

Notes for AdS

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I. INTRODUCTION AND SUMMARY

Choose the metric

$$ds^2 = -(1 - b^2 r^2) dt^2 + (1 - b^2 r^2)^{-1} dr^2 + r^2 d\Omega_2^2 \quad (1)$$

where $b^2 = \frac{\Lambda}{3}$. For a black hole of mass M we have

$$ds^2 = -\left(1 - \frac{2M}{r} - b^2 r^2\right) dt^2 + \left(1 - \frac{2M}{r} - b^2 r^2\right)^{-1} dr^2 + r^2 d\Omega_2^2 \quad (2)$$

we know

$$\frac{\Delta T}{T} = \sqrt{\frac{g_{00}(b, r_2)g_{00}(b, \Delta M, r_0)}{g_{00}(b, r_1)g_{00}(b, \Delta M, r_1)}} - 1 \quad (3)$$

where

$$\begin{aligned} g_{00}(\Lambda, r) &= -(1 - b^2 r^2) \\ g_{00}(\Lambda, \Delta M, r) &= -\left(1 - \frac{2\Delta M}{r} - b^2 r^2\right) \end{aligned} \quad (4)$$

The induced metrics we will use are

$$ds_I^2 = g_{\alpha\beta} dx^\alpha dx^\beta = -(1 - b^2 r^2) dt^2 + (1 - b^2 r^2) dr^2 + r^2 d\Omega_2^2 \quad (5)$$

$$ds_{II}^2 = g_{\alpha\beta} dx^\alpha dx^\beta = -(1 - b^2 r^2) dt^2 + (1 - b^2 r^2) dr^2 + r^2 d\Omega_2^2 \quad (6)$$

The induced metrics are

$$ds_{3(I)}^2 = h_{ab}^{(I)} dy^a dy^b = h_{00}^{(I)} dt^2 + h_{11}^{(I)} d\hat{\theta}^2 + h_{22}^{(I)} d\hat{\phi}^2 \quad (7)$$

$$ds_{3(II)}^2 = h_{ab}^{(II)} dy'^a dy'^b = h_{00}^{(II)} dt'^2 + h_{11}^{(II)} d\hat{\theta}'^2 + h_{22}^{(II)} d\hat{\phi}'^2 \quad (8)$$

matching the induced metrics at r_1 gives

$$dt = \frac{g_{00}^{(II)}(r_1)}{g_{00}^{(I)}(r_1)} dt' \quad (9)$$

We will need the stress energy of the shell and use the IJC for that. Lets look at the extrinsic curvature components first

$$K_{ab}^{(I)} = \frac{1}{2} g_{\alpha\beta}^{(I)} e_a^\alpha e_b^\beta \quad (10)$$

where

$$e_a^\alpha = \frac{dx^\alpha}{dy^a} \quad (11)$$

which we can simplify

$$K_{tt}^{(I)} = \frac{1}{2}(g_{tt}^{(I)})^{-\frac{1}{2}}\partial_r g_{tt}^{(I)} \quad (12)$$

similarly the other components of the extrinsic curvature are

$$K_{\theta\theta}^{(I)} = \frac{1}{2}n^r\partial_r g_{\theta\theta}^{(I)} = \frac{1}{2}(g_{tt}^{(I)})^{-\frac{1}{2}}\partial_r g_{\theta\theta}^{(I)} = K_{\phi\phi}^{(I)} \quad (13)$$

$$K_{tt}^{(II)} = \frac{1}{2}(g_{tt}^{(II)})^{-\frac{1}{2}}\partial_r g_{tt}^{(II)} \quad (14)$$

$$K_{\theta\theta}^{(II)} = \frac{1}{2}n^r\partial_r g_{\theta\theta}^{(II)} = \frac{1}{2}(g_{tt}^{(II)})^{-\frac{1}{2}}\partial_r g_{\theta\theta}^{(II)} = K_{\phi\phi}^{(II)} \quad (15)$$

The surface stress energy is

$$S_{00} = \sigma = \frac{1}{4\pi}((K_\theta^\theta)^{(I)} - (K_\theta^\theta)^{(II)}) \quad (16)$$

$$\sigma = \frac{1}{4\pi r_1^2} \left(\left(1 - b^2 r_1^2 - \frac{2\Delta M}{r_1} \right)^{-\frac{1}{2}} - (1 - b^2 r_1^2)^{-\frac{1}{2}} \right) \quad (17)$$