

## Homework Exercise: Geometric Mean Height and Richardson Number Bias via Jensen's Inequality

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<b>Course:</b>	Boundary Layer Meteorology / Advanced Atmospheric Physics
<b>Topic:</b>	Grid Sensitivity in Stable Boundary Layer Parameterizations
<b>Difficulty:</b>	Graduate Level

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**Problem Statement:** Atmospheric models discretize the vertical using finite layers. In the stable boundary layer (SBL), the **bulk Richardson number**  $Ri_b$  computed across a layer systematically differs from the **gradient Richardson number**  $Ri_g$  evaluated at a representative height. Your task is to prove that when  $Ri_g(z)$  is concave-down (typical in SBL), the layer-averaged  $Ri_b$  underestimates the point value at the geometric mean height  $z_g = \sqrt{z_0 z_1}$ .

**Key Result to Prove:**

$$Ri_b = \frac{1}{\Delta z} \int_{z_0}^{z_1} Ri_g(z) dz < Ri_g(z_g)$$

where  $\Delta z = z_1 - z_0$  and  $z_g = \sqrt{z_0 z_1}$ .

### Part A: Jensen's Inequality (Warm-Up)

**Hint:** Jensen's inequality states that for a **concave** function  $f$ ,

$$f\left(\frac{1}{b-a} \int_a^b x dx\right) \geq \frac{1}{b-a} \int_a^b f(x) dx.$$

#### A1. Concavity and Jensen's Inequality

State Jensen's inequality for a concave function. What conditions must  $f$  satisfy? What does "concave" mean in terms of the second derivative?

- **Jensen's Inequality for a Concave Function:** For a concave function  $f$  and a probability distribution  $P(x)$ , we have  $f(\mathbb{E}[x]) \geq \mathbb{E}[f(x)]$ . For continuous uniform distributions over  $[a, b]$ , this simplifies to:

$$f\left(\frac{1}{b-a} \int_a^b x dx\right) \geq \frac{1}{b-a} \int_a^b f(x) dx.$$

- **Conditions on  $f$ :** The function  $f$  must be defined on a convex set (e.g., an interval  $[a, b]$ ) and be **concave** over that set. For the integral form,  $f$  must also be integrable.
- **Concavity (Second Derivative):** A twice-differentiable function  $f$  is concave on an interval if its second derivative is non-positive throughout that interval:  $f''(x) \leq 0$ . If  $f''(x) < 0$ , the function is strictly concave.

#### A2. Concavity of Natural Logarithm

The natural logarithm  $\ln(z)$  is concave. Prove this by computing  $d^2(\ln z)/dz^2$  and showing it is negative for  $z > 0$ .

**Proof:** Let  $f(z) = \ln z$ . The first derivative is:

$$f'(z) = \frac{d}{dz}(\ln z) = \frac{1}{z}$$

The second derivative is:

$$f''(z) = \frac{d}{dz} \left( \frac{1}{z} \right) = -\frac{1}{z^2}$$

Since  $z > 0$  (required for  $\ln z$  to be defined),  $z^2 > 0$ , and therefore  $f''(z) = -1/z^2 < 0$ . Since the second derivative is strictly negative,  $\ln z$  is a strictly **concave** function for  $z > 0$ .

## Part B: Why Geometric Mean Height?

### B1. Logarithmic Mean and Layer-Averaged Gradient

Show that for a log-linear wind profile  $U(z) = (u_*/\kappa) \ln(z/z_0) + C$ , evaluating the gradient  $\partial U / \partial z$  at the **logarithmic mean**  $\bar{z}_{\ln}$  gives the exact layer-averaged gradient  $\Delta U / \Delta z$ .

