



DPW-VI Status

**John Vassberg
Chairman, DPW-OC**

August 28, 2015

For Public Release

DPW Nomenclature

| | |
|------------|--|
| • AE | Aero-Elastic |
| • AoA | Angle-of-Attack / Alpha |
| • CFD | Computational Fluid Dynamics |
| • CL,CD,CM | Coefficients of Lift, Drag, Pitching-Moment |
| • CRM | NASA Common Research Model |
| • DPW OC | Drag Prediction Workshop Organizing Committee |
| • FEM | Finite-Element Model |
| • M-DOF | Million Degrees-of-Freedom |
| • N | Grid Size in Number DOFs |
| • PD | Public Domain |
| • SOA | State of the Art |
| • SOP | State of the Practice |
| • TMR | Transition Modeling Resource Website |
| • WBNPT | Wing/Body/Nacelle/Pylon/Tail (Any Combination) |
| • WT | Wind Tunnel |

DPW Series – Brief History

- **DPW Charter Formalized** Jan 2000
 - State of the Art/Practice CFD Drag Prediction
- **DPW-I, Anaheim, CA** Jun 2001
 - DLR-F4 WB, Fixed CL & Drag Polar Studies
 - Scatter > 100 Counts → SOP Worse Than Expected
- **DPW-II, Orlando, FL** Jun 2003
 - DLR-F6 WB & WBNP, Fixed-CL Grid Convergence
 - Scatter > 50 Counts, Drag Deltas, Juncture Flow Issues
- **DPW-III, San Francisco, CA** Jun 2006
 - DLR-F6 WB & WBF, DPW-W1/W2 Wing-Only Fixed AoA
- **DPW-IV, San Antonio, TX** Jun 2009
 - CRM WBT, Trim-Drag Study, Blind CFD Predictions
- **DPW-V, New Orleans, LA** Jun 2012
 - CRM WB, Common Grid Study, TMR Verification Case
- **DPW-VI, Washington, DC** Jun 2016
 - CRM WB & WBNP, Aero-Elastic Deflection Study

DPW-VI: Organizing Committee

- Olaf Brodersen, DLR
- Ed Feltrop, Cessna
- Martin Gariepy, École Polytechnique de Montréal
- David Hue, ONERA
- Stefan Keye, DLR
- Kelly Laflin, Cessna
- Mori Mani, Boeing
- Dimitri Mavriplis, UWy
- Joe Morrison, NASA
- Mitsuhiro Murayama, JAXA
- Ben Rider, Boeing
- Chris Roy, VaTech
- Ed Tinoco, Retired
- John Vassberg, Boeing
- Rich Wahls, NASA

