

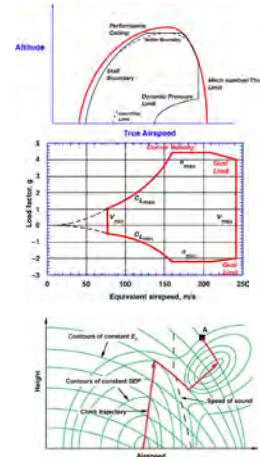
Gliding, Climbing, and Turning Flight Performance

Robert Stengel, Aircraft Flight Dynamics,
MAE 331, 2016

Learning Objectives

- Conditions for gliding flight
- Parameters for maximizing climb angle and rate
- Review the V - n diagram
- Energy height and specific excess power
- Alternative expressions for steady turning flight
- The *Herbst maneuver*

Reading:
Flight Dynamics
Aerodynamic Coefficients, 130-141



Copyright 2016 by Robert Stengel. All rights reserved. For educational use only.
<http://www.princeton.edu/~stengel/MAE331.html>
<http://www.princeton.edu/~stengel/FlightDynamics.html>

1

Review Questions

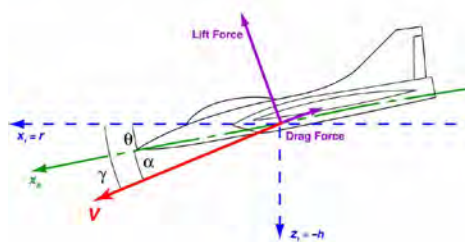
- How does air density decrease with altitude?
- What are the different definitions of airspeed?
- What is a "lift-drag polar"?
- Power and thrust: How do they vary with altitude?
- What factors define the "flight envelope"?
- What were some features of the first commercial transport aircraft?
- What are the important parameters of the "Breguet Range Equation"?
- What is a "step climb", and why is it important?

2

Gliding Flight

3

Equilibrium Gliding Flight



$$D = C_D \frac{1}{2} \rho V^2 S = -W \sin \gamma$$

$$C_L \frac{1}{2} \rho V^2 S = W \cos \gamma$$

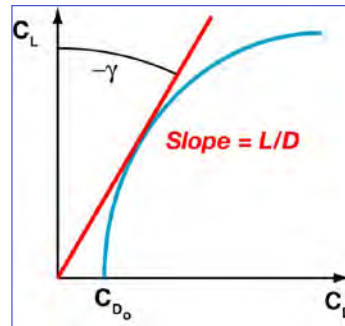
$$\dot{h} = V \sin \gamma$$

$$\dot{r} = V \cos \gamma$$

4

Gliding Flight

- Thrust = 0
- Flight path angle < 0 in gliding flight
- Altitude is decreasing
- Airspeed \sim constant
- Air density \sim constant



Gliding flight path angle

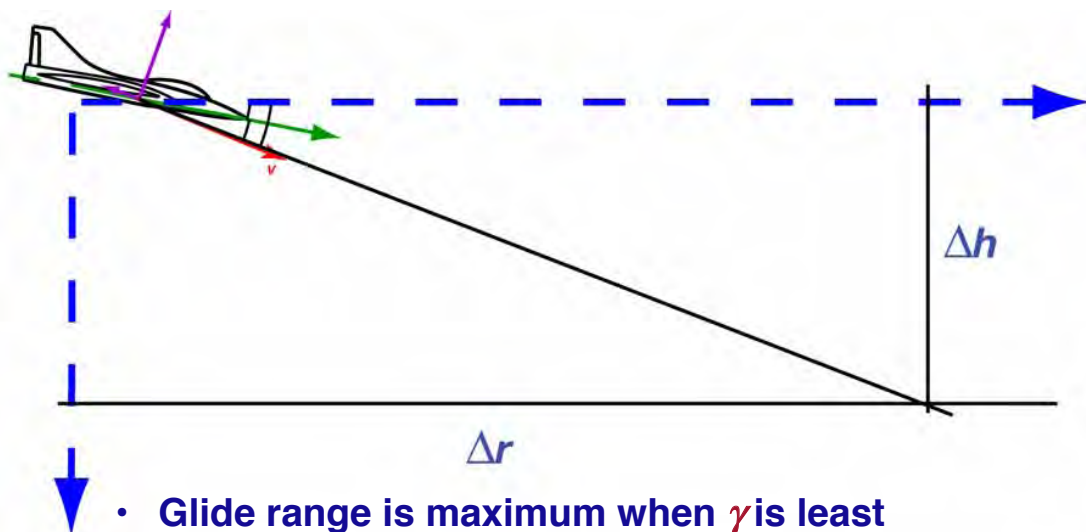
$$\tan \gamma = -\frac{D}{L} = -\frac{C_D}{C_L} = \frac{\dot{h}}{\dot{r}} = \frac{dh}{dr}; \quad \gamma = -\tan^{-1}\left(\frac{D}{L}\right) = -\cot^{-1}\left(\frac{L}{D}\right)$$

Corresponding airspeed

$$V_{glide} = \sqrt{\frac{2W}{\rho S \sqrt{C_D^2 + C_L^2}}}$$

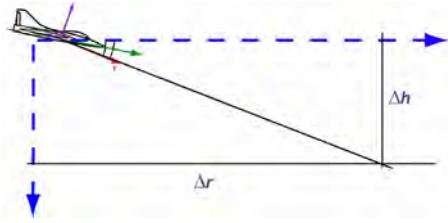
5

Maximum Steady Gliding Range



- Glide range is maximum when γ is least negative, i.e., most positive
- This occurs at $(L/D)_{max}$

6



Maximum Steady Gliding Range

- Glide range is maximum when γ is least negative, i.e., most positive
- This occurs at $(L/D)_{\max}$

$$\gamma_{\max} = -\tan^{-1}\left(\frac{D}{L}\right)_{\min} = -\cot^{-1}\left(\frac{L}{D}\right)_{\max}$$

$$\tan \gamma = \frac{\dot{h}}{\dot{r}} = \text{negative constant} = \frac{(h - h_o)}{(r - r_o)}$$

$$\Delta r = \frac{\Delta h}{\tan \gamma} = \frac{-\Delta h}{-\tan \gamma} = \text{maximum when } \frac{L}{D} = \text{maximum}$$

