# SUNAIR AWNINGS & SCREENS LEVEL PERGOLA UNITS

Engineering Report published revision 1/10/18

### **CALCULATIONS ENGINEERED BY**

# Sullaway Engineering



# Pergola Engineering Request

#### Determine what you need from Sunair

#### Options available:

- You may use the enclosed documents in conjunction with you existing or future efforts to obtain your permit.
- ➤ You may have the enclosed document stamped, with your state and project referenced, for a flat fee of \$340.00 which you will pay directly to Sullaway Engineering to the contact below. (price may change, contact Sullaway Eng. directly for costing)
- ➤ If you need a full site specific engineering package done for your project you will need to contact Sullaway Engineering and reference project ID #16017. They will then price your job and you will work directly with them.
  - Sullaway Engineering: Attn Pruthvi (Raji) Chauhan
     10815 Rancho Bernardo Rd, Ste 260 San Diego, CA
     92198 phone: 858-312-5150

These signed engineering calculations may be utilized by your engineer to certify your Sunair/Pratic Pergola Awning system project. In order to secure your permit this engineering report may also require alterations or recalculations by a local engineer in your state. Any such alterations and costs is the responsibility of the customer. Neither Sunair Awnings or Pratic will be liable for the use of these calculations to certify and secure permits for your project. Sunair or Pratic will not be liable for the performance of subject Pergola structures in the field using any calculations we provide. It is up to each customer to do site specific engineering calculations for each project signed by a local engineer licensed in the state in which the project resides. Sunair is not responsible for any lack of or unsuitability of structure to properly fasten the Pergola to the customer's existing structure, walls, decking, floors or footers. Sunair's current Pergola warranty and current "Sales Terms" also applies to all projects and these engineering calculations. The most recent revisions of engineered drawings apply.

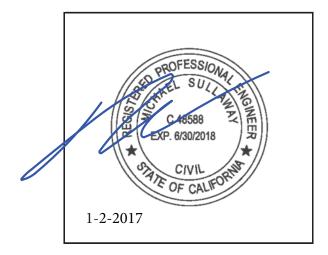


# STRUCTURAL CALCULATIONS for

# Pratic LEVEL Pergola Awning

PROJECT: 9263-2

DATE: 12/12/2017





www.sullawayeng.com



#### STRUCTURAL CALCULATIONS

for

# Pratic LEVEL Pergola Awning

This structural calculation package addresses the maximum allowable windspeeds for the Pratic LEVEL pergola awning distributed by Sunair Awnings and Solar Screens. The evaluation is solely base on the ASCE 7-10 Minimum Design Loads for Buildings and Other Structures as referenced in the 2012 International Building Code.

This report establishes the maximum allowable windspeeds derived from ultimate windspeeds under exposure C conditions for various dimensional configurations of the LEVEL model pergola awning based on the above mentioned references. The intent of this report is to allow an end-user, supplier, or designer to make an educated decision in selecting dimensions for planning purposes. All factors affecting wind speed and structural performance are site-specific and cannot be captured in a report of this nature as to completely assess structural adequacy.

As such, this report is not intended to substitute site specific engineering documentation. Such engineering services to check connections of members to each other, connections to existing structure, and anchorage to the ground is highly recommended. Additionally, certain topographical features may contribute to a higher wind pressure and lower the structural performance contained herein. Under no circumstance shall Sullaway Engineering, Sunair, or Pratic be held liable for the performance of any connections or any loading conditions not specified in this report.

- 1. The maximum allowable and ultimate wind speeds for various configurations are presented on pages 4 and 5.
- 2. Reaction outputs are available on pages 6 and 7 for use by a designer for site-specific anchorage.
- 3. Frames should be anchored to the ground to prevent uplift as listed on pages 6 and 7.
- 4. Unit is assumed to be a fully open structure for wind analysis.
- 5. Unit is analyzed with a ground snow load of 30 psf in the retracted position. Snow load was not applied to the expanded position.
- 6. Aluminum should be 6061-T6.