15 Members
5 New Members
10 Institutions
5 Countries
3 Continents

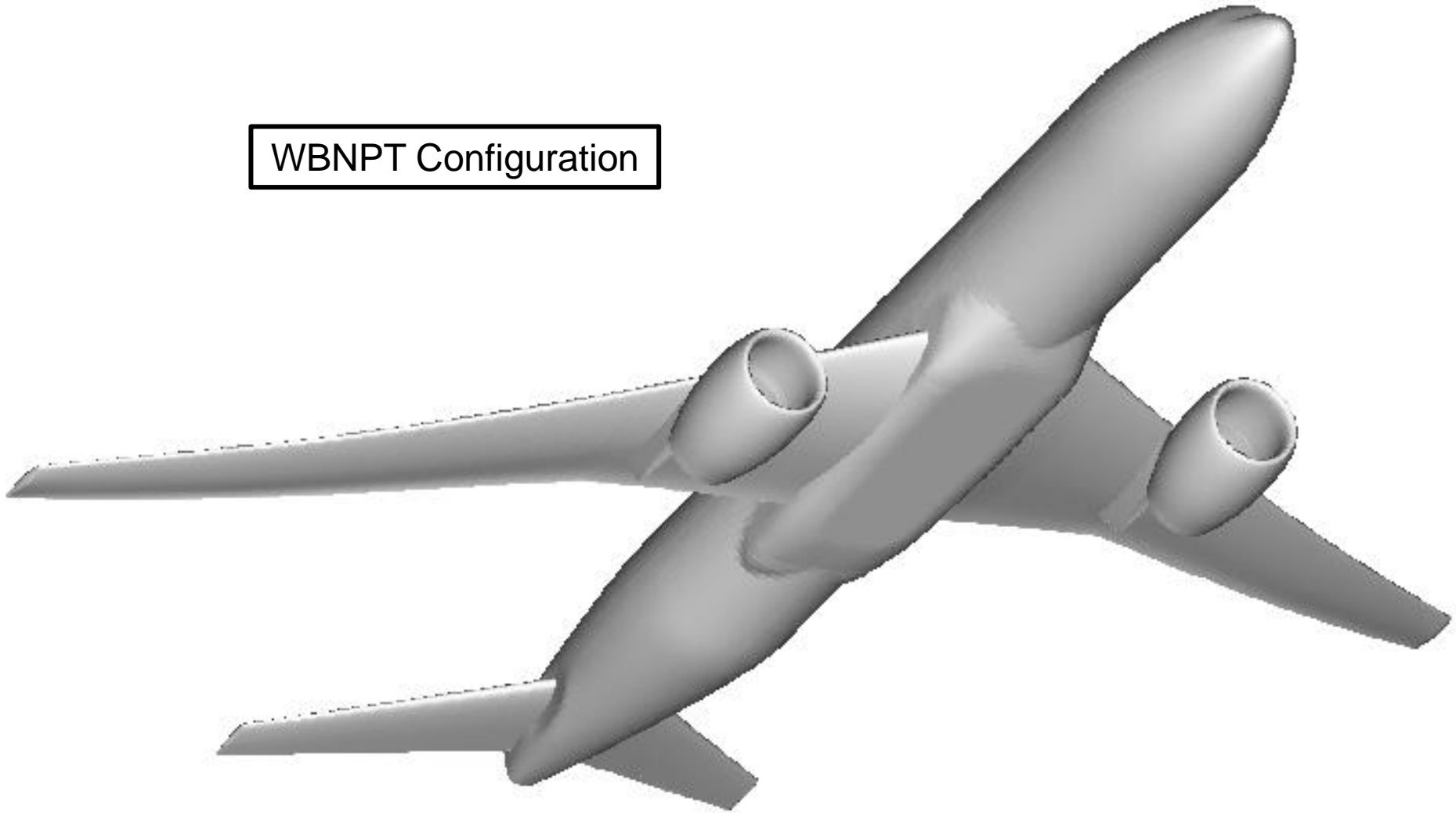
DPW-VI: (Working) Schedule of Events

- Rough Draft Test Cases 15 Jan 2015 ✓
- Finalize Aero-Elastic Deformations 31 Jan 2015 ✓
- Finalize IGES Geometry Definitions 31 Apr 2015 ✓
- Finalize Test Cases 15 May 2015 ✓
- Finalize DPW-VI Flyer 01 Jun 2015 ✓
- Release IGES Files to Public Domain 21 Jun 2015
- Release Standard Grids to PD 31 Jul 2015
- Notice of Intent to Participate 01 Dec 2015
- Acceptance Notification 31 Jan 2016
- Data Submittal 01 May 2016
- Workshop, WDC 11–12 Jun 2016

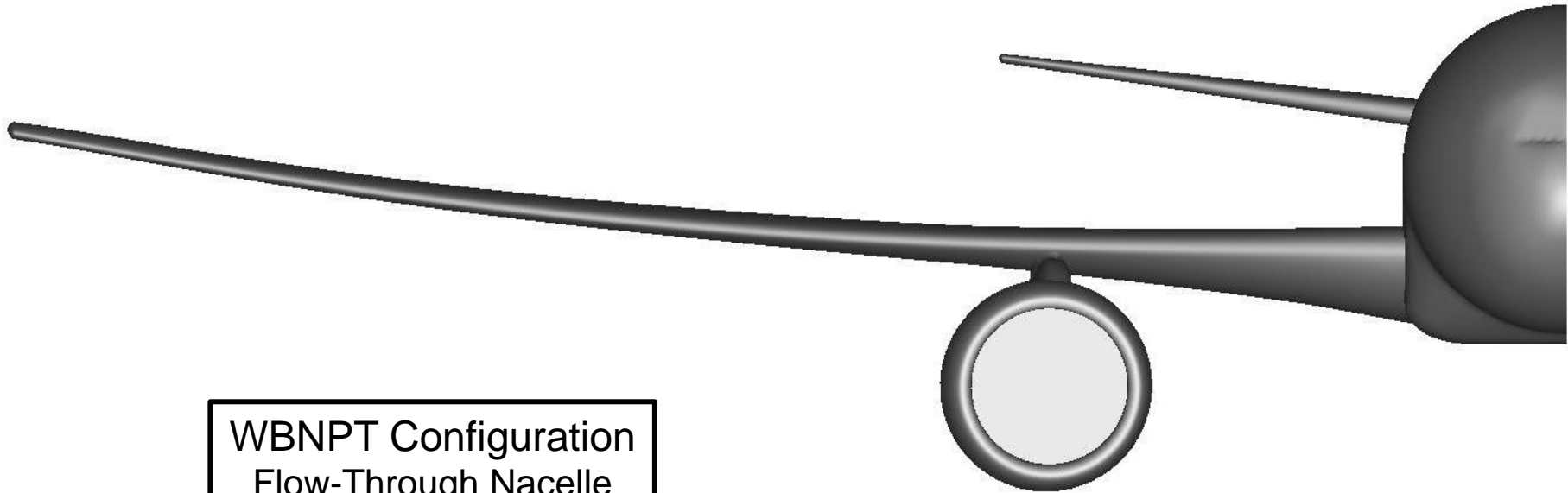
- Registration- Handled by AIAA

NASA Common Research Model (CRM)

WBNPT Configuration



NASA Common Research Model (CRM)



WBNPT Configuration
Flow-Through Nacelle
Horizontal Tail @ $\alpha_H=0^\circ$
Undelected Wing

DPW-VI: Requested Test Cases

- **Case 1: Verification Study**

- 2D NACA0012 Airfoil - Turbulence Modeling Resource (TMR)
- $M=0.15$, $Re=6$ million, $AoA=10$ deg, Farfield BC @ 2400 Chords
- Solution Converged on Adapted or Fixed Sequence Grid Family

- **Case 2: CRM Nacelle-Pylon Drag Increment**

- $Mach=0.85$, $Re=5$ million, $CL=0.5 \pm 0.0001$, $ae2.75deg$ geometry
- Grid Convergence Study on Baseline WB & WBNP Grid Families
- [CD , CM , AoA , Mass-Flux] .vs. $N^{-(2/3)}$ [or other metric]

- **Case 3: CRM WB Static Aero-Elastic Effect**

- $Mach=0.85$, $Re=5$ million
- AoA Sweep with ETW Deflections
- $AoA=[2.50, 2.75, 3.00, 3.25, 3.50, 3.75, 4.00]$ degrees
- Medium Baseline Grids: [7 Solutions on 7 Grids]