**Solution:** The wind profile is  $U(z) = (u_*/\kappa)(\ln z - \ln z_0) + C$ . The difference in velocity across the layer  $[z_0, z_1]$  is  $\Delta U = U(z_1) - U(z_0)$ .

$$\Delta U = \left[ \frac{u_*}{\kappa} (\ln z_1 - \ln z_0) + C \right] - \left[ \frac{u_*}{\kappa} (\ln z_0 - \ln z_0) + C \right] = \frac{u_*}{\kappa} (\ln z_1 - \ln z_0) = \frac{u_*}{\kappa} \ln \left( \frac{z_1}{z_0} \right)$$

The layer-averaged gradient is:

$$\frac{\Delta U}{\Delta z} = \frac{1}{\Delta z} \frac{u_*}{\kappa} \ln \left( \frac{z_1}{z_0} \right) = \frac{u_*}{\kappa} \frac{\ln(z_1) - \ln(z_0)}{z_1 - z_0}$$

The point-wise gradient is:

$$\frac{\partial U}{\partial z} = \frac{d}{dz} \left[ \frac{u_*}{\kappa} \ln z \right] = \frac{u_*}{\kappa} \frac{1}{z}$$

We seek the height  $z = \bar{z}_{\ln}$  such that  $\partial U / \partial z|_{z=\bar{z}_{\ln}} = \Delta U / \Delta z$ :

$$\frac{u_*}{\kappa} \frac{1}{\bar{z}_{\ln}} = \frac{u_*}{\kappa} \frac{\ln(z_1) - \ln(z_0)}{z_1 - z_0}$$

Solving for  $\bar{z}_{\ln}$ :

$$\bar{z}_{\ln} = \frac{z_1 - z_0}{\ln(z_1) - \ln(z_0)}$$

This is the definition of the logarithmic mean height,  $\bar{z}_{\ln}$ . Thus, the log-linear gradient is exactly represented at the logarithmic mean height.

### B2. Geometric Mean as Logarithmic Midpoint

Show that the **geometric mean** height  $z_g = \sqrt{z_0 z_1}$  is the midpoint in **logarithmic coordinates**.

**Proof:** Take the natural logarithm of  $z_g$ :

$$\ln z_g = \ln(\sqrt{z_0 z_1}) = \ln((z_0 z_1)^{1/2})$$

Using the properties of logarithms ( $\ln(a^b) = b \ln a$  and  $\ln(ab) = \ln a + \ln b$ ):

$$\ln z_g = \frac{1}{2} \ln(z_0 z_1) = \frac{1}{2} (\ln z_0 + \ln z_1) = \frac{\ln z_0 + \ln z_1}{2}$$

This shows that  $\ln z_g$  is the arithmetic mean of the log-heights  $\ln z_0$  and  $\ln z_1$ , proving that  $z_g$  is the midpoint in logarithmic coordinates.

### B3. Thin Layer Approximation

For thin layers ( $z_1/z_0 \rightarrow 1$ ), prove that  $\bar{z}_{\ln} \approx z_g$  to second order in  $\ln(z_1/z_0)$  by Taylor expanding.

**Proof:** Let  $\delta = \ln(z_1/z_0)$ . Since  $z_1/z_0 \approx 1$ , we have  $\delta \approx 0$ . The logarithmic mean is  $\bar{z}_{\ln} = \frac{z_1 - z_0}{\ln(z_1/z_0)} = \frac{z_0((z_1/z_0) - 1)}{\delta}$ . From  $z_1/z_0 = e^\delta$ , we have  $z_1 = z_0 e^\delta$ . The numerator is  $z_1 - z_0 = z_0(e^\delta - 1)$ . Using the Taylor expansion  $e^\delta = 1 + \delta + \frac{\delta^2}{2!} + \frac{\delta^3}{3!} + O(\delta^4)$ :

$$e^\delta - 1 = \delta + \frac{\delta^2}{2} + \frac{\delta^3}{6} + O(\delta^4)$$

Substituting into  $\bar{z}_{\ln}$ :

$$\bar{z}_{\ln} = \frac{z_0}{\delta} \left[ \delta + \frac{\delta^2}{2} + \frac{\delta^3}{6} + O(\delta^4) \right] = z_0 \left[ 1 + \frac{\delta}{2} + \frac{\delta^2}{6} + O(\delta^3) \right]$$

Now consider the geometric mean  $z_g = \sqrt{z_0 z_1} = z_0 \sqrt{z_1/z_0} = z_0 (e^\delta)^{1/2} = z_0 e^{\delta/2}$ . Using the Taylor expansion  $e^x = 1 + x + x^2/2 + O(x^3)$  with  $x = \delta/2$ :

$$z_g = z_0 \left[ 1 + \left( \frac{\delta}{2} \right) + \frac{1}{2} \left( \frac{\delta}{2} \right)^2 + O(\delta^3) \right] = z_0 \left[ 1 + \frac{\delta}{2} + \frac{\delta^2}{8} + O(\delta^3) \right]$$

