



UNIVERSITÉ CATHOLIQUE DE LOUVAIN

Study of the stress relieve heat-treatment of additively manufactured AlSi10Mg alloy:

Influence on microstructure and mechanical properties

Dissertation presented by

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"The gem cannot be polished without friction, nor man perfected without trials."

Confucius

Acknowledgements

Blablabla. blabla. bla.

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List of Abbreviations

AM	Additive Manufacturing
CAD	Computer Aided Design
DMLS	Direct Metal Laser Sintering
DMP	Direct Metal Printer
ICP	Inductively Coupled Plasma
RODIA	Relative Optical Density Image Analysis
SEM	Scanning Electron Microscope
SLM	Selective Laser Melting

Symbols

D_a	Average particle size	$[\mu\text{m}]$
E_d	Volumetric energy density	$[\frac{\text{J}}{\text{mm}^3}]$
h	Hatch space	$[\mu\text{m}]$
H_v	Vickers hardness	$[HV]$
P	Laser power	$[\text{W}]$
p_{O_2}	Oxygen pressure	$[\text{mbar}]$
t	Layer thickness	$[\mu\text{m}]$
v_s	Scanning speed	$[\frac{\text{mm}}{\text{s}}]$
W_a	Specimen dry weight	$[\text{g}]$
W_w	Specimen underwater weight	$[\text{g}]$
ϵ_f	Strain at fracture	$[-]$
$\phi_{99\%}$	Laser spot size at the 99% contour	$[\mu\text{m}]$
λ	Laser wavelength	$[\text{nm}]$
ρ_a	Apparent density	$[\frac{\text{g}}{\text{cm}^3}]$
$\rho_{a,rel}$	Apparent relative density	$[-]$
ρ_w	Water density	$[\frac{\text{g}}{\text{cm}^3}]$
ρ_{rel}	Relative density	$[-]$
σ_u	Ultimate tensile stress	$[\text{MPa}]$

Nous dédions ce travail à nos familles et amis

Chapter 1

Introduction

This is, with the concluding chapter, a significant portion of memory. This should especially present the context and objectives of the work. Generally, the memory structure (content of chapters) is briefly exposed

Chapter 2

State of the art

2.1 Selective laser melting technology

Selective laser melting (SLM) - also referred to as direct metal laser sintering (DMLS) - is an additive manufacturing (AM) technique making use of a high power-density laser that locally melts powder materials. When a layer of powder has been melted, a new layer is spread on top of the previous one, and is in turn melted, in order to progressively build a 3D object. The technique is illustrated on figure 2.1 [13]. The materials used include mostly metals but also ceramics and composites. Parts to build must first be drawn in a computer-aided design (CAD) software and broken down in 2D slices, each one corresponding to a powder layer. During the process, the oxygen pressure p_{O_2} must be kept low to prevent the oxidation of the metal. A shielding gas - such as argon - is thus used to fill the build chamber at all time, while p_{O_2} is monitored.

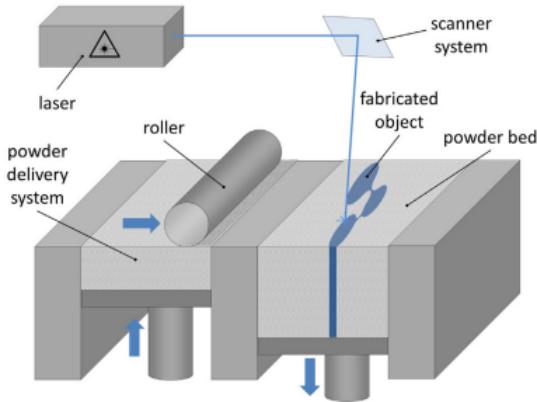


FIGURE 2.1: Selective laser melting technology principle (from Leitz et al., 2016).

LSM is still a young technology. Its popularity only increased significantly over the last decade, as depicted by figures 2.2 (a) and (b). Works concerning AlSi10Mg began to emerge noticeably in 2014. The technique usage spread rapidly in many sectors: biomedical, heat exchangers, aerospace and automotive - to name just a few [25]. This is due to the numerous appeals of SLM compared to the other technologies, including:

- Geometrical flexibility: parts can be designed with thin walls or even with hidden cavities and/or channels. This offers promising prospects regarding light-weight potentials for parts solicited mechanically [15];
- Increased reliability of the parts [8];
- Reduced equipment costs [9];
- Better operational efficiency: the fabrication is quick and easy which reduces time-to-market as well as assembly times and capital tied up in stocks [9];
- Individual production facilitation [8];
- Reduced material waste and better energy usage: the process is environmentally friendly as a whole [8].



FIGURE 2.2: (a)Research publications on SLM of ceramics, composites and all materials types combined. (b)Research publications on SLM of different metallic materials. Data are derived from the research publications on SLM, LaserCusing and DMLS existing on ScienceDirect website.

The properties of parts produced through SLM stem from the coupled effects of a great deal of parameters (see figure 2.3) [3]. Results are very sensitive to their variations. The process parameters must thus be monitored thoroughly. This complicates the search for their optimisation, still not fully resolved for aluminium alloys.

In recent years, works aiming at facing this challenge multiplied. The minimisation of the porosity is at the center of attention. It is indeed closely related to the quality of the mechanical properties. As porosity contributes to lowering the load-bearing surface, it reduces the apparent material strength. It was also observed to have a critical influence on the fatigue life of the produced parts. Their lifetime is especially diminished if the values of pores amount and size go beyond a certain threshold [5]. Studies investigating the effects of various parameters on the AlSi10Mg fabrication through SLM abound in the literature.

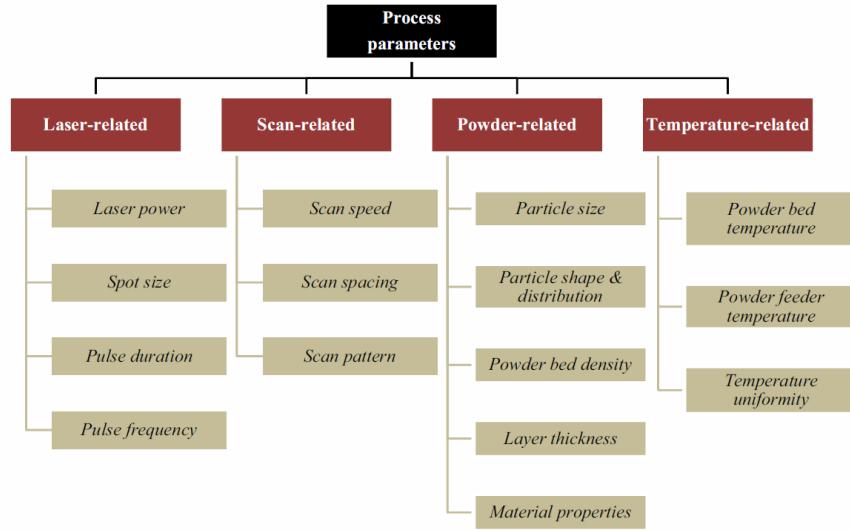


FIGURE 2.3: Parameters involved in SLM (from Aboulkhair et al., 2014).

