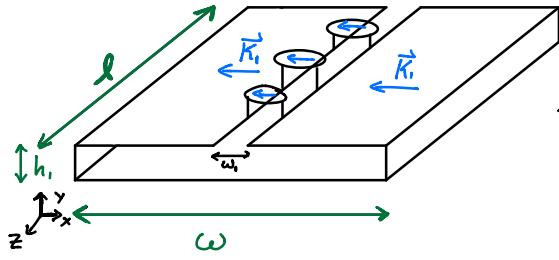


Flux Linkage

Given the following diagram:

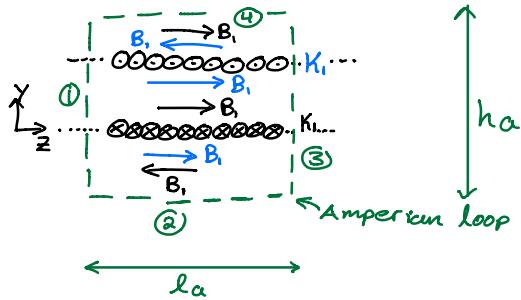


Assume the conductor is thin enough that current is similar to flowing on a sheet

9.1.1.

Assuming $\omega \gg h_i$ & $l \gg h_i$:

Looking at y-z cross-section (currents coming into and out of page) at



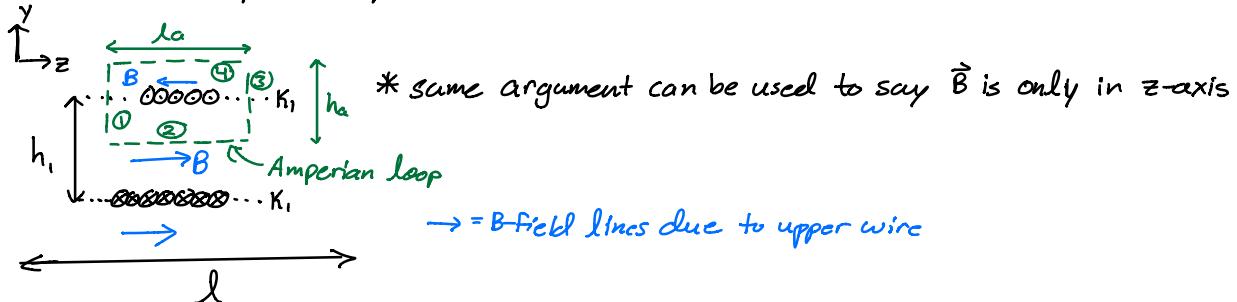
* because $l \gg h_i$, we can approximate that magnetic field is only in z-axis direction.

$$\oint \mathbf{B} \cdot d\mathbf{l} = \mu_0 I_{\text{enc}}$$

When outside of duct, $I_{\text{enc}} = Kl - Kl = 0$

$$\therefore \mathbf{B} = 0$$

For a new Amperian loop:



Using Ampere's Law:

$$\oint \vec{B} \cdot d\vec{l} = \mu_0 I_{\text{enc}}$$

$$\oint \vec{B} \cdot d\vec{l}_1 + \oint \vec{B} \cdot d\vec{l}_2 + \oint \vec{B} \cdot d\vec{l}_3 + \oint \vec{B} \cdot d\vec{l}_4 = \mu_0 I, \quad * B \text{ is only in } z\text{-direction & is then parallel to } d\vec{l}_2 \text{ & } d\vec{l}_4$$

$$\int B dl_2 + \int B dl_4 = \mu_0 I_a K_1$$

$$2B l_a = \mu_0 I_a K_1$$

$$B = \frac{\mu_0 K_1}{2} * \text{due to top sheet}$$

$$\therefore \vec{B}_{\text{top}} = \begin{cases} -\frac{\mu_0 K_1}{2} \hat{z} & \text{above sheet} \\ \frac{\mu_0 K_1}{2} \hat{z} & \text{below sheet} \end{cases}$$