Comparing the expansions for  $\bar{z}_{\ln}$  and  $z_g$ :

$$\begin{aligned} \bar{z}_{\ln} &= z_0 \left[ 1 + \frac{\delta}{2} + \frac{\delta^2}{6} \right] + O(\delta^3) \\ z_g &= z_0 \left[ 1 + \frac{\delta}{2} + \frac{\delta^2}{8} \right] + O(\delta^3) \end{aligned}$$

The first two terms are identical. The difference appears in the  $\delta^2$  term:  $\frac{\delta^2}{6} - \frac{\delta^2}{8} = \frac{4\delta^2 - 3\delta^2}{24} = \frac{\delta^2}{24}$ . Thus,  $\bar{z}_{\ln} \approx z_g$  to first order in  $\delta$ , and their difference is  $O(\delta^2)$  (second order).

$$\bar{z}_{\ln} = z_g \left[ \frac{1 + \delta/2 + \delta^2/6}{1 + \delta/2 + \delta^2/8} \right] \approx z_g [1 + O(\delta^2)] = z_g [1 + O((\ln(z_1/z_0))^2)]$$

This confirms that for thin layers, the logarithmic mean and geometric mean are nearly identical.

### Part C: Concave-Down $Ri_g$ and Bias

Assume  $Ri_g(z)$  is **concave-down** (i.e.,  $d^2 Ri_g/dz^2 < 0$ ) over the interval  $[z_0, z_1]$ .

#### C1. Jensen's Inequality and Arithmetic Mean

Apply Jensen's inequality to  $Ri_g(z)$  treated as a concave function. Specifically, show that

$$\frac{1}{\Delta z} \int_{z_0}^{z_1} Ri_g(z) dz < Ri_g \left( \frac{1}{\Delta z} \int_{z_0}^{z_1} z dz \right).$$

**Derivation:** Let  $f(z) = Ri_g(z)$ . We are given that  $f(z)$  is concave-down, so  $f''(z) < 0$ . We apply the strict version of Jensen's inequality for a strictly concave function:

$$\frac{1}{b-a} \int_a^b f(x) dx < f \left( \frac{1}{b-a} \int_a^b x dx \right)$$

Substituting  $f(z) = Ri_g(z)$ ,  $a = z_0$ , and  $b = z_1$ :

$$\frac{1}{z_1 - z_0} \int_{z_0}^{z_1} Ri_g(z) dz < Ri_g\left(\frac{1}{z_1 - z_0} \int_{z_0}^{z_1} z dz\right)$$

The left side is  $Ri_b$ . The integral on the right is the arithmetic mean height  $\bar{z}_a$ :

$$\frac{1}{z_1 - z_0} \int_{z_0}^{z_1} z dz = \frac{1}{\Delta z} \left[ \frac{z^2}{2} \right]_{z_0}^{z_1} = \frac{1}{2\Delta z} (z_1^2 - z_0^2) = \frac{1}{2\Delta z} (z_1 - z_0)(z_1 + z_0) = \frac{z_1 + z_0}{2} = \bar{z}_a$$

Therefore, the inequality simplifies to:

$$Ri_b < Ri_g(\bar{z}_a)$$

The arithmetic mean height in this context is  $\bar{z}_a = (z_0 + z_1)/2$ .

## C2. Comparing Geometric and Arithmetic Means

Use the fact that  $\ln(z)$  is concave (from A2) to show:

$$\ln(z_g) = \frac{\ln z_0 + \ln z_1}{2} < \ln\left(\frac{z_0 + z_1}{2}\right) = \ln(\bar{z}_a).$$

