# Calculus Cheat Sheet

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## Based on notes by Dr A.G. Walton

## 1 Basics

Formulae relating permutation and Kronecker delta:

$$\epsilon_{ijk}\epsilon_{klm} = \delta_{il}\delta_{jm} - \delta_{im}\delta_{jl}$$

$$\epsilon_{ijk}\epsilon_{ilm} = \delta_{jl}\delta_{km} - \delta_{jm}\delta_{kl}$$

Dot product

$$\mathbf{a}.\mathbf{b} = a_i b_i$$

Cross product

$$[\boldsymbol{a} \times \boldsymbol{b}]_i = \epsilon_{ijk} a_j b_k$$

Triple scalar product

$$\boldsymbol{a}.(\boldsymbol{b}\times\boldsymbol{c})=\epsilon_{ijk}a_ib_ic_k$$

$$\boldsymbol{a}.(\boldsymbol{b}\times\boldsymbol{c})=0\Leftrightarrow a,b,c$$
 are coplanar.

$$a.(b \times c) = (a \times b).c$$

Triple vector product

$$a \times (b \times c) = (a.c)b - (a.b)c$$

# 2 Gradient, divergence and curl

Gradient & directional derivative

$$\nabla \phi = \frac{\partial \phi}{\partial x} \hat{\boldsymbol{i}} + \frac{\partial \phi}{\partial y} \hat{\boldsymbol{j}} + \frac{\partial \phi}{\partial z} \hat{\boldsymbol{k}}, \frac{\partial \phi}{\partial s} = \hat{\boldsymbol{s}}.\nabla \phi$$

note that  $\hat{s}$  here must be unit vector.

Formal definition of gradient, S is a surface,  $\tau$  is the volume of region enclosed by S:

$$\nabla \phi = \lim_{\tau \to 0} \frac{1}{\tau} \int_{S} \widehat{\boldsymbol{n}} \, \phi \, dS$$

Laplace

$$\nabla^2 \phi := \nabla \cdot \nabla \phi = \frac{\partial^2}{\partial x_i^2} \phi$$
$$[\nabla^2 \mathbf{A}]_i = \frac{\partial^2}{\partial x_i^2} \mathbf{A}_i$$

Finding tangent plane at point P:

1. Change the equation of surface to  $\phi(x, y, z) = c$  where c is a constant. Try to use addition instead of multiplication so that  $\phi$  is more linear.

2.

$$\left. \frac{\partial \phi}{\partial x} \right|_{P} (x - x_{P}) + \left. \frac{\partial \phi}{\partial y} \right|_{P} (y - y_{P}) + \left. \frac{\partial \phi}{\partial z} \right|_{P} (z - z_{P})$$

is the equation of tangent plane.

For a vector field A

$$div(\mathbf{A}) = \nabla \cdot \mathbf{A}, \quad curl(\mathbf{A}) = \nabla \times \mathbf{A}$$

Note: 2D curl is defined assuming it is on x - y plane of 3-D space, so

$$curl(\mathbf{A}) = \left(\frac{\partial A_2}{\partial x} - \frac{\partial A_1}{\partial y}\right) \hat{\mathbf{k}}$$

Strict definitions:

$$div(\mathbf{A}) = \lim_{\tau \to 0} \frac{1}{\tau} \int_{S} (\widehat{\mathbf{n}}.\mathbf{A}) dS \qquad curl(\mathbf{A}) = \lim_{\tau \to 0} \frac{1}{\tau} \int_{S} (\widehat{\mathbf{n}} \times \mathbf{A}) dS$$

Properties:

- $\nabla(\phi_1 + \phi_2) = \nabla\phi_1 + \nabla\phi_2$
- $div(\mathbf{A} + \mathbf{B}) = div(\mathbf{A}) + div(\mathbf{B}), \ curl(\mathbf{A} + \mathbf{B}) = curl(\mathbf{A}) + curl(\mathbf{B})$
- $\nabla(\phi\psi) = \phi\nabla\psi + \psi\nabla\phi$
- $div(\phi \mathbf{A}) = \phi div(\mathbf{A}) + \nabla \phi \cdot \mathbf{A}$ ,  $curl(\phi \mathbf{A}) = \phi curl(\mathbf{A}) + \nabla \phi \times \mathbf{A}$
- $div(\mathbf{A} \times \mathbf{B}) = \mathbf{B}.curl(\mathbf{A}) \mathbf{A}.curl(\mathbf{B})$
- $curl(\mathbf{A} \times \mathbf{B}) = (\mathbf{B} \cdot \nabla)\mathbf{A} (\mathbf{A} \cdot \nabla)\mathbf{B} + div(\mathbf{B})\mathbf{A} div(\mathbf{A})\mathbf{B}$
- $\nabla(A.B) = (B.\nabla)A + (A.\nabla)B + B \times curl(A) + A \times curl(B)$
- $curl(\nabla \phi) = 0$
- $div(curl(\mathbf{A})) = 0$
- $curl(curl(\mathbf{A})) = \nabla(div(\mathbf{A})) \nabla^2 \mathbf{A}$

