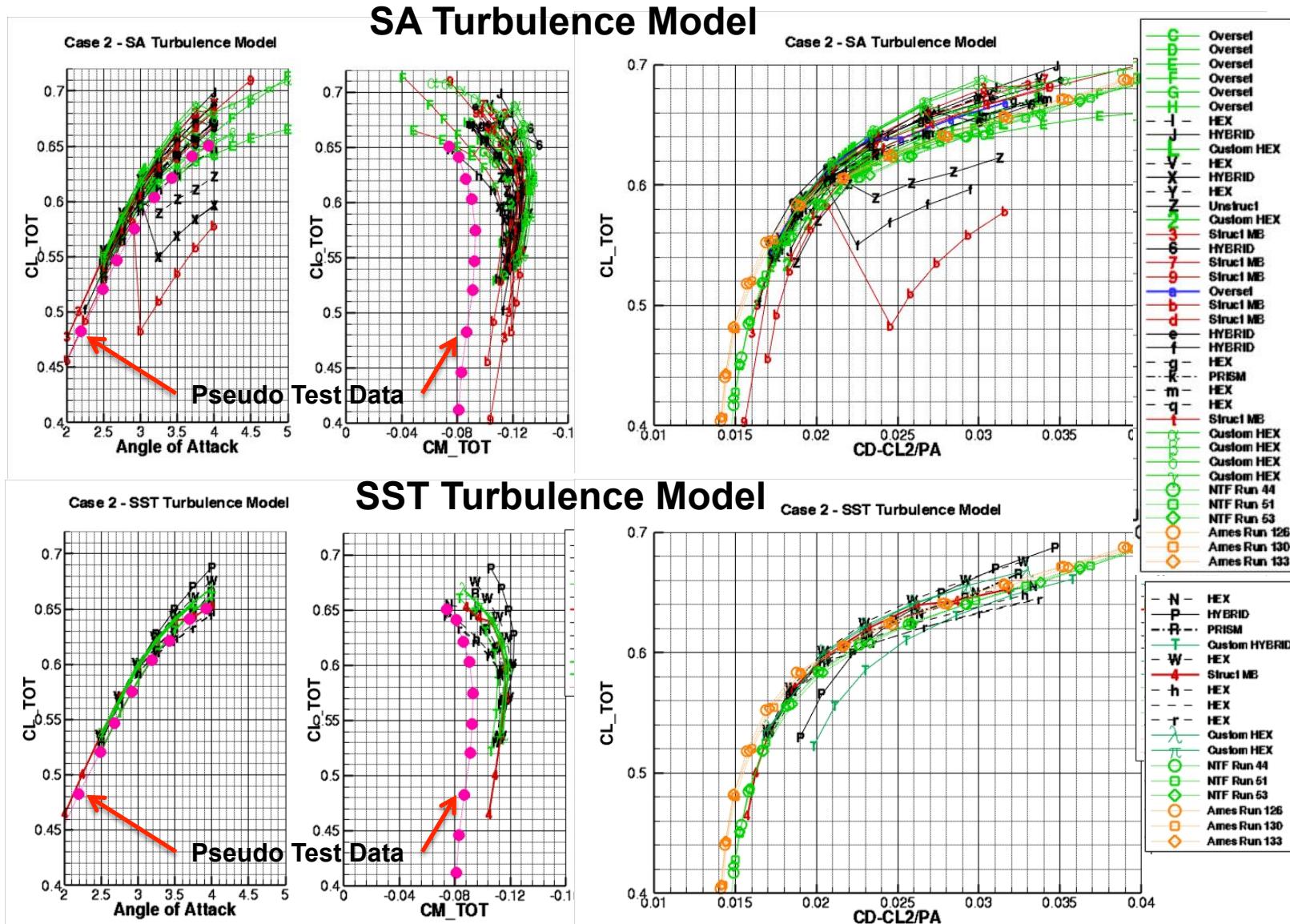
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Pseudo Test data based on NTF test data modified by results from AIAA-2012-3209

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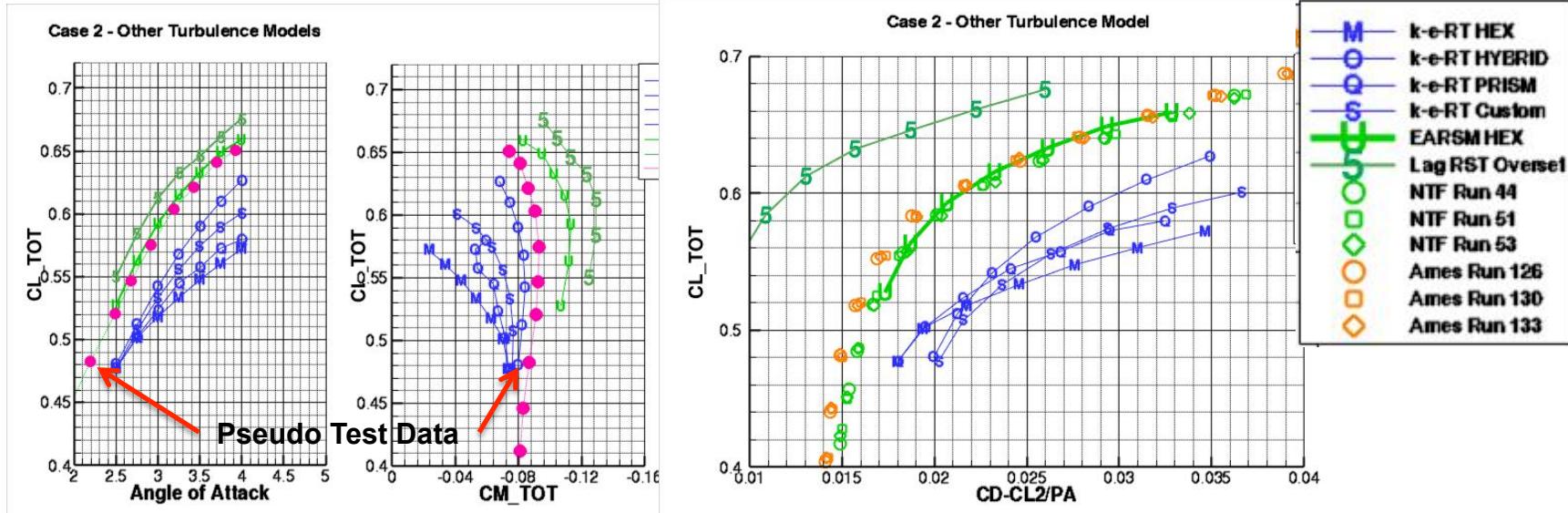


Pseudo Test data based on NTF test data modified by results from AIAA-2012-3209

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Other Turbulence Models

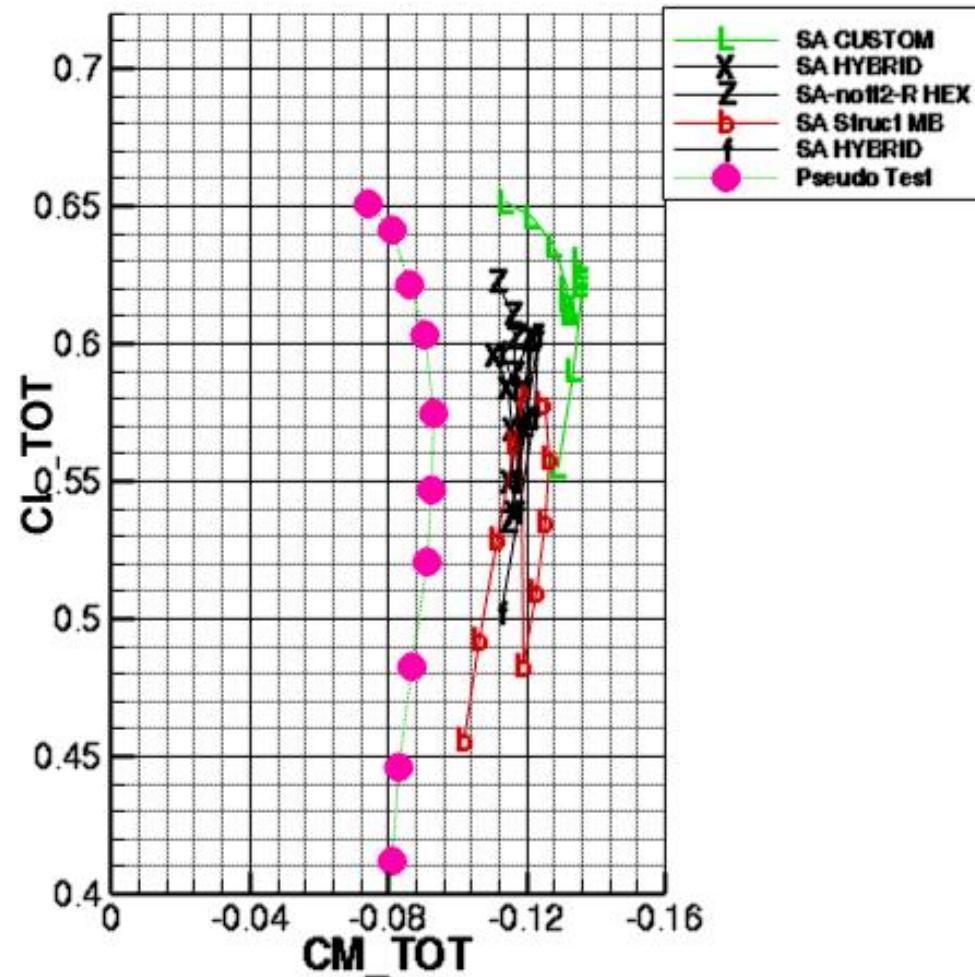
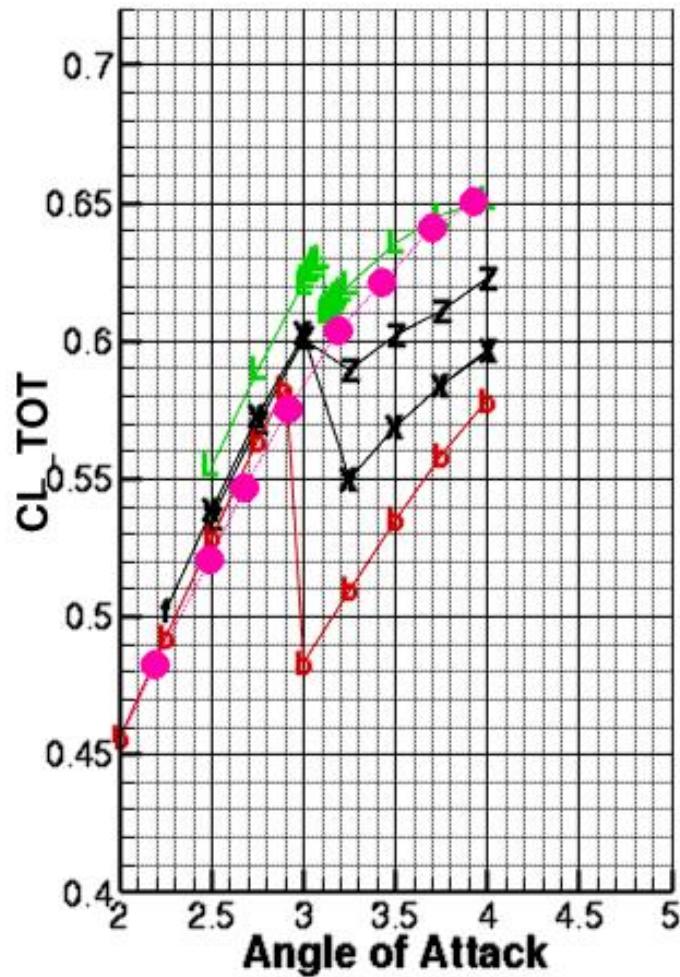


Pseudo Test data based on NTF test data modified by results from AIAA-2012-3209

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Case 2 - CL Break AoA=3.0 or Lower

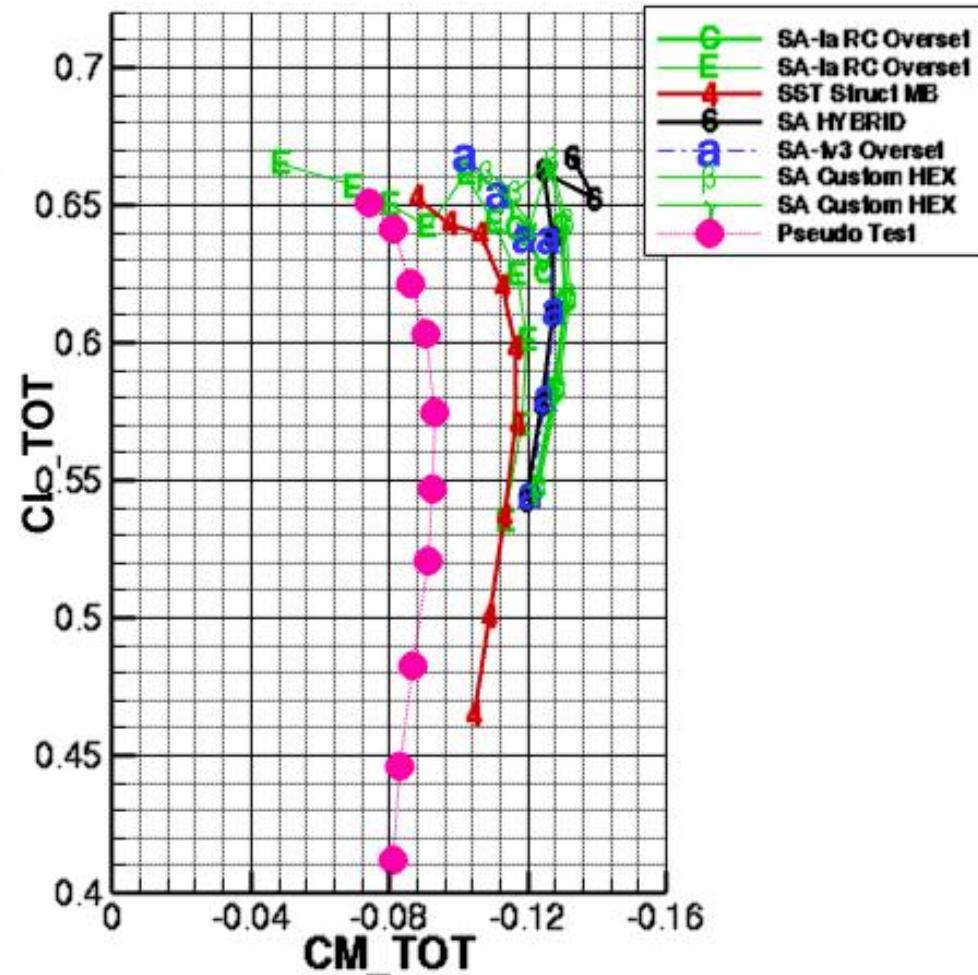
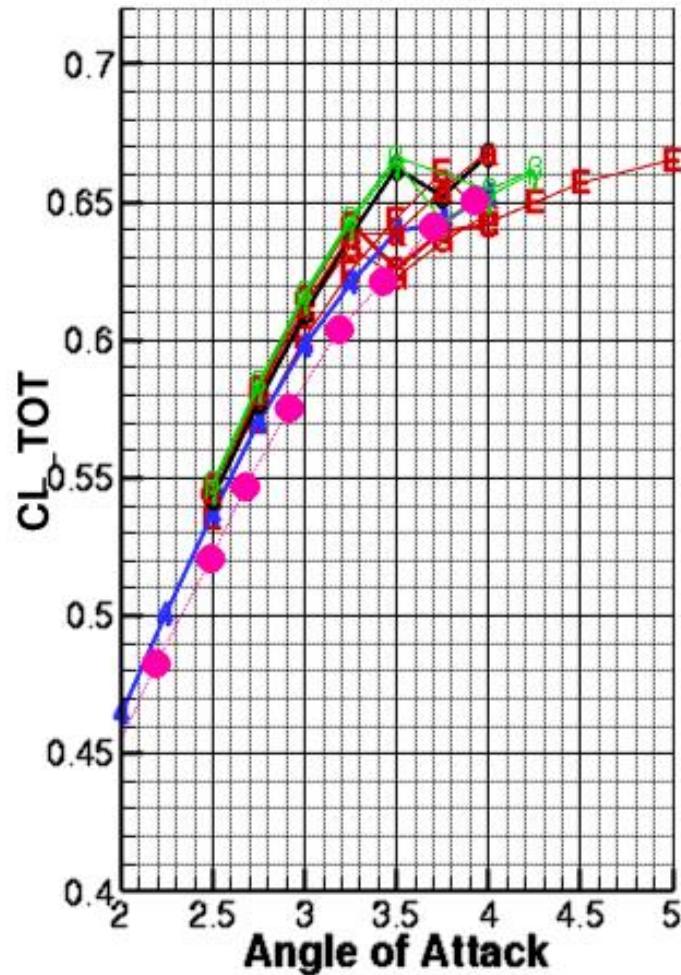


Pseudo Test data based on NTF test data modified by results from AIAA-2012-3209

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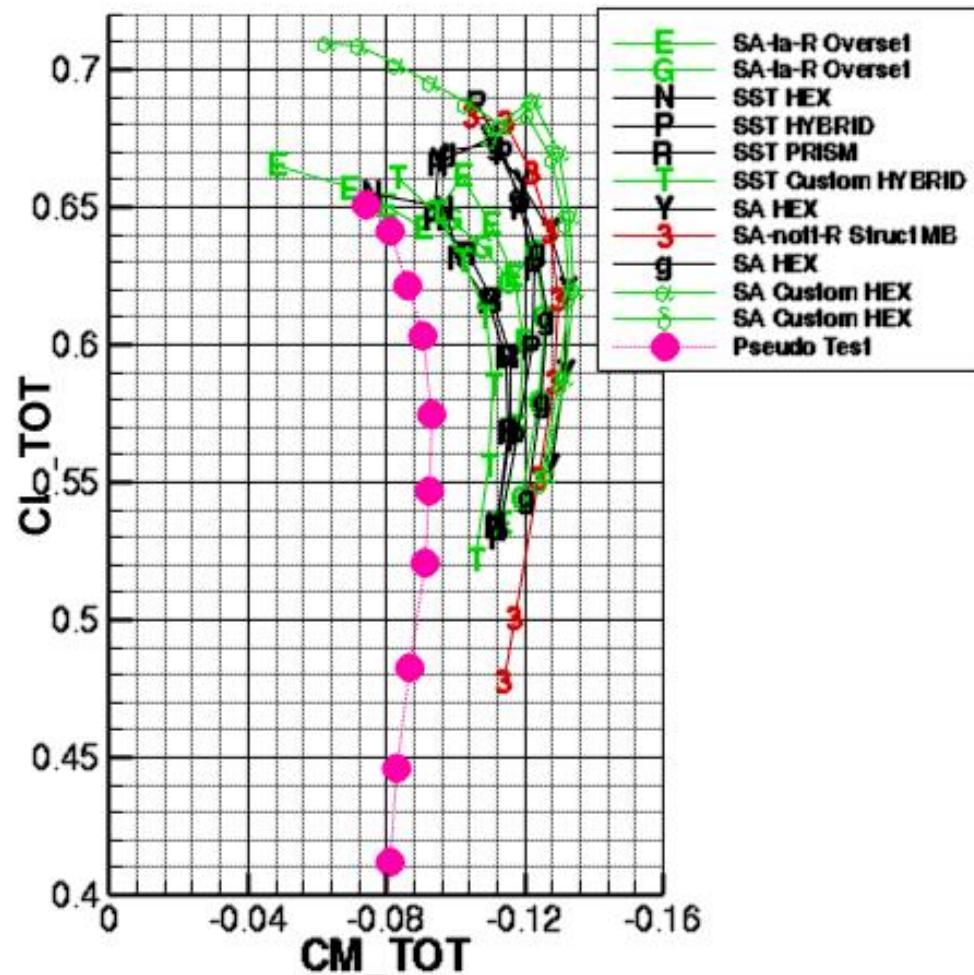
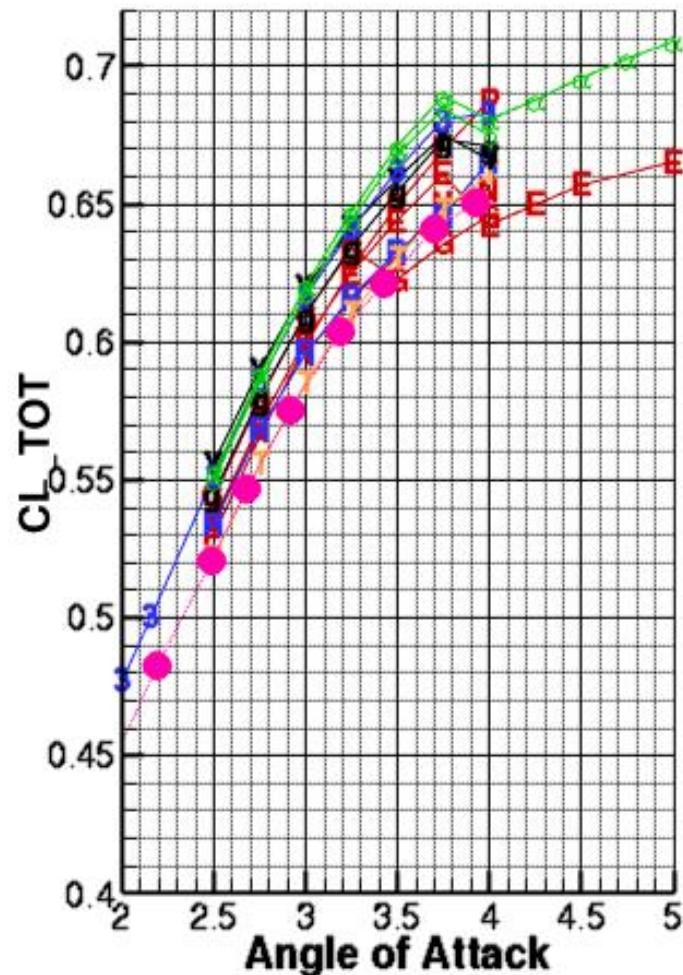
**Case 2 - CL Break between
AoA=3.25 to 3.75**



