

COM303: Digital Signal Processing

Lecture 7: The DTFT Formalism

Overview:

- ▶ the DTFT of non square-summable sequences
- ► relationships between transforms
- ► modulation

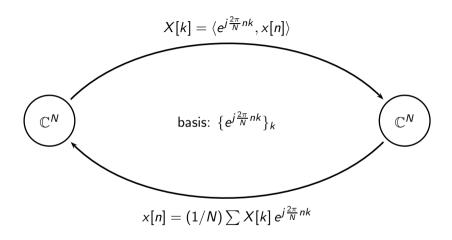


Discrete-Time Fourier Transform

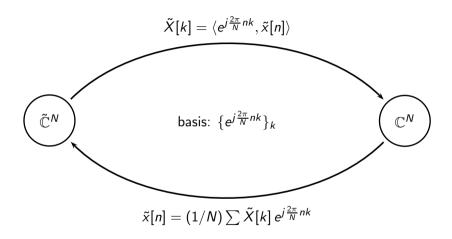
$$X(e^{j\omega}) = \sum_{n=-\infty}^{\infty} x[n] e^{-j\omega n}$$

$$x[n] = rac{1}{2\pi} \int_{-\pi}^{\pi} X(e^{j\omega}) e^{j\omega n} d\omega, \qquad n \in \mathbb{Z}$$

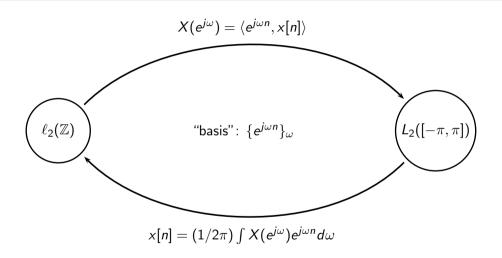
Review: DFT



Review: DFS



DTFT



DTFT as basis expansion

Some things are OK:

- ▶ DFT $\{\delta[n]\}=1$
- $\qquad \text{DTFT} \left\{ \delta[n] \right\} = \langle \mathrm{e}^{\mathrm{j} \omega n}, \delta[n] \rangle = 1$

DTFT as basis expansion

Some things are OK:

- ▶ DFT $\{\delta[n]\}=1$
- lacksquare DTFT $\{\delta[n]\}=\langle e^{j\omega n},\delta[n]
 angle=1$

DTFT as basis expansion

Some things aren't:

- ▶ DFT $\{1\} = \delta[n]$
- ▶ DTFT $\{1\} = \sum_{n=-\infty}^{\infty} e^{-j\omega n} = ?$

▶ problem: too many interesting sequences are *not* square summable!

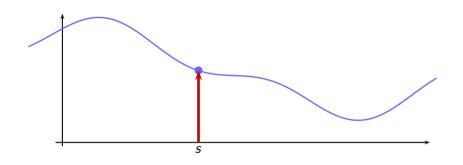


the functional $\delta(t)$ is defined by its "sifting" property:

$$\int_{-\infty}^{\infty} \delta(t-s) f(t) dt = f(s)$$
 for all $f(t), \quad t \in \mathbb{R}.$

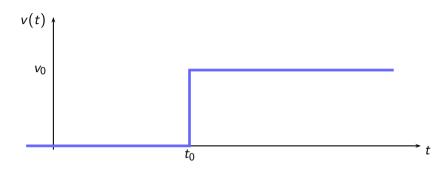
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$$\int_{s-\delta}^{s+\delta} \delta(t-s)f(t)dt = f(s) \qquad orall s \in \mathbb{R}^+$$
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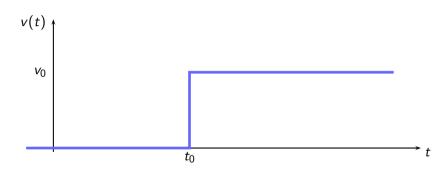


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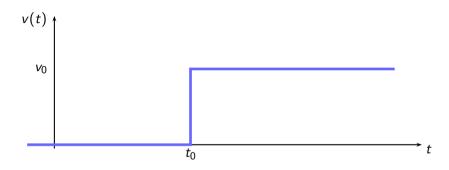
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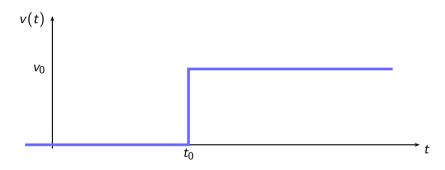
$$F(t) = ma(t) = m \frac{\partial v(t)}{\partial t}$$



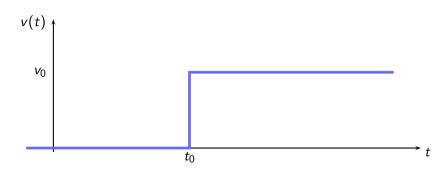
$$a(t_0)=\infty$$
?