* if consider loop going CCW, loop moves in direction of B for both loops, w/ both having constant B field due to $l \gg h$,

* if $h \ll w$, can ignore fields produced to left and right in comparison

Similar arguments can be made for a 2nd loop enclosing bottom sheet such that

$$\vec{B}_{\text{top}} = \begin{cases} \frac{\mu_0 K_1}{2} \hat{z} & \text{above sheet} \\ -\frac{\mu_0 K_1}{2} \hat{z} & \text{below sheet} \end{cases}$$

$$\vec{B}_{\text{Total}} = \vec{B}_{\text{top}} + \vec{B}_{\text{bot}} = \begin{cases} \mu_0 K_1 \hat{z} & * \text{inside duct} \\ 0 & * \text{outside duct since } B \text{'s cancel} \end{cases}$$

9.1.2

Because duct has relatively small enough thickness, internal magnetic field of conductor is 0. Leaving only an external magnetic field that exists inside the cross sectional area of duct $A_i = h_i w$

$$\therefore L_{\text{int}} \approx 0$$

EMF is given by the following

$$\mathcal{E}_i = - \frac{\partial \Phi_m}{\partial t}, \text{ rewrite this as: } \mathcal{E} = -L_i \frac{\partial I}{\partial t}$$

Recall $\Phi_m = L_i I_i$,

$$\mathcal{E}_i = - \frac{\partial}{\partial t} (L_i I_i)$$

$$\mathcal{E}_i = -L_i \frac{\partial I_i}{\partial t}$$

$$\Phi_m = \int \vec{B} \cdot d\vec{A}_i$$

$$= \int (\mu_0 K_i \hat{z}) (dA_i \hat{z})$$

$$\Phi_m = \mu_0 K_i \int dA_i = \mu_0 K_i h_i w$$

Substituting :

$$E = -\frac{d}{dt}(\mu_0 K_i h_i w) * \text{Since } \mu_0, h_i, w \text{ are constants}$$

$$\textcircled{1} E = -\mu_0 h_i w \frac{dK_i}{dt}$$

$$E = -L_i \frac{\partial I_i}{\partial t} * I_i = K_i l$$

$$\textcircled{2} E = -L_i \cdot l \frac{dK_i}{dt}$$

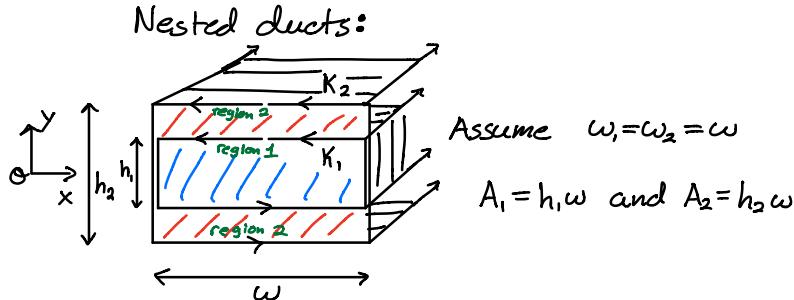
Relating both eqn \textcircled{1} & \textcircled{2}:

$$\mu_0 h_i w \cancel{\frac{dK_i}{dt}} = +L_i \cdot l \cancel{\frac{dK_i}{dt}}$$

$$\therefore L_i = \frac{\mu_0 h_i w}{l}$$

$$L_i \equiv \frac{\mu_0 A_i}{l}$$

9.1.3. Given the following nested ducts:



for region 1, \vec{B} is composed of magnetic field produced by both ducts.

$$\vec{B} = \vec{B}_1 + \vec{B}_2$$

Because physical symmetry arguments are unchanged, Ampere's Law yield:

$$B_2 = \begin{cases} \mu_0 K_2, & \text{inside duct 2 (in cross-section } A_2) \\ 0, & \text{outside duct 2} \end{cases}$$

\therefore inside region 1

$$\vec{B} = \mu_0 \vec{K}_1 + \mu_0 \vec{K}_2 = \mu_0 (K_1 + K_2) \hat{z} * \text{currents in same direction}$$