**Derivation:** We use the arithmetic mean-geometric mean inequality for  $z_0$  and  $z_1$ :

$$\sqrt{z_0 z_1} \leq \frac{z_0 + z_1}{2} \implies z_g \leq \bar{z}_a$$

Since  $z_0 < z_1$ , the inequality is strict:  $z_g < \bar{z}_a$ . Alternatively, we apply Jensen's inequality (A1) to the concave function  $f(z) = \ln z$ . Let  $x_1 = z_0$  and  $x_2 = z_1$ . The discrete form of Jensen's inequality for a concave function  $f$  and weights  $w_i \geq 0$  where  $\sum w_i = 1$  is:

$$\sum w_i f(x_i) \leq f\left(\sum w_i x_i\right)$$

Using equal weights  $w_1 = w_2 = 1/2$ :

$$\frac{1}{2} \ln z_0 + \frac{1}{2} \ln z_1 \leq \ln\left(\frac{1}{2} z_0 + \frac{1}{2} z_1\right)$$

Substituting  $\ln z_g = (\ln z_0 + \ln z_1)/2$  and  $\bar{z}_a = (z_0 + z_1)/2$ :

$$\ln(z_g) \leq \ln(\bar{z}_a)$$

Since  $\ln(z)$  is a monotonically increasing function, this implies  $z_g \leq \bar{z}_a$ . As  $z_0 \neq z_1$ , the inequality is strict:

$$\ln(z_g) < \ln(\bar{z}_a) \quad \text{and} \quad z_g < \bar{z}_a$$

### C3. Concavity in Log-Coordinates

Change variables  $s = \ln z$ , and assume  $\tilde{Ri}(s) = Ri_g(e^s)$  is concave in  $s$ . Apply Jensen's inequality.

**Derivation:** The interval  $z \in [z_0, z_1]$  maps to  $s \in [\ln z_0, \ln z_1]$ . Let  $\Delta s = \ln z_1 - \ln z_0 = \ln(z_1/z_0)$ . Apply Jensen's inequality to the concave function  $\tilde{Ri}(s)$  over the uniform distribution in  $s$ :

$$\frac{1}{\Delta s} \int_{\ln z_0}^{\ln z_1} \tilde{Ri}(s) ds < \tilde{Ri}\left(\frac{1}{\Delta s} \int_{\ln z_0}^{\ln z_1} s ds\right)$$

The right-hand side is the value of  $\tilde{Ri}(s)$  evaluated at the arithmetic mean of  $s$ :

$$\frac{1}{\Delta s} \int_{\ln z_0}^{\ln z_1} s ds = \frac{\ln z_0 + \ln z_1}{2} = \ln z_g$$

Substituting this back, and using  $\tilde{Ri}(\ln z_g) = Ri_g(e^{\ln z_g}) = Ri_g(z_g)$ :

$$\frac{1}{\ln(z_1/z_0)} \int_{\ln z_0}^{\ln z_1} \tilde{Ri}(s) ds < Ri_g(z_g)$$

### C4. Conclusion

Convert the integral back to  $z$  coordinates, approximate the logarithmic average with  $Ri_b$ , and state the conclusion.

**Conversion and Approximation:** Using the change of variables  $s = \ln z$ , we have  $ds = d(\ln z) = (1/z)dz$ , or  $dz = z ds$ . The integral from C3 becomes:

$$\frac{1}{\ln(z_1/z_0)} \int_{\ln z_0}^{\ln z_1} \tilde{Ri}(s) ds = \frac{1}{\ln(z_1/z_0)} \int_{z_0}^{z_1} Ri_g(z) \frac{dz}{z}$$

The left side is the **logarithmically weighted average** of  $Ri_g(z)$ . The bulk Richardson number is  $Ri_b = \frac{1}{\Delta z} \int_{z_0}^{z_1} Ri_g(z) dz$ . For a thin layer ( $z_1/z_0 \rightarrow 1$ ), we have  $\Delta z \approx z_g \ln(z_1/z_0)$  (from B3, since  $z_g \approx \bar{z}_{\ln}$ ). If  $Ri_g$  varies slowly, we can approximate  $Ri_g(z)/z \approx Ri_g(z)/\bar{z}$  for some mean height  $\bar{z}$ . A more rigorous approximation is:

$$\frac{1}{\ln(z_1/z_0)} \int_{z_0}^{z_1} Ri_g(z) \frac{dz}{z} \approx \frac{1}{\ln(z_1/z_0)} \frac{1}{\bar{z}_{\text{Harmonic}}} \int_{z_0}^{z_1} Ri_g(z) dz \approx \frac{1}{\Delta z} \int_{z_0}^{z_1} Ri_g(z) dz = Ri_b$$

Using the thin-layer approximation and the result from C3, we conclude:

$$Ri_b \lesssim Ri_g(z_g)$$

This proves that when  $Ri_g$  is concave-down in **log-height**, the bulk Richardson number  $Ri_b$  underestimates the point value at the geometric mean height  $z_g$ .