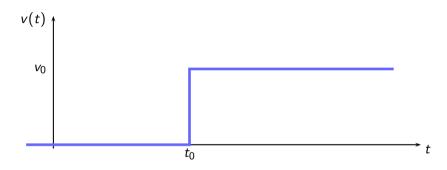
from the other side:
$$v(t) = \int_{-\infty}^{t} a(\tau) d\tau = \begin{cases} 0 & \text{for } t < t_0 \\ v_0 & \text{for } t > t_0 \end{cases}$$



from the other side:
$$v(t) = \int_{-\infty}^{t} v_0 \delta(\tau - t_0) d\tau$$



$$a(t) = v_0 \delta(t - t_0)$$



$$F(t) \propto \delta(t-t_0) pprox egin{cases} \infty & ext{for } t=t_0 \ 0 & ext{otherwise} \end{cases}$$

Intuition

consider a family of *localizing* functions $r_k(t)$ with $k \in \mathbb{N}$ and $t \in \mathbb{R}$ where:

- ightharpoonup support inversely proportional to k
- constant area

1:

Intuition

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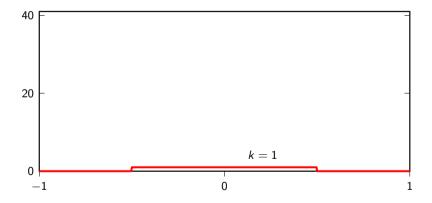
- ► support inversely proportional to *k*
- constant area

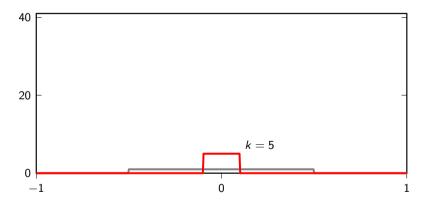
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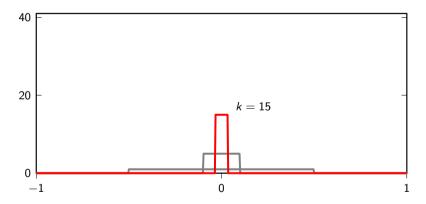
$$\operatorname{rect}(t) = egin{cases} 1 & \operatorname{for}\ |t| < 1/2 \ 0 & \operatorname{otherwise} \end{cases}$$

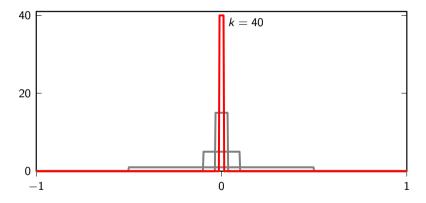
we can build a localizing family as $r_k(t) = k \operatorname{rect}(kt)$:

- ▶ nonzero over [-1/2k, 1/2k], i.e. support is 1/k
- ▶ area is 1







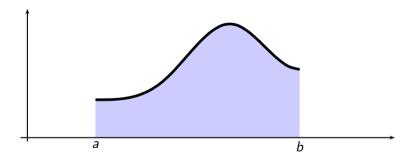


Remember the Mean Value Theorem?

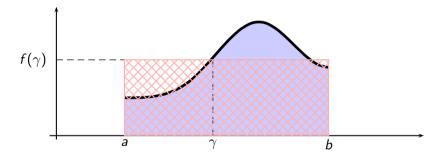
for any continuous function over the interval [a, b] there exists $\gamma \in [a, b]$ s.t.

$$\int_a^b f(t)dt = (b-a)f(\gamma)$$

The Mean Value Theorem



The Mean Value Theorem



Extracting a point value

for our family of localizing functions:

$$\int_{-\infty}^{\infty} r_k(t)f(t)dt = k \int_{-1/2k}^{1/2k} f(t)dt$$
$$= f(\gamma)|_{\gamma \in [-1/2k, 1/2k]}$$

and so:

$$\lim_{k\to\infty}\int_{-\infty}^{\infty}r_k(t)f(t)dt=f(0)$$

The delta functional is a shorthand. Instead of writing

$$\lim_{k\to\infty}\int_{-\infty}^{\infty}r_k(t-s)f(t)dt$$

we write

$$\int_{-\infty}^{\infty} \delta(t-s)f(t)dt.$$

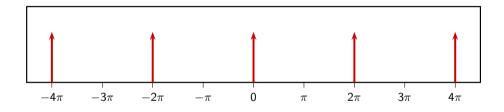
as if
$$\lim_{k\to\infty} r_k(t) = \delta(t)$$
,

The "pulse train"

$$\tilde{\delta}(\omega) = 2\pi \sum_{k=-\infty}^{\infty} \delta(\omega - 2\pi k)$$

just a technicality to use the Dirac delta in the space of 2π -periodic functions

Graphical representation



Now let the show begin!

$$\begin{split} \mathsf{IDTFT}\left\{\tilde{\delta}(\omega)\right\} &= \frac{1}{2\pi} \int_{-\pi}^{\pi} \tilde{\delta}(\omega) e^{j\omega n} d\omega \\ &= \int_{-\pi}^{\pi} \delta(\omega) e^{j\omega n} d\omega \\ &= e^{j\omega n}|_{\omega=0} \\ &= 1 \end{split}$$

Now let the show begin!