Irrotational vector field:  $curl(\mathbf{A}) = 0$  solenoid vector field:  $div(\mathbf{A}) = 0$ 

# 3 Integrals

### 3.1 Line Integral

$$\int_{\gamma} f \, ds := \lim_{N \to \infty, \max(\delta s_n) \to 0} \sum_{n=1}^{N} f_n \delta s_n$$

where  $\delta s_n$  are lengths of segments on the path  $\gamma$ (must be smooth or piece-wise smooth). Function f is usually a scalar field, if it is vector field, integral is calculated element-wise.

Length of path  $\gamma$  can be calculated using integration  $l = \int_{\gamma} ds$ . If  $\gamma$  is y = y(x), then the arc length between (a, f(a)), (b, f(b)) is

$$\int_{a}^{b} \sqrt{1 + \left(\frac{dy}{dx}\right)^2} \, dx$$

ds - Change of arc length,  $\hat{\boldsymbol{t}} = \frac{d\boldsymbol{r}}{ds}$  - tangent vector,  $d\boldsymbol{r} = \hat{\boldsymbol{t}}ds$  - path element. So we have another line integral defined for vector field  $\boldsymbol{F}$ :

$$\int_{\gamma} \boldsymbol{F} \cdot d\boldsymbol{r} := \int_{\gamma} (\boldsymbol{F} \cdot \hat{t}) \ ds$$

Circulation: when the path is closed (same beginning and end point) denoted as  $\oint_{\gamma} F . dr$ 

Field  $\mathbf{F}$  is conservative (circulation around any closed path  $\gamma$  is 0)  $\Leftrightarrow \mathbf{F} = \nabla \phi$  for some function  $\phi$ . ( $\phi$  is called potential)  $\Leftrightarrow curl(\mathbf{F}) = 0$ . In this case, given any path  $\gamma$  joining point A, B, we have

$$\int_{\gamma} f \ ds = \phi(B) - \phi(A)$$

Steps to find potential  $\phi$ :

- $\frac{\partial \phi}{\partial x} = F_1$  so integrate  $F_1$  w.r.t. x to find  $\phi$ . The integration constant should be C(y,z) (a function depending on y,z only)
- Then differentiation  $\phi$  w.r.t y and compare with  $F_2$  to solve for C(y,z). It should be of the form g(y,z) + C(z).
- Finally differentiation  $\phi$  w.r.t. z. You may leave the constant c there as there is no way to ger rid of it.

Another practical result is if there is a vector field  $\mathbf{B}$  s.t.  $curl(\mathbf{B}) = \mathbf{A}$ , then  $div(\mathbf{A}) = 0$ 

#### **Evaluation Line Integral**

With parameterisation  $x = x(t), y = y(t), z = z(t)t_0 \le t \le t_1$ , we have

$$\int_{\gamma} \mathbf{F} \cdot d\mathbf{r} = \int_{t_0}^{t_1} \left( F_1 \frac{dx}{dt} + F_2 \frac{dy}{dt} + F_3 \frac{dz}{dt} \right) dt$$

#### 3.2 Surface Integral

Some definitions: Convex surface: crossed by any straight line at most twice. Closed surface: can divide the space into two non-connected regions. (interior & exterior)

Simply Connected Region: Any curve inside the region can be shrunk to a point (any point) without leaving the region. Otherwise the region is called multiply-connected.

Similar to line integral, we define surface integral on surface S as below

$$\int_{S} f \, dS := \lim_{N \to \infty, \max(\delta S_n) \to 0} \sum_{n=1}^{N} f_n \delta S_n$$

dS - area element (infinite small area of surface),  $d\mathbf{S} = \hat{\mathbf{n}} dS$  - vector areal element ( $\hat{\mathbf{n}}$  is normal to dS). Note area of S can be calculated using  $\int_{S} 1 \, dS$ .

