

Flujos de Potencia Newton Raphson (Con SVC - FA Model)					
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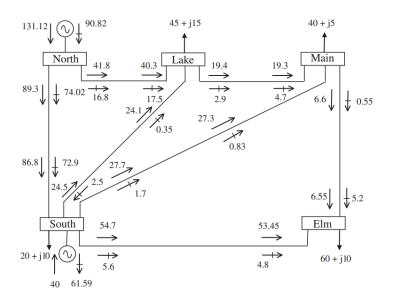
1) Se definen las bases del sistema

- Potencia base $S_b = 100 \cdot 10^6 \, \text{[VA]}$
- Voltaje base $V_b = 230 \cdot 10^3 \, [V]$

```
Sb = 100e6; %[VA]
Vb = 230e3; %[V]
```

2) Se crean las matrices con la información de la red (br_data, N_data):

Se deben crear dos matrices para ingresar la información referente al circuito. La primera (br_data) brinda información acerca de las conexiones entre buses como la impedancia de la línea o los buses entre los cuales se realiza la conexión, mientras que la segunda (N_data) da información acerca de la naturaleza de cada uno de los buses, tipo de bus (SL, PV o PQ).



a) Para la matriz br data se tiene que el formato es

brdata = [Bus_{from}, Bus_{to}, R, X, G, B] in p. u.

b) Para la matriz **N_data** se tiene que el formato es:

 $N \text{data} = \{ \# \text{Bus}, \text{type}(\text{'SL'}, \text{'PQ'}, \text{'PV'}), V[p.\,u.], \angle \text{V}^{\circ}, \text{PG}[p.\,u.], \text{QG}[p.\,u.], \text{PL}[p.\,u.], \text{QL}[p.\,u.] \}$

```
% Branches data R, X, G, B
% Types: General in form of impedance. (G & B are split in half at both ends).
```

```
% br data=[ bus1, bus2, R, X,
                                              B] in p.u.
                                      G,
br_data = [
                  2, 0.02,
                              0.06,
                                      0.0,
                                              0.06;
           1,
                  3, 0.08,
                              0.24,
                                      0.0,
                                              0.05;
           1,
           2,
                  3, 0.06,
                                              0.04;
                              0.18,
                                      0.0,
           2,
                  4, 0.06,
                              0.18,
                                      0.0,
                                              0.04;
           2,
                  5, 0.04,
                              0.12,
                                      0.0,
                                              0.03;
                  4, 0.01,
           3,
                              0.03,
                                      0.0,
                                              0.02;
                  5, 0.08,
                                              0.05];
           4,
                            0.24,
                                      0.0,
% Node definitions
% {  #, type, Vpu,
                     <Vº, PG pu, QG pu, PL pu, QL pu}
N_{data} = {
      'SL',
   1,
              1.06,
                      0.0,
                             0.0,
                                    0.0,
                                            0.00,
                                                    0.00;
      'PV',
   2,
             1.0,
                      0.0,
                             0.4,
                                    0.0,
                                            0.20,
                                                    0.10;
      'PQ',
             1.0,
                                    0.0,
                                            0.45,
                      0.0,
                             0.0,
                                                    0.15;
   3,
       'PQ', 1.0,
                                    0.0,
                                            0.40,
                                                    0.05;
   4,
                      0.0,
                             0.0,
      'PQ',
              1.0,
                      0.0, 0.0,
                                    0.0, 0.60,
   5,
                                                    0.10;  };
br_data=array2table(br_data, 'VariableNames', {'FromBus', 'ToBus', 'R', 'X', 'G', 'B'});
N_data=cell2table(N_data,'VariableNames',{'n','type','Vm','Va','PG','QG','PL','QL'});
```

c) Para el SVC:



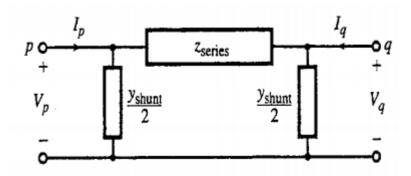
```
% STATIC VAR COMPENSATION
% FIRING ANGLE MODEL
% NSVC : Number of SVC's
% SVCsend : Compensated bus
% Xc : Capacitive reactance (p.u.)
% Xl : Inductive reactance (p.u.)
% FA : Initial SVC's firing angle value (Deg)
% FALo : Lower limit of firing angle (Deg)
% BHi : Higher limit of firing angle (Deg)
% TarVol : Target nodal voltage magnitude to be controlled by SVC (p.u.)
% VSta : Indicate the status to get control over voltage magnitude nodal : 1
% is on; 0 is off
% SVCsend(1)=3; Xc(1)=1.07; Xl(1)=0.288; FA(1)=140; FALo(1)=90;
% FAHi(1)=180; TarVol(1)=1.0; VSta(1)=1;
% SVC_data = [SVC node, Xc, XL, FA , FAmax, Famin, SVC TarVol, SVC Vsta]
SVC data = \begin{bmatrix} 3 & 1.07, 0.288, 140, 180, 90, 1, \end{bmatrix}
SVC_data=array2table(SVC_data,'VariableNames',{'SVCBus','Xc','XL', 'FA', 'FAmax', 'FAmin', '
```