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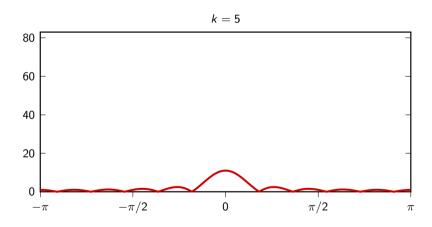
In other words

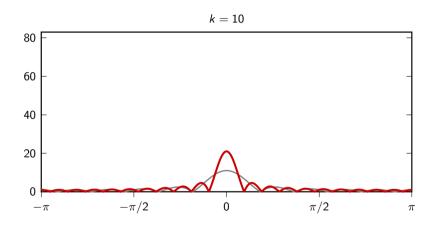
$$\mathsf{DTFT}\left\{1
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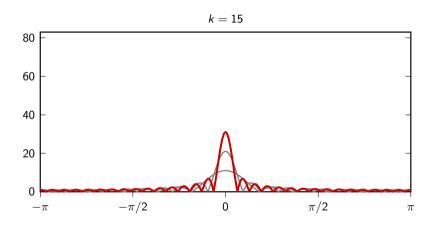
Does it make sense?

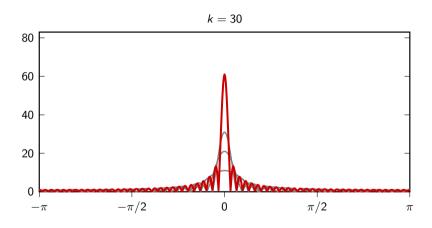
Partial DTFT sum:

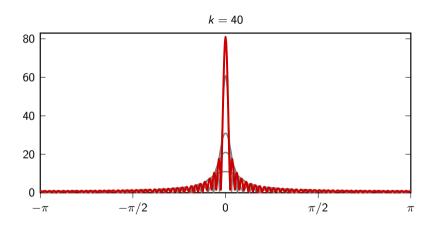
$$S_k(\omega) = \sum_{n=-k}^k e^{-j\omega n}$$











Does it make sense?

Partial DTFT sums look like a family of localizing functions:

$$S_k(\omega) o ilde{\delta}(\omega)$$

$$\mathsf{IDTFT}\left\{ ilde{\delta}(\omega-\omega_0)
ight\}=e^{j\omega_0 n}$$

- ▶ DTFT $\{1\} = \tilde{\delta}(\omega)$
- $\blacktriangleright \mathsf{DTFT}\left\{e^{j\omega_0 n}\right\} = \tilde{\delta}(\omega \omega_0)$
- ▶ DTFT $\{\cos \omega_0 n\} = [\tilde{\delta}(\omega \omega_0) + \tilde{\delta}(\omega + \omega_0)]/2$
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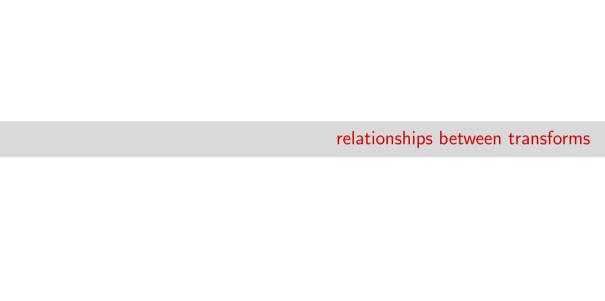
- ▶ Dirac delta in the DTFT ⇒ signal is NOT finite-energy (eg. periodic, constant etc)
- ▶ signal must still be a power signal (finite energy over finite sections)
- Dirac deltas make sense only if integrals are involved; where are the integrals?
 - $\bar{w}[n] = 1$ only for $M \le n \le N \Rightarrow \mathsf{DTFT}\{x[n]\bar{w}[n]\} = \int_{-\pi}^{\pi} X(e^{j(\sigma-\omega)})W(e^{j\sigma})d\sigma$: OKK
 - h[n] stable filter \Rightarrow DTFT $\{x[n]*h[n]\} = X(e^{i\omega})H(e^{i\omega})$: Diracs still there

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Overview:

- ▶ DFT, DFS, DTFT
- ▶ DTFT of periodic sequences
- ► DTFT of finite-support sequences
- Zero padding

- ▶ DFT, DFS: change of basis in \mathbb{C}^N
- ▶ DTFT: "formal" change of basis in $\ell_2(\mathbb{Z})$
- basis vectors are "building blocks" for any signal
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- ▶ N-tap signal x[n]
- ▶ natural spectral representation: DFT X[k]
- two ways to embed x[n] into an infinite sequence:
 - periodic extension: $\tilde{x}[n] = x[n \mod N]$
 - finite-support extension: $\bar{x}[n] = \begin{cases} x[n] & 0 \leq n < N \\ 0 & \text{otherwise} \end{cases}$
- ▶ how does X[k] relate to the DTFT of the embedded signals?

