

MECHANICS OF DEFORMABLE BODIES

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LECTURE 14

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Introduction

Mechanical properties of materials

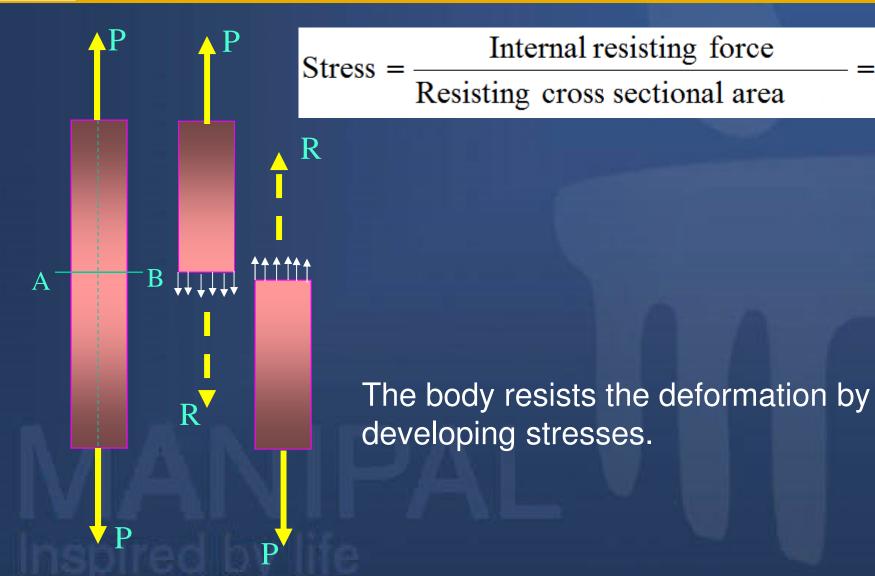
Normal stress and strain

Hooke's law

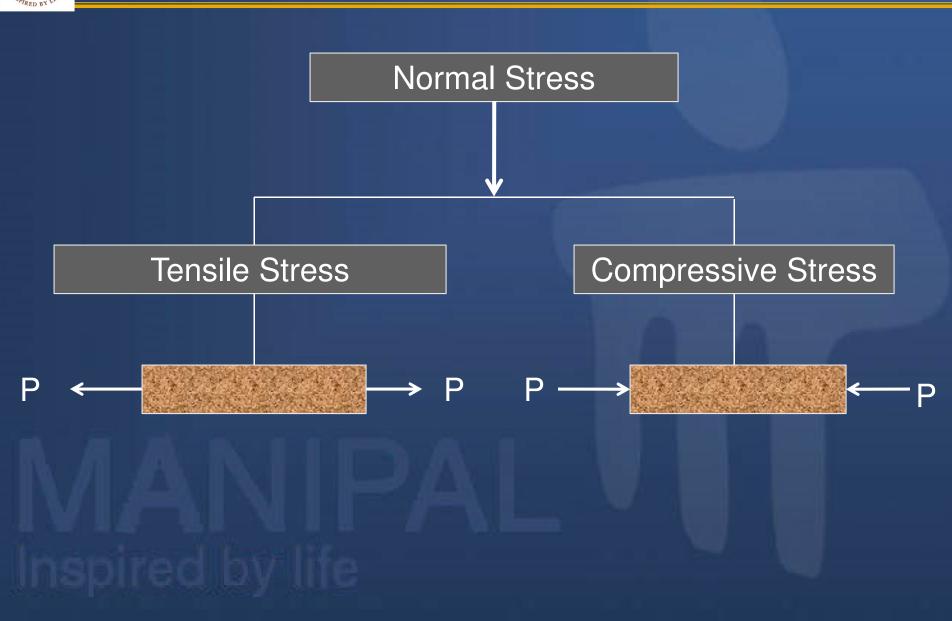
Modulus of elasticity

HOME

Normal stress







SI unit for stress is Pascal (Pa)

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	= 八	\mathbb{N}/\mathbb{I}	

	N/m ²	N/mm ²
1kPa	10^3	10-3
1MPa	10^{6}	1
1GPa	109	10^3

Kilopascal, 1kPa= 1000 N/m²

Megapascal, $1MPa = 1x 10^6 \text{ N/m}^2$

$$= 1 \times 10^6 \text{ N/} (10^6 \text{ mm}^2) = 1 \text{ N/mm}^2$$

$$1MPa = 1 N/mm^2$$

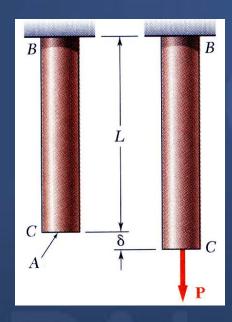
Gigapascal, $1GPa = 1 \times 10^9 \text{ N/m}^2$

$$= 1x 10^3 MPa$$

$$=1x 10^3 \text{ N/mm}^2$$

STRAIN

$$\varepsilon = \frac{\delta L}{L} = \frac{\text{Change in the length}}{\text{Original length}}$$



$$\sigma = \frac{P}{A} = \text{stress}$$

$$\varepsilon = \frac{\delta}{L} = \text{Linear strain}$$

Hooks law and Modulus of elasticity

Hooks law:

$$\frac{Stress(\sigma)}{Strain(\varepsilon)} = \text{constant}$$

Modulus of elasticity:

$$\frac{Stress(\sigma)}{Strain(\varepsilon)} = \frac{PL}{Adl}$$



The following table shows modulus of elasticity of important materials:

Material	Modulus of elasticity
Steel	210 GPa
Aluminium	73Gpa
Brass	96 – 110 GPa
Cast Iron	83 – 170 GPa
Concrete	17 – 31 GPa
Rubber	0.0007 – 0.004 GPa
Tungsten	340 – 380 GPa



Tension test on ductile and brittle material Factor of safety
Allowable stress

<u>HOME</u>

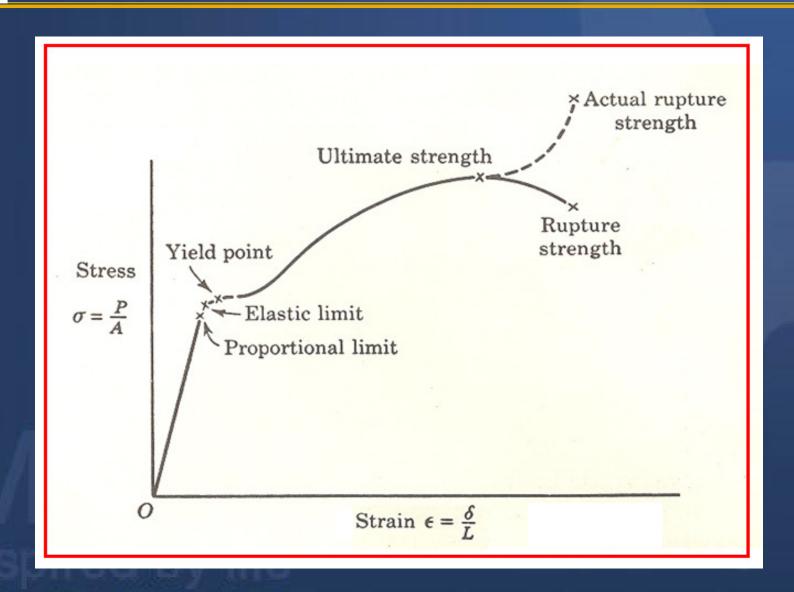


Tension test on ductile and brittle material





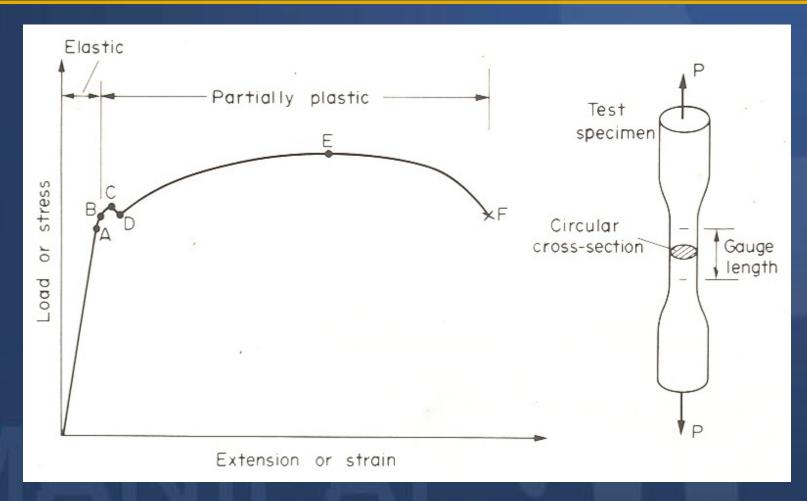
STRESS-STRAIN DIAGRAM



Typical tensile test curve for mild steel



STRESS-STRAIN DIAGRAM



Typical tensile test curve for mild steel showing upper yield point and lower yield point and also the elastic range and plastic range

Elastic limit:

Limit of Proportionality:
$$\sigma_P = \frac{\text{Load at proportionality limit}}{\text{Original crosssectional area}} = \frac{P_P}{A}$$

$$\sigma_E = \frac{\text{Load at elatic limit}}{\text{Original cross sectional area}} = \frac{P_E}{A}$$

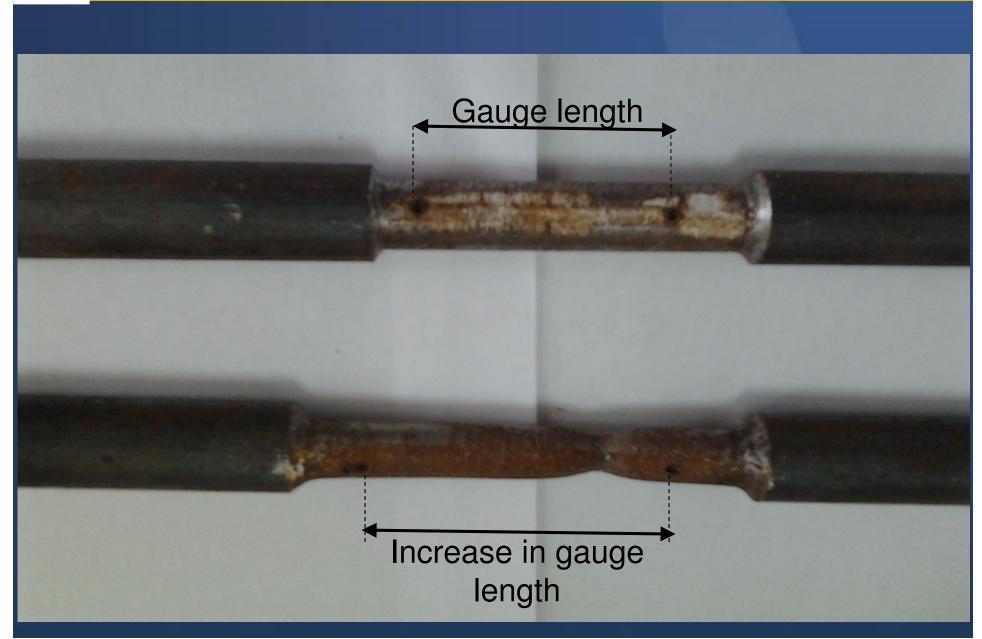
Yield point:
$$\sigma_{\gamma} = \frac{\text{Load at yield point}}{\text{Original cross sectional area}} = \frac{P_{\gamma}}{A}$$