DPW-VI: Optional Test Cases

- **Case 4: CRM WB Grid Adaptation**

- Mach=0.85, Re=5 million, CL=0.5 +/-0.0001, ae2.75deg geometry
- Start Adaption Process from Tiny (or Coarse) Baseline Mesh
- Participants Document Adaptation Process

- **Case 5: CRM WB Coupled Aero-Structural Simulation**

- Mach=0.85, Re=5 million, CL=0.5 +/-0.0001
- Medium Baseline Grid
- FEM Supplied by NASA via CRM Website (Melissa Rivers)
 - Modal Shapes and Frequencies available

- **Cases 1-5: Participant Generated Grids**

- Provide Documentation of Their Grid Systems
- Submit Their Grids to the Public Domain
- Also Run the Cases on the Baseline Grids

DPW-VI: Baseline Grid Families

| Name | WB | WBNP | Δy_1 |
|----------------|------|---------|--------------|
| Tiny (T) | ~20 | 25-30 | 0.001478" |
| Coarse (C) | ~30 | 40-45 | 0.001285" |
| Medium (M) | ~45 | 60-70 | 0.001118" |
| Fine (F) | ~70 | 85-100 | 0.000972" |
| Extra Fine (X) | ~100 | 130-150 | 0.000845" |
| Ultra Fine (U) | ~150 | 190-225 | 0.000735" |

Nominal Size of Grid System in M-DOF

At Least 4 Sequential Mesh Levels & Bias Towards Finest

DPW-VI: Gridding Guidelines (1/2)

- **Tiny Grid**

- Viscous Wall Spacing: $Y^+ \sim 1.0 \rightarrow \Delta y_1 = 0.001478''$
- At Least 2 Constantly-Spaced Cells at Viscous Walls, $\Delta y_2 = \Delta y_1$
- Growth Rates $< 1.2X$ Normal to Viscous Walls
- Wing Spanwise Spacing $< 0.1\% \cdot \text{Semispan}$ at Root, Engine & Tip
- WNP Chordwise Spacing $< 0.1\% \cdot C$ (local chord) at LE & TE
- Wing & Nacelle TE Base $\gg 8$ Cells [Pylon TE is Sharp]
- Spacing Near Fuselage Nose & Afterbody $< 1\% \cdot C_{ref}$

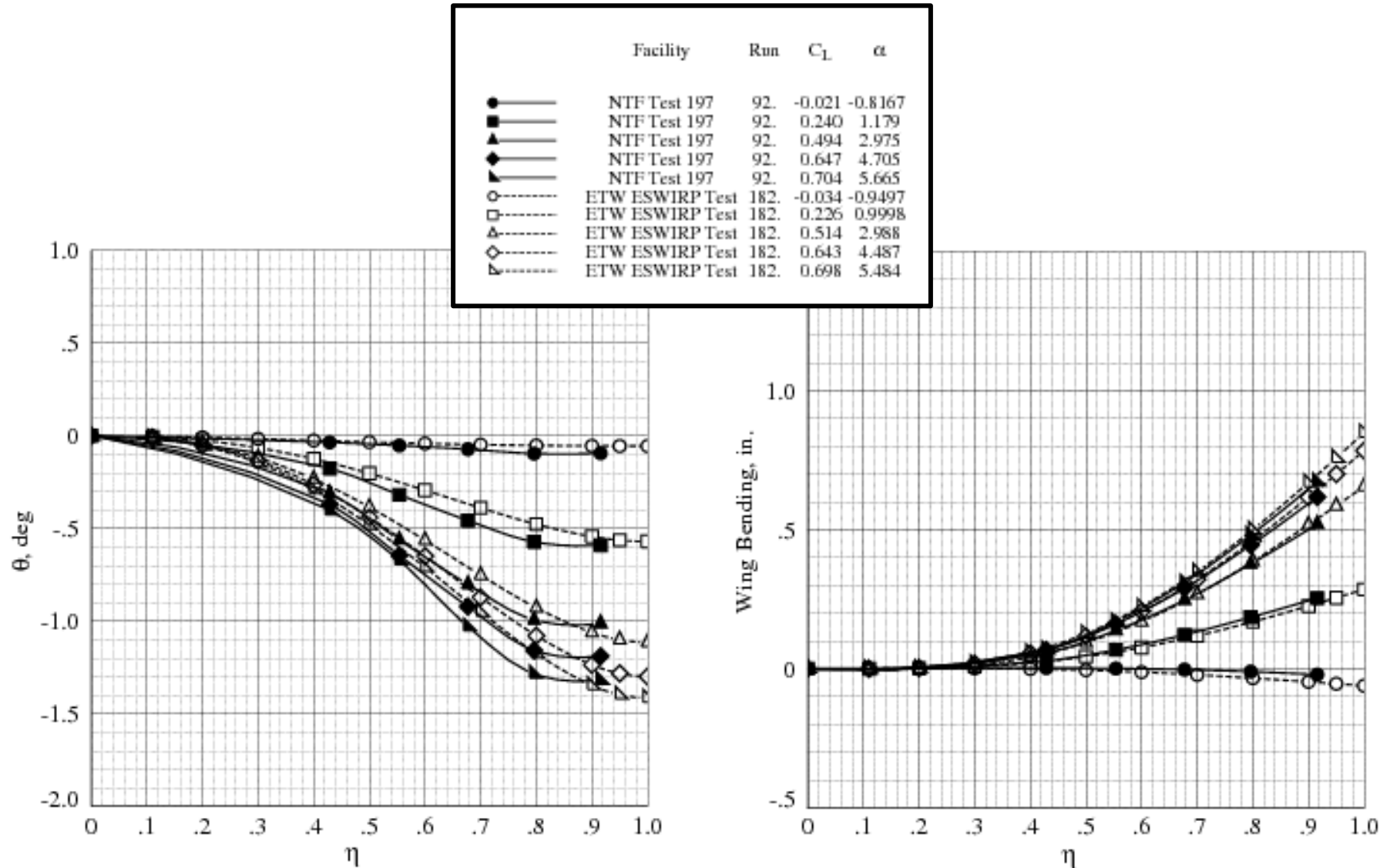
- **Grow Next-Finer Grid in Family by $\sim 1.5X$ in Size**

