

National Hydrology Research Institute

NHRI PÄPERINO. 24

Operational Estimates of Areal Evapotranspiration and Lake Evaporation — Program WREVAP

,F. H. Morton, F. Ricard and S. Fogarasi

MHRI

NATIONAL HYDROLOGY RESEARCH INSTITUTE INLAND WATERS DIRECTORATE OTTAWA, CANADA, 1985

Contents

	raye
ABSTRACT	v
RÉSUMÉ	٧
1. INTRODUCTION	1
2. CONCEPTUAL BASIS	2
3. LIMITATIONS	4
4. OPTIONS	5 5 6
5. PROGRAM LANGUAGE	6
6. DATA PREPARATION 6.1 Record A of File Tape 1 6.2 Record B of File Tape 1 6.3 Record C of File Tape 1 6.4 Record D of File Tape 1 6.5 Record E of File Tape 1 6.6 Record F of File Tape 2 6.7 Record G of File Tape 3 6.8 Useable daily estimates	6 6 6 7 8 8 8 8
7. PROGRAM OPERATION	10
8. PROGRAM OUTPUT	10 10 13
9. CONCLUSIONS	15
10. ACKNOWLEDGMENTS	15
11. REFERENCES	15
APPENDIX I. Description of files	17
APPENDIX II. Listing of Program WREVAP	21
APPENDIX III. Listing of diagnostic errors	43
APPENDIX IV. Output samples	47
APPENDIX V. List of variable names used in the Program WREVAP	6
APPENDIX VI. Licting of Vapour Pressure Correction Program VPCOR	7

Table

	Page
Frequencies of monthly differences between REVAP and WREVAP estimates of areal evapotranspiration values for five years at 185 stations in Canada and the southern United States	2
Illustrations	
Figure 1. Schematic representation of the complementary relationship.	3
Figure 2. Schematic representation of the relationship between E_W and E_{WP}	4
Figure 3. Flowchart of Program WREVAP	11

Abstract

Program WREVAP has evolved from the previously documented Programs REVAP and WEVAP by providing greater flexibility in the input and time period options and by including a technique for taking into account the effects of subsurface heat storage changes on lake evaporation. It includes the CRAE (complementary relationship areal evapotranspiration), CRWE (complementary relationship wet-surface evaporation) and CRLE (complementary relationship lake evaporation) options. The workings of the complementary relationship, the input requirements and the possible options are explained. The program can be run for time periods ranging from one day to a month. Finally, output samples for various options and diverse climatic regions are presented and discussed in some detail.

Résumé

Le programme WREVAP découle des programmes vérifiés REVAP et WEVAP. Ce nouveau programme WREVAP est plus souple pour les paramètres et les options temporelles. Il tient compte des effets, sur l'évaporation lacustre, des variations du stockage de la chaleur sous la surface. Il englobe les options suivantes : évaporation surfacique (CRAE), évaporation à la surface mouillée (CRWE) et évaporation lacustre (CRLE), toutes complémentaires. Les mécanismes de la complémentarité, les paramètres à utiliser et les options possibles sont tous expliqués. Le programme peut être exécuté pour des périodes allant d'une journée à un mois. Enfin, quelques exemples des résultats obtenus pour diverses options et diverses régions climatiques sont présentés et analysés avec suffisamment de détails.

Operational Estimates of Areal Evapotranspiration and Lake Evaporation — Program WREVAP

F.I. Morton, F. Ricard and S. Fogarasi

1. INTRODUCTION

Program WREVAP is the latest in a series of computer models for estimating actual evaporation and transpiration from routinely published records of temperature, humidity and sunshine duration. Like the previous models, Program WREVAP is founded on the concept of a complementary relationship between areal and potential evapotranspiration. The concept takes into account interactions between the evaporating surfaces and the overpassing air, whereby a decrease in the availability of water for areal evapotranspiration causes the overpassing air to become hotter and drier, which in turn causes the potential evapotranspiration to increase. It provides the basis for what is referred to as a CRAE (complementary relationship areal evapotranspiration) model, which permits areal evapotranspiration to be estimated from its effects on the routinely observed temperatures and humidities used in computing potential evapotranspiration, thereby avoiding the complexities of the soil-plant system and the need for locally calibrated coefficients. 1 This means that the results are independent and falsifiable, so that errors in the associated assumptions can be detected and corrected by progressive testing against long-term water-balance estimates of river basin evapotranspiration from an ever-widening range of environments. During the past decade the test range has been expanded from Canada and Ireland to the United States, Australia, New Zealand, Brazil and a number of countries in Africa. The conceptual and empirical foundations of the complementary relationship, its use in providing the basis for operational estimates of areal evapotranspiration, the testing of such estimates against 143 comparable waterbudget values and the potential use of such estimates in transforming hydrology from a descriptive and a predictive science are discussed in detail elsewhere (Morton, 1983a).

The complementary relationship can also take into account the modification of the air as it passes from the land environment to the environment of a shallow lake. Thus a few minor changes (Morton, 1983a,b) convert the CRAE model to a CRWE (complementary relationship wet-

surface evaporation) model which can provide estimates of lake-size wet surface evaporation from routine climatological observations in the land environment with no locally calibrated coefficients. Although the lake-size wet surface evaporation corresponds to the evaporation from a lake so shallow that seasonal subsurface heat storage changes are negligible, monthly values can be accumulated to provide reliable estimates of annual evaporation from lakes with depths of up to 30 m. This capability has been demonstrated by the good agreement between the annual totals of monthly CRWE model estimates and the comparable water budget estimates for ten lakes in North America and Africa, including two that had average depths exceeding the 30-m limit by more than 100% (Morton, 1983b).

Good monthly estimates of evaporation for lakes of significant depth must take into account seasonal changes in subsurface heat storage by means of vertical temperature profiles. Since this is operationally impracticable, the subsurface heat storage changes have been taken into account in an approximate way (Morton, 1983b) by routing model estimates of lake-size wet surface evaporation through hypothetical heat reservoirs with delay times and storage constants related to the depth and salinity of the lake, using a routing technique similar to those used in routing water through natural reservoirs in hydrology. Although this procedure provided reasonable agreement with water budget estimates for the ten lakes referred to in the preceding paragraph, it proved to be conceptually inadequate when applied to a lake 150 m deep. This is because the routing technique required that the annual lake evaporation be equal to the annual lake-size wet surface evaporation and thus failed to recognize that heat is absorbed into storage during seasons when evaporation consumes a high proportion of the available energy and is released from storage during seasons when evaporation consumes a low proportion of the available energy. The newest version of the CRLE (complementary relationship lake evaporation) models solves this problem by routing the absorbed global radiation (rather than the lake-size wet surface evaporation) through the hypothetical heat reservoir. A paper submitted for publication (Morton, in press) presents the formulation of this most recent CRLE model and a comparison of its

¹Program VPCOR is needed to process one of the humidity input options for Program WREVAP.

results with the corresponding CRWE model estimates and the corresponding water budget estimates for 17 lakes in North America and Africa.

The main purpose of this report is to provide a complete documentation of the data requirements and operation of Program WREVAP with its CRAE, CRWE and CRLE options. The chief differences between the CRAE and CRWE options of Program WREVAP and the previously documented Programs REVAP and WEVAP (Morton et al., 1980) are

- (1) The inclusion of the CRLE model has introduced much complexity, because the routing process requires the storage of data and information from previous months.
- (2) The provision of greater flexibility has led to the use of values for the declination and radius vector of the sun that are averages of the daily values for each day of the period rather than values for the middle day of each period. Table 1 presents the resultant monthly frequency distributions of the deviations of the Program REVAP (Morton et al., 1980) estimates of areal evapotranspiration from the comparable Program WREVAP estimates for 925 station-years in Canada and the southern United States. The monthly deviations are small, and the seasonal pattern ensures

that the annual deviations remain small. Because the deviations for the lake-size wet surface evaporation estimates would be even smaller, it can be concluded that CRAE and CRWE model estimates produced by Program WREVAP do not differ significantly from the estimates produced by the models documented in Morton et al. (1980) and Morton (1983a,b).

(3) The minimum constraint on the net long-wave radiation has been changed from 5% to 3% of the surface long-wave radiation. This has little effect and applies only under very hot, humid and cloudy conditions, such as those that prevail at Manaus in the Amazonian rain forest from December to May inclusive (see sample computation in Appendix IV.4).

Program WREVAP is also available for the Hewlett-Packard HP-41CV and HP-41CX hand-held calculators. The documentation is available on request to the senior author.

2. CONCEPTUAL BASIS

The equation describing the complementary relationship is expressed as follows:

$$E_T + E_{TP} = 2E_{TW}$$

Table 1. Frequencies of Monthly Differences between REVAP and WREVAP Estimates of Areal Evapotranspiration Values for Five Years at 185 Stations (925 station-years) in Canada and the Southern United States

mm	January	February	March	April	May	June	July	August	September	October	November	December
1.0	0	0	0	0	0	0	0	0	0	О	0	0
0.9	0	0	0	0	0	0	0	0	0	0	0	0
0.8	0	0	0	0	0	0	0	0	0	0	0	0
0.7	0	0	0	0	0	0	0	0	0	0	0	0
0.6	0	0	0	0	0	0	1	19	0	0	0	0
0.5	0	0	0	0	0	0	4	151	0	0	0	0
0.4	0	0	0	1	0	0	9	213	0	0	0	0
0.3	0	0	0	0	0	0	279	301	0	0	22	· O
0.2	0	0	0	0	0	0	341	181	0	136	83	0
0.1	0	0	0	0	0	0	197	48	150	169	31	0
0.0	38	15	0	0	0	0	94	12	773	619	787	924
- 0. 1	842	735	377	51	4	100	0	0	2	1	2	1
-0.2	18	79	102	52	60	565	0	0	0	0	0	0
-0.3	0	20	80	45	54	256	0	0	0	0	0	0
~0.4	2	32	143	54	110	3	0	0	0	0	0	0
-0.5	11	2	141	69	140	1	0	0	0	0	0	0
~0.6	14	2	65	98	122	0	0	0	0	0	0	0
-0.7	0	3	17	157	135	0	0	0	0	0	0	0
-0.8	0	11	0	176	97	0	0	0	0	0	0	0
-0.9	0	17	0	107	107	0	0	0	0	0	0	0
~ 1.0	0	9	0	66	80	0	0	0	0	0	"O	0
-1.1	o	0	0	41	16	0	0	0	o	0	0	0
-1.2	0	0	0	8	0	0	0	0	O	0	0	0
-1.3	0	0	0	0	0	0	0	0	o	0	0	0

where E_T = areal evapotranspiration, the actual evapotranspiration from an area so large that the effects of the evapotranspiration on the temperature and humidity of the overpassing air are fully developed.

ETP = potential evapotranspiration, as estimated from a solution of the energy balance and vapour transfer equations and representing the evapotranspiration that would occur from a hypothetical moist surface with radiation absorption, heat transfer and vapour transfer characteristics similar to those of the area, and so small that the effects of the evapotranspiration on the overpassing air would be negligible.

E_{TW} = wet environment evapotranspiration, the evapotranspiration that would occur if the soil-plant surfaces of the area were saturated and there were no limitations on the availability of water for evapotranspiration.

