

Chapter VI: The Kinematics of Rigid Body Motion

4.1 The Independent Coordinates of a Rigid Body

1. For a rigid body with N particles, the degrees of freedom are reduced by the constraints $r_{ij} = c_{ij}$. To fix a rigid body, we just need to specify any three non-collinear points, thus the degrees of freedom can't be more than 9, and with $r_{12} = c_{12}$, $r_{23} = c_{23}$, $r_{13} = c_{13}$, they're reduced to 6.

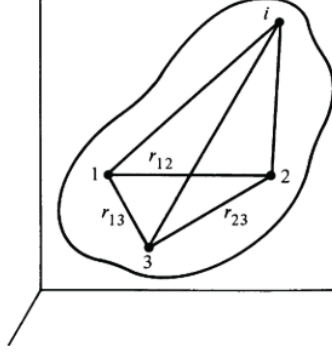


FIGURE 4.1 The location of a point in a rigid body by its distances from three reference points.

Figure 1:

2. For two Cartesian coordinates, the direction cosines are defined by

$$\begin{cases} \cos \theta_{11} = \cos(\mathbf{i}', \mathbf{i}) = \mathbf{i}' \cdot \mathbf{i} \\ \cos \theta_{12} = \cos(\mathbf{i}', \mathbf{j}) = \mathbf{i}' \cdot \mathbf{j} \\ \cos \theta_{21} = \cos(\mathbf{j}', \mathbf{i}) = \mathbf{j}' \cdot \mathbf{i}, \text{ etc.} \end{cases}$$

In terms of the unit vectors of the unprimed system, the unit vector in the primed system can be expressed

$$\begin{aligned} \mathbf{i}' &= \cos \theta_{11} \mathbf{i} + \cos \theta_{12} \mathbf{j} + \cos \theta_{13} \mathbf{k} \\ \mathbf{j}' &= \cos \theta_{21} \mathbf{i} + \cos \theta_{22} \mathbf{j} + \cos \theta_{23} \mathbf{k} \\ \mathbf{k}' &= \cos \theta_{31} \mathbf{i} + \cos \theta_{32} \mathbf{j} + \cos \theta_{33} \mathbf{k} \end{aligned}$$

Thus, we can write

$$\mathbf{r} = x\mathbf{i} + y\mathbf{j} + z\mathbf{k} = x'\mathbf{i}' + y'\mathbf{j}' + z'\mathbf{k}'$$

where $x' = (\mathbf{i}' \cdot \mathbf{r})$, $y' = (\mathbf{j}' \cdot \mathbf{r})$, $z' = (\mathbf{k}' \cdot \mathbf{r})$. Note that $\mathbf{i}' \cdot \mathbf{j}' = \mathbf{j}' \cdot \mathbf{k}' = \mathbf{k}' \cdot \mathbf{i}' = 0$ and $\mathbf{i}' \cdot \mathbf{i}' = \mathbf{j}' \cdot \mathbf{j}' = \mathbf{k}' \cdot \mathbf{k}' = 1$.

We can use the Kronecker symbol

$$\sum_{l=1}^3 \cos \theta_{li'} \cos \theta_{lj'} = \delta_{ij}$$

4.2 Orthogonal Transformations

1. As showed before, for $x \rightarrow x_1, y \rightarrow x_2, z \rightarrow x_3$, we write $a_{ij} = \cos \theta_{ij}$, thus

$$\begin{aligned} x'_1 &= a_{11}x_1 + a_{12}x_2 + a_{13}x_3 \\ x'_2 &= a_{21}x_1 + a_{22}x_2 + a_{23}x_3 \\ x'_3 &= a_{31}x_1 + a_{32}x_2 + a_{33}x_3 \end{aligned}$$

We use the summation convention introduced by Einstein

$$x'_i = \sum_j a_{ij}x_j, \quad i = 1, 2, 3$$

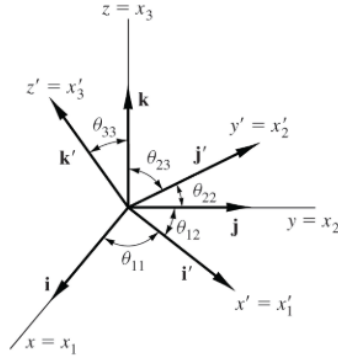


FIGURE 4.3 Direction cosines of the body set of axes relative to an external set of axes.

Figure 2:

and $\sum_i x'_i x'_i$ can be written as $x'_i x'_i$.