Ultimate strength:
$$\sigma_U = \frac{\text{Maximum load taken by the material}}{\text{Original cross sectional area}} = \frac{P_U}{A}$$

Rupture strength (Nominal Breaking stress):
$$\sigma_B = \frac{\text{Load at failure}}{\text{Original cross sectional area}} = \frac{P_B}{A}$$

True breaking stress:
$$\sigma_B = \frac{\text{Load at failure}}{\text{Actual cross sectional area}} = \frac{P_B}{A}$$







Ductile Materials

Percentage elongation
Percentage reduction in area

Measures of ductility

Cup and cone fracture for a Ductile Material



Percentage elongation = $\frac{\text{Increase in the gauge length (upto fracture)}}{\text{Original gauge length}} \times 100$

Percentage reduction in area = $\frac{\text{Reduction in cross sectional area of neck portion (at fracture)}}{\text{Original cross sectional area}} \times 100$

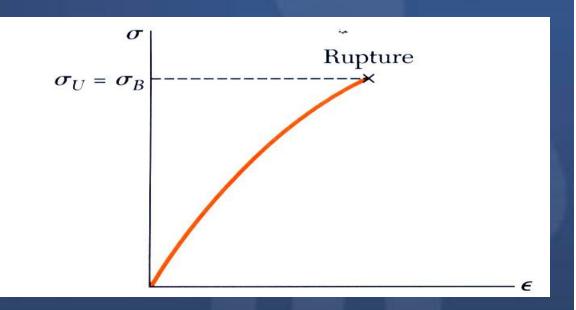
Example: Low carbon steel, mild steel, gold, silver, aluminum



Stress-strain Diagram

Brittle Materials:





Stress-strain diagram for a typical brittle material



Working stress & Factor of safety

Ductile Material:

Working stress = Yield Stress / Factor of Safety

Brittle Material:

Working stress = Ultimate Stress / Factor of Safety

Factor of Safety = Maximum stress / Allowable working stress



LECTURE 16

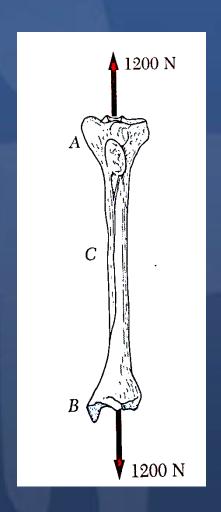
Contents:

Numerical problems

НС



N1. A strain gauge located at C on the surface of bone AB indicates that the average normal stress in the bone is 3.80 MPa when the bone is subjected to two 1200 N forces as shown. Assuming the cross section of the bone at C to be annular and Knowing that its outer diameter is 25mm, determine the inner diameter of the bones cross section at C.



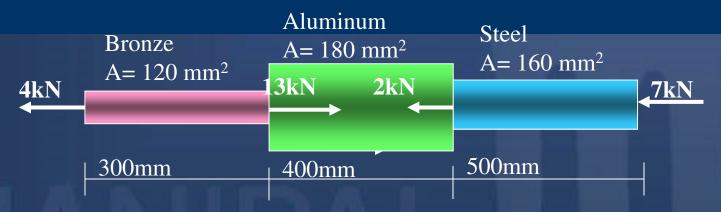
$$A = \frac{\pi}{4} \left(\frac{d^2 - d^2}{\pi} \right)$$

$$d^2 = d^2 - \frac{4A}{\pi}$$





N2 A composite bar consists of an aluminum section rigidly fastened between a bronze section and a steel section as shown in figure. Axial loads are applied at the positions indicated. Determine the stress in each section. Also determine the change in each section and the change in total length.





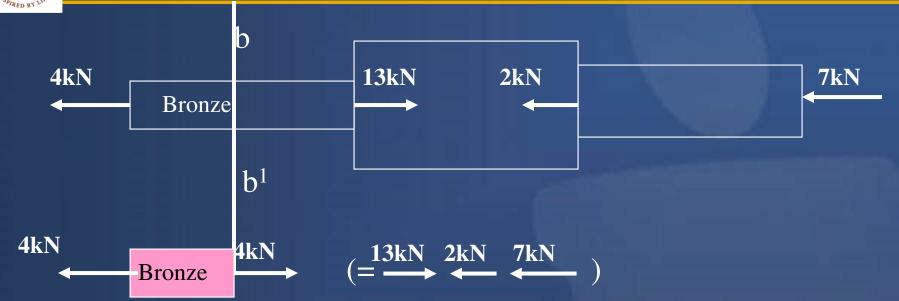
To calculate the stresses, first determine the forces in each section.

To find the Force in bronze section, consider a section bb¹ as shown in the figure



For equilibrium condition algebraic sum of forces on LHS of the section must be equal to that of RHS





Force acting on Bronze section is 4kN, tensile

Stress in Bronze section =

Force in Bronze section

Resisting cross sectional area of the Bronze section

$$= \frac{4kN}{120mm^2} = \frac{4 \times 1000N}{120mm^2} = 33.33N / mm^2 = 33.33MPa$$

(Tensile stress)



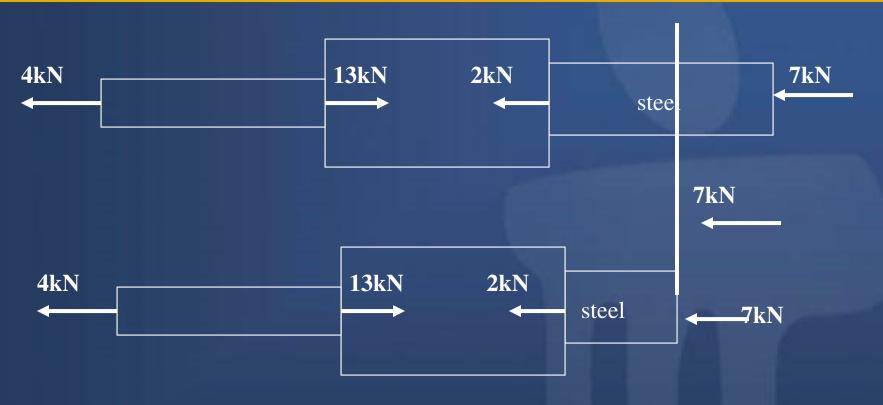
Force in Aluminum section



Force acting on Aluminum section is 9kN, (Compressive)



Force in steel section



Force acting on Steel section is 7kN, (Compressive)



Stress in Aluminum section

Force in Al section

Resisting cross sectional area of the Al section

$$= \frac{9kN}{180mm^2} = \frac{9 \times 1000N}{180mm^2} = 50N / mm^2 = 50MPa$$

Compressive stress

Stress in Steel section =

Force in Steel section

Resisting cross sectional area of the Steel section

$$= \frac{7kN}{160mm^2} = \frac{7 \times 1000N}{160mm^2} = 43.75N / mm^2 = 43.75MPa$$

(Compressive stress)



we know that,

$$P_{br} = +4kN$$
 (Tension)

$$P_{al} = -9kN$$
 (Compression)

$$P_{st} = -7kN$$
 (Compression)

Deformation due to compressive force is shortening in length, and is considered as -ve

$$E = \frac{\text{stress}(\sigma)}{\text{strain}(\varepsilon)} = \frac{PL}{A \delta L}$$

Change in length =
$$\delta L = \frac{PL}{AE}$$

$$\delta L_{br} = \frac{4000N \times 300mm}{120mm^2 \times 100 \times 10^3 (N / mm^2)}$$

= 0.1 mm



Change in length of aluminum section =
$$\delta L_{al} = \frac{-9000N \times 400mm}{180mm^2 \times 70 \times 10^3 (N/mm^2)} = -0.286mm$$

gth of

$$= \delta L_{st} = \frac{-7000N \times 500mm}{160mm^2 \times 200 \times 10^3 (N/mm^2)} = -0.109mm$$

$$= \delta L_{br} + \delta L_{al} + \delta L_{st} = +0.1 - 0.286 - 0.109$$

= -0.295mm

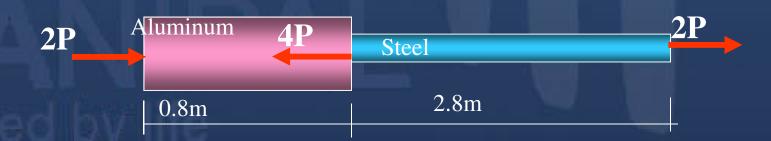


N3. An aluminum rod is fastened to a steel rod as shown. Axial loads are applied at the positions shown. The area of cross section of aluminum and steel rods are 600mm² and 300mm² respectively. Find maximum value of P that will satisfy the following conditions.

a) $\sigma_{st} \le 140 \text{ MPa}$ b) $\sigma_{al} \le 80 \text{ MPa}$

c)Total elongation ≤ 1mm,

Take
$$E_{al} = 70$$
GPa,
 $E_{st} = 200$ GPa





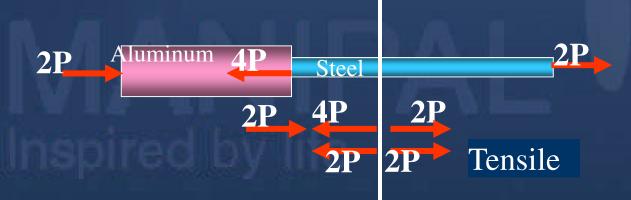
To find P, based on the condition, $\sigma_{st} \leq 140 \text{ MPa}$

Stress in steel must be less than or equal to 140MPa.

Hence,
$$\sigma_{st}$$
 =
$$= 140 \text{MPa}$$

$$= \frac{P_{st}}{A_{st}} = \frac{2P}{A_{st}} = 140 N / mm^2$$

$$P = \frac{140 \times A_{st}}{2} = 21000N = 21kN$$





To find P, based on the condition, $\sigma_{al} \leq 80 \text{ MPa}$

Stress in aluminum must be less than or equal to 80MPa.

