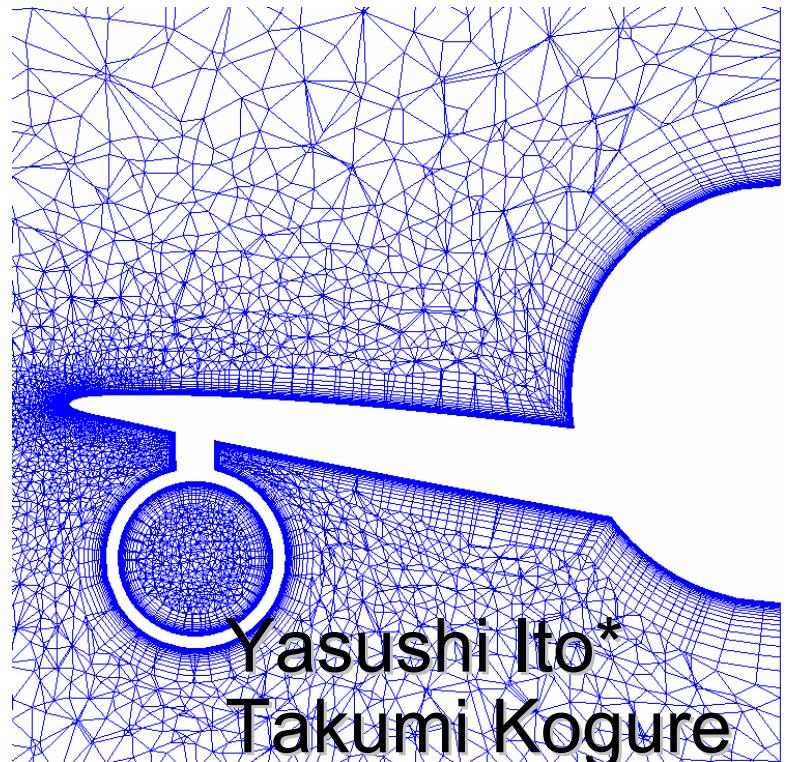
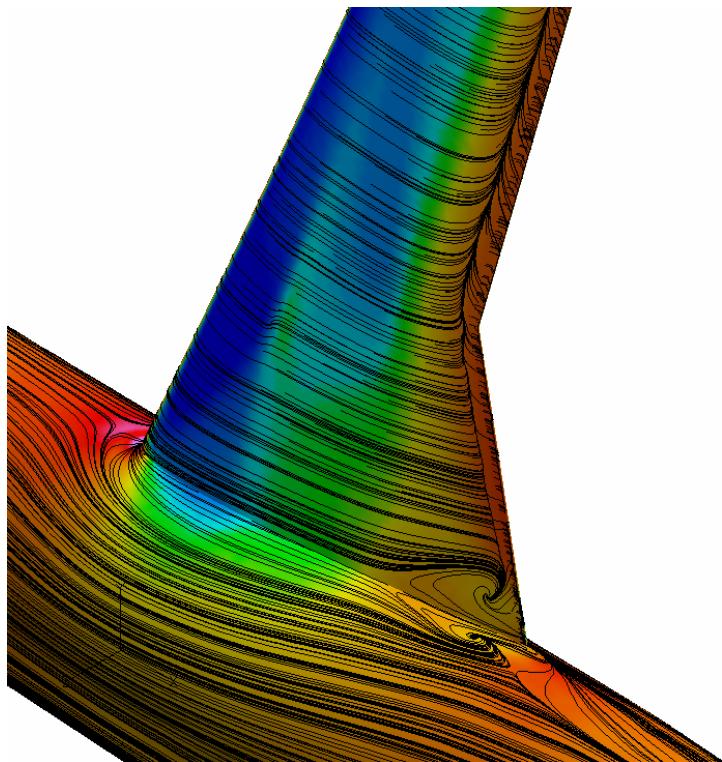