Pseudo Test data based on NTF test data modified by results from AIAA-2012-3209

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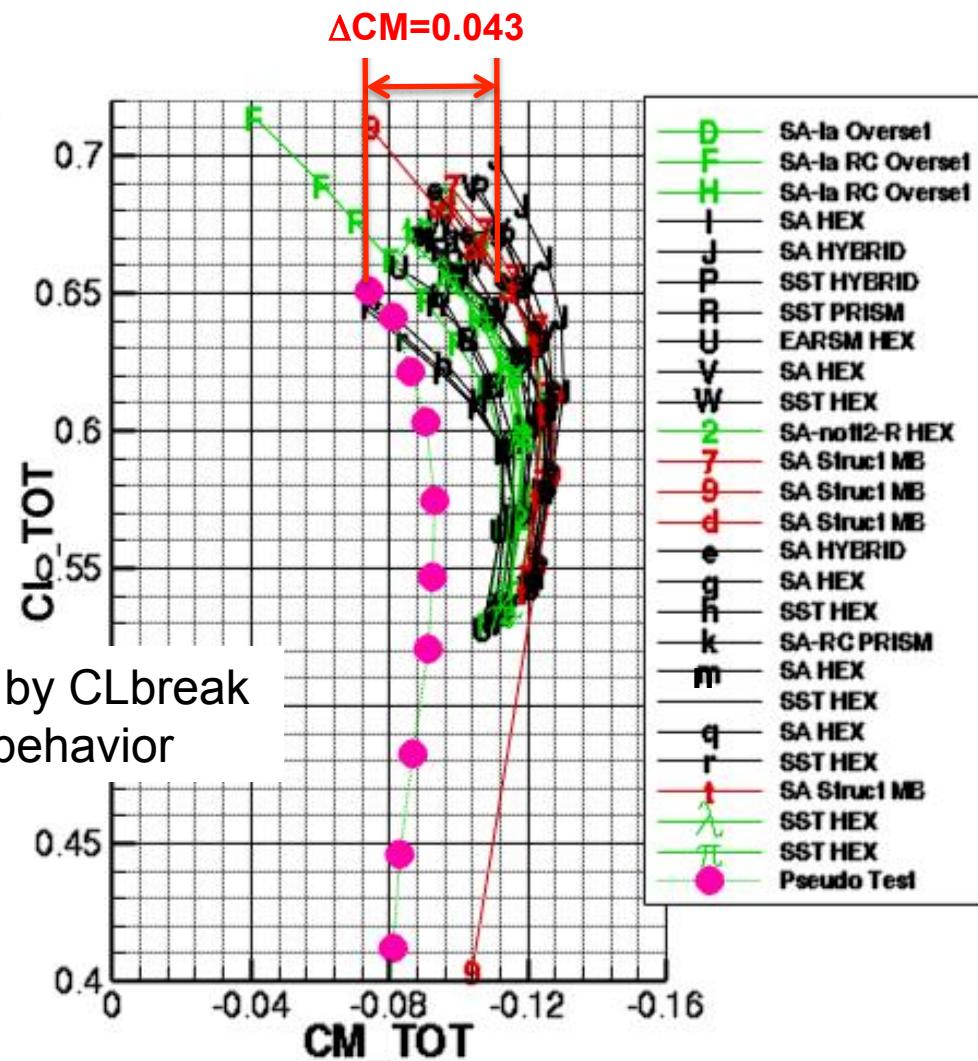
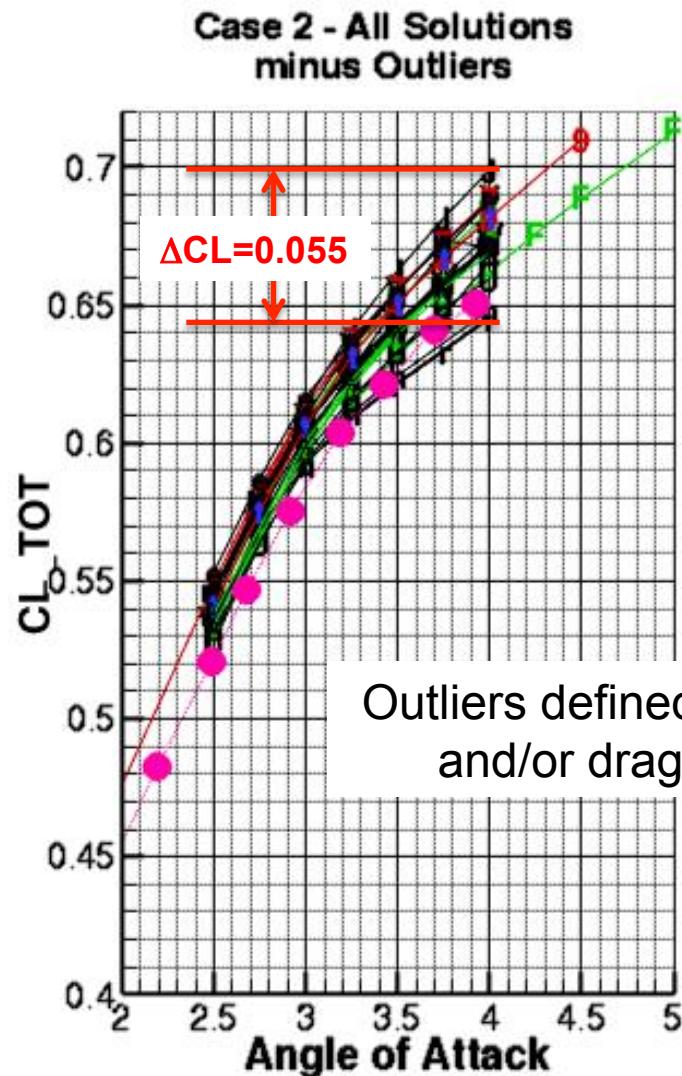
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Case 2 - CL Break AoA=3.75


Pseudo Test data based on NTF test data modified by results from AIAA-2012-3209

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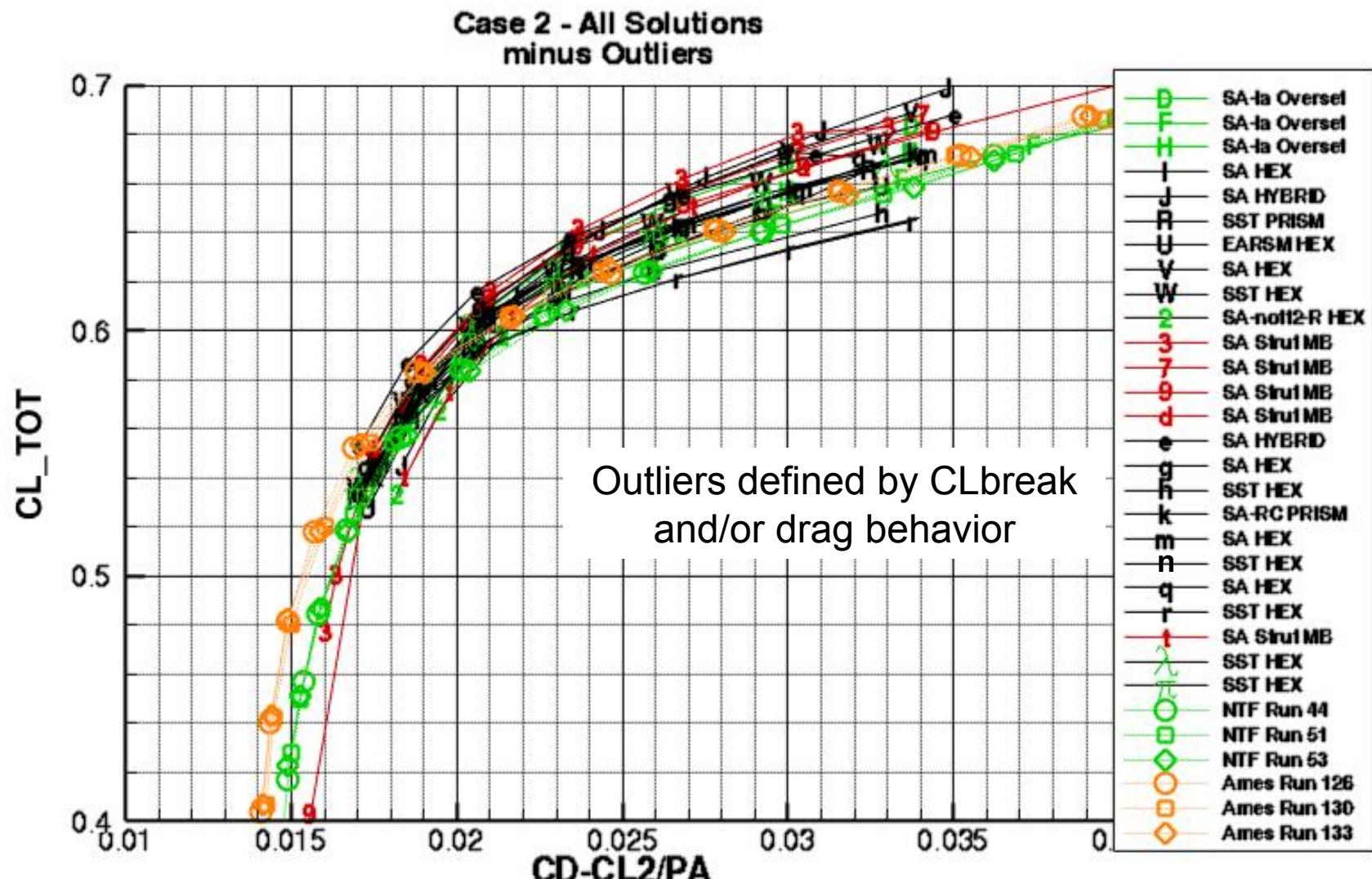


Pseudo Test data based on NTF test data modified by results from AIAA-2012-3209

)

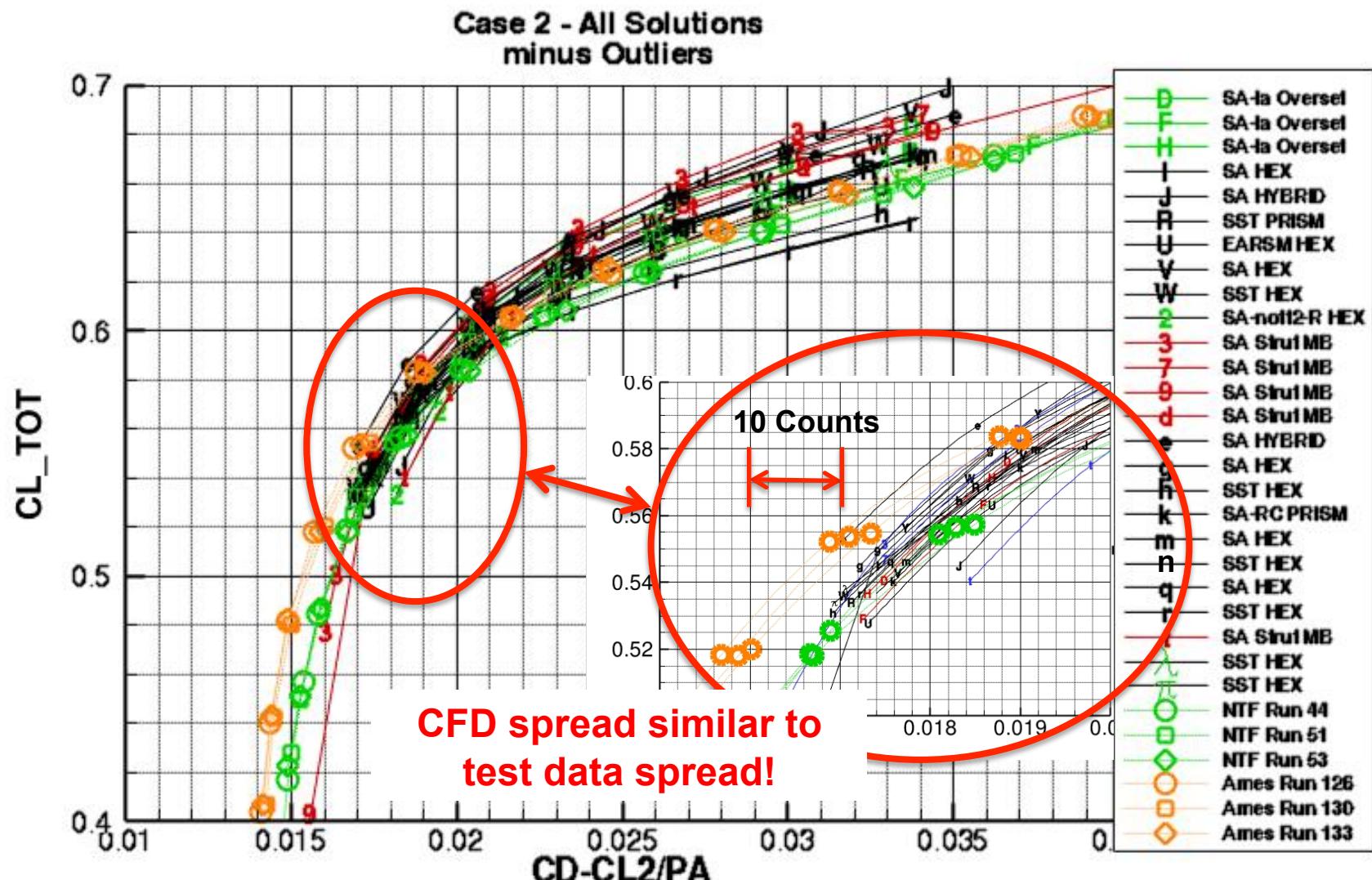
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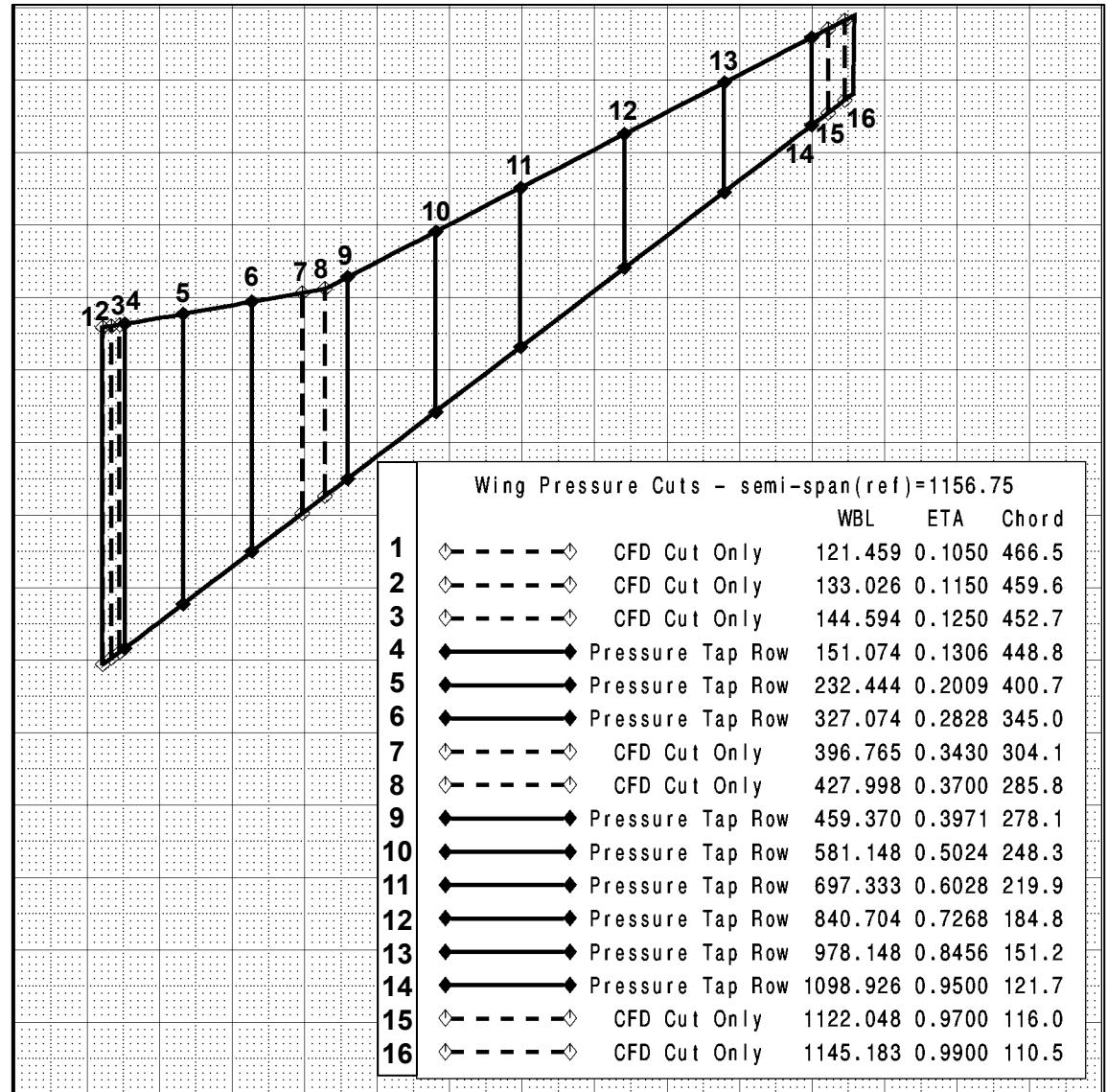
Case 2 - Concluding Remarks

- No clear break-outs with grid type or turbulence model (except for some outliers)
- In general, the k-e-RT and Lag RST results tend outside the norm of the other solutions.
- For all solutions minus outliers
 - Relatively tight forces and moment at $\alpha=2.5^\circ$
 - Significant force and moment spread at $\alpha=4.0^\circ$ $\Delta CL=0.055$, $\Delta CM=0.043$
- CM predicted too negative – is it CFD, test, geometry, etc.?
- Steady aeroelastic effects are significant
 - Must be included in CFD to better assess accuracy
- Wing section characteristics (section CL, CM) needed to better assess CFD
- High angles of attack characterized by significant shock induced separation
 - How steady is the real flow at these conditions? Need dynamic test data?
 - If there is a significant amount of flow unsteadiness at high angles of attack is RANS adequate or do we need URANS or DES?