Hence,
$$\sigma_{al} = 80\text{MPa} = \frac{P_{al}}{A_{al}} = \frac{2P}{A_{al}} = 80N / mm^2$$

$$P = \frac{80 \times A_{al}}{2} = 24000N = 24kN$$

2P Aluminum 4P Steel
2P 4P 2P
2P Compressive



To find P, based on the condition, total elongation ≤ 1mm

Total elongation = elongation in aluminum + elongation in steel.

$$1 \text{mm} = \left(\frac{PL}{AE}\right)_{al} + \left(\frac{PL}{AE}\right)_{st}$$

$$1 \text{mm} = \left(\frac{-2PL_{al}}{A_{al}E_{al}}\right) + \left(\frac{+2PL_{st}}{A_{st}E_{st}}\right)$$

$$1 \text{mm} = \left(\frac{-2P \times 800}{600 \times 70 \times 10^{3}}\right) + \left(\frac{+2P \times 2800}{300 \times 200 \times 10^{3}}\right)$$

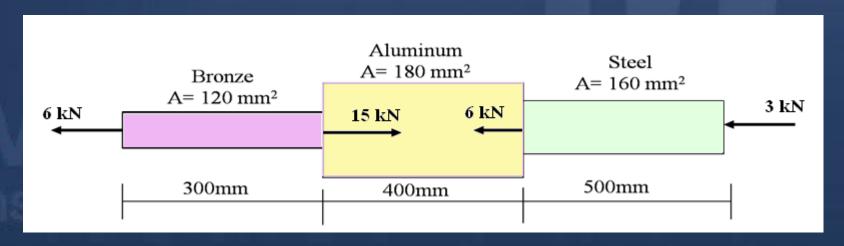
$$P = 18.1 \text{kN}$$

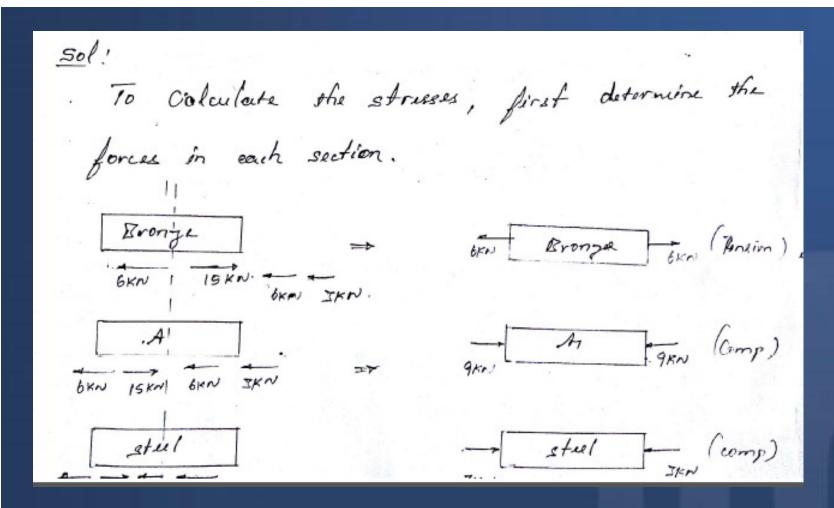
Ans: P = 18.1kN (minimum of the three values)



N4. A composite bar consists of an aluminum section rigidly fastened between a bronze section and a steel section as shown in figure. Axial loads are applied at the positions indicated. Determine the stress in each section. Also determine the change in each section and the change in total length.

Given
$$E_b = 100 \text{ GPa}$$
, $E_a = 70 \text{ GPa}$, $E_s = 200 \text{ GPa}$





NANIPAL V Inspired by life

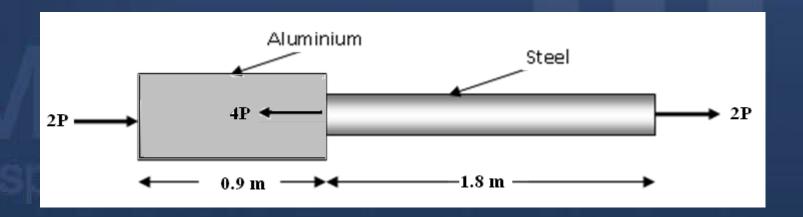
struce in bronge section !-= Force in bronze section als area (resulting) = 6x103 = 50 N/mm2 (T) stress in Alluminium section: = Force in alluminium section = 9x10 = 50 N/mm2 (c) struck in steel 3/n = Force in stul sin cls ona = 3×10 = 18.75 N/mm? (c)

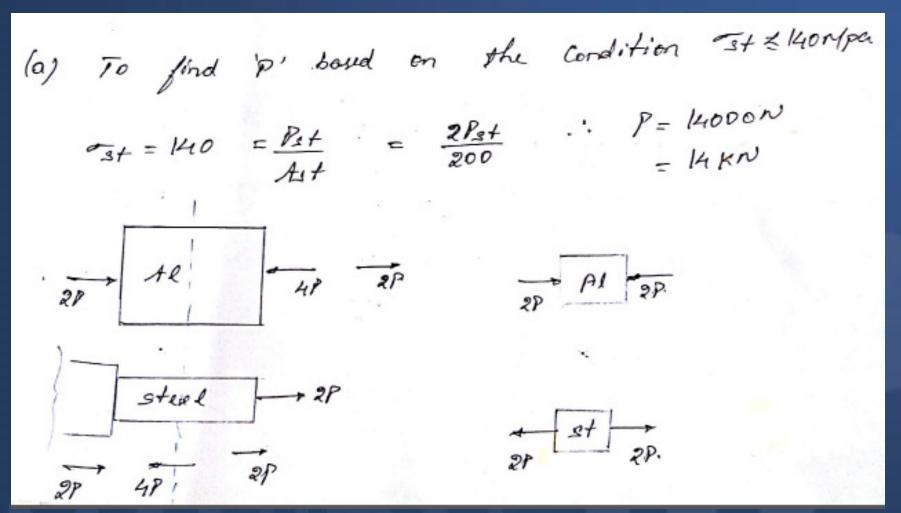
. change in longth d = PHAE change in length of bronze of = [20x100 1105 = 0.15mm (+) Change in longth of Alleminium = -9000 x400 =-0.286 mm change in length of stud = -3000 x500 = -0.469 mm Total change in longth = 0.15 -0.286 -0.469 = -0.605 mm - DARE mm [chartering)



N5. An aluminum rod is fastened to a steel rod as shown. Axial loads are applied at the positions shown. The area of cross section of aluminum and steel rods are 400 mm² and 200mm² respectively. Find maximum value of P that will satisfy the following conditions.

- a) $\sigma_s \leq 140 \text{ MPa}$
- b) $\sigma_a \leq 80 \text{ MPa}$
- c) Total elongation ≤ 0.5 mm, Take $E_a = 70$ GPa and $E_s = 210$ GPa





$$0.5 = \frac{-2P \times 900}{400 \times 40 \times 10^{3}} + \frac{2P \times 1800}{200 \times 210 \times 10^{3}}$$

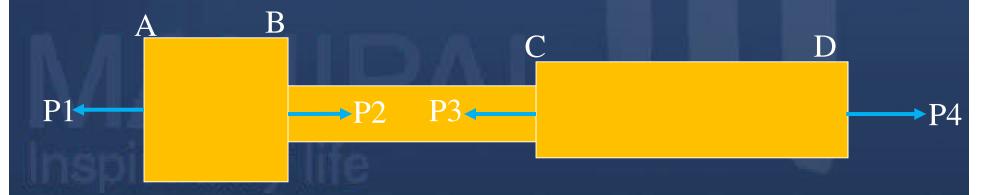


N6. A member ABCD is subjected to point loads P1, P2,P3 and P4 as shown in figure below.

Calculate the force P3 necessary for equilibrium if P1 = 120 kN, P2 = 220 kN and P4 = 160 kN.

Determine the net change in the length of the member. Take $E = 200 \text{ GN/m}^2$.

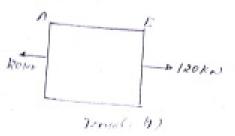
Given: area and length of AB: 1600 mm², 0.75 m; area and length of BC: 625 mm², 1.0 m; area and length of CD: 900mm², 1.2 m.

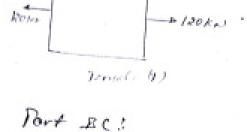


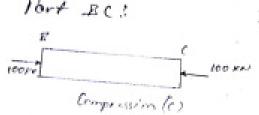
20 lu! value of P3 recusory for equilibrium! Equate the forces acting towards right to thou

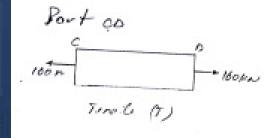
acting towards left P. + P2 = B+ P4 120+ P3 = 220+160 Pg = 260 km

Applying method of sections. Port AE:

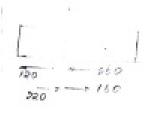


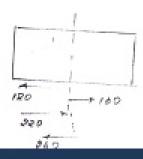












Not change in length of = Increase in longth of AFF + decrease in length of EC + Increase in length of 00 derest - dlas + desc + deco = Pih - Rhe + Pihs = 180×10 × 7450 - 100×10 + 160×10 × 1000 + 160×100 × 1000 = +0-28 -0.8 +1.07 = -0.55mm

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LECTURE 17

Contents:

Expression for deformation of a tapered bar

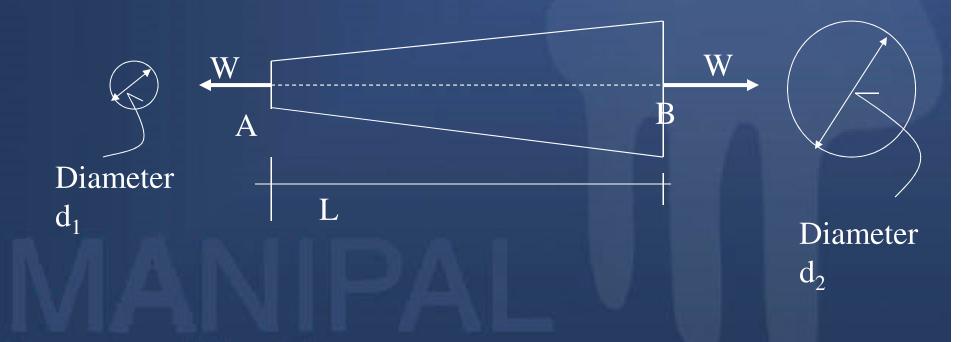
Expression for deformation of a tapered flat

Application problems

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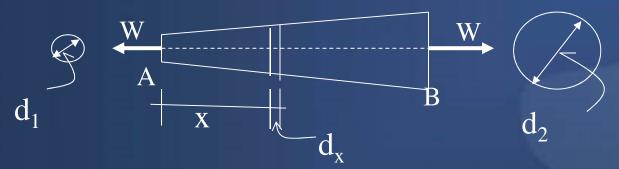