Unstructured Hybrid Mesh Generation for DLR-F6 Configuration

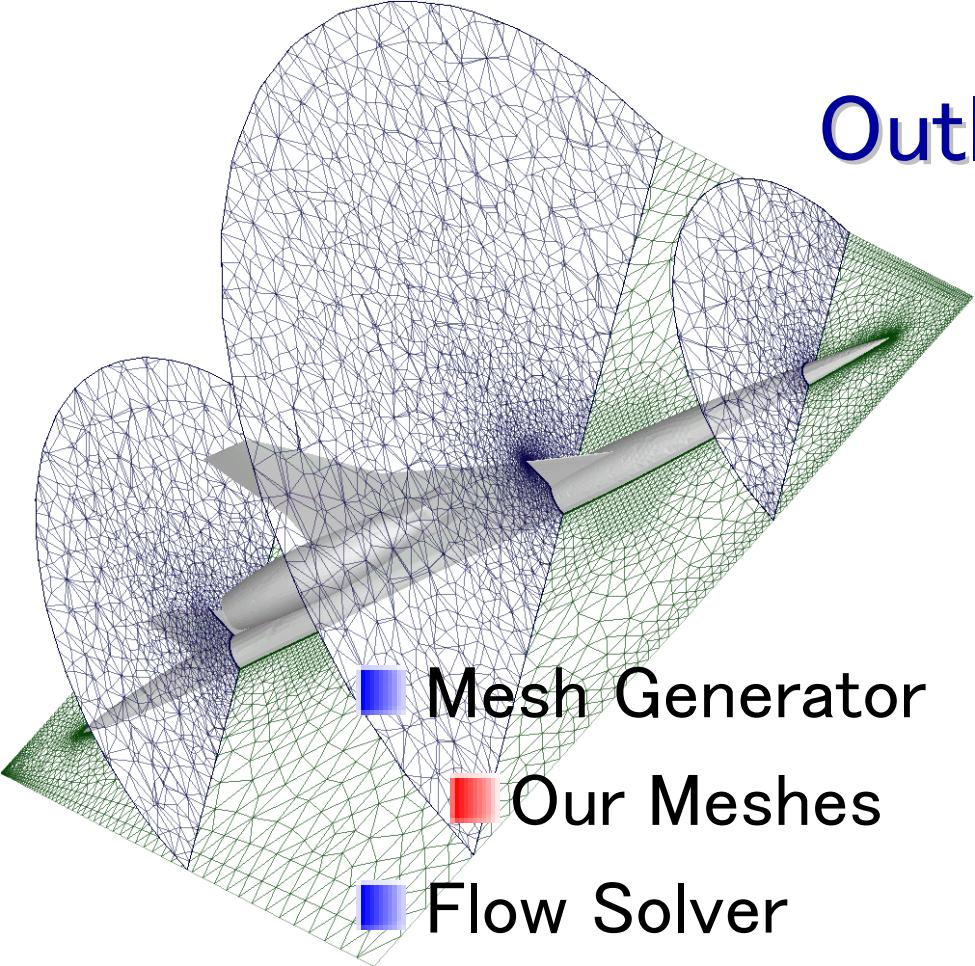


Yasushi Ito*
Takumi Kogure
Kazuhiro Nakahashi

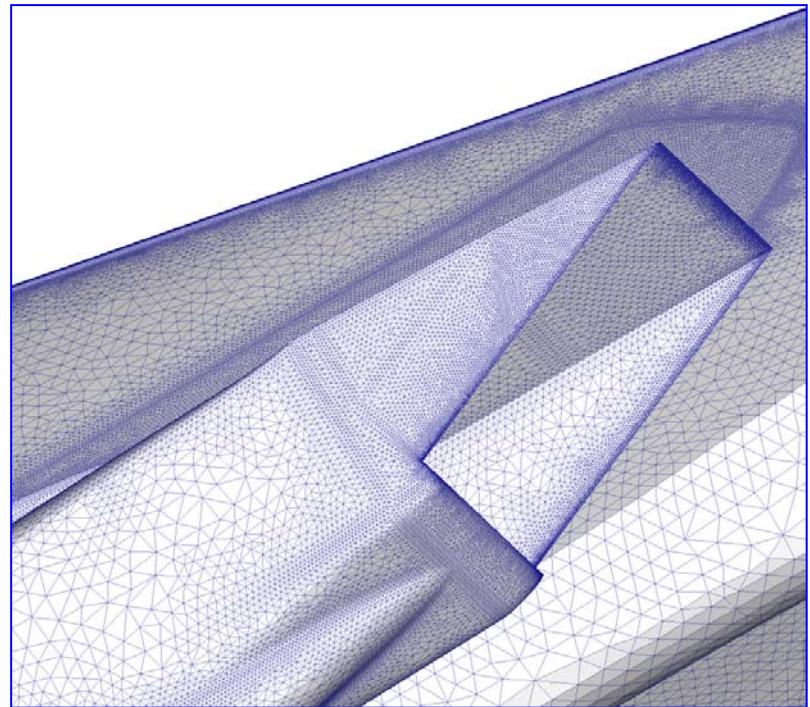
Dept. of Aeronautics and Space Eng., Tohoku Univ., JAPAN

*Currently, Dept. of Mechanical Eng., Univ. of Alabama at Birmingham

Outline



- Mesh Generator
- Our Meshes
- Flow Solver
- Result
 - Mesh Density Effect (WB)
 - Turbulence Model Effect (WBNP)
- Conclusions



Tohoku Univ. Aerodynamic Simulation Codes

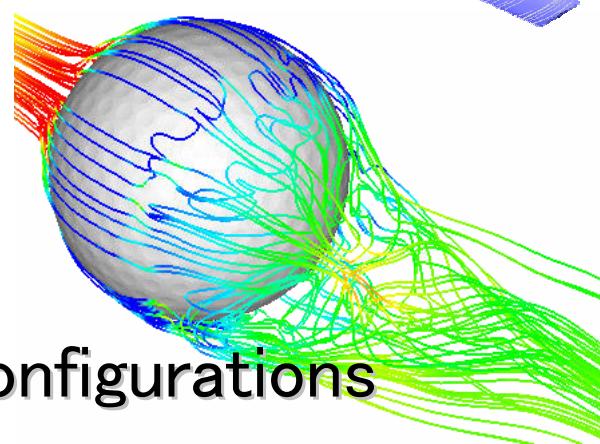
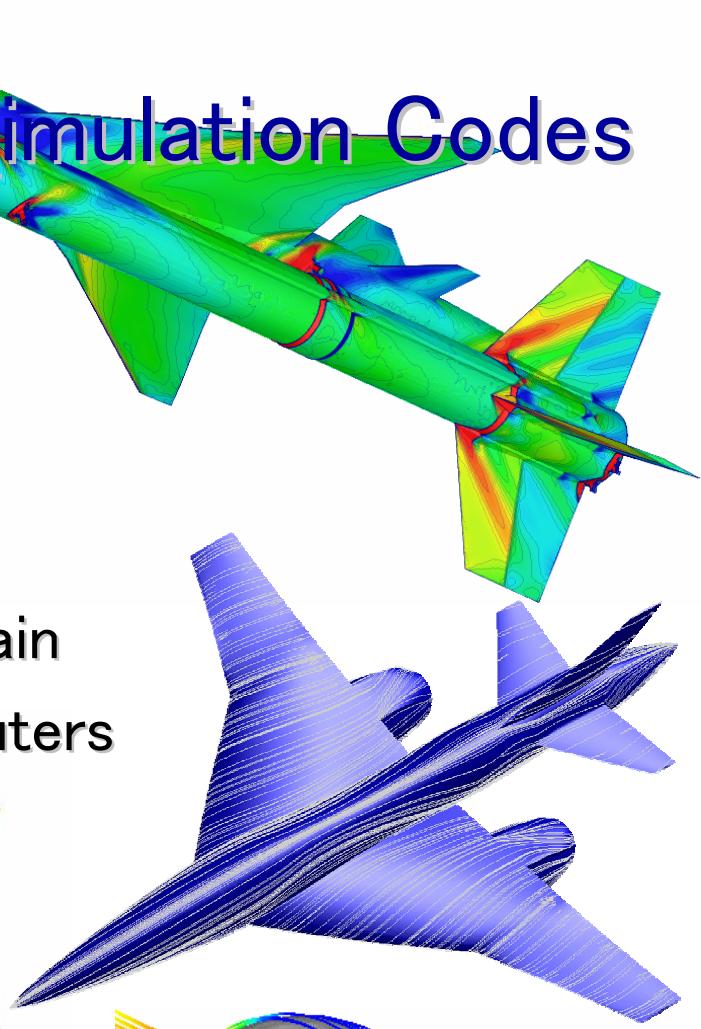
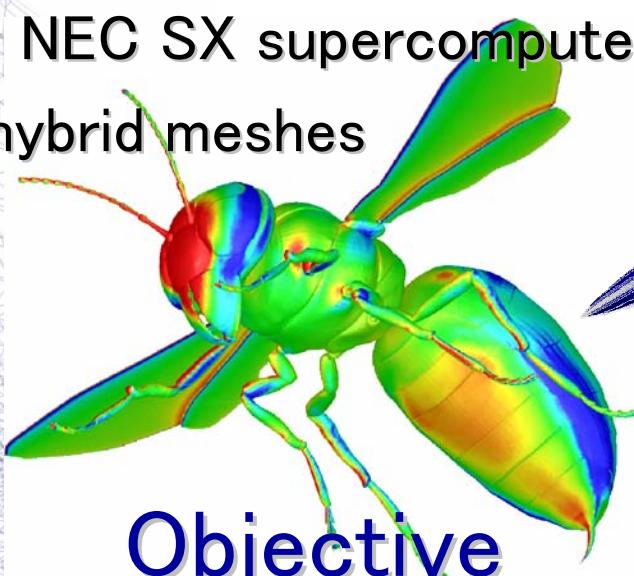
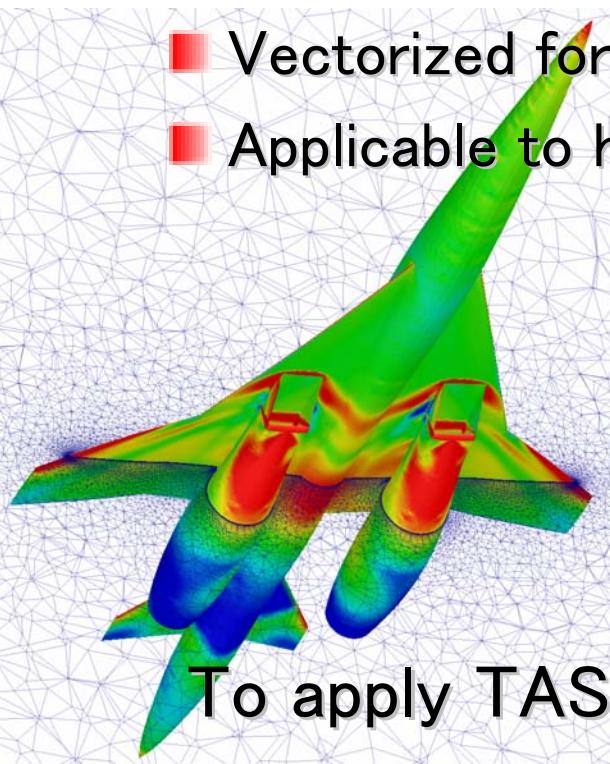
■ Unstructured Mesh Generator