2.2 AlSi10Mg alloy

Parler de l'AlSi10Mg; quel est l'intérêt de travailler avec? Difficultés? (reflectivité etc).. Qu'est ce qui existe en coulé, forgé etc
Microstructure homogène, diagramme de phase

2.3 Fabrication process parameters

Let us now investigate the influence of the parameters on the properties of AlSi10Mg parts manufactured with SLM. The analysis of the paired impacts of the laser power P and scan speed v_s provides a first insight. As depicted by figures 2.4 and 2.5, low P and high v_s lead to an insufficient energy input to melt the powder and re-melt the substrate, which causes the formation of droplets [12]. The opposite leads to good penetration but also to distortions and irregularities. A trend to use both high P and v_s rose in accordance with these findings. Doing so has the advantage to increase productivity. However, it also has multiple downsides including a decrease of the surface quality due to balling, excessive spatter, and an augmented gas induced porosity [17]. Therefore, a trade-off must be found.

A popular approach is to regroup multiple operating parameters into one, the volumetric energy density E_d . It is estimated through the following formula:

$$E_d = \frac{P}{v_s h t}$$

where t is the layer thickness and h is the hatch space. As a rule of thumb, E_d should be chosen in the range between 60 and 75 [$\frac{J}{mm^3}$] [19]. However, the criterion is insufficient and other phenomena, such as melt pools overlapping, should be considered [22]. Very few studies were carried out to optimize h and t independently. Their values lie generally respectively in the intervals [50 ; 200] [μm] and [20 ; 60] [μm]

[SOURCES?]. It was observed that for $t = 30 \text{ } [\mu\text{m}]$, an optimal set of parameters values in terms of density is $P = 200 \text{ [W]}$, $v_s = 1400 \text{ [mm/s]}$ and $h = 105 \text{ } [\mu\text{m}]$ [12]. The apparent relative density $\rho_{a,rel}$ was then above 99.5 [%].

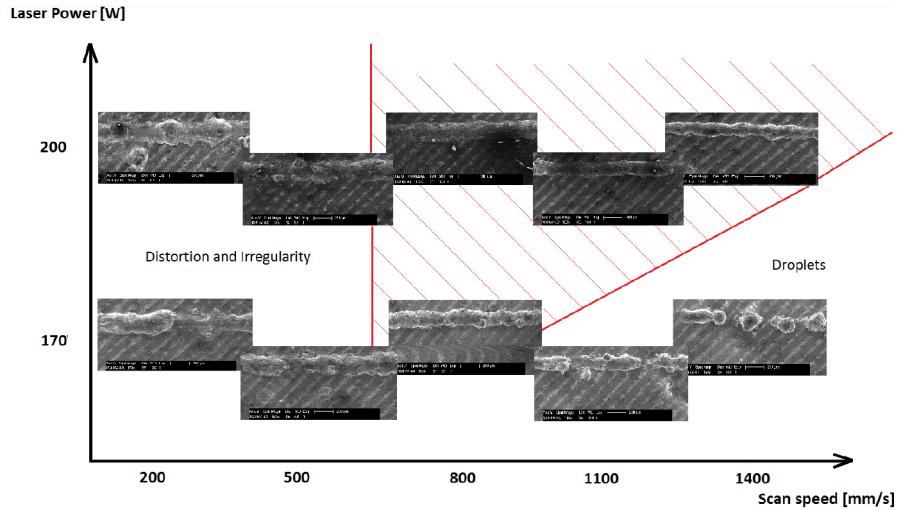


FIGURE 2.4: Process window for SLM of AlSi10Mg, based on the top view of single track scans (from Kempen et al., 2011).

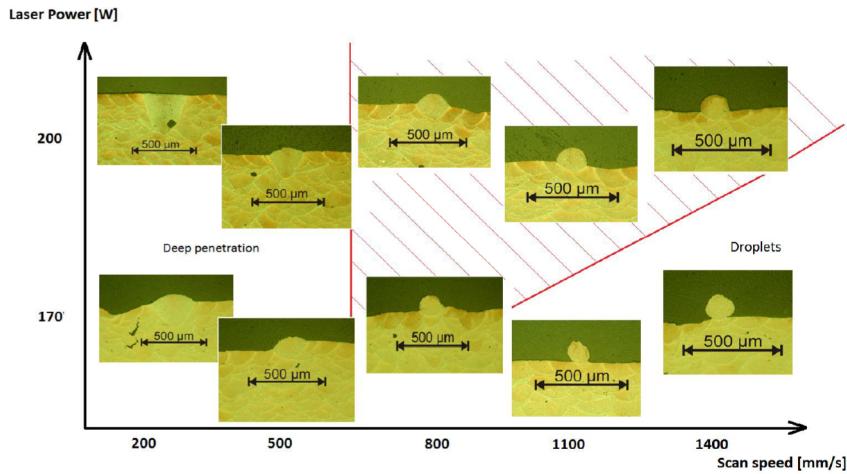


FIGURE 2.5: Process window for SLM of AlSi10Mg, based on the front view of single track scans (from Kempen et al., 2011).

The other process parameters will be covered for the sake of completeness. Let us first look into the particle-related parameters. The particle size D_a of the powder should be as small as possible to ensure a good flowability and allow for thin layers [12]. Typical values stretch from 15 to 60 $[\mu\text{m}]$ [SOURCES?]. The size distribution is more delicate to outline. On one hand, wider distributions often generate better bed density, parts with higher density and better surface finish. On the other hand, narrower ones usually provide better flowability and parts with better strength and hardness [16]. In most cases, a middle ground between the two should be sought. In SLM applications, powder is often successively recycled multiple times. This leads

to their progressive contamination with moisture, which causes an increase of hydrogen porosity in the produced parts [24]. The problem can be overcome by drying the powder or using fresh one. Unfortunately - in the case of aluminium alloys - no findings were made regarding the prediction of a threshold at which one should take action [4].