7

Sink Rate, m/s

- Lift and drag define γ and V in gliding equilibrium

$$D = C_D \frac{1}{2} \rho V^2 S = -W \sin \gamma$$

$$\sin \gamma = -\frac{D}{W}$$

$$L = C_L \frac{1}{2} \rho V^2 S = W \cos \gamma$$

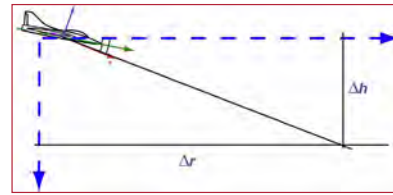
$$V = \sqrt{\frac{2W \cos \gamma}{C_L \rho S}}$$

- Sink rate = altitude rate, dh/dt (negative)

$$\begin{aligned} \dot{h} &= V \sin \gamma \\ &= -\sqrt{\frac{2W \cos \gamma}{C_L \rho S}} \left(\frac{D}{W}\right) = -\sqrt{\frac{2W \cos \gamma}{C_L \rho S}} \left(\frac{L}{W}\right) \left(\frac{D}{L}\right) \\ &= -\sqrt{\frac{2W \cos \gamma}{C_L \rho S}} \cos \gamma \left(\frac{1}{L/D}\right) \end{aligned}$$

8

Conditions for Minimum Steady Sink Rate



- Minimum sink rate provides **maximum endurance**
- Minimize sink rate by setting $\partial(dh/dt)/\partial C_L = 0$ ($\cos \gamma \sim 1$)

$$\begin{aligned}\dot{h} &= -\sqrt{\frac{2W \cos \gamma}{C_L \rho S}} \cos \gamma \left(\frac{C_D}{C_L} \right) \\ &= -\sqrt{\frac{2W \cos^3 \gamma}{\rho S}} \left(\frac{C_D}{C_L^{3/2}} \right) \approx -\sqrt{\frac{2}{\rho} \left(\frac{W}{S} \right)} \left(\frac{C_D}{C_L^{3/2}} \right)\end{aligned}$$

$$C_{L_{ME}} = \sqrt{\frac{3C_{D_o}}{\epsilon}} \quad \text{and} \quad C_{D_{ME}} = 4C_{D_o}$$

9

L/D and V_{ME} for Minimum Sink Rate

$$\left(\frac{L}{D} \right)_{ME} = \frac{1}{4} \sqrt{\frac{3}{\epsilon C_{D_o}}} = \frac{\sqrt{3}}{2} \left(\frac{L}{D} \right)_{\max} \approx 0.86 \left(\frac{L}{D} \right)_{\max}$$

$$V_{ME} = \sqrt{\frac{2W}{\rho S \sqrt{C_{D_{ME}}^2 + C_{L_{ME}}^2}}} \approx \sqrt{\frac{2(W/S)}{\rho}} \sqrt{\frac{\epsilon}{3C_{D_o}}} \approx 0.76 V_{L/D_{\max}}$$

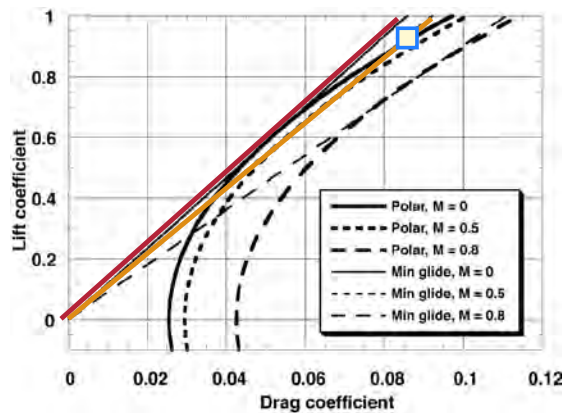
10

L/D for Minimum Sink Rate

- For $L/D < L/D_{\max}$, there are two solutions
- Which one produces smaller sink rate?

$$\left(\frac{L}{D}\right)_{ME} \approx 0.86 \left(\frac{L}{D}\right)_{\max}$$

$$V_{ME} \approx 0.76 V_{L/D_{\max}}$$



11

Checklist

- ☐ *Steady flight path angle?*
- ☐ *Corresponding airspeed?*
- ☐ *Sink rate?*
- ☐ *Maximum-range glide?*
- ☐ *Maximum-endurance glide?*

12

Historical Factoids

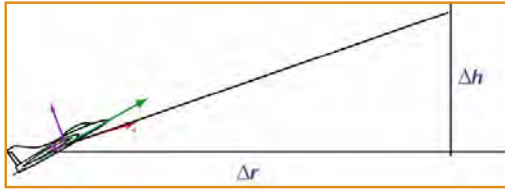
Lifting-Body Reentry Vehicles



13

Climbing Flight

14



Climbing Flight

- Flight path angle

$$\dot{V} = 0 = \frac{(T - D - W \sin \gamma)}{m}$$

$$\sin \gamma = \frac{(T - D)}{W}; \quad \gamma = \sin^{-1} \frac{(T - D)}{W}$$

- Required lift

$$\dot{\gamma} = 0 = \frac{(L - W \cos \gamma)}{mV}$$

$$L = W \cos \gamma$$

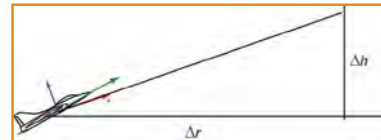
Rate of climb, dh/dt = Specific Excess Power

$$\dot{h} = V \sin \gamma = V \frac{(T - D)}{W} = \frac{(P_{thrust} - P_{drag})}{W}$$

$$\text{Specific Excess Power (SEP)} = \frac{\text{Excess Power}}{\text{Unit Weight}} \equiv \frac{(P_{thrust} - P_{drag})}{W}$$