- Surface mesh
- Volume mesh (inviscid/viscous)

■ Unstructured Euler/NS Solver

- Parallelized by partitioning the domain
- Vectorized for NEC SX supercomputers
- Applicable to hybrid meshes

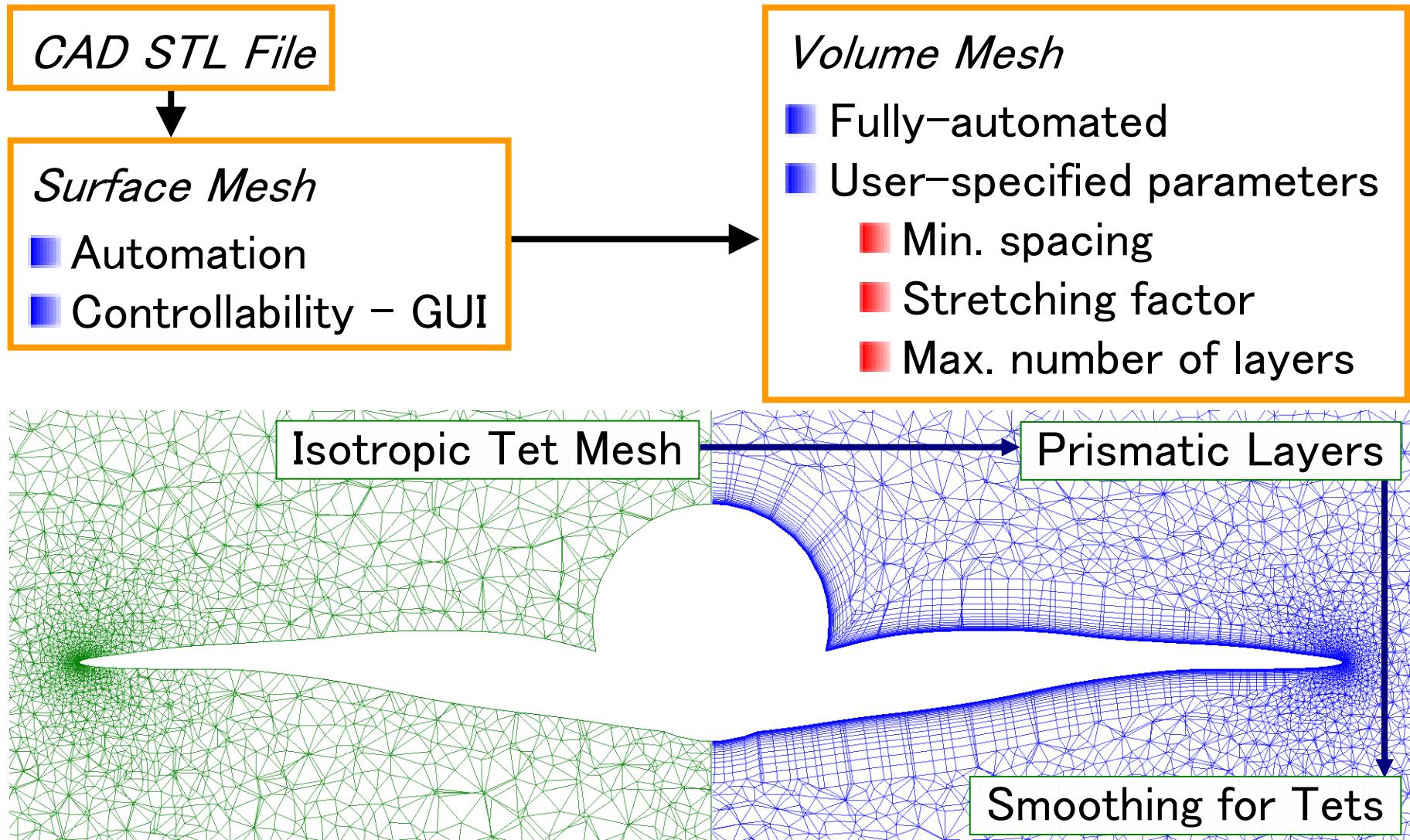
To apply TAS codes to DLR F-6 configurations



Objective

Mesh Generation: TAS-Mesh

(*Tohoku Univ. Aerodynamic Simulation*)



Surface Mesh Generation

Use of repaired STL data for background grids



Extraction of geometrical features

- To represent models more accurately
- To control local grid density
- To simplify initial front setup