- Scale Dimensions in All Three Computational Directions by $\sim 1.15X$
- Grid Spacings Reduce by $0.87 = (1/1.15)$ per Mesh Level
 - 0.1% in Tiny $\rightarrow [T,C,M,F,X,U] = [0.100, 0.087, 0.076, 0.066, 0.057, 0.050]\%$

DPW-VI: Gridding Guidelines (2/2)

- **WB Grids Consistent with Those within WBNP Systems**
 - Helps Minimize Deltas due to Grid → Better NP-Deltas
- **WBNP Grid Sizes ~ 1.3X-1.5X WB Grid Sizes**
 - Pick Factor, Then Keep Constant Throughout Grid Family
- **Farfield Boundary > 100*Semispans**
 - Note: This is Farther than before, which was 100*Crefs
- **Miscellaneous Notes:**
 - Try to be Multigrid Friendly on Structured Meshes
 - Store Grid Coordinates in 64-bit Precision
 - If Storing Grids in Plot3D Format, Keep Zones < 33M Nodes
 - Itemize Surface Elements by Components [W, B, N, P, Sym, Far]
 - Itemize Element Count for Unstructured Meshes
 - Volume: Tetrahedra, Prisms, Pyramids, Hexahedra
 - Surface: Triangles, Quads

CRM Wing Deflections in NTF, ETW



DPW-6 Utilizes ETW Deflections

CRM WBNPT Geometry Definitions (IGES)

| Size | Date | Time | Name |
|----------|--------|-------|---|
| 25853452 | Jul 16 | 10:40 | DPW6_CRM_wbnpt_ih+0_v08_2015-07-01_ae2.50deg_cf.igs |
| 25824424 | Jul 16 | 10:58 | DPW6_CRM_wbnpt_ih+0_v08_2015-07-01_ae2.75deg_cf.igs |
| 26077968 | Jul 16 | 11:10 | DPW6_CRM_wbnpt_ih+0_v08_2015-07-01_ae3.00deg_cf.igs |
| 25973664 | Jul 16 | 11:24 | DPW6_CRM_wbnpt_ih+0_v08_2015-07-01_ae3.25deg_cf.igs |
| 26253366 | Jul 16 | 11:57 | DPW6_CRM_wbnpt_ih+0_v08_2015-07-01_ae3.50deg_cf.igs |
| 25789738 | Jul 16 | 12:07 | DPW6_CRM_wbnpt_ih+0_v08_2015-07-01_ae3.75deg_cf.igs |
| 25773912 | Jul 16 | 12:19 | DPW6_CRM_wbnpt_ih+0_v08_2015-07-01_ae4.00deg_cf.igs |
| 17608516 | Jul 16 | 10:42 | DPW6_CRM_wbnpt_ih+0_v08_2015-07-01_cf.igs |

Notes:

- * DPW6 Common Research Model Wing/Body/Nacelle/Pylon/Tail Configuration
- * Horizontal Tail rigged at $iH = 0$ degrees
- * Geometry Version v08 created on 16 July, 2015
- * Aero-Elastic Deflections of ETW at $M=0.85$, $Re=5$ million, $\alpha=As_In_Name$
- * Deflected IGES/STEP Files Courtesy of Mark Gammon (CADfix Developer)
- * Deflected Discrete Surface Triangulations Courtesy of Stefan Keye (DLR)
- * Although Included in IGES/STEP Files, DPW6 Test Cases Do Not Utilize Tail

FEM Modal Shapes & Frequencies

Mode 1



Mode 2



Mode 3

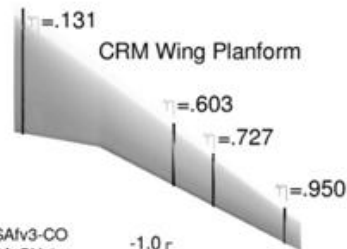


| Mode | Frequency (Hz) |
|------|----------------|
| 1 | 39.398 |
| 2 | 40.958 |
| 3 | 58.531 |
| 4 | 63.638 |
| 5 | 68.536 |
| 6 | 71.789 |
| 7 | 82.503 |
| 8 | 85.588 |
| 9 | 107.43 |
| 10 | 113.79 |
| 11 | 122.95 |
| 12 | 127.18 |
| 13 | 151.16 |
| 14 | 162.29 |
| 15 | 166.98 |
| 16 | 177.64 |
| 17 | 202.51 |
| 18 | 204.49 |
| 19 | 206.54 |
| 20 | 267.08 |

