

## NUMERICALS ON PROPERTIES OF STEAM

**1) Determine the condition and related parameter of the steam in the following cases: (i) Pressure of 10 bar and temperature of 200°C and (ii) Pressure of 8 bar and enthalpy of 2500kJ/kg. (iii) Steam at 20bar and 300°C is cooled at constant pressure during which the heat lost is 400kJ/kg. Assume specific heat of superheated steam as 2.25kJ/Kg K.**

Solution:

i) Pressure = 10 bar and T = 200 °C

From steam tables at a pressure of 10 bar,

$$T_{\text{sat}} = 179.9 \text{ °C}, h_f = 762.6 \text{ kJ/kg}$$

$$h_{fg} = 2013.6 \text{ kJ/kg}, h_g = 2776.2 \text{ kJ/kg}$$

Since the temperature of the steam is greater than the saturation temperature the steam sample is superheated.

$$\begin{aligned} \text{Enthalpy } h_{\text{sup}} &= h_g + C_{\text{sup}} (T_{\text{sup}} - T_{\text{sat}}) \\ &= 2776.2 + 2.25(200 - 179.9) \end{aligned}$$

$$h_{\text{sup}} = 2821.43 \text{ kJ/kg}$$

Degree of Superheat (DOS)

$$\begin{aligned} \text{DOS} &= (T_{\text{sup}} - T_{\text{sat}}) \\ &= 200 - 179.9 \\ &= 20.1^\circ\text{C} \end{aligned}$$

ii) Pressure = 8 bar and h = 2500 kJ/kg

From steam tables at a pressure of 8 bar,

$$T_{\text{sat}} = 170.4 \text{ °C}, h_f = 720.9 \text{ kJ/kg}$$

$$h_{fg} = 2046.5 \text{ kJ/kg}, h_g = 2767.4 \text{ kJ/kg}$$

Since enthalpy of dry saturated steam ( $h_g = 2767.4 \text{ kJ/kg}$ ) is greater than the enthalpy of steam sample ( $h = 2500 \text{ kJ/kg}$ ) the given sample of steam is wet Steam.

Dryness fraction of the steam (X):

$$h = h_f + X h_{fg}$$

$$2500 = 720.9 + X * 2046.5$$

$$X = 0.8693 \text{ or } 86.93 \%$$

iii) Pressure = 20 bar, T = 300 °C, Heat loss = 400 kJ/kg

From steam tables at a pressure of 20 bar,

$$T_{\text{sat}} = 212.4 \text{ °C } h_f = 908.5 \text{ kJ/kg}$$

$$h_{fg} = 1888.7 \text{ kJ/kg } h_g = 2797.2 \text{ kJ/kg}$$

Since the temperature of the steam is greater than the saturation temperature the steam sample is superheated.

$$\begin{aligned} \text{Enthalpy } h_{\text{sup}} &= h_g + C_{\text{sup}} (T_{\text{sup}} - T_{\text{sat}}) \\ &= 2797.2 + 2.25(300 - 212.4) \end{aligned}$$

$$h_{\text{sup}} = 2994.3 \text{ kJ/kg}$$

$$\begin{aligned} \text{Enthalpy after heat loss of 400 kJ/kg} &= 2994.3 - 400 \\ &= 2594.3 \text{ kJ/kg} \end{aligned}$$

Since the enthalpy after heat loss (2594.3 kJ/kg) is less than the enthalpy of dry saturated steam ( $h_g = 2797.2 \text{ kJ/kg}$ ), the steam is Wet.

Dryness fraction of the steam (X):

$$h = h_f + X * h_{fg}$$

$$2594.3 = 908.5 + X \times 1888.7$$

$$X = 0.8926 \text{ or } 89.26\%$$

**2) 2 Kg of water at 30°C is heated at a constant pressure of 5 bar. The total amount of heat added is 500 KJ. Determine the condition and related parameter of water after heat addition. Assume specific heat of water as 4.187kJ/Kg K.**

At P= 5 bar  $T_{\text{sat}} = 151.9^{\circ}\text{C}$ ,  $h_f = 640.1 \text{ KJ/Kg}$ ,

$h_{fg} = 2107.4 \text{ KJ/Kg}$ ,  $h_g = 2747.5 \text{ KJ/Kg}$ .