15

Steady Rate of Climb



Climb rate

$$\dot{h} = V \sin \gamma = V \left[\left(\frac{T}{W} \right) - \frac{(C_{D_o} + \epsilon C_L^2) \bar{q}}{(W/S)} \right]$$

$$L = C_L \bar{q} S = W \cos \gamma$$

$$C_L = \left(\frac{W}{S} \right) \frac{\cos \gamma}{\bar{q}}$$

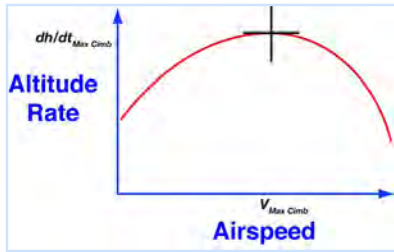
$$V = \sqrt{2 \left(\frac{W}{S} \right) \frac{\cos \gamma}{C_L \rho}}$$

Note significance of thrust-to-weight ratio and wing loading

$$\dot{h} = V \left[\left(\frac{T}{W} \right) - \frac{C_{D_o} \bar{q}}{(W/S)} - \frac{\epsilon (W/S) \cos^2 \gamma}{\bar{q}} \right]$$

$$= V \left(\frac{T(h)}{W} \right) - \frac{C_{D_o} \rho(h) V^3}{2(W/S)} - \frac{2\epsilon (W/S) \cos^2 \gamma}{\rho(h) V}$$

16



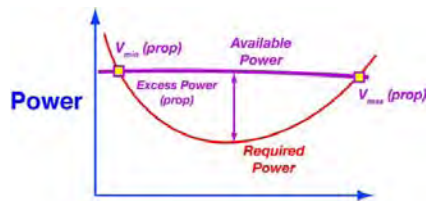
Condition for Maximum Steady Rate of Climb

$$\dot{h} = V \left(\frac{T}{W} \right) - \frac{C_{D_o} \rho V^3}{2(W/S)} - \frac{2\varepsilon (W/S) \cos^2 \gamma}{\rho V}$$

Necessary condition for a maximum with respect to airspeed

$$\frac{\partial \dot{h}}{\partial V} = 0 = \left[\left(\frac{T}{W} \right) + V \left(\frac{\partial T / \partial V}{W} \right) \right] - \frac{3C_{D_o} \rho V^2}{2(W/S)} + \frac{2\varepsilon (W/S) \cos^2 \gamma}{\rho V^2}$$

17



Maximum Steady Rate of Climb: Propeller-Driven Aircraft

True Airspeed

- **At constant power**

$$\frac{\partial P_{thrust}}{\partial V} = 0 = \left[\left(\frac{T}{W} \right) + V \left(\frac{\partial T / \partial V}{W} \right) \right]$$

- With $\cos^2 \gamma \sim 1$, optimality condition reduces to

$$\frac{\partial \dot{h}}{\partial V} = 0 = -\frac{3C_{D_o} \rho V^2}{2(W/S)} + \frac{2\varepsilon (W/S)}{\rho V^2}$$

- **Airspeed for maximum rate of climb at maximum power, P_{max}**

$$V^4 = \left(\frac{4}{3} \right) \frac{\varepsilon (W/S)^2}{C_{D_o} \rho^2}; \quad V = \sqrt{2 \frac{(W/S)}{\rho} \sqrt{\frac{\varepsilon}{3C_{D_o}}}} = V_{ME}$$

18



Maximum Steady Rate of Climb: Jet-Driven Aircraft

Condition for a maximum at constant thrust and $\cos^2 \gamma \sim 1$

$$\boxed{\frac{\partial \dot{h}}{\partial V} = 0} \quad \begin{cases} -\frac{3C_{D_o}\rho}{2(W/S)}V^4 + \left(\frac{T}{W}\right)V^2 + \frac{2\varepsilon(W/S)}{\rho} = 0 \\ -\frac{3C_{D_o}\rho}{2(W/S)}(V^2)^2 + \left(\frac{T}{W}\right)(V^2) + \frac{2\varepsilon(W/S)}{\rho} = 0 \end{cases}$$

Quadratic in V^2

Airspeed for maximum rate of climb at maximum thrust, T_{max}

$$\boxed{0 = ax^2 + bx + c \text{ and } V = +\sqrt{x}}$$

19

Checklist

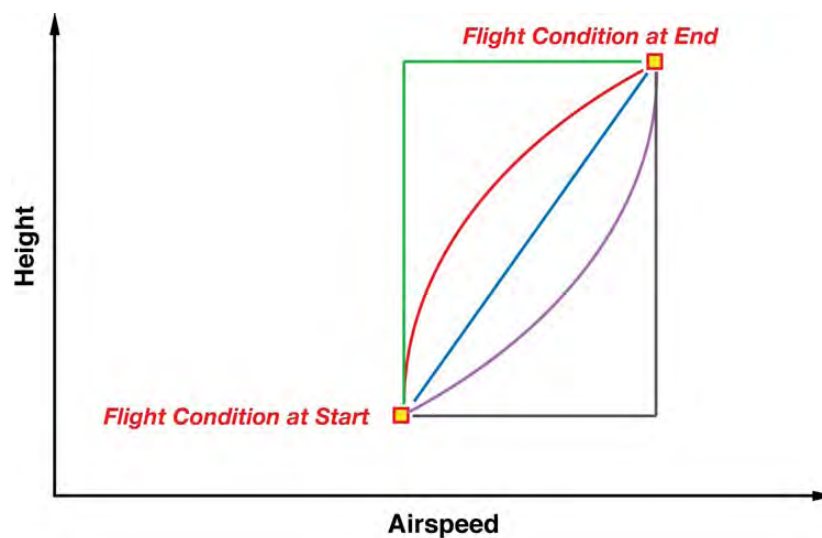
- ☐ Specific excess power?
- ☐ Maximum steady rate of climb?
- ☐ Velocity for maximum climb rate?