These signed engineering calculations may be utilized by your engineer to certify your Sunair/Pratic Pergola Awning system project. In order to secure your permit this engineering report may also require alterations or recalculations by a local engineer in your state. Any such alterations and costs is the responsibility of the customer. Neither Sunair Awnings or Pratic will be liable for the use of these calculations to certify and secure permits for your project. Sunair or Pratic will not be liable for the performance of subject Pergola structures in the field using any calculations we provide. It is up to each customer to do site specific engineering calculations for each project signed by a local engineer licensed in the state in which the project resides. Sunair is not responsible for any lack of or unsuitability of structure to properly fasten the Pergola to the customer's existing structure, walls, decking, floors or footers. Sunair's current Pergola warranty and current "Sales Terms" also applies to all projects and these engineering calculations.



## **TYPICAL INSTALLATIONS**













#### **SINGLE-BAY MAXIMUM ALLOWABLE WINDSPEEDS**

	FABRIC FULLY EXPANDED									
				Bay Le	ngth, I	-				
		8	10	12	14	16	16.5			
<u> </u>	8	139	139	139	139	139	139			
(ft)	10	139	139	139	139	136	132			
۵	12	139	139	132	120	112	112			
on,	14	139	128	116	105	97	97			
tic	16	124	112	101	93	85	81			
jec	18	112	97	89	81	74	74			
Projection,	20	101	85	77	70	66	62			
4	22	89	77	70	62	58	54			

	FABRIC FULLY RETRACTED									
			[	Bay Le	ngth, I	_				
		8	10	12	14	16	16.5			
<u> </u>	8	139	139	139	139	139	139			
(ft)	10	139	139	139	139	139	139			
۵	12	139	139	139	139	139	139			
Ju,	14	139	139	139	139	139	139			
l ij l	16	139	139	139	139	139	139			
jec	18	139	139	139	139	139	139			
Projection,	20	139	139	139	139	139	139			
4	22	139	139	139	139	139	139			

#### **SINGLE-BAY ASCE 7-10 ULTIMATE WINDSPEEDS**

	FABRIC FULLY EXPANDED								
			1	Bay Le	ngth, I	L			
		8	10	12	14	16	16.5		
$\widehat{}$	8	180	180	180	180	180	180		
(ft)	10	180	180	180	180	175	170		
۵	12	180	180	170	155	145	145		
Ju,	14	180	165	150	135	125	125		
ţį	16	160	145	130	120	110	105		
jec	18	145	125	115	105	95	95		
Projection,	20	130	110	100	90	85	80		
а.	22	115	100	90	80	75	70		

FABRIC FULLY RETRACTED								
			ı	Bay Le	ngth, I	L		
		8	10	12	14	16	16.5	
$\overline{}$	8	180	180	180	180	180	180	
(ft)	10	180	180	180	180	180	180	
۵	12	180	180	180	180	180	180	
n,	14	180	180	180	180	180	180	
ij	16	180	180	180	180	180	180	
jeć	18	180	180	180	180	180	180	
Projection,	20	180	180	180	180	180	180	
4	22	180	180	180	180	180	180	





#### **MULTI-BAY MAXIMUM ALLOWABLE WINDSPEEDS**

	FABRIC FULLY EXPANDED									
			[	Bay Le	ngth,	L				
		8	10	12	14	16	18			
<u> </u>	8	139	139	132	120	112	105			
(ft)	10	136	120	108	97	89	85			
Ъ	12	112	101	89	81	74	70			
Jn,	14	97	85	77	70	62	58			
ij	16	85	74	66	58	54	46			
je(	18	74	62	54	50	43	39			
Projection,	20	66	54	46	43	35	31			
4	22	58	46	39	35					