The choice of scan pattern has great importance. There exist a few different strategies. The common ones use unidirectional, bidirectional or islands patterns (see figure 2.6). The scan direction(s) should always be rotated between successive layers to favorise isotropy, especially in the unidirectional case since it causes height variations along a layer [2]. The islands pattern is based on a decomposition in small domains with short scanning tracks. Two usual strategies can be distinguished among this group: the chessboard and the hexagonal one. A study proved the superiority of an island pattern over a bidirectional one in terms of both ultimate tensile stress σ_u and strain at fracture ϵ_f for a 316L stainless steel-Inconel 718 material [26]. It was also shown that it was possible to fabricate pure titanium samples without cracks using an island pattern, and not with a bidirectional one [14]. This is seemingly due to the greater accumulation of internal stresses and to the weaker interlayer bounding in the second case.

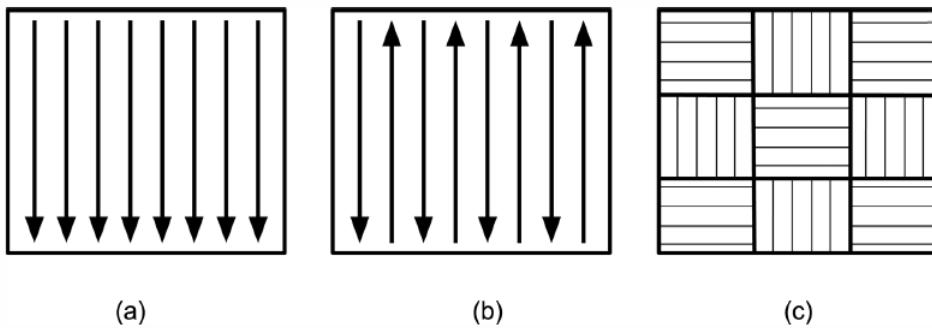


FIGURE 2.6: Schematic representation of scanning strategies commonly used in LSM (a) unidirectional long scan track; (b) bidirectional long scan track, and (c) islands (from Mertens et al., 2017).

Furthermore, dual scanning strategies were proven to be effective. For example, a pre-scan with low E_d can flatten the powder bed before it is consolidated, which leads to a reduction of porosity [17]. It was also shown that scanning the contour of the part being built at lower E_d can better the surface roughness for AlSi12Mg [18]. One should note too that the final properties of the fabricated part can strongly depend on the building direction (see figure 2.7) [7].

Other laser-related parameters - the spot size and the pulse properties - can also influence the process. Only the laser spot size at the 99% contour $\phi_{99\%}$ is frequently cited in literature. Its value lies between 100 and 200 [μm] [Sources?].

Finally, the temperature of the powder bed and feeder affect the final properties of the fabricated parts as well. In particular, it was observed that pre-heating the powder at 300° C mitigates the differences of fatigue resistance between tensile specimens built in different directions: it is possible that the operation induces a slower

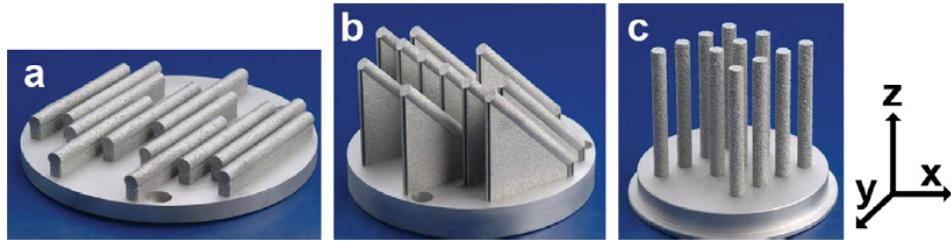


FIGURE 2.7: Samples (static tensile) built in different directions: (a) 0° , (b) 45° , and (c) 90° (from Brandl et al., 2012).

cooling rate which helps reducing the distortions and internal stresses [5].

Once the porosity problem is sorted out, other matters can be addressed such as productivity and surface roughness. The latter is problematic as the surface finish obtained with SLM is typically of such poor quality that all cracks initiate near the surface for a sample with relative density $\rho_{rel} > 99\%$ [5]. As said before, it is possible to reduce the surface roughness by mean of a dual scan strategy. However, the only options to obtain significantly better surface finish is currently to machine or polish the fabricated parts. This is one of the main weak points of SLM.

2.4 Mechanical properties

In a work of Kempen et al., additively manufactured AlSi10Mg samples were observed to have mechanical properties (Vickers hardness HV , ultimate tensile stress, fracture strain ϵ_f and impact energy) better or at least comparable to the conventionally casted and high pressure die casted (HPDC) casted alloy [11]. The tensile specimens built in an horizontal direction (XY) had slightly different characteristics than those built in the vertical direction (Z). The results obtained in the mentioned work are gathered in tables 2.1 and 2.2 in order to compare them to common cast AlSi10Mg properties.

Process	Young Modulus [GPa]	σ_u [MPa]	ϵ_f [%]	HV
SLM - XY direction	68 ± 3	391 ± 6	5.55 ± 0.4	127
SLM - Z direction		396 ± 8	3.47 ± 0.6	
Conventional cast and aged				
As built HPDC	71	300-317	2.5-3.5	86
T6 treated HPDC		300-350	3-5	95-105
		330-365		130-133

TABLE 2.1: Mechanical properties of SLM built parts and cast + aged parts (from Kempen et al., 2012)

Process	Impact energy [J]
SLM - XY direction	3.94 ± 0.5
SLM - Z direction	3.69 ± 0.48
Conventional cast	2.5-3.0

TABLE 2.2: Results of Charpy impact testing (from Kempen et al., 2012)

2.5 Post treatments

Post-traitements dont traitements thermiques, sur lesquels on se focalise. Expliquer

Chapter 3

Materials and methods

Description expériences et machines

3.1 Powder follow-up

3.1.1 Sieving

3.1.2 Grain size and distribution

3.1.3 Composition

3.2 Fabrication process parameters

The same direct metal printer (DMP) was used to fabricate all specimens throughout this work. It is a *ProX DMP 200* printer, manufactured by *3D Systems* (see figure 3.1). It uses a laser with a theoretical maximal power of 300 [W] and wavelength $\lambda = 1070$ [nm] [1]. Its actual maximal power is $P_{max} = 273.6$ [W]. [QUEL EST LE SPOT SIZE?] The maximal envelope capacity of the machine (W x D x H) is 140 x 140 x 125 [mm]. Its typical accuracy is +/- 50 [μm] for small parts and +/- 0.2% for large parts. It allows for the set-up of a protection atmosphere. However, it does not integrate any heating feature for the build bed.