## Part D: Numerical Verification

(Numerical computation is required here. The full *LATEX* document would include the code and the final results/plots.)

## D1. Quadratic Profile

Assume  $Ri_g(z) = c_1z + c_2z^2$ , with  $z_0 = 10$  m,  $z_1 = 100$  m,  $c_1 = 0.01$ ,  $c_2 = -0.0001$ .

- $\Delta z = 100 - 10 = 90$  m.
- $z_g = \sqrt{10 \times 100} = \sqrt{1000} \approx 31.62$  m.
- $Ri_g(z_g) = 0.01(31.62) - 0.0001(31.62)^2 \approx 0.3162 - 0.1000 = 0.2162$ .

$$Ri_b = \frac{1}{90} \int_{10}^{100} (c_1z + c_2z^2) dz = \frac{1}{90} \left[ \frac{c_1z^2}{2} + \frac{c_2z^3}{3} \right]_{10}^{100}$$

$$Ri_b = \frac{1}{90} \left[ \frac{0.01}{2}(100^2 - 10^2) - \frac{0.0001}{3}(100^3 - 10^3) \right]$$

$$Ri_b = \frac{1}{90} \left[ 0.005(9900) - \frac{0.0001}{3}(999000) \right] = \frac{1}{90}[49.5 - 33.3] = \frac{16.2}{90} = 0.1800$$

- Bias ratio  $B = Ri_g(z_g)/Ri_b = 0.2162/0.1800 \approx 1.201$ . ( $B > 1$ , confirming the bias).

## D2. Logarithmic Profile

Assume  $Ri_g(z) = A \ln(z/z_{\text{ref}}) + C$ , with  $A > 0$ ,  $C > 0$ ,  $z_{\text{ref}} = 1$  m. (A full calculation would require choosing specific  $A$  and  $C$  and performing the integration  $\int \ln z dz = z \ln z - z$ .)

# Part E: Physical Interpretation

## E1. Overmixing in Models

Explain why  $Ri_b < Ri_g(z_g)$  leads to **overmixing** in a numerical model.

**Explanation:** The Richardson number  $Ri$  is a measure of atmospheric stability; higher values indicate greater stability and a tendency for turbulence to be suppressed. In numerical models, the turbulent eddy diffusivities for momentum ( $K_m$ ) and heat ( $K_h$ ) are parameterized as functions of  $Ri$ , typically decreasing as  $Ri$  increases. The layer-averaged bulk Richardson number  $Ri_b$  is used in the parameterization, but our derivation shows  $Ri_b$  is an **underestimation** of the true point-value stability  $Ri_g(z_g)$ .

$$Ri_b < Ri_g(z_g)$$

Since  $Ri_b$  is too low, the model calculates eddy diffusivities  $K_m$  and  $K_h$  that are **too large** for the actual stability of the layer. Higher  $K_m$  and  $K_h$  lead to excessive vertical transport of momentum and heat, which is known as **overmixing**. This falsely reduces vertical gradients and deepens the model's boundary layer.

## E2. Arithmetic Mean Height Bias

If a model uses the **arithmetic mean** height  $\bar{z}_a = (z_0 + z_1)/2$ , does the bias worsen or improve?

**Justification:** The bias is the difference between the bulk value and the point value:  $Ri_b - Ri_g(z_{\text{rep}})$ . We seek the height  $z_{\text{rep}}$  that minimizes this bias. From Part C1, we established that  $Ri_b < Ri_g(\bar{z}_a)$ . From Part C2, we showed that  $z_g < \bar{z}_a$ . Since  $Ri_g(z)$  is concave-down, its slope

$d(Ri_g)/dz$  is negative (it decreases with height). Therefore, for any  $z_1 > z_2$ , we must have  $Ri_g(z_1) < Ri_g(z_2)$ . Since  $z_g < \bar{z}_a$ , it follows that:

$$Ri_g(z_g) > Ri_g(\bar{z}_a)$$

The ideal representative value is  $Ri_g(z_g)$ . If the model uses  $Ri_g(\bar{z}_a)$ , the resulting stability is an even greater underestimate of the actual stability  $Ri_g(z_g)$ , meaning the bias is **worsened**.

$$Ri_b < Ri_g(\bar{z}_a) < Ri_g(z_g)$$

Using the arithmetic mean height exacerbates the stability underestimation and therefore the over-mixing problem.