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DTFT of periodic signals

$$\tilde{x}[n] = x[n \mod N]$$

$$\tilde{X}(e^{j\omega}) = \sum_{n=-\infty}^{\infty} \tilde{x}[n]e^{-j\omega n}$$

$$= \sum_{n=-\infty}^{\infty} \left(\frac{1}{N} \sum_{k=0}^{N-1} \tilde{X}[k]e^{j\frac{2\pi}{N}nk}\right) e^{-j\omega n}$$

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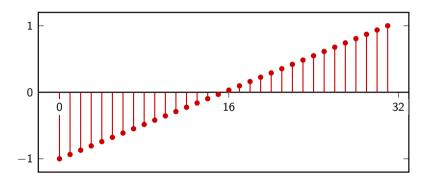
We've seen this before

$$\begin{split} \sum_{n=-\infty}^{\infty} e^{j\frac{2\pi}{N}nk} e^{-j\omega n} &= \mathsf{DTFT}\left\{e^{j\frac{2\pi}{N}nk}\right\} \\ &= \tilde{\delta}(\omega - \frac{2\pi}{N}k) \end{split}$$

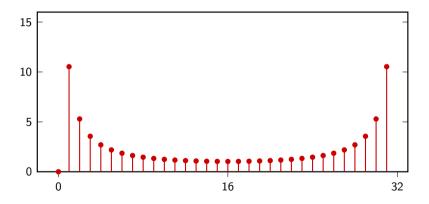
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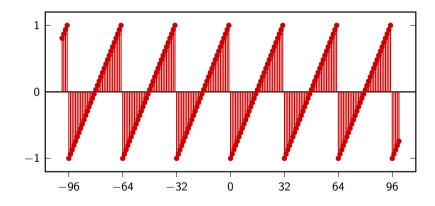
32-tap sawtooth



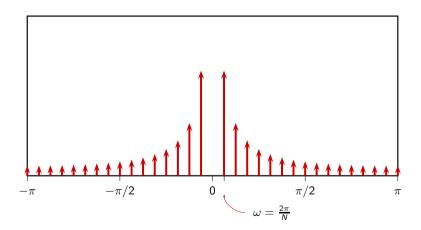
DFT of 32-tap sawtooth



32-periodic sawtooth



DTFT of periodic extension



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$$= \sum_{n=0}^{N-1} \left(\frac{1}{N} \sum_{k=0}^{N-1} X[k]e^{j\frac{2\pi}{N}nk}\right) e^{-j\omega n}$$

$$= \frac{1}{N} \sum_{k=0}^{N-1} X[k] \left(\sum_{n=0}^{N-1} e^{-j(\omega - \frac{2\pi}{N}k)n}\right)$$

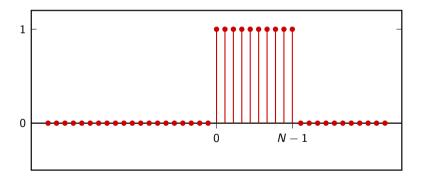
$$\sum_{n=0}^{N-1} e^{-j(\omega - \frac{2\pi}{N}k)n} = \bar{R}(e^{j(\omega - \frac{2\pi}{N}k)})$$

where $\bar{R}(e^{j\omega})$ is the DTFT of $\bar{r}[n]$, the rectangular signal:

$$ar{r}[n] = egin{cases} 1 & 0 \leq n < N \ 0 & ext{otherwise} \end{cases}$$

Rectangular step signal

$$ar{r}[n] = egin{cases} 1 & 0 \leq n < N \ 0 & ext{otherwise} \end{cases}$$



$$\bar{R}(e^{j\omega}) = \sum_{n=0}^{N-1} e^{-j\omega n}$$

$$= \frac{1 - e^{-j\omega N}}{1 - e^{-j\omega}}$$

$$= \frac{e^{-j\frac{\omega N}{2}} \left[e^{j\frac{\omega N}{2}} - e^{-j\frac{\omega N}{2}} \right]}{e^{-j\frac{\omega}{2}} \left[e^{j\frac{\omega}{2}} - e^{-j\frac{\omega}{2}} \right]}$$

$$= \frac{\sin\left(\frac{\omega}{2}N\right)}{\sin\left(\frac{\omega}{2}\right)} e^{-j\frac{\omega}{2}(N-1)}$$

$$\bar{R}(e^{j\omega}) = \sum_{n=0}^{N-1} e^{-j\omega n}$$

$$= \frac{1 - e^{-j\omega N}}{1 - e^{-j\omega}}$$

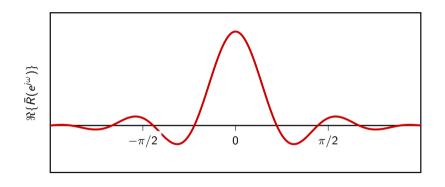
$$= \frac{e^{-j\frac{\omega N}{2}} \left[e^{j\frac{\omega N}{2}} - e^{-j\frac{\omega N}{2}} \right]}{e^{-j\frac{\omega}{2}} \left[e^{j\frac{\omega}{2}} - e^{-j\frac{\omega}{2}} \right]}$$

$$= \frac{\sin\left(\frac{\omega}{2}N\right)}{\sin\left(\frac{\omega}{2}\right)} e^{-j\frac{\omega}{2}(N-1)}$$

$$\begin{split} \bar{R}(e^{j\omega}) &= \sum_{n=0}^{N-1} e^{-j\omega n} \\ &= \frac{1 - e^{-j\omega N}}{1 - e^{-j\omega}} \\ &= \frac{e^{-j\frac{\omega N}{2}} \left[e^{j\frac{\omega N}{2}} - e^{-j\frac{\omega N}{2}} \right]}{e^{-j\frac{\omega}{2}} \left[e^{j\frac{\omega}{2}} - e^{-j\frac{\omega}{2}} \right]} \\ &= \frac{\sin\left(\frac{\omega}{2}N\right)}{\sin\left(\frac{\omega}{2}\right)} e^{-j\frac{\omega}{2}(N-1)} \end{split}$$