Figure 1 provides a schematic representation of the workings of the complementary relationship under conditions of a relatively high radiant-energy supply (solid line) and of a relatively low radiant-energy supply (dashed line). The ordinate represents evapotranspiration and the abscissa represents water supply to the soil-plant surfaces of the area, a quantity that is usually unknown. When there is no water available for areal evapotranspiration (extreme left of Fig. 1), it follows that $E_T=0$, the air is very hot and dry, and E_{TP} is at its maximum rate of $2E_{TW}$ (the dry environment potential evapotranspiration). As the water supply to

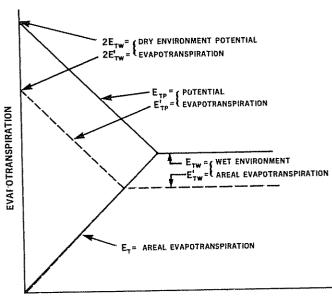


Figure 1. Schematic representation of the complementary relationship.

the soil-plant surfaces of the area increases (moving to the right in Fig. 1) the resultant equivalent increase in E_T causes the overpassing air to become cooler and more humid, and this in turn produces an equivalent decrease in E_{TP}. Finally, when the supply of water to the soil-plant surfaces of the area has increased sufficiently, the values of E_T and E_{TP} converge to that of E_{TW}. Thus, the potential evapotranspiration under completely humid conditions is equal to one-half the potential evapotranspiration under completely arid conditions. Neither E_T nor the availability of water are known, but both E_{TP} and E_{TW} can be estimated from routine climatological observations. Therefore, the CRAE model uses the complementary relationship in the following form:

$$E_T = 2E_{TW} - E_{TP}$$

In the CRAE model, E_{TP} is estimated from a quickly converging solution of the energy balance and vapour transfer equations, and E_{TW} is estimated from the equation for potential evaporation proposed by Priestley and Taylor (1972), as adjusted to take into account the effects of large-scale advection during winter. The two coefficients needed for the adjustment and the vapour transfer coefficient needed in the computation of E_{TP} have been calibrated using data for dry months in arid regions where the sum of E_{TP} and the precipitation approximates 2E_{TW} (Morton, 1983a).

The outputs of the CRAE option of Program WREVAP are E_{TP} and E_T in millimetres, and R_T, the net radiation corresponding to soil-plant surfaces at air temperature, in millimetres of evaporation equivalent. The value of E_{TW} is not normally of interest, but if required it can be computed from the following version of the complementary relationship:

$$E_{TW} = (E_T + E_{TP})/2$$

The evaporation from a lake-size wet surface, E_W, differs from the wet-environment areal evapotranspiration, E_{TW}, only because the radiation absorption and vapour transfer characteristics of water differ from those of vegetated land surfaces. The potential evaporation (hereinafter referred to as pan-size wet surface evaporation and denoted by the symbol E_{WP}) differs from the potential evapotranspiration, E_{TP}, for the same reasons. Although the E_W is equal to the value of E_{WP} estimated from observations in the lake environment, it can differ significantly from the value of E_{WP} estimated from observations in the land environment.

Figure 2 provides a schematic representation of the relationship between the lake-size wet surface evaporation

and the pan-size wet surface evaporation in the land environment under conditions of constant radiant-energy supply. The ordinate represents evaporation and the abscissa represents the water supply to the soil-plant surfaces of the land environment. Since a lake is defined to be so wide that the effects of upwind shoreline transitions are insignificant (Morton, 1983a,b, in press), the lake-size wet surface evaporation is independent of variations in the water supply to the soil-plant surfaces of the land environment. The complementary relationship, however, predicts that the pan-size wet surface evaporation in a completely dry land environment would be twice the lake-size wet surface evaporation and that it would decrease in response to increases in the water supply to the soil-plant surfaces until it reached a minimum equal to the lake-size wet surface evaporation as shown in Figure 2.

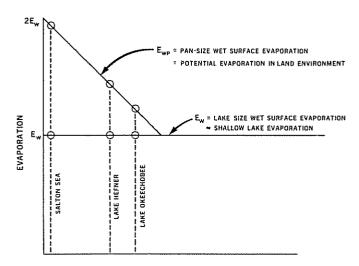


Figure 2. Schematic representation of the relationship between $E_{\mathbf{W}}$ and $E_{\mathbf{WP}}.$

The ratios E_W/E_{WP} have a close correspondence to the well-known pan coefficients that are used to estimate lake evaporation from pan evaporation in the land environment, and the complementary relationship can be used to explain systematic variations in the coefficients. Thus the plotted points in Figure 2 correspond closely to data published by Hounam (1973), which show that the annual Class-A pan coefficient is 0.52 for the Salton Sea in California, where the precipitation less runoff (the water supply to the soil-plant surfaces of the land environment) ~ 60 mm/year; 0.70 for Lake Hefner in Oklahoma, where the precipitation less runoff ~ 700 mm/year; and 0.81 for Lake Okeechobee in Florida, where the precipitation less runoff ~ 1000 mm/year.

The techniques used for estimating E_W and E_{WP} in the CRWE option are almost identical with those used to estimate E_{TW} and E_{TP} in the CRAE option. The only differences are in the use of radiation absorption and vapour transfer characteristics compatible with water surfaces rather than vegetated land surfaces and their effects on the results of the calibration (Morton, 1983a). The outputs of the CRWE option are E_{WP} and E_{W} in millimetres and R_{W} , the net radiation corresponding to a wet surface at air temperature, in millimetres of evaporation equivalent.

In the CRLE option, the procedures used to compute the lake evaporation, E1, and the potential evaporation, E_{LP} , are identical with those used to compute E_{W} and EWP in the CRWE option. However, the results can be very different because the energy term used in the CRLE option is the net available energy, which depends on the solar and waterborne energy inputs for previous months, rather than the net radiation, which depends on the solar energy input for only the current month. The degree to which the net available energy is affected by the solar and waterborne energy inputs of previous months is controlled by a routing procedure with delay times and storage constants that are functions of the depth and salinity of the lake. With the CRLE option, Figure 2 would make no sense because of the lag between energy inputs and energy availability. Thus for Lake Superior (average depth ~ 148 m) the CRLE estimates of lake evaporation and potential evaporation are both 96 mm during December, when the CRWE estimate of pan-size wet surface evaporation in the land environment is -3 mm.

The main outputs of the CRLE model are E_{LP} and E_{L} in millimetres and R_{L} , the net available energy corresponding to a lake surface at air temperature, in millimetres of evaporation equivalent. Subsidiary results are the solar and waterborne energy inputs, G_{L}^{*} [GW(W/M**2) in the computer output listing] for the last 12 months of the period and the available solar and waterborne energy at the end of the last month of the period, G_{LE} (GLEND in the computer output listing). These subsidiary outputs, which are in watts per square metre, can be used as inputs if further updating is required.

3. LIMITATIONS

Program WREVAP can provide reliable estimates of areal evapotranspiration, lake-size wet surface evaporation and lake evaporation from routine observations of temperature, humidity and insolation anywhere in the world, with no need for locally optimized coefficients. The latitude and altitude must be known, as must be the long-term average

annual precipitation for the areal evapotranspiration option, the water salinity for the lake-size wet surface evaporation option or the water salinity and the average depth for the lake evaporation option. The widespread use of Program WREVAP, however, is subject to several limitations. The most stringent, those related to the CRAE (areal evapotranspiration) option, are as follows:

- (1) The CRAE option requires accurate humidity data and these have depended on frequent observations by skilled personnel. This is now one of the more serious limitations to the use of the CRAE models. However, the Humicell, a simple device developed by the Saskatchewan Research Council (Langham, 1969), provides integrated vapour pressure estimates within ±2% for periods exceeding three days. Another more convenient instrument system, which includes a two-channel recorder with temperature sensor, dewcel sensor, solar panel and battery, has been evaluated and is being put into use.
- (2) The CRAE option cannot be used for short time intervals because of subsurface heat-storage changes and because of the lag times associated with the change in storage of heat and water vapour in the atmospheric boundary layer after changes in surface conditions or the passage of frontal systems. The time periods could probably be shortened to five days, but for intervals of three days or less the results would always be suspect. This limitation has little significance in hydrological applications because it does not matter much whether the daily evapotranspiration is 3 or 6 mm, as long as the accumulated values for the week or for a longer period are reliable.
- (3) It cannot be used near sharp environmental discontinuities, such as a high-latitude coastline or the edge of an oasis, because of advection of heat and water vapour in the lower layers of the atmosphere. Analysis of data from irrigated areas (Morton, 1983a) indicates that the effects of such advections can decrease to near zero with 300 m, but this finding may not be generally applicable.
- (4) It requires temperature and humidity inputs from a climatological station whose surroundings are representative of the area of interest.
- (5) It cannot be used to predict the effects of natural or man-made changes because it neither uses nor requires knowledge of the soil-vegetation system and because post-change temperatures and humidities are not predictable. However, it can detect and monitor the effects of these changes as temperature, humidity and insolation data become available.

The wet surface and lake evaporation options are relatively insensitive to errors in the humidity and temperature inputs. Furthermore, it does not matter much where in the vicinity of the lake the temperature and humidity inputs are observed, because the complementary relationship automatically takes into account the effects of differing surroundings. Thus the difference between estimates derived from observations in the land environment and estimates derived from observations over the lake would be due primarily to the relatively minor effects of the difference in humidity on the radiation. Moreover, the effects of shoreline advection on the evaporation from lakes or lake-size surfaces can be disregarded and for smaller wet surfaces (i.e., ponds) they can be taken into account by weighting E_{L} and the E_{LP} using a technique described elsewhere (Morton, in press). However, for the lake evaporation option the length of period is restricted to one month. Finally, the lake evaporation option cannot provide meaningful results unless at least 12 months of continuous input data are available.

4. OPTIONS

This section provides a summary of the output and input options for Program WREVAP. Practical aspects of option selection are discussed in much greater detail in Section 6.2. The output options follow.

4.1 Output Options

The first output option is the choice of outputs from the areal evapotranspiration (CRAE) model, from the wet surface evaporation (CRWE) model, from the lake evaporation (CRLE) model when the required antecedent information is not available or from the lake evaporation (CRLE) model when the required antecedent information is available.

Secondly, there is the choice of outputs for time periods corresponding to months, fractions of months, unequal numbers of days or equal number of days. This choice is available for only the CRAE and CRWE model options, because the CRLE model will provide correct results only for monthly time periods. However, a technique that permits the complementary relationship models to produce hydrologically meaningful daily estimates, with no significant accumulation of error, is described in Section 6.8.

The third choice is a summary tabulation of monthly mean model outputs (entitled MONTHLY TOTALS AVERAGED OVER NYR YEARS). This choice is available only for time period options corresponding to months and fractions of a month.

4.2 Input Options

The input options are used to widen the range of data that can be accepted by Program WREVAP.

The first input option is the choice of average atmospheric pressure (in millibars) or station altitude (in metres above sea level) as the station altitude input.

Secondly, there is the choice of dewpoint temperature (in degrees Celsius or Fahrenheit), vapour pressure (in millibars) or relative humidity (a ratio) as the required humidity inputs. As discussed in Section 6.2, the latter two options must be used with care in estimating areal evapotranspiration.