Derive an expression for the total extension of the tapered bar of circular cross section shown in the figure, when subjected to an axial tensile load, W





Consider an element of length, δx at a distance x from A



Diameter at
$$x$$
, $= d_1 + \frac{(d_2 - d_1)}{L} \times x$ c/s area at x , $= \frac{\pi d_1^2}{4} = \frac{\pi}{4} (d_1 + kx)^2$
 $= d_1 + k \times x$

Change in length over a $= \left(\frac{PL}{AE}\right)_{dx} = \left[\frac{Wdx}{\frac{\pi}{4}(d_1 + kx)^2 \times E}\right]$

Change in length over a length L is

$$= \int_0^L \left(\frac{Wdx}{\frac{\pi}{4} (d_1 + kx)^2 \times E} \right)$$



Consider an element of length, δx at a distance x from A

Change in length over a length L is

$$= \int_0^L \left(\frac{Wdx}{\frac{\pi}{4} (d_1 + kx)^2 \times E} \right)$$

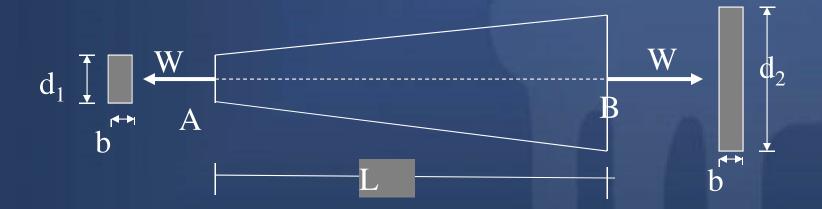
$$= \int_0^L \left(\frac{W \frac{dt}{k}}{\frac{\pi}{4} (t)^2 \times E} \right)$$
 Put $d_1 + kx = t$,
Then $k dx = dt$

$$= \frac{4W}{\pi E k} \left[\frac{t^{-2+1}}{-1} \right]_{0}^{L} = \frac{4W}{\pi E k} \left[\frac{-1}{t} \right]_{0}^{L} = \frac{-4W}{\pi E k} \left[\frac{1}{(d_{1} + kx)} \right]_{0}^{L}$$

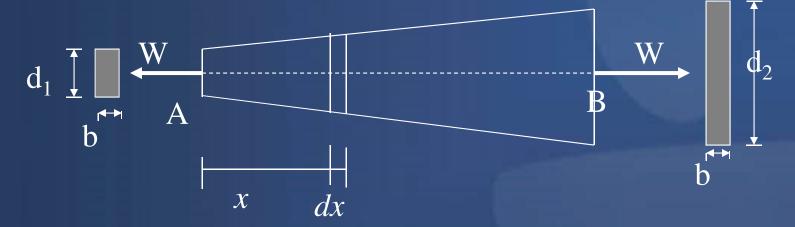
$$= \frac{4WL}{\pi E d_1 d_2} = \frac{WL}{\frac{\pi d_1 d_2}{4} \times E}$$



Derive an expression for the total extension of the tapered bar AB of rectangular cross section and uniform thickness, as shown in the figure, when subjected to an axial tensile load, W.







Consider an element of length, δx at a distance x from A

depth at
$$x$$
,
$$= d_1 + \frac{(d_2 - d_1)}{L} \times x$$
 c/s area at x ,
$$= (d_1 + kx)b$$
$$= d_1 + k \times x$$

Change in length over a
$$= \left(\frac{PL}{AE}\right)_{dx} = \left(\frac{Wdx}{(d_1 + kx)b \times E}\right)$$

length dx is



Change in length over a length *L* is

$$= \int_0^L \left(\frac{Wdx}{(d_1 + kx)b \times E} \right)$$

$$= \frac{P}{b \times E \times k} (\log_e d_2 - \log_e d_1)$$

$$= \frac{2.302 \times P \times L}{b \times E \times (d_2 - d_1)} (\log d_2 - \log d_1)$$



N7. Find the modulus of elasticity of the material of a tapering bar from the following data: The bar has 20 mm diameter at one end, 40 mm diameter at the other, length 1.0 m and axial load of 10 kN. The elongation observed was 0.1 mm.

$$DL = \frac{4P2}{Fd, deE}$$

$$0.1 = \frac{4X10X10^{2}X110^{3}}{FX80 X40XE}$$

$$E = 159, 165 N/mm^{2} = 1596 Pa.$$



N8. A tapered bar of rectangular cross section is 20 mm wide at one end and 40 mm wide at the other, 8 mm thick and 800 mm long. The elongation of 0.08 mm was observed under load P. find the load P, if the modulus of elasticity of the material of the bar is 100 GPa.

$$\Delta L = \frac{PL}{FF(+\frac{1}{2}-N_1)} \log_e(\frac{N_2}{N_1})$$

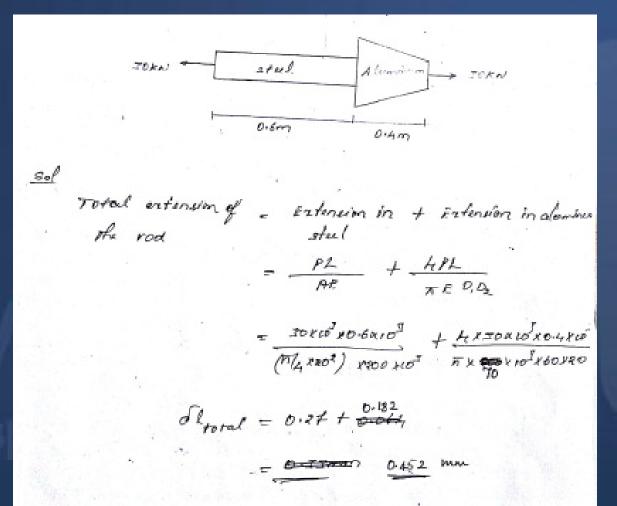
$$0.08 = \frac{PX800}{100 \times 10^{2} \times 8(40-20)} \log_e(\frac{N_2}{N_2})$$

$$P = 2.3 KN$$

$$P = 2.3 KN$$



N9. A uniform steel rod of diameter 20 mm is connected to an aluminium rod of diameter 60 mm at one end. The aluminium rod tapers to a diameter of 20 mm at the other end. The steel rod is 0.6 m long and is connected rigidly to 60 mm diameter end of the aluminium rod which is 0.4 m long. If E = 200 GPa for steel and 70 GPa for aluminium, find the total extension under an axial load of 30 kN.





LECTURE 18

Contents:

Shear stress

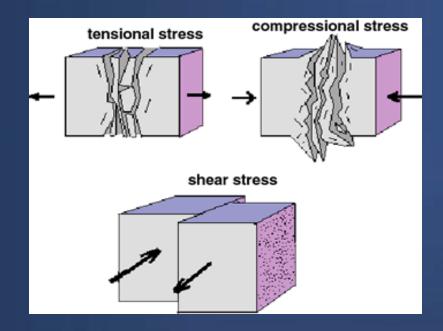
Shear strain

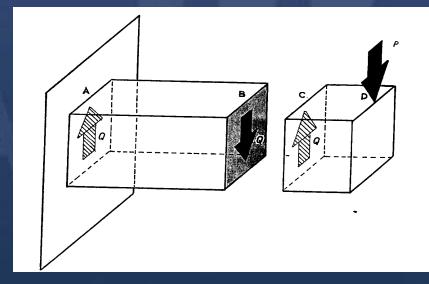
Modulus of rigidity

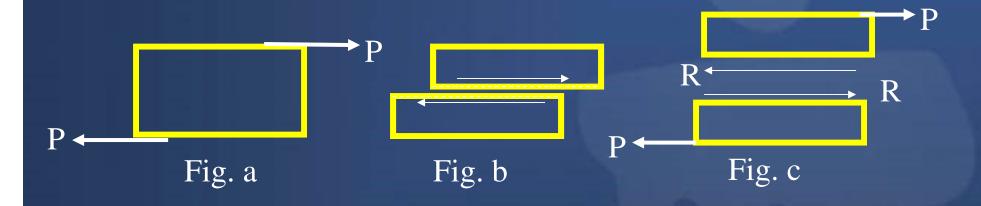
State of simple shear & Complementary shear

Direct stress due to pure shear





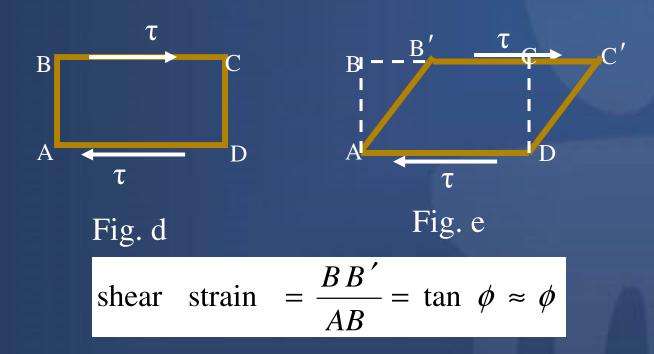




Shear stress(
$$\tau$$
) = $\frac{\text{Shear resistance}}{\text{Area resisting shear}} = \frac{R}{A} = \frac{P}{A}$

This shear stress will always be tangential to the area on which it acts

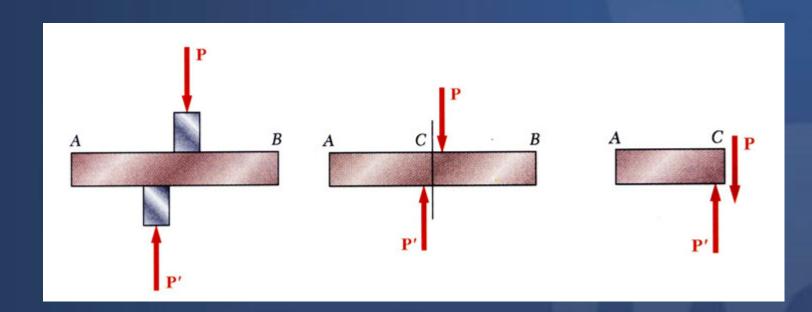




Shear modulus:

 $\frac{\text{Shear stress }(\tau)}{\text{Shear strain }(\phi)} = \text{constant} = G = \text{Shear Modulus or Modulus of Rigidity}$