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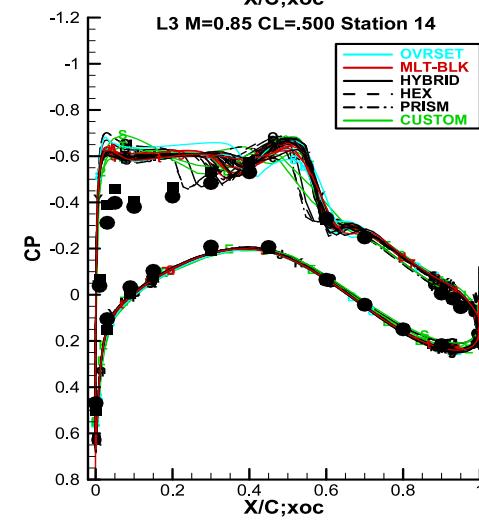
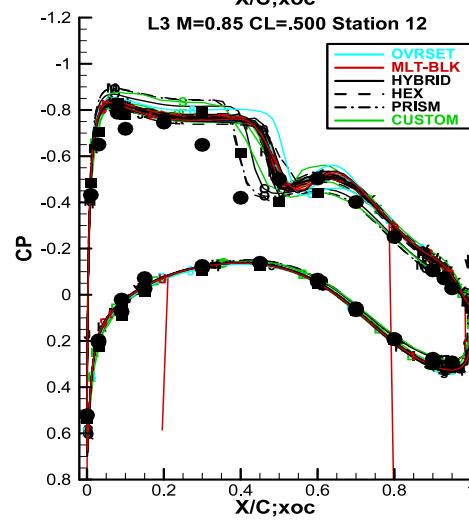
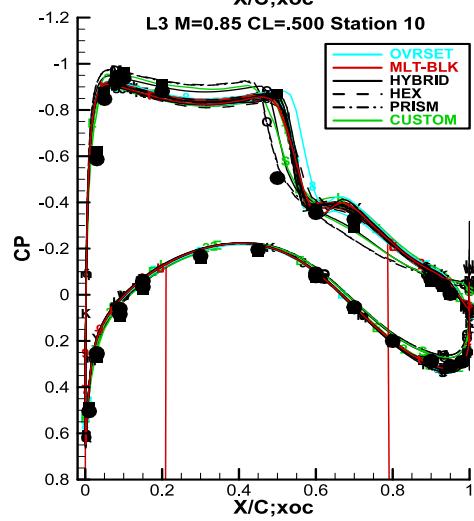
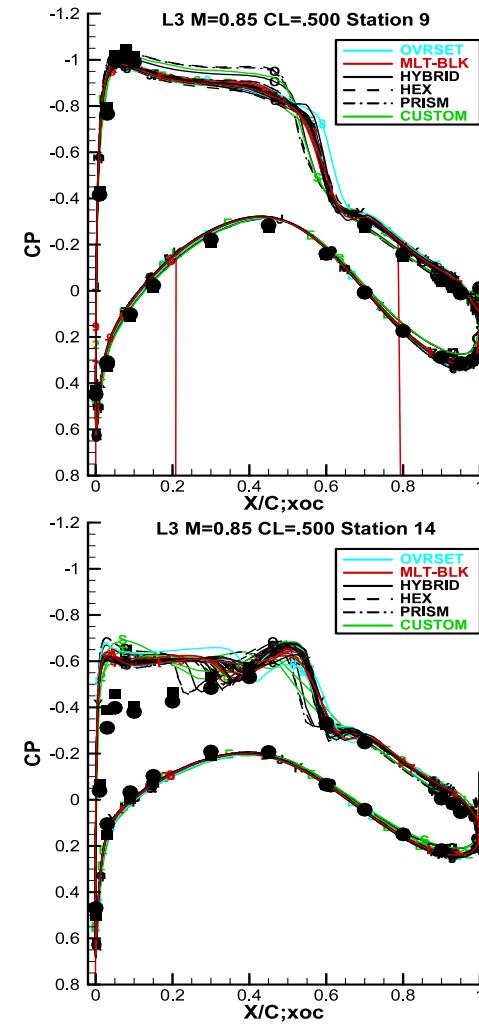
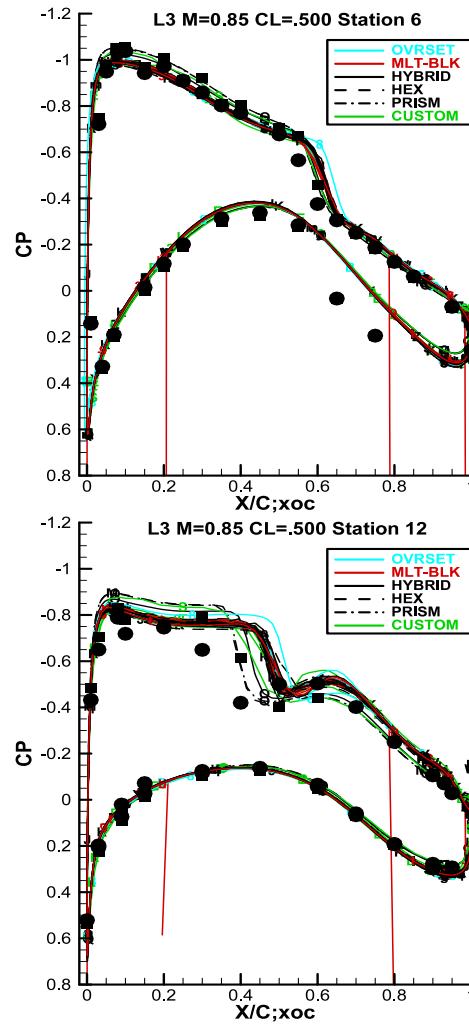
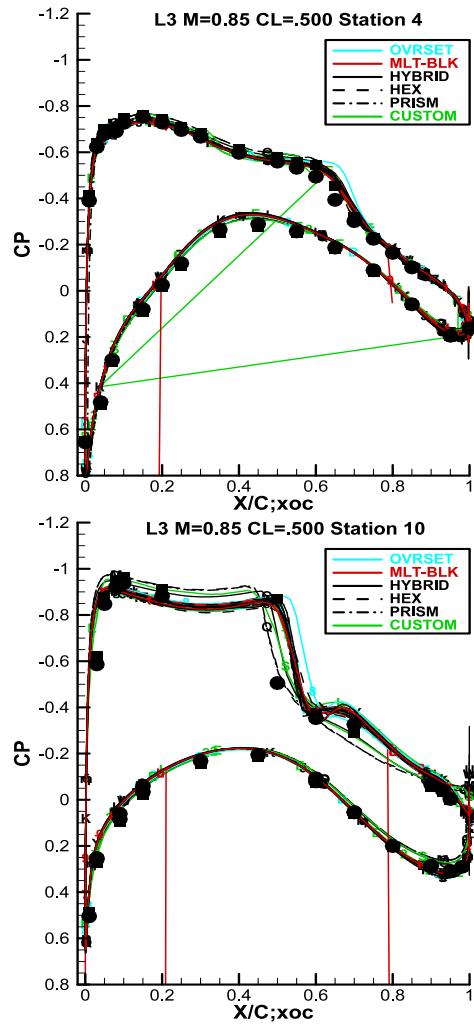
Pressure Data



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Case 1: Level 3 Grid, $M=0.85$, $C_L=.50$
 Spanwise Variation



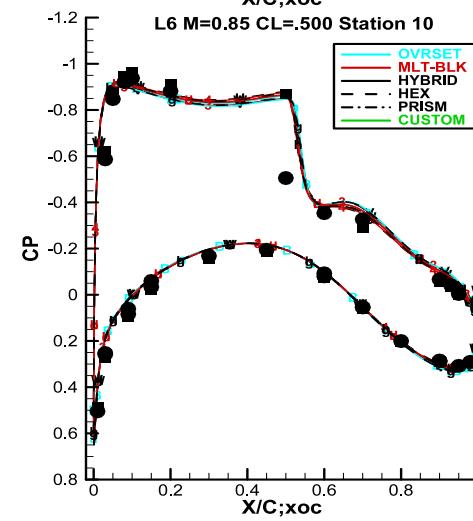
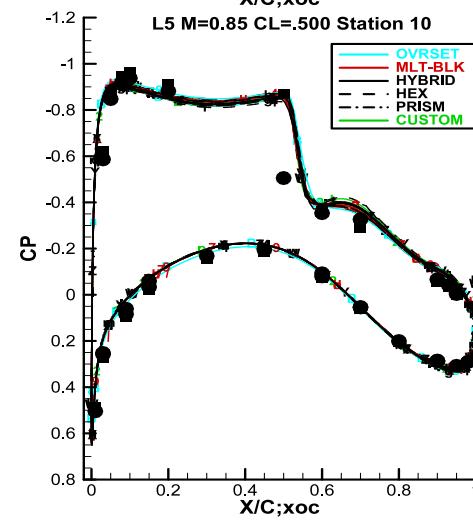
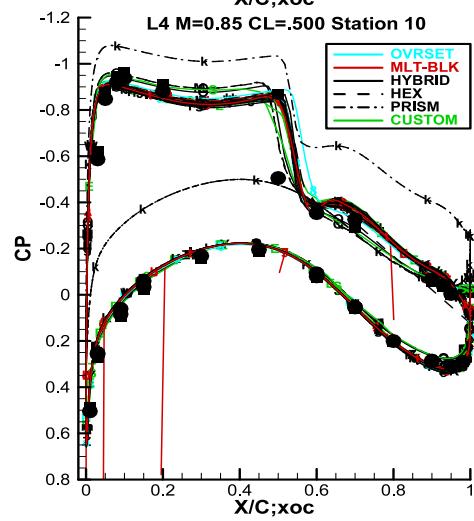
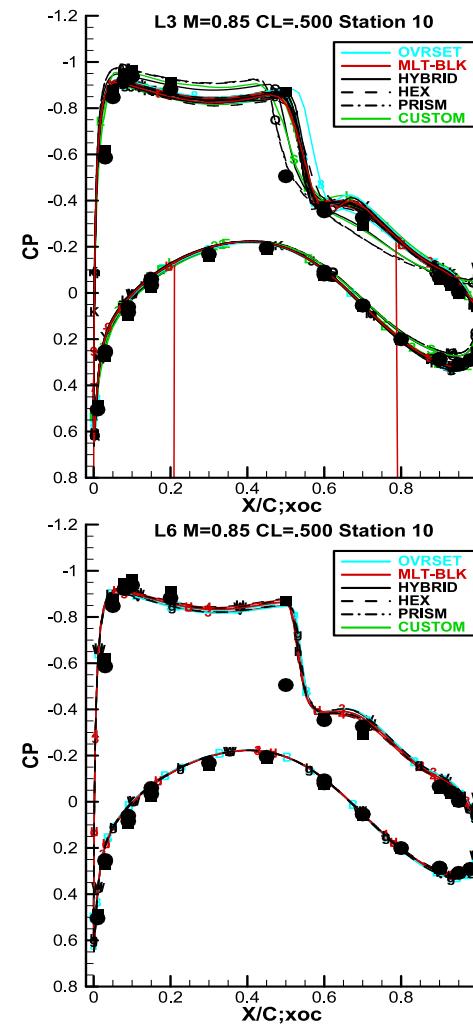
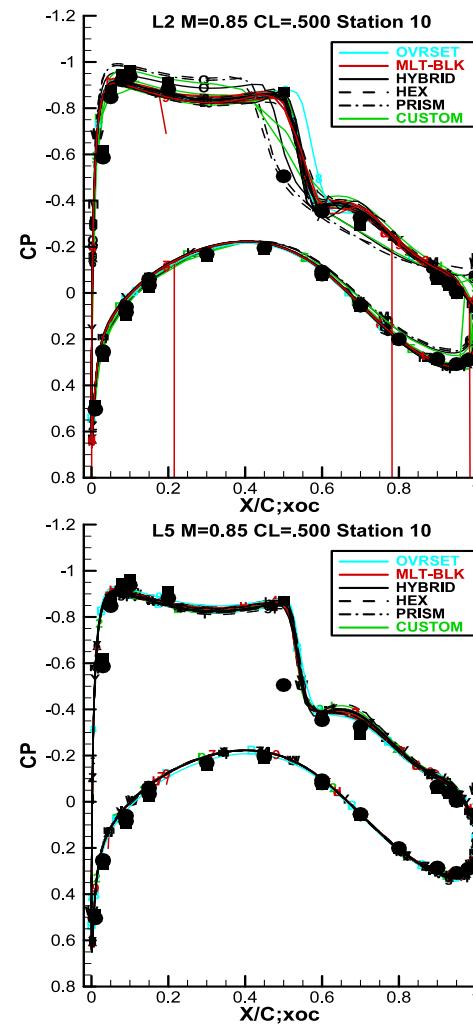
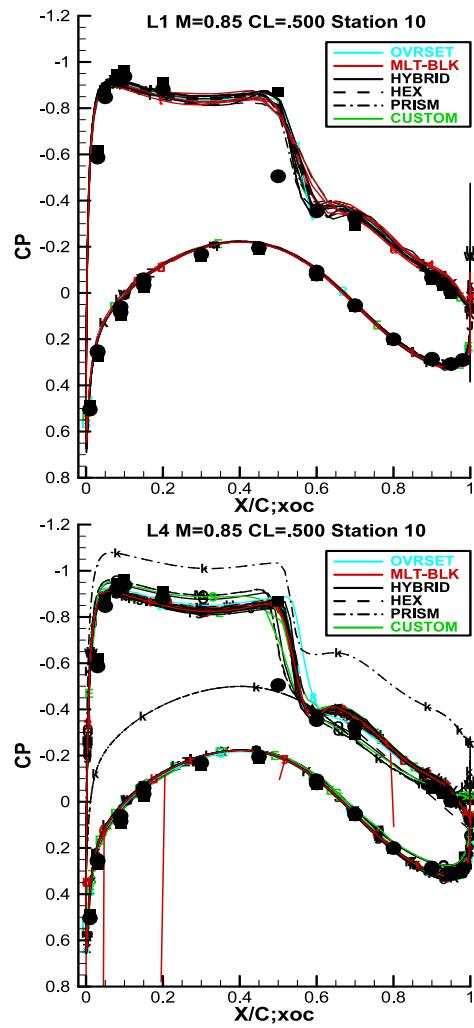
NTF Test 197 Run 44:
 ● $\alpha=2.68^\circ$, $CL=0.485$
 ■ $\alpha=2.91^\circ$, $CL=0.519$

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Case 1: Grid Refinement Study, $M=0.85$, $C_L=.50$
 Station 10, $\eta=.502$

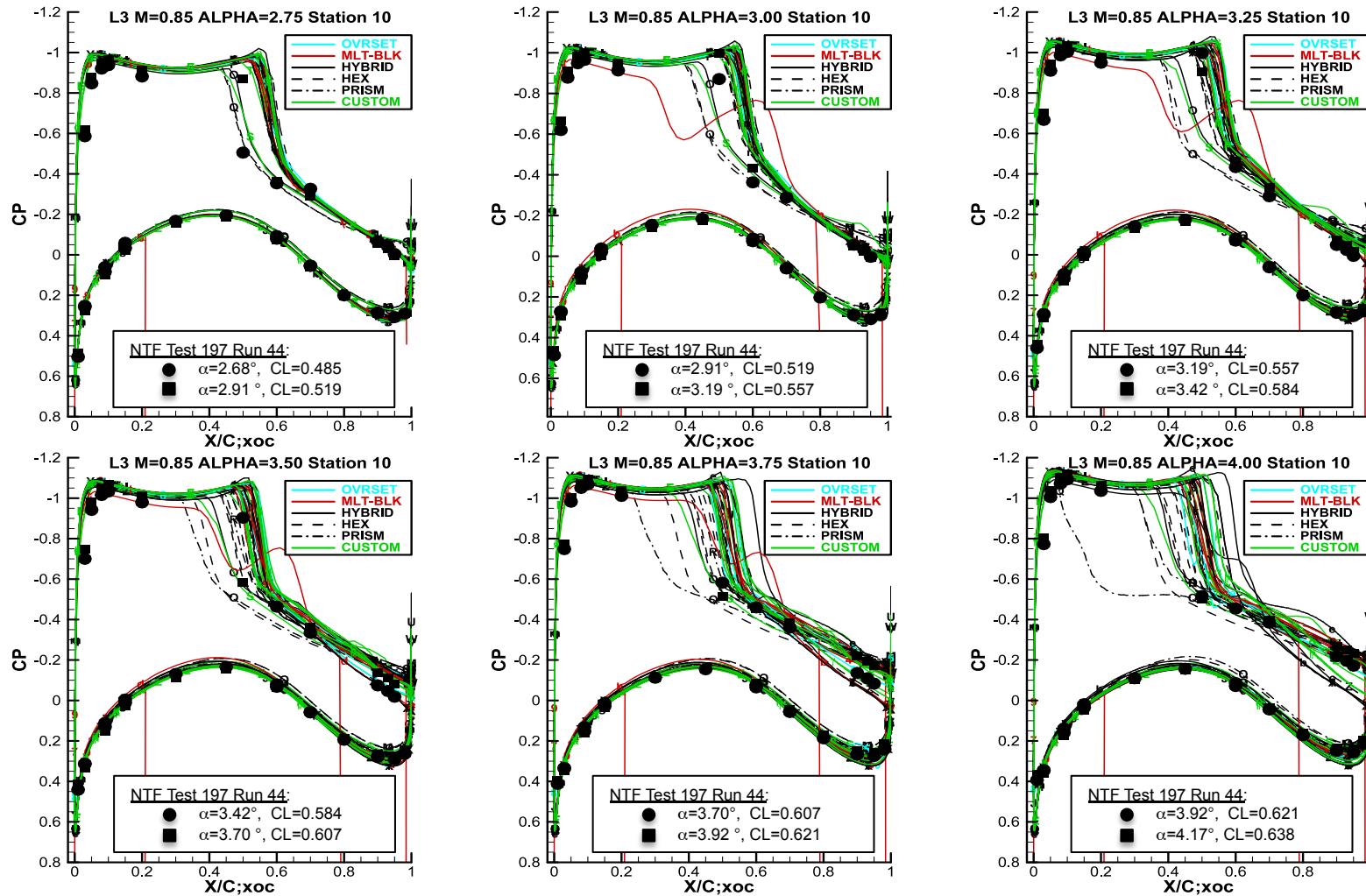
NTF Test 197 Run 44:
 ● $\alpha=2.68^\circ$, $CL=0.485$
 ■ $\alpha=2.91^\circ$, $CL=0.519$



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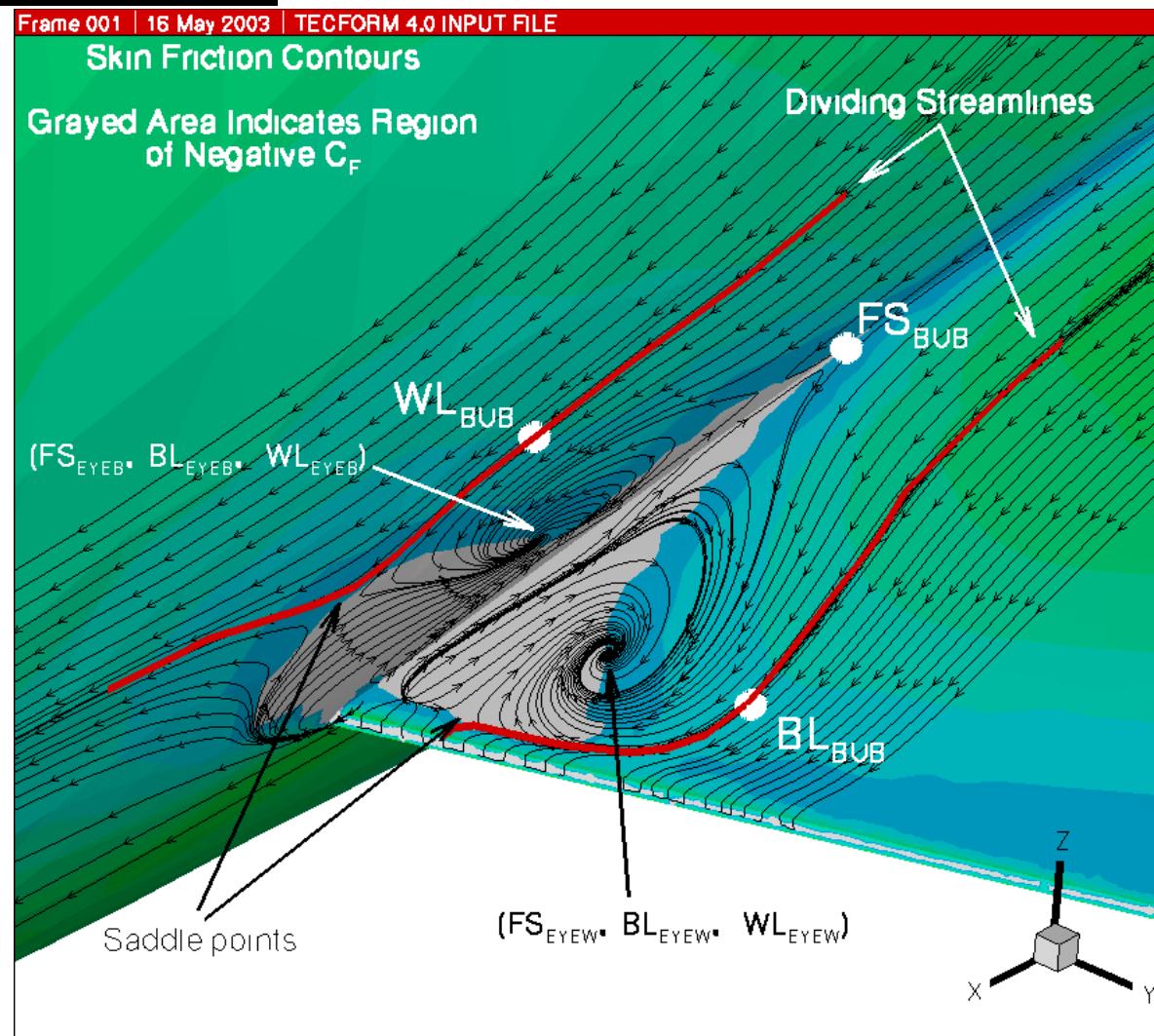
Case 2: Buffet Study, Level 3 Grids, M=0.85
 Station 10, $\eta=.502$



Conclusions from Pressure Data:

- Agreement with experiment deteriorates at outboard stations, likely due to aeroelastic effects
- Variations with grid level hard to discern due to reduced number of data sets
- Variation at high alphas due to separation effects on shock location
- No clear break-out with grid type (Turbulence model affects not examined yet)