20

Optimal Climbing Flight

21

**What is the Fastest Way to Climb
from One Flight Condition to
Another?**



22

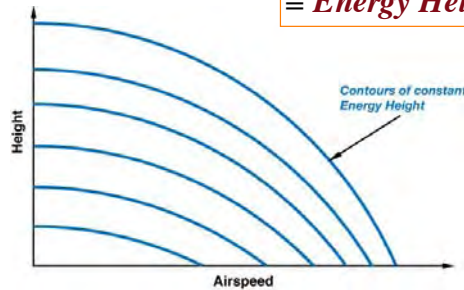
Energy Height

- **Specific Energy**
 - = (Potential + Kinetic Energy) per Unit Weight
 - = Energy Height

$$\frac{\text{Total Energy}}{\text{Unit Weight}} \equiv \text{Specific Energy}$$

$$= \frac{mgh + mV^2/2}{mg} = h + \frac{V^2}{2g}$$

$$\equiv \text{Energy Height}, E_h, \text{ ft or m}$$



Can trade altitude for airspeed with no change in energy height if thrust and drag are zero

23

Specific Excess Power

Rate of change of Specific Energy

$$\frac{dE_h}{dt} = \frac{d}{dt} \left(h + \frac{V^2}{2g} \right) = \frac{dh}{dt} + \left(\frac{V}{g} \right) \frac{dV}{dt}$$

$$= V \sin \gamma + \left(\frac{V}{g} \right) \left(\frac{T - D - mg \sin \gamma}{m} \right) = V \frac{(T - D)}{W}$$

$$= \text{Specific Excess Power (SEP)}$$

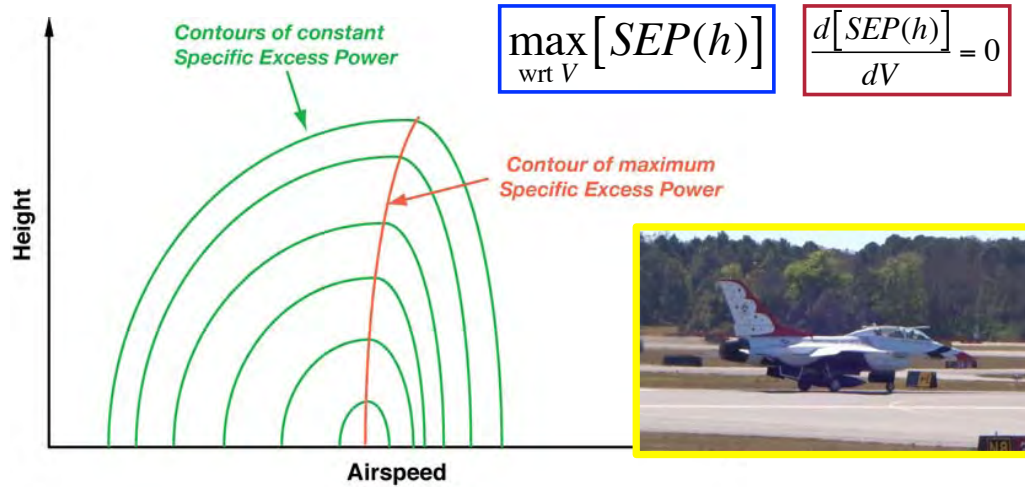
$$= \frac{\text{Excess Power}}{\text{Unit Weight}} \equiv \frac{(P_{\text{thrust}} - P_{\text{drag}})}{W}$$

$$= V \frac{(C_T - C_D) \frac{1}{2} \rho(h) V^2 S}{W}$$

24

Contours of Constant Specific Excess Power

- Specific Excess Power is a function of altitude and airspeed
- **SEP** is maximized at each altitude, h , when

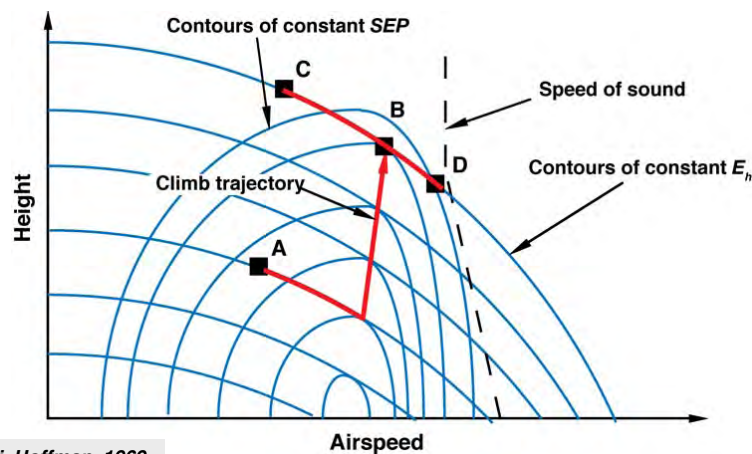


25

Subsonic Minimum-Time Energy Climb

Objective: Minimize time to climb to desired altitude and airspeed

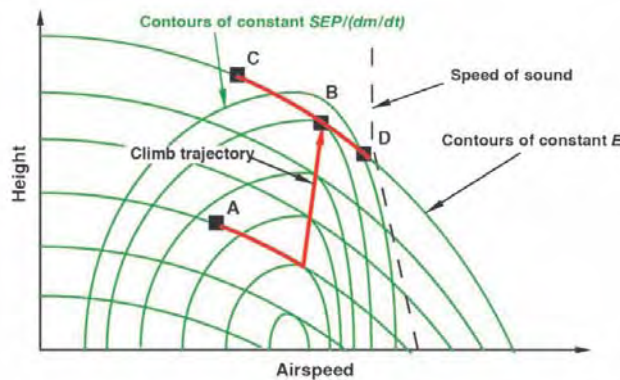
- **Minimum-Time Strategy:**
 - Zoom climb/dive to intercept $SEP_{\max}(h)$ contour
 - Climb at $SEP_{\max}(h)$
 - Zoom climb/dive to intercept target $SEP_{\max}(h)$ contour



26

Subsonic Minimum-Fuel Energy Climb

Objective: Minimize fuel to climb to desired altitude and airspeed



- **Minimum-Fuel Strategy:**
 - Zoom climb/dive to intercept $[SEP(h)/(dm/dt)]_{\max}$ contour
 - Climb at $[SEP(h)/(dm/dt)]_{\max}$
 - Zoom climb/dive to intercept target $[SEP(h)/(dm/dt)]_{\max}$ contour