Then flux for region 2:

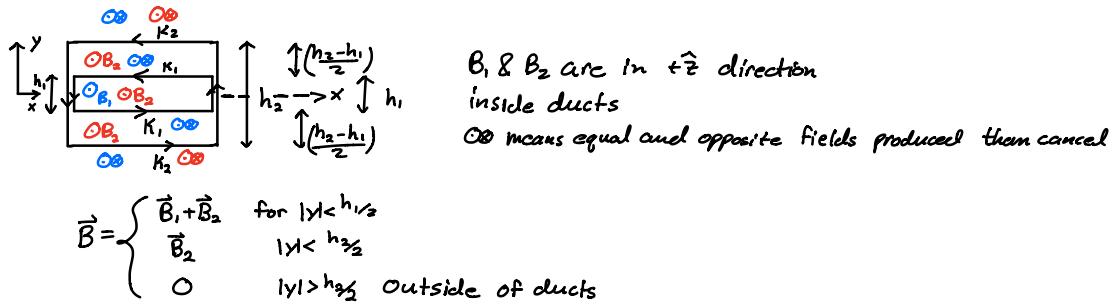
$$\Phi_m = \int \vec{B} \cdot d\vec{A}_2 * dA_2 \parallel \vec{B} \text{ w/ } \vec{B} \text{ being constant due to } l \gg h_1 \text{ & } \omega \gg h_1$$

$$= B \int dA_2 * B = B_2 + B_1$$

$$\Phi_m = BA_1 = h_1 \omega \mu_0 (K_1 + K_2)$$

$$\therefore E_1 = -h_1 \omega \mu_0 \frac{d}{dt} (K_1 + K_2)$$

For E_2 , must account for B -field in regions 1 & 2 (all of A_2):



Flux can then be:

$$\Phi_m = \int \vec{B} \cdot d\vec{A}_2$$

$$= \int_{w=-h_{1/2}}^{h_{1/2}} \int (B_1 + B_2) \cdot d\vec{A}_2 + \int_{0-h_{2/2}}^{w-h_{1/2}} \int \vec{B}_2 \cdot d\vec{A}_2 + \int_{0-h_{2/2}}^{h_{2/2}} \int \vec{B}_2 \cdot d\vec{A}_2$$

recall: B_1 & B_2 is constant inside due to $h_2 \ll w$ & $h_2 \ll l$

$$= (B_1 + B_2) h_1 w + B_2 (h_2 - h_1) \frac{w}{2} + B_2 (h_2 - h_1) \frac{w}{2}$$

$$= (B_1 + B_2) h_1 w + B_2 (h_2 - h_1) w$$

$$= B_1 A_1 + \cancel{B_2 A_1} + B_2 A_2 - \cancel{B_2 A_1}$$

$$\Phi_m = B_1 A_1 + B_2 A_2 = \mu_0 K_1 h_1 w + \mu_0 K_2 h_2 w$$

$$\Phi_m = \mu_0 \omega (K_1 h_1 + K_2 h_2)$$

$$\therefore E_2 = -\mu_0 \omega \left[h_1 \frac{d}{dt} K_1 + h_2 \frac{d}{dt} K_2 \right]$$

* if $K_1 + K_2 = K$

Thus total EMF is:

$$\mathcal{E} = \mathcal{E}_1 + \mathcal{E}_2$$

$$= -h_1 \omega \mu_0 \frac{d}{dt} (K_1 + K_2) - \mu_0 \omega \left[h_1 \frac{\partial}{\partial t} K_1 + h_2 \frac{\partial}{\partial t} K_2 \right]$$

$$* I_1 = K_1 \cdot l, \quad I_2 = K_2 \cdot l$$

$$\mathcal{E} = -A_1 \frac{\mu_0}{l} \frac{dI}{dt} - \frac{\mu_0 A_1}{l} \frac{d}{dt} I_1 - \frac{\mu_0 A_2}{l} \frac{d}{dt} I_2$$