#### Evaluating surface integral

$$I = \int_{S} f(P)dS$$

where P is a general point on surface S.

#### 1. (From our notes) Projection

Choose a plane to project to (say the x, y plane) and find projection area  $\Sigma$  and normal vector  $\widehat{\boldsymbol{m}} = \widehat{\boldsymbol{k}}$  to projected plane. Change variables in f(x, y, z) if necessary to get rid of z (using the equation of surface S, NOT equation of  $\Sigma$ )

$$I = \int_{\Sigma} f(P) \frac{dx \, dy}{|\widehat{\boldsymbol{n}}.\widehat{\boldsymbol{k}}|}$$

where  $\hat{\boldsymbol{n}}$  is normal to S and it may depend on x,y,z. If the surface is given by g(x,y,z)=c for some constant c, then  $\hat{\boldsymbol{n}}=\nabla g/|\nabla g|$  (ALWAYS remember to check  $\hat{\boldsymbol{n}}$  is pointing to exterior of region). Projection to other planes can be done similarly.

#### 2. Parameterisation

Any surface can be parameterised by two parameters say  $\mathbf{r} = \mathbf{r}(\theta, \phi)$ . For scalar function f:

$$\int_{S} f(\boldsymbol{r}) dS = \iint_{A} f(\boldsymbol{r}(\theta, \phi)) \left| \frac{\partial \boldsymbol{r}}{\partial \theta} \times \frac{\partial \boldsymbol{r}}{\partial \phi} \right| d\phi \ d\theta$$

where A is the corresponding area on  $\theta - \phi$  plane. For vector field F:

$$\int_{S} \boldsymbol{F}(\boldsymbol{r}) . d\boldsymbol{S} = \iint_{A} (\boldsymbol{F}(\boldsymbol{r}(\theta, \phi)) . \widehat{\boldsymbol{n}}) \left| \frac{\partial \boldsymbol{r}}{\partial \theta} \times \frac{\partial \boldsymbol{r}}{\partial \phi} \right| d\phi \ d\theta$$

where  $\hat{n}$  is unit normal to surface S.

## 3.3 Volume Integral

If  $\tau$  is a region in 3D space,  $\int_{\tau} f d\tau$  (defined similar to above) is volume integral where  $d\tau = dx \, dy \, dz$  is volume element.

### 3.4 Some useful Integrals

Given curve  $y = y(x), x \in [a, b]$ , the arc length is

$$\int_a^b \sqrt{1 + (\frac{dy}{dx})^2} \, dx$$

surface area of surface generated by revolving y = y(x) between x = a, b about x-axis is:

$$2\pi \int_a^b y\sqrt{1+(\frac{dy}{dx})^2}\ dx$$

for revolution about y-aixs:

$$2\pi \int_a^b x \sqrt{1 + (\frac{dy}{dx})^2} \ dx$$

volume of revolution about x-axis is

$$\int_{a}^{b} \pi y^{2} dx$$

volume of revolution about y-axis is

$$\int_a^b \pi x^2 \ dy$$

# 4 Green's theorem, divergence theorem and Stokes theorem

Green's theorem gives an important connection between line integral and surface integral. If R is a closed plane region bounded by simple closed convex curve C (anti-clockwise) and  $\boldsymbol{F} = \begin{pmatrix} P \\ Q \end{pmatrix}$ :

$$\oint_C \boldsymbol{F}.d\boldsymbol{r} = \oint_C \left(P \; dx + Q \; dy\right) = \iint_R \left(\frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y}\right) \; dS$$

Green's theorem is proved directly for simply connected convex R but can be generalised to non-convex/multiply connected regions using suitable breakdown. For example, given a region R is bounded by an interior boundary  $C_0$  (clockwise) and an exterior boundary  $C_1$  (anti-clockwise):

$$\oint_{C_1} \mathbf{F} . d\mathbf{r} - \oint_{C_0} \mathbf{F} . d\mathbf{r} = \iint_R \left( \frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y} \right) dS$$

If F is undefined at some point P in region R, you should dig a circle with radius r around point P, calculate the integral and then let  $r \to 0$ .