Solving on a per kg basis

Enthalpy of water at 30°C

$$\begin{aligned}h &= mC_p(T-0) \\&= 1 \times 4.187 \times (30-0) \\&= 125.61 \text{ kJ/Kg}\end{aligned}$$

Heat added on per kg basis

$$\begin{aligned}&= 500/2 \\&= 250 \text{ kJ/kg}\end{aligned}$$

Enthalpy after heat addition

$$\begin{aligned}&= 125.61 + 250 \\&= 375.61 \text{ kJ/kg} < h_f\end{aligned}$$

Since enthalpy after heat addition is less than sensible heat the resulting condition after heat addition is unsaturated water.

Temperature of unsaturated water after heat addition

$$\begin{aligned}h &= mC_p(T-0) \\375.61 &= 1 \times 4.187 \times (T-0) \\T &= 89.71^{\circ}\text{C}\end{aligned}$$

**OR**

Considering the actual mass of water

Enthalpy of water at 30°C

$$h = mC_p(T-0)$$

$$= 2 \times 4.187 \times (30-0)$$

$$= 251.22 \text{ kJ/2Kg}$$

Enthalpy after heat addition

$$= 251.22 + 500$$

$$= 751.22 \text{ kJ/2kg}$$

∴ Sensible heat for 2 Kg =  $h_f \times 2$

$$= 640.1 \times 2 = 1280.2 \text{ KJ}$$

Since enthalpy after heat addition is less than sensible heat the resulting condition after heat addition is unsaturated water.

Temperature of unsaturated water after heat addition

$$h = mC_p(T-0)$$

$$751.22 = 2 \times 4.187 \times (T-0)$$

$$T = 89.71^\circ\text{C}$$

**3) 10 Kg. of steam at a pressure of 1.15 MPa and temperature of 250°C loses 27578.2 kJ of heat at constant pressure. Determine the resulting temperature? Assume specific heat of water and superheated steam as 4.187 kJ/kg K and 2.25 kJ/kg K respectively.**

$$P = 1.15 \text{ MPa} = 11.5 \text{ bar},$$

$$T_{\text{sat}} = 186^\circ\text{C}, h_f = 789.9 \text{ kJ/kg}, h_{fg} = 1991.4 \text{ kJ/kg}, h_g = 2781.3 \text{ kJ/kg}.$$