Construction of an initial front

- Mouse picking to specify parameters

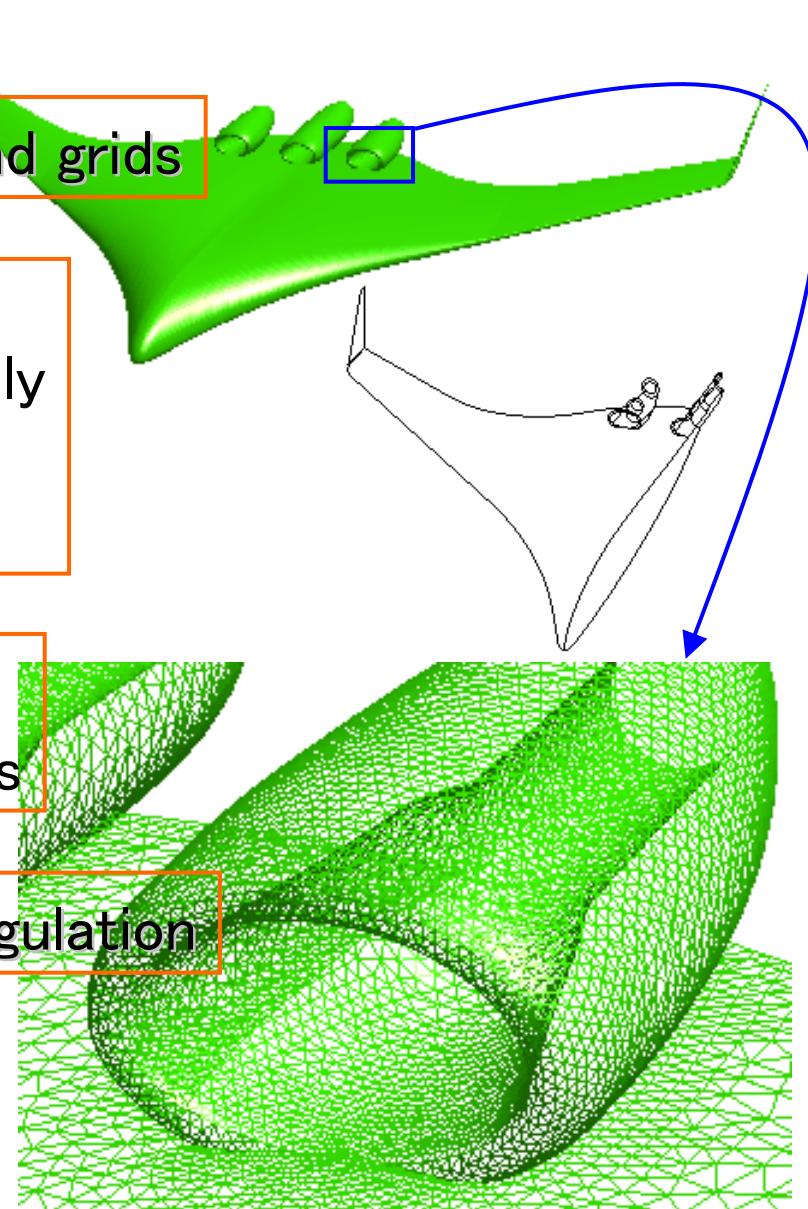


Direct advancing front method for triangulation



Surface recovery

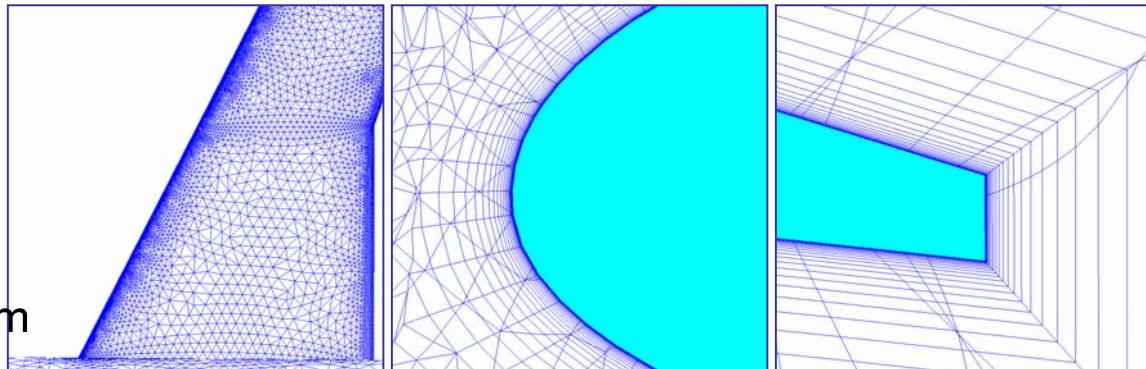
- To enhance mesh quality



Three Meshes

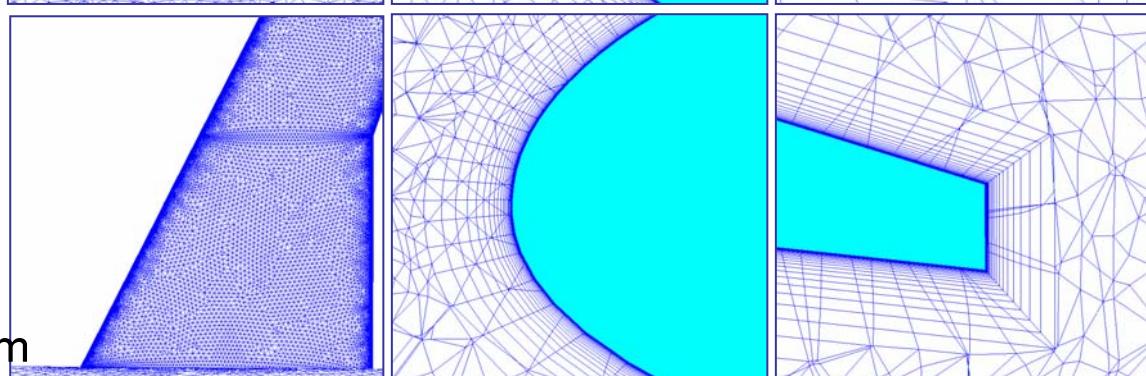
Coarse

- 1.3M nodes (WB)
- 2.0M nodes (WBNP)
- TE base: 1 cell
- Min. spacing: 2.4×10^{-3} mm



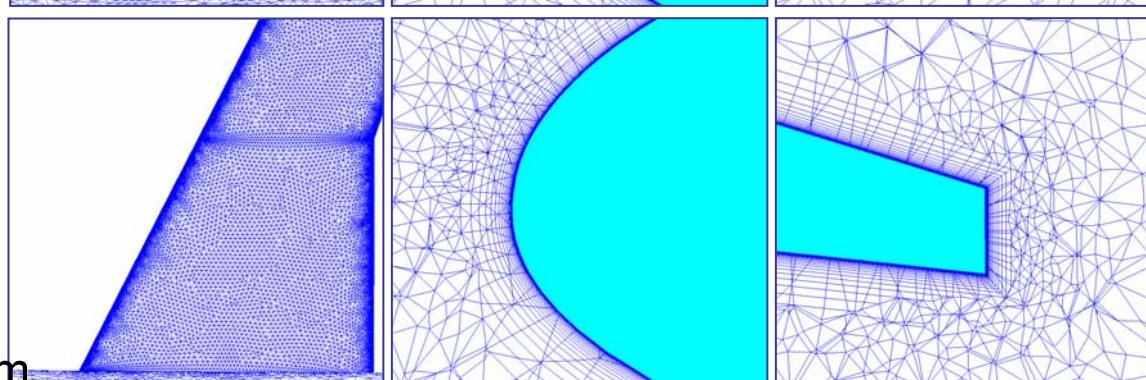
Intermediate

- 3.9M nodes (WB)
- 5.6M nodes (WBNP)
- TE base: 3 cells
- Min. spacing: 6.0×10^{-4} mm



Fine

- 11.3 M nodes (WB)
- 17.0 M nodes (WBNP)
- TE base: 9 cells
- Min. spacing: 1.5×10^{-4} mm



Wing upper surf.