In this thesis, argon was used as shielding gas. The composition of the gas environment was monitored so as to keep $p_{O_2} < 500$ [ppm]. Laser compensations were set to take into account the excess energy at the start and end of the scanning vectors (see figure 3.2). These were chosen in accordance with the manufacturer recommendations (figure 3.3). Values for h and t were respectively set to 100 [μm] and 30 [μm]. The other process parameters were varied so as to optimize the properties of the built specimens. Educated guesses were made based on literature and previous works done at the UCL. The parameters used are resumed in annex A.1. Batches were named in the format X200-yyymmdd. The prefix "X200" refers to the DMP used. It is followed by the date of printing (6 digits). Recycled powder was used for every batch except for X200-180222 and X200-180228. In the case of samples with contour scanning strategy, the contours were pre scanned for each powder layer with the same P and v_s used for the bulk.

All batches were first prepared on *DMP ProX Manufacturing*, a dedicated CAD software. It enabled to select the values for the parameters previously mentioned, as well as the position of the specimens. For this thesis, all cylinders and tensile specimens were fabricated vertically. [Parler des éprouvettes utilisées, dimensions? -> Dessin]



FIGURE 3.1: ProX DMP 200 printer (from the user's ProX DMP 200 general instructions document).

An island scanning strategy was chosen on account of research done on the subject (see section 2.3). It is a hexagonal pattern with [OVERLAP? TAILLE DES HEXAGONES?] The scanning order was automatically chosen. Figures with detailed specimens positions, denominations, scanning orders and sintering durations are available in annex A.2.

[Insérer images de trajets du laser].

3.3 Heat treatments

The heat treatments were conducted inside a unique oven of the ... model, manufactured by ..., which is able to reach a temperature of 400° C. Samples temperature data was obtained through a thermocouple welded to the sample surface. [Méthode de soudage, élévation de la température durant l'opération] The data was displayed and saved every 10 seconds, with a precision of 0.1° C, thanks to a ..., connected to the thermocouple (see Fig. for both devices).

Samples that were subject to a heat treatment were named in a particular format, to ease distinction between them. They received the name of the batch, followed by "TT-holdingtemperature-holdingtime-specific conditions".

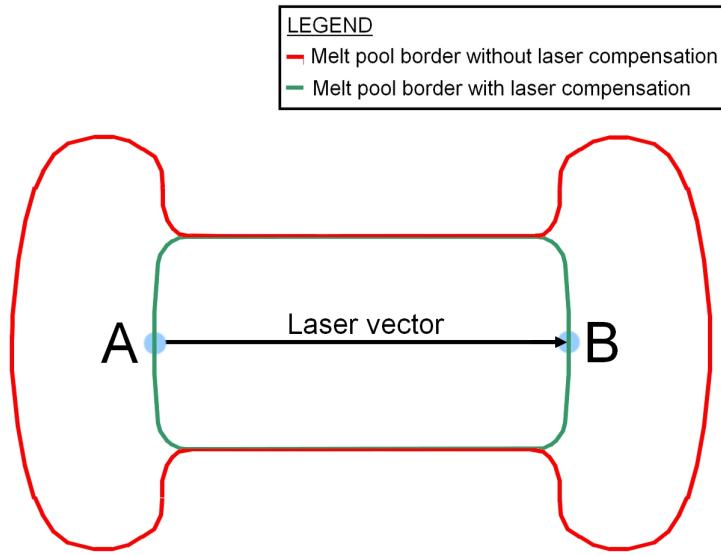


FIGURE 3.2: Melt pool contours with and without laser compensation (exaggeration).

3.4 Characterisation

3.4.1 Density

Hydrostatic weighing

Multiple methods were considered to estimate the relative density of the fabricated specimens. The first one is hydrostatic weighting (also called hydrodensitometry). It is a direct application of the well-known Archimedes' principle, which can be stated as follows: "When a body is (partially or totally) immersed in a fluid, the upthrust on the body is equal to the weight of fluid displaced." [6]. By weighing each pieces in air and in water - giving respectively values of dry weight W_a and underwater weight W_w - one can calculate the apparent density ρ_a [10]:

$$\rho_a = \frac{W_a}{W_a - W_w} \cdot \rho_w$$

where ρ_w is the water density. The apparent relative density $\rho_{a,rel}$ of the specimens can then be calculated with:

$$\rho_{a,rel} = \frac{\rho_a}{\rho_b}$$

where $\rho_b = 2.68[\frac{g}{mm^3}]$ is the theoretical bulk density of AlSi10Mg [20]. All weightings were done with a *Sartorius BP121S* analytical balance with precision of 0.1 [mg] [21]. Samples were immersed in demineralised water for more than twelve hours before the measurements to impregnate them. The weightings were also done in demineralised water. Water temperature was measured with a precision glass thermometer to compute ρ_w as accurately as possible thanks to tabulated values [23]. Multiple measurements were done for each sample in order to increase the method's reliability.

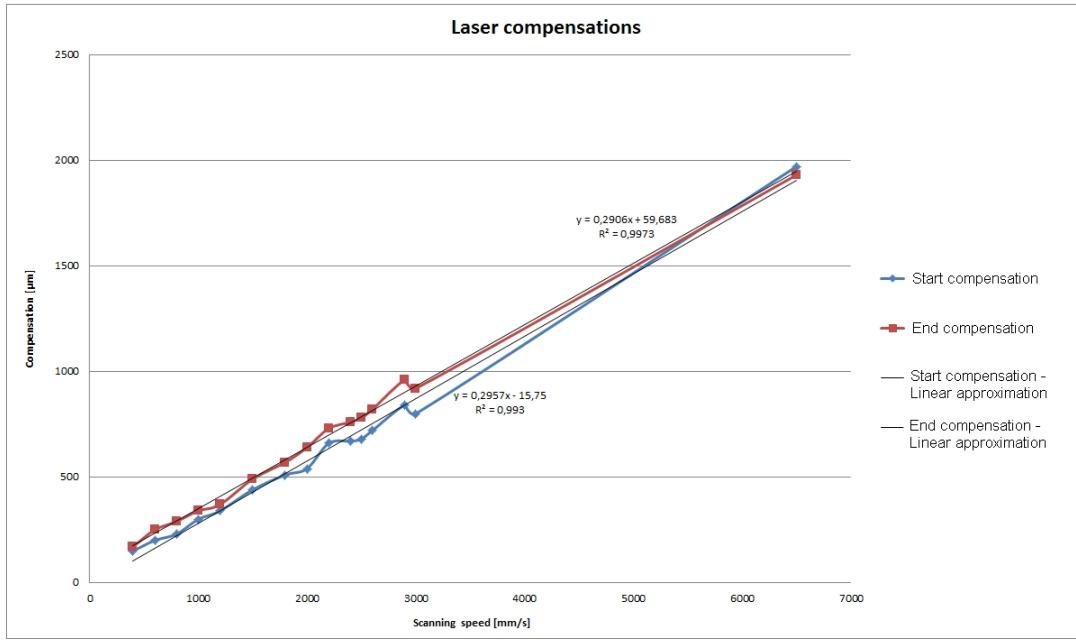


FIGURE 3.3: Laser compensations as a function of the scanning speed (as recommended by the manufacturer).