	SVCBus	Xc	XL	FA	FAmax	FAmin	Tv	Status
1	3	1.0700	0.2880	140	180	90	1	1

3) Se crea Ybus con las redes de 2 puertos:

Se tiene la siguiente red de dos puertos, que representa el circuito del modelo pi de la línea de transmisión

$$\begin{bmatrix} V_i \\ V_j \end{bmatrix} = \begin{bmatrix} \frac{1}{z} + \frac{y}{2} & -\frac{1}{z} \\ -\frac{1}{z} & \frac{1}{z} + \frac{y}{2} \end{bmatrix} \begin{bmatrix} I_i \\ I_j \end{bmatrix}$$



Pi-equvalent model of a transmission line (Pag 296, Bergen)

Se extrae la información de las potencias y voltajes:

4) Construcción de la matriz Jacobiana

Se encuentran las dimensiones de la matriz jacobiana:

```
% Jacobian matrix size.

nL = sum(strcmp(N_data.type,'PQ'));% Number of PQ nodes (#Loads)
nG = sum(strcmp(N_data.type,'PV'));% Number of PV nodes (#Generators)
```

Se divide la matriz Jacobiana en la submatrices H-N-M-L

$$\int_{nL+nG}^{nL+nG} \begin{bmatrix} H & N \\ M & L \end{bmatrix}^k \begin{bmatrix} \Delta \theta \\ \Delta V/V \end{bmatrix}^k = \begin{bmatrix} \Delta P \\ \Delta Q \end{bmatrix}^k$$

(Eq. 3.32, pag108, Gómez - Exposito)

$$H_{ij} = \frac{\partial P_i}{\partial \theta_j}; \qquad N_{ij} = \frac{V_j}{\partial V_j} \frac{\partial P_i}{\partial V_j}$$
 $M_{ij} = \frac{\partial Q_i}{\partial \theta_j}; \qquad L_{ij} = \frac{V_j}{\partial V_j} \frac{\partial Q_i}{\partial V_j}$

(Eq. 3.34, pag109, Gómez - Exposito)

```
H = zeros( nL + nG, nL + nG );
L = zeros( nL, nL );
N = zeros( nL + nG , nL );
M = zeros( nL , nL + nG );
J = [H, N; M, L];
```

Se crea el vector de estados ($X = [\theta|V]^T$) y el vector de funciones no lineales ($f(x) = [\Delta P|\Delta Q]$

```
x_th = zeros( nL + nG, 1 ); % State vector for storing angles (theta)
x_v = zeros( nL , 1); % State vector for storing Voltages
```

$$x = [\theta|V]^{\mathrm{T}} = [\theta_1, \theta_2, \dots, \theta_{n-1}|V_1, V_2, \dots, V_{n_{\mathrm{L}}}]^{\mathrm{T}}$$
 dim= (2nL+nG)

```
x = [x_th; x_v];
```

• Donde se tiene que:

$$\Delta P_i = P_i^{\text{sp}} - V_i \sum_{j=1}^n V_j (G_{ij} \cos \theta_{ij} + B_{ij} \sin \theta_{ij}) \quad i = 1, 2, ..., n-1$$

$$\Delta Q_i = Q_i^{\text{sp}} - V_i \sum_{i=1}^n V_j (G_{ij} \sin \theta_{ij} - B_{ij} \cos \theta_{ij}) \quad i = 1, 2, \dots, n_{\text{L}}$$

(Eq. 3.30-3.31, pag108, Gómez - Exposito)