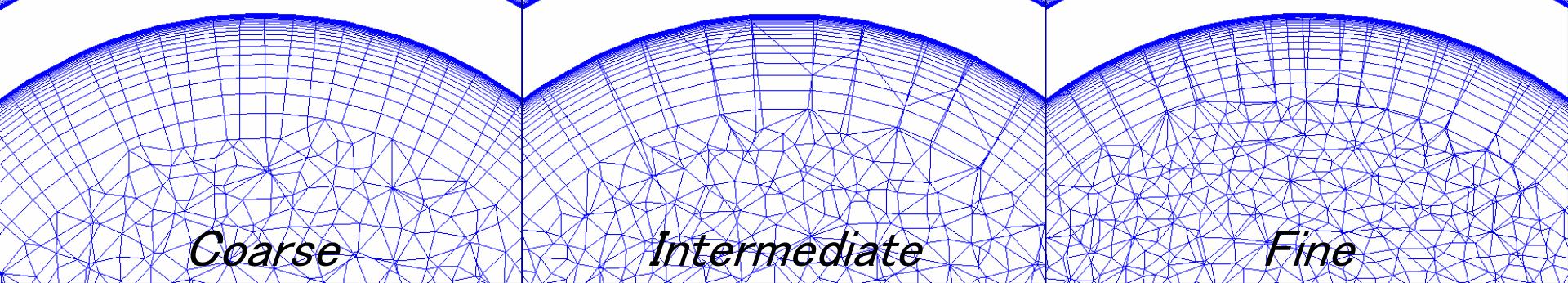
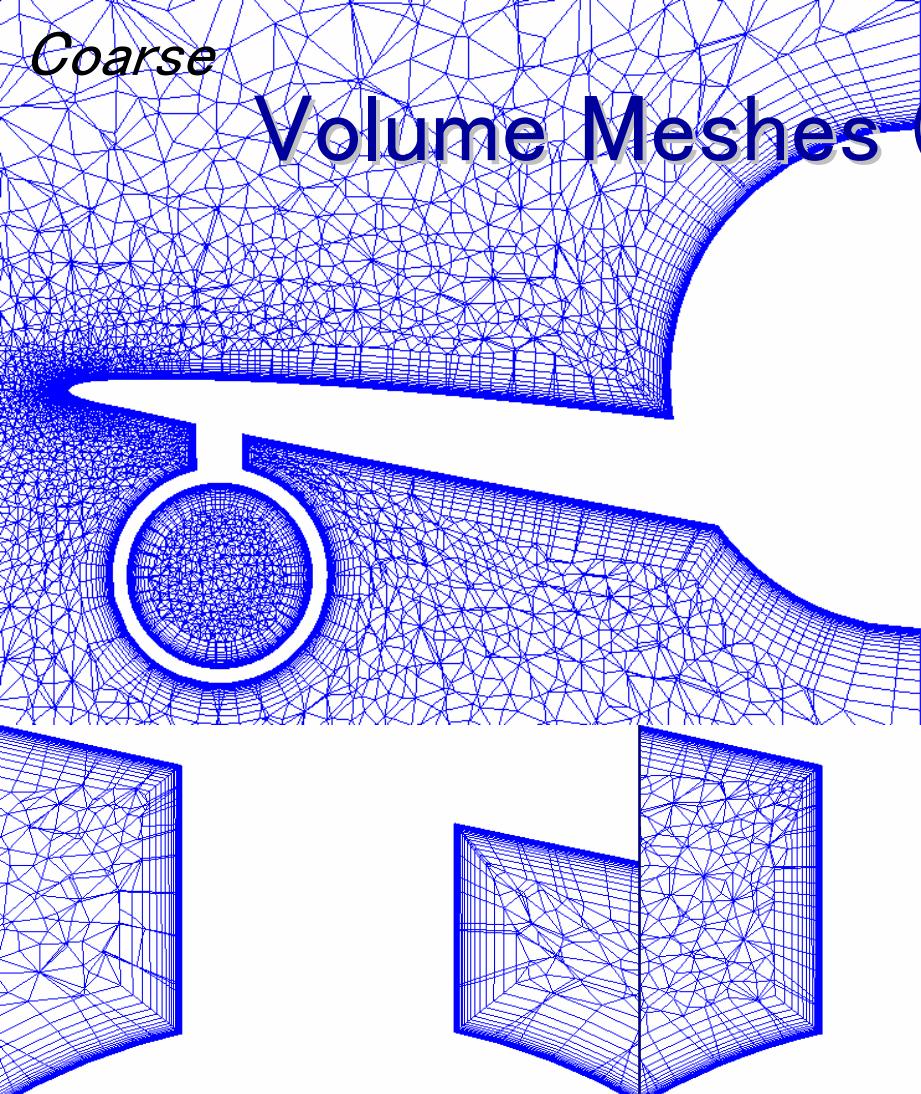
LE

TE

Coarse

Volume Meshes (WBNP, $x/L = 40\%$)

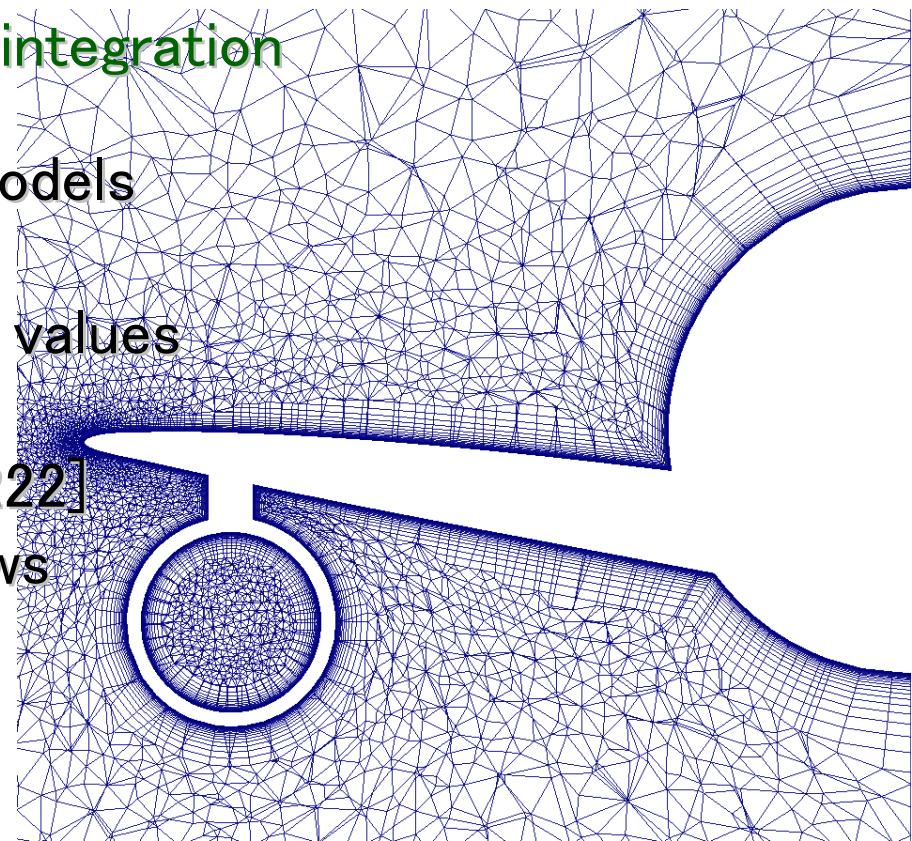
- Smooth transition from prismatic layers to tets