Separation Bubble





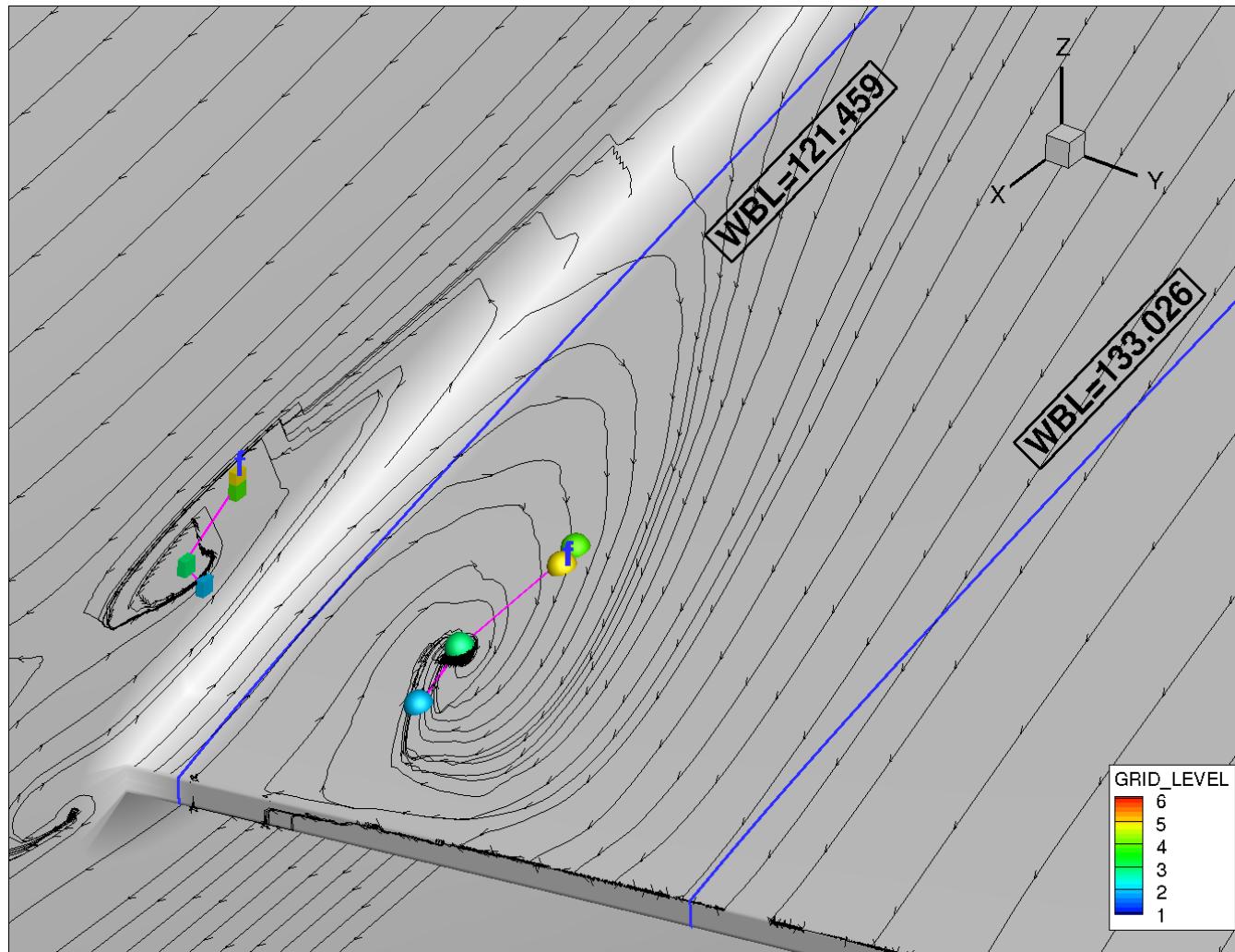
Side of Body Separation Bubble

1. Reported some level of SOB Separation:
I, J, K, L, X, Y, Z, 3, 4, 5, 6, 7, 9,
b, d, f, g, h, k, t, α , β , δ , γ , λ , π
2. Reported no SOB Separation (SOB File Provided):
U, V, W, 2, e, m, n, q, r
3. No Report (No SOB File Provided):
A, B, C, D, E, F, G, H, M, N, O, P, Q, R, S, T, 8, a

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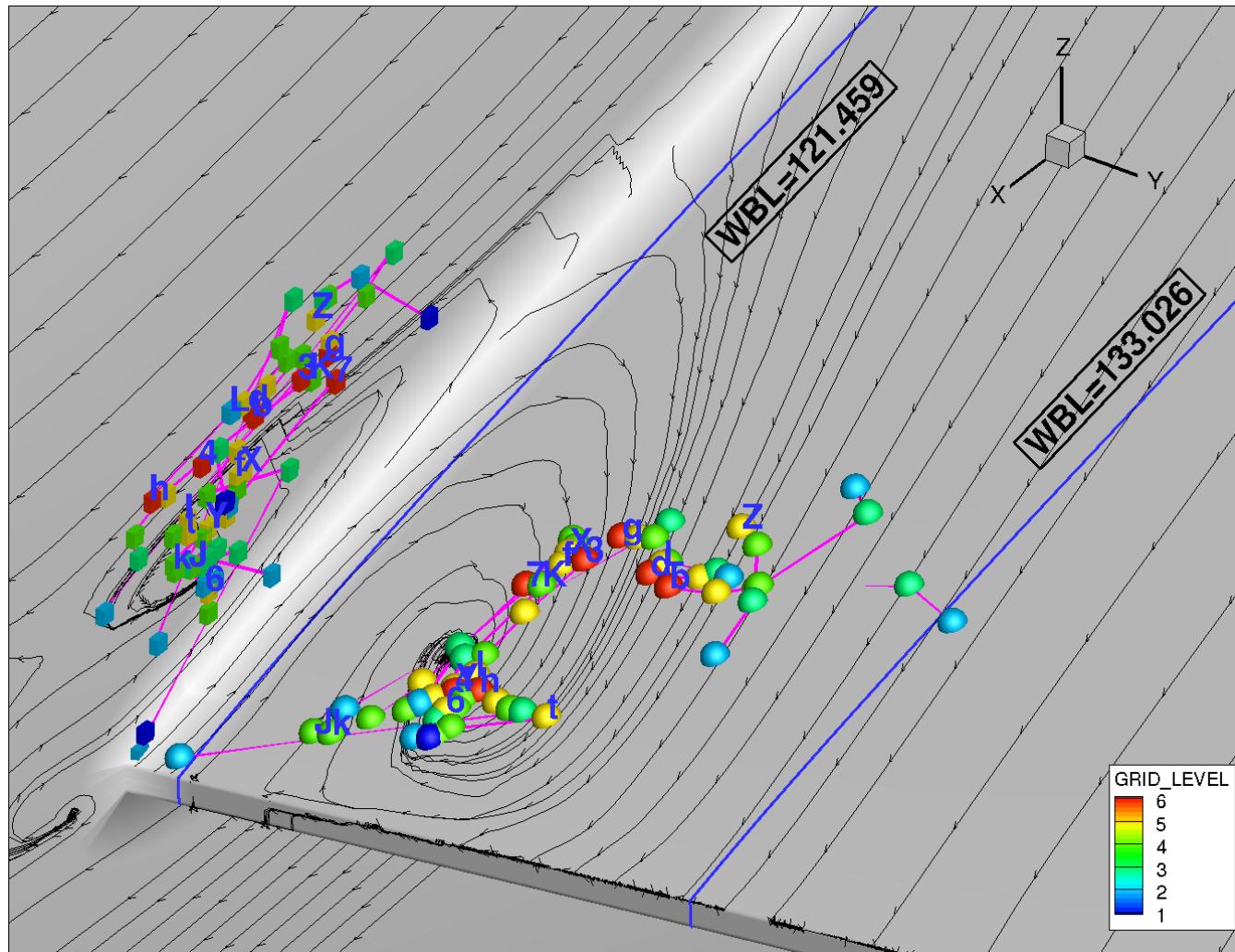
Example Grid Refinement: with Dataset “f” only



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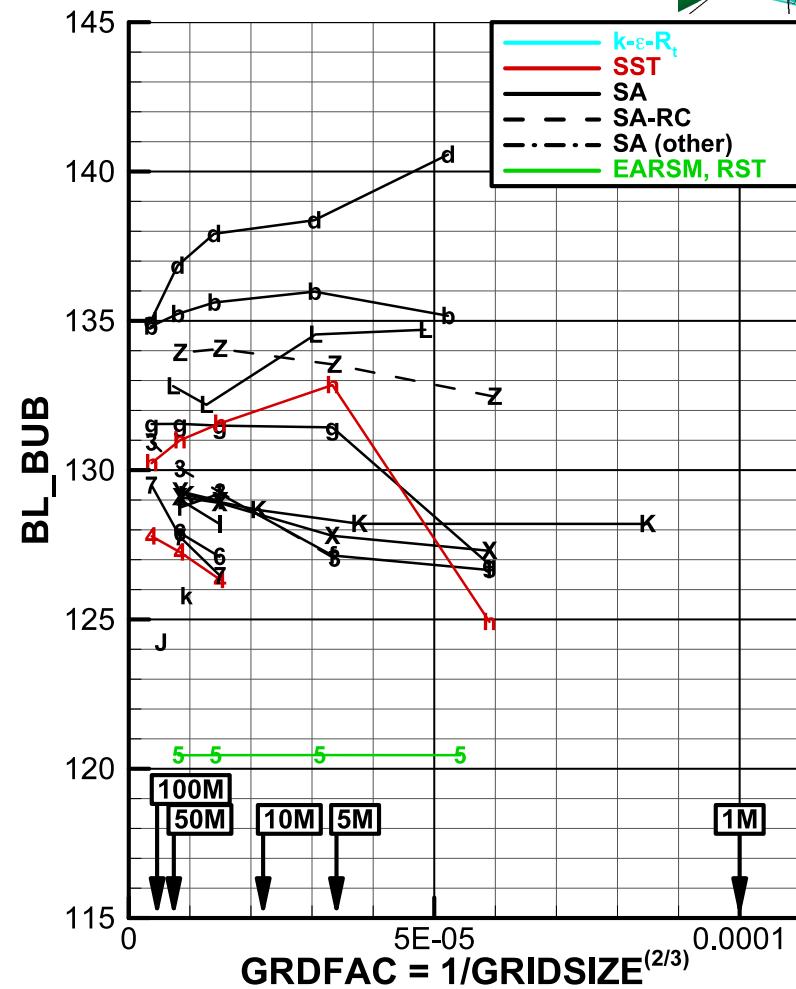
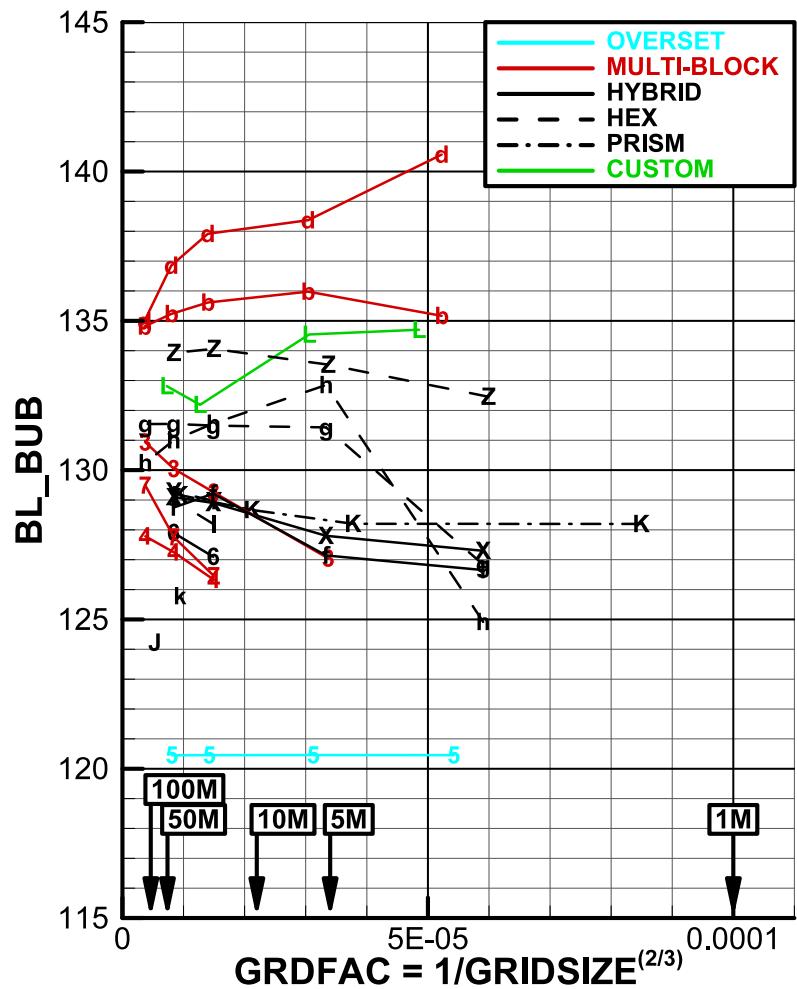
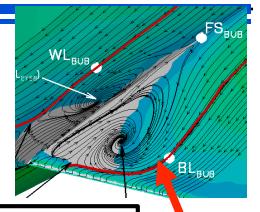
Grid Refinement: All Data



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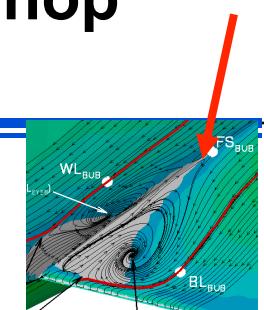
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Bubble Width (Wing): Case 1 By Grid Type and Turbulence Model

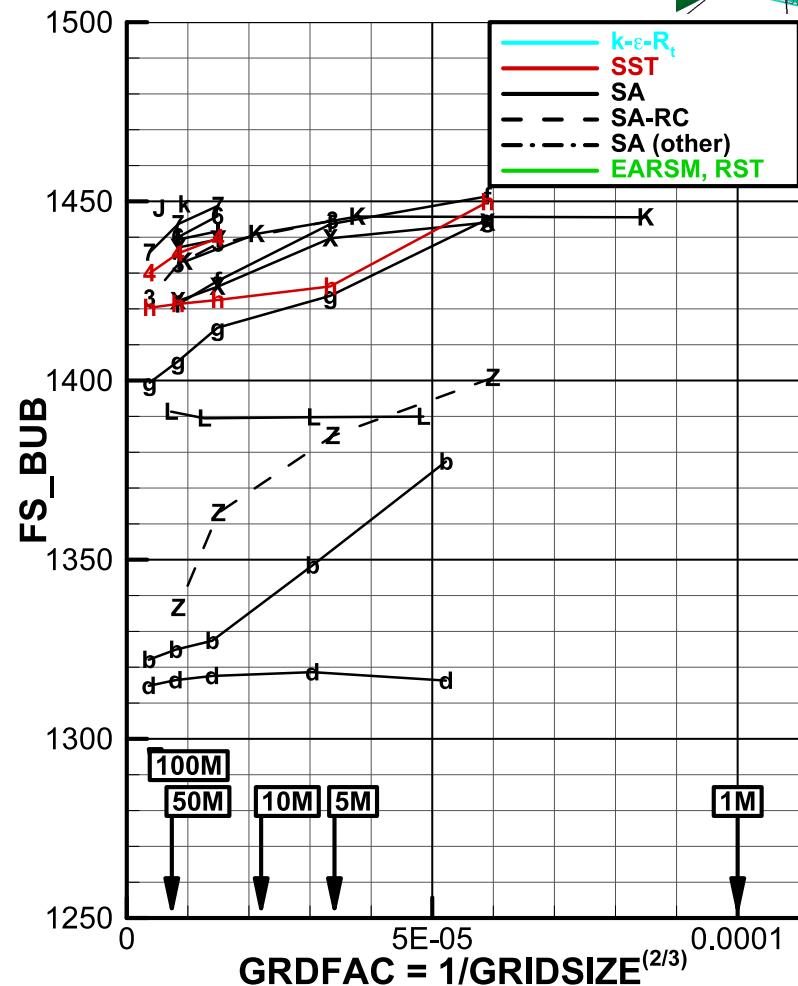
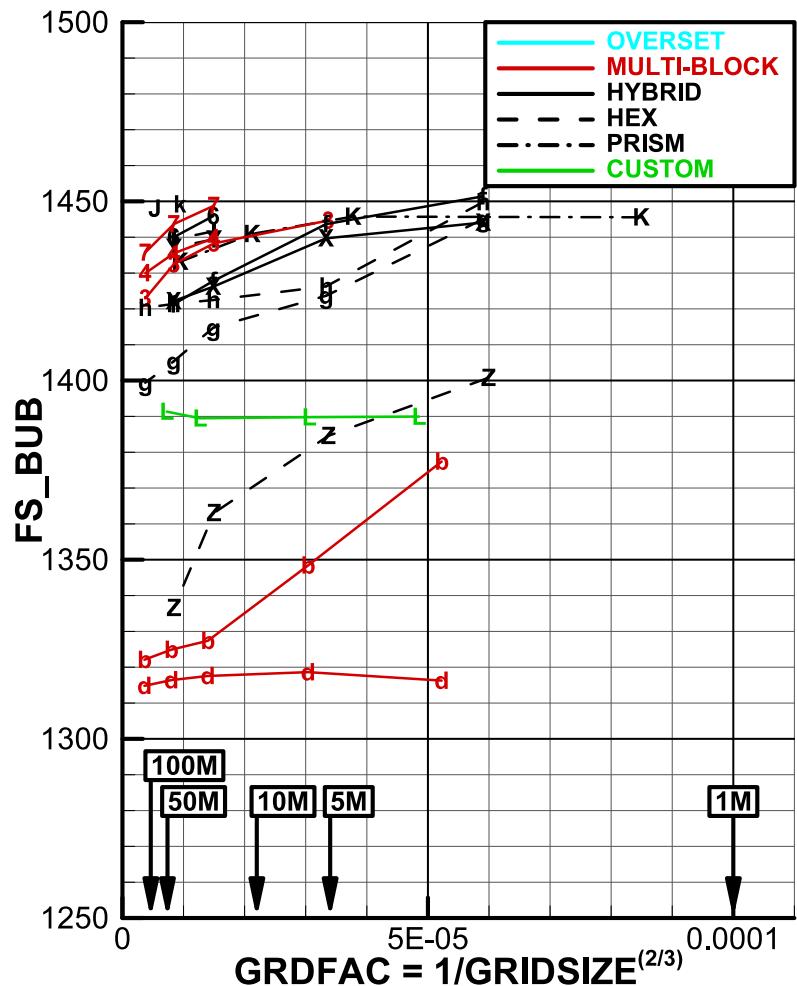


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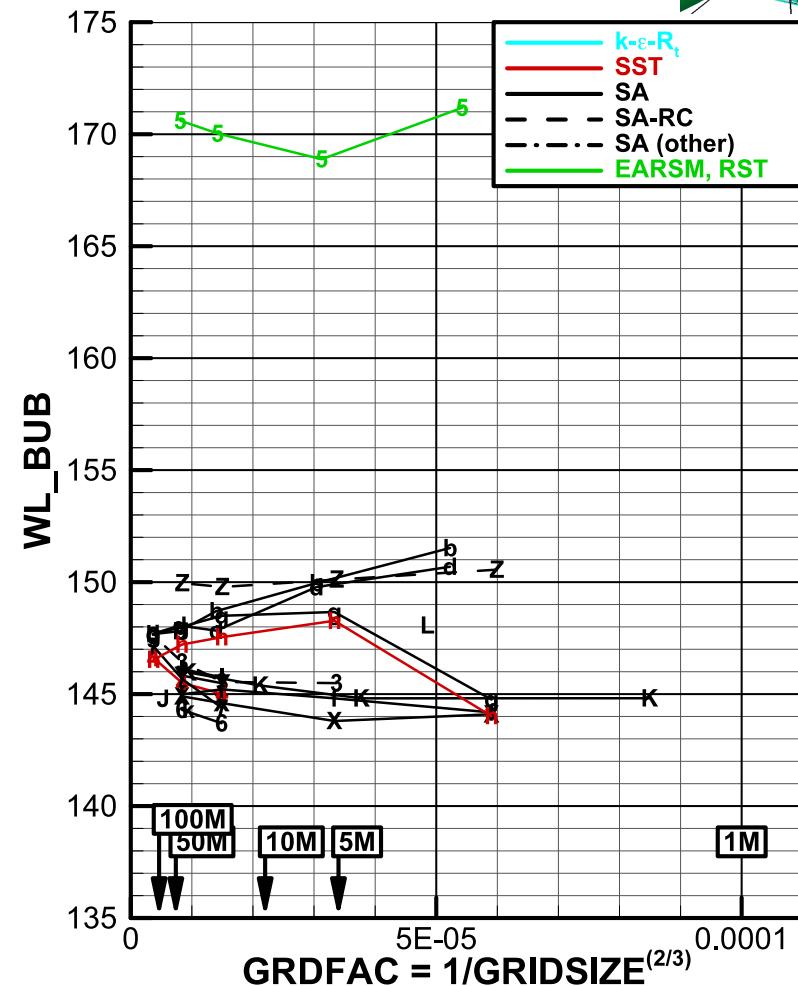
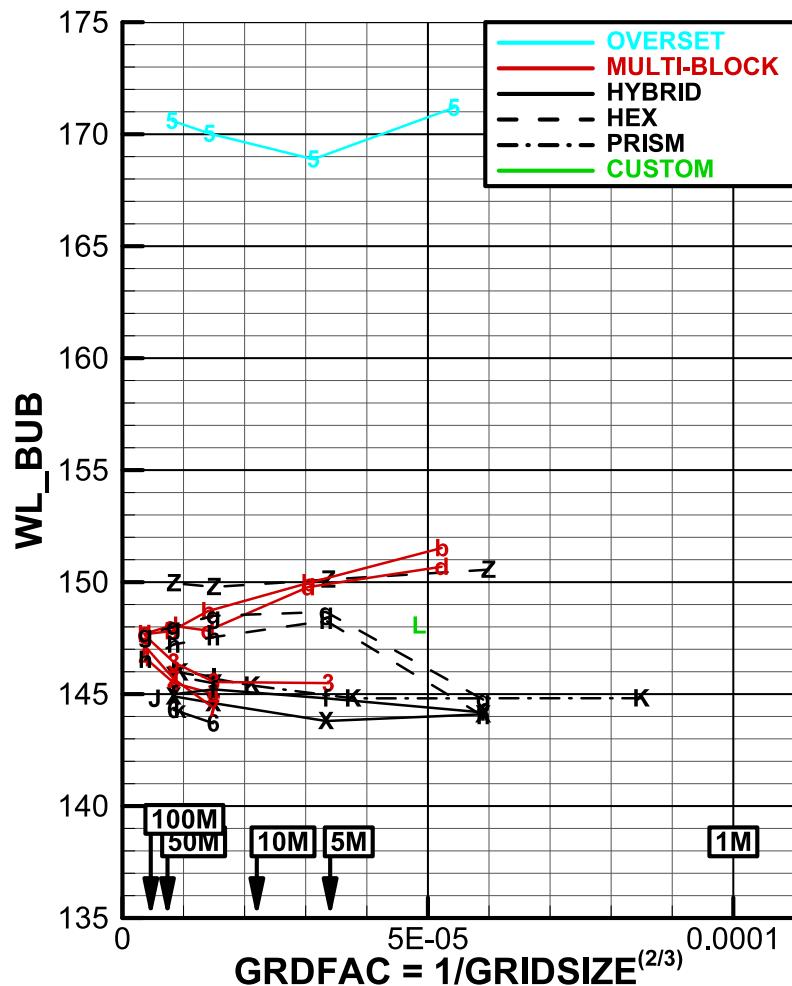
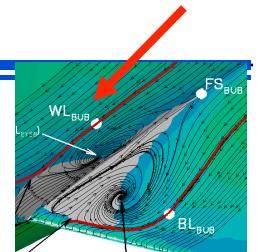
Bubble Leading Edge: Case 1 By Grid Type and Turbulence Model