**Area of a region** If a closed region has boundary curve C, then its area is given by

$$\frac{1}{2} \oint_C (x \, dy - y \, dx)$$

This integral can be calculated by parametrisation.

#### Flux

Flux of a surface S and vector field A is

$$\int_{S} \mathbf{A} \cdot \widehat{\mathbf{n}} dS$$

where  $\hat{n}$  is normal to surface S.

#### Divergence theorem

For closed convex surface S with normal  $\hat{n}$  and region  $\tau$  enclosed by S that is simply connected. A is a vector field with continuous derivative on  $\tau$ :

$$\int_{S} \mathbf{A} . d\mathbf{S} = \int_{S} \mathbf{A} . \hat{\mathbf{n}} \ dS = \int_{\tau} div(\mathbf{A}) d\tau$$

This can be generalised to non-convex surfaces and multiply-connected regions just like Green's theorem.

You can use divergence theorem to evaluate  $\int_{\tau} f(\mathbf{r}) d\tau$  but you have to first find function  $\mathbf{A}(\mathbf{r})$  s.t.  $div \mathbf{A} = f$ . Try to pick  $\mathbf{A}$  as simple as possible (say,  $\mathbf{A} = x\mathbf{i}$ )

Green's identities:  $(\phi, \psi)$  are scalar functions, other symbols have the same meaning as in Divergence theorem)

$$\iint_{S} \phi \frac{\partial \psi}{\partial \boldsymbol{n}} dS = \int_{\tau} \phi \nabla^{2} \psi + \nabla \phi \cdot \nabla \psi d\tau$$

$$\iint_{S} \phi \frac{\partial \psi}{\partial \boldsymbol{n}} - \psi \frac{\partial \phi}{\partial \boldsymbol{n}} dS = \int_{\tau} \left( \phi \nabla^{2} \psi - \psi \nabla^{2} \phi \right) d\tau$$

Generalised integration by part: (R is region enclosed by curve C)

$$\iint_{R} \phi \nabla^{2} \psi \, dx \, dy = \oint_{C} \phi \frac{\partial \psi}{\partial \mathbf{n}} dS - \iint_{R} \nabla \phi \cdot \nabla \psi \, dx \, dy$$

Gauss's flux theorem: S is closed surface with normal  $\hat{n}$  and O means origin.

$$\int_{S} \frac{\widehat{\boldsymbol{n}}.\boldsymbol{r}}{|\boldsymbol{r}|^{3}} dS = \begin{cases} 0 & \text{if O is exterior} \\ 4\pi & \text{if O is interior} \end{cases}$$

Stokes theorem S is open surface with boundary curve  $\gamma$ .  $\boldsymbol{A}$  is continuously differentiable on S,

$$\oint_{\gamma} \boldsymbol{A}.d\boldsymbol{r} = \int_{S} curl(\boldsymbol{A}).\widehat{\boldsymbol{n}} \ dS$$

Note LHS is independent of the surface S chosen.

# 5 Curvillinear system

For coordinate system  $\mathbf{x} = (x_1, x_2, x_3)$ , transformation to new coordinate system  $\mathbf{u} = (u_1, u_2, u_3)$  is possible if

$$\det(J(u_x)) = \det\left(\begin{pmatrix} \frac{\partial u_1}{\partial x_1} & \frac{\partial u_1}{\partial x_2} & \frac{\partial u_1}{\partial x_3} \\ \frac{\partial u_2}{\partial x_1} & \frac{\partial u_2}{\partial x_2} & \frac{\partial u_2}{\partial x_3} \\ \frac{\partial u_3}{\partial x_1} & \frac{\partial u_3}{\partial x_2} & \frac{\partial u_3}{\partial x_3} \end{pmatrix}\right) \neq 0$$

Also remember that  $J(x_u)J(u_x)=I$ , so  $\det(J(x_u))\det(J(u_x))=1$ . This means if  $\det(J(x_u))\neq 0$ , the above condition is satisfied.

For a given point  $P = (x_1, x_2, x_3)$ , by finding  $\nabla u_i(P)$  and normalising (change to a unit vector). We have  $\hat{\boldsymbol{u}}_i$ , the unit normal vector to the surface  $u_i = u_i(P)$  (where  $u_i(P)$  is a constant). So

$$\widehat{\boldsymbol{u}}_i = \frac{\nabla u_i(P)}{|\nabla u_i(P)|}$$

system is orthogonal of  $\hat{u}_i$  are mutually orthogonal.