Thirdly, there is the choice of either the Celsius or the Fahrenheit scale for the required temperature inputs and optional dewpoint inputs.

The fourth choice is the ratio of observed to maximum possible sunshine duration, of observed sunshine duration in hours per day, of observed global radiation in langleys per day or of observed global radiation in megajoules per square metre per day as the required insolation input.

Fifthly, waterborne energy inputs (in watts per square metre) can be accepted when entered in the proper format (see Sections 6.4 and 6.5). If zero, the space can remain blank.

5. PROGRAM LANGUAGE

Program WREVAP has been used successfully on the Control Data Corporation CDC CYBER 74 with the NOS/BE (Network Operating System/Batch Environment) operating system at the Department of Energy, Mines and Resources in Ottawa. It is written in FORTRAN EXTENDED (version 4) language and requires about 52 000 octal words of program storage space. Although execution time varies according to the size of the data base, five years of monthly records would require approximately 0.4 s of the execution time.

It took less than one day for a student to convert Program WREVAP for successful use on both the IBM and the HYPERION microcomputers.

6. DATA PREPARATION

Program WREVAP is designed to accept climatological input data averaged over time periods varying from one

day to one month, although as noted in Section 3, the model estimates for periods of three days or less would always be suspect. Calculations can be performed for only a single station or for many stations at a time. The input specifications, data structures and option selections are shown in Appendix I. They are arranged and organized into logical groupings and referred to as Records A to G inclusive. (Appendix V gives the definitions of variable names used in Appendix I, the main program and the subroutines.)

6.1 Record A of File Tape 1

This record specifies the required station characteristics. In the following list, each of these is identified by the appropriate Record A field number.

- (1) SITE is the station name.
- (2) PHID is the geographical latitude of the station in decimal degrees.
- (3) P may be either the average atmospheric pressure in millibars or the altitude of the station above sea level in metres, depending on which option is selected (Record B, field 9).
- (4) PPN is the average annual precipitation in millimetres per year. It is used only in the areal evapotranspiration option (Record B, field 4) and may be left blank or have any other value, when the wet surface and lake evaporation options are selected.
- (5) DA is the average lake depth in metres. It is used only in the lake evaporation option (Record B, field 4) and may be left blank or have any other real value when the areal evapotranspiration or wet surface evaporation options are selected.
- (6) SALT is the salinity or the total dissolved solids in parts per million. Because it is applied in all three options and is applicable only in the wet surface and lake evaporation options (Record B, field 4), it must be left blank or set equal to zero when the areal evapotranspiration option is selected.

6.2 Record B of File Tape 1

This record contains the data control specifications, such as the total number of periods, the number of periods per month and the settings for the output and input options. In the following list, each of these is identified by the appropriate Record B field number.

- (1) NN is the total number of time periods for which computations are required. It must be known in advance of the computer run.
- (2) M is an integer used to define time periods that correspond to fractions of a month (when INDEX = 2 in field 3 below). With this option the months are divided into M time periods in such a way that the first M-1 periods have the same number of days and the last period has the number of days required to complete the specific months. When INDEX ≠ 2, M must be set equal to 1.
- (3) INDEX is the control parameter used in selecting time periods. Choice of monthly periods requires that INDEX = 1; choice of time periods corresponding to fractions of a month (i.e., having M periods per month) requires that INDEX = 2; choice of time periods having unequal numbers of days requires that INDEX = 3; and choice of time periods having an equal number of days (e.g., weeks) requires that INDEX = 4. The use of this control parameter has the advantage that it is only when INDEX = 3 that the starting dates and durations for individual time periods need to be specified. Some suggestions for deriving useful results for daily periods are discussed in Section 6.8.
- LK is the control parameter used in model selection. (4) Choice of the CRAE (areal evapotranspiration) option requires that LK = 0, choice of the CRWE (wet surface evaporation) option requires that LK = 1, choice of the CRLE (lake evaporation) option, when there is no antecedent information (see discussion of File Tape 2 and File Tape 3 in Sections 6.6 and 6.7), requires that LK = 2 and choice of the CRLE option when antecedent information is available requires that LK = 3. The setting LK = 3 is used in an updating situation when the solar and waterborne energy inputs for the 12 previous months and the available solar and waterborne energy at the end of the preceding month are known from previous computations and can be used as input. The setting LK = 2 is used when antecedent information is not available, and errors in arbitrarily selected initial values are substantially removed by computing the monthly lake evaporation for the first year three times in succession.
- (5) ISUM is a control parameter that can provide a summary tabulation of monthly mean model outputs entitled "MONTHLY TOTALS AVERAGED OVER NYR YEARS." When no tabulation is required the setting must be ISUM = 0, and when the tabulation

- is required, the setting must be ISUM = 1. This option is available only when INDEX = 1 or 2.
- (6) IT is a control parameter in the selection of the Celsius or the Fahrenheit scale for the required air temperature and optional dewpoint temperature inputs. The use of Celsius degrees requires that IT = 0 and the use of Fahrenheit degrees requires that IT = 1.
- (7) IS is a control parameter for the selection of optional insolation inputs. The use of the ratio of observed to maximum possible sunshine duration requires that IS = 0, the use of the observed sunshine duration in hours per day requires that IS = 1, the use of the observed global radiation in langleys per day requires that IS = 2, and the use of the observed global radiation in megajoules per square metre per day requires that IS = 3.
- (8) IV is a control parameter for the selection of optional humidity inputs. Choice of dewpoint temperatures (in degrees Celsius or Fahrenheit) requires that IV = 0, choice of vapour pressure (in millibars) requires that IV = 1, and choice of relative humidity (as a ratio) requires that IV = 2. Significant errors may result from the use of vapour pressures or relative humidities in the CRAE option (Morton, 1983a), although the vapour pressures can be adjusted satisfactorily by using Program VPCOR (Appendix VI).
- (9) IP is a control parameter for the selection of optional station altitude inputs. The choice of average atmospheric pressure (in millibars) requires that IP = 0 and the choice of station altitude (in metres above sea level) requires that IP = 1.

6.3 Record C of File Tape 1

This record contains the date and the period length for the first computation period for each station. It is used only when INDEX = 1, 2 or 4. With these options the information is updated after each computation so that Record C only has to be made once, provided the periods follow a sequence without interruption. This is the chief advantage of the INDEX control parameter. In the following brief comments, each of the time period specifications is identified by the appropriate Record C field number.

(1) STRTDY is the day of the month on which the first computation period starts. For monthly periods (INDEX = 1), and for periods corresponding to

fractions of a month (INDEX = 2), it will always be 1. For time periods having an equal number of days (INDEX = 4), however, it could have any number from 1 to 31.

- (2) MONTH is the month number in which STRTDY occurs, beginning with 1 for January and ending with 12 for December.
- (3) STRTYR is the calendar year (e.g., 1967) in which STRTDY and MONTH occur.
- (4) LENGTH can be any integer value greater than or equal to 1 when INDEX = 1 or 2 and is the number of days in each computation period when INDEX = 4.

6.4 Record D of File Tape 1

This record is used only when INDEX = 1, 2 or 4. It specifies the required climatological data input for each individual time period. If punch cards are being used, one card is required for each period. The data are averages for the specified periods. In the following list, each of the data categories is identified by the appropriate Record D field number.

- (1) TD is the optional humidity input as selected with control parameter IV in Table B, field 8.
- (2) C1 permits estimated values to be distinguished by the letter "E", when tabulated with the model results. Thus C1 is blank when TD is observed, and C1 = E when TD is estimated.
- (3) T is the optional temperature input as selected with control parameter IT in Table B, field 6.
- (4) C2 is to T as C1 is to TD.
- (5) S is the optional insolation input as selected with control parameter IS in Table B, field 7.
- (6) C3 is to S as C1 is to TD.
- (7) HADD is the waterborne energy input to the lake in watts per square metre. It can be estimated from the difference between the heat content of the inflows and the heat content of the outflows and is significant only for relatively small, deep reservoirs on large rivers (e.g., Lake Mead or Lake Nasser) and for small lakes that receive cooling water from thermal power plants. When insignificant, HADD can remain blank.

6.5 Record E of File Tape 1

This record is used only when INDEX = 3, i.e., with time periods of unequal length. It specifies the required climatological data input, the date and the period length for individual time periods. As such, it represents a combination of Record C and Record D. Thus field numbers 1 to 7 inclusive are identical with those of Record D. and field numbers 8 to 11 inclusive differ from fields 1 to 4 inclusive of Record C only because STRTDY, MONTH, STRTYR and LENGTH refer to the specific time period rather than to the first computation period. Thus the use of INDEX = 3 and Record E adds considerably to the time needed for data preparation, when compared with the use INDEX \neq 3 and Records C and D. The INDEX = 3 option, however, permits great flexibility in the definition of LENGTH and this can be helpful in applying Program WREVAP to operational problems. An example of its practicability in deriving useful results for daily periods is presented in Section 6.8.

6.6 Record F of File Tape 2

This record contains the antecedent information required to estimate lake evaporation when LK = 3. It is used in an updating situation, after errors due to arbitrarily selected antecedent information have been substantially removed by computing the monthly lake evaporation for the first year three times in succession, using the option LK = 2. The record can be created by copying Record G of File Tape 3 from the previous run or by copying the information from the output listing of the previous run. GLBGN is the available solar and waterborne energy at the beginning of the month in watts per square metre and is equal to the available solar and waterborne energy at the end of the preceding month (GLEND in Record G of File Tape 3). The quantities denoted by TGW are the antecedent solar and waterborne energy inputs in watts per square metre, with TGW (12) being the value for the preceding month, TGW (11) being the value for the month previous to that, and so on down to TGW (1), which is the value for the current month of the previous year.

6.7 Record G of File Tape 3

This record contains information produced by the lake evaporation model (options LK = 2 or LK = 3), which can provide the antecedent information needed for further updating. Thus the solar and waterborne energy inputs (in watts per square metre) for the first to the twelfth preceding months (TGW (12) to TGW (1), respectively) are identical with those needed in Record F of File Tape 2, and GLEND, the available solar and waterborne energy at the end of the last month of the computation period

(in watts per square metre) is identical with GLBGN. The information in Record G of File Tape 3 is automatically listed with the model results, so that it can be preserved in hard copy and used to create a new Record F at some unpredictable time in the future, when updating is required. It should be noted that the record can be created only after at least 12 months of the required data have been observed and used as input to the CRLE model, with LK set equal to 2, followed, optionally, by further updating with LK set equal to 3.

6.8 Useable Daily Estimates

As noted in Section 3, it may be possible to estimate areal evapotranspiration for time periods as short as five days, although for intervals of three days or less the results would always be suspect. The same considerations apply to wet surface evaporation, although such estimates have little physical significance unless accumulated to provide annual totals. It has also been noted in Section 3 that the length of period for the lake evaporation option is restricted to one month. However, there are some applications, such as the real-time water budgets used in forecasting, where daily estimates are required and where Program WREVAP can provide useful results. This is because in hydrological applications it does not matter much whether the daily evapo(transpi)ration is 3 or 6 mm, as long as the accumulated values for five days or more are reliable.