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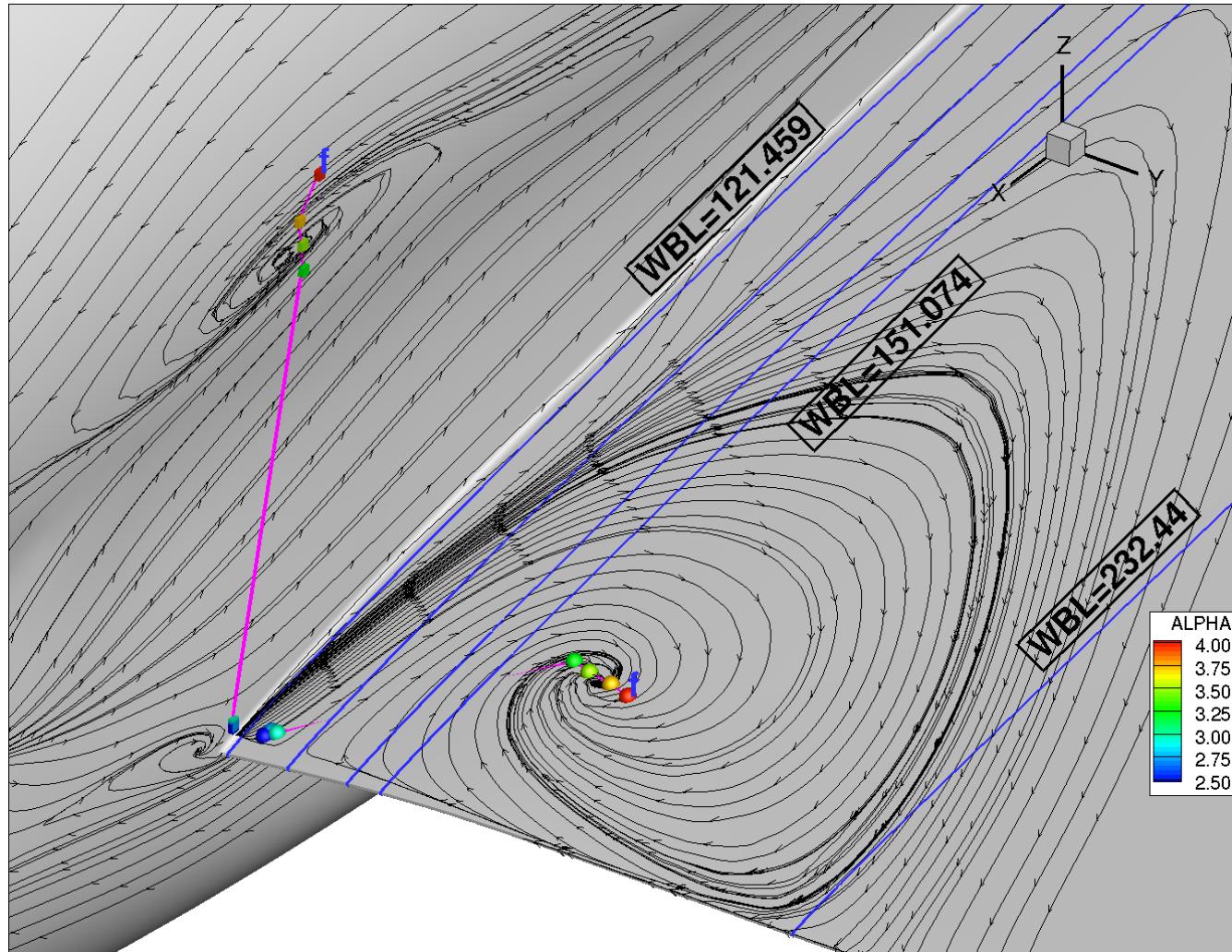
Bubble Height (Fuselage): Case 1 By Grid Type and Turbulence Model



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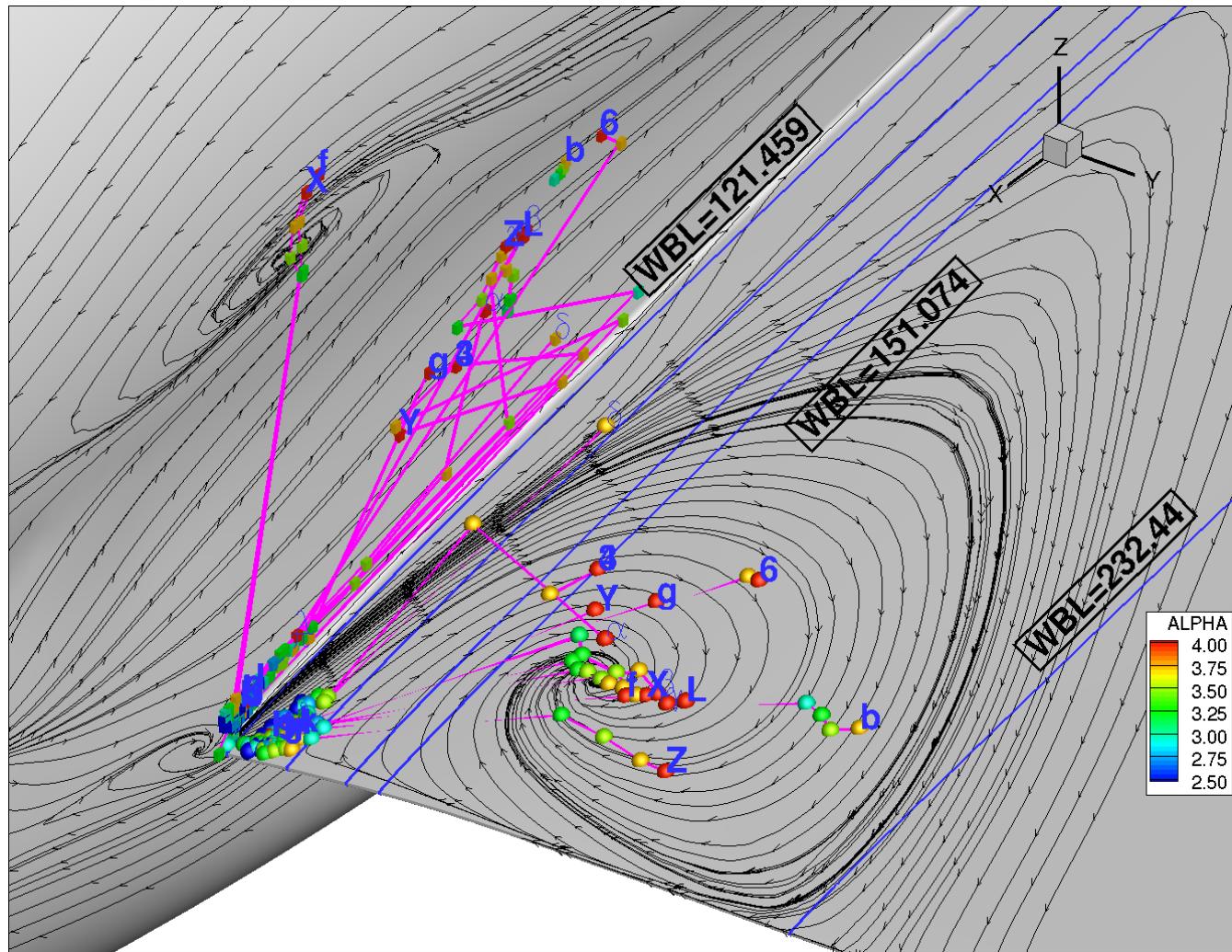
Example Alpha Sweep: with Dataset “f” only



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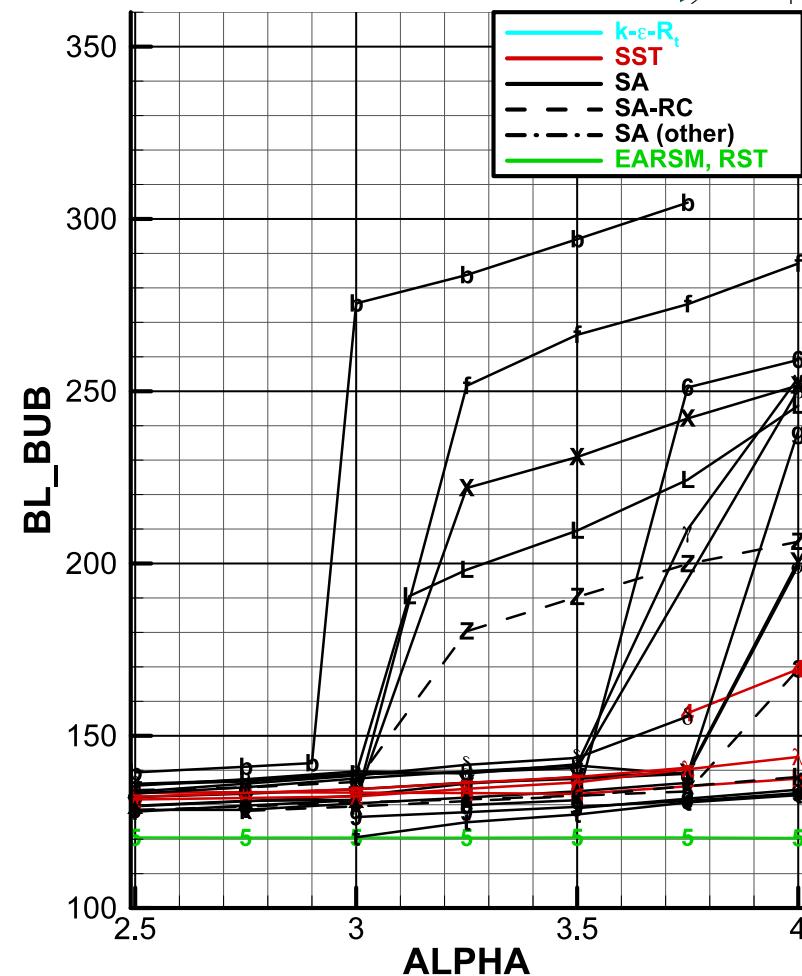
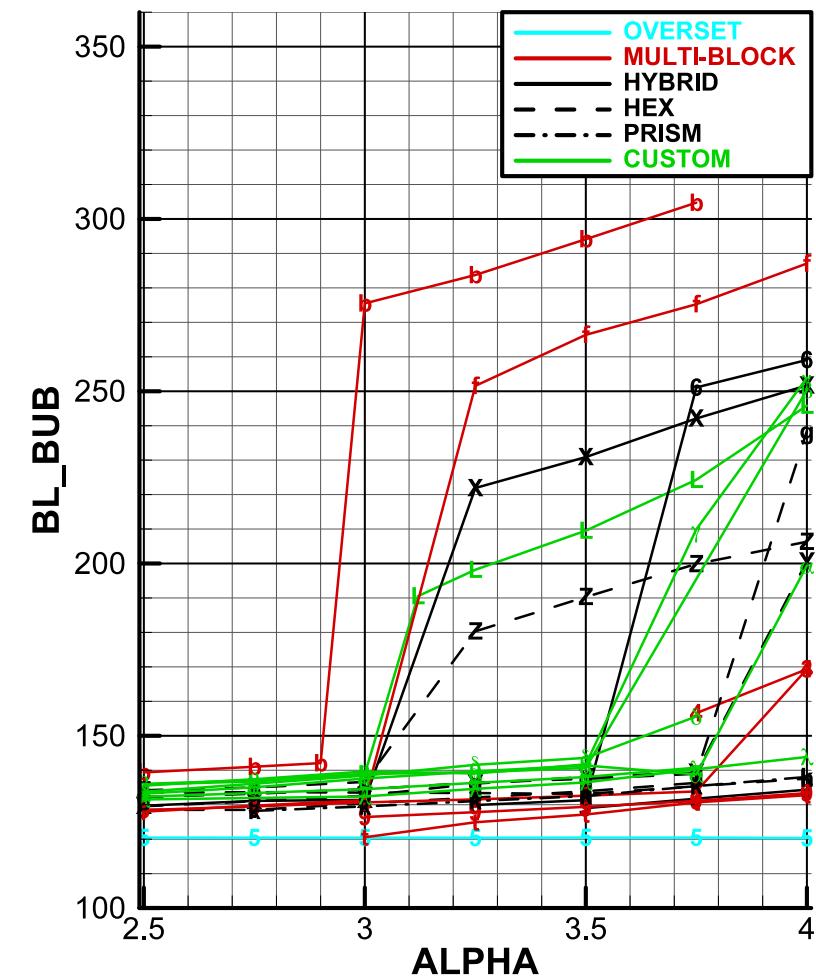
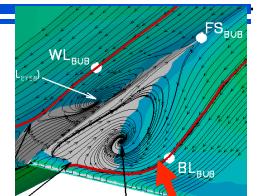
Alpha Sweep: All Data



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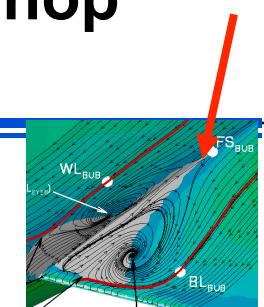
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Bubble Width (Wing): Case 2 By Grid Type and Turbulence Model

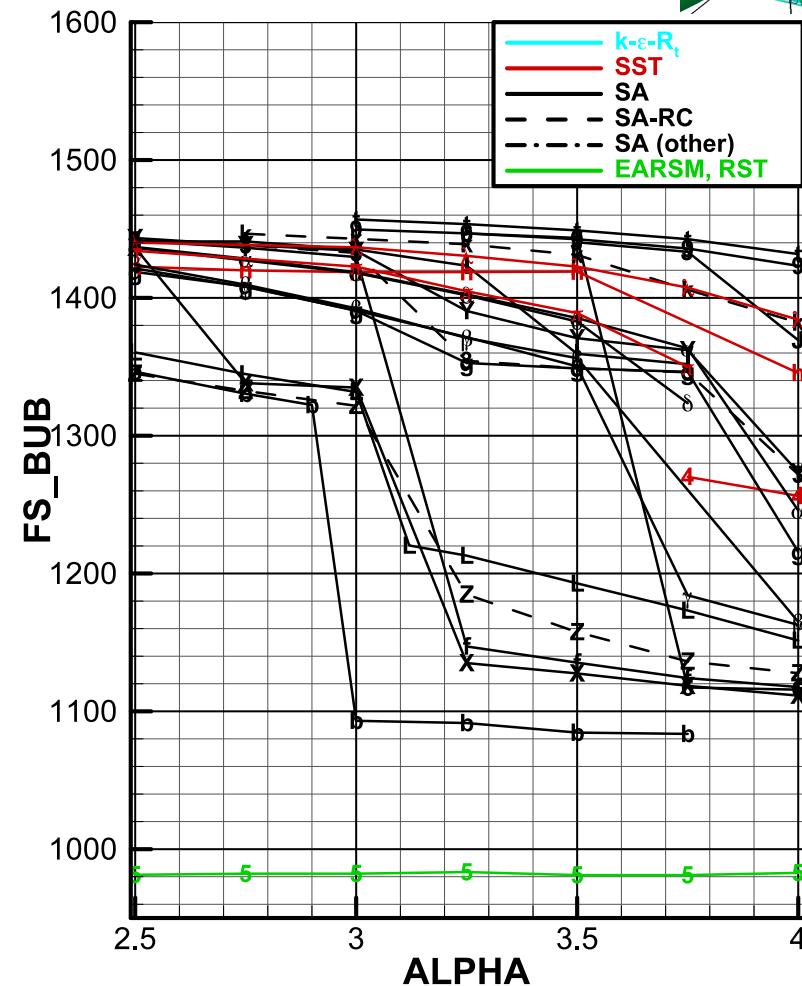
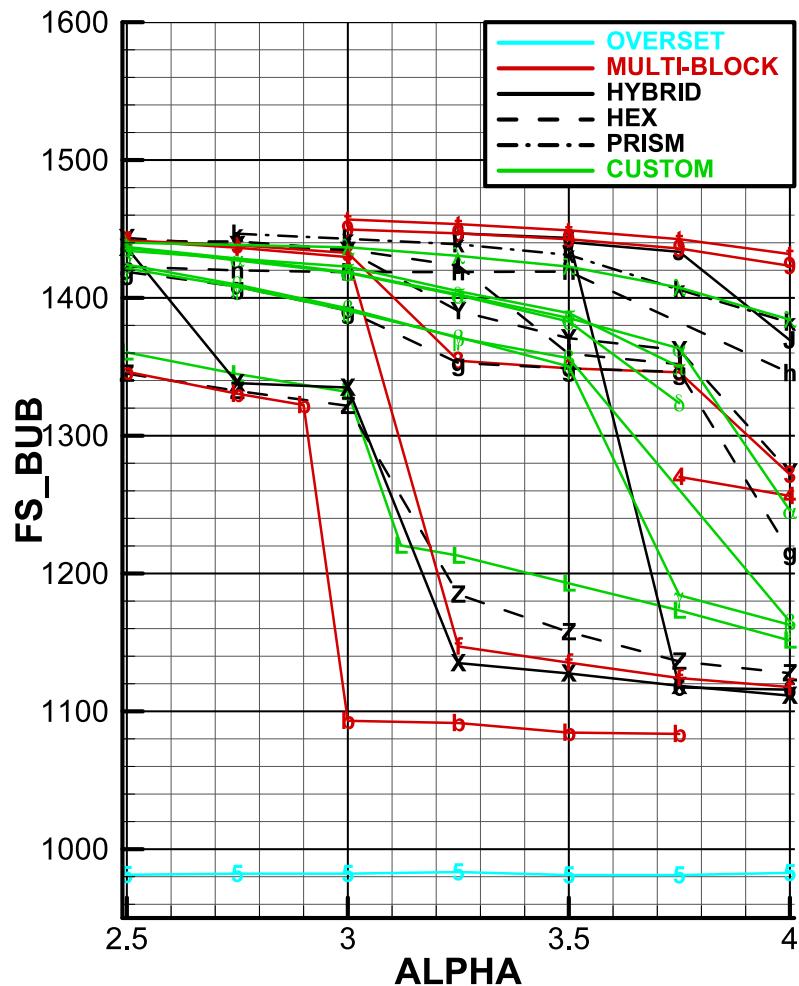