	FABRIC FULLY RETRACTED									
			E	Bay Le	ngth,	L				
		8	10	12	14	16	18			
$\overline{}$	8	139	139	139	139	139	139			
(ft)	10	139	139	139	139	139	139			
۵	12	139	139	139	139	139	139			
Jn,	14	139	139	139	139	139	139			
ij	16	139	139	139	139	139	139			
jeć	18	139	139	139	139	139	139			
Projection,	20	139	139	139	139	139	139			
4	22	139	139	139	139	139	139			

#### **MULTI-BAY ASCE 7-10 ULTIMATE WINDSPEEDS**

	FABRIC FULLY EXPANDED								
			E	Bay Le	ngth,	L			
		8	10	12	14	16	18		
<u> </u>	8	180	180	170	155	145	135		
(ft)	10	175	155	140	125	115	110		
۵	12	145	130	115	105	95	90		
Jn,	14	125	110	100	90	80	75		
ij	16	110	95	85	75	70	60		
jec	18	95	80	70	65	55	50		
Projection,	20	85	70	60	55	45	40		
4	22	75	60	50	45				

FABRIC FULLY RETRACTED								
			E	Bay Le	ngth, I	L		
		8	10	12	14	16	18	
$\overline{}$	8	180	180	180	180	180	180	
(ft)	10	180	180	180	180	180	180	
۵	12	180	180	180	180	180	180	
n,	14	180	180	180	180	180	180	
Ţ.	16	180	180	180	180	180	180	
Projection,	18	180	180	180	180	180	180	
ro Lo	20	180	180	180	180	180	180	
4	22	180	180	180	180	180	180	





### **SINGLE-BAY SERVICE REACTIONS**

	VERTICAL WALL LOAD PER GUIDE (lb)									
			Bay Length, L							
		8	10	12	14	16	16.5			
<u> </u>	8	556	695	834	973	1112	1147			
(£	10	624	624 780 935 1091 1189							
۵.	12	691	864	943	948	977	1007			
Ľ,	14	758	823	851	848	869	896			
Iĕ	16	684	736	755	790	807	786			
je	18	639	649	698	729	744	767			
Projection,	20	592	597	642	669	723	706			
Δ.	22	543	577	620	649	702	686			

Ь	22	543	577	620	649	702	686				
DOWNWARD FOOTING LOAD PER COL (Ib)											
	)	VANDI	Bay Length, L								
		8	10	12	14	16	16.5				
· ·	8	509	636	763	890	1017	1049				
(ft)	10	571	714	856	999	1090	1072				
۵	12	679	849	927	933	961	992				
Jn,	14	787	853	881	877	897	925				
ojection,	16	739	793	810	844	859	835				
jec	18	711	716	766	795	806	831				
0	20	671	660	712	726	701	760				

651 693 715 769 747

	ORTHO. WALL LOAD PER GUIDE (lb)										
				Bay Le	ngth,	L					
		8	10	12	14	16	16.5				
<u> </u>	8	221	270	319	368	418	430				
(ft)	10	207	207 253 299 345 371 363								
۵	12	202	247	263	258	260	268				
'n.	14	198	207	207	200	200	205				
ij	16	159	163	160	163	161	154				
Projection,	129	132									
2	20	109	102	105	104	110	105				
Ъ	22	89	88	90	89	93	89				

	UPLIFT FOOTING LOAD PER COL (lb)									
Bay Length, L										
		8	10	12	14	16	16.5			
$\overline{}$	8	71	89	107	125	143	147			
(ft)	10	89	111	133	155	157	142			
۵	12	106	133	124	86	58	60			
Jn,	14	124	104	68	20	0	0			
Ţ	16	80	48	2	0	0	0			
12 106 133 124 86 58 14 124 104 68 20 0 16 80 48 2 0 0 18 43 0 0 0 0 20 1 0 0 0 0										
o'	20	1	0	0	0	0	0			
4	22	0	0	0	0	0	0			