Solving on a per kg basis

Enthalpy at 250°C

$$h_{\text{sup}} = h_g + C_{\text{sup}}(T_{\text{sup}} - T_{\text{sat}})$$

$$= 2781.3 + 2.25(250 - 186)$$

$$= 2925.3 \text{ kJ/kg}$$

$$\text{Enthalpy after heat loss.} = 2925.3 - 27578.2/10$$

$$= 167.48 \text{ kJ/kg} < h_f$$

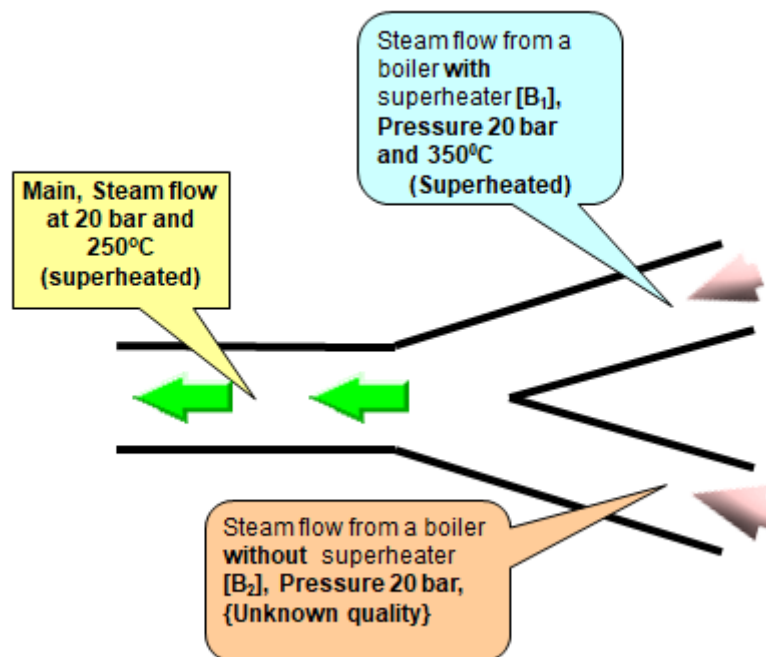
Resulting Temperature

$$hw = mC_p(T - 0)$$

$$167.48 = 1 \times 4.187 \times (T - 0)$$

$$T = 40^\circ\text{C}$$

4) Two boilers one with super heater and another without super heater are delivering equal quantities of steam into a common main. The pressure in the boiler and in the main is 20 bar. The temperature of the steam from a boiler with a superheater is  $350^\circ\text{C}$  and the temperature of steam in the main is  $250^\circ\text{C}$ . Determine the quality of steam supplied by the other boiler. Assume specific heat of superheated steam as  $2.25 \text{ kJ/Kg K}$ .



$P = 20 \text{ bar}$ .

At 20 bar.

$T_{\text{sat}} = 212.4^\circ\text{C}$ ,  $h_f = 908.5 \text{ kJ/kg}$ ,  $h_{fg} = 1888.7 \text{ kJ/kg}$  &  $h_g = 2797.2 \text{ kJ/kg}$

Enthalpy of steam generated in the boiler (B<sub>1</sub>) having super heater

T=350°C >T<sub>sat</sub>, steam is superheated.

$$\begin{aligned}h_{\text{sup}} &= h_g + C_{\text{sup}} (T_{\text{sup}} - T_{\text{sat}}) \\&= 2797.2 + 2.25 (350 - 212.4) \\&= 3106.8 \text{ kJ/kg} \quad \text{-----}(A)\end{aligned}$$

Enthalpy of steam in the main

T=250°C >T<sub>sat</sub>, steam is superheated

$$\begin{aligned}h_{\text{sup}} &= h_g + C_{\text{sup}} (T_{\text{sup}} - T_{\text{sat}}) \\&= 2797.2 + 2.25 (250 - 212.4) \\&= 2881.8 \text{ kJ/kg}\end{aligned}$$

Total enthalpy in the main for 2kg of steam

$$\begin{aligned}&= 2 \times 2881.8 \\&= 5763.6 \text{ kJ/2kg} \quad \text{-----}(B)\end{aligned}$$

Enthalpy of steam generated in the boiler (B<sub>2</sub>) without the super heater

$$\begin{aligned}h &= h_f + X \cdot h_{fg} \\&= 908.5 + X \cdot 1888.7 \text{ kJ/kg} \quad \text{-----}(C)\end{aligned}$$

For heat balance

$$(A) + (C) = (B)$$

$$3106.8 + 908.5 + X \cdot 1888.7 = 5763.6$$

X= 0.9257 or 92.57%. Steam generated in the boiler without the super heater is 92.57% dry.

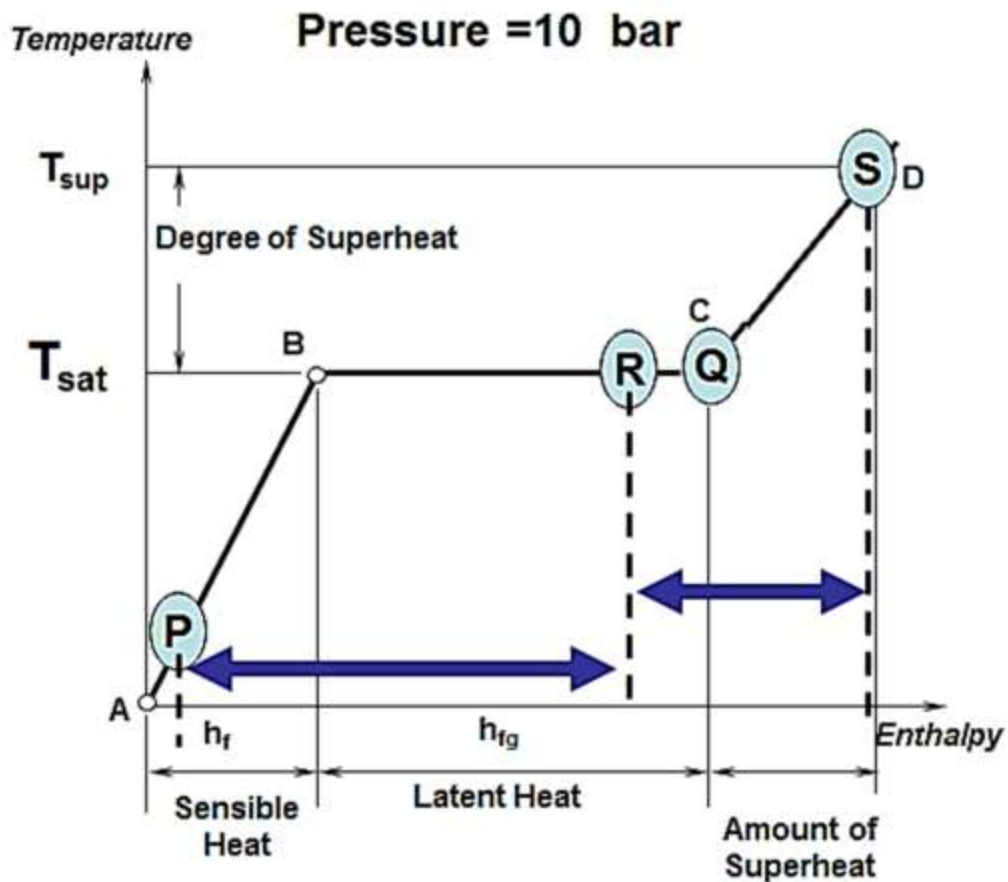
**5) A dry saturated steam at a pressure of 1 MPa is generated in a boiler. Dry saturated steam leaves the boiler to enter a super heater, where it loses heat equal to 400 kJ/kg. In the super heater, steam is super-heated to temperature of 300°C. If temperature of feed water is 28°C, determine:**