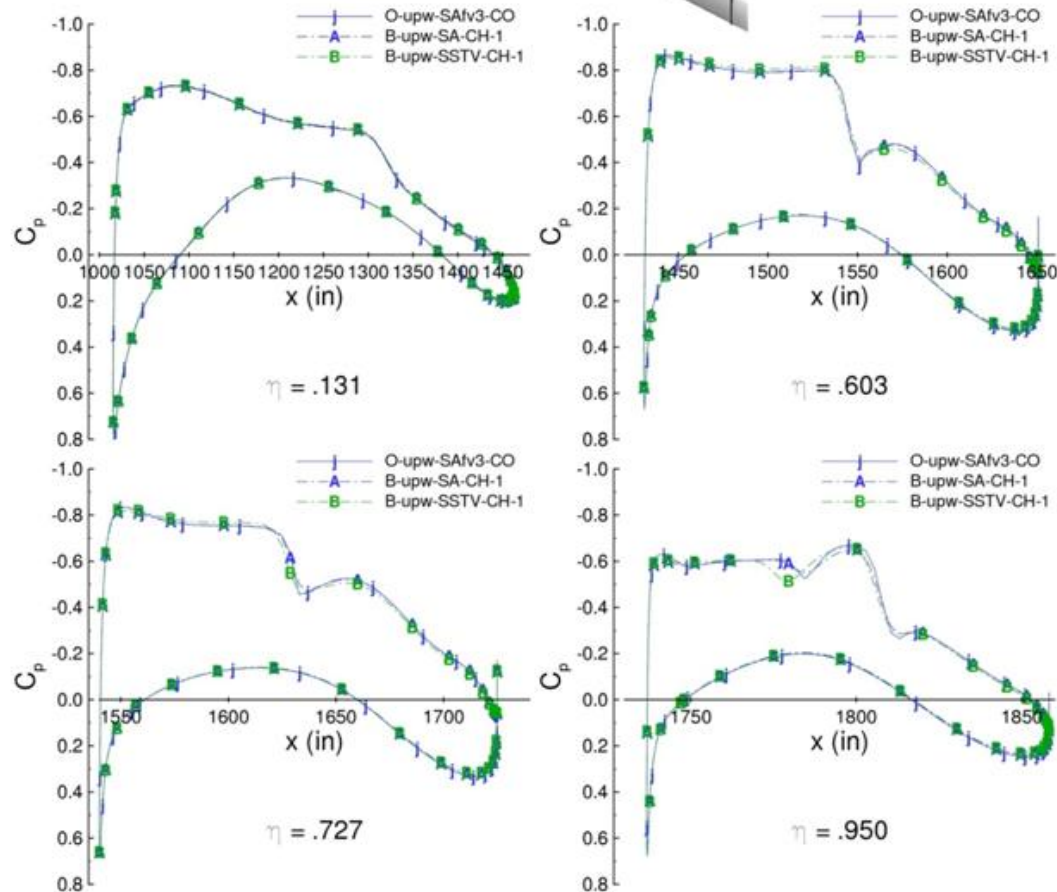
Sample CP Distributions from DPW-V

CRM Wing Cp Comparison

Test Case 1:
Solver Comparison (L3 Grid)



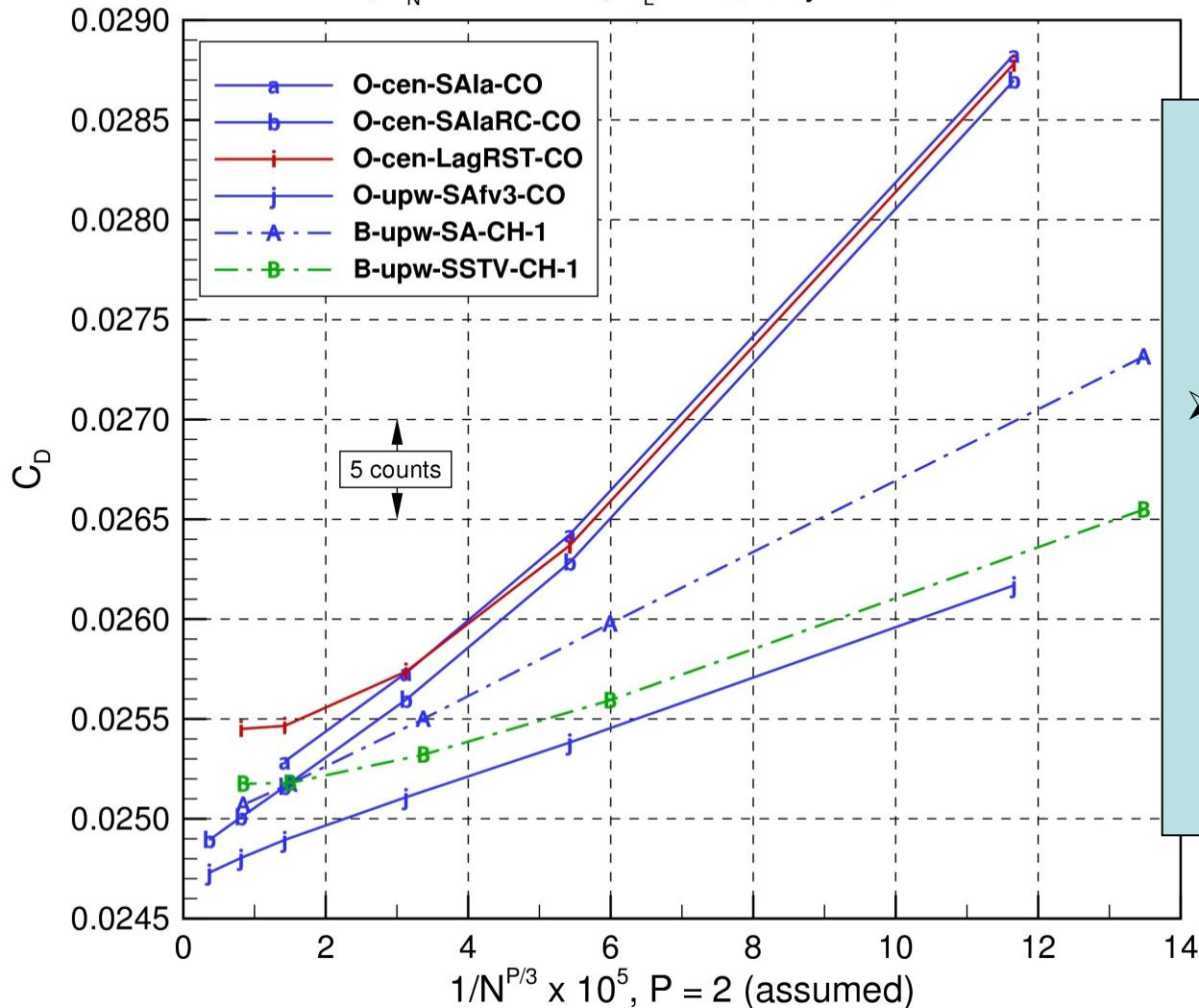
RN = 5.0 million
Mach = 0.85
 $C_L = 0.50$