Thus,

$$\begin{aligned} x'_i x'_i &= x_j x_j = a_{ij} a_{ik} x_j x_k \\ \Rightarrow a_{ij} a_{ik} &= \delta_{jk}, \quad j, k = 1, 2, 3 \end{aligned}$$

which is the orthogonal condition.

The matrix of transformation is

$$A = \begin{pmatrix} a_{11} & a_{12} & a_{13} \\ a_{21} & a_{22} & a_{23} \\ a_{31} & a_{32} & a_{33} \end{pmatrix}$$

such that $\mathbf{x}' = A\mathbf{x}$.

4.3 Formal Properties of the Transformation Matrix

1. We consider two successive transformations

$$\mathbf{x}' = B\mathbf{x} \quad \text{and} \quad \mathbf{x}'' = A\mathbf{x}'$$

or

$$x'_k = b_{kj} x_j \quad \text{and} \quad x''_i = a_{ik} x'_k$$

Thus, we have

$$x''_i = a_{ik} b_{kj} x_j \Rightarrow x''_i = c_{ij} x_j$$

where $C = AB$ where $c_{ij} = a_{ik} b_{kj}$.

or $C = BA$ is defined by $d_{ij} = b_{ik} a_{kj}$.

- 2.

$$\begin{aligned} x &= \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix}, \quad x' = \begin{bmatrix} x'_1 \\ x'_2 \\ x'_3 \end{bmatrix} \\ (Ax)_i &= a_{ij} x_j = x'_i \Rightarrow x' = Ax \end{aligned}$$

3. $(AB)C = A(BC)$

4. $C = A + B \Rightarrow c_{ij} = a_{ij} + b_{ij}$

5. For A^{-1} where $x_i = a_{ij} x'_j$

$$\Rightarrow a_{ki} a_{ij} = \delta_{kj} \quad \text{and} \quad AA^{-1} = \begin{bmatrix} 1 & & \\ & \ddots & \\ & & 1 \end{bmatrix}$$

where $x = Ix$.

6. Let's consider $a_{kl}a_{ki}a_{ij}$ or $c_{lj}a_{ij}$ with $c_{li} = a_{kl}a_{ki}$ or $a_{ki}d_{kj}$ with $d_{kj} = a_{ki}a_{ij}$.

$$a_{kl}\delta_{kj} = a_{lj}$$

7. $A \rightarrow A^{-1} : a'_{ij} = a_{ji}$. For orthogonal matrices, $A^{-1} = \tilde{A}$ where \tilde{A} is the transposed matrix, and thus we have

$$a_{ki}a_{ji} = \delta_{kj} \Rightarrow A\tilde{A} = I$$

8. $A_{ij}x_j = x_j(A)_{ji} \Rightarrow Ax = x\tilde{A}$

9. If $A_{ij} = A_{ji}$, the matrix is symmetric.

If $A_{ij} = -A_{ji}$, the matrix is antisymmetric.

10. $|AB| = |A||B|$

$$A\tilde{A} = I \Rightarrow |A||\tilde{A}| = |A|^2 = 1$$

$$|A^{-1}||A| = 1$$

4.4 The Euler Angles

We consider a transformation

$$xyz \xrightarrow[\text{about } z]{\text{rotate by } \phi \text{ counterclockwise}} \xi\eta\zeta \xrightarrow[\text{about } \xi]{\text{rotate by } \theta \text{ counterclockwise}} \xi'\eta'\zeta' \xrightarrow[\text{about } \zeta']{\text{rotate by } \psi \text{ counterclockwise}} x'y'z'$$

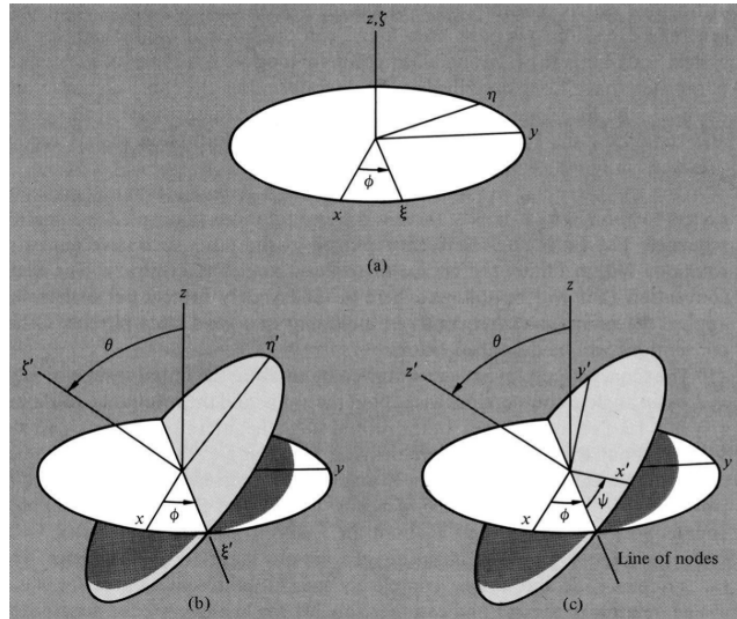


FIGURE 4.7 The rotations defining the Eulerian angles.