In updating Program WREVAP estimates on a daily basis, it is the lake evaporation option that presents the greatest difficulties. Therefore lake evaporation is discussed in some detail here. The recommended procedure is as follows:

- (1) Prepare Record A of File Tape 1 using the characteristics of the lake and leaving PPN blank.
- (2) Prepare Record B of File Tape 1 with NN = 1, M = 1, INDEX = 3, LK = 3 and ISUM = 0. The other four fields specify the input data options.
- (3) Prepare Record E of File Tape 1 with TD, T, S and HADD being the mean values for the first day of the month, with STRTDY, MONTH and STRTYR describing the first day of the month and with LENGTH = 1.
- (4) Prepare Record F of File Tape 2 from the values for the end of the preceding month on Record G of File Tape 3. This defines the required antecedent information for the beginning of the current month. It should be noted that this record can be created only after at least 12 months of the required data

- have been observed and used as input to CRLE model with LK set equal to 2, followed, optionally, by further updating with LK set equal to 3.
- (5) The CRLE model estimate of lake evaporation for the first day is equal to the mean daily evaporation in millimetres per day for a month, with mean climatological inputs and solar declination equal to those of the first day.
- (6) In making computations for the second day of the month, it is not necessary to change Records A and B of File Tape 1. Furthermore, Record F of File Tape 2, which provides the required antecedent information at the beginning of the month, remains unchanged throughout the month (the contents of Record G of File Tape 3 are correct only for the last day of the month). Thus the only changes required are in Record E of File Tape 1, where TD, T, S and HADD are set equal to the mean values for the first two days of the month and LENGTH is set equal to 2.
 - 7) The CRLE model estimate of lake evaporation for the first two days of the month has the same daily mean value as that for a month, with mean climatological inputs and solar declination equal to those of the first two days. The estimated daily evaporation, which is the difference between accumulated evaporation estimate and that for the previous day, has an error that partially compensates for error in the previous estimate. Thus, although percentage errors in the evaporation estimates for individual days are large, the absolute errors due to the use of data for short time periods are not hydrologically significant, and they do not accumulate.
- Procedures similar to those set out in steps (6) and (8) (7) should be repeated for each of the remaining days of the month. Near the fifth day the accumulated error associated with the use of short time period data should approach zero, although errors associated with the proration of monthly changes in subsurface heat storage might still be significant. For the last day of the month the input data in Record E of File Tape 1 would be the monthly means, LENGTH would be the number of days in the month, the outputs would be the correctly computed monthly totals with no error associated with the use of short time period data, or with prorating subsurface heat storage changes, and Record G of File Tape 3 would contain the antecedent information needed for Record F of File Tape 2 in continuing with the computation of daily evaporation for the next month.

(9) In continuing the computation into the next month, it is only necessary to read into Record F of File Tape 2 the Record G of File Tape 3 for the previous day (i.e., the last day of the previous month), to repeat step (3), remembering to make the necessary changes in STRTDY, MONTH and STRTYR, and finally to repeat steps (5) to (8) inclusive.

It would not be necessary to start this procedure on the first day of the month. For example, the decision to start daily updating on the twentieth day would require only a single computation of the evaporation for the first 19 days, rather than 19 separate ones.

The procedure described above can be simplified to permit daily updating of areal evapotranspiration or wet surface evaporation estimates. With these options there is no need to use antecedent information so that Record F of File Tape 2, Record G of File Tape 3 and the rigid monthly structure can be dispensed with. Furthermore, the daily estimates would be more reliable because they would not include errors associated with prorating subsurface heat storage changes. This means that the extension of the period length past five days or a week, when errors caused by short period input data become insignificant, is purely a matter of convenience.

There is an alternative procedure for daily updates of areal evapotranspiration or wet surface evaporation estimates. This would involve the use of daily mean input to provide daily estimates, the provisional use of the estimates for a period of five days or a week, and a subsequent proportional correction to make the total for the period agree with the model estimate derived from the mean input for the period. This may provide more realistic daily values than the procedure described in the preceding paragraphs because the error, being prorated, does not include the effects of compensating error. There is no way of proving this possibility, however, and if there were, it is doubtful that the difference would be hydrologically significant. Furthermore, there is the possibility that the accumulated error could become hydrologically significant before being corrected, and there is the obvious nuisance of having to go back and make the corrections. These considerations indicate that it is probably better and certainly more convenient to use the procedure set out in the preceding paragraphs.

7. PROGRAM OPERATION

Program WREVAP is the main program. It reads station specifications, data control specifications, period specifications and input data, and it coordinates the opera-

tion of Subroutines INIT, ERRCOD, INIJUL, ORBIT, BDGT 1, TRANLK, BDGT 2, COMPGL, EVANYR and PRTOUT. The main program and the subroutines are listed, with appropriate descriptions and comments, in Appendix II, and their operations and interactions are summarized in Figure 3, the flowchart for the main program.

8. PROGRAM OUTPUT

Subroutine ERRCOD can detect certain obvious errors in the input data or in the station, data control or period specifications and print an appropriate error message. A complete list of the diagnostic error messages is presented in Appendix III. If no such errors are encountered, Subroutine PRTOUT organizes and lists in chronological order, the model outputs and the input data used to calculate them, together with the necessary station and time period identification. Samples of output listings are presented in Appendix IV and are discussed in some detail in Section 8.2. As some of the headings and other information are expressed as symbols that have not been defined in either the text or Appendix V, they are discussed in Section 8.1.

It should be noted that user given input data are normally provided with two decimal accuracy (page 57). However, the input data shown again in the output samples are listed to one decimal accuracy only (page 56). If reproduction of the same results, as shown for example on page 56, is desired, then input data must be in the same decimal accuracy as listed on page 57; otherwise slight differences from the output samples can develop. If evaporation values are required to 1/10 of a millimetre accuracy, then the format statements 321 and 331 of subroutine PRTOUT have to be changed from F5.0 to F5.1 (page 40).

8.1 Output Symbols

Most, but not all, of the output symbols appear on the sample computations shown in Appendix IV. The top line includes the station specifications and provides identification for the model options. Starting from the left of the top line there are

- (1) The station name.
- (2) PHID, the latitude of the station in decimal degrees.
- (3) P, the average atmospheric pressure in millibars; or ALTI, the altitude above sea level in metres, depending on which option has been selected. The former symbol (P) is used generically for both options in the station specifications and the program.

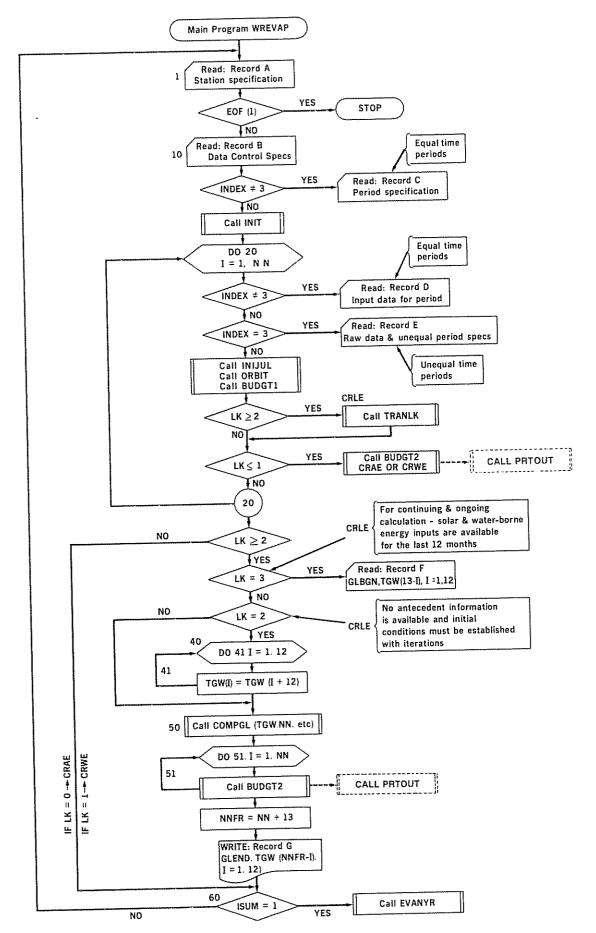


Figure 3. Flowchart of Program WREVAP.

- (4) PPN, the average annual precipitation in millimetres per year, when the areal evapotranspiration option has been selected; or DA, the average depth of the lake in metres, when the lake evaporation options have been selected. The space remains blank for the wet surface evaporation option.
- (5) SALT, the salinity or total dissolved solids in parts per million. The space remains blank for the areal evapotranspiration option.
- (6) NET combines with symbol RAD. directly below to identify the tabulated model estimates, in millimetres of evaporation equivalent, of the net radiation or the net available energy. These estimates correspond to soil-plant surfaces at air temperature, wet surfaces at air temperature or lake surfaces at air temperature, depending on which model option has been selected.
- EVAPOTRANSPIRATION identifies the areal evapotranspiration option and combines with the symbols POTENT, and AREAL in the line directly below to provide column headings for the model estimates (in millimetres) of potential evapotranspiration and areal evapotranspiration. WET SURFACE EVAP. identifies the wet surface evaporation option and combines with the symbols PAN-SIZE and LAKE-SIZE in the line directly below to provide column headings for the model estimates (in millimetres) of pan-size wet surface evaporation and lake-size wet surface evaporation. EVAPORATION identifies the lake evaporation options and combines with the symbols POTENT, and LAKE in the line directly below to provide column headings for the model estimates (in millimetres) of potential evaporation and lake evaporation.

(8) The page number.

The second line from the top of the output listing is used to provide column headings for identification of time periods, input data and model estimates. Starting from the left of the second line, these are

- (1) YEAR, the year in which the time period begins.
- (2) MONTH, the month in which the time period begins.
- (3) STARTDAY, the day of the month on which the period begins.
- (4) LENGTH, the number of days in the period.

- (5) TD, the dewpoint temperature in degrees Celsius; TDF, the dewpoint temperature in degrees Fahrenheit; VD, the vapour pressure in millibars; or RELH, the relative humidity as a ratio, depending on which humidity option is selected. The first of these symbols (TD) is used generically for all four options in the observed data record and the program.
- (6) T, the average air temperature in degrees Celsius; or TF, the average air temperature in degrees Fahrenheit, depending on which temperature option is selected. The former symbol (T) is used generically for both options in the observed data record and the program.
- (7) S, the ratio of observed to maximum possible sunshine duration; HS, the observed sunshine duration in hours per day; GIL, the incident global radiation in langleys per day; or GIJ, the incident global radiation in megajoules per square metre per day, depending on which insolation option is selected. The first of these symbols (S) is used generically for all four options in the observed data record and in the program.
- (8) HADD, the waterborne energy input in watts per square metre. This appears only when data have been entered in field 7 of Record D. Thus the space remains blank for the areal evapotranspiration and wet surface evaporation options and for most lakes with the lake evaporation option.
- (9) RAD combines with the symbol NET in the line immediately above (space 6 of top line) to identify, depending on the model option, the net radiation corresponding to soil-plant surface at air temperature, the net radiation corresponding to wet surface at air temperature or the net available energy corresponding to lake surface at air temperature, all in millimetres of evaporation equivalent.
- (10) POTENT. or PAN-SIZE combine with the symbols EVAPOTRANSPIRATION, WET SURFACE EVAP. or EVAPORATION in the line directly above (space 7 of the top line), to identify, depending on the model option, the potential evapotranspiration, pan-size wet surface evaporation or potential evaporation, all in millimetres.
- (11) AREAL, LAKE-SIZE or LAKE combine with the symbols EVAPOTRANSPIRATION, WET SURFACE EVAP. or EVAPORATION in the line directly above (space 7 of top line), to identify, depending on the model option, the areal evapotranspiration, the

lake-size wet surface evaporation and the lake evaporation, all in millimetres.