## **SINGLE-BAY FACTORED REACTIONS**

	VERTICAL WALL LOAD PER GUIDE (lb)										
			E	Bay Le	ngth, I	L					
		8	10	12	14	16	16.5				
· ·	8	1126	1407	1689	1970	2252	2322				
(ft)	10	1249	1561	1873	2185	2369	2314				
۵	12	1371	1714	1849	1820	1842	1900				
Jn,	14	1493	1589	1603	1549	1548	1596				
;tic	16	1301	1362	1349	1372	1355	1295				
<u>8</u> 18 1174 1134 1182 1188 1160											
Projection,	20	1041	1014	1008	1059	1002					
Т	22	905	905	926	913	957	903				

	DOWNWARD FOOTING LOAD PER COL (lb)										
			E	Bay Le	ngth, I	L					
		8	10	12	14	16	16.5				
<u> </u>	8	1020	1275	1529	1784	2039	2103				
(ft)	10	1131	1414	1697	1979	2146	2097				
۵	12	1344	1680	1812	1784	1806	1863				
Jn,	14	1556	1656	1669	1612	1609	1659				
Ţ.	16	1423	1487	1470	1492	1470	1403				
Projection,	18	1333	1281	1332	1335	1297	1337				
o.	20	1216	1141	1170	1155	1210	1140				
4	22	1080	1070	1087	1062	1106	1037				

	ORTHO. WALL LOAD PER GUIDE (lb)										
Bay Length, L											
		8	10	12	14	16	16.5				
· ·	8	355	438	521	604	687	708				
(ft)	10	326	401	476	552	595	580				
۵	12	314	387	412	401	402	415				
Jn,	14	306	319	317	302	299	308				
Ţ	16	240	246	239	239	233	222				
<u>18</u> 196 184 189 186 179											
Projection,	20	159	145	146	142	147	138				
д	22	126	122	122	117	120	112				

	UPLIFT FOOTING LOAD PER GUIDE (lb)									
	Bay Length, L									
		8	10	12	14	16	16.5			
<del></del>	8	0	0	0	0	0	0			
Projection, P (ft)	10	0	0	0	0	0	0			
۵	12	0	0	0	0	0	0			
n,	14	0	0	0	0	0	0			
ij	16	0	0	0	0	0	0			
18 0 0 0 0 0										
<u>20</u> 0 0 0 0 0										
4	22	0	0	0	0	0	0			



## **MULTI-BAY SERVICE REACTIONS**

	VERTICAL WALL LOAD PER GUIDE (lb)									
Bay Length, L										
		8	10	12	14	16	18			
<u> </u>	8	1112	1390	1512	1512	1550	1557			
(ft)	10	1189	1218	1244	1225	1243	1316			
۵	12	977	1038	1049	1086	1099	1162			
Jn,	14	869	916	978	1013	1026	1087			
ξį	16	807	849	907	941	1016	1021			
jec	18	744	784	841	928	954	1020			
Projection,	20	723	766	827	917	953	1026			
Д	22	702	750	816	910					

	DOWNWARD FOOTING LOAD PER COL (lb)									
			E	Bay Le	ngth,	L				
		8	10	12	14	16	18			
$\widehat{}$	8	1017	1271	1386	1389	1428	1438			
(ft)	10	1090	1120	1149	1137	1158	1229			
۵	12	961	1022	1034	1073	1087	1150			
Jn,	14	897	944	1005	1039	1050	1111			
ti	16	859	898	954	984	1059	1057			
18 806 839 891 979 996										
Projection,	20	791	824	878	967	991	1061			
Δ.	22	769	804	862	953					

	ORTHO. WALL LOAD PER GUIDE (lb)									
	Bay Length, L									
		8	10	12	14	16	18			
$\overline{}$	8	353	436	468	462	470	468			
(ft)	10	311	311	312	301	302	317			
۵	12	219	226	222	226	224	234			
Ju,	14	169	172	179	180	178	186			
ij	16	137	138	143	144	153	148			
<u>8</u> 18 111 111 114 124 122 1										
14 169 172 179 180 178 16 137 138 143 144 153 18 111 111 114 124 122 20 95 95 99 107 107										
Ъ	22	82	82	86	93					