**a) Total heat supplied to feed water in the boiler**

**b) Dryness fraction of steam at the entry of super heater**

**c) Total heat supplied in the super heater.**

**Assume specific heat of water as 4.187 kJ/Kg K and that of superheated steam as 2.25 kJ/Kg K**



Data: Pressure = 1 MPa = 10 bar,  $T_{\text{sup}} = 300^\circ\text{C}$ ,  $T = 28^\circ\text{C}$

Heat loss before entering superheater = 400 kJ/kg

Let

P – Point at which water enters the boiler

Q – Point at which steam leaves the boiler in dry saturated condition.

R – Point at which steam enters the superheater as wet steam

S – Point at which superheated steam leaves the superheater.

At 10 bar,

$T_{\text{sat}} = 179.9^\circ\text{C}$ ,  $h_f = 762.6\text{ kJ/kg}$ ,  $h_{fg} = 2013.6\text{ kJ/kg}$ ,  $h_g = 2776.2\text{ kJ/kg}$

Enthalpy of water at  $28^\circ\text{C}$  or enthalpy at P

$$\begin{aligned}
 h_P &= mC_p(T-0) \\
 &= 1 \times 4.187 \times (28-0) \\
 &= 117.24\text{ kJ/Kg}
 \end{aligned}$$

Enthalpy at Q =  $h_Q = h_g = 2776.2 \text{ kJ/kg}$

Enthalpy of steam at the entry point of superheater (R),

$$\begin{aligned}h_R &= h_Q - 400 \\&= 2776.2 - 400 \\&= 2376.2 \text{ kJ/kg}\end{aligned}$$

Enthalpy of superheated steam (S),

$$\begin{aligned}h_S &= h_g + C_{\text{sup}} (T_{\text{sup}} - T_{\text{sat}}) \\&= 2776.2 + 2.25 (300 - 179.9) \\&= 3046.43 \text{ kJ/kg}\end{aligned}$$

a) Total heat supplied to feed water in the boiler

$$\begin{aligned}&= h_Q - h_P \\&= 2776.2 - 117.24 \\&= 2658.96 \text{ kJ/kg}\end{aligned}$$

b) Dryness fraction of steam at the entry to the superheater (X)

$$h = h_R = h_f + X h_{fg}$$

$$2376.2 = 762.6 + X \times 2013.6$$

$$X = 0.8014 \text{ or } 80.14\%$$

c) Total heat supplied in the superheater

$$\begin{aligned}&= h_S - h_R \\&= 3046.43 - 2376.2 \\&= 670.23 \text{ kJ/kg}\end{aligned}$$

**6) 600 kg of 10% wet steam at a pressure of 16bar is generated in a boiler per hour. Steam leaves the boiler to enter a super heater. Steam loses heat equal to 300 kJ/kg before entering the super heater. In the super heater, steam is superheated to temperature of 375<sup>0</sup> C. If temperature of feed water is 40<sup>0</sup> C, determine**

- i) Total heat supplied to feed water per hour to produce wet steam in the boiler.**
- ii) Total heat absorbed per hour in the super heater.**



**Assume specific heat of water as 4.187kJ/Kg K and that of superheated steam as 2.25kJ/Kg K**

P= 16bar.