Figure 3:

We have

$$\begin{cases} \textcircled{1} & \xi = Dx \\ \textcircled{2} & \xi' = C\xi \\ \textcircled{3} & x' = B\xi' \end{cases} \quad \text{where } \xi \text{ and } x \text{ are column matrices}$$

Hence, $A = BCD$ where

$$B = \begin{bmatrix} \cos \psi & \sin \psi & 0 \\ -\sin \psi & \cos \psi & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$C = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos \theta & \sin \theta \\ 0 & -\sin \theta & \cos \theta \end{bmatrix}$$

$$D = \begin{bmatrix} \cos \phi & \sin \phi & 0 \\ -\sin \phi & \cos \phi & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

4.5 The Cayley-Klein Parameters and Related Quantities

We consider four parameters $\alpha, \beta, \gamma, \delta$ with the constraints that $\beta = -\gamma^*$ and $\delta = \alpha^*$.

The transformation matrix

$$A = \begin{bmatrix} \frac{1}{2}(\alpha^2 - \gamma^2 + \delta^2 - \beta^2) & \frac{i}{2}(\gamma^2 - \alpha^2 + \delta^2 - \beta^2) & \gamma\delta - \alpha\beta \\ \frac{i}{2}(\alpha^2 + \gamma^2 - \beta^2 - \delta^2) & \frac{1}{2}(\alpha^2 + \gamma^2 + \beta^2 + \delta^2) & -i(\alpha\beta + \gamma\delta) \\ \beta\delta - \alpha\gamma & i(\alpha\gamma + \beta\delta) & \alpha\delta + \beta\gamma \end{bmatrix}$$

And we choose the Euler parameters e_0, e_1, e_2, e_3 where $\sum_{i=0}^3 e_i^2 = 1$ and

$$\alpha = e_0 + ie_3$$

$$\beta = e_2 + ie_1$$

4.6 Euler's Theorem on the Motion of a Rigid Body

1. **Euler's Theorem:** The general displacement of a rigid body with one point fixed is a rotation about some axis.

$$\Rightarrow R' = AR = R\lambda$$

where λ is a complex constant where we have the eigenvalue equations

$$(A - \lambda I)R = 0 \Rightarrow |A - \lambda I| = \begin{vmatrix} a_{11} - \lambda & a_{12} & a_{13} \\ a_{21} & a_{22} - \lambda & a_{23} \\ a_{31} & a_{32} & a_{33} - \lambda \end{vmatrix} = 0$$

which is the characteristic equation.

The eigenvalue equation can also be written:

$$\sum_j a_{ij} x_{jk} = \lambda_k x_{ik} = \sum_j x_{ij} \delta_{jk} \lambda_k$$

4.6 Euler's Theorem (Continued)

We designate the matrix by

$$\Lambda = \begin{bmatrix} \lambda_1 & 0 & 0 \\ 0 & \lambda_2 & 0 \\ 0 & 0 & \lambda_3 \end{bmatrix}$$

Hence: $AX = X\Lambda \Rightarrow X^{-1}AX = \Lambda$.

2. Consider the expression $(A - I)\tilde{A} = I - \tilde{A}$ (orthogonal matrices).

$$\Rightarrow |A - I||\tilde{A}| = |I - \tilde{A}| = |I - A|$$

Since $|-B| = (-1)^n |B|$, we have $|I - A| = 0$.

3. **Chasles' Theorem:** The most general displacement of a rigid body is a translation plus a rotation.

4.7 Finite Rotations

1. For $\vec{r} = \vec{OP}$, $\vec{r}' = \vec{OQ}$, $\vec{ON} = \vec{n}(\vec{n} \cdot \vec{r})$, $\vec{NP} = \vec{r} - \vec{n}(\vec{n} \cdot \vec{r})$.

$$\vec{NQ} = \vec{r} \times \vec{n}, \quad \vec{r}' = \vec{ON} + \vec{NV} + \vec{VQ}$$

$$\Rightarrow \vec{r}' = \vec{r} \cos \Phi + \vec{n}(\vec{n} \cdot \vec{r})(1 - \cos \Phi) + (\vec{r} \times \vec{n}) \sin \Phi$$

which is the rotation formula.