Sample Grid Convergence from DPW-V

CRM Wing-Body Results: Total Drag

Mach = 0.85, $R_N = 5.0$ million, $C_L = 0.5$, Fully Turbulent



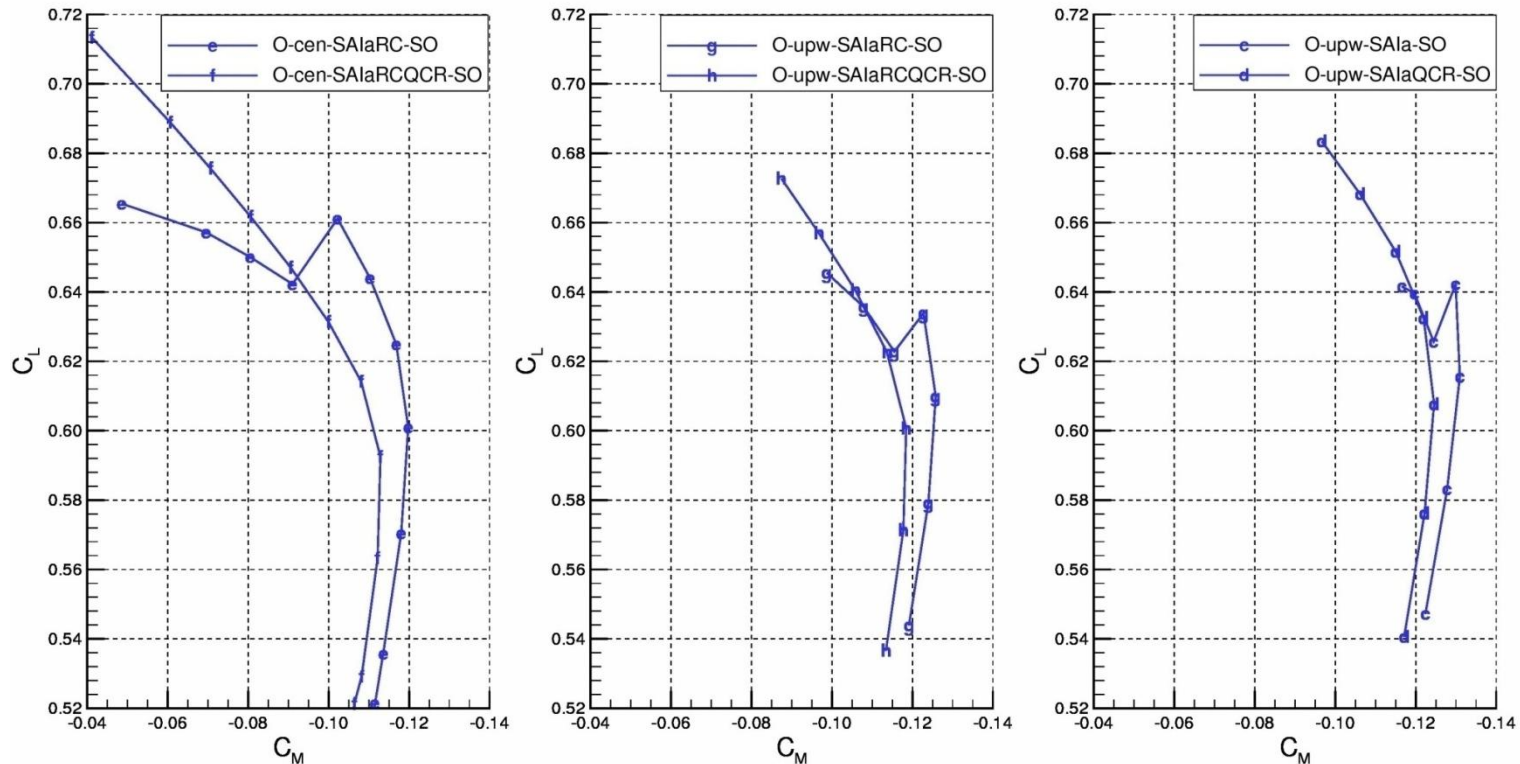
- All SA results trend in a consistent manner with grid refinement and have a relatively small spread in C_D at the finest grid level (~5 counts)
- Lag RST exhibits nonlinear trend for finer grid levels
- BCFD SST-V data also breaks from a linear trend for the two most dense grid levels
- Upwind data follows a lower slope trend line compared to central