	UPLIFT FOOTING LOAD PER COL (Ib)										
Bay Length, L											
		8	10	12	14	16	18				
$\overline{}$	8	143	178	166	116	77	30				
(ft)	10	157	103	48	0	0	0				
۵	12	58	2	0	0	0	0				
Jn,	14	0	0	0	0	0	0				
ξi	16	0	0	0	0	0	0				
<u>u</u> 18 0 0 0 0 0											
C 14 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0											
۵	22	0	0	0	0						

### **MULTI-BAY FACTORED REACTIONS**

	VERTICAL WALL LOAD PER GUIDE (lb)									
			6	Bay Le	ngth, I	L				
		8	10	12	14	16	18			
$\overline{}$	8	2252	2815	3032	2975	3005	2966			
(ft)	10	2369	2363	2354	2242	2214	2307			
۵,	12	1842	1894	1837	1838	1784	1842			
n,	14	1548	1557	1598	1579	1512	1552			
Ţ	16	1355	1338	1357	1324	1379	1281			
je(	18	1160	1127	1198	1132	1156				
Projection,	20	1059	1017	1014	1077	1020	1046			
Ъ	22	957	912	909	968					

	DOWNWARD FOOTING LOAD PER COL (lb)									
			Bay Le	ngth,	L					
		8	10	12	14	16	18			
<u> </u>	8	2039	2549	2748	2700	2730	2698			
(ft)	10	2146	2145	2141	2044	2023	2111			
۵	12	1806	1859	1804	1806	1754	1812			
n,	14	1609	1616	1657	1635	1563	1602			
l iž	16	1470	1446	1460	1418	1473	1359			
<u>je</u>	18	1297	1247	1239	1311	1224	1242			
Projection,	20	1210	1145	1127	1188	1105	1122			
а	22	1106	1031	1009	1062					

	ORTHO. WALL LOAD PER GUIDE (lb)									
	Bay Length, L									
		8	10	12	14	16	18			
· ·	8	623	772	827	808	813	800			
(ft)	10	534	527	521	493	485	504			
۵	12	361	367	352	350	337	346			
Jn,	14	268	265	269	263	250	254			
Projection,	16	209	203	203	195	201	184			
<u>8</u> 18 161 152 150 157 145										
<b>2</b> 20 133 124 120 126 116										
п.	22	109	100	96	101					

	UPLIFT FOOTING LOAD PER GUIDE (lb)									
	Bay Length, L									
		8	10	12	14	16	18			
<del></del>	8	0	0	0	0	0	0			
Œ)	10	0	0	0	0	0	0			
۵	12	0	0	0	0	0	0			
n,	14	0	0	0	0	0	0			
ij	16	0	0	0	0	0	0			
jeć	<b>u</b> 18 0 0 0 0 0 0									
DE COLUMN TO THE										
4	22	0	0	0	0					