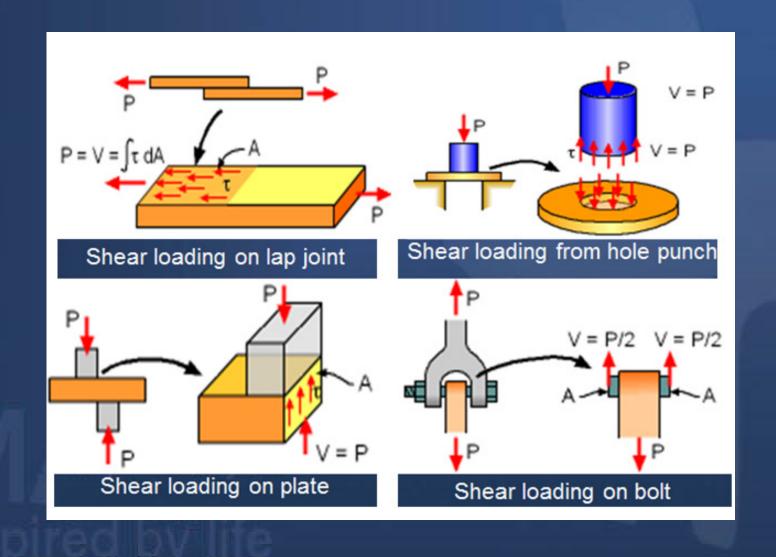




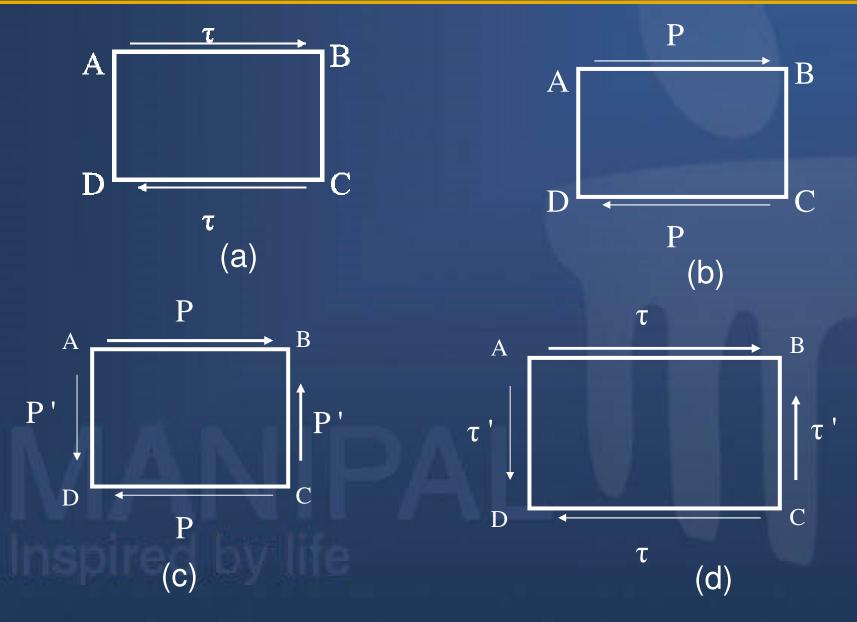
$$\tau_{ave} = \frac{P}{A}$$



Examples of Shear

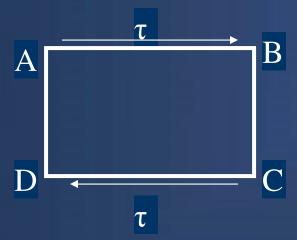








Consider an element ABCD in a strained material subjected to shear stress, T as shown in the figure



Force on the face $AB = P = \tau \times AB \times t$

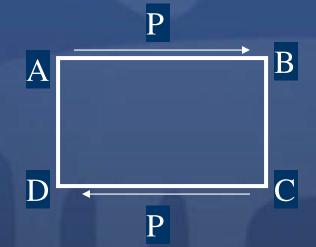
Where, t is the thickness of the element.

Force on the face DC is also equal to P



Now consider the equilibrium of the element. (i.e., $\Sigma Fx = 0$, $\Sigma Fy = 0$, $\Sigma M = 0$.)

For the force diagram shown,
$$\Sigma Fx = 0$$
, & $\Sigma Fy = 0$, But $\Sigma M = 0$



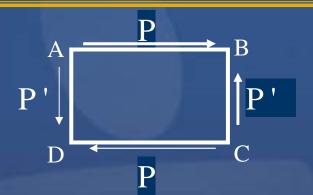
The element is subjected to a clockwise moment

$$P \times AD = (T \times AB \times t) \times AD$$

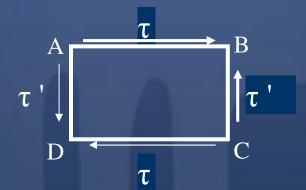
But, as the element is actually in equilibrium, there must be another pair of forces say P' acting on faces AD and BC, such that they produce a anticlockwise moment equal to (P × AD)



P'
$$\times$$
 AB = P \times AD
= $(\tau \times$ AB \times t) \times AD ----- (1)



If τ^1 is the intensity of the shear stress on the faces AD and BC, then P'can be written as, P'= T' × AD × t



Equn.(1) can be written as

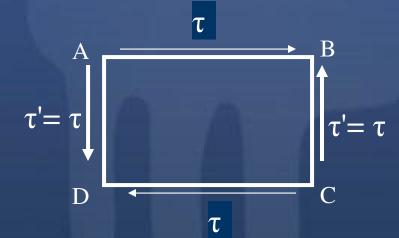
$$(\tau' \times AD \times t) \times AB = (\tau \times AB \times t) \times AD ---- (1)$$

$$\tau' = \tau$$



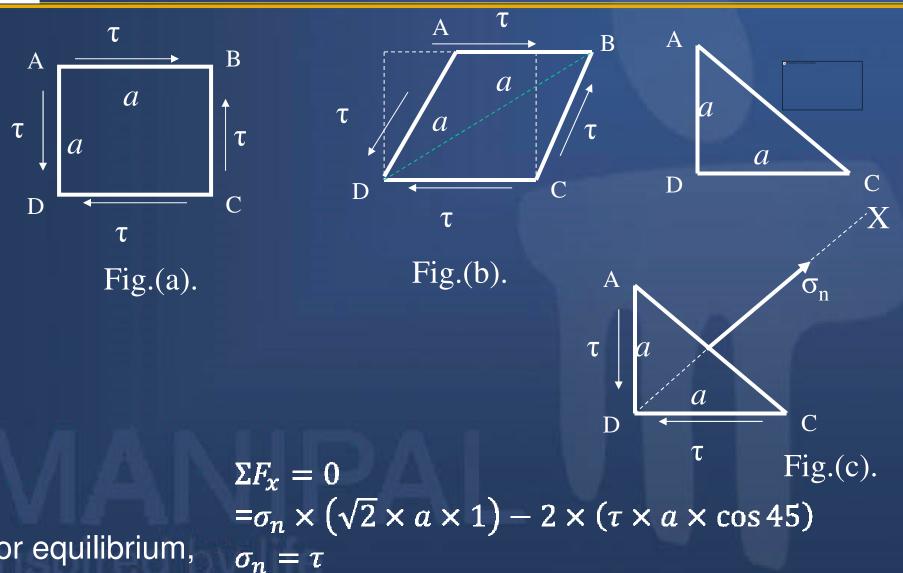
Thus in a strained material a shear stress is always accompanied by a balancing shear of same intensity at right angles to itself. This balancing shear is called "complementary shear".

The shear and the complementary shear together constitute a state of simple shear





Direct stress due to pure shear



For equilibrium,



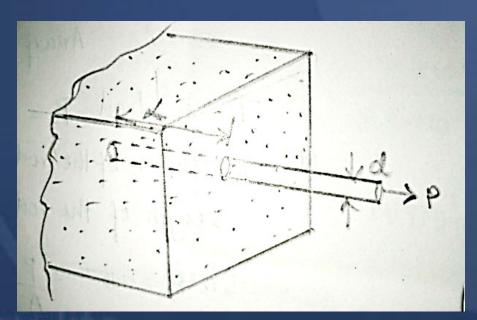
Direct stress due to pure shear

Therefore the intensity of normal tensile stress developed on plane BD is numerically equal to the intensity of shear stress.

Similarly it can be proved that the intensity of compressive stress developed on plane AC is numerically equal to the intensity of shear stress.



N10. To check the bond strength between reinforcing bars and concrete, a tensile force of P=30 kN is applied to the end of the bar of diameter d=12 mm and length L= 100 mm. Calculate the average shear stress developed between steel and concrete.

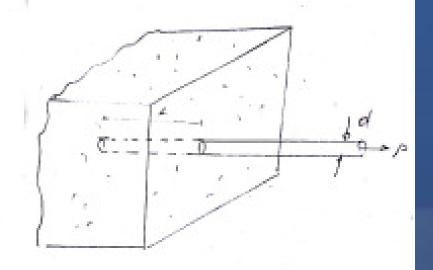


shear = shear force

Area of visiting

shear $Z = \frac{20 \times 10^{3}}{\pi \times 121100}$ E = 7.96 rea

- 1000



NAM F Inspired by life



N11. A hole is to be punched out of a plate having an ultimate shear stress of 300 MPa. If the compressive stress in the punch is limited to 400 MPa,

determine:

(a) Maximum thickness of the plate for which a 100 mm dia hole can be punched.

(b) If the plate is 10mm thick, smallest diameter hole that

can be punched.

Ans: t=33.33 mm d=30 mm Sol @ Shear stress = Shear force Area resisting sheer 300 = FS comp stress = load 400 = F = HOO = T X 1002 F = 3141.6 x 103 N abstituting the value of F in ego O 300 = 3141.6 × 103 2x(50)xt + = 33.33 mm b) t= lomm ; 400 = Force 300 = force area resulting these Area resisting shear = 2 Tot = 2To x 10 .. 300 = 400 x Tx2 2 Trx10 8= 15mm; d=30 mm



LECTURE 19

Contents:

Poisson's ratio

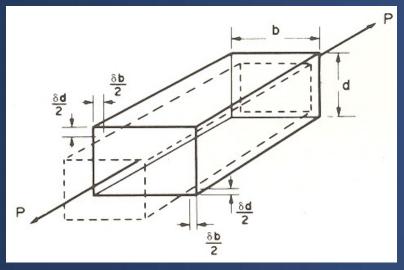
Volumetric strain

Bulk modulus

Relationship between volumetric strain and linear strain

HOME

POISSON'S RATIO



$$\varepsilon_{lat} = -\frac{\delta b}{b} = -\frac{\delta d}{d}$$

Fig.(a)

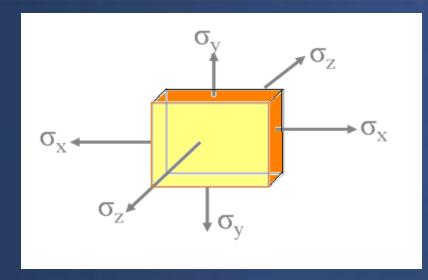
$$\epsilon_l = \frac{\delta l}{l}$$

Poisson's ratio = $\frac{Lateral\ Strain}{Longitudinal\ Strain}$

$$=\frac{\left(-\frac{\delta b}{b}\right)}{\frac{\delta l}{l}} \quad \text{or} \quad \frac{\left(-\frac{\delta d}{d}\right)}{\frac{\delta l}{l}}$$