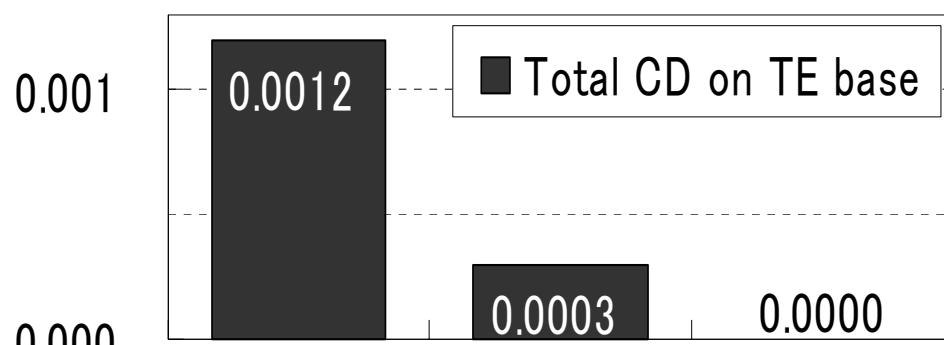
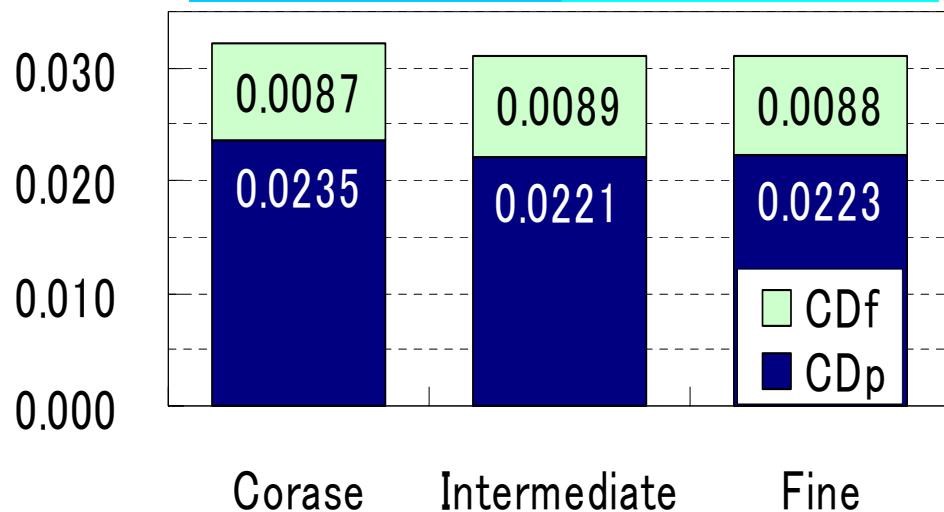
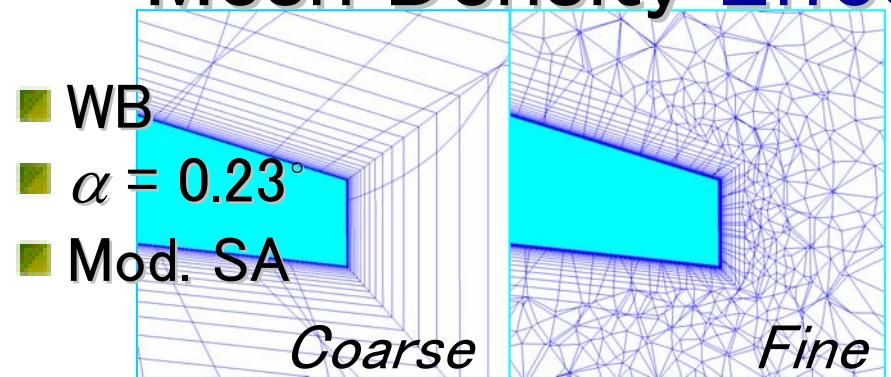
Flow Solver: TAS-FLOW

(*Tohoku Univ. Aerodynamic Simulation*)

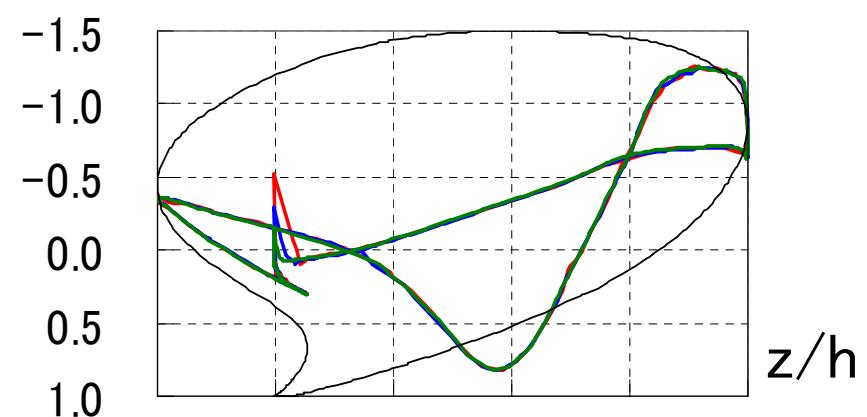
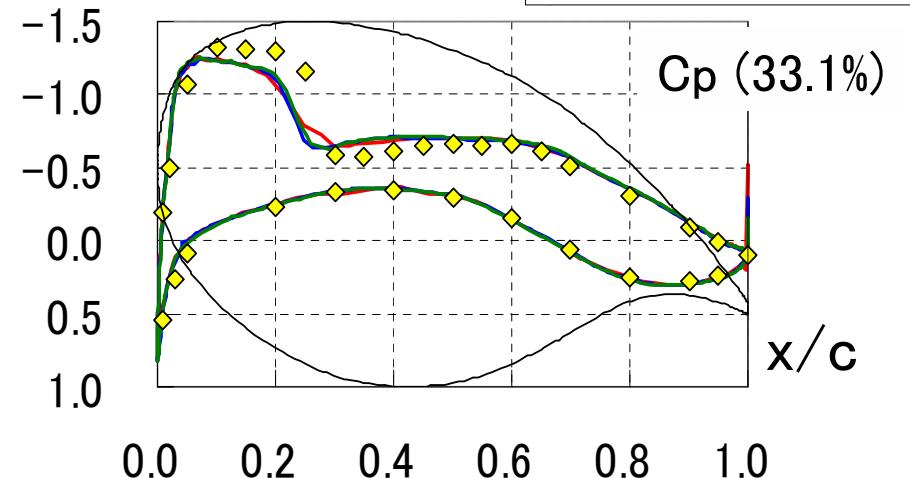
- RANS equations
- Cell-vertex finite volume method
- HLLEW Riemann solver for flux computation
- Venkatakrishnan's limiter to reconstruct 2nd order accuracy
- LU-SGS implicit method for time integration
- Three one-equation turbulence models
 - Goldberg–Ramakrishnan (GR)
 - ✓ Not requiring wall distance values
 - Spalart–Allmaras (SA)
 - Mod. SA [AIAA Paper 2000–2222]
 - ✓ Modified for free shear flows
- Fully turbulent