(12) GW(W/M**2) is the solar and waterborne energy input in- watts per square metre. This space is blank for the areal evapotranspiration and wet surface evaporation options, and even in the lake evaporation options the data are listed only for the last 12 months of the period. They represent the TGW values in File Tape 3.

The lake evaporation options automatically print two other pieces of information in the line immediately following the input and output listing for the last time period. GLBGN is the available solar and waterborne energy at the beginning of the first time period, and GLEND is the available solar and waterborne energy at the end of the last time period, both in watts per square metre. GLEND is also recorded in File Tape 3.

Subroutine EVANYR is used to produce a table entitled MONTHLY TOTALS AVERAGED OVER NYR YEARS. This requires that ISUM be set equal to 1, that time periods corresponding to months or fractions of months (INDEX = 1 or 2) be selected, and that the total number of time periods be divisible by the number of time periods per year with no remainder. The identifying symbols in the table have been defined previously in this subsection.

8.2 Sample Computations

The use of the CRWE option to compute monthly wet surface evaporation for Pyramid Lake in Nevada, U.S.A., is demonstrated in Appendix IV.1, which includes the output listing for 1935 and 1936, the summary tabulation of MONTHLY TOTALS AVERAGED OVER 2 YEARS and the contents of File Tape 1. In Record B (sixth line, File Tape 1 of Appendix IV.1), NN = 24 time periods, M = 1 time period per month, INDEX = 1 for time periods of a month, LK = 1 for the wet surface evaporation option, ISUM = 1 for production of the summary tabulation, IT = 1 for temperatures and dewpoint temperatures in degrees Fahrenheit, IS = 0 for the use of the ratio of observed to maximum possible sunshine duration as the insolation input, IV = 0 for the use of dewpoint temperature as the humidity input, and IP = 1 for the use of the altitude in metres above sea level as the station altitude input. In Record C (seventh line, File Tape 1 of Appendix IV.1), STRTDY = 1 for the day of the month on which the first period starts, MONTH = 1 for the month (January) during which the first period starts, STRTYR = 1935 for the year during which the first period starts and LENGTH = 1 or any other arbitrarily set integer greater

than zero, because when INDEX = 1 or INDEX = 2 the lengths of the time periods are set automatically in the program. In Record D, the dewpoint temperatures, air temperatures and sunshine duration ratios (the first, second and third columns, respectively, File Tape 1, of Appendix IV.1) are monthly means of the observations at Reno, Nevada.

The CRWE model estimates of wet surface evaporation for the two years average 1346 mm/year, which is 71 mm/year, or 5.6% higher than the water budget estimate of evaporation from the lake for the same two years.

The use of the CRLE model to compute monthly lake evaporation for Pyramid Lake without the required antecedent information is demonstrated in Appendix IV.2, which includes the output listing for 1935, the summary tabulation of MONTHLY TOTALS AVERAGED OVER 1 YEARS, the contents of File Tape 1 and the contents of File Tape 3. The contents of Records A, B, C and D of File Tape 1 differ from those for the CRWE sample in Appendix IV.1 only because DA = 61.0 (new entry), NN = 12, LK = 2, and the input data for 1936 are omitted. File Tape 3 contains output data which are presented as GLEND and in the column designated GW(W/M**2) in the output listing.

The very small difference between GLBGN and GLEND for 1935 is of significance because it demonstrates that the effects of antecedent information arbitrarily selected in the program can be substantially removed by computing the monthly evaporation for the first year three times in succession. However, it also points out a potential source of error in the evaporation estimates for the first year when antecedent information is not available, because it is highly unlikely that the amount of subsurface heat storage would be the same at the end as at the beginning of a year. It may also be of interest to note that the CRLE model estimate of the evaporation from Pyramid Lake during 1935 is 1238 mm, which is 38 mm, or 3.0% lower than the 1935 water budget estimates.

The use of the CRLE model to compute monthly lake evaporation for Pyramid Lake when the required antecedent information is available is demonstrated in Appendix IV.3, which includes the output listing for 1936, the summary tabulation of MONTHLY TOTALS AVERAGED OVER 1 YEARS, the contents of File Tapes 1, 2 and 3. The contents of Records A, B, C and D of File Tape 1 differ from those in the sample for 1935 in Appendix IV.2 only because LK = 3, STRTYR = 1936 and the input data for 1936 are used. The contents of File Tape 2 are read from the contents of File Tape 3 for

1935 in Appendix IV.2 with GLBGN set equal to GLEND. File Tape 3 contains output data which are presented as GLEND and in the column designated GW(W/M**2) in the output listing.

The difference between GLBGN and GLEND is of interest because it shows the total evaporation estimated for 1936 with no antecedent information available (LK = 2) would have been 5 mm (4.5885 W-months/m²) less than the total shown in Appendix IV.3 (LK = 3). It is hoped that this relatively small amount is typical of the error that can be expected during the first year because of the lack of antecedent information. It may also be of interest to note that the CRLE model estimate of the evaporation from Pyramid Lake during 1936 is 1261 mm, which is 12 mm, or 0.9% less than the comparable water budget estimate.

The use of the CRAE option to estimate monthly areal evapotranspiration in the Amazonian rain forest at Manaus, Brazil, is demonstrated in Appendix IV.4, which includes the output listing for a year of long-term monthly mean input data, the summary tabulation of MONTHLY TOTALS AVERAGED OVER 1 YEARS and the contents of File Tape 1. In Record B, NN = 12 time periods, M = 1 time period per month, INDEX = 1 for time periods of a month, LK = 0 for the areal evapotranspiration option, ISUM = 1 for production of the summary tabulation, IT = 0 for temperatures in degrees Celsius, IS = 1 for use of the sunshine duration in hours per day as the insulation input, IV = 1 for use of the vapour pressure in millibars as the humidity input and IP = 1 for use of the altitude in metres above sea level as the station altitude input. In Record C, STRTDY = 1 for the day of the month on which the first period starts, MONTH = 1 for the month (January) during which the first period starts, STRTYR = 9999 (for any value equal to or exceeding 9900 the program prints AVYR) and LENGTH = 31 for the number of days in MONTH (this could be any integer greater than zero, because the period lengths are set internally when INDEX = 1 or INDEX = 2). In Record D. the climatological inputs are the long-term monthly means for Manaus that were published in the World Survey of Climatology, Volume 12, page 272.

The CRAE model estimate of areal evapotranspiration at Manaus for an average year is 1564 mm/year, which is 16 mm, or 1% higher than the difference between precipitation and runoff for the nearby 23.5 km² Model Basin from February 2, 1980, to February 10, 1981. Furthermore, the use of vapour pressure as the humidity inputs produces model estimates that are somewhat too high, although in the climate of the Amazon, where temperature variations are quite small, the error would not exceed 2 mm/month or 20 mm/year.

The use of the CRAE model to estimate areal evapotranspiration for fractions of a month at Val d'Or. Quebec, is demonstrated in Appendix IV.5, which includes the output listing for 1968, the summary tabulation of MONTHLY TOTALS AVERAGED OVER 1 YEARS and the contents of File Tape 1. In Record B, NN = 60, M = 5 time periods per month, INDEX = 2 for time periods of a fraction of a month, LK = 0 for the areal evapotranspiration option, ISUM = 1 for production of the summary tabulation, IT = 0 for temperatures and dewpoint temperatures in degrees Celsius, IS = 1 for the use of sunshine duration in hours per day as the insolation input, IV = 0 for the use of dewpoint temperature as the humidity input and IP = 0 for the use of average atmospheric pressure in millibars as the station altitude input. In Record C, STRTDY = 1 for the day of the month on which the first period starts, MONTH = 1 for the month (January) during which the first period starts, STRTYR = 1968 for the year during which the first period starts and LENGTH = 31 for the number of days in MONTH (as noted previously this could be any integer greater than zero, because the period lengths are set by the program when INDEX = 1 or INDEX = 2). In Record D, the climatological inputs are period means of the observations at Val d'Or during 1968. It should be noted that the CRAE model estimates are based on the unrounded inputs in Record D and not on the rounded inputs shown on the output listing.

The CRAE model estimate of areal evapotranspiration at Val d'Or during 1968 is 419 mm. Val d'Or is in the basin of the Harricanaw River (drainage area of 3680 km²), where the difference between the precipitation and runoff during 1968 was 427 mm.

The use of the CRAE model to estimate weekly areal evapotranspiration at Simcoe, Ontario, is demonstrated in Appendix IV.6, which includes the output listing for 52 weeks in 1968 and the contents of File Tape 1. In Record B, NN = 52, M = 1 (for the equal time period or unequal time period options this is not used), INDEX = 4 for equal time periods, LK = 0 for areal evapotranspiration estimates, ISUM = 0 because the summary tabulation cannot be produced, IT = 0 for temperatures and dewpoint temperatures in degrees Celsius, IS = 1 for the use of the sunshine duration in hours per day as the insolation input option, IV = 0 for the use of dewpoint temperature as the humidity input option and IP = 1 for the use of altitude in metres above sea level as the station altitude option. In Record C, STRTDY = 1 for the day of the month on which the first period starts, MONTH = 1 for the month (January) during which the first period starts. STRTYR = 1968 for the year in which the first period starts, and LENGTH = 7 for the number of days in each time period (this is the first example for which this field has had any meaning). In Record D, the climatological inputs are weekly means of the observations at Simcoe during 1968.

The CRAE model estimate of areal evapotranspiration at Simcoe during 52 weeks in 1968 is 653 mm. Simcoe is near to the 591 $\rm km^2$ drainage area of Big Creek, where the precipitation less runoff for 1968 was 613 mm.

9. CONCLUSIONS

Program WREVAP is based on the complementary relationship between areal and potential evapotranspiration. It comprises the only available technique that can use routine climatological observations to provide reliable independent estimates of areal evapotranspiration, wet surface evaporation or lake evaporation anywhere in the world with no need for locally calibrated coefficients. The conceptual and empirical foundations for the complementary relationship, its superiority to other hydrometeorological concepts, its use in the formulation of the CRAE, CRWE and CRLE models and evaluations of the reality of the models using comparable water budget estimates from a wide range of environments are documented elsewhere (Morton, 1983a,b, in press). It has also been demonstrated (Morton, 1983a) how independent estimates of evaporation and transpiration, which have been until now the largest and most intractable unknown in the hydrological cycle, can do much to overcome the current stagnation in the science and practice of hydrology by permitting solutions to the water balance equation, by providing a realistic basis for hydrological forecasts, by detecting and monitoring the effects of land-use changes, by detecting the development of errors in hydrometeorological records and by other more obvious applications. Program WREVAP expedites the exploitation of these potentialities by the flexibility of its input, time period and output requirements.