Bryson, Desai, Hoffman, 1969

27

Supersonic Minimum-Time Energy Climb

Objective: Minimize time to climb to desired altitude and airspeed

- **Minimum-Time Strategy:**
 - Intercept subsonic $SEP_{\max}(h)$ contour
 - Climb at $SEP_{\max}(h)$ to intercept matching zoom climb/dive contour
 - Zoom climb/dive to intercept supersonic $SEP_{\max}(h)$ contour
 - Climb at $SEP_{\max}(h)$ to intercept target $SEP_{\max}(h)$ contour
 - Zoom climb/dive to intercept target $SEP_{\max}(h)$ contour

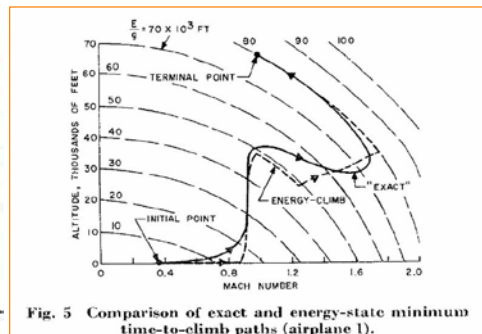
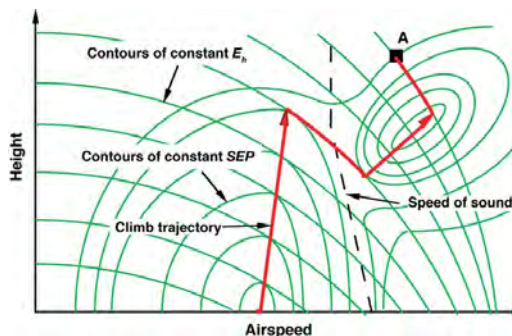


Fig. 5 Comparison of exact and energy-state minimum time-to-climb paths (airplane 1).

Bryson, Desai, Hoffman, 1969

28

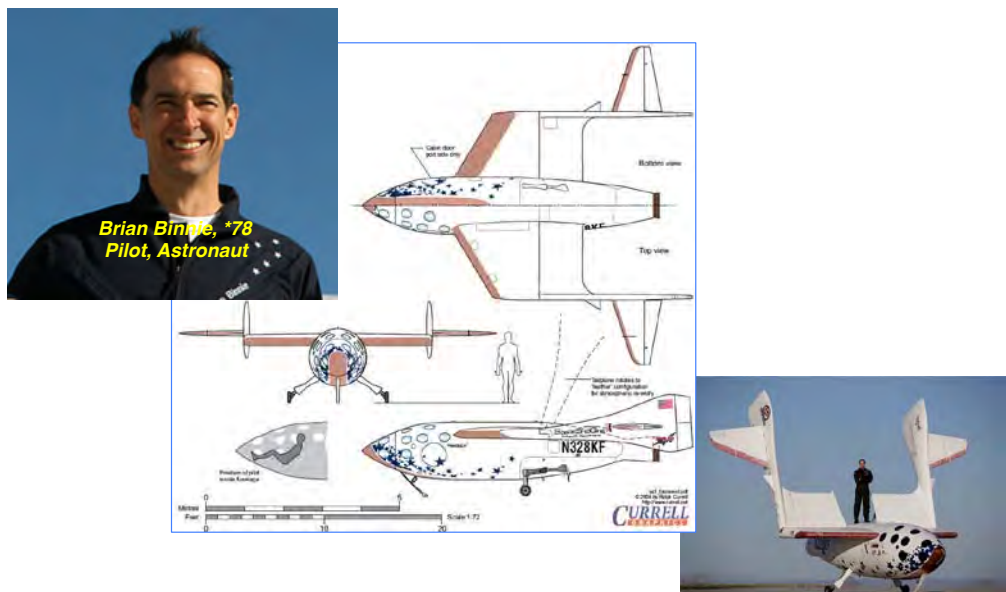
Checklist

- ☐ *Energy height?*
- ☐ *Contours?*
- ☐ *Subsonic minimum-time climb?*
- ☐ *Supersonic minimum-time climb?*
- ☐ *Minimum-fuel climb?*

$$\frac{dE_h}{dm_{fuel}} = \frac{dE_h}{dt} \frac{dt}{dm_{fuel}} = \frac{1}{\dot{m}_{fuel}} \left[\frac{dh}{dt} + \left(\frac{V}{g} \right) \frac{dV}{dt} \right]$$

29

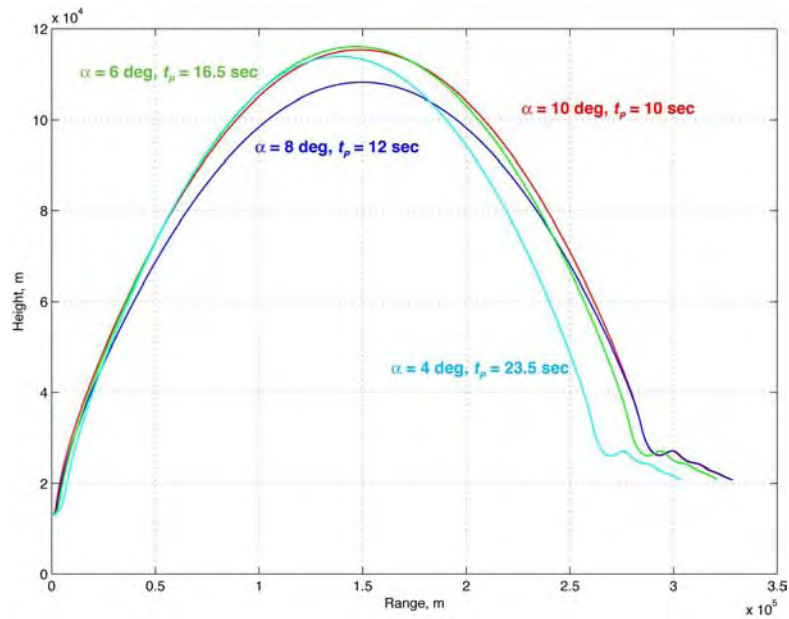
SpaceShipOne Ansari X Prize, December 17, 2003