www.sullawayeng.com



#### MEMBER PROFILE INFORMATION

LEVEL GUIDE							
У	120 mm	=	4.724 in	c <sub>x</sub> 2.362 in	А	918 mm <sup>2</sup>	$= 1.423 \text{ in}^2$
X	60 mm	=	2.362 in	c <sub>v</sub> 1.181 in			
I <sub>x</sub>	1437578 mm <sup>4</sup>	=	3.454 in <sup>4</sup>	$S_{x}^{'}$ 1.462 in <sup>3</sup>			r <sub>x</sub> 1.558 in
I <sub>y</sub>	513037 mm <sup>4</sup>	=	1.233 in <sup>4</sup>	$S_v = 1.044 \text{ in}^3$			r <sub>v</sub> 0.931 in
j	2010615 mm <sup>4</sup>	=	4.831 in <sup>4</sup>	,			,
LEVEL POST							
У	120 mm	=	4.724 in	c <sub>x</sub> 2.362 in	А	695 mm <sup>2</sup>	$= 1.077 \text{ in}^2$
X	60 mm	=	2.362 in	c <sub>v</sub> 1.181 in			
l <sub>x</sub>	1469344 mm <sup>4</sup>	=	3.53 in <sup>4</sup>	$S_x = 1.494 \text{ in}^3$			r <sub>x</sub> 1.81 in
I <sub>y</sub>	398278 mm <sup>4</sup>	=	0.957 in <sup>4</sup>	$S_v = 0.81 \text{ in}^3$			r <sub>v</sub> 0.942 in
j	1867621 mm <sup>4</sup>	=	4.487 in <sup>4</sup>	,			,
LEVEL GUTTER							
У	120 mm	=	4.724 in	c <sub>x</sub> 2.362 in	А	695 mm <sup>2</sup>	$= 1.077 \text{ in}^2$
X	125 mm	=	4.921 in	c <sub>v</sub> 2.461 in			
I <sub>x</sub>	2418321 mm <sup>4</sup>	=	5.81 in <sup>4</sup>	$S_{x}^{'}$ 2.46 in <sup>3</sup>			<sub>r<sub>x</sub></sub> 2.322 in
I <sub>v</sub>	746840 mm <sup>4</sup>	=	1.794 in <sup>4</sup>	$S_{v} = 0.729 \text{ in}^{3}$			r <sub>v</sub> 1.291 in
j	3165161 mm <sup>4</sup>	=	7.604 in <sup>4</sup>	,			•

#### 6061-T6 ALUMINUM PROPERTIES AND CONSTANTS

F <sub>tu</sub> 42 ksi	E	10100 ksi		
F <sub>ty</sub> 35 ksi	G	3787.5 ksi		
F <sub>cv</sub> 35 ksi				
F <sub>su</sub> 24 ksi				
UCKLING CONSTANTS			REDUCTIO	ON FACTORS
B <sub>c</sub> 39.37	k <sub>1</sub> 0	.35	φ,	0.9
D <sub>c</sub> 0.246	k <sub>2</sub> 2	.27	фь	0.9
C <sub>c</sub> 65.67	k <sub>t</sub>	1		
C <sub>b</sub> 1				

#### LOAD VALUES AND REFERENCES

$K_d$	0.85 Table 26.6-1	Roof Live Load	5 psf			$C_{NW}$	$C_{NL}$
$K_z$	0.85 Table 27.3-1	Dead Load	1 psf	0	Α	1.2	0.3
$K_{zt}$	1 26.8.2	Ground Snow Load	30 psf	U	В	-1.1	-0.1
G	0.85				Α	0.9	1.5
				7.5	В	1.6	0.3

WIDTHS (FT):	8	10	12	14	16	16.5	18	
PROJECTIONS (FT):	8	10	12	14	16	18	20	22
EAVE HEIGHT (FT):		8						
ROOF HEIGHT DELTA (FT):		1						
MEAN ROOF HEIGHT (FT):		8.5						