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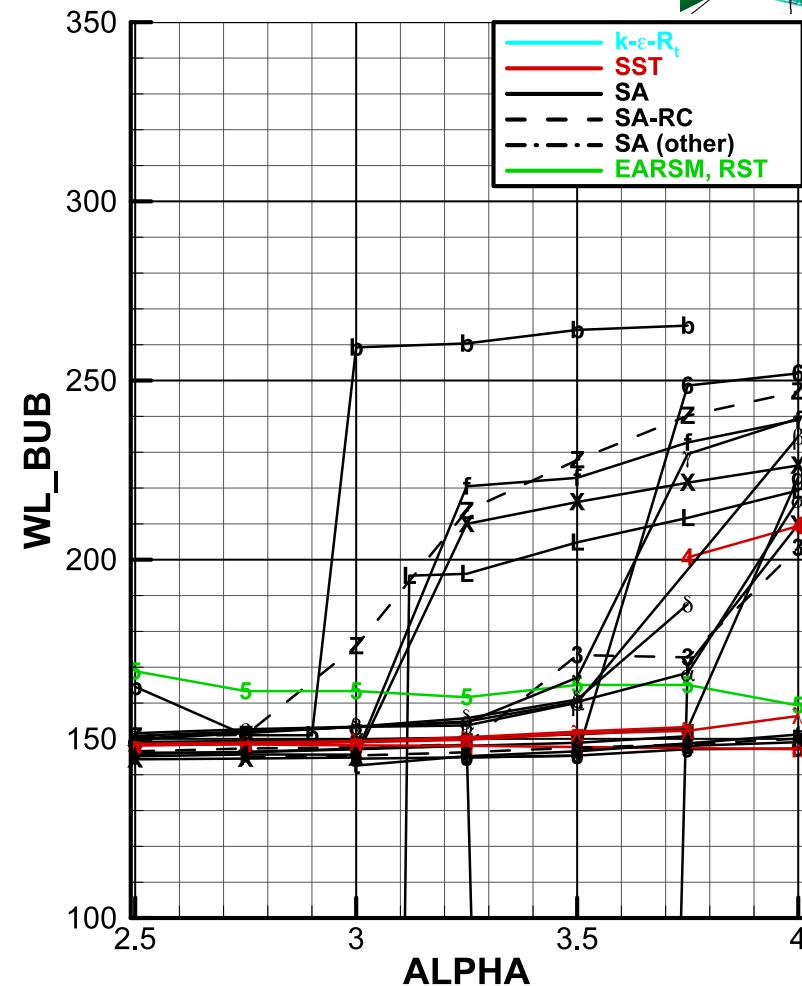
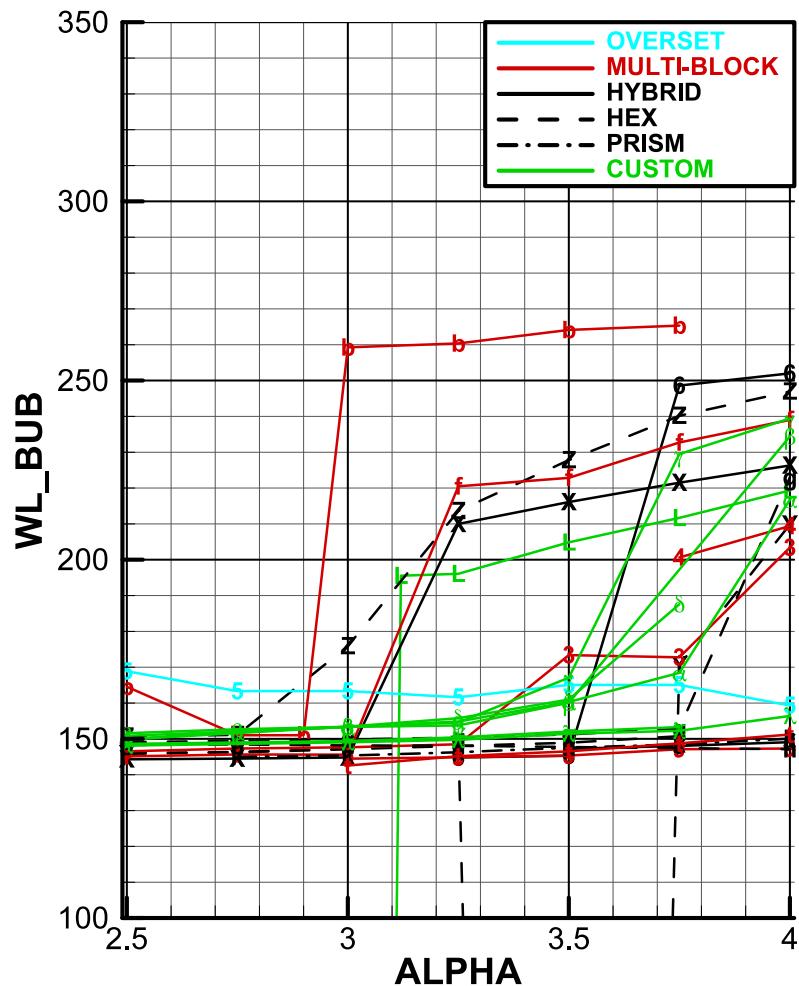
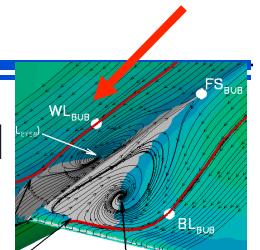
Bubble Leading Edge: Case 2 By Grid Type and Turbulence Model



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Bubble Height (Fuselage): Case 2 By Grid Type and Turbulence Model



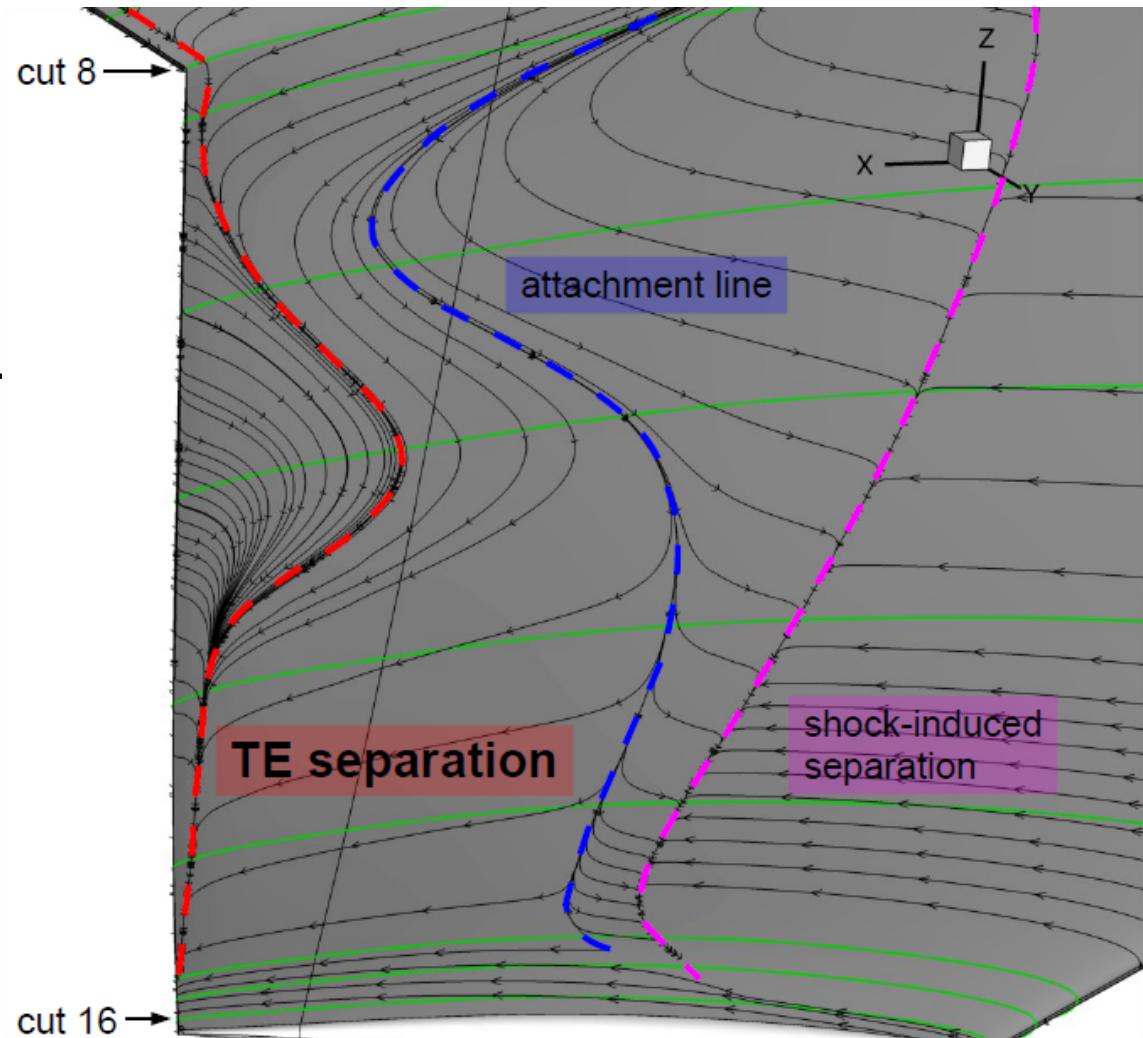


Conclusions from Separation Bubble:

- Variation with grid level fairly consistent (note that coarse level grids do not have proper resolution)
- Some data sets show dramatic increase in bubble size at higher alpha
 - Mostly for Spalart-Allmaras results

Trailing Edge Separation:

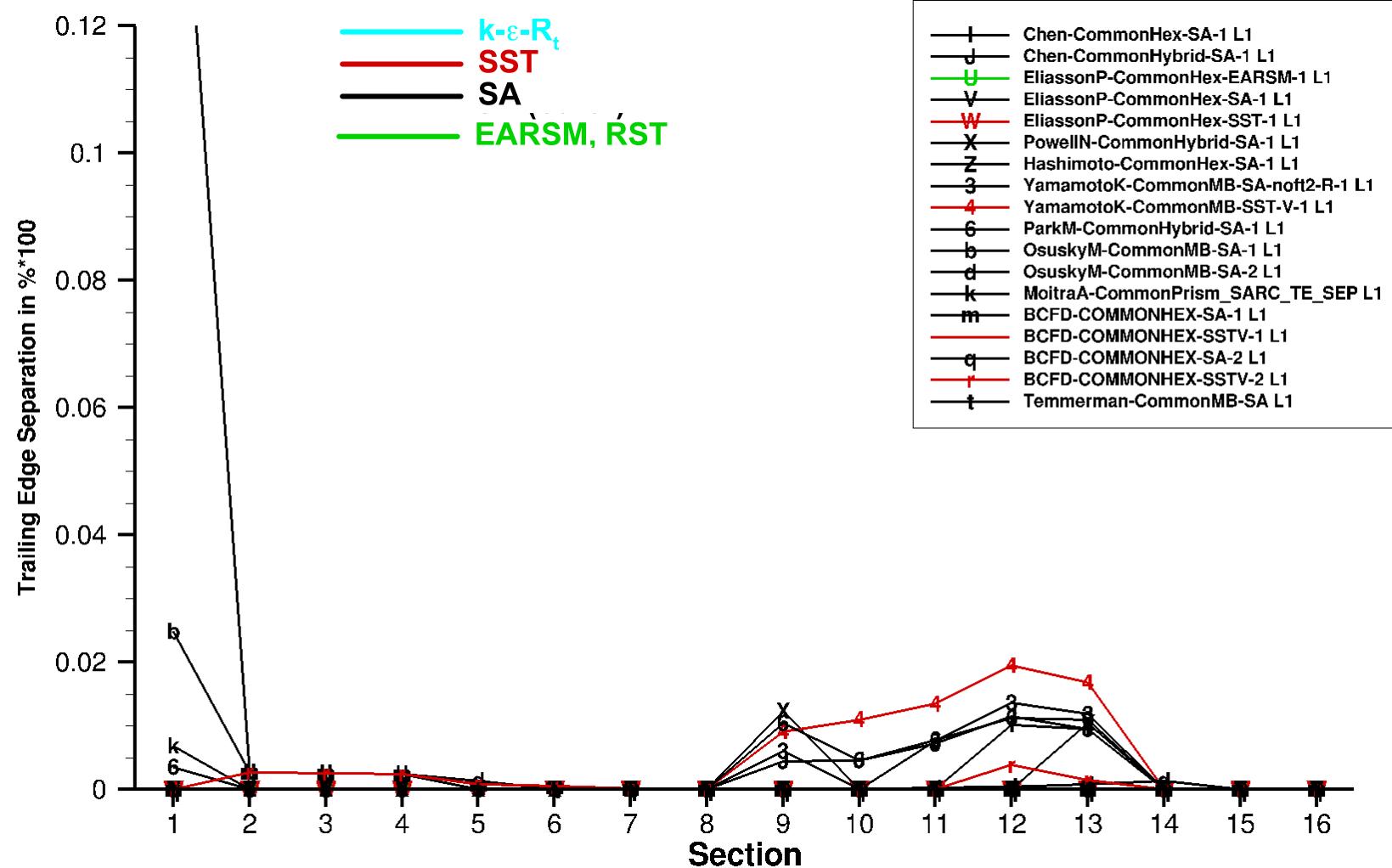
- DPW-4: C_f normal to TE < 0 as criteria
- For higher α more difficult to define & detect



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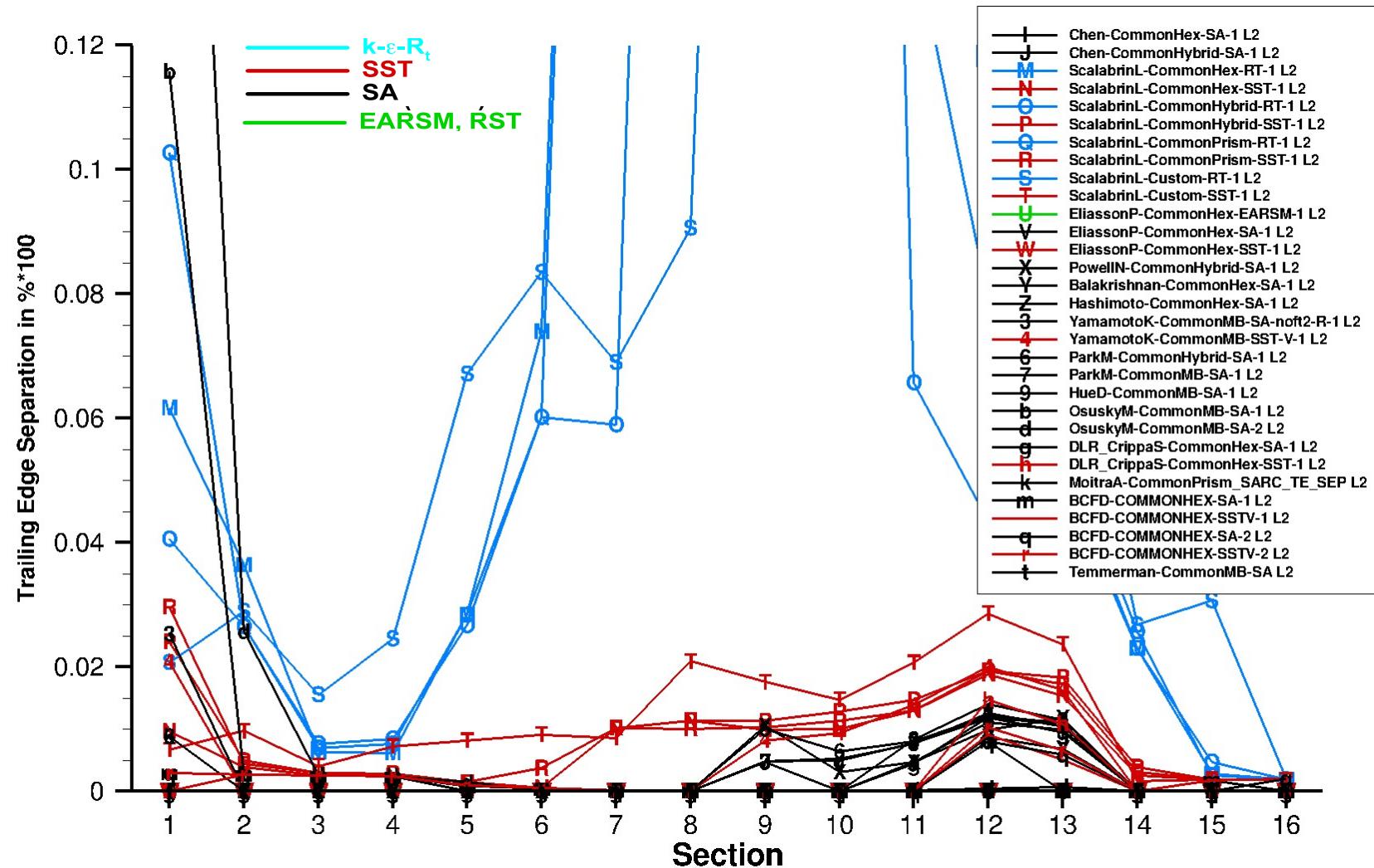
Case 1: Trailing Edge Separation, Level 1



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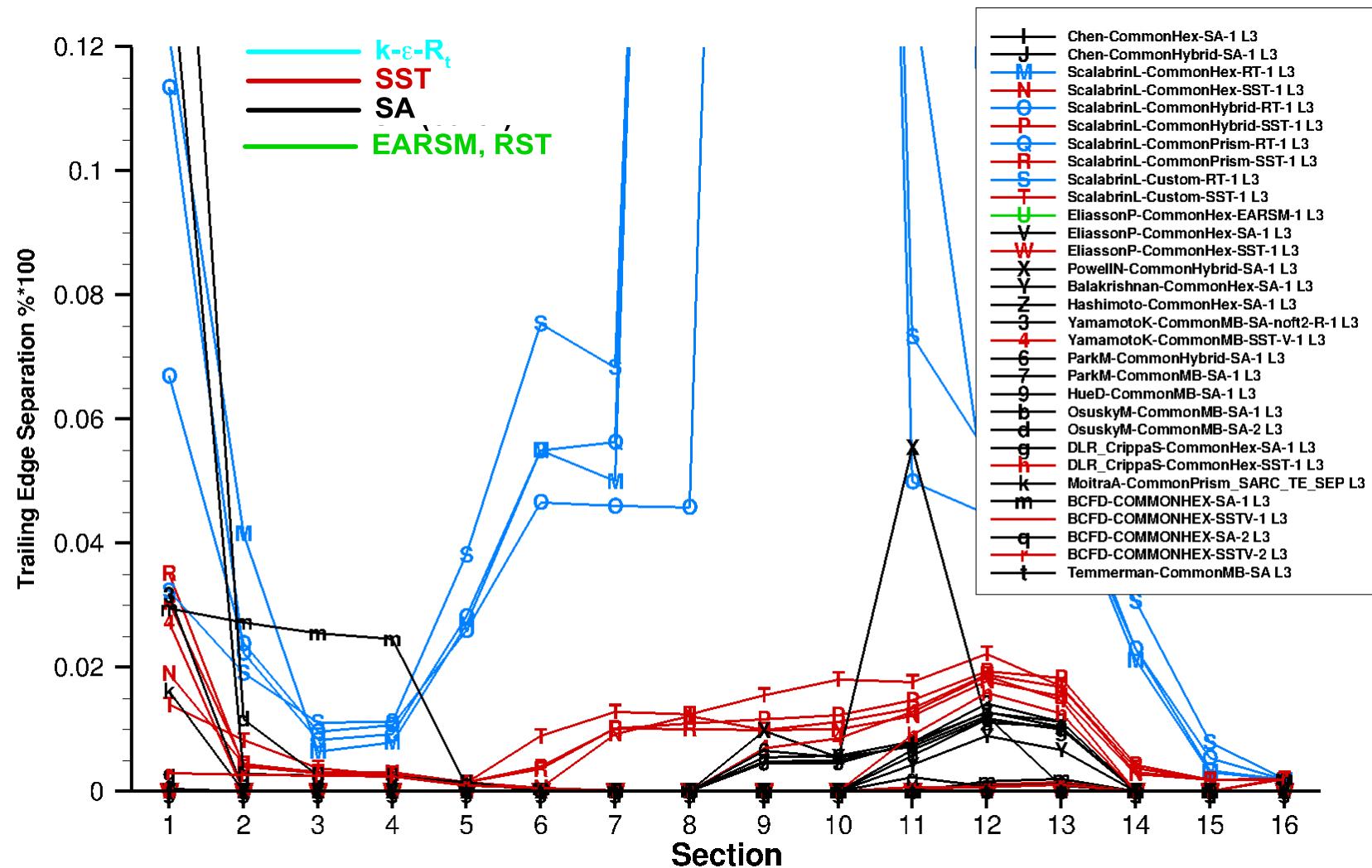
Case 1: Trailing Edge Separation, Level 2