The technique was employed with "as-built" and polished cubes. For this second option, all six faces of the tested cubes were polished with P320 silicon carbide sandpaper sheets and briefly with P1200 ones.

Relative optical density image analysis

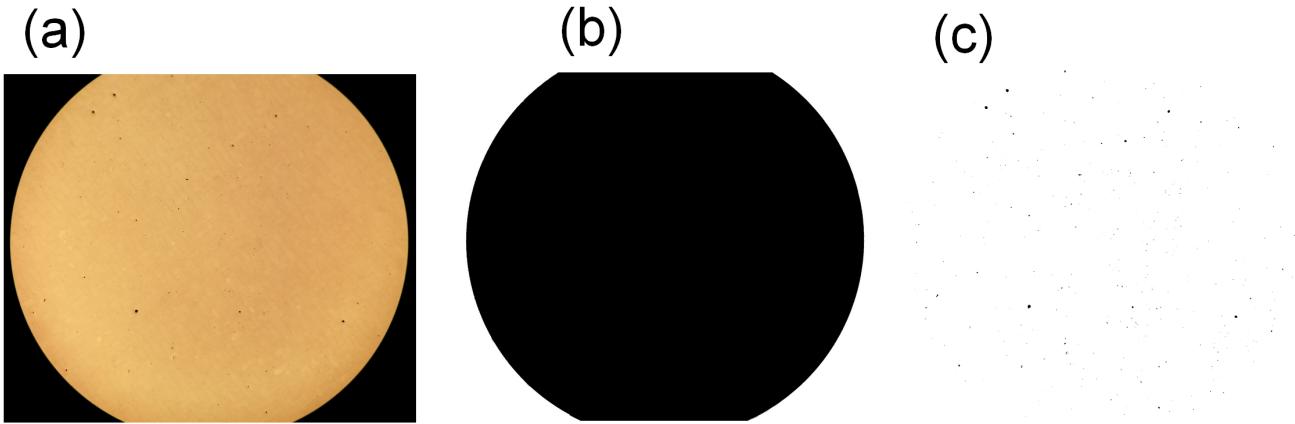
Another method was used to estimate the relative density of the various samples: the relative optical density image analysis (RODIA). For this purpose, the samples were cut with a micro-cutting machine and underwent the polishing routine detailed in table 4.2. Pictures of the polished sections were then taken under the optical microscope. An *Olympus AX70* microscope was used, with 5x and 10x magnification. The pictures were taken with a smart-phone trough the lens of the microscope. The used camera has a resolution of 16 [MP]. A camera is directly connected to the microscope at the laboratory, but it only has 5 [MP] resolution. It was thus chosen not to use it.

With the help of the *ImageJ* software, the surface of both the porosities and the whole surface could be isolated for each analysed image (see figure 3.4). The surface fraction occupied by porosities could then be obtained as the ratio between the areas of the two (in pixels). If we approximate that the porosities surface fraction is equal to the volumetric one, that method gives an estimation of the relative density ρ_{rel} .

The images isolations in "foregrounds" and "backgrounds" were done trough manual thresholding based on pixel intensity quantifications. An optimal threshold was sought for porosities isolation so as to include only holes, and as many as possible. Particular attention was given to the photography in order to obtain the best

Step	Polishing surface	Abrasive	Grain size	Lubricant type	Rotation speed [rpm]
1	MD-piano 220	Diamond	P220	Water	200-300
2	MD-piano 1200	Diamond	P1200	Water	200-300
3	MD-largo	DP-spray	9 μm	Alcohol	150
4	DP-DAC	DP-spray	3 μm	Alcohol	150
5	DP-NAP	DP-spray	1 μm	Alcohol	150

TABLE 3.1: Polishing routine for Al-Si alloys

FIGURE 3.4: RODIA procedure for specimen X200-180319-cub 1: (a) Original picture of polished section (b) Whole surface isolation with *ImageJ* (c) Porosities isolation with *ImageJ*.

contrast, focus and intensity homogeneity. Several pictures were taken for each specimen to build a representative sample.

3.4.2 Microstructure

Scanning electron microscopy

Optical microscopy

Mesures Taille de bains Densité Autre chose?

3.4.3 Composition

3.4.4 Internal stress

3.4.5 Mechanical properties

Hardness test

Vickers hardness measurements were made with a *Wolpert Dia-Testor 2RC* tester. All analysed specimens were previously cut with a micro-cutting machine to enable the measurement of the bulk hardnesses of the samples (at least at a few millimetres from the initial surfaces). For each test, a pyramidal indenter (see figure 3.5) was pressed during 10 [sec] onto the material with a load of 10 [kg]. The indentation durations were measured with a digital timer and the tests were stopped manually. The two diagonals lengths of the resulting indents were then evaluated using a ruler

on the screen of the machine, which displays the image of the sample's surface that is captured by an embedded optical microscope.

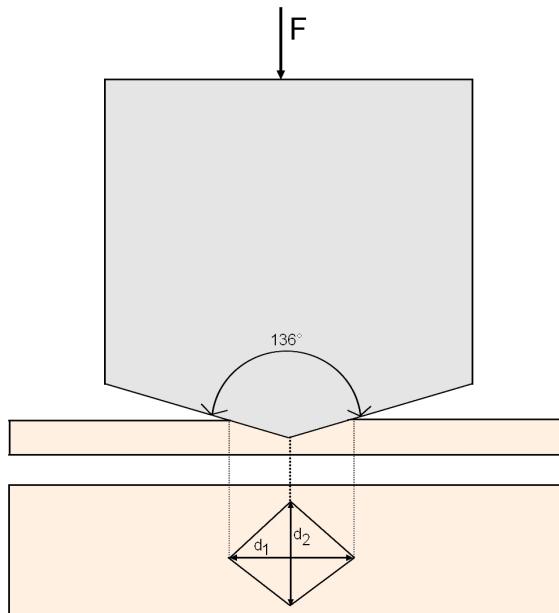


FIGURE 3.5: Schematization of the Vickers hardness test

Multiple tests were made for each sample and the mean diagonal length value was computed for every test. The corresponding Vickers hardness values HV could then be estimated by means of a conversion table.

Tensile test

The traction tests were performed on [Machine?]. The tensile specimens used all originated from batch X200-190417. Details about their geometry and undergone heat treatments can be consulted respectively in sections 3.2 and 3.3. [Fonctionnement de la machine] [Calcul des caractéristique matériau]

For each test, the extensometer gauge length was set to 18 [mm] and the pre load to 15 [N]. A cross head speed of 1 [$\frac{mm}{min}$] was chosen. It was decided to interrupt the tensile tests of one specimen of every group that underwent the same heat treatment. In that way, the damage mechanisms could be observed afterwards. Table 3.2 regroups the deformation limits at which the tests were stopped.