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DTFT of interval signal (N = 9)



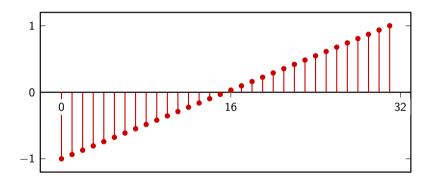
note that
$$ar{R}(e^{j\omega})=0$$
 for $\omega=2\pi k/N$, $k\in\mathbb{Z}/\{0\}$

define
$$\Lambda(\omega)=rac{1}{N}ar{R}(e^{j\omega})$$

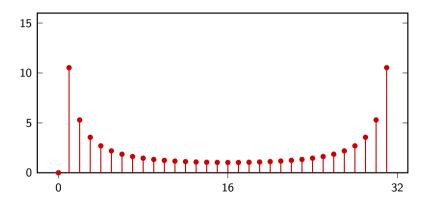
$$ar{X}(e^{j\omega}) = \sum_{k=0}^{N-1} X[k] \Lambda(\omega - \frac{2\pi}{N}k)$$

smooth interpolation of DFT values

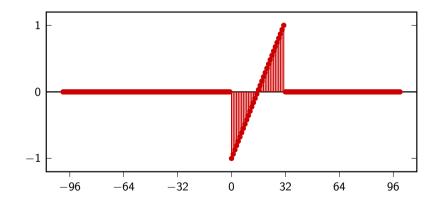
32-tap sawtooth

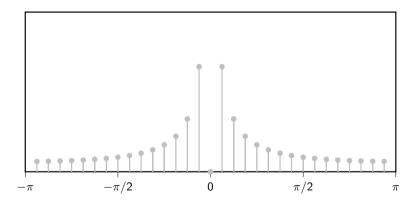


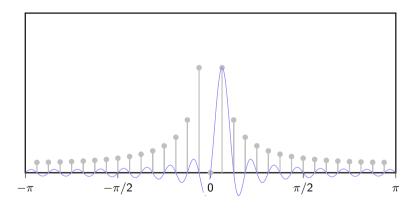
DFT of 32-tap sawtooth

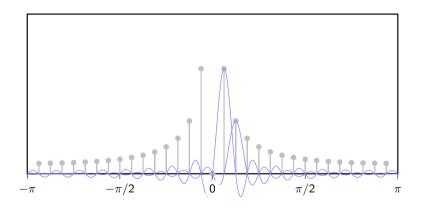


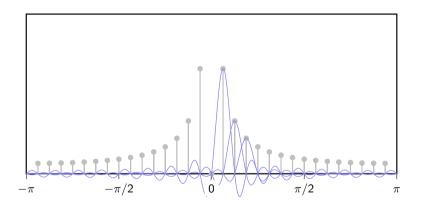
Sawtooth: finite support extension

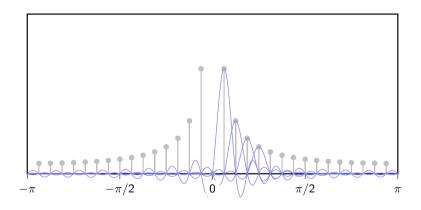


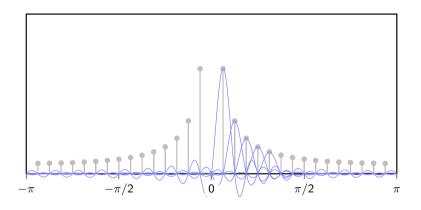




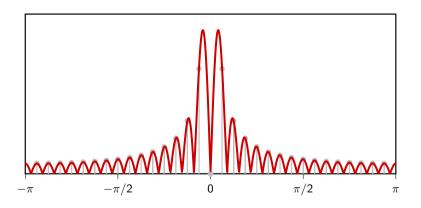




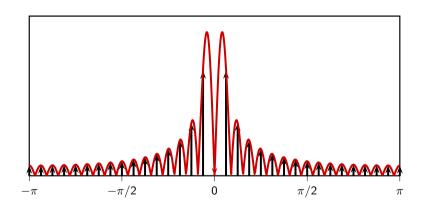




DTFT of finite support extension

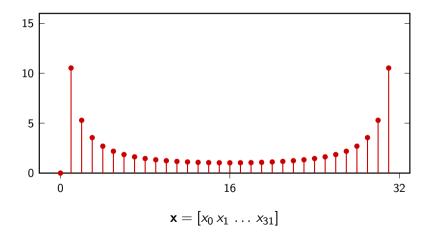


As a comparison...