10. ACKNOWLEDGMENTS

The authors would like to thank J. Haas for his valuable advice and assistance in the preparation of this report.

11. REFERENCES

- Hounam, C.E. 1973. Comparison between pan and lake evaporation.
 World Meteorol. Org. (W.M.O.), Geneva, Tech. Note No. 126.
 p. 15.
- Langham, E.J. 1969. Discussion paper. Proc. Hydrol. Symp. No. 7. Vol. II, Energy, Mines and Resources, Ottawa, p. 18.
- Morton, F.I. 1983a. Operational estimates of areal evapotranspiration and their significance to the science and practice of hydrology. J. Hydrol. 66(1/4): 1-76.
- Morton, F.I. 1983b. Operational estimates of lake evaporation, J. Hydrol. 66(1/4): 77-100.
- Morton, F.I. Practical estimates of lake evaporation. Submitted for publication. In press.
- Morton, F.I., R. Goard and J. Piwowar. 1980. Programs REVAP and WEVAP for estimating areal evapotranspiration and lake evaporation from climatological observations NHRI Paper No. 12, Inland Waters Directorate, Environment Canada, Ottawa
- Priestley, C.H.B. and R.J. Taylor. 1972. On the assessment of the surface heat flux and evaporation using large-scale parameters.

 Mon. Weather Rev. 100: 81–92.

CRAE Model

Station Altitude (meters) relative houndity (vatio) tempusture (°F° or °C) obs global vadistion (MJ/mz/day) Worterburne Energy Units (W/m²)

Record A Station Characteristics 1) SITE - Station nome

2) PhiD - latitude of Station in dec. deg

3) P - Altitude of Station (m)

4) PPN - Avg Annual Precip (mm)

5) DA - Avg Lake depth (m) - blank for Areal Et

6) SAIT - Salinity (Ppm) - blank For Aveal Et

```
Record B data control specficitions
1) NN - total number of time periods
2) M - time periods or fractions of month
3) INDEX - Control paremeter for Derives/month (3?)
4) LK - model 3 election (RAE = LK = 0
   ISUM - SUMMY tabelation of From (RAE => 150M = 0
   17 - Temperature Units F= IT=1, °C=> IT=0
    15 - insolation units 15 when readition units lang = Z
```

- hum. d. ty inputs viscor pressure units mbors => IV = 1 1 🗸 => significant errors occur in CRHE when using we havidity

or vapor pressure options

- Station Altitude control perconeter Units of Alt (m) => IP=

RECORD C Date and period length

1) STRTDY - Start day Fmonth

2) MONTH - month number which STRTDY Starts

3) STRTYR - calender year

4) lenth -

RECORD D VSEO WHEN INDEX = 1, 2, 4

1) TD

2) C1

3) T

4) CZ

5) 5

6) C3

7) HADD

RECORD E VIED WHEN INDEX = 3

RECORD F USED FOR LAKE Et

RECORD 9 USED when RECORD F 15 being used.

ERROR	LOSICALINPUT ERROR DIAGNOSTIC
н	STARTING YEAR OF THE PERIOD(STRTYR) SHOULD BE GREATER THAN O
N	STARTING HONTH OF THE PERIOD(MONTH) SHOULD CORRESPOND TO ONE OF THE MONTHS OF THE CALENDAR YEAR (E.G. 1 FOR JANUARY AND 12 FOR DECEMBER)
m	STARTING DAY OF THE PERIOD(STRIDY) SHOULD BE ONE OF THE DAYS OF THE MONTH(MONTH)
*	LENGTH OF THE PERIOD(LENGTH) SHOULD BE GREATER OR EQUAL TO 1
Ŋ	TO VALUE SHOULD BE GREATER THAN O WHENEVER THE TO VALUE REPRESENTS THE VAPOUR PRESSURE At dew point or relative humidity.
ø	S VALUE SHOULD BE GREATER THAN OR EQUAL TO 0.
10	INDEX VALUE SHOULD BE EQUAL TO 1, 2, 3 OR 4 (SEE INDEX DESCRIPTION)
11	THE CONTROL PARAMETER IS SHOULD BE EQUAL TO 0, 1, 2 OR 3 (SEE IS DESCRIPTION)
12	THE CONTROL PARAMETER IT SHOULD BE EQUAL TO 0 OR 1 (SEE IT DESCRIPTION)
13	THE CONTROL PARAMETER IV SHOULD BE EQUAL TO 0, 1 OR 2 (SEE IV DESCRTHE CONTROL PARAMETER IPTION)
14	THE CONTROL PARAMETER IP SHOULD BE EQUAL TO 0 OR 1 (SEE IP DESCRIPTION)
13	THE CONTROL PARAMETER LK SHOULD BE EGUAL TO 0, 1 ,2 OR 3
11	THE TOTAL NUMBER OF PERIODS(NN) SHOULD BE GREATER THAN OR EQUAL TO 1, AND WHEN LAKE EVAPORATION ESTINATES ARE REQUIRED THE TOTAL NUMBER OF PERIODS SHOULD LESS THAN OR EQUAL TO 120. HOWEVER THE LATTER RESTRICTION CAN BE RELAXED IF THE TABLES DIMENSIONED TO 120 ARE CHANGED TO THE TOTAL NUMBER OF PERIODS, THE TABLE DIMENSIONED TO 132 IS CHANGED TO THE TOTAL NUMBER OF PERIOD PLUS 12 AND THE CHARACTER STRING 120 IN THE FORTRAN STATEMENT CALL ERRCOD(10) IS CHANGED TO THE TOTAL NUMBER OF PERIODS
18	THE NUMBER OF PERIODS PER MONTH(M) SHOULD ALWAYS BE GREATER OR EQUAL I AND SHOULD ALWAYS BE EQUAL TO I WHEN INDEX EQUAL 1, 3 OR 4
19	WHEN ISUM EQUAL 1 (I.E. WHEN MONTHLY TOTALS AVERAGED OVER NYR YEARS ARE REQUIRED) INDEX SHOULD BE EQUAL TO 1 OR 2 (DENOTING MONTHLY STRUCTURE) AND THE TOTAL NUMBER OF PERIODS SHOULD BE DIVISIBLE BY NUMBER OF PERIODS PER YEAR WITH NO REMAINDER
20	VALUE OF DA SHOULD BE GREATER THAN OR EQUAL TO 0.
21	VALUE OF SALT SHOULD BE GREATER THAN OR EQUAL TO 0.
22	VALUE OF PPN SHOULD BE GREATER THAN OR EQUAL TO 0.
6 2	VALUE OF P SHOULD BE GREATER THAN OR EQUAL TO 0.

Z S S S S S S S S S S S S S S S S S S S	STARTOAY TARTOAY	LENGTH 23 31	10F 25.0 25.0 23.0	999 999 900 900 900	. 570 . 580 . 760	## ## ## ## ## ## ## ## ## ## ## ## ##	PAN=SIZE L 30. 63. 113.	AK
ш >-	ने इन्ते इन्ते इन्ते इन्ते	40 H 0 H	34.0 34.0 34.0	547.0 547.0 54.0 54.0 54.0	.710 .790 .960	100000 90000 90000 90000 90000	20 20 20 40 40 40 40 40 40 40 40 40 40 40 40 40	119. 172. 216. 211.
· . -	न्त्रम् ललन		000000 - n m m m n N N N N	는 今 속 ଲ ଲ c 시	00000000000000000000000000000000000000	# 0 0 0 0 0 1 2	* * * * * * * 6	* * * * * * 0 M H N O M > 4 E M N N 1 H
	A A A A A	1 6 H 0 H	10000 10000 10000) (C) (C) (C) (C) (C) (C) (C) (C) (C) (C	00000	46. 126. 245.	2044.	8 2 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6
JUNE JULY AUG SEPT OCCT NOV	: a a a a a a a a a		64 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	\$ ~ ~ ~ & ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	11221 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	* * * * * * * * * * * * * * * * * * *	

IV.1 PYRAMID LAKE - CRWE OPTION

YEARS	ACE EVAP. Lake—Size	_			_	-			-	-			æ	2040	1346.0	MODEL ESTIMATES OF		13333	23426																											
OVER 2	WET SURFAC	32.0	0.09	9 6	9	9	EU EU	8	9	2	254.0	5	0.49	2540	2123.0	- 20	ON_EDR_PYR	222333333	26722212342678			570	580	.760	.710	.790	.960	• 920	.970	040	670	080	0,0	010	270	.780	.850	.890	.770	.890	*880	.920	.840	006*	. 560	
TOTALS AVERAGED	NET RAD.		0.44		120.5	177.0	234.5	234.5	230.5	199.0	152.0	0.20	0	41	1345.0	PET USED AS 1	EACE_EXAPORA]	11111112222	345678901234	- DT		33	39.6	37.9	47.7	55.6	67.	69.4	72.2	67.1	40.0	m :	3396	'n	30	4	52	5	9	74.	71.	61.	E	41.	33.00	
MONTHLY	HONTH	24.	E 0	r :	α *	APR	MAY	JUNE	TITA	717	100	F	- > C	080	Y AVERAGES	1111		000000000111	123456789012	2411111001	1 11935 1	25.0	26.0	23.0	29.0	31.0	34.0	37.0	37.0	33.0	28.0	23.0	23.0	25.0	26.0	25.0	29.0	31.0	38.0	41.0	38.0	32.0	30.0	21.0	22.0	ì
															TOTAL OF MONTHLY			NXII IU	NUMBER																											

PYRAMID LAKE

IV.2 PYRAMID LAKE — CRLE OPTION WITHOUT ANTECEDENT INFORMATION

PYRAMID	LAKE	-DHID=	40.00	ALTI= 1160.0	DA	w	3500.00	F 8 6	EVAPORATION	2	3
YEAR	HUNTH	STARTDAY	LENGTH			v į	HADD	X X De	- 22 F	1 P F T	E/M/MO
1933	ZY	 4	31		D en	0) (0	00.0	0007	607	•	•
1935			28		9000	. 580	00.0	107	9	•27	-
400	MAR		31		37.9	• 160	000	73•	•06	33.	_
200	90 4		O.F.		47.7	.710	00.0	47.	#8±	*6*	_
100	< >< X	1	ה ה		100 an	.790	00.0	46.	100.	58.	_
100	- 2	4	10		67.1	096	00.0	•09	160.	81.	-
	2 N	4	0 6		7.09	.920	00.0	100.	223.	114.	316.2
700	200	4	1 17		72.2	.970	00.0	141.	293.	140.	•
	100	4	1 6		67-1	046	00.0	173.	283.	160.	241.3
n #	- Fi	4 -	9.5		0 0	.870	00.0	209	206.	151.	177.6
700		4 -	4 6		. K.	089	00.0	214.	136.	128.	-
730	> C	e	7 6	72.0	60 er	570	00.0	206.	125.	121.	
1933	מבר הבר	4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	ŗ	P 4 4	7446 - 04812	•))	•	! !		
				YONTHI	NTHIY INTALS AVERAGED	OVER 1	YEARS				
					⊢ 11 2	FVAPO	XC L				
				HONTH	RAD.	POTENT.	LAKE				
				Z	168.0	103.0	100.0				
				e u	107.0	0.86	72.0				
				T T	73.0	0.06	55.0				
				0.4	47.0	88.0	0.64				
				×	0.94	109.0	58.0				
					0.09	160.0	81.0				
				JULY	100.0	223.0	114.0				
				904	141.0	293.0	149.0				
				9. 0. 1.	173.0	283.0	160.0				
				100	209.0	206.0	151.0				
				AON	214.0	136.0	128.0				
				DEC	20640	123+0	121.0				
		TOTAL OF	MONTHLY	AVERAGES	1544.0	1914.0	1238.0				