General case:



Strain in X-direction =
$$\varepsilon_x = \frac{\sigma_x}{E} - \mu \frac{\sigma_y}{E} - \mu \frac{\sigma_z}{E}$$

Strain in Y-direction =
$$\varepsilon_y = \frac{\sigma_y}{E} - \mu \frac{\sigma_x}{E} - \mu \frac{\sigma_z}{E}$$

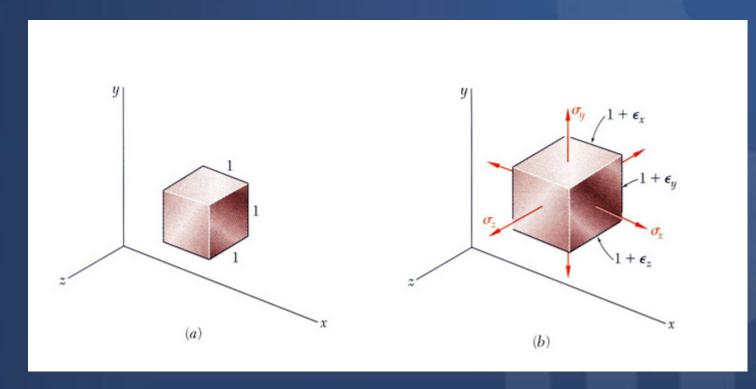
Strain in Z-direction =
$$\varepsilon_z = \frac{\sigma_z}{E} - \mu \frac{\sigma_y}{E} - \mu \frac{\sigma_x}{E}$$

Bulk modulus,
$$K = \frac{o}{\left(\frac{dV}{V}\right)}$$

A body subjected to three mutually perpendicular equal direct stresses then the ratio of stress to volumetric strain is called Bulk Modulus.



Relationship between volumetric strain and linear strain



$$\frac{dV}{1} = \left[(1 + \varepsilon_x)(1 + \varepsilon_y)(1 + \varepsilon_z) \right] - 1 = \left[1 + \varepsilon_x + \varepsilon_y + \varepsilon_z \right] - 1$$

$$= \varepsilon_x + \varepsilon_y + \varepsilon_z$$

$$= \text{change in volume per unit volume}$$

Relationship between volumetric strain and linear strain

Volumetric Strain

$$\frac{dV}{V} = \varepsilon_x + \varepsilon_y + \varepsilon_z$$

$$= \left(\frac{\sigma_x}{E} - \mu \frac{\sigma_y}{E} - \mu \frac{\sigma_z}{E}\right) + \left(\frac{\sigma_y}{E} - \mu \frac{\sigma_z}{E} - \mu \frac{\sigma_x}{E}\right) + \left(\frac{\sigma_z}{E} - \mu \frac{\sigma_x}{E} - \mu \frac{\sigma_y}{E}\right)$$

$$= \frac{1 - 2\mu}{E} \left(\sigma_x + \sigma_y + \sigma_z\right)$$

For element subjected to uniform hydrostatic pressure,

$$\sigma_x = \sigma_y = \sigma_z = \sigma$$

$$\frac{dV}{V} = \frac{1 - 2\mu}{E} (\sigma_x + \sigma_y + \sigma_z)$$

$$\frac{dV}{V} = \frac{1 - 2\mu}{E} (3\sigma)$$

$$K = \frac{\sigma}{\left(\frac{dV}{V}\right)}$$

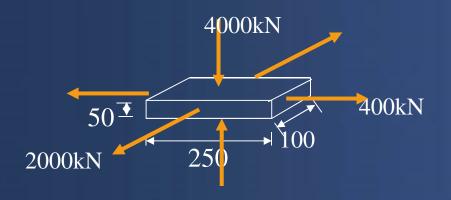
$$E=3K(1-2\mu)$$



N12. A bar of metal 100x50 mm in cross section is 250 mm long. It carries a tensile load of 400 kN in the direction of its length, a compressive load of 4000 kN on its 100 mm x 250 mm faces and a tensile load of 2000 kN on its 50 mm x 250 mm faces. If $E=2x10^5$ N/mm² and poisson's ratio is 0.25, find the change in volume of the bar.

What change must be made in the 4000 kN load in order that there shall be no change in volume of the bar.





Stresses in different directions

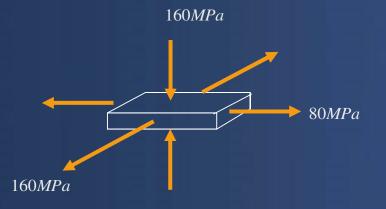
$$\sigma_{y} = \frac{4000 \times 1000N}{250 \times 100mm^{2}} = 160MPa$$

$$\sigma_{x} = \frac{400 \times 1000N}{100 \times 50mm^{2}} = 80MPa$$

$$\frac{2000 \times 1000N}{250 \times 50mm^{2}} = 160MPa$$



Stresses in different direction

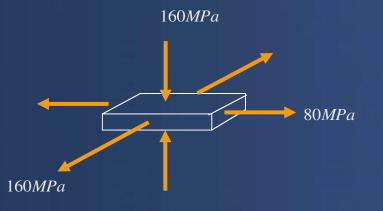


$$\varepsilon_{x} = \frac{\sigma_{x}}{E} - \mu \frac{\sigma_{y}}{E} - \mu \frac{\sigma_{z}}{E}$$

$$\varepsilon_{x} = \frac{+80}{E} - \mu \frac{-160}{E} - \mu \frac{+160}{E} = 4 \times 10^{-4}$$

$$\frac{\delta l_x}{l_x} = \frac{\delta l_x}{250} = 4 \times 10^{-4}$$
$$\delta l_x = 0.1mm$$





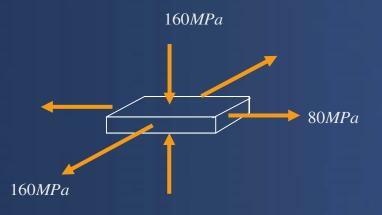
$$\varepsilon_{y} = \frac{\sigma_{y}}{E} - \mu \frac{\sigma_{x}}{E} - \mu \frac{\sigma_{z}}{E}$$

$$\varepsilon_{y} = \frac{-160}{E} - \mu \frac{+80}{E} - \mu \frac{+160}{E} = -(1.1 \times 10^{-3})$$

$$\frac{\delta l_y}{l_y} = \frac{\delta l_y}{50} = -(1.1 \times 10^{-3})$$

$$\delta l_y = -0.005mm$$



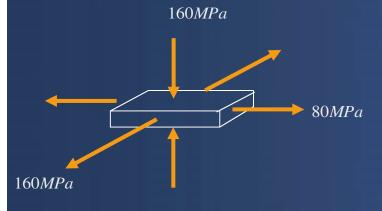


$$\varepsilon_z = \frac{\sigma_z}{E} - \mu \frac{\sigma_y}{E} - \mu \frac{\sigma_x}{E}$$

$$\varepsilon_z = \frac{+160}{E} - \mu \frac{-160}{E} - \mu \frac{+80}{E} = +(9 \times 10^{-4})$$

$$\frac{\delta l_z}{l_z} = \frac{\delta l_z}{250} = +(9 \times 10^{-4})$$
$$\delta l_z = +0.09mm$$





To find change in volume

$$\frac{dV}{V} = \varepsilon_x + \varepsilon_y + \varepsilon_z$$

$$\frac{dV}{V} = (4-11+9)\times 10^{-4} = 2\times 10^{-4}$$

$$dV = (2\times 10^{-4})\times V = (2\times 10^{-4})\times 250\times 100\times 50$$

$$dV = +250mm^{3}$$

Alternatively,

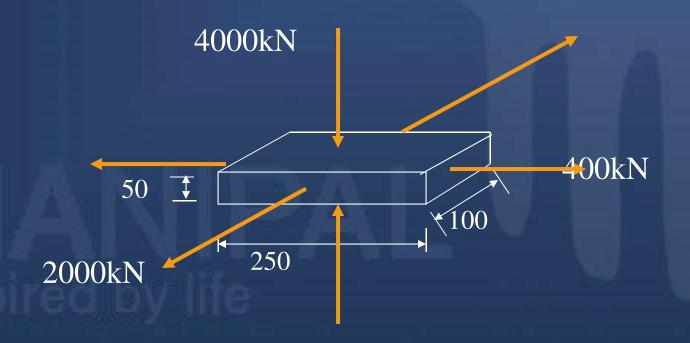
$$\frac{dV}{V} = \frac{1 - 2\mu}{E} \left(\sigma_x + \sigma_y + \sigma_z \right)$$

$$\frac{dV}{V} = \frac{1 - 2\mu}{E} \left(+80 - 160 + 160 \right)$$

$$= \frac{1 - 2\mu}{E} \left(80 \right) = 2 \times 10^{-4}$$

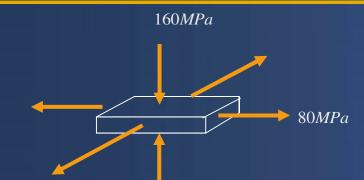


The change in value that should be made in 4000kN load, in order that there should be no change in the volume of the bar.





160*MPa*



We know that

$$\frac{dV}{V} = \frac{1 - 2v}{E} \left(\sigma_x + \sigma_y + \sigma_z \right)$$

In order that change in volume to be zero 1-2n

$$0 = \frac{1 - 2v}{E} \left(\sigma_x + \sigma_y + \sigma_z \right)$$
$$\left(\sigma_x + \sigma_y + \sigma_z \right) = 0$$

$$(+80 + \sigma_y + 160) = 0$$

$$\sigma_y = -240MPa$$

$$-240 = \frac{P_y}{250 \times 100}$$

$$P_y = -6000kN$$

The change in value should be an addition of 2000kN compressive force in Y-direction

N13. A bar of steel 40 mm x 40 mm cross section and 150 mm long is subjected to a tensile load of 200 kN along its longitudinal axis and tensile load of 600 kN and 400 kN along lateral axis.

Find,

- (a) Change in each dimension and change in volume
- (b) What longitudinal force alone can produce same longitudinal strain as in case (a).