$$\mathcal{E} = -\left\{ \frac{\mu_0}{l} A_1 \frac{d}{dt} (I + I_1) + \frac{\mu_0 A_2}{l} \frac{d}{dt} I_2 \right\} * I = I_1 + I_2$$

$$= -\left\{ \frac{\mu_0}{l} A_1 2 \frac{d}{dt} (I_2) + \frac{\mu_0}{l} A_1 \frac{d}{dt} I_2 + \frac{\mu_0 A_2}{l} \frac{d}{dt} I_2 \right\}$$

$$\therefore \mathcal{E} = -\left\{ 2 \frac{\mu_0}{l} A_1 \frac{dI_1}{dt} + \frac{\mu_0}{l} (A_1 + A_2) \frac{dI_2}{dt} \right\}$$

$$* \mathcal{E}_1 = -L_1 \frac{\partial I_1}{\partial t}, \quad \mathcal{E}_2 = -L_2 \frac{\partial I_2}{\partial t}$$

$$\text{then } \mathcal{E} = -(L_1 \frac{\partial I_1}{\partial t} + L_2 \frac{\partial I_2}{\partial t}) * \text{at low frequencies } I_1 = I_2 = I$$

Comparing equations:

$$\mathcal{E} = -(L_1 + L_2) \frac{\partial I}{\partial t} * L = L_1 + L_2 = \frac{2\mu_0}{l} A_1 + \frac{\mu_0}{l} (A_1 + A_2) = \frac{3\mu_0}{l} A_1 + \frac{\mu_0}{l} A_2$$

9.1.4) Since calculations were done previously in this manner we can use the results from Φ_m computed for region 1 (used to compute \mathcal{E}_1)

In region 1 (A_1 , area)

$$B = B_1 + B_2$$

$$\Phi_{m_1} = \int \vec{B} \cdot d\vec{A}_1$$

$$= \int \vec{B}_1 \cdot \vec{A}_1 + \int \vec{B}_2 \cdot \vec{A}_1, * B_1 \text{ & } B_2 \text{ still remain the same formulas as: } B_i = \mu_0 K_i \quad (i=1,2) \\ \text{and independent of } x \text{ or } y$$

$$= \mu_0 K_1 A_1 + \mu_0 K_2 A_1$$

$$\Phi_{B_1} = \mu_0 A_1 (K_1 + K_2) = L_{ext} I$$

$$L_{ext} = \frac{\mu_0 A_1}{l} \frac{(K_1 + K_2)}{K_{ext}} * K_2 \text{ & } K_1 \text{ contribute}$$

In region 2:

$$\Phi_{m_2} = \int \vec{B} \cdot d\vec{A} * \vec{B} = B_2 \text{ since } B_1 = 0 \text{ outside of } A_1$$

leading to similar result of:

$$\Phi_{m_2} = B_2 \int_{\text{region}_2} dA = \mu_0 K_2 (A_2 - A_1)$$

$$L_{\text{int}} = \frac{\Phi_{m_2}}{I} = \frac{\mu_0 K_2 (A_2 - A_1)}{l} \quad * K_2 \text{ is the effective magnetic field producing flux}$$

$$L_{\text{int}} = \frac{\mu_0 (A_2 - A_1)}{l}$$

and if $h_2 = h_1 + \delta h \rightarrow A_2 \approx A_1$ as $\delta h \rightarrow 0$

$$\begin{aligned} L_{\text{tot}} &= L_{\text{ext}} + L_{\text{int}} \\ &= \frac{\mu_0 A_1}{l} + \frac{\mu_0}{l} (A_2 - A_1) \end{aligned}$$

$$L_{\text{tot}} = \frac{\mu_0}{l} A_2$$

Q.1.5.) Flux linkage accounts for the mutual inductance that occurs between 2 current elements that link one another. Although regions use different magnetic fields, each one contributes an induced magnetic field linking both the regions. This is seen from the example that even though the "internal inductance region had a magnetic field that was only contributed by the outer, we do not consider how the internal loop is also linked to the outer and must be accounted for.