IV.3 PYRAMID LAKE — CRLE OPTION WITH ANTECEDENT INFORMATION

(W#W/ M) M9	79.92	118.36	40 +01	00 1 107	270.43	319.26	200 50		124)08	276.19	245*37	173.54	130.21	76.86																		
TION	106.	72		34	* 6 *	57.0	.76		# 12 m	155.	R.	153.	N	1170																		
EVAPORATION POTENT.	126.	ā		100	43*	110.	162) i	• 962	292	240	221.	168.	123.																		
NET RAD.	160	114		•	39.	41.	7.1		111	137	175.	*66T	196.	200	1																	
3500.00 HADD	0.0		5	00.0	00.0	00.0	0	•	00.0	00.0	00.0	00.0	00.0	00.0	•		YEARS	TION	LAKE	106.0	72,0	59.0	49.0	57.0	94.0	131,0	135.0	150.0	153.0	128.0	11Ze0	1261.0
SALT.	, E			• 780	.830	.890	140	2	.890	. 880	.920	0+8*	000	260	•		2	EVAPORATION	POTENT.	126.0	85.0	106.0	93.0	110.0	162.0	256.0	292.0	249.0	221.0	168.0	123.9	1991.0
0A# 61.0	- 0		0.00	8***	52.6	47.4) 	0	74.3	71.4	61.6	90) (" 4 (T	}	7490°647 # 0	TOTALS AVERAGED	F H J	RAD.	169.0	114.0	67.0	39.0	41.0	71.0	111.0	151.0	175.0	199.0	196.0		1533.0
ALTI= 1160.0	- 4) (0 * 0 7	25.0	29.0		•	36.0	41.0	38.0	32.0	30.0		22.0	, '	**** GLENU	MONTHLY TO		HONIE	NAU	## ##	2 4	A 9 8	× ×	E SE	701	AUG	SEPT	100	X0.X		VERAGES
4 0.00 4	ריינ	# (P	62	m	0.00) r	7.	30	37	E	0	, F	4 C	2		177																MONTHLY AVERAGES
	SIAKIUAT	-4 ,	-	-		٠,		-	-			• -	٠.	- 4 #-	-	6L86N • 248.2777																TOTAL OF
LAKE	H NOR	247	FEB	X W	00	C 2	-		JULY	A 115	Tou			202		879 ***																
PYRAMID	YEAR	1936	1936	1036	4604	0.00	7.430	1936	1936	1026	, 0	7 7 7 7	2	1930	7	•																

ILE TAPEL USED AS TAKE_EYARDRALION_EOR 500001111111112222 56789012345678901234 78MID LAKE 40.	2255 2255 2255 3315 3315 225 225 225 225 225 225 225 225 225 2	O O	119.2077 B5.9173 B5.9173 FILE TAPES RESULTING FROM THE CRLE MODEL ESTIMATES OF 000000000111111111112222222233333333333
23.4	ี่ผลผลตระตุดตลงพ	122 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	22 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2

TIND				DEG. K								¥/ H++2	D-930	H/H++2		RAD/DEG.					XC.		MB/DEG.C	MB/DE6.C
LIST OF VARIABLE NAMES USED IN THE PROGRAM Definition	AVERAGE ALBEDO	COSINE OF OMEGA	COSINE OF OMEGAA	ABSOLUTE AVERAGE AIR TEMPERATURE	CONSTANT IN COMPUTATION OF VAPOUR PRESSURE	WEIGHTING FACTOR FOR THE EFFECT OF SNOW ON ALBEDO	WEIGHTING FACTOR FOR THE EFFECT OF CLOUDS ON ATMOSPHERIC RADIATION	CLEAR SKY ALBEDO IF SUN WERE AT ZENITH	SNOW-FREE, CLEAR SKY ALBEDO IF SUN WERE AT ZENITH	INTERMEDIATE STEP IN COMPUTATION OF AZZ	CLEAR SKY ALBEDO	NET LONG WAVE RADIATION LOSS WITH SURFACE AT T	CONSTANT IN COMPUTATION OF VAPOUR PRESSURE	CONSTANT USED IN CALCULATING ETW	CONSTANT USED IN CALCULATING ETW	CONSTANT FOR CONVERSION FROM DEGREES TO RADIANS	COSINE OF THE AVERAGE SOLAR ZENITH DISTANCE	COSINE OF NOON SOLAR ZENITH DISTANCE	COSINE OF NOON SOLAR ZENITH DISTANCE PLUS 0.005	ALPHA-NUMERIC VALUE. BLANK INDICATES AN ACTUAL Observation, and "e" an estimated value	AVERAGE DEPTH OF THE LAKE	FIRST DAY OF THE PERIOD AS A CALENDAR DAY	SLOPE OF THE SATURATION VAPOUR PRESSURE CURVE AT TP	SLOPE OF THE SATURATION VAPOUR PRESSURE CURVE AT T
# DO Y		ACOM	ACOMA	ΑĶ	ALPHA(J)	ARAT	ATA	4.2	A22	A Z Z Z	A 0	æ	BETA(J)	CONSTI	CONSTZ	CONV	2500	CZENA	CZENAA	C1, C2, C3	V O	DAY	DELP	DELTA

	LIST OF VARIABLE NAMES USED IN THE PROGRAM	
VARIABLE	DEFINITION	UNIT
DUST	TURBIDITY COEFFICIENT	
OUSTT	INTERMEDIATE STEP IN CALCULATION OF TAUT	
m	FTZ(J) * (V = VD)	W/H++2
<u>н</u>	POWER EQUIVALENT OF AREAL EVAPOTRANSPIRATION, LAKE-SIZE WET SURFACE EVAPORATION OR LAKE EVAPORATION	Z++H/A
# H W	ET IN EVAPORATION UNITS	X.
ETNYR	SUM OF MONTHLY VALUES OF ETMM	X.
ETP	POWER EQUIVALENT OF POTENTIAL EVAPOTRANSPIRATION. PAN-SIZE WET SURFACE EVAPORATION OR POTENTIAL EVAPORATION	W/H++2
ETPMM	ETP IN EVAPORATION UNITS	Ŧ
ETPNYR	SUM OF MONTHLY VALUES OF ETPMM	X.
N ET A	POWER EQUIVALENT OF WET ENVIRONMENT AREAL EVAPOTRANS— PIRATION, LAKE—SIZE WET SURFACE EVAPORATION OR LAKE EVAPORATION	Z++#/X
FRACT	FRACTIONAL COMPONENT OF DELAY TIME	HONTH
←	VAPOUR TRANSFER COEFFICIENT	W/H**2/HB
FTZ(J)	VAPOUR TRANSFER COEFFICIENT * STABILITY FACTOR	W/H**2/HB
7.4	COEFFICIENT USED IN COMPUTING FTZ(J)	W/H**2/MB
g	INCIDENT GLOBAL RADIATION	1/ M++2
GAHNA(J)	SENSIBLE HEAT TRANSFER COEFFICIENT	MB/DE6.C
e E	EXTRA-ATHOSPHERIC GLUBAL RADIATION	W/Me+2
1 9	IF LK = 0 OR LK = 1, GL = ABSORBED GLOBAL RADIATIONS(GW) IF LK = 2 OR LK = 3, GL = AVAILABLE SOLAR & WATER-BORNE ENERGY	W/H++2
GLB	GL AT THE BEGINNING OF THE PRESENT MONTH	N/H**2
N9879	GL AT THE BEGINNING OF THE FIRST PERIOD	N/84+2
GLE	GL AT THE END OF THE PRESENT MONTH	N/H++2
GLEND	GL AT THE END OF THE LAST PERIOD	17 H++2

PROGRAM
THE T
USED IN
NAMES U
VARIABLE
O.
LIST

 (1 t)	7	N/###2	N/H++2	Z++W/K						HONTH	HONTH	8	X.	HOUR/DAY LY/DAY HJ/H*+2/DAY		DEG.C DEG.F	DEG.C MB G.F TIO
DEFINITION	IF LK = 0 OR LK = 1, GW = ABSURSED GLUBAL RADIALION IF LK = 2 OR LK = 3, GW = SOLAR G WATER-BORNE ENERGY INPUT	DELAYED SOLAR & WATER-BORNE ENERGY	CLEAR SKY GLOBAL RADIATION	WATER-BORNE ENERGY INPUT TO LAKE (CAN BE IGNORED IF HADD IS ZERO)	SUBSCRIPT	SUBSCRIPT	IF INDEX = 1, MONTHLY STRUCTURE IS USED IF INDEX = 2, MONTHLY STRUCTURE WITH M PERIODS PER	MONTH IS USED IF INDEX = 3, UNEQUAL TIME PERIOD STRUCTURE IS USED (I.e. 5 DAY, 16 DAY, 9 DAY,ETC) IF INDEX = 4, EQUAL TIME PERIOD STRUCTURE IS USED	(I.E. VEEKLY) #NOTE WHEN LK > 1 INDEX MUST BE FQUAL TO 1	INTEGER VALUE OF THE DELAY TINE	INTEGER VALUE OF THE DELAY TINE PLUS 1	CONTROL STATION PARAMETER FOR STATION ALTITUDE IF IP = 0, P IS THE AVERAGE ATMOSPHERIC PRESSURE	AT STATION IF IP = 1, P IS THE ALTITUDE OF STATION ABOVE MEAN SEA LEVEL	CONTROL PARAMETER FOR INSOLATION DATA. IF IS = 0, S IS THE SUNSHINE DURATION RATIO IF IS = 1, S IS THE SUNSHINE DURATION IF IS = 2, S IS THE INCIDENT GLOBAL RADIATION IF IS = 3, S IS THE INCIDENT GLOBAL RADIATION	CONTROL PARAMETER FOR STATION SUMMARY. IF ISUM = 0, TABULATION OF MONTHLY TOTALS AVERAGED OVER NYR YEARS IS NOT LISTED IF ISUM = 1, TABULATION OF MONTHLY TOTALS AVERAGED OVER NYR YEAR IS LISTED (NYR MUST BE AN INTEGER)	CONTROL PARAMETER FOR TEMPERATURE DATA. IF IT = 0, T IS AIR TEMPERATURE IN CELSIUS IF IT = 1, T IS AIR TEMPERATURE IN FAHRENHEIT	CONTROL PARAMETER FOR HUMIDITY DATA. IF IV * O AND IT * O, TD IS THE DEW POINT IF IV * O AND IT * 1, TD IS DEW POINT IF IV * I, TD IS VAPOUR PRESSSURE AT THE DEW POINT IF IV * 2, TD IS RELATIVE HUMIDITY
VARIABLE	N O	THO	09	HADD	+-4	p=4 p=4	INDEX			INTE	INT	dП		IS	I SUM	Ħ	>