Given E=200 GPa $\mu=0.3$

Set:

street in x, y, Z direction. $\frac{Set}{x} = \frac{R_t}{Ax} = \frac{200 \times t0^3}{100 \times 40} = 125 \text{ N/m}^2$ $\frac{Set}{Ax} = \frac{R_t}{Ax} = \frac{200 \times t0^3}{100 \times 40} = 100 \text{ N/mm}^2$ $\frac{Set}{Ax} = \frac{R_t}{Ay} = \frac{600 \times t0^3}{150 \times 40} = 100 \text{ N/mm}^2$ $\frac{Set}{Ax} = \frac{R_t}{Ay} = \frac{600 \times t0^3}{150 \times 40} = 100 \text{ N/mm}^2$ $\frac{Set}{Ax} = \frac{R_t}{Ay} = \frac{410 \times t0^3}{150 \times 40} = 100 \text{ N/mm}^2$ $\frac{Set}{Ax} = \frac{R_t}{Ay} = \frac{410 \times t0^3}{150 \times 40} = 100 \text{ N/mm}^2$ $\frac{Set}{Ax} = \frac{R_t}{Ay} = \frac{410 \times t0^3}{150 \times 400} = 100 \text{ N/mm}^2$ $\frac{Set}{Ax} = \frac{R_t}{Ay} = \frac{410 \times t0^3}{150 \times 400} = 100 \text{ N/mm}^2$ $\frac{Set}{Ax} = \frac{R_t}{Ay} = \frac{410 \times t0^3}{150 \times 400} = 100 \text{ N/mm}^2$ $\frac{Set}{Ax} = \frac{R_t}{Ay} = \frac{410 \times t0^3}{150 \times 400} = 100 \text{ N/mm}^2$ $\frac{Set}{Ax} = \frac{R_t}{Ay} = \frac{410 \times t0^3}{150 \times 400} = 100 \text{ N/mm}^2$ $\frac{Set}{Ax} = \frac{R_t}{Ay} = \frac{410 \times t0^3}{150 \times 400} = 100 \text{ N/mm}^2$ $\frac{Set}{Ax} = \frac{R_t}{Ay} = \frac{410 \times t0^3}{150 \times 400} = 100 \text{ N/mm}^2$ $\frac{Set}{Ax} = \frac{R_t}{Ay} = \frac{410 \times t0^3}{150 \times 400} = 100 \text{ N/mm}^2$ $\frac{Set}{Ax} = \frac{R_t}{Ay} = \frac{410 \times t0^3}{150 \times 400} = 100 \text{ N/mm}^2$ $\frac{Set}{Ax} = \frac{R_t}{Ay} = \frac{410 \times t0^3}{150 \times 400} = 100 \text{ N/mm}^2$ $\frac{Set}{Ax} = \frac{R_t}{Ay} = \frac{410 \times t0^3}{150 \times 400} = 100 \text{ N/mm}^2$ $\frac{Set}{Ax} = \frac{R_t}{Ay} = \frac{410 \times t0^3}{150 \times 400} = 100 \text{ N/mm}^2$ $\frac{Set}{Ax} = \frac{R_t}{Ay} = \frac{R_$

$$\frac{E}{E} = \frac{4}{E} - 11 \frac{\pi}{E} = \frac{125}{E}$$

$$= \frac{100}{2 \times 10^{5}} = 0.3 \times \frac{125}{2 \times 10^{5}} = 0.3 \times \frac{66.67}{2 \times 10^{5}} = \frac{2.125 \times 16^{4}}{2 \times 10^{5}}$$

$$\frac{E}{E} = \frac{7}{E} - 11 \frac{\pi}{E} - 11 \frac{\pi}{E}$$

$$= \frac{66.67}{2 \times 10^{5}} = 0.3 \times \frac{125}{2 \times 10^{5}} = 0.3 \times \frac{100}{2 \times 10^{5}}$$

$$= -4.167 \times 10^{6}$$

$$\frac{6}{E} = 0.056 \text{ mm}$$

$$\frac{6}{E} = 0.056 \text{ mm}$$

$$\frac{6}{E} = -1.667 \times 10^{6} \times 10^{6} \text{ mm}$$

$$\frac{6}{E} = -1.667 \times 10^{6} \times 1$$



LECTURE 20

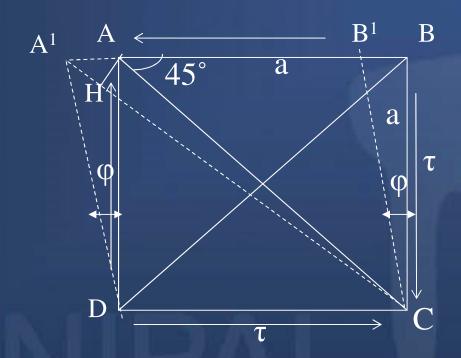
Contents:

Relationship between modulus of elasticity and modulus of rigidity
Relationship between E, G and K
Application problems

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Relationship between young's modulus of elasticity (E) and modulus of rigidity (G):-



Consider a square element ABCD of side 'a' subjected to pure shear't'. DA'B'C is the deformed shape due to shear t.

Drop a perpendicular AH to diagonal A'C.

Strain in the diagonal AC =
$$\tau$$
 /E - μ (- τ /E) [$\sigma_n = \tau$] = τ /E [1 + μ] -----(1)

```
Strain along the diagonal AC=(A'C-AC)/AC=(A'C-
CH)/AC=A'H/AC
In Δle AA'H
Cos 45^{\circ} = A'H/AA'
A'H = AA' \times 1/\sqrt{2}
AC = \sqrt{2 \times AD} (AC = \sqrt{AD^2 + AD^2})
Strain along the diagonal AC = AA'/ (\sqrt{2} \times \sqrt{2} \times AD) = \varphi/2 ----(2)
Modulus of rigidity = G = \tau / \phi
                        \Phi = T/G
Substituting in (2)
Strain along the diagonal AC = T/2G ----(3)
Equating (1) & (3)
T/2G = T/E[1+\mu]
                         E=2G(1+\mu)
```

Relationship between E, G, and K:-

We have $E = 2G(1 + \mu)$ -----(1) $E = 3K(1-2\mu)$ -----(2) Equating (1) & (2) $2G(1 + \mu) = 3K(1-2\mu)$ $2G + 2G\mu = 3K - 6K\mu$ $\mu = (3K - 2G)/(2G + 6K)$ Substituting in (1) E = 2G[1 + (3K - 2G)/(2G + 6K)] E = 18GK/(2G + 6K)

$$E = 9GK/(G+3K)$$



N14.A circular rod of 100 mm dia and 500 mm length is subjected to a tensile force of 2000 kN. Determine the modulus of rigidity, bulk modulus and the change in volume, if the poisson's ratio=0.3 and E=2x10⁵ N/mm².

Ans:

 $G=0.77x10^5 N/mm^2$

 $K=1.67 \times 10^5 \text{ N/mm}^2$

dv=1994.9 mm³

A = 1/4 × 1002 = 7853.98 mm2 L = 500mm P = 2000 200 N 4 = 0. I & E = 2×105 N/mm2 (i) E = 26 (1+u) . . g = E B = 2x105 = 0.44 MOS N/mm2 (11) K - E = 2×105 = 1.67×105 Wmm2 (11) To find the change in volume using the velation for volumetric strain re have dv = 6x + Gy + 62 Longitudiral strain is given by Gx = TE = P = 2000 x105 = 1.24x103

Gx = \sqrt{E} AE $2x10^5x+853.98$ Lateral strain is given by. $6z = 6y = -1.6x = -0.3 \times 1.24 \times 10^{-5} = -1.82 \times 15^{-4}$ 9 = dv = 6x - 21.6x - 21.6x





N15. The modulus of rigidity of a material is 0.8 x 10⁵ N/mm². When a 6 mm x 6 mm bar of this material is subjected to an axial pull of 3600 N, it was found that the lateral dimension of bar is changed to 5.9991 mm x 5.9991 mm.

Find μ and E.

Lateral strain =
$$\frac{5b}{b} = \frac{6-5.9991}{6} = \frac{1.5 \times 10^{-4}}{6}$$

Avial strue, $\sigma = P/A = \frac{5600}{616} = \frac{100 \text{ N/mm}^2}{616}$

Lateral strain = $\mu \left(\frac{\sigma}{F}\right)$
 $\mu = \frac{1.5 \times 10^{-4}}{(1.0/F)} = \frac{1.5 \times 10^{4}}{110}$

or $E = \frac{10 \text{ M}}{1.5 \times 10^{4}} = 0$

also $G = \frac{E}{2(1+M)} = 10.810^{5} = \frac{E}{2(1+M)}$
 $P = 160 \times 10^{5} \left(1+M\right) = 0$

Equating $O \neq O$
 $P = 160 \times 10^{5} \left(1+M\right) = 0$
 $P = 160 \times 10^{5} \left(1+M\right) = 0$

Substituting
$$u = 0.316$$
 m ()
$$E = \frac{100 \times 0.316}{1.5 \times 10^{-4}} = 2.105 \times 10^{5} \text{ N/mm}^{2}$$



TUTORIAL 8

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T1. Find the Young's modulus of a brass rod of diameter 25 mm and of length 250 mm which is subjected to a tensile load of 75 kN when the extension of the rod is equal to 0.3 mm.

Given, diameter of nod = 25 mm

Area of rod =
$$\frac{1}{4} \times 25^2 = 490.87 \text{ mm}^2$$

tenule load, $P = 75 \text{ kN} = 75000 \text{ N}$

(dl) extension of nod = 0.3 mm

length of nod = 250 mm

Stress (σ) = $\frac{P}{A} = \frac{75,000}{490.87} = 152.79 \text{ N/mm}^2$

Strain (ϵ) = $\frac{dL}{L} = \frac{0.3}{250} = 1.2 \times 10^{-3}$

Young's modulus (ϵ) = $\frac{\sigma}{E} = \frac{152.79}{1.2 \times 10^{-3}} = 127325 \text{ N/m}$

T2. The ultimate stress, for a hollow steel column which carries an axial load of 2.0 MN is 480 N/mm². If the external diameter of the column is 200 mm, determine the internal diameter. Take factor of safety as 3.

```
Axial load = 2 MN = 2x106 N
       External diameter (D) = 200 mm
         Factor of softly = 3
let d'be internal diameter
: Area of US of the column;
            Ac = \frac{\pi}{4} (D^2 - d^2) = \frac{\pi}{4} (200^2 - d^2)
 Fos = ultimate stress
Working stress / allowable stress
     3 = 480
working stress
working = 160 N/mm²
```



TUTORIAL 9

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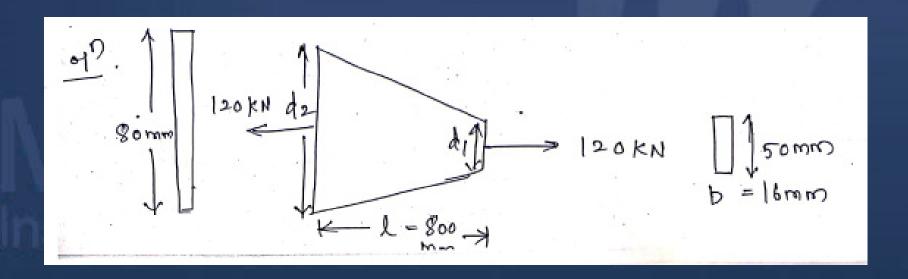
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T3. A steel flat of thickness 16 mm tapers uniformly from 80 mm at one end to 50 mm at the other end in a length of 800 mm, If the flat is subjected to a load of 120 kN, find the extension of the flat. Also calculate the percentage error if average area is used for calculating its extension. Take $E=2x10^5$ Mpa.