Sample	Strain limit [-]
X200-180417-3	0.01
X200-180417-6	0.06
X200-180417-9	0.08

TABLE 3.2: Strain limits for interrupted tensile tests of batch X200-180417 specimens

Chapter 4

Results

Analyses statistiques etc...

4.1 Parameters optimisation

4.2 Reproducibility

4.2.1 Relative density and mechanical properties

4.2.2 Melt pool size and distribution

4.3 Internal homogeneity

4.4 Powder ageing

4.4.1 Grain size and distribution

Fresh powder

Recycled powder

4.4.2 Composition

Fresh powder

Recycled powder

Date of sampling	Date of last addition of fresh powder	Composition [%wt]			
		Al	Fe	Mg	Si
23/10/2017	07/09/2017	89.2	0.12	0.49	10.2
09/01/2018	07/09/2017	89.3	0.13	0.48	10.1
12/01/2018	07/09/2017	89.4	0.13	0.48	10
21/02/2018	07/09/2017	89.1	0.19	0.51	10.3
13/03/2018	22/02/2018	89.1	0.16	0.51	10.1

TABLE 4.1: Composition of recycled AlSi10Mg powder as a function of the date

4.5 Heat treatments

4.5.1 Heating process

4.5.2 Microscopy

4.5.3 Hardness testing

4.5.4 Tensile testing

Specimen	Contour	TT	E [GPa]	σ_y [MPa]	σ_u [MPa]	ϵ_f [%]
X200-180417-1	Yes	None	85.3	260.8	366.4	2.2
X200-180417-2	Yes	None	68.2	290.2	388.3	2.4
X200-180417-3	Yes	None	64.0	275.9	-	-
X200-180417-A	No	None	61.0	257.1	379.2	2.8
X200-180417-7	Yes	250°C (2h)	72.2	230.7	334.5	9.1
X200-180417-8	Yes	250°C (2h)	70.2	238.9	347.4	8.6
X200-180417-9	Yes	250°C (2h)	71.3	227.7	$\simeq 328.7$	-
X200-180417-4	Yes	300°C (2h)	164.4	164.4	249.6	14.1
X200-180417-5	Yes	300°C (2h)	68.4	172.4	256.24	13.1
X200-180417-6	Yes	300°C (2h)	68.6	168.5	$\simeq 242.5$	-

TABLE 4.2: Tensile mechanical properties of the specimens from batch
X200-180417

4.5.5 Internal stress testing

Chapter 5

Discussion

Que conclure d'après les résultats?

5.1 Parameters optimisation

5.2 Reproducibility

5.2.1 Melt pool size distribution

5.3 Powder ageing

5.3.1 Grain size and distribution

5.3.2 Composition

5.4 Density measures assessments

5.4.1 Hydrostatic weighing

This second option reduces the risks of air trapping by the surface roughness, which can distort the results (by overestimating the closed porosities volume).

5.4.2 Relative optical density image analysis

The estimation of the relative density through RODIA can be distorted on many grounds. First, the distribution of porosities is inhomogeneous on the analysed surface. Multiple photos must thus be taken with a systematic manner for each specimen to constitute a representative sample.

Second, the quality of the photographs has a critical role. The isolation of the porosities during the thresholding requires a substantial difference of pixel intensity between the holes and the material. Since some porosities and some zones of the material can appear respectively brighter or darker than what is expected, there are risks that one isolates spots and/or not actual porosities. Additionally, the thresholding is manual and thus prone to slight human errors.

Most importantly, the finite resolution of the camera implies that sufficiently small porosities are not visible on the pictures. The exact shape of the holes are also imperfectly transcribed due to the discretization in pixels. Results for pictures with different magnifications were compared to quantify these effects. For this purpose, a picture was taken under 5x magnification and two under 10x magnification. The former was delimited to match the visible zones on the latter (see figure 5.1).

The same two zones - named A and B - were thus analysed for different levels of resolution.

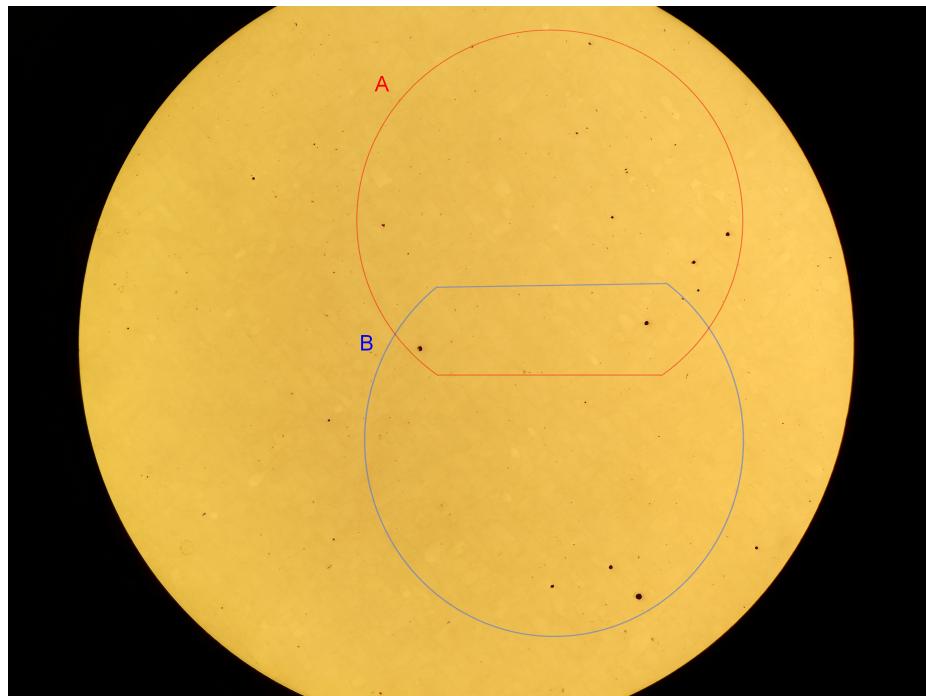


FIGURE 5.1: 50x magnification picture of specimen X200-180319-cub1
and delimitation of the zones A and B

The comparison of figures 5.2 (b) and (d) shows that much more small porosities are isolated if the resolution is refined - as expected. This is confirmed by the histograms on figure 5.3. The threshold of porosity area for detection in the case of 5x magnification is $7.84 \text{ } [\mu\text{m}^2]$ whereas it is $1.96 \text{ } [\mu\text{m}^2]$ for 10x magnification. This area corresponds to a pixel in each case. It is also worth noting that there is an overall tendency to overestimate the areas at lower resolution, which counterbalances slightly the low number of detected porosities.