30

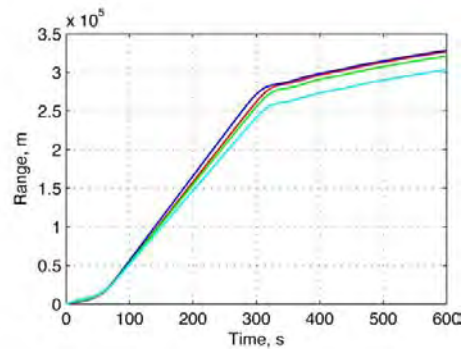
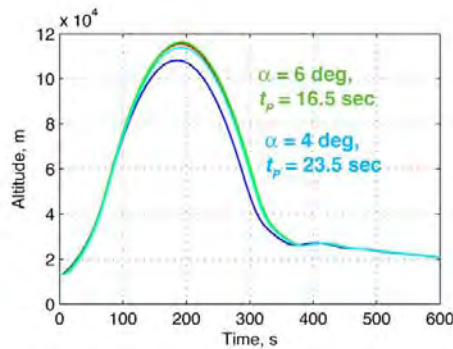
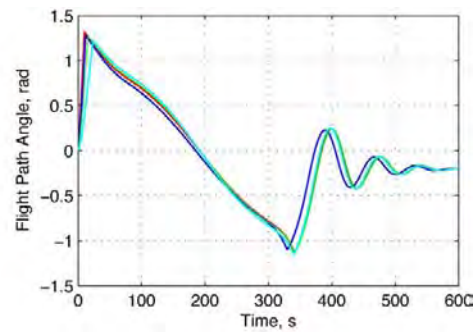
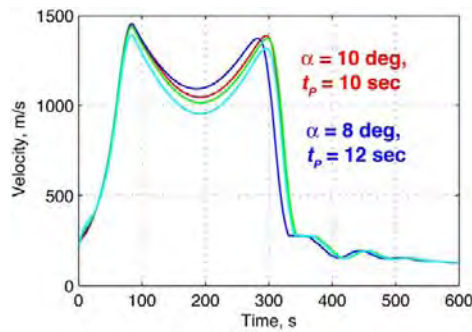
SpaceShipOne Altitude vs. Range

MAE 331 Assignment #4, 2010



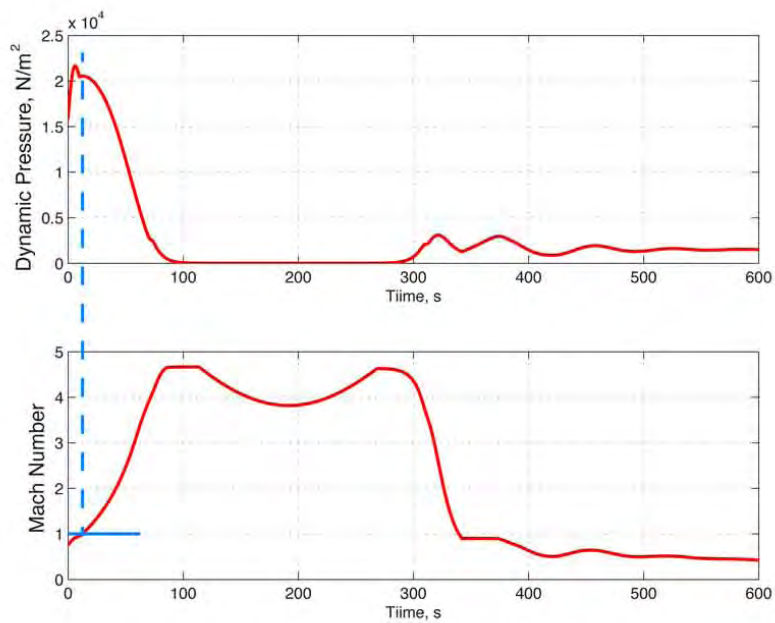
31

SpaceShipOne State Histories



32

SpaceShipOne Dynamic Pressure and Mach Number Histories



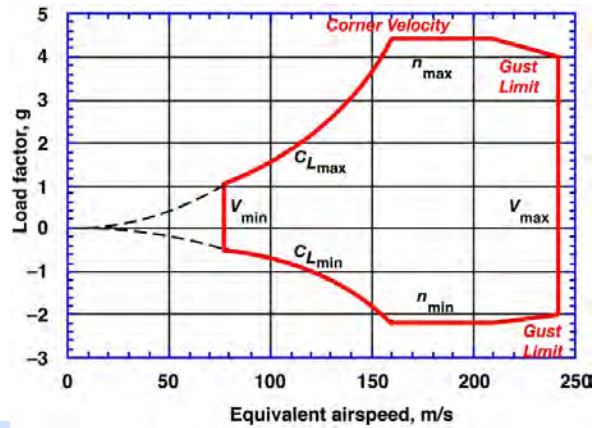
33

The Maneuvering Envelope

34

Typical Maneuvering Envelope: V-n Diagram

- **Maneuvering envelope:** limits on normal load factor and allowable equivalent airspeed
 - Structural factors
 - Maximum and minimum achievable lift coefficients
 - Maximum and minimum airspeeds
 - Protection against overstressing due to gusts
 - **Corner Velocity:** Intersection of maximum lift coefficient and maximum load factor