QCR Effect on SOB Flow at Buffet On-Set

CRM Wing-Body Results: Pitching Moment Comparison

Mach = 0.85, $R_N = 5.0$ million, Fully Turbulent, Medium Grid

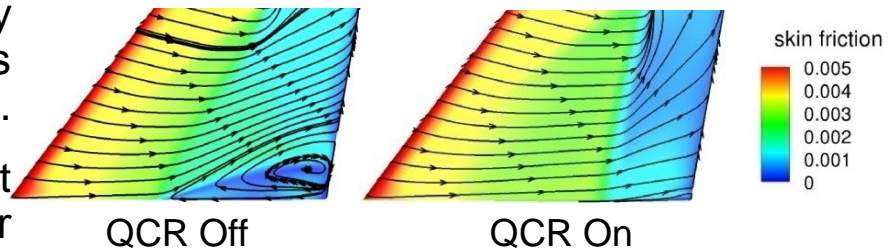
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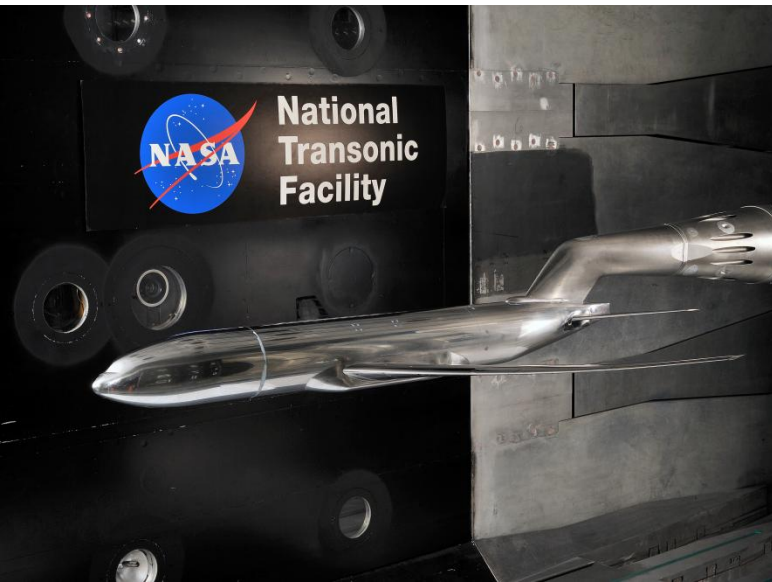
$\alpha = 4^\circ$

➤ When QCR is used, side-of-body separation does not form at the CRM's wing-body juncture.

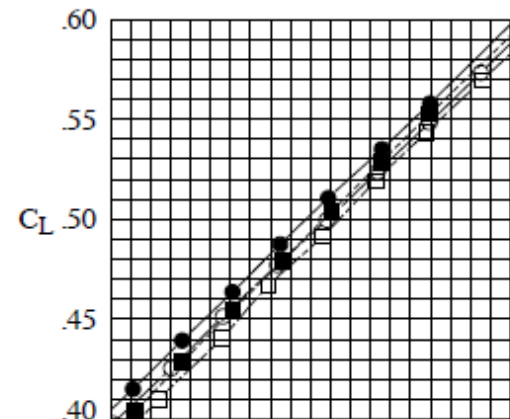
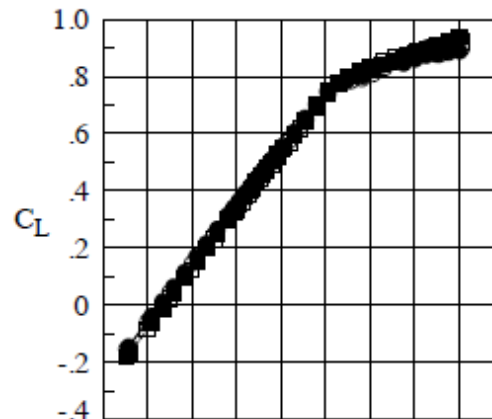
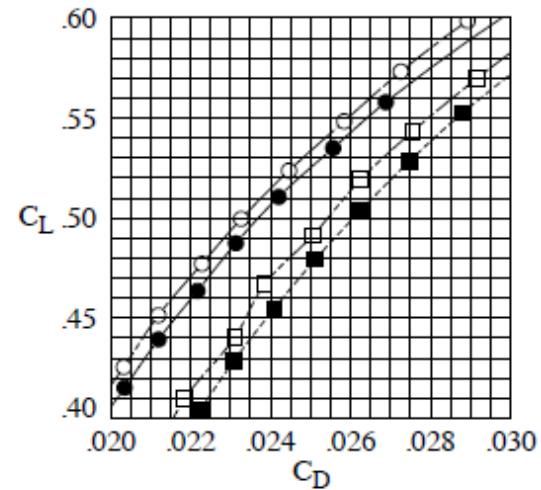
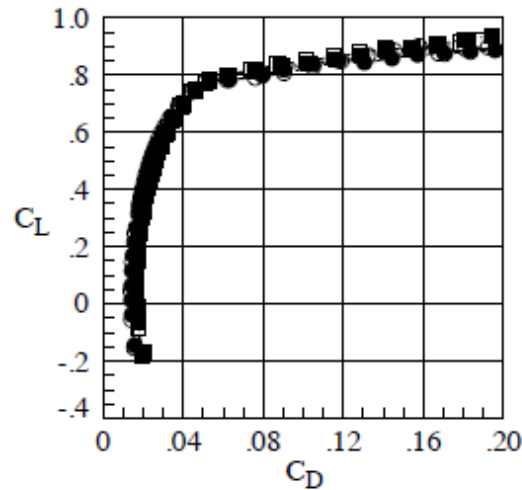
➤ The nose-up shift in pitching moment at lower C_L 's is caused by a more triangular spanload with QCR turned on.