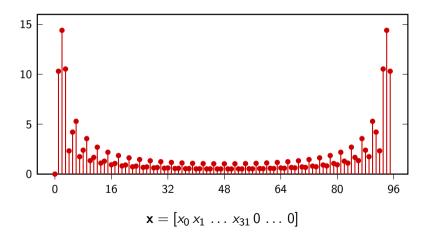


When computing the DFT numerically one may "pad" the data vector with zeros to obtain "nicer" plots

DFT of 32-tap sawtooth



DFT of 32-tap sawtooth, zero-padded to 96 points



$$x_M[n] = \begin{cases} x[n] & \text{for } 0 \le n < N \\ 0 & \text{for } N \le n < M \end{cases}$$

$$X_{M}[h] = \sum_{n=0}^{M-1} x'[n] e^{-j\frac{2\pi}{M}nh} = \sum_{n=0}^{N-1} x[n] e^{-j\frac{2\pi}{M}nh}$$

$$= \sum_{n=0}^{N-1} \left(\frac{1}{N} \sum_{k=0}^{N-1} X[k] e^{j\frac{2\pi}{N}nk}\right) e^{-j\frac{2\pi}{M}nh}$$

$$= \frac{1}{N} \sum_{k=0}^{N-1} X[k] \left(\sum_{n=0}^{N-1} e^{-j(\frac{2\pi}{M}h - \frac{2\pi}{N}k)n}\right)$$

$$= \bar{X}(e^{j\omega})|_{\omega = \frac{2\pi}{M}h}$$

$$X_{M}[h] = \sum_{n=0}^{M-1} x'[n]e^{-j\frac{2\pi}{M}nh} = \sum_{n=0}^{N-1} x[n]e^{-j\frac{2\pi}{M}nh}$$

$$= \sum_{n=0}^{N-1} \left(\frac{1}{N}\sum_{k=0}^{N-1} X[k]e^{j\frac{2\pi}{N}nk}\right) e^{-j\frac{2\pi}{M}nh}$$

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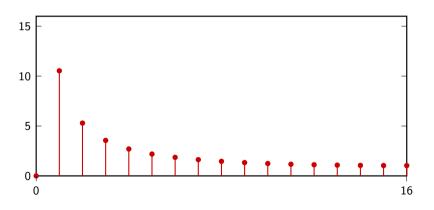
$$= \sum_{n=0}^{N-1} \left(\frac{1}{N}\sum_{k=0}^{N-1} X[k]e^{j\frac{2\pi}{N}nk}\right) e^{-j\frac{2\pi}{M}nh}$$

$$= \frac{1}{N}\sum_{k=0}^{N-1} X[k] \left(\sum_{n=0}^{N-1} e^{-j(\frac{2\pi}{M}h - \frac{2\pi}{N}k)n}\right)$$

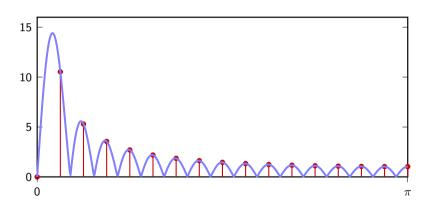
$$= \bar{X}(e^{j\omega})|_{\omega = \frac{2\pi}{M}h}$$

- zero padding does not add information
- ▶ a zero-padded DFT is simply a sampled DTFT of the finite-support extension

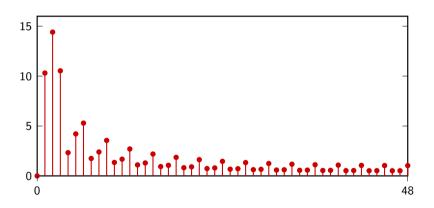




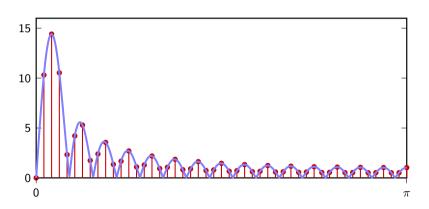




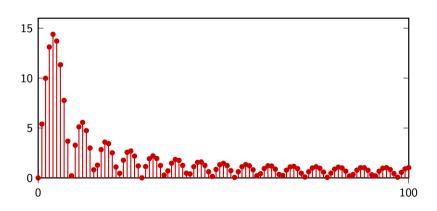


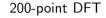


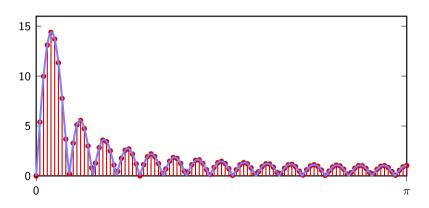




200-point DFT









Overview:

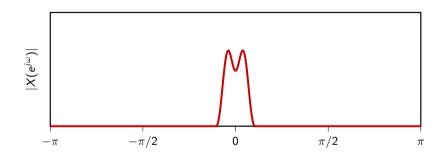
- ► Lowpass, highpass and bandpass signals
- ► Sinusoidal modulation
- ► Tuning a guitar

Classifying signals in frequency

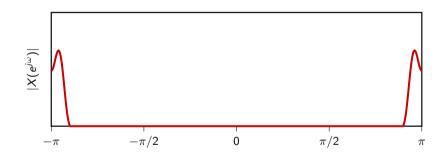
Three broad categories according to where most of the spectral energy resides:

- ▶ lowpass signals (also known as "baseband" signals)
- highpass signals
- bandpass signals