In general, tangential vectors(to the line where only  $u_i$  varies)  $\hat{e_i}$  are used more. In Cartesian coordinates,  $\hat{e}_i$  are  $\hat{i}, \hat{j}, \hat{k}$ . To find  $\hat{e}_i$ , use this formulae:

$$\frac{\partial \boldsymbol{r}}{\partial u_i} = h_i \hat{e}_i$$
, where  $h_i = \left| \frac{\partial \boldsymbol{r}}{\partial u_i} \right|$ ,  $\boldsymbol{r} = x \hat{\boldsymbol{i}} + y \hat{\boldsymbol{j}} + z \hat{\boldsymbol{k}}$ 

 $h_i$  are called length scale. Showing  $\hat{e}_i$  are mutually orthogonal also proves orthogonality of the coordinate system.

In orthogonal system:

$$\widehat{m{e}}_i = \widehat{m{u}}_i$$

Path element

$$d\mathbf{r} = \sum h_i du_i \widehat{e_i}$$

(for orthogonal system)

$$(ds)^2 = (d\boldsymbol{r}.d\boldsymbol{r}) = \sum h_i^2 du_i^2$$

Volume element

$$dV = h_1 h_2 h_3 du_1 du_2 du_3$$

Area element (on the surface where  $u_1$  is constant)

$$dS = h_2 h_3 du_2 du_3$$

Gradient

$$\nabla = \sum \frac{1}{h_i} \hat{e_i} \frac{\partial}{\partial u_i}$$

from this we have  $\hat{\boldsymbol{e}}_i = \nabla \boldsymbol{u}_i h_i$ 

Divergence

$$div(\mathbf{A}) = \frac{1}{h_1 h_2 h_3} \left\{ \sum \frac{\partial}{\partial u_i} (A_i h_j h_k) \right\}$$

Curl

$$curl(\mathbf{A}) = \frac{1}{h_1 h_2 h_3} \begin{vmatrix} h_1 \widehat{e_1} & h_2 \widehat{e_2} & h_3 \widehat{e_3} \\ \frac{\partial}{\partial u_1} & \frac{\partial}{\partial u_2} & \frac{\partial}{\partial u_3} \\ h_1 A_1 & h_2 A_2 & h_3 A_3 \end{vmatrix}$$

Laplacian

$$\bigtriangledown^2\Phi = \frac{1}{h_1h_2h_3} \left\{ \sum \frac{\partial}{\partial u_i} (\frac{h_jh_k}{h_i} \frac{\partial \Phi}{\partial u_i}) \right\}$$

#### 5.1 Cartesian, Cylindrical and Spherical

Three systems are all orthogonal.

Definition of Cylindrical coordinates:

$$x = r \cos \theta, y = r \sin \theta, z = z$$

Definition of Spherical coordinates:

$$x = r \sin \theta \cos \phi, y = r \sin \theta \sin \phi, z = r \cos \theta$$

where  $r \geq 0$  is radius,  $\theta \in [0, \pi]$  is rotation above x-y plane and  $\phi \in [0, 2\pi]$  is rotation with in x-y plane.

Tables below are ordered by (x, y, z),  $(r, \theta, z)$ ,  $(r, \theta, \phi)$ 

Coordinate system	$h_i$	$\widehat{e_i}$	
Cartesian	1,1,1	$\hat{m{i}},\hat{m{j}},\hat{m{k}}$	
Cylindrical	1	$\cos heta\hat{m i} + \sin heta\hat{m j}$	
	r	$-\sin heta \hat{m{i}} + \cos heta \hat{m{j}}$	
	1	$\hat{m{k}}$	
Spherical	1	$\sin\theta\cos\phi\hat{\pmb{i}} + \sin\theta\sin\phi\hat{\pmb{j}} + \cos\theta\hat{\pmb{k}}$	
	r	$\cos\theta\cos\phi\hat{\pmb{i}} + \cos\theta\sin\phi\hat{\pmb{j}} - \sin\theta\hat{\pmb{k}}$	
	$r\sin\theta$	$-\sin\theta\sin\phi\hat{\boldsymbol{i}} + \sin\theta\cos\phi\hat{\boldsymbol{j}}$	