Mesh Density Effect on CD & Cp



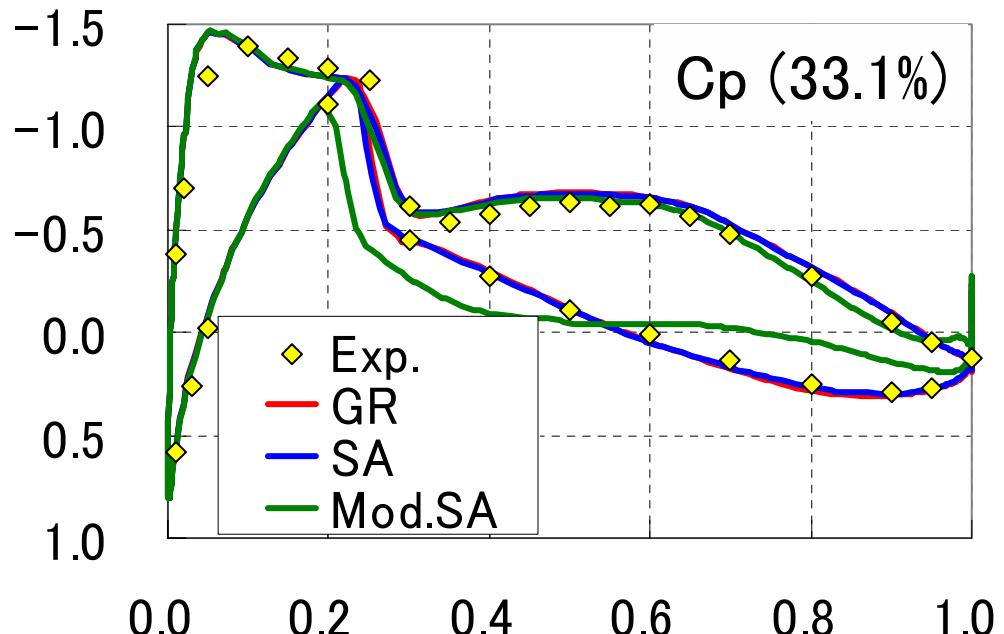
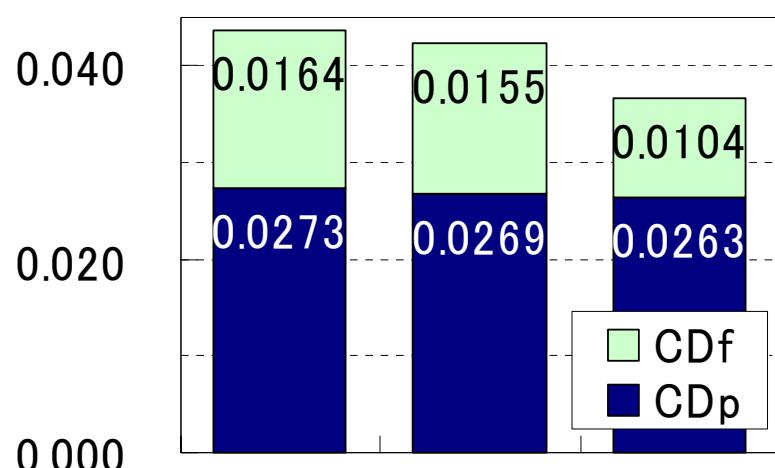
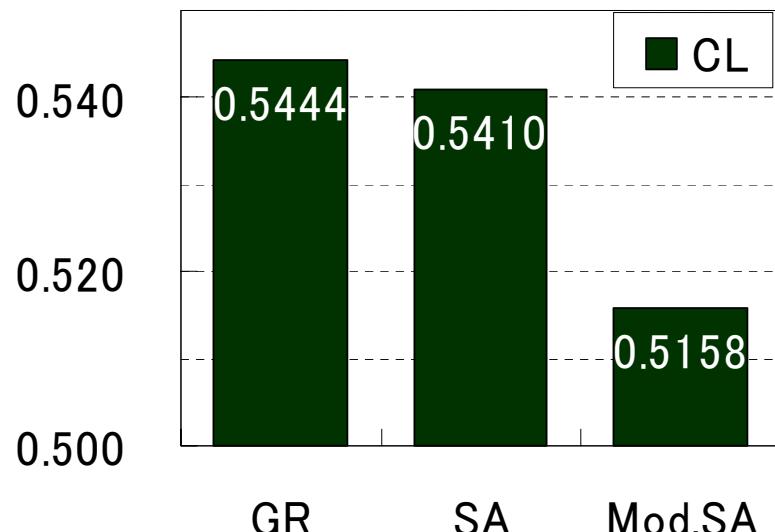
- Coarse
- Intermediate
- Fine
- ◆ Exp.
- Wing



- Almost the same total CD
- Big difference at TE base

Turbulence Model Effect on CL, CD & Cp

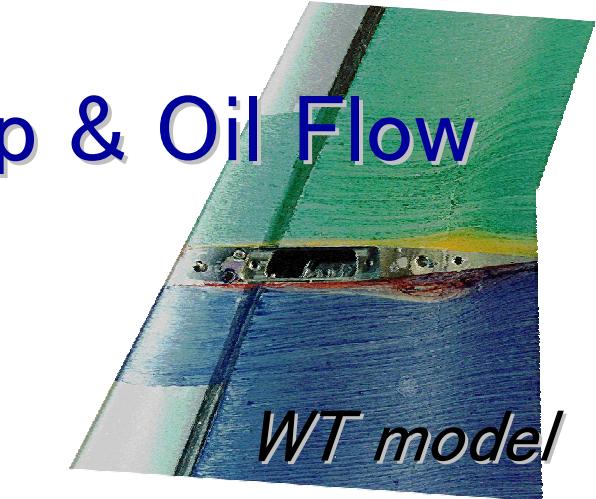
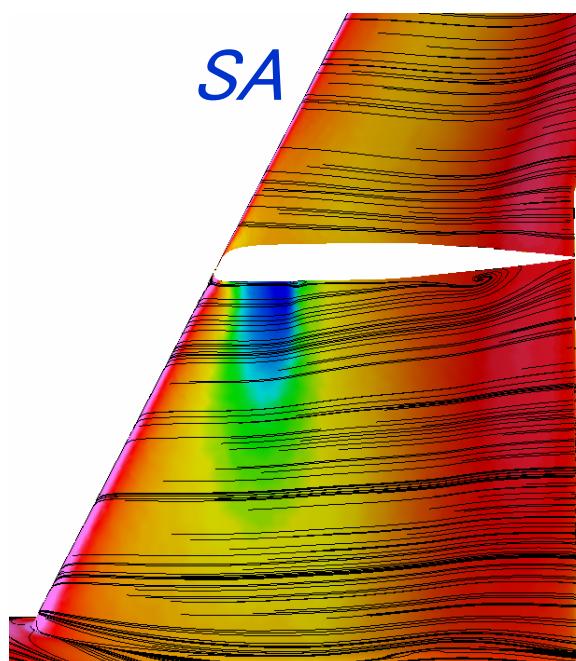
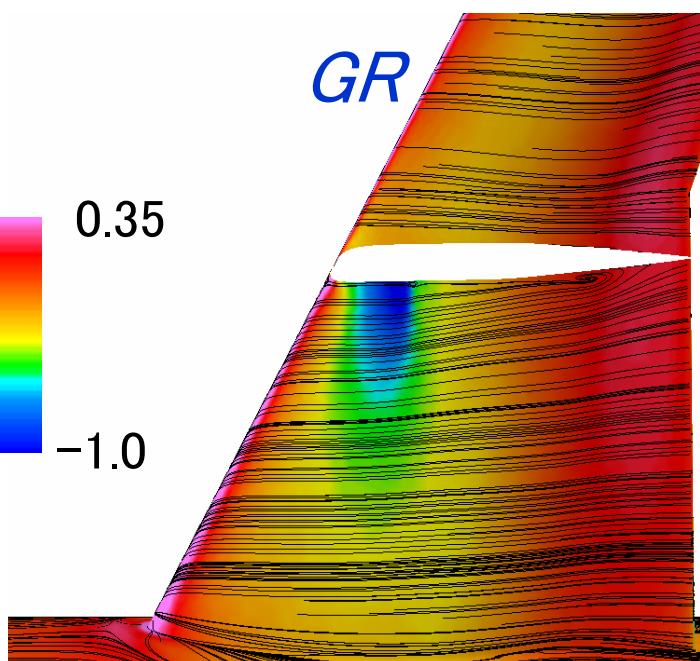
- WBNP (Intermediate)
- $\alpha = 1.0^\circ$ ($CL = 0.5$)