- **Typical positive load factor limits**

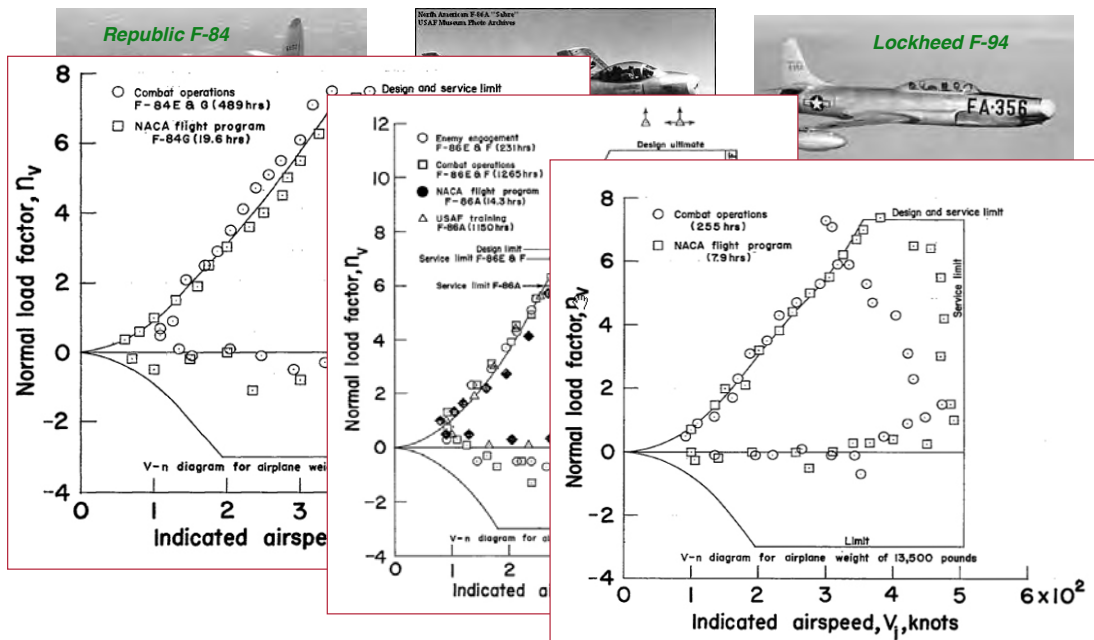
- Transport: > 2.5
- Utility: > 4.4
- Aerobatic: > 6.3
- Fighter: > 9

- **Typical negative load factor limits**

- Transport: < -1
- Others: < -1 to -3

35

Maneuvering Envelopes (*V-n Diagrams*) for Three Fighters of the Korean War Era



36

Turning Flight

37

Level Turning Flight

- Level flight = constant altitude
- Sideslip angle = 0
- Vertical force equilibrium

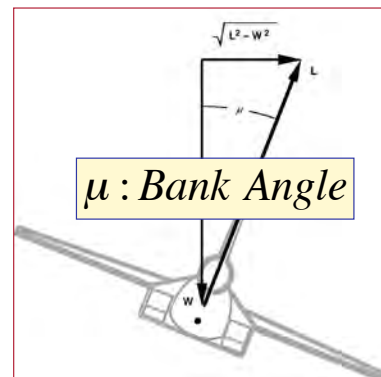
$$L \cos \mu = W$$

- Load factor

$$n = \frac{L}{W} = \frac{L}{mg} = \sec \mu, "g"s$$

- Thrust required to maintain level flight

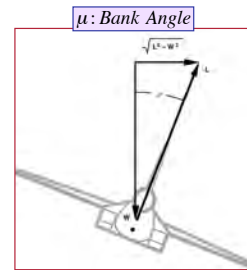
$$\begin{aligned} T_{req} &= \left(C_{D_o} + \epsilon C_L^2 \right) \frac{1}{2} \rho V^2 S = D_o + \frac{2\epsilon}{\rho V^2 S} \left(\frac{W}{\cos \mu} \right)^2 \\ &= D_o + \frac{2\epsilon}{\rho V^2 S} (nW)^2 \end{aligned}$$



38

Maximum Bank Angle in Steady Level Flight

Bank angle



$$\begin{aligned}\cos \mu &= \frac{W}{C_L \bar{q} S} \\ &= \frac{1}{n} \\ &= W \sqrt{\frac{2\varepsilon}{(T_{req} - D_o) \rho V^2 S}}\end{aligned}$$

$$\begin{aligned}\mu &= \cos^{-1} \left(\frac{W}{C_L \bar{q} S} \right) \\ &= \cos^{-1} \left(\frac{1}{n} \right) \\ &= \cos^{-1} \left[W \sqrt{\frac{2\varepsilon}{(T_{req} - D_o) \rho V^2 S}} \right]\end{aligned}$$

Bank angle is limited by

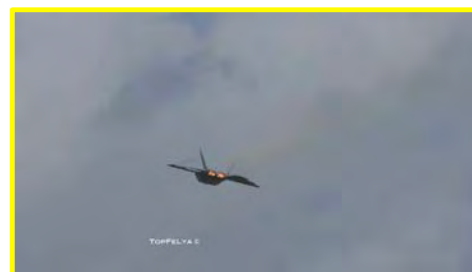
$$C_{L_{\max}} \text{ or } T_{\max} \text{ or } n_{\max}$$

39

Turning Rate and Radius in Level Flight

Turning rate

$$\begin{aligned}\dot{\xi} &= \frac{C_L \bar{q} S \sin \mu}{mV} \\ &= \frac{W \tan \mu}{mV} \\ &= \frac{g \tan \mu}{V} \\ &= \frac{\sqrt{L^2 - W^2}}{mV} \\ &= \frac{W \sqrt{n^2 - 1}}{mV} \\ &= \frac{\sqrt{(T_{req} - D_o) \rho V^2 S / 2\varepsilon - W^2}}{mV}\end{aligned}$$



Turning rate is limited by

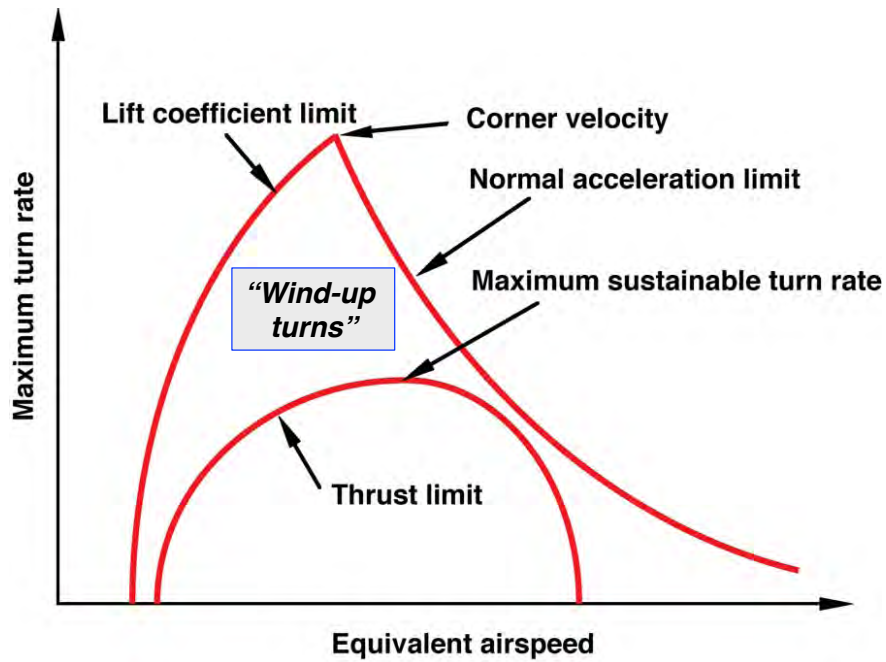
$$C_{L_{\max}} \text{ or } T_{\max} \text{ or } n_{\max}$$