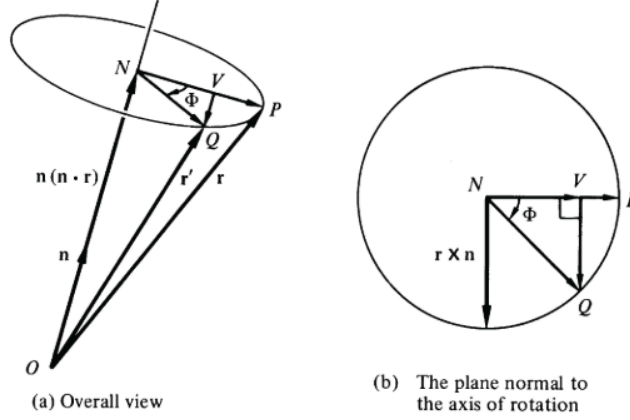


FIGURE 4.8 Vector diagrams for derivation of the rotation formula.

Figure 4:

4.8 Infinitesimal Rotations

1. From \vec{x} to \vec{x}' , we consider

$$x'_i = x_i + \epsilon_{i1}x_1 + \epsilon_{i2}x_2 + \epsilon_{i3}x_3 \Rightarrow x'_i = (\delta_{ij} + \epsilon_{ij})x_j$$

where $\epsilon_{11}, \epsilon_{12}$ are infinitesimals.

$$\Rightarrow x' = (I + \epsilon)x$$

In fact, $(I + \epsilon_1)(I + \epsilon_2) = I + \epsilon_1 + \epsilon_2$ where $\epsilon_1\epsilon_2$ is neglected.

$A = I + \epsilon$ and $A^{-1} = I - \epsilon$ since $AA^{-1} = I$.

Further, as for orthogonality, $\tilde{A} = I + \tilde{\epsilon} = A^{-1} = I - \epsilon \Rightarrow \tilde{\epsilon} = -\epsilon$.

2. For Euler infinitesimal rotation:

$$A = \begin{bmatrix} 1 & d\phi & 0 \\ -d\phi & 1 & d\theta \\ 0 & -d\theta & 1 \end{bmatrix} \text{ and } d\Omega = \hat{i}d\theta + \hat{k}(d\phi + d\psi)$$

$$\epsilon = \begin{bmatrix} 0 & d\Omega_3 & -d\Omega_2 \\ -d\Omega_3 & 0 & d\Omega_1 \\ d\Omega_2 & -d\Omega_1 & 0 \end{bmatrix}$$

we write the form: $\vec{r}' - \vec{r} = d\vec{r} = \epsilon\vec{r}$

$$\Rightarrow \begin{cases} dx_1 = x_2d\Omega_3 - x_3d\Omega_2 \\ dx_2 = x_3d\Omega_1 - x_1d\Omega_3 \\ dx_3 = x_1d\Omega_2 - x_2d\Omega_1 \end{cases} \implies d\vec{r} = \vec{r} \times d\vec{\Omega}$$

3. In another fashion: $\vec{r}' - \vec{r} = d\vec{r} = \vec{r} \times \vec{n}d\Phi$ where $d\vec{\Omega} = \vec{n}d\Phi$.

The magnitude is: $dr = r \sin \theta d\Phi$.

4.9 Rate of Change of a Vector

1. For a general vector \vec{G} , we have

$$(d\vec{G})_{\text{space}} = (d\vec{G})_{\text{body}} + (d\vec{G})_{\text{rot}}$$

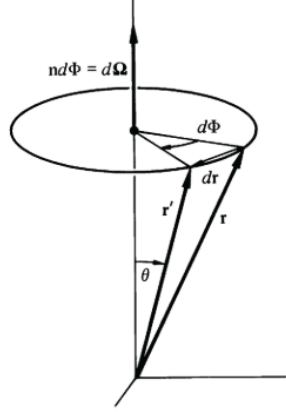


FIGURE 4.11 Change in a vector produced by an infinitesimal clockwise rotation of the vector.