- CL & CD_f: Mod. SA estimating smaller
- Cp: Big difference at 33.1% station

Turbulence Model Effect on Cp & Oil Flow

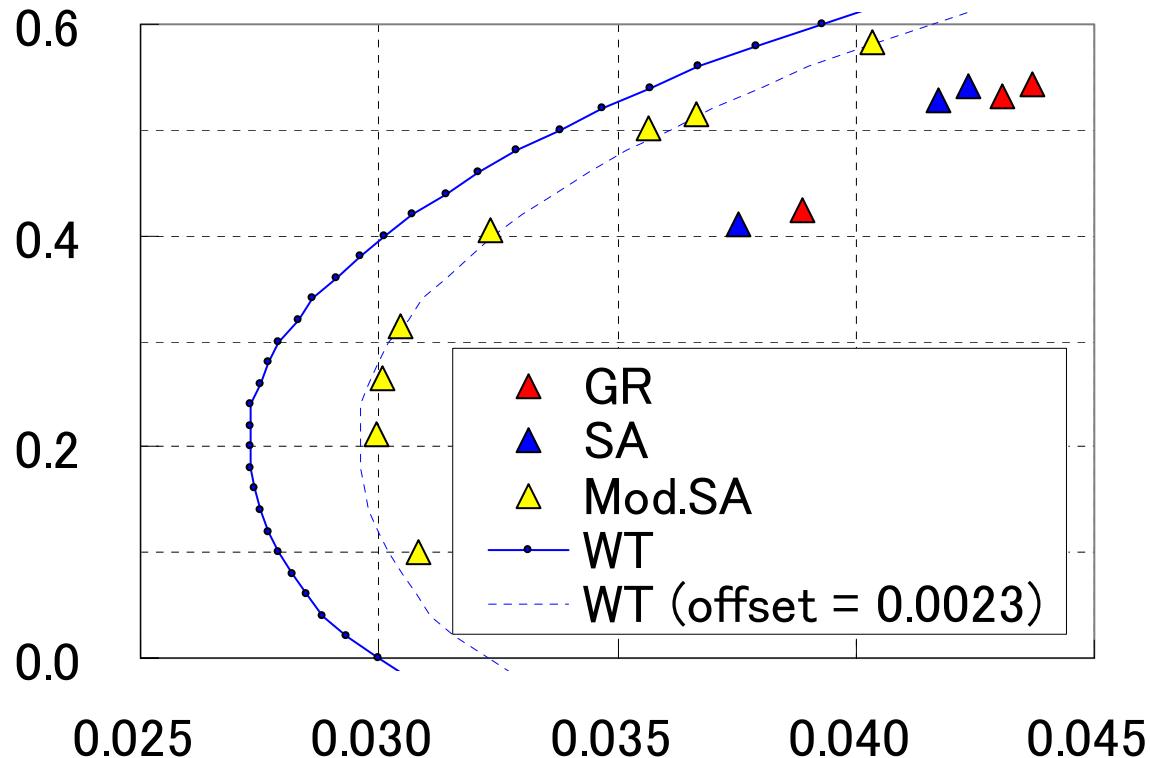
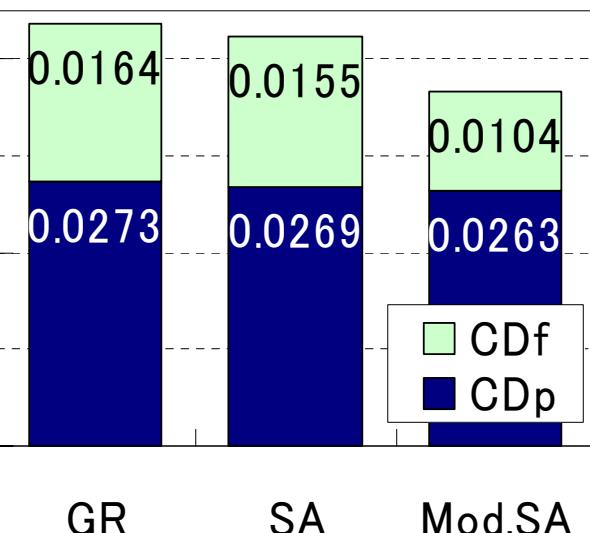
- WBNP (Intermediate)
- $\alpha = 1.0^\circ$ ($CL = 0.5$)



- Mod. SA estimating
- Too big separation
- Different shock wave location

Turbulence Model Effect on Drag Polar

■ WBNP (Intermediate)



- Fully turbulent
- Mod. SA estimating smaller CD_f
- Still higher CD comparing with exp.
- Higher CD_p ?
- Spatial mesh resolution?

Conclusions

Tohoku Univ. Aerodynamic Simulation codes were applied to the numerical simulation of the DLR F-6 configurations

- TAS-Mesh: Unstructured mesh generator
- TAS-FLOW: Unstructured, parallelized flow solver
- Attached flow regions were not affected by
 - Mesh resolutions
 - Type of turbulence models
- GR and SA produced basically similar results
- Mod. SA estimated
 - Smaller CL and CDf
 - Bigger separations
- The effect of the spatial mesh resolution to the solution accuracy should be evaluated