From tables properties of steam at 16 bar.

$T_{\text{sat}} = 201.4^{\circ}\text{C}$ ,  $h_f = 858.5 \text{ kJ/kg}$ ,  $h_{fg} = 1933.2 \text{ kJ/kg}$  &  $h_g = 2791.7 \text{ kJ/kg}$

Solving on a per kg basis

Enthalpy of water at  $40^{\circ}\text{C}$

$$\begin{aligned} h_w &= mC_p(T-0) \\ &= 1 \times 4.187 \times (40-0) \\ &= 167.48 \text{ kJ/Kg} \end{aligned}$$

Enthalpy of wet steam generated in the boiler

$$\begin{aligned} X &= (1-0.1) = 0.9 \\ h &= h_f + X \cdot h_{fg} \\ h &= 858.5 + 0.9 \times 1933.2 \\ h &= 2598.38 \text{ kJ/Kg} \end{aligned}$$

Enthalpy of the steam at the entry point of Super heater

$$\begin{aligned} h &= 2598.38 - 300 \\ h &= 2298.38 \text{ kJ/Kg} \end{aligned}$$

Enthalpy of the steam at the exit point of superheater

$$\begin{aligned} h_{\text{sup}} &= h_g + C_{\text{sup}} (T_{\text{sup}} - T_{\text{sat}}) \\ &= 2791.7 + 2.25 (375 - 201.4) \\ &= 3182.3 \text{ kJ/Kg} \end{aligned}$$

Total heat supplied to feed water per hour to produce 10% wet steam in the boiler.

$$\begin{aligned} &= (2598.38 - 167.48) \times 600 \\ &= 1458540 \text{ kJ} \\ &= 1458.54 \text{ MJ} \end{aligned}$$

Total heat absorbed per hour in the super heater.

$$\begin{aligned} &= (3182.3 - 2298.38) \times 600 \\ &= 530352 \text{ J} \\ &= 530.352 \text{ MJ} \end{aligned}$$

**7) A chemical company planning to install a coal fired boiler in its plant for process heating is weighing different technical options due to investment constraints. The steam generation capacity required is 5000kg per hour at a pressure of 0.56MPa and at a temperature of 220°C. The feed water is available from a nearby reservoir at an average temperature 30°C. The coal consumption is 1500 kg/hr, having a calorific value of 24MJ/kg. Assess the improvement in boiler efficiency if the following accessories are used.**

**i) Economizer which will increase the feed water temperature by 58°C. and reduce the coal consumption by 14%.**

**ii) Air Preheater which will reduce the coal consumption by 20%.**

**iii) Both Economizer and Air Preheater whose combined effect will reduce the coal consumption by 30%.**

**Assume specific heat of water and superheated steam as 4.187kJ/kg K and 2.25kJ/kg k respectively.**

$T = 30^\circ\text{C}$ ,  $T_{\text{sup}} = 220^\circ\text{C}$ ,  $Q = 5000\text{kg/hr}$ ,  $\text{GCV} = 24\text{MJ/kg} = 24000\text{kJ/kg}$ ,  $m_{\text{fu}} = 1500\text{ kg/hr}$

From Steam tables properties of steam at 0.56MPa or 5.6bar.

$T_{\text{sat}} = 156.2^\circ\text{C}$ ,  $h_f = 658.8\text{ kJ/kg}$ ,  $h_{fg} = 2093.7\text{ kJ/kg}$  &  $h_g = 2752.5\text{ kJ/kg}$

Enthalpy of water at 30°C

$$\begin{aligned} h_w &= mC_p(T - 0) \\ &= 1 \times 4.187 \times (30 - 0) \\ &= 125.61\text{ kJ/kg.} \end{aligned}$$

Enthalpy at a temperature of 220°C

$$\begin{aligned}h_{sup} &= h_g + C_{sup}(T_{sup} - T_{sat}) \\&= 2752.5 + 2.25 \times (220 - 156.2) \\&= 2896.05 \text{ kJ/Kg}\end{aligned}$$