Figure 5:

where $(d\vec{G})_{\text{rot}} = d\vec{\Omega} \times \vec{G}$.

$$\left(\frac{d\vec{G}}{dt} \right)_{\text{space}} = \left(\frac{d\vec{G}}{dt} \right)_{\text{body}} + \vec{\omega} \times \vec{G}$$

where $\vec{\omega} dt = d\vec{\Omega}$ and $\vec{\omega}$ is along the instantaneous axis of rotation.

We have $dG_i = a_{ji} dG'_j + da_{ji} G'_j$.

where $a_{ji} G'_j = dG_i$ and $da_{ji} = (\tilde{\epsilon})_{ij} = -\epsilon_{ij}$.

By antisymmetry of ϵ , $-\epsilon_{ij} = -\epsilon_{ijk} d\Omega_k = \epsilon_{ikj} d\Omega_k$.

$$\Rightarrow dG_i = dG'_i + \epsilon_{ikj} d\Omega_k G_j$$

$$dG_i = dG'_i + (d\vec{\Omega} \times \vec{G})_i$$

2. We consider the transformation $A = BCD$.

where $\omega_\phi = \dot{\phi}$, $\omega_\theta = \dot{\theta}$, $\omega_\psi = \dot{\psi}$.

$$\Rightarrow \begin{cases} (\omega_\phi)x' = \dot{\phi} \sin \theta \sin \psi, & (\omega_\phi)y' = \dot{\phi} \sin \theta \cos \psi, & (\omega_\phi)z' = \dot{\phi} \cos \theta \\ (\omega_\theta)x' = \dot{\theta} \cos \psi, & (\omega_\theta)y' = -\dot{\theta} \sin \psi, & (\omega_\theta)z' = 0 \\ (\omega_\psi)z' = \dot{\psi} \end{cases}$$

$$\Rightarrow \begin{cases} \omega_{x'} = (\omega_\phi)x' + (\omega_\theta)x' \\ \omega_{y'} = (\omega_\phi)y' + (\omega_\theta)y' \\ \omega_{z'} = (\omega_\phi)z' + (\omega_\psi)z' \end{cases}$$

4.10 The Coriolis Effect

1. We have $\vec{v}_s = \vec{v}_r + \vec{\omega} \times \vec{r}$ where \vec{v}_s, \vec{v}_r are the velocities of the particle relative to the space and rotating set of axes.

$$\begin{aligned} \Rightarrow \left(\frac{d\vec{v}_s}{dt} \right)_s &= \vec{a}_s = \left(\frac{d}{dt} (\vec{v}_r + \vec{\omega} \times \vec{r}) \right)_s + \vec{\omega} \times \vec{v}_s \\ &= \vec{a}_r + 2(\vec{\omega} \times \vec{v}_r) + \vec{\omega} \times (\vec{\omega} \times \vec{r}) \end{aligned}$$

The equation of motion $\vec{F} = m\vec{a}_s$.

$$\Rightarrow \vec{F} - 2m(\vec{\omega} \times \vec{v}_r) - m\vec{\omega} \times (\vec{\omega} \times \vec{r}) = m\vec{a}_r = \vec{F}_{\text{eff}}$$

where $-2m(\vec{\omega} \times \vec{v}_r)$ is the Coriolis effect and $-m\vec{\omega} \times (\vec{\omega} \times \vec{r}) \{m\omega^2 r \sin \theta\}$ is the centrifugal force.

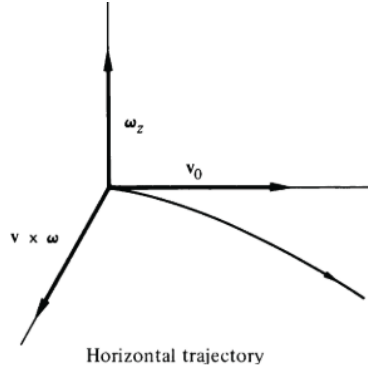


FIGURE 4.13 Direction of Coriolis deflection in the northern hemisphere.

Figure 6:

2. Example: the equation of motion:

$$m \frac{d^2 x}{dt^2} = -2m(\vec{\omega} \times \vec{v}_r)_x = -2m\omega v_z \sin \theta$$

where $v_z = -gt$, $t = \sqrt{2z/g}$.

The deflection caused by Coriolis effect on v_z is

$$x = \frac{\omega g}{3} t^3 \sin \theta = \frac{\omega}{3} \sqrt{\frac{8z^3}{g}} \sin \theta$$

Normally, for the equator ($\theta = \pi/2$) and $z = 100\text{m}$,

$$x \approx 2.2 \text{ cm}$$