Sample NTF & Ames 11' WT Data



| | Facility | Run | Config | M_∞ | $Re_c \cdot 10^6$ |
|---|------------|------|--------|------------|-------------------|
| ● | LaRC NTF | 39. | WB | 0.70 | 5.00 |
| ■ | LaRC NTF | 69. | WBPN | 0.70 | 4.99 |
| ○ | Ames 11-ft | 118. | WB | 0.70 | 5.00 |
| □ | Ames 11-ft | 107. | WBPN | 0.70 | 5.00 |



6th AIAA CFD Drag Prediction Workshop

Sponsored by the
Applied Aerodynamics TC

2-Day Workshop Preceding

AIAA AVIATION 2016
Washington, D.C. USA

June 11-12, 2016



For more information
and results from past workshops,
visit the DPW website at:

[http://aaac.larc.nasa.gov/tsab/cfdlarc/
aiaa-dpw/](http://aaac.larc.nasa.gov/tsab/cfdlarc/aiaa-dpw/)

or send email to:

aiaadpw@gmail.com

CFD Drag Prediction Workshop VI

*In addition to CFD practitioners, flow-
solver developers and grid-generation
experts...*

*The DPW Organizing Committee invites
members of the*

Solution-Adaptation & Aero-Elastic
communities to participate in DPW VI.

Focus

The focus of this workshop will be the NASA Common Research Model (CRM) with wind-tunnel measured wing twist; both wing-body and wing-body-pylon-nacelle configurations will be considered. CFD predictions of absolute and incremental force and moment values will be examined and compared. The workshop will include grid convergence and code verification studies. Additionally, an angle-of-attack sweep with static aero-elastic deformations will be considered. Grids will be made available for all required cases.

Optionally, participants are invited to perform solution-adaptation calculations and/or a coupled aero-structural simulation of the CRM wing-body configuration. A finite element model will be made available to participants to calculate twist/deflection due to aerodynamic load.

CFD Drag Prediction Workshop VI

Organizing Committee

John Vassberg, Ben Rider, Mori Mani
The Boeing Company

Olaf Brodersen, Stefan Keye
DLR

Martin Gariépy
École Polytechnique de Montréal

Mitsuhiro Murayama
JAXA

Joseph Morrison, Richard Wahls
NASA Langley Research Center

David Hue
ONERA

Edward Tinoco
Retired

Edward Feltrop, Kelly Laflin
Textron Aviation

Dimitri Mavriplis
University of Wyoming

Chris Roy
Virginia Tech

Dates

*Check the DPW website for additional
information and updates.*

| | |
|---------------------------------|-------------|
| Release Geometry | Jun 1, 2015 |
| Release Standard Grids | Aug 1, 2015 |
| Notice of Intent to Participate | Dec 1, 2015 |
| Abstract Deadline | Apr 1, 2016 |
| Data Submittal Deadline | May 1, 2016 |

**Workshop registration will be handled
through normal AIAA procedures.**

Workshop presentations will not be official AIAA papers; however, several participants will be invited to support a special session on drag prediction to be held during the AIAA SciTech Meeting, January 2017.

CFD Drag Prediction Workshop VI

Objectives

- To build on the success of past AIAA Drag Prediction Workshops.
- To assess the state-of-the-art computational methods as practical aerodynamic tools for aircraft force and moment prediction of industry relevant geometries.
- To provide an impartial forum for evaluating the effectiveness of existing computer codes and modeling techniques using Navier-Stokes solvers.
- To identify areas needing additional research and development.



NASA Common Research Model (CRM)

CFD Drag Prediction Workshop VI

General Information

- This workshop is open to participants worldwide. Efforts will be made to ensure representation from all areas of industry, academia and government laboratories.
- Participation in the drag studies is not required to attend the workshop. Everyone is welcome!
- Open forums will be included in the workshop to discuss the solutions and modeling techniques.
- Results will be made available after the workshop in a report and on the DPW website.
- A nominal registration fee will be required for attendance.
- AIAA membership is not required



CFD Drag Prediction Workshop VI

Test Cases

Check the DPW VI website for additional details and updates.

Required

Case 1: 2D Code Verification Study

Case 2: CRM Nacelle-Pylon Drag Increment / Grid Convergence Study (single condition on a family of grids)

Case 3: CRM Wing-Body Static Aero-Elastic Effect (7 solutions on 7 grids)

Optional

Case 4: CRM Wing-Body Solution Adaptation and/or a 2D Solution Adaptation Study

Case 5: CRM Wing-Body Coupled Aero-Structural Simulation (FEMA supplied)

Case 6: Participant Generated Grids

All participants are encouraged to build their own grids using 'best practice' techniques. IGES and STP models are available for grid construction. Grid size requirements can be found on the DPW VI website. All grids used for results presented at the workshop must be submitted to the DPW Organizing Committee to be made available to all interested parties. *Note: All results and grids will be published electronically on the DPW website:*

<http://aaac.larc.nasa.gov/tsab/cfdlarc/aiaa-dpw/>

Questions?

DPW-VI Workshop
11-12 June, 2016

Weekend Before AIAA
Applied Aerodynamics Conference

Washington, DC