Solution:



$$\delta = \frac{2.302 \text{ PL}}{6 \times \text{ELd}_2 - d_1} \left(\log_2 d_2 - \log_2 d_1 \right)$$

$$= \frac{2.302 \times 120 \times 10 \times 900}{16 \times 2 \times 10^5 \times (90-50)} \left(\log_2 80 - \log_2 50 \right)$$

$$= 0.469 \text{ mms}$$

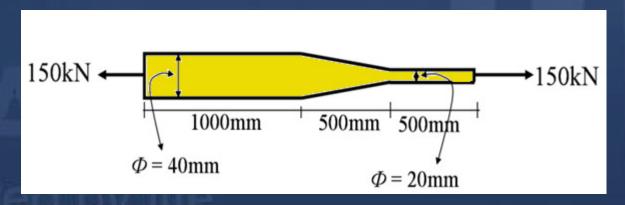
Area of c/s at larger end $A_2 = 80 \times 16 = 1280 \text{ mm}^2$ Area of c/s at smaller end $A_1 = 50 \times 16 = 800 \text{ mm}^2$ Average c/s area = $A = A_1 + A_2 = \frac{1240 + 800}{2}$

Percentage ever in extension

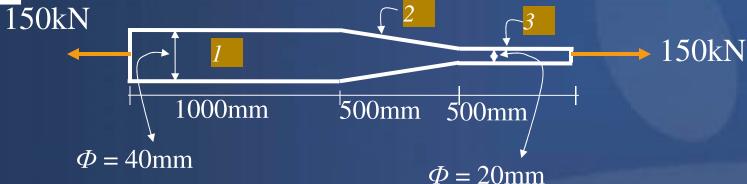
$$= \frac{\delta - \delta q}{\delta} = \frac{0.469 - 0.462}{0.469}$$
$$= 1.5\%$$



T4. A two meter long steel bar is having uniform diameter of 40 mm for a length of 1 m, in the next 0.5 m its diameter gradually reduces to 20 mm and for remaining 0.5 m length diameter remains 20 mm uniform as shown in the figure. If a load of 150 kN is applied at the ends, find the stresses in each section of the bar and total extension of the bar. Take E = 200 GPa.







If we take a section any where along the length of the bar, it is subjected to a load of 150kN.

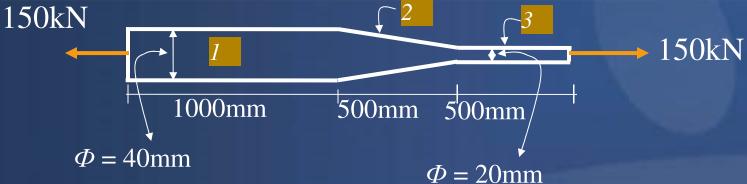
$$\sigma_{1} = \frac{150kN}{\pi 40^{2}/4} = 119.37MPa$$

$$\sigma_{2} = \frac{150kN}{\pi d^{2}/4} \Rightarrow \sigma_{2,\text{max}} = \frac{150kN}{\pi 40^{2}/4} = 119.37MPa$$

$$\sigma_{2,\text{min.}} = \frac{150kN}{\pi 20^{2}/4} = 477.46MPa$$

$$\sigma_3 = \frac{150kN}{\pi 20^2 / 4} = 477.46MPa$$





If we take a section any where along the length of the bar, it is subjected to a load of 150kN.

$$\delta l_{1} = \frac{150kN \times 1000}{(\pi 40^{2}/4) \times E} = 0.597mm$$

$$\delta l_{2} = \frac{4PL}{\pi E d_{1}d_{2}} = \frac{4 \times 150kN \times 500}{\pi \times E \times 40 \times 20} = 0.597mm$$

$$\delta l_{3} = \frac{150kN \times 500}{(\pi 20^{2}/4) \times E} = 1.194mm$$

$$total, \delta l = 2.388mm$$

TUTORIAL 10

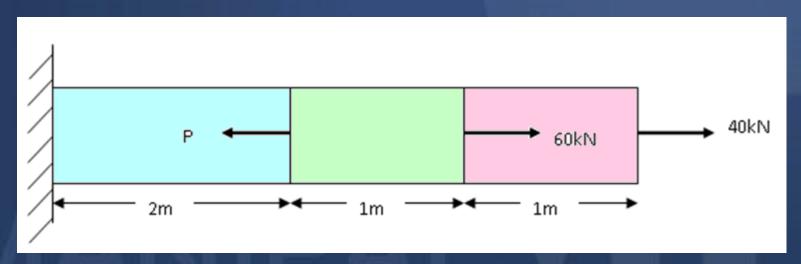
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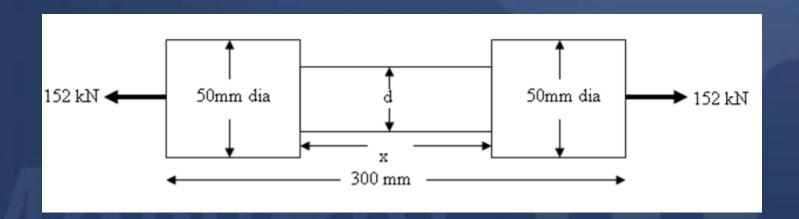
T5. Determine the magnitude of the load P necessary to produce zero net change in the length of the bar shown in the figure below. Take A=400 mm².



o's got let the fection R'at the suppor acts towards right. for the equillibrium of the bar R+60+40=P R= P-100 2.000 mm BC-100×1000 - 250 SCD = 40 × 1000 = 100 HOOKE E - (Ploo) 400mm 40 KN # 1000000->1 Total extension & = FAB + 8Be+ 8CD 0 - 5P-500 + 250 + 100 E .. P= 1+0 KN



T6. For the bar shown below, determine diameter of the central portion and its length, if the total extension of the bar is 0.16 mm. Take E=200 GPa. Stress at central portion is limited to 140 N/mm²



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Extension of end portion + extension of middle portion $\frac{-(300-1)+-(1)}{E}$ $\frac{-(140.20 \text{ mm})}{200}$

Us area of the middle partion, etners = $\frac{Force}{c|s}$ area C|s area = $\frac{F}{140}$ = $\frac{15200}{140}$ $A = 1085.71 \text{ mm}^2 = \frac{740}{4}$

d= 37.18mm

Let the length of the middle parties be 2 mm

Stress in the end parties, == P = 152000

Ty x502

= 77.41 N/mm² | 01=0.16 mm



T7. A tension test is carried out subjected on a mild steel tube of external diameter 18 mm and internal diameter 12 mm. An an axial load of 2 kN produces an extension of 3.36 x 10⁻³ mm on a length of 50 mm and a lateral contraction of 3.62 x 10⁻⁴ mm of outer diameter.

Determine E, µ,G and K.

Ans:

 $E=2.11x10^5 \text{ N/mm}^2$

 $\mu = 0.3$

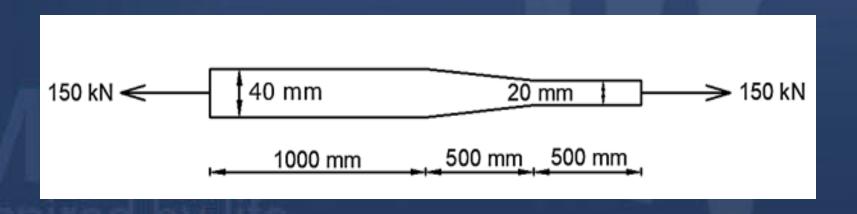
 $G=81.15x10^3 \text{ N/mm}^2$

 $K=175.42x10^3 N/mm^2$

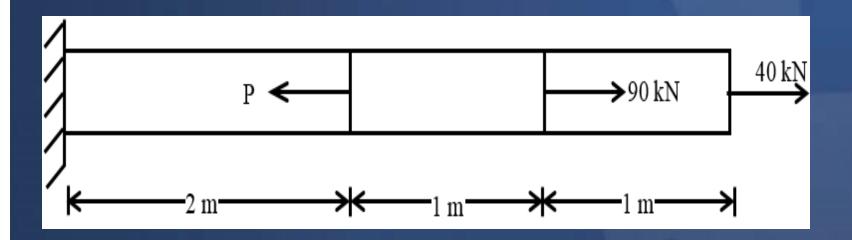
ADDITIONAL TUTORIAL PROBLEMS

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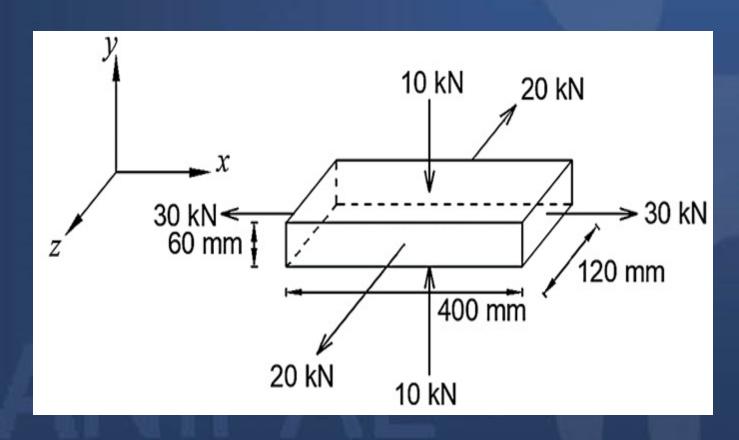
AT1. A two meter long steel bar is having uniform diameter of 40 mm for a length of 1 m, in the next 0.5 m its diameter gradually reduces to 20 mm and for remaining 0.5 m length diameter remains 20 mm uniform as shown in the figure. If a load of 150 kN is applied at the ends, find the stress in each section and total extension of the bar. Take E = 200 Gpa



AT2. Determine the magnitude of the load P necessary to produce zero net change in the length of the bar shown in the figure below. Take A=400 mm².



AT3. A steel bar of 400 mm x 120 mm x 60 mm is subjected to forces as shown in the figure. Find the change in dimension. Taking E = 200 GPa and $\mu = 0.25$.



AT4. A circular concrete pillar consists of six steel rods of total area 2280 mm². Determine the area of concrete required when it has to carry a load of 1000 kN. Take allowable stresses for steel & concrete as 140 MPa & 8 MPa respectively. Take $E_s = 15 \ E_c$.