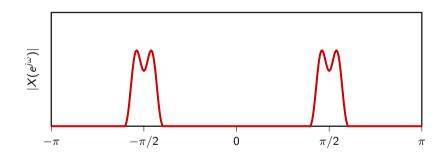
Lowpass example



Highpass example



Bandpass example



DTFT
$$\{x[n]\cos(\omega_c n)\}$$
 = DTFT $\left\{\frac{1}{2}e^{j\omega_c n}x[n] + \frac{1}{2}e^{-j\omega_c n}x[n]\right\}$
= $\frac{1}{2}\left[X(e^{j(\omega-\omega_c)}) + X(e^{j(\omega+\omega_c)})\right]$

- ightharpoonup usually x[n] baseband
- $ightharpoonup \omega_c$ is the *carrier* frequency

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$$= \frac{1}{2}\left[X(e^{j(\omega-\omega_c)}) + X(e^{j(\omega+\omega_c)})\right]$$

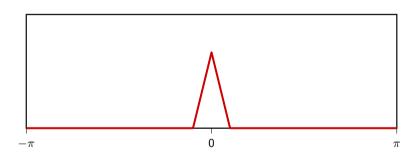
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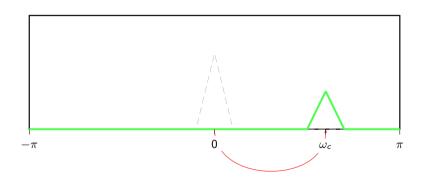
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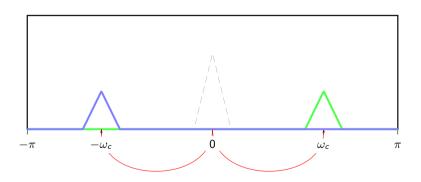
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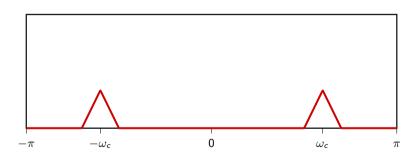
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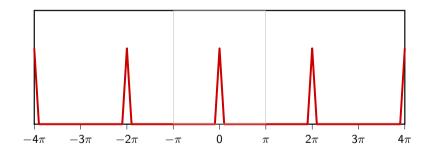
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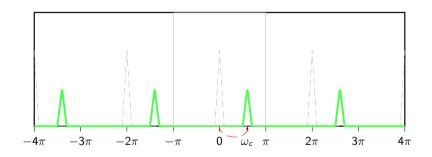


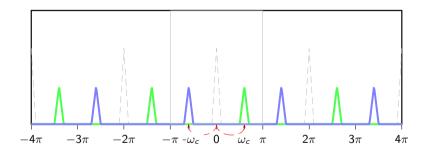


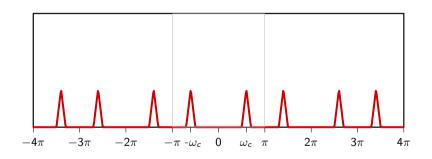


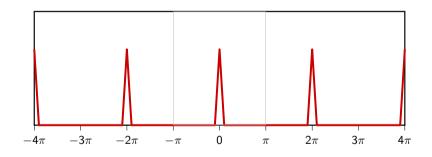


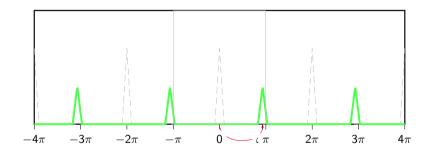


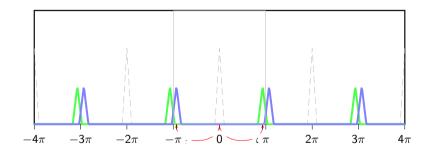


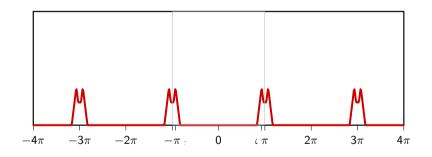


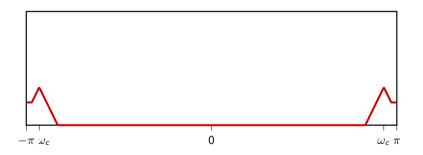












Sinusoidal modulation: applications

- voice and music are lowpass signals
- radio channels are bandpass, in much higher frequencies
- modulation brings the baseband signal in the transmission band
- demodulation at the receiver brings it back

just multiply the received signal by the carrier again

$$y[n] = x[n]\cos(\omega_c n)$$
 $Y(e^{j\omega}) = \frac{1}{2}\left[X(e^{j(\omega-\omega_c)}) + X(e^{j(\omega+\omega_c)})\right]$

$$DTFT \{y[n] \cdot 2\cos(\omega_c n)\} = Y(e^{j(\omega - \omega_c)}) + Y(e^{j(\omega + \omega_c)})$$

$$= \frac{1}{2} \left[X(e^{j(\omega - 2\omega_c)}) + X(e^{j(\omega)}) + X(e^{j(\omega)}) + X(e^{j(\omega + 2\omega_c)}) \right]$$

$$= X(e^{j(\omega)}) + \frac{1}{2} \left[X(e^{j(\omega - 2\omega_c)}) + X(e^{j(\omega + 2\omega_c)}) \right]$$