Phone: 858-312-5150 Fax: 858-777-3534

SULLAWAY ENGINEERING

www.sullawayeng.com

#### SAMPLE CALCULATION ALGORITHM FOR FABRIC FULLY EXPANDED

3/11VII EE	CALCOL	7111011	ALGORITTI		I OLLI L	1171110								
	ı	16	٦,,		CLIIDE D	ENIDINI	G STRENGTH			DOST ST	DONC B	BENDING	DOST	WEAK BENDING
	P	20	ft ft			1.462					68.73			S 75.07 -
	V	45	mph		SX	1.402	ın .			S1				1 123.2 -
M	ulti-Bay	Yes	- IIIPII							S2	1685			2 1685 -
1011	l'	32	ft		ΔMn	69.08	R k₋in			φF <sub>h</sub>	31.5		ф	
	٠.	32	<b>J</b> ''		ψινιτι	05.00	) K III			ΨЪ	51.5	KJI	Ψι	b 31.3 K31
	θ	2.862	deg		GUIDE C	OMP S	TRENGTH			POST CC	OMP STE	RENGTH	GUTTI	ER WEAK BENDING
	1	20.02	_		λ	4.838	3			λ	1.909			S 75.81 -
	h	8			D*.	13.12	)			D*.	13.12		S	1 123.2 -
	q	3.745	psf		S* <sub>1</sub>	0.333	3			S* <sub>1</sub>	0.333		S	2 1685 -
					S* <sub>2</sub>	1.231	L			S*2	1.231		фГ	<sub>b</sub> 31.5 ksi
					Фсс	0.95				$\Phi_{cc}$	0.847			
					$\varphi F_c$	1.421	L ksi			$\varphi F_c$	8.14	ksi		
	STRON	G AXIS \	WIND		T WEAK	AXIS V	VIND			GUT	TER			
$C_p$	0.8			$C_p$	0.8				$C_p$	0.8				
р	2.547			р	2.547					2.547				
=	0.501			=	1.003				=	1.003				
R <sub>1</sub>	1.504		(top)	$R_1$	3.008		(top)		$R_1$	8.022				
R <sub>2</sub>	2.507		(btm)	R <sub>2</sub>	5.014		(btm)		R <sub>2</sub>	8.022				
$M_{max}$	4.011 0.048		(btm)	M <sub>max</sub>	8.022 0.096		(btm)		M <sub>max</sub>	32.09 0.385				
	0.032				0.119					0.528				
f <sub>b</sub> D/C	0.032			f <sub>b</sub>	0.004				f <sub>b</sub>	0.017				
D/C	0.001	OK		D/C	0.004	OK			D/C	0.017	OIL			
	18	0° CAS	ΕA	18	0° CASE	В		90°	CASE A 8	& B		COLUMN	COMPRESSION	I
(btm)		1.086			-0.07			$C_{N,A}$	-0.8	-		$P_{u}$	1103 lb	
(top)	C <sub>NL, A</sub>	0.758	-		0.053			C <sub>N, B</sub>	0.8	-		=	1.10 kip	
(btm)	$p_{\text{NW, A}}$				-0.221				-2.547			$f_c$	1.02 ksi	_
(top)	P <sub>NL, A</sub>	2.413	psf	P <sub>NL, B</sub>	0.168	psf		P <sub>B</sub>	2.547	psf		D/C	0.13 <b>O</b> K	
(btm)	p <sub>NW, A</sub>	7.156	psf	p <sub>NW, B</sub>	3.479	psf		$p_A$	1.153	psf		FOOTING	REACTION (FA	CTORED)
(top)	p <sub>NL, A</sub>	6.113	psf	p <sub>NL, B</sub>	3.868	psf		$p_{\text{B}}$	6.247	psf		$P_{y}$	1.105 kip	Compression
												Гу	0.0 kip	Uplift
(btm)	$w_1$	114.5	lb/ft	$w_1$	55.66	lb/ft		W	99.95	lb/ft				
(top)	$W_2$	97.81		$W_2$	61.88							WALL REA	ACTION (FACTO	RED)
(btm)	$R_1$	1105		$R_1$	572.9			$R_1$	1001			$R_y$	1020 lb	
(top)	$R_2$	1021		$R_2$	604			$R_2$	1001			$R_x$	116 lb	
	M <sub>max</sub>		lb-ft kip-in	M <sub>max</sub>	2948		N	Λ <sub>max</sub>	5010					
	=	05.54	KIP-III	=	35.37	KIP-III		=	60.12	кір-ііі				
	D/C	0.926	OK	D/C	0.512	OK		D/C	0.87	OK				
CED: "C=	10455		OTINIC 25:	DING CALCUIT	TIONS									
				RING CALCULA					2.6			FOOTING	DEACTION (SE	DV/ICE)
(btm)	p <sub>NW, A</sub>		psf	P <sub>NW, B</sub>	4.7 4.83			p <sub>A</sub>	3.6 5.90			FUUTING	REACTION (SEI 0.991 kip	KVICE) Compression
(top)	p <sub>NL, A</sub>	3.84	psf	p <sub>NL, B</sub>	4.83	h21		P <sub>B</sub>	3.90	hai		$P_{y}$	0.991 kip	Uplift
(btm)	$W_1$	101	lb/ft	$w_1$	74	lb/ft		$W_1$	58	lb/ft				
(top)	W <sub>2</sub>	93	lb/ft	W <sub>2</sub>	77	lb/ft		W <sub>2</sub>	94	lb/ft		WALL REA	ACTION (SERVIC	CE)
(btm)	$R_1$	991		$R_1$	752			$R_1$	669			$R_y$	953 lb	
(top)	$R_2$	954	· lb	$R_2$	766	lb		$R_2$	853	lb		$R_x$	107 lb	