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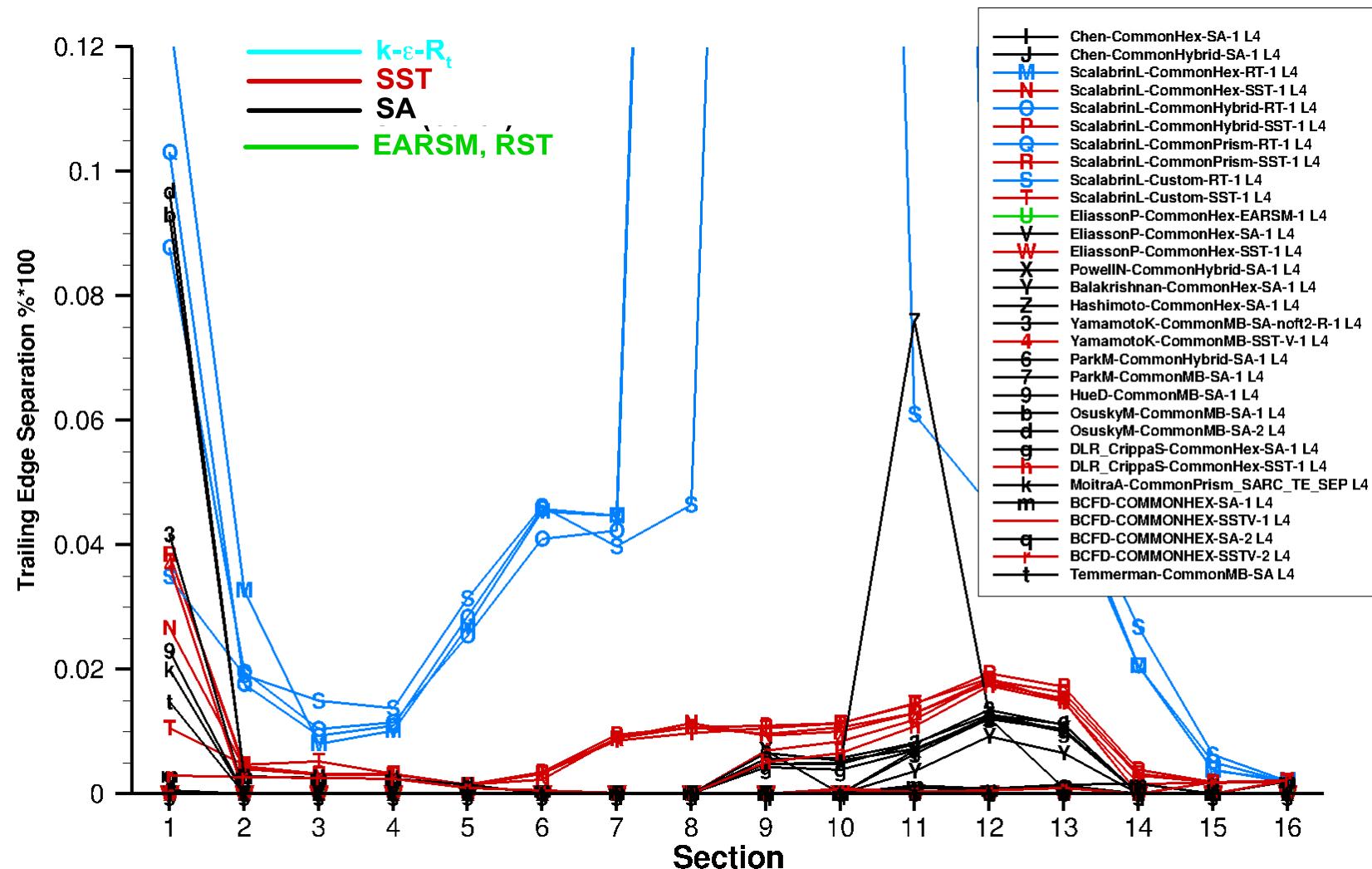
Case 1: Trailing Edge Separation, Level 3



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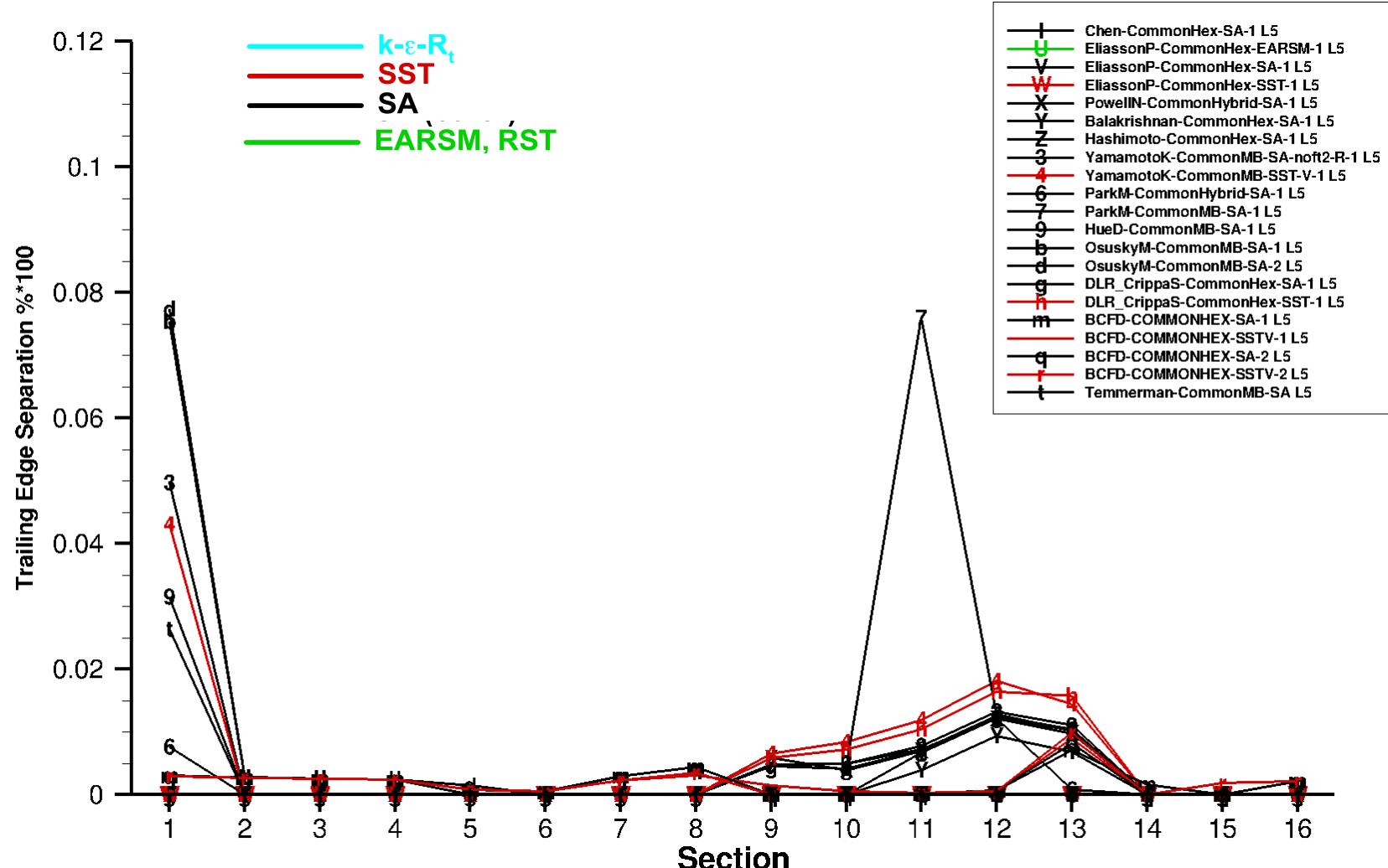
Case 1: Trailing Edge Separation, Level 4



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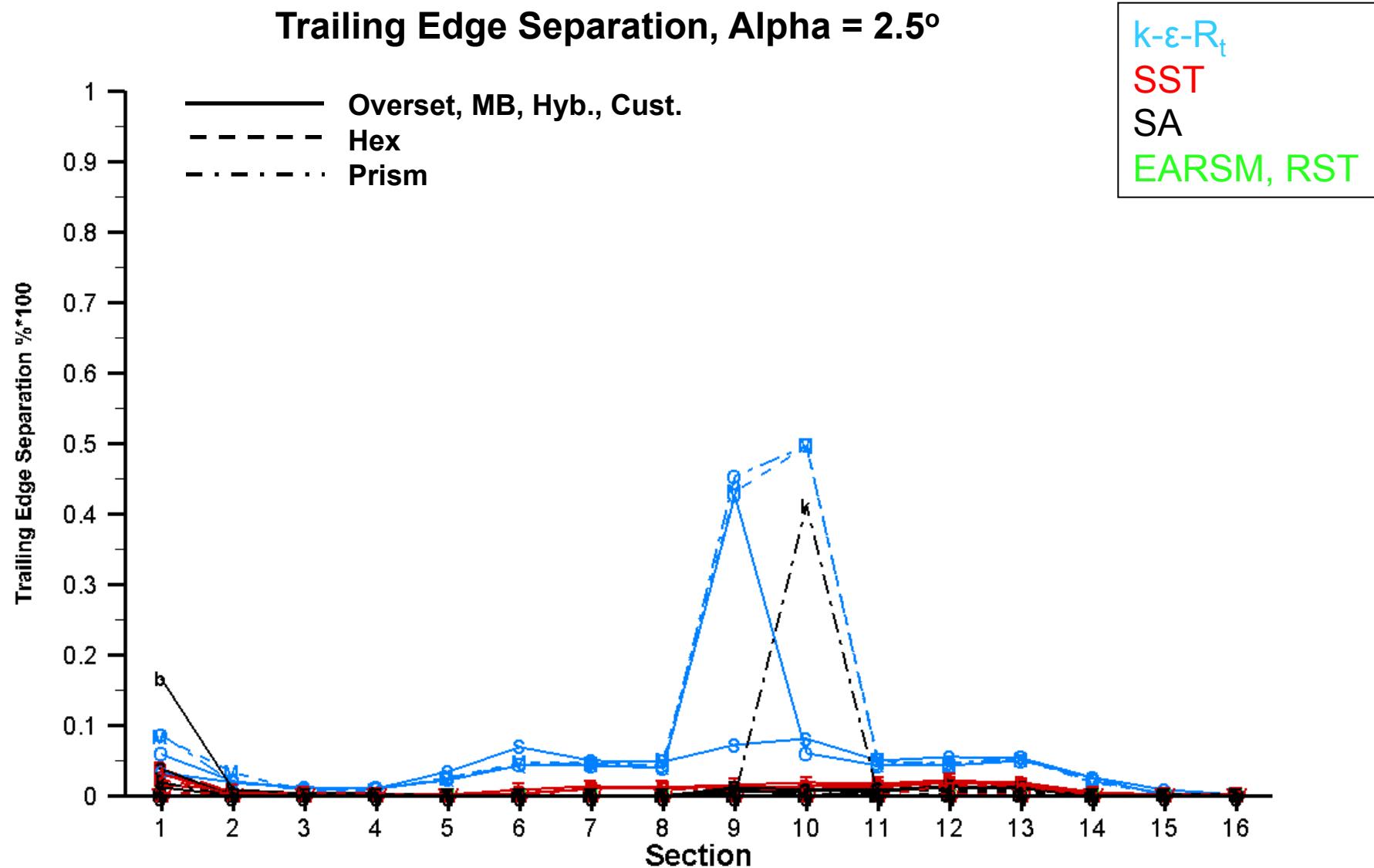
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Case 1: Trailing Edge Separation, Level 5



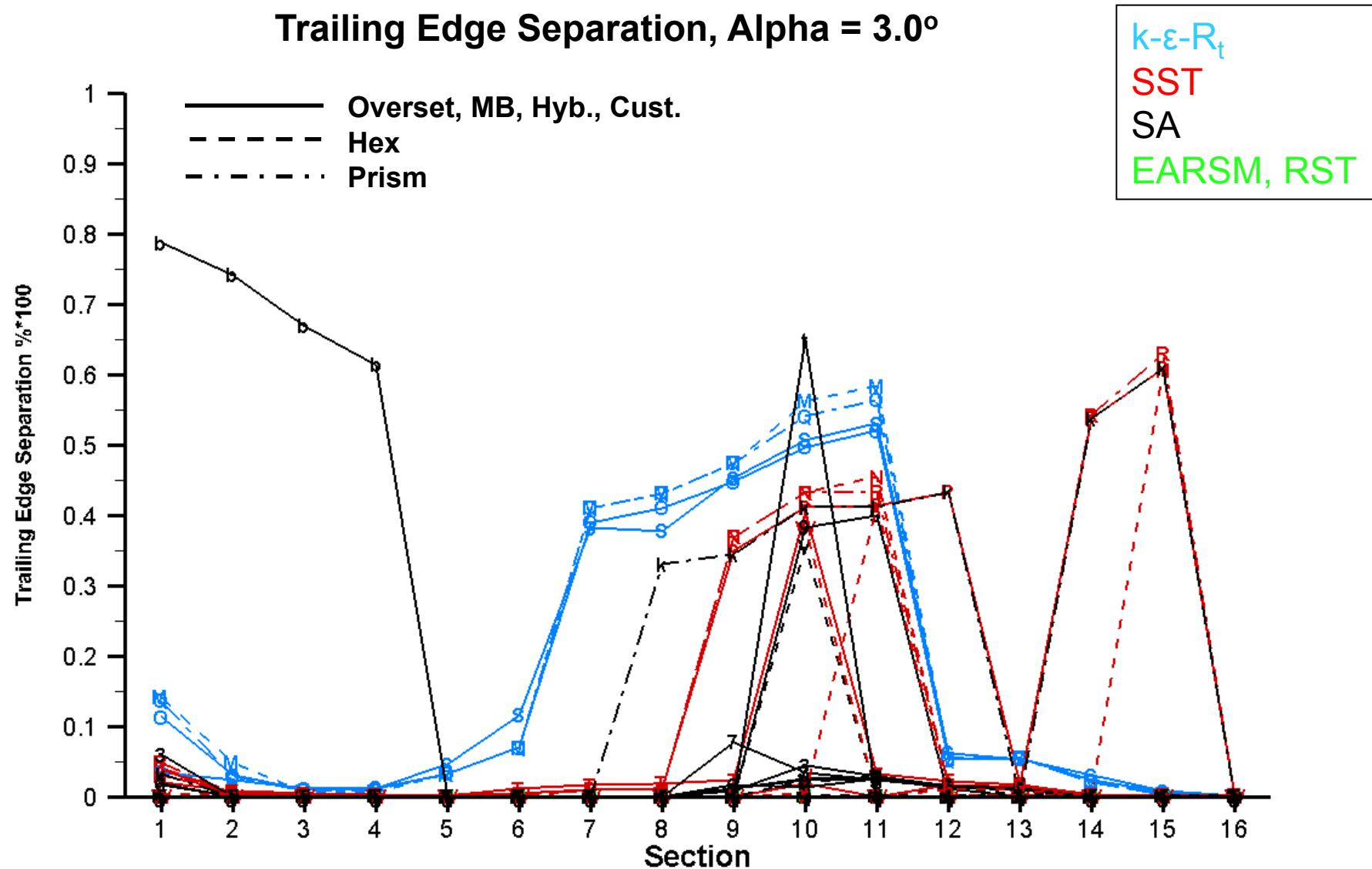
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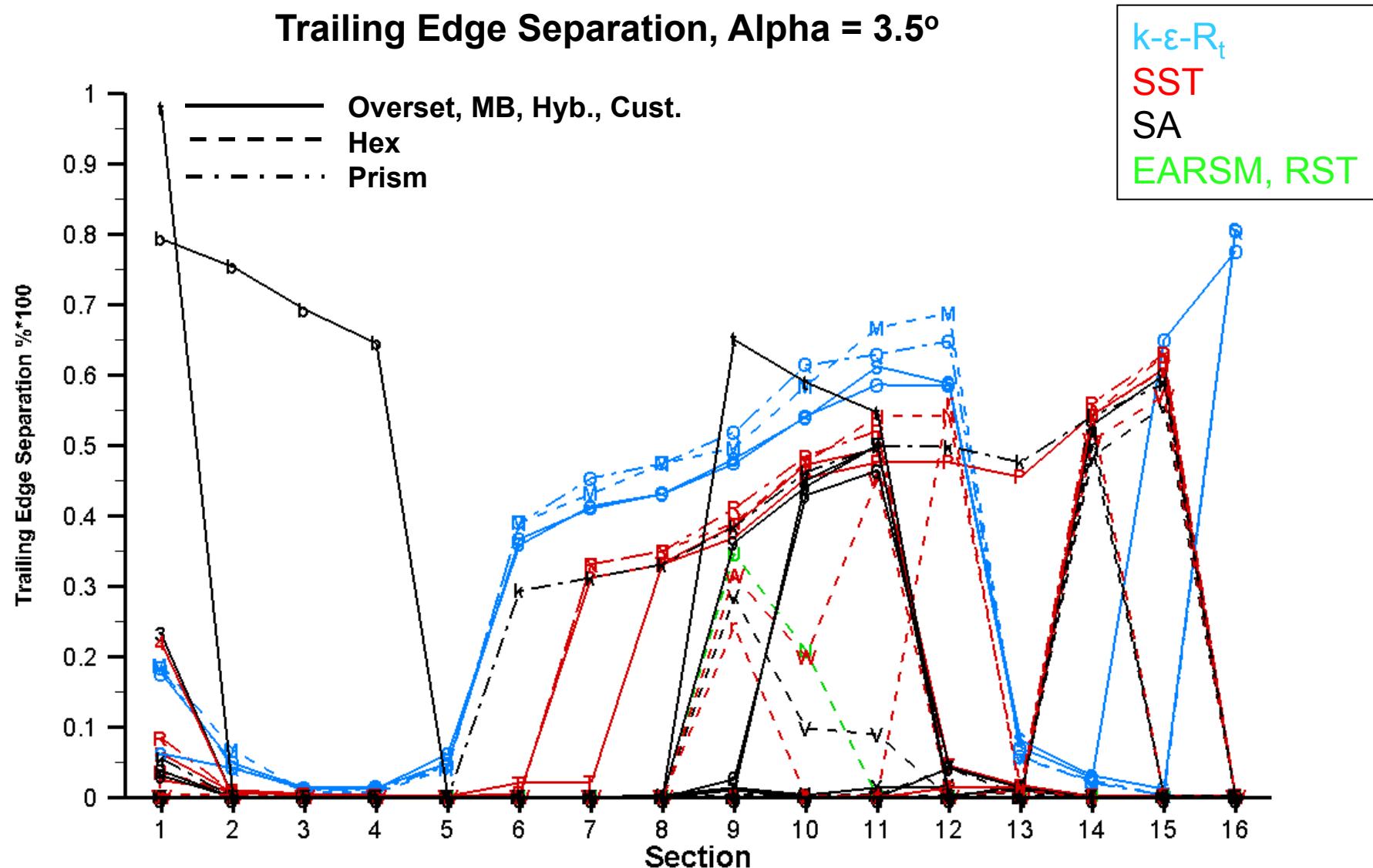
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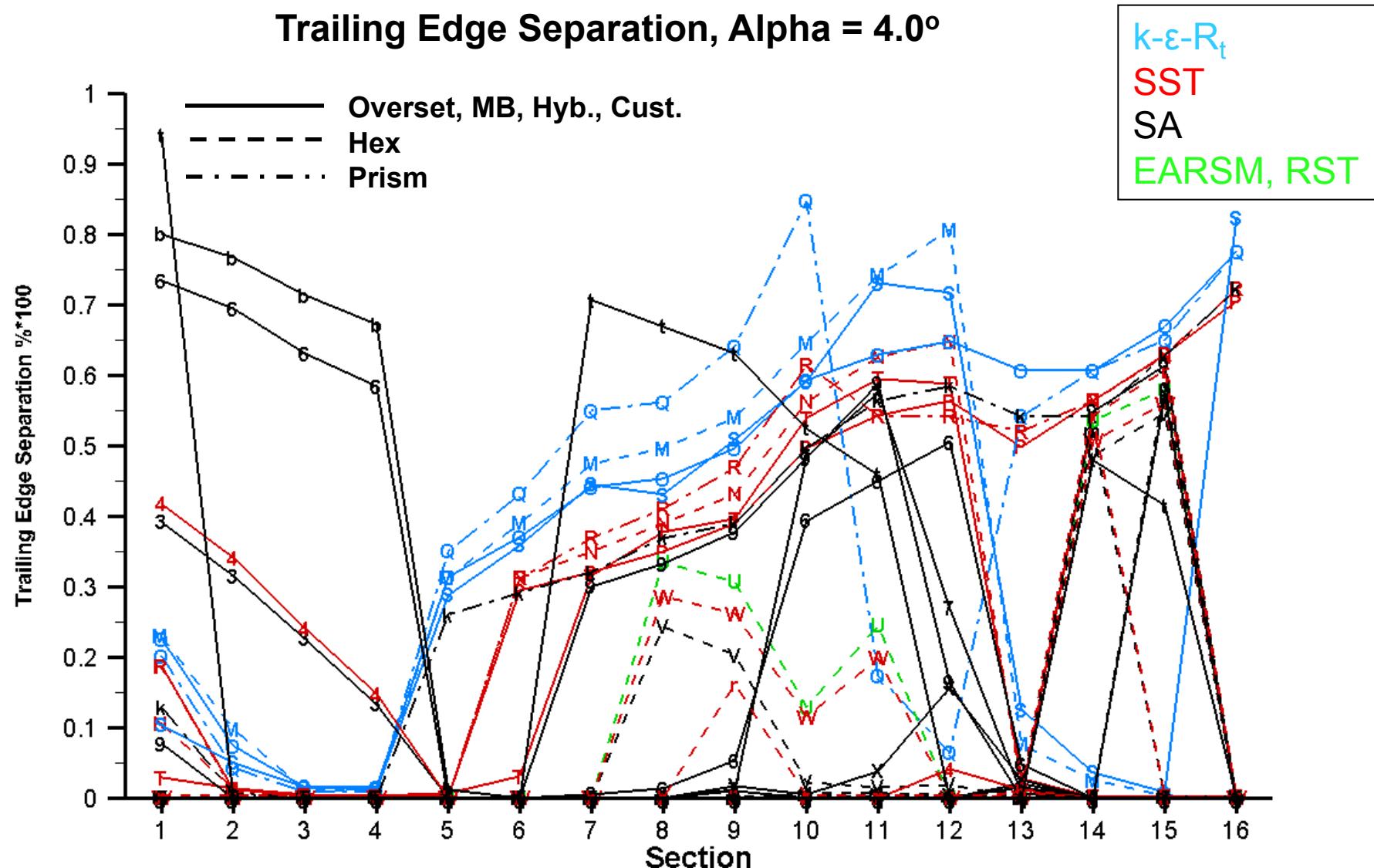
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Conclusions from Trailing Edge Separation:

- Case 1:
 - SA, SST show similar small TE sep $\leq 2\%$ between sections 8, ..., 14
 - Slightly larger for SST on coarse, medium grids
- Case 2:
 - Trend to extend towards sections 5 & 16 for $\alpha \geq 2.5^\circ$
 - No clear conclusion
- Overall check necessary whether same TE sep identification procedure has been applied



General Conclusions:

- Very successful workshop. **Thank You!**
 - 54 data submittals, many with parametric variations in grid type and/or turbulence model
- Still more variation than desired
 - Some improvement from DPW4: We are getting better
 - Mixed results from common grid study. Discretization and turbulence modeling are still a factor
- Drag comparisons to wind tunnel generally favorable
 - Variations similar between WT and CFD
 - ALPHA and CM_TOT offsets
 - Aeroelasticity



General Conclusions (Cont'd):

- Force/Moment predictions better at $\alpha=2.5^\circ$
 - Less separation
 - Bigger spread at $\alpha=4.0^\circ$
- Pressures consistent with Force/Moments
 - Correlation outboard supports aeroelastic effects
 - Wide variation in α for shock separation
- Large variations in separation prediction
 - SOB Separation
 - TE Separation and Buffet onset alpha
 - Is RANS good enough? Is flow steady?