The RODIA results for zones A and B are outlined in table 5.1. The lack of resolution seems to cause an overestimation of a few hundredths of percent of the relative density. The method is thus presumably positively biased. However, the observed effect is minor: this is probably due to the fact that the undetected porosities are the smallest, which influence the less the calculated density value.

Taking pictures at refined magnification could be considered to better the precision of the method. This would, however, require to augment the number of analysed pictures to have a sample of pictures as representative. A picture with doubled magnification covers indeed four times less surface. The number of analysis should thus be quadrupled to take as much information into account.

Zone	Magnification	Measured relative density [%]
A	50x	99.87
A	100x	99.84
B	50x	99.86
B	100x	99.85

TABLE 5.1: RODIA results for zones A and B of specimen X200-180317 with 50x and 100x magnification

5.5 Heat treatments

5.5.1 Heating process??

5.5.2 Microstructure

5.5.3 Mechanical properties

5.5.4 Internal stress

5.5.5 Optimisation

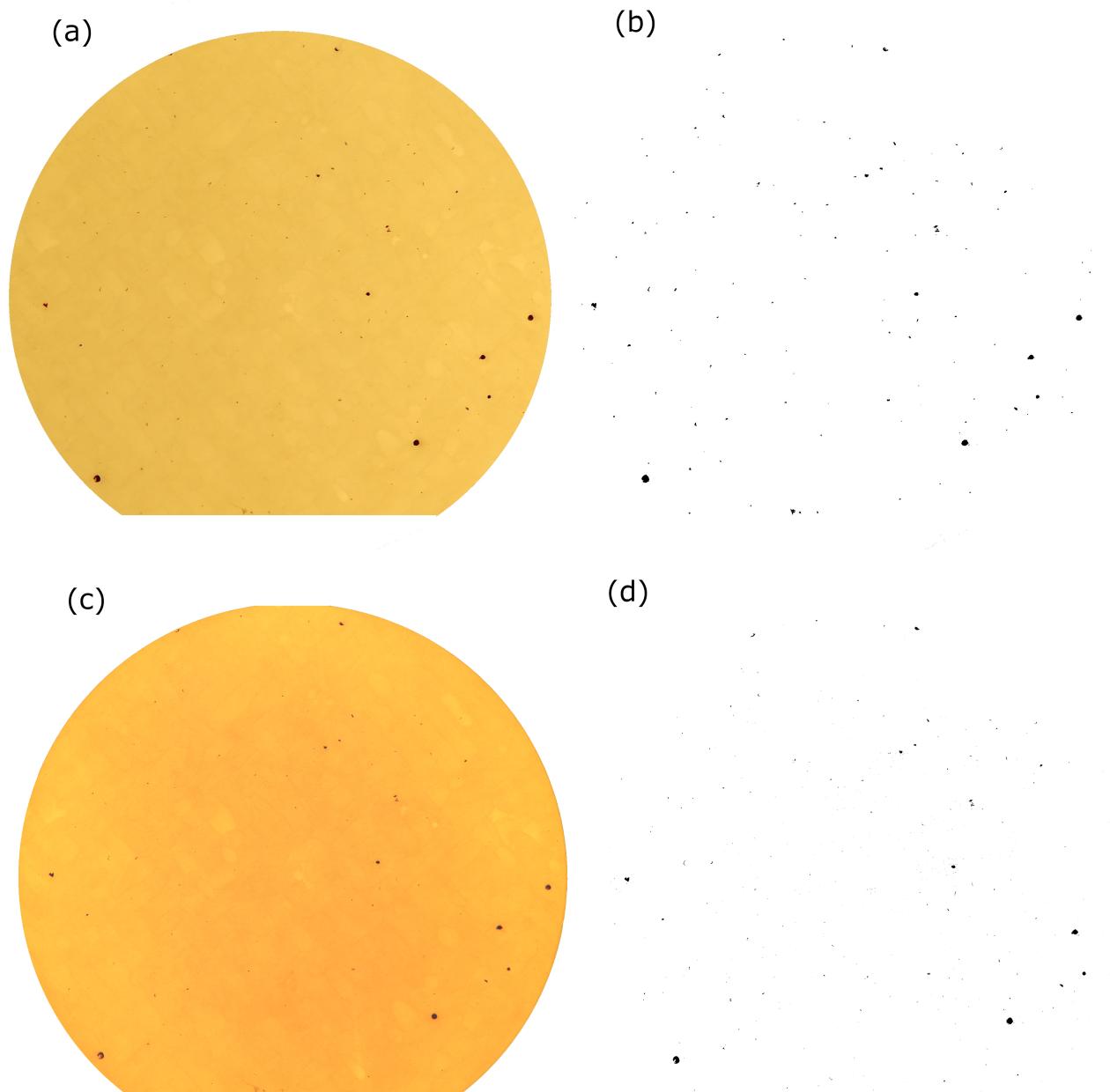


FIGURE 5.2: Zone A of specimen X200-180319-cub1: (a) Delimitation from original picture under 50x magnification (b) Porosities isolation from 50x magnification picture (c) Original picture under 100x magnification (d) Porosities isolation of 100x magnification picture