Boiler Efficiency without using the accessories

$$\begin{aligned}\eta &= \frac{Q(h_s - h_w) * 100}{m_{fu} * GCV} \\&= \frac{5000(2896.05 - 125.61) * 100}{1500 * 24000}\end{aligned}$$

$$\eta = 38.48\%$$

**i) Boiler Efficiency if Economizer is used.**

$$T = 30 + 58 = 88^\circ\text{C}, \quad m_{fu} = 1500 - 0.14 \times 1500 = 1290 \text{ kg/hr}$$

Enthalpy of water at 88°C

$$\begin{aligned}h_w &= mC_p(T - 0) \\&= 1 \times 4.187 \times (88 - 0) \\&= 368.46 \text{ kJ/kg.}\end{aligned}$$

$$\eta = \frac{5000(2896.05 - 368.46) * 100}{1290 * 24000}$$

$$\eta = 40.52\%$$

Improvement in efficiency =  $40.52 - 38.48 = 2.04\%$  in absolute terms.

OR

$$\frac{2.05}{38.48} \times 100 = 5.32\% \quad \text{in percentage terms.}$$

**ii) Boiler Efficiency if Air Preheater is used.**

$$m_f = 1500 - 0.2 \times 1500 = 1200 \text{ kg/hr}$$

$$\eta = \frac{5000(2896.05 - 125.61) * 100}{1200 * 24000}$$

$$\eta = 48.09\%$$

Improvement if efficiency =  $48.09 - 38.48 = 9.61\%$  in absolute terms.

OR

$$\frac{9.61}{38.48} \times 100 = 24.97\% \quad \text{in percentage terms.}$$

**iii) Boiler Efficiency if both Economizer and Air Preheater are used.**

$$T = 30 + 58 = 88^\circ\text{C}, \quad m_f = 1500 - 0.3 \times 1500 = 1050 \text{ kg/hr}$$

Enthalpy of water at  $88^\circ\text{C}$

$$\begin{aligned} hw &= mC_p(T - 0) \\ &= 1 \times 4.187 \times (88 - 0) \\ &= 368.46 \text{ kJ/kg.} \end{aligned}$$

$$\eta = \frac{5000(2896.05 - 368.46) * 100}{1050 * 24000}$$

$$\eta = 50.15\%$$

Improvement if efficiency =  $50.15 - 38.48 = 11.67\%$  in absolute terms.

OR

$$\frac{11.67}{38.48} \times 100 = 30.33\% \quad \text{in percentage terms.}$$

8) A restaurant, daily uses 600 kg of 95% dry steam produced at a pressure of 3bar. The boiler is fitted with an economizer which increases the feed water temperature to 94° C and is fired using wood and paddy husk in equal proportions. The gross calorific values of wood and paddy husk are 15500kJ/kg and 12600 kJ/kg respectively. The boiler has been operating with an average efficiency of 78%. Calculate the daily consumption of wood and paddy husk?

P = 3bar, T= 94°C, X = 0.95, Q= 600kg/day,

GCV(wood) = 15500kJ/kg, GCV(husk) = 12600kJ/kg ,  $\eta$  = 78%,  $m_{fu}$  = ?

From Steam tables at P= 3bar.

$T_{sat}$  = 133.5°C,  $h_f$  = 561.5 kJ/kg,  $h_{fg}$  = 2163.2 kJ/kg &  $h_g$  = 2724.7 kJ/kg

Enthalpy of water at 94°C

$$\begin{aligned} h_w &= mC_p(T-0) \\ &= 1 \times 4.187 \times (94-0) \\ &= 393.58 \text{ kJ/kg} \end{aligned}$$

Enthalpy at X= 0.95

$$\begin{aligned} h &= h_f + X h_{fg} \\ &= 561.5 + 0.95 \times 2163.2 \\ &= 2616.54 \text{ kJ/kg} \end{aligned}$$

$$\eta = \frac{Q(h_s - h_w) \times 100}{m_{fu} \times GCV}$$

$$78 = \frac{600(2616.54 - 393.58) \times 100}{0.5 \times m_{fu} \times 15500 + 0.5 \times m_{fu} \times 12600}$$

$$m_{fu} = 121.71 \text{ kg/day}$$

Quantity of wood and paddy husk consumed= 0.5\* 121.71

$$= 60.86 \text{ kg each/day}$$