#### SAMPLE CALCULATION ALGORITHM FOR FABRIC FULLY RETRACTED

Н	ood (H)	30 in	= 2.5	ft						
	pg	30 psf	Ground Sno	ow Lo	ad					
	$C_{e}$	1	Exposure F	actor	(Table 7-2)					
	$C_{t}$	1.2	Thermal Fa	ctor (	Table 7-3)					
	$I_s$	1	Importance	e Facto	or (Table 1.5-1)					
	$p_f$	25.2 psf	Flat Roof Si	now L	oad					
	θ	2.862 deg	Roof Section	n Slop	oe					
	Cs	1			ure 7-2 per 7.4.3)					
	ps	25.2 psf	Sloped Roo	of Snov	w Load					
	18	0° CASE A		18	0° CASE B	90°	CASE A & B	COLUMN	N COMPRESSION	ON
	p <sub>NL, A</sub>	2.413 psf	I	p <sub>NL, A</sub>	0.168 psf	$p_{\text{NL, A}}$	2.547 psf	P <sub>u</sub> =	106.7 lb 0.107 kip	
LC#	3 w/ Lr	10.41 psf	LC #3 \	w/ Lr	9.284 psf	LC #3 w/ Lr	10.47 psf	f	0.099 ksi	
LC:	#3 w/ S	42.73 psf	LC #3	w/S	41.6 psf	LC #3 w/ S	42.79 psf	D/C	0.012 <b>OK</b>	
LC#	4 w/ Lr	6.113 psf	LC #4 \	w/ Lr	3.868 psf	LC #4 w/ Lr	6.247 psf			
LC:	#4 w/ S	16.21 psf	LC #4	w/S	13.97 psf	LC #4 w/ S	16.35 psf	FOOTING	G REACTION (	FACTORED)
								D	107 lb	Compression
	MAX	42.73 psf	MA	XΑ	41.6 psf	MAX	42.79 psf	$P_{y}$	0 lb	Uplift
		683.6 lb/ft			665.7 lb/ft		684.7 lb/ft	WALL BE	EACTION (FAC	TORED)
(top)	W <sub>H</sub>	1602 lb		W <sub>H</sub>	1560 lb	W <sub>H</sub>	1605 lb		1605 lb	TOKEDJ
(btm)	R <sub>1</sub>	106.7 lb		R <sub>1</sub>	103.9 lb	R <sub>1</sub>	106.9 lb	$R_y$ $R_x$	95.0 lb	
(DUIII)	R <sub>2</sub>	1878 lb-ft	,	R <sub>2</sub>	1829 lb-ft	R <sub>2</sub>	1881 lb-ft	N <sub>X</sub>	93.0 lb	
	M <sub>max</sub>	22.54 kip-ir		M <sub>max</sub>	21.94 kip-in	M <sub>max</sub>	22.57 kip-ir	1		
		22.5 1 Kip II	•		21.0 1 Mp III		22.57 KIP II	•		
	D/C	0.326 <b>O</b> K		D/C	0.318 <b>OK</b>	D/C	0.327 <b>OK</b>			