PRUGRAM
IN THE
USED
NAMES
VARIABLE
6
LIST

ARIABLE	DEFINITION	UNIT
Ħ	MONTH THAT IS INTI MONTHS BEFORE THE PRESENT MONTH IN THE TGW TABLE	HONTH
_	INDEX FOR THE SELECTION OF CONSTANTS THAT DEPEND ON WHETHER THE TEMPERATURE IS ABOVE, AT OR BELOW FREEZING J = 1, IF I IS GREATER THAN OR EQUAL TO C J = 2, IF I IS LESS THAN O C	
9830	BEGINNING OF THE PERIOD AS A JULIAN DAY	DAY
JULDAY	REAL VALUE OF JULIAN PLUS REAJUL (SEE DEFINITIONS BELOW)	DAY
JULEND	LAST DAY OF THE PERIOD AS A JULIAN DAY	DAY
JULIAN	COUNTER FOR JULIAN DAY	DAY
~	STORAGE ROUTING CONSTANT	MONTH
LAMDA	HEAT TRANSFER COEFFICIENT	MB/DE6.C
LENGTH	LENGTH OF THE PERIOD	DAY
LIMITL	NUMBER OF LINES PRINTED PER PAGE	LINES/PAGE
تخ	CONTROL PARAMETER FOR SELECTION OF MODEL OPTION SELECTED IF LK = 1, WET SURFACE EVAPORATION(CRME) OPTION IS SELECTED IF LK = 2, LAKE EVAPORATION(CRME) OPTION WITH NO PREVIOUS GW INPUT IS SELECTED IF LK = 3, LAKE EVAPORATION(CRLE) OPTION WITH PREVIOUS GW IF LK = 3, LAKE EVAPORATION(CRLE) OPTION WITH PREVIOUS GW IF LK = 3, LAKE EVAPORATION(CRLE)	CTED US GW
LNX	USED AS ARGUMENT IN CALCULATION OF TAUT	
LNY	USED AS ARGUMENT IN CALCULATION OF TAUA	
-	DELAY TIME	HUNTH
LTHEAT	LATENT HEAT OF VAPORIZATION(OR SUBLIMATION)	W-DAY/NH
÷.	NUMBER OF TIME PERIODS PER MONTH IN A MONTHLY STRUCTURE. IF INDEX.NE.2 THEN M " I	
I	NUMBER OF ITERATIONS NEEDED TO COMPUTE TGL (USED ONLY FOR LAKE EVAPORATION) IF LK = 3, THEN MM =	æ ⊶
NON	TABLE FOR THE NAMES OF THE MONTHS	

	I	HONTH	HOUR / DAY	DAY										RADIANS	RADIANS				RADIANS	DEGREES		MM/YR		ກ • ວ ຄ. ;
LIST OF VARIABLE NAMES USED IN THE PROGRAM	DEFINITION	NUMBER FOR MONTH DURING WHTCH THE PERIOD BEGINS.	MAXIMUM POSSIBLE SUNSHINE DURATION	TABLE FOR THE LENGTHS OF THE MONTHS	RADIUS VECTOR OF THE EARTH'S ORBIT AROUND THE SUN	COUNTER FOR RAW DATA INPUT	TOTAL NUMBER OF TIME PERIODS	COUNTER USED ALSO AS A SUBSCRIPT	COUNTER USED ALSO AS A SUBSCRIPT	LINE COUNTER FOR PAGE PRINTOUT	PAGE COUNTER FOR STATION PRINTOUT	COUNTER FOR PERIODS IN A MONTH	NUMBER OF YEARS OF DATA	HALF THE ANGLE THE EARTH ROTATES BETWEEN THEORETICAL Sunrise and theoretical sunset	HALF THE ANGLE THE EARTH ROTATES BETWEEN APPARENT Sunrise and apparent sunset	INTERMEDIATE STEP IN CALCULATION OF ORB2	INTERMEDIATE STEP IN CALCULATION OF THETA AND NETA	SEE CONTROL PARAMETER IP	LATITUDE	LATITUDE IN DECIMAL DEGREES	CONSTANT = 3.141392654	AVERAGE ANNUAL PRECIPITATION	USED TO KEEP THE ORIGINAL VALUE OF P FOR PRINTOUT	ADJUSTHENT TO THE INTEGER VALUE OF THE JULIAN DAY IF MONTH = 1 OR 2, THEN REAJUL = 0.0 IF MONTH > 2 AND IT IS A LEAP YEAR, THEN REAJUL = -0.5 IF MONTH > 2 AND IT IS NOT A LEAP YEAR, THEN REAJUL = (
	VARIABLE	HINDE	#SD	· -	NETA	NINPUT	Z	NNFR	OTNN	NOLINE	NOPAGE	NTINE	X X	ONEGA	UNEGAA	0881	0882	a	H	PHID	Id	Nd d	× d.	REAJUL

 *	LIST OF VARIABLE NAMES USED IN THE PROGRAM	UNIT
VARIABLE		3
REMAIN N	NUMBER OF DAYS IN LAST PERIOD OF MONTH (USED ONLY WHEN INDEX = 2)	DAY
20	PROPORTIONAL INCREASE IN ATMOSPHERIC RADIATION Due to clouds	
	NET RADIATION CORRESPONDING TO SOIL-PLANT SURFACES AT T. NET RADIATION CORRESPONDING TO WET SURFACE AT TOR NET AVAILABLE ENERGY CORRESPONDING TO LAKE SURFACE AT T	2++H/K
. –	RT CONSTRAINED FOR USE IN ZETA ESTIMATES	N/H++2
> X	RT IN EVAPORATION UNITS	E E
œ	SUMS OF MONTHLY VALUES OF RTMM	X.
	NET RADIATION CORRESPONDING TO SOIL-PLANT SURFACES AT TP, NET RADIATION CORRESPONDING TO TP OR NET AVAILABLE ENERGY CORRESPONDING TO TP	2++W/A
	SEE CONTROL PARAMETER IS	
- T - T - T - T - T - T - T - T - T - T	TOTAL DISSOLVED SOLIDS OR SALINITY	** 0.0
-		W/H**2/K**4
SITE	STATION NAME	
SLT	SOFT WATER DELAY TIME	H NO
STRTOY	STARTING DAY OF THE CURRENT PERIOD	DAY
STRTAN	STARTING MONTH OF THE CURRENT PERIOD	HONTH
STRTYR	STARTING YEAR OF THE CURRENT PERIOD. FOR ANY INPUT VALUE EQUAL TO OR EXCEEDING 9900 THE PROGRAM PRINTS AVYR FOR AVERAGE YEAR	~ ≪ ≪
	USED TO KEEP ORIGINAL VALUE OF S FOR PRINTOUT	
	AVERAGE AIR TEMPERATURE(SEE OPTION IT)	DEG.C OR DEG.F
TAUA	PART OF TAUT THAT IS RESULT OF ABSORPTION	
TAUT	TRANSHITTANCY OF CLEAR SKIES TO DIRECT BEAM SOLAR Radiation	
TC1, TC2, TC3	TABLES OF C1, C2,C3	
10	SEE CONTROL PARAMETER IV	
	TALL TO LEADED DAV	DAY

CTION FOR THE TO KEEP ORIGINATION FOR THE TO KEEP ORIGINATION OF SUBSIDING YEAR AND THE TOP AND THE TOP AND THE TOP AND THE TO THE EVAPORTIAL EVAPORTIAL EVAPORTIAL EVAPORTIAL EVAPORTIAL EVARIABLE OF VARIABLE	VARIABLE NAMES USED IN THE PROGRAM	DEFINITION	P IN THE ITERATION PROCESS	GINAL VALUE OF TO FOR PRINTOUT	ETMM FOR STATION SUMMARY	ETPHM FOR STATION SUMMARY	ב פו	GW VALUES WITH SUBSCRIPT OF 13 FOR FIRST MONTH, WITH VALUES SUBSCRIPTED FROM 1 TO 12 FOR THE PRECEDING YEAR, FROM 13 TO 24 FOR THE FIRST YEAR AND 25 TO NN + 12 FOR ANY SUBSEQUENT YEARS, IF VALUES FOR PRECEDING YEAR ARE NOT AVAILABLE, THE VALUES FOR THE STARTING YEAR ARE USED TWICE WITH SUBSCRIPTS FROM 1 TO 12 AND 13 TO 24	E HADD	n.		E LENGTH	E MONTH	. EVAPOTRANSPIRATION EQUILIBRIUM TEMPERATURE. WET SURFACE EQUILIBRIUM TEMPERATURE OR . EVAPORATION EQUILIBRIUM TEMPERATURE	INH FOR STATION SUMMARY	N H	R FOR EFFECTS OF TEMPERATURE	3× 0	LE +	LE TDW		LE TW
CORRECTORS OF TABLE		DEFINITI	<u>-</u>	TO KEEP ORIGINAL	MONTHLY TOTAL OF ETMM FI	OF ETPHM	VARIABLE	GW VALUES WITH SUBSCRIPT OF 13 YEAR, FROM 13 TO 24 FOR THE FII YEAR, FROM 13 TO 24 FOR THE FII NN + 12 FOR ANY SUBSEQUENT YEAR PRECEDING YEAR ARE USED TWILL 1 TO 12 AND 13 TO 24	VARIABLE	DECLINATION OF SUN	VARIABLE	VARIABLE	VARIABLE	POTENTIAL EVAPOTRANSPIR PAN-SIZE WET SURFACE EQ POTENTIAL EVAPORATION E	MONTHLY TOTAL RIMM FOR	VARIABLE	GHTING FACTOR FOR Turbidity	VARIABLE	VARIABLE	VARIABLE	TABLE OF VARIABLE TH	

	UNIT	0E6.C UR 0E6.F	YEAR	W.	6 0	8 9	Q	£			ADE YEAR	DAY	RADIANS	
LIST OF VARIABLE NAMES USED IN THE PROGRAM	DEFINITION	USED TO KEEP ORIGINAL VALUE OF T FOR PRINT OUT	TABLE OF VARIABLE YEAR	SATURATION VAPOUR PRESSURE AT T	SATURATION VAPOUR PRESSURE AT DEW POINT	SATURATION VAPOUR PRESSURE AT TP	VAPOUR PRESSURE DEFICIT	PRECIPITABLE WATER VAPOUR	INTERMEDIATE STEP IN COMPUTATION OF TAUA	INTERMEDIATE STEP IN COMPUTATION OF TAUT	YEAR IN WHICH CLIMATOLOGICAL OBSERVATION WAS MADE	SHORT FORM FOR YEAR USED AS HEADING	NOON SOLAR ZENITH DISTANCE	STABILITY FACTOR
	VARIABLE	*	TYEAR	>	٥٨	ΛÞ	VPDL	>	AVA	TAN	YEAR	≺ R	ZENA	ZETA