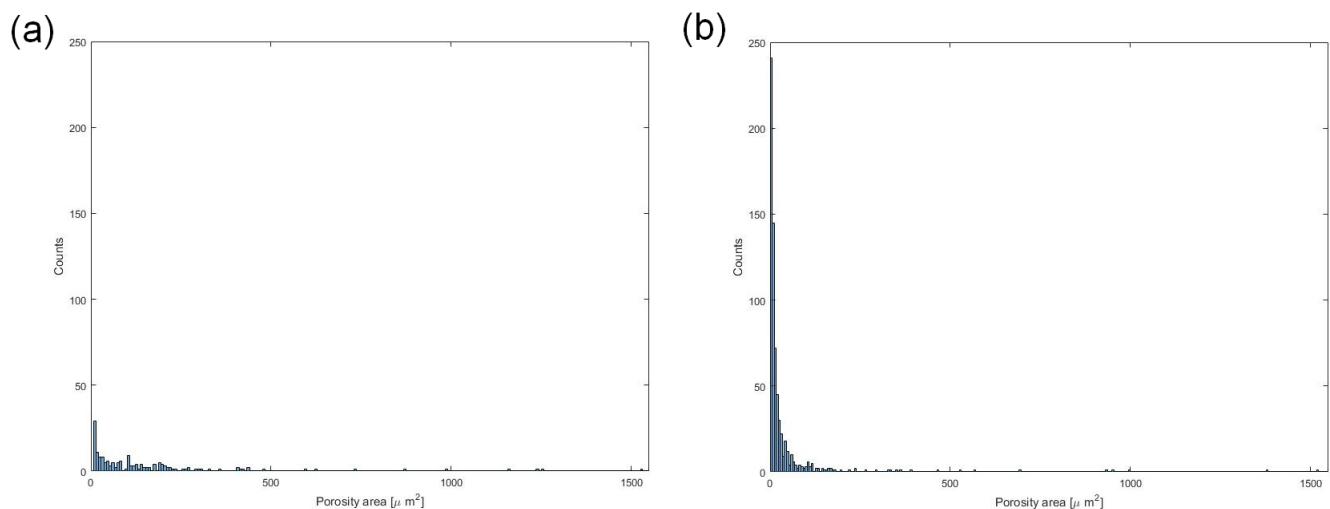


FIGURE 5.3: Histograms of porosities areas occurrences from pictures of specimen X200-180319 on zone A under (a) 50x magnification (b) 100x magnification. Truncation along the x axis.

Chapter 6

Conclusion

They incorporate in a synthetic way the main results and compare them with the initial objectives. Generally, this final chapter also presents prospects for the continuation of the work undertaken.

Appendix A

Batches fabrication details

A.1 Process parameters

Dimensions of the cubic and cylindrical specimens are noted in accordance with figure A.1. [AJOUTER DERNIER BATCH]

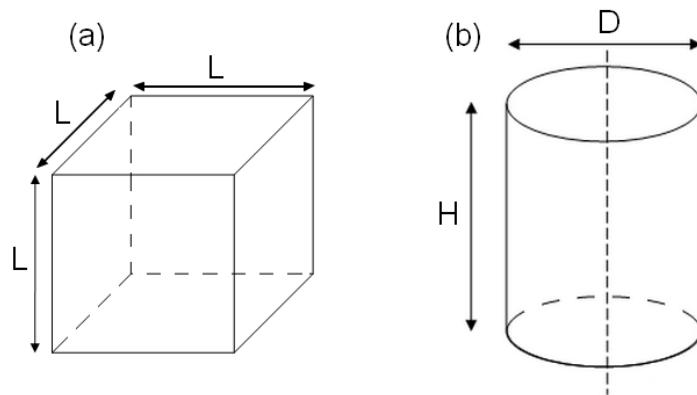


FIGURE A.1: Dimensions notations for (a) cubic specimens (b) cylindrical specimens

A.2 Specimens positioning, fabrication orders and sintering times

A.2.1 Batch X200-171024

A.2.2 Batch X200-180109

...

A.2.3 ...Other batches



FIGURE A.2: Specimens positions, order of fabrication and sintering times for batch X200-171024



FIGURE A.3: Photography of the manufacturing plate after completion of the fabrication of batch X200-171024

Batch name	Contour	Type	Dimensions [mm]	Specimen name	$\frac{P}{P_{max}} [-]$	$v_s [\frac{mm}{s}]$
X200-171024	No	Cubic	L=10	1 2 3 4 5 6 7, 7a, 7b 8, 8a, 8b	0.85 1 0.75	900 1000 1059 1500 900 1059 1200 900
X200-180109	No	Cubic	L=10	7c,...7q (15 spec.) 8c,...8q (15 spec.)	0.75	1200 900
X200-180220	No	Cubic	L=5	TT150-2 TT200-2 TT300-2 TT300-2-plaque TT150-2-real TT200-2-real TT250-2-real TT300-2-real	0.75	1200
X200-180222	No	Cubic	L=10	12 13	0.75	1200
X200-180228	Yes	Cylindrical	D=6, H=2	1 2 3	0.75	1200
X200180313	Yes	Cylindrical	D=6, H=10 D=12, H=10	1 2 3 4	0.75	1200
X200-180319	No	Cubic	L=10	cub 1 cub 2 cub 3 cub 4 cub 5	0.75	1200
	Yes	Cylindrical	L=5 D=6, H=10 D=12, H=10	TT300-1-real cyl 1 cyl 2 cyl 3 cyl 4		

TABLE A.1: Manufacturing process parameters

Appendix B

Extract of Vickers hardness conversion table (HV10)

Mean diagonal length [mm]	0	1	2	3	4	5	6	7	8	9
0.34	160	160	159	158	157	156	155	154	153	152
0.35	151.4	150.5	149.7	148.8	148.0	147.1	146.3	145.5	144.7	143.9
0.36	143.1	142.3	141.5	140.7	140.0	139.2	138.4	137.7	136.9	136.2
0.37	135.5	134.7	134.0	133.3	132.6	131.9	131.2	130.5	129.8	129.1
0.38	128.4	127.7	127.1	126.4	125.8	125.1	124.5	123.8	123.2	122.6
0.39	121.9	121.3	120.7	120.1	119.5	118.9	118.3	117.7	117.1	116.5
0.40	115.9	115.3	114.8	114.2	113.6	113.1	112.5	111.9	111.4	110.9
0.41	110.3	109.8	109.3	108.7	108.2	107.7	107.2	106.6	106.1	105.6
0.42	105.1	104.6	104.1	103.6	103.1	102.7	102.2	101.7	101.2	100.8
0.43	100.3	99.8	99.4	98.9	98.5	98.0	97.6	97.1	96.7	96.2
0.44	95.8	95.3	94.9	94.5	94.1	93.6	93.2	92.8	92.4	92.0
0.45	91.6	91.2	90.8	90.4	90.0	89.6	89.2	88.8	88.4	88.0
0.46	87.6	87.3	86.9	86.5	86.1	85.8	85.4	85.0	84.7	85.3
0.47	84.0	83.6	83.2	82.9	82.5	82.2	81.8	81.5	81.2	80.8
0.48	80.5	80.2	79.8	79.5	79.2	78.8	78.5	78.2	77.9	77.6
0.49	77.2	76.9	76.6	76.3	76.0	75.7	75.4	75.1	74.8	74.5
0.50	74.2	73.9	73.6	73.3	73.0	72.7	72.4	72.1	71.9	71.6
0.51	71.3	71.0	70.7	70.5	70.2	69.9	69.6	69.4	69.1	68.8
0.52	68.6	68.3	68.1	67.8	68.5	67.3	67.0	66.8	66.5	66.3
0.53	66.0	65.8	65.5	65.3	65.0	64.8	64.5	64.3	64.1	63.8
0.54	63.6	63.4	63.1	62.9	62.7	62.4	62.2	62.0	61.7	61.5

TABLE B.1: Extract of Vickers hardness conversion table (HV10)

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