Further Study:

- Check SOB/TE separation with wind tunnel data
 - Is flow visualization data available?
- Include static aeroelastics in CFD
 - Needed to match wind tunnel data
- Include boundary layer transition model
 - Forced/Free
- Unsteady RANS?
 - Will only help if flow is unsteady
- LES/DES?
 - DES only helps for off-body separation
 - LES (beyond current SOA?)



Applied Aerodynamics
Technical Committee

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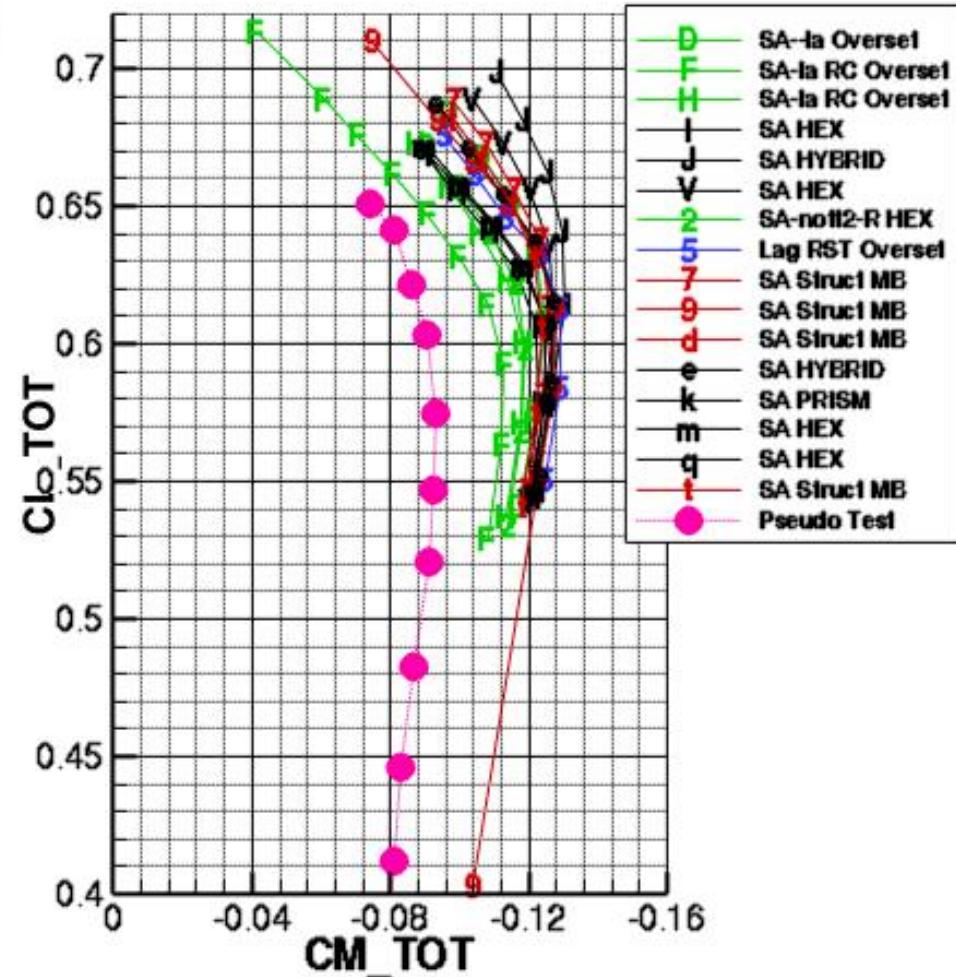
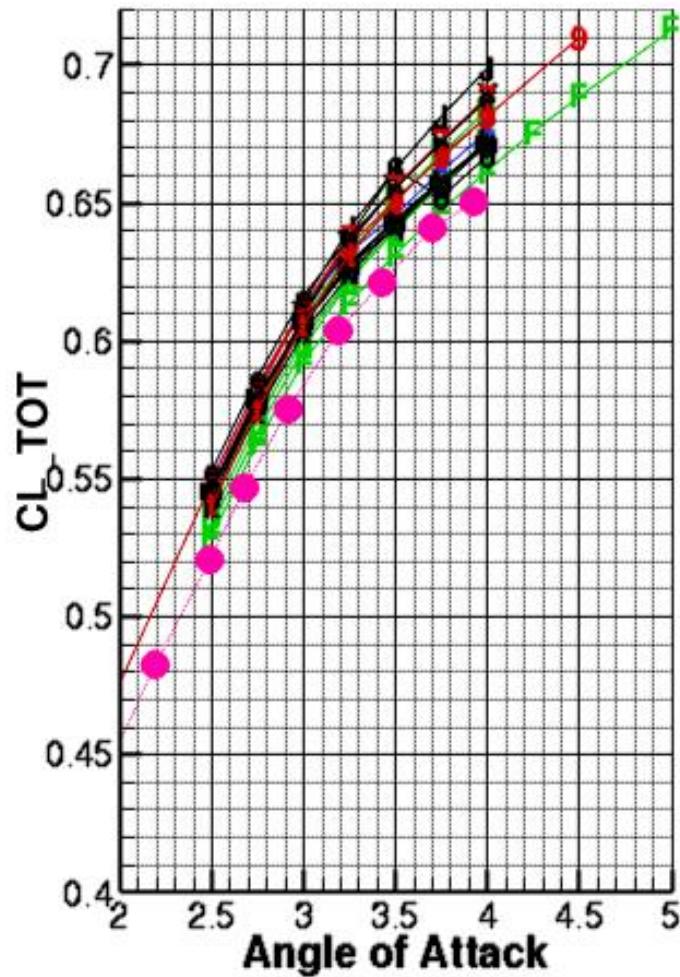
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Backup

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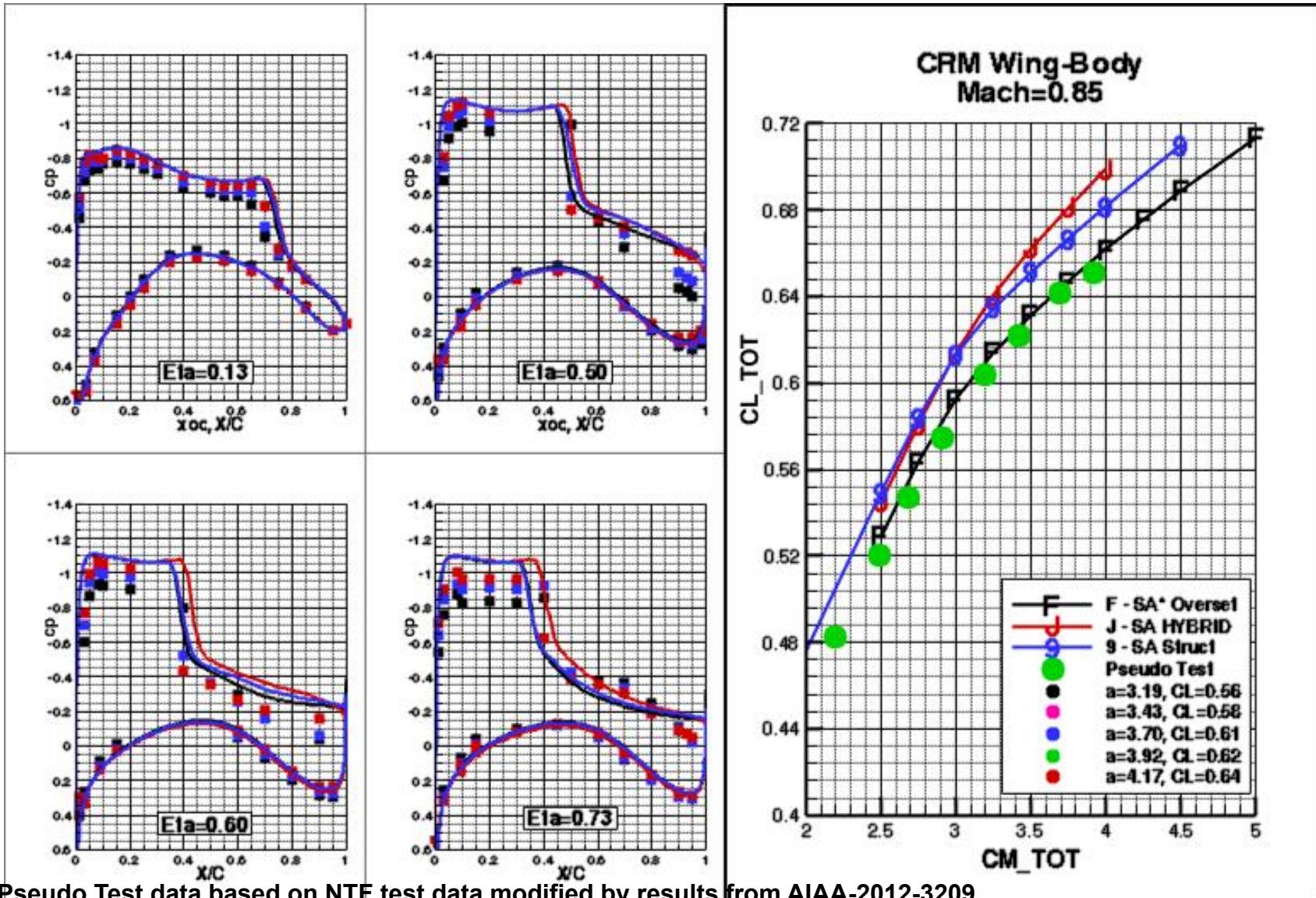
Case 2 - SA Turbulence Model
No CL Break below AoA=4.0



Pseudo Test data based on NTF test data modified by results from AIAA-2012-3209

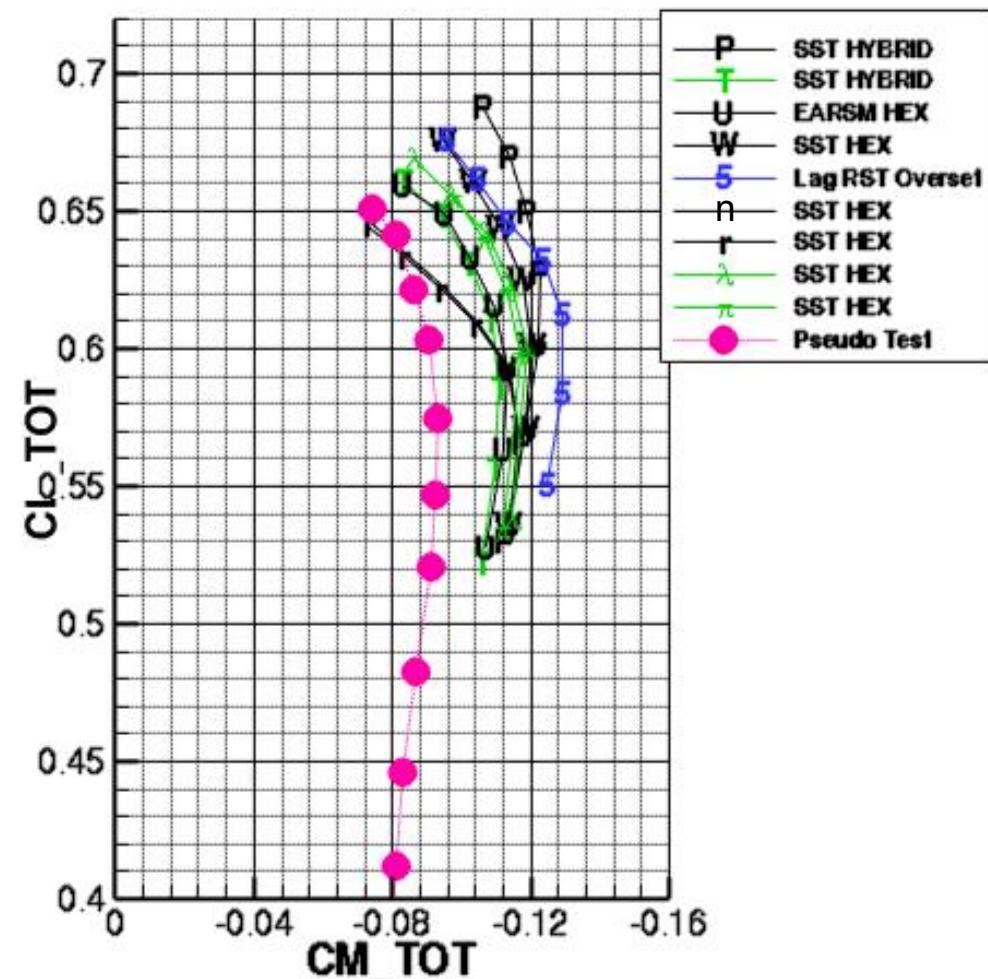
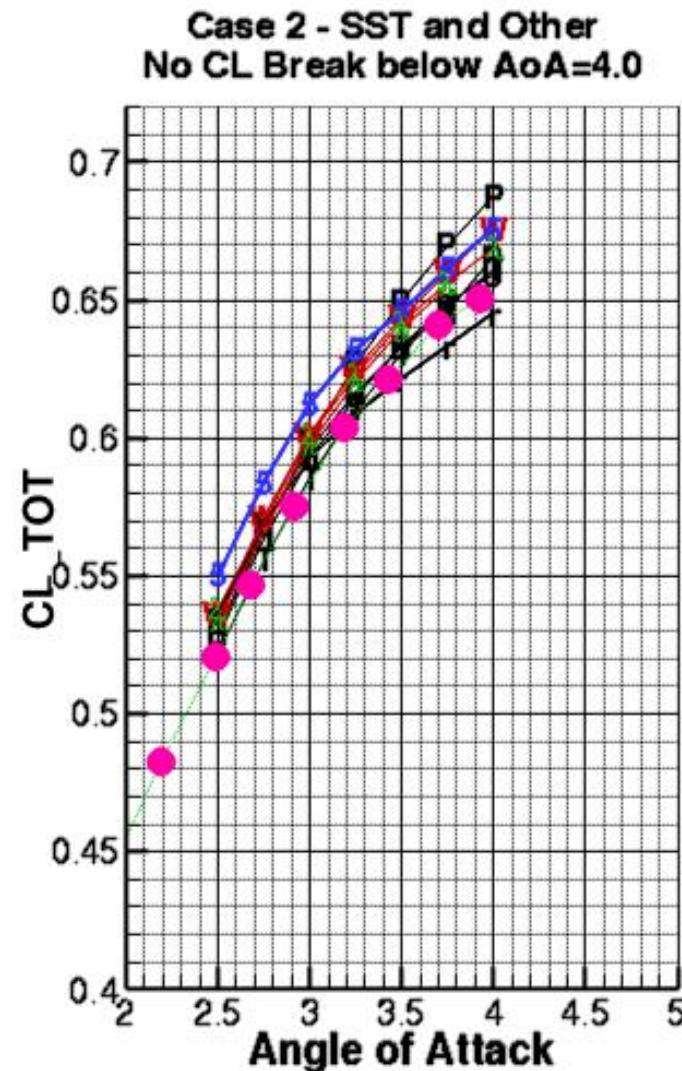
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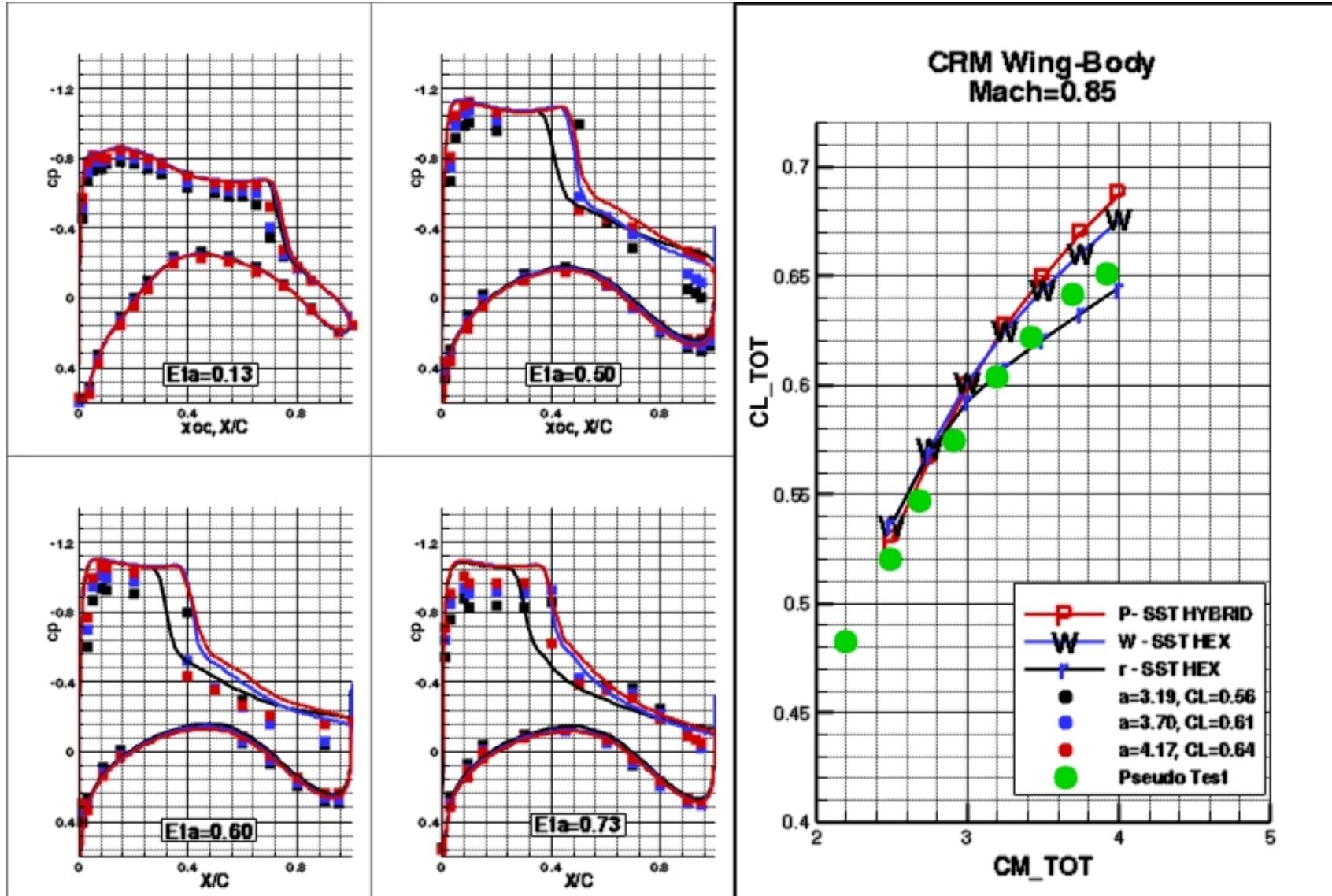
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Pseudo Test data based on NTF test data modified by results from AIAA-2012-3209