Turning radius

$$R_{turn} = \frac{V}{\dot{\xi}} = \frac{V^2}{g \sqrt{n^2 - 1}}$$

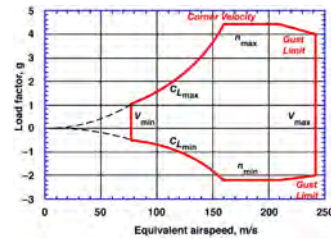
40

Maximum Turn Rates



41

Corner Velocity Turn



- Corner velocity

$$V_{corner} = \sqrt{\frac{2n_{max}W}{C_{L_{max}}\rho S}}$$

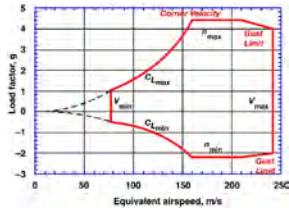
- For steady climbing or diving flight

$$\sin \gamma = \frac{T_{max} - D}{W}$$

- Turning radius

$$R_{turn} = \frac{V^2 \cos^2 \gamma}{g \sqrt{n_{max}^2 - \cos^2 \gamma}}$$

42



Corner Velocity Turn

- Turning rate
- Time to complete a full circle
- Altitude gain/loss

$$\dot{\xi} = \sqrt{\frac{g(n_{\max}^2 - \cos^2 \gamma)}{V \cos \gamma}}$$

$$t_{2\pi} = \frac{V \cos \gamma}{g \sqrt{n_{\max}^2 - \cos^2 \gamma}}$$

$$\Delta h_{2\pi} = t_{2\pi} V \sin \gamma$$

43

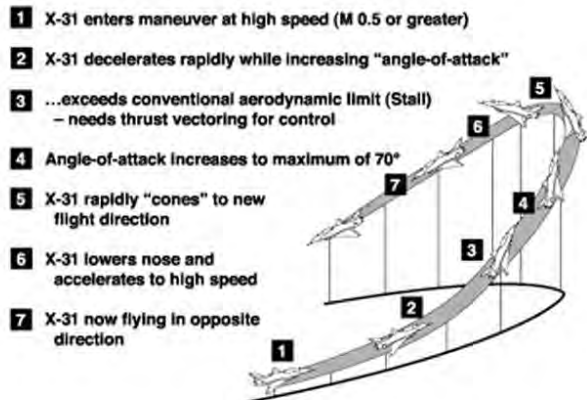
Checklist

- ☐ V-n diagram?
- ☐ Maneuvering envelope?
- ☐ Level turning flight?
- ☐ Limiting factors?
- ☐ Wind-up turn?
- ☐ Corner velocity?

44

Herbst Maneuver

- Minimum-time reversal of direction
- Kinetic-/potential-energy exchange
- Yaw maneuver at low airspeed
- X-31 performing the maneuver



45

Next Time: Aircraft Equations of Motion

Reading:
Flight Dynamics,
Section 3.1, 3.2, pp. 155–161

Learning Objectives

- What use are the equations of motion?*
- How is the angular orientation of the airplane described?*
- What is a cross-product-equivalent matrix?*
- What is angular momentum?*
- How are the inertial properties of the airplane described?*
- How is the rate of change of angular momentum calculated?*

46

Supplemental Material

47

Gliding Flight of the P-51 Mustang



Maximum Range Glide

Loaded Weight = 9,200 lb (3,465 kg)

$$(L/D)_{\max} = \frac{1}{2\sqrt{\epsilon C_{D_o}}} = 16.31$$

$$\gamma_{MR} = -\cot^{-1}\left(\frac{L}{D}\right)_{\max} = -\cot^{-1}(16.3) = -3.5^\circ$$

$$(C_D)_{L/D_{\max}} = 2C_{D_o} = 0.0326$$

$$(C_L)_{L/D_{\max}} = \sqrt{\frac{C_{D_o}}{\epsilon}} = 0.531$$

$$V_{L/D_{\max}} = \frac{76.49}{\sqrt{\rho}} \text{ m/s}$$

$$\dot{h}_{L/D_{\max}} = V \sin \gamma = -\frac{4.68}{\sqrt{\rho}} \text{ m/s}$$

$$R_{h_o=10 \text{ km}} = (16.31)(10) = 163.1 \text{ km}$$

Maximum Endurance Glide

Loaded Weight = 9,200 lb (3,465 kg)

$$S = 21.83 \text{ m}^2$$

$$C_{D_{ME}} = 4C_{D_o} = 4(0.0163) = 0.0652$$

$$C_{L_{ME}} = \sqrt{\frac{3C_{D_o}}{\epsilon}} = \sqrt{\frac{3(0.0163)}{0.0576}} = 0.921$$

$$(L/D)_{ME} = 14.13$$

$$\dot{h}_{ME} = -\sqrt{\frac{2}{\rho} \left(\frac{W}{S} \right)} \left(\frac{C_{D_{ME}}}{C_{L_{ME}}^{3/2}} \right) = -\frac{4.11}{\sqrt{\rho}} \text{ m/s}$$

$$\gamma_{ME} = -4.05^\circ$$

$$V_{ME} = \frac{58.12}{\sqrt{\rho}} \text{ m/s}$$

48