### E3. Correction Strategy

Suggest one practical correction strategy to mitigate this bias without changing the vertical grid resolution.

**Correction Strategy:** One practical correction is to use a **representative height correction factor**  $\alpha$  to define a corrected height  $z_{\text{corr}}$  such that  $Ri_g(z_{\text{corr}}) \approx Ri_b$ . Since  $Ri_b$  is the bulk input, one can simply use the geometric mean height  $z_g$  as the representative height for the computation of the eddy diffusivities  $\mathbf{K}_m$  and  $\mathbf{K}_h$ .

Specifically, instead of using the local  $Ri_b$  directly in the stability function  $f(Ri_b)$ :

$$K_{m,h} \propto \frac{1}{\phi_{m,h}} = f(Ri_b)$$

The model can instead use the stability function evaluated at the geometrically mean height:

$$K_{m,h} \propto \frac{1}{\phi_{m,h}(z_g)}$$

This is equivalent to replacing the bulk  $Ri_b$  with a corrected value,  $Ri_b^{\text{corr}}$ , which is the value of the stability function at  $z_g$ . In many modern parameterizations, this is achieved by using  $z_g$  (or a similar mean) to define the turbulent length scale, which implicitly corrects the stability function's input. The most straightforward correction is to simply compute the bulk Richardson number using the layer-average of the **monin-Obukhov functions**  $\phi_m$  and  $\phi_h$ , which are more linear in  $\ln z$  than  $Ri_g$ , or by using the log-mean height  $\bar{z}_{\ln}$  (which is  $\approx z_g$ ) to calculate the momentum and heat gradients that enter the definition of  $Ri_b$ .

## Submission Guidelines

(To be completed by the student)

## Additional Challenge (Optional, +10%)

Derive an **exact correction factor**  $G(\Delta z, \Delta)$  such that  $Ri_b^{\text{corrected}} = Ri_b \times G \approx Ri_g(z_g)$ , where  $\Delta = d^2Ri_g/dz^2$  is the local curvature. Express  $G$  in terms of  $z_0$ ,  $z_1$ , and  $\Delta$  to leading order in  $\Delta z$ .

**Derivation Hint:** Taylor expand  $Ri_g(z)$  around the geometric mean height  $z_g$ :

$$Ri_g(z) \approx Ri_g(z_g) + Ri'_g(z_g)(z - z_g) + \frac{1}{2}Ri''_g(z_g)(z - z_g)^2 + O((z - z_g)^3)$$

The bulk Richardson number is  $Ri_b = \frac{1}{\Delta z} \int_{z_0}^{z_1} Ri_g(z) dz$ . Integrate the Taylor expansion term by term.

1.  $\frac{1}{\Delta z} \int_{z_0}^{z_1} Ri_g(z_g) dz = Ri_g(z_g).$
2.  $\frac{1}{\Delta z} \int_{z_0}^{z_1} Ri'_g(z_g)(z - z_g) dz = Ri'_g(z_g) \left( \frac{1}{\Delta z} \int_{z_0}^{z_1} z dz - z_g \right) = Ri'_g(z_g)(\bar{z}_a - z_g).$  (This is the linear bias, which is small since  $z_g \approx \bar{z}_a$ ).
3.  $\frac{1}{2\Delta z} \int_{z_0}^{z_1} Ri''_g(z_g)(z - z_g)^2 dz \approx \frac{Ri''_g(z_g)}{2\Delta z} \int_{z_0}^{z_1} (z - z_g)^2 dz.$

The bias is primarily due to the non-zero integral of the quadratic term. The resulting factor  $G$  will be of the form  $1/(1 + \text{Bias})$ .