Table 1: Table of tangential vectors and length scales

Coordinate system	gradient div		Laplacian
Cartesian	$\hat{m{i}}rac{\partial}{\partial x}+\hat{m{j}}rac{\partial}{\partial y}+\hat{m{k}}rac{\partial}{\partial z}$	$\frac{\partial A_1}{\partial x} + \frac{\partial A_2}{\partial y} + \frac{\partial A_3}{\partial z}$	$\frac{\partial^2 \Phi}{\partial x^2} + \frac{\partial^2 \Phi}{\partial y^2} + \frac{\partial^2 \Phi}{\partial z^2}$
Cylindrical	$\hat{m{r}}rac{\partial}{\partial r}+rac{\hat{m{ heta}}}{r}rac{\partial}{\partial heta}+\hat{m{k}}rac{\partial}{\partial z}$	$\frac{\partial A_1}{\partial r} + \frac{A_1}{r} + \frac{1}{r} \frac{\partial A_2}{\partial \theta} + \frac{\partial A_3}{\partial z}$	$\frac{\partial^2 \Phi}{\partial r^2} + \frac{1}{r} \frac{\partial \Phi}{\partial r} + \frac{1}{r^2} \frac{\partial^2 \Phi}{\partial \theta} + \frac{\partial^2 \Phi}{\partial z}$
Spherical	$\hat{m{r}} rac{\partial}{\partial r} + rac{\hat{m{ heta}}}{r} rac{\partial}{\partial  heta} + rac{\hat{m{\phi}}}{r \sin  heta} rac{\partial}{\partial \phi}$	$\frac{1}{r^2 \sin \theta} \left\{ \frac{\partial}{\partial r} (r^2 \sin \theta A_1) + \frac{\partial}{\partial \theta} (r \sin \theta A_2) + \frac{\partial}{\partial \phi} (r A_3) \right\}$	$\frac{\partial^2 \Phi}{\partial r^2} + \frac{2}{r} \frac{\partial \Phi}{\partial r} + \frac{\cot \theta}{r^2} \frac{\partial \Phi}{\partial \theta} + \frac{1}{r^2} \frac{\partial^2 \Phi}{\partial \theta} + \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 \Phi}{\partial \phi}$

Table 2: Table of div, gradient and Laplacian for vector valued function  $\boldsymbol{A}$  or scalar valued function  $\Phi$ 

## 5.2 Change of variables

If we parameterise surface S by  $(u_1, u_2)$ ,

$$dS = |J| du_1 du_2$$
, where  $J = \frac{\partial \mathbf{r}}{\partial u_1} \times \frac{\partial \mathbf{r}}{\partial u_2}$ 

If S is on x-y plane

$$J = J(\boldsymbol{x}_{\boldsymbol{u}})$$
, where  $\boldsymbol{x} = (x, y)$ 

If S is z = f(x, y) and we parameterise using x, y:

$$|J| = \sqrt{1 + |\nabla f|^2}$$

So surface area of any surface S is

$$\int_{\Sigma} \sqrt{1+|\nabla f|^2} \, dx dy$$

where  $\Sigma$  is projection of S onto x-y plane.

## 6 Calculus of Variation

**Vanishing lemma** If g is a continuous function s.t. for every smooth function  $\eta(x)$  with  $\eta(x_1) = \eta(x_2) = 0$ ,

$$\int_{x}^{x_2} g(x)\eta(x) \ dx = 0$$

then  $g \equiv 0$ 

Target of this section: find function y = y(x) that minimises the integral

$$I := \int_{x_1}^{x_2} L(x, y, y') \ dx$$

L is a functional.

#### 1D E-L equation and special cases

Full equation

$$\frac{\partial L}{\partial y} = \frac{d}{dx} \left\{ \frac{\partial L}{\partial y'} \right\}$$

L independent of y

$$\frac{\partial L}{\partial u'} = \text{constant}$$

L independent of y'

$$\frac{\partial L}{\partial y} = 0$$

L independent of x:

$$L - y' \frac{\partial L}{\partial y'} = \text{constant}$$

Finding extrema of  $I = \int_{x_1}^{x_2} L(x, y, y') dx$  where L is a functional

- 1. Use E-L equation to obtain a differential equation.
- 2. Solve it, remember to include the integration constants.
- 3. Check that I''(0) > 0 or I''(0) < 0
- 4. use boundary conditions to determine integration constants