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69

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69

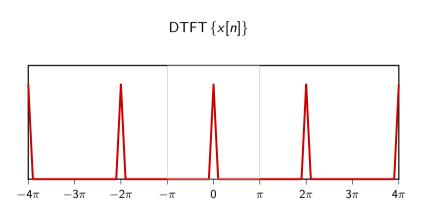
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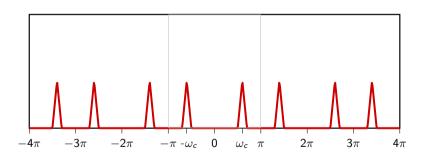
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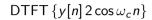
69

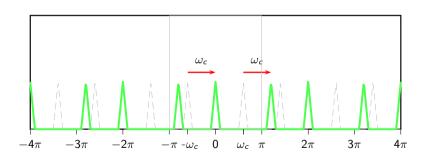
Demodulation in the frequency domain

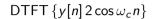


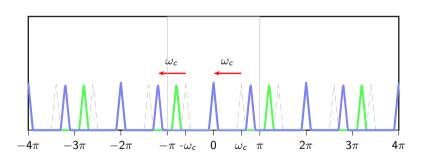
$$\mathsf{DTFT}\{y[n]\} = \mathsf{DTFT}\{x[n]\cos\omega_c n\}$$

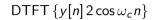


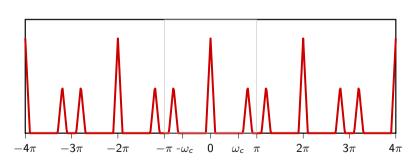


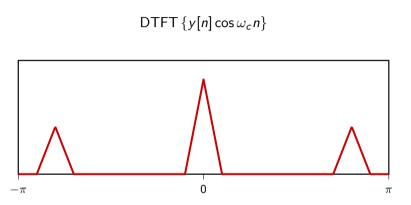












- ▶ we recovered the baseband signal exactly...
- ▶ but we have some spurious high-frequency components
- ▶ in the next lectures we will learn how to get rid of them!

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Another application: tuning a guitar

Problem (abstraction):

- lacktriangleright reference sinusoid at frequency ω_0
- ightharpoonup tunable sinusoid of frequency ω
- ▶ make $\omega = \omega_0$ "by ear"

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The procedure

- 1. bring ω close to ω_0 (easy)
- 2. when $\omega \approx \omega_0$ play both sinusoids together
- 3. trigonometry comes to the rescue:

$$\begin{aligned} & \times[n] = \cos(\omega_0 n) + \cos(\omega n) \\ & = 2\cos\left(\frac{\omega_0 + \omega}{2}n\right)\cos\left(\frac{\omega_0 - \omega}{2}n\right) \\ & \approx 2\cos(\Delta_\omega n)\cos(\omega_0 n) \end{aligned}$$

The procedure

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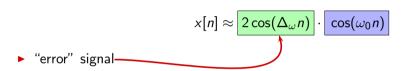
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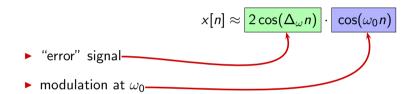
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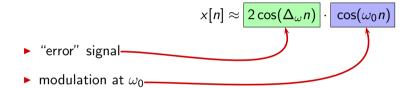
- "error" signal
- ightharpoonup modulation at ω_0
- when $\omega \approx \omega_0$, the error signal is too low to be heard; modulation brings it up to hearing range and we perceive it as amplitude oscillations of the carrier frequency



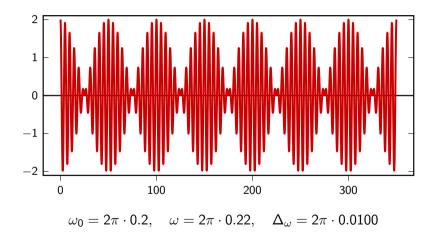
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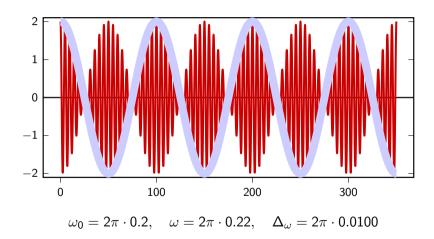


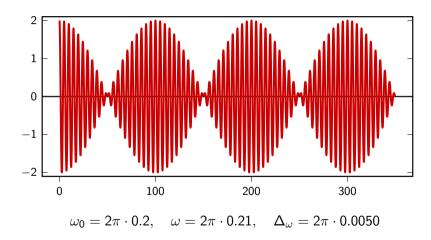
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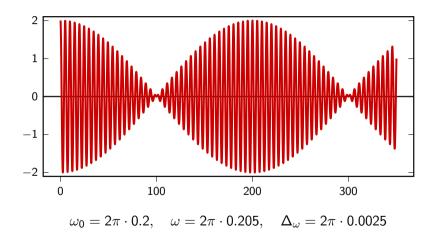


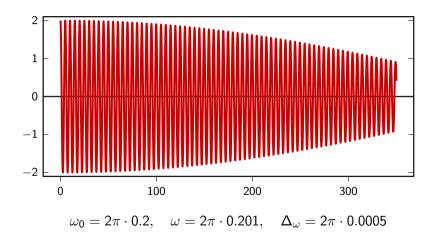
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demonstration