Multivariate E-L If we are finding extrema of

$$I = \int_{t_1}^{t_2} L(t, x_1(t), x_1'(t), ..., x_n(t), x_n'(t)) dt$$

E-L equation becomes a set of equations

$$\frac{\partial L}{\partial x_i} = \frac{d}{dt} \left\{ \frac{\partial L}{\partial x_i'} \right\}$$

With constraint

$$J = \int_{t_1}^{t_2} g(t, x_1(t), x_1'(t), ..., x_n(t), x_n'(t)) \ dt = \text{constant}$$

E-L becomes

$$\frac{\partial}{\partial x_i}(L+\lambda g) - \frac{d}{dt}\frac{\partial}{\partial x_i'}(L+\lambda g) = 0$$

Leave  $\lambda$  there and after finishing regular steps, plug in integral J to determine  $\lambda$ . However, the order you determine the constants is not restricted, you may as well find  $\lambda$  in terms of an integration constant c first, then solve c using the restriction.

**E-L for surface integral** The function f(r) where r = xi + yj that maximises

$$I = \int_R L(\boldsymbol{r}, f(\boldsymbol{r}), \nabla f(\boldsymbol{r})) \ dx \ dy$$

can be found by solving the following equation

$$\frac{\partial L}{\partial f} = div(\nabla_{\nabla_f} L) = div(\widehat{\boldsymbol{i}}\frac{\partial L}{\partial f_x} + \widehat{\boldsymbol{j}}\frac{\partial L}{\partial f_y})$$

where  $f_x, f_y$  are partial derivatives of f.

**Isoperimetric inequality** For any simple curve with area A and perimeter l,

$$4\pi A \leq l^2$$

equality holds iff curve is circle.

# 7 Integration Techniques

Ways of showing  $f(x) \equiv 0$  using integration:

- 1. Use vanishing lemma
- 2. Prove  $\int_{x_1}^{x_2} f^2 dx = 0$ . Or if you know  $f(x) \ge 0$ , prove  $\int_{x_1}^{x_2} f dx = 0$ . Some inverse trig integrals

$$\int \frac{dx}{\sqrt{a^2 - x^2}} = \sin^{-1}(\frac{x}{a}) + c$$

$$\int \frac{dx}{a^2 + x^2} = \frac{1}{a} \tan^{-1}(\frac{x}{a}) + c$$

$$\int \frac{dx}{x\sqrt{x^2 - a^2}} = \frac{1}{a} \sec^{-1}(\frac{|x|}{a}) + c$$

Some inverse hyperbolic integrals

$$\int \frac{dx}{\sqrt{a^2 + x^2}} = \sinh^{-1}(\frac{x}{a}) + c$$

$$\int \frac{dx}{\sqrt{x^2 - a^2}} = \cosh^{-1}(\frac{x}{a}) + c$$

$$\int \frac{dx}{a^2 - x^2} = \frac{1}{a} \tanh^{-1}(\frac{x}{a}) + c \quad (x^2 < a^2)$$

$$\int \frac{dx}{a^2 - x^2} = \frac{1}{a} \coth^{-1}(\frac{x}{a}) + c \quad (x^2 > a^2)$$

Derivatives of trigs:

$$(\sin(x))' = \cos(x) \quad (\cos(x))' = -\sin(x) \quad (\tan(x))' = \sec^2(x)$$
  
 $(\csc(x))' = -\cot(x)\csc(x) \quad (\sec(x))' = \tan(x)\sec(x) \quad (\cot(x))' = -\csc^2(x)$ 

Reduction formulas:

$$I_n = \int \cos^n(x) \, dx = \frac{1}{n} \cos^{n-1}(x) \sin(x) + \frac{n-1}{n} I_{n-2}$$

$$I_n = \int \sin^n(x) \, dx = -\frac{1}{n} \sin^{n-1}(x) \cos(x) + \frac{n-1}{n} I_{n-2}$$

$$I_n = \int x^n e^{ax} \, dx = \frac{x^n e^a x}{a} - \frac{1}{n} I_{n-1}$$

Product to sum rules for trigs:

$$\sin(x)\cos(y) = \frac{1}{2}[\sin(x+y) + \sin(x-y)]$$

$$\cos(x)\sin(y) = \frac{1}{2}[\sin(x+y) - \sin(x-y)]$$

$$\cos(x)\cos(y) = \frac{1}{2}[\cos(x+y) + \cos(x-y)]$$

$$\sin(x)\sin(y) = -\frac{1}{2}[\cos(x+y) - \cos(x-y)]$$