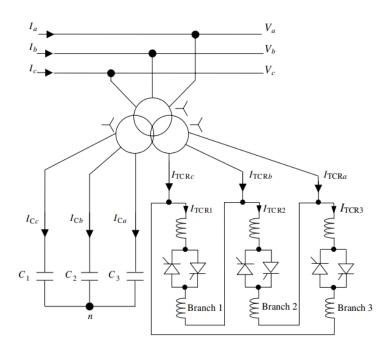
$$f(x) = [\Delta P | \Delta Q]^{\mathrm{T}} = [\Delta P_1, \Delta P_2, \dots, \Delta P_{n-1} | \Delta Q_1, \Delta Q_2, \dots, \Delta Q_{n_{\mathrm{L}}}]^{\mathrm{T}}$$
 dim= (2nL+nG)

```
Dt = [Dt_P;Dt_Q]; %Delta Vector (same as f(x) Vector)
%% Define Unkown Values (Voltage and angle in PQ node - Angle in PV node)
% #Buses with unknwon voltage magnitudes ('PO' buses) (Delta Q index)
x_v_n=N_data(strcmp(N_data.type,'PQ'),:).n;
% #Buses with unknwon voltage angles ('PQ'|'PV' buses) (Delta P index)
x_th_n=N_data(strcmp(N_data.type,'PV')|strcmp(N_data.type,'PQ'),:).n;
x_n = [x_{n}, x_{n}]; #Buses with unknown Angles and unknown voltages
max_iter = 100; %Define Max iteration number
V = zeros(n, max iter); % Matrix for storing node voltages per iter
V(:,1) = Vm_sp .* exp(1j .* th_sp); % Fill with initial Specified Voltages
Vm(:,1) = Vm_sp;
                                % Fill with initial Specified Magnitud
th(:,1) = th_sp;
                                % Fill with initial Specified Angle
err = 1.0; % Define Error
          % iteration counter
k = 1;
```

5) Inicia el método Newton Raphson

```
while (err > 1e-12 && k < max_iter)</pre>
```

Se tiene que para un SVC:



Para el delta de los TCR la susceptancia es:

$$B_{\mathrm{TCR}} = rac{2(\pi-lpha) + \sin 2lpha}{\omega L\pi}$$
 (Eq. 2.6, Acha)

Por ende en el SVC al tener en paralelo el banco de capacitores en Y con el delta de TCR:

$$B_{\rm SVC} = B_{\rm C} - B_{\rm TCR} = \frac{1}{X_C X_L} \left\{ X_L - \frac{X_C}{\pi} [2(\pi - \alpha) + \sin 2\alpha] \right\},$$

$$X_{\rm L} = \omega L,$$

$$X_{\rm C} = \frac{1}{\omega C}.$$
 (Eq. 2.20, Acha)

Para los reactivos del sistema se sabe que:

$$Q_{
m SVC}=Q_k=-V_k^2\,B_{
m SVC}._{ ext{(Eq. 5.5, Acha)}}$$

es decir,

$$Q_k = \frac{-V_k^2}{X_C X_L} \bigg\{ X_L - \frac{X_C}{\pi} \big[2(\pi - \alpha_{\rm SVC}) + \sin(2\alpha_{\rm SVC}) \big] \bigg\}. \tag{Eq. 5.8, Achaelander}$$

```
%% Calculate injected bus powers by the SVC
for kk = 1 : size(SVC_data,1)
   FA=SVC_data{kk,"FA"}*pi/180; % Firing Angle [rads]
   SVC_data{kk,"B"} = (2*(pi-FA) + sin(2*FA))*SVC_data{kk,"Xc"}/pi; %Btcr
   SVC_data{kk,"B"} = (SVC_data{kk,"XL"} - SVC_data{kk,"B"})/(SVC_data{kk,"Xc"}*SVC_data{la}
   Qn(SVC_data{kk,"SVCBus"})=Qn(SVC_data{kk,"SVCBus"})-(Vm(SVC_data{kk,"SVCBus"}))^2*SVC_dend
```

Se obtienen las matrices H,L,N,M donde:

For
$$i \neq j$$

$$H_{ij} = L_{ij} = V_i V_j (G_{ij} \sin \theta_{ij} - B_{ij} \cos \theta_{ij})$$

$$N_{ij} = -M_{ij} = V_i V_j (G_{ij} \cos \theta_{ij} + B_{ij} \sin \theta_{ij})$$
For $i = j$

$$H_{ii} = -Q_i - B_{ii} V_i^2 \quad L_{ii} = Q_i - B_{ii} V_i^2$$

$$N_{ii} = P_i + G_{ii} V_i^2 \quad M_{ii} = P_i - G_{ii} V_i^2$$

(Table 3.1, pag109, Gómez - Exposito)

```
% H Matrix.
            H -> Dim: (nL+nG) X (nL+nG)
for mm = 1 : nL + nG
                         %Iter over rows H matrix
   for nn = 1 : nL + nG
                        %Iter over cols H matrix
       jj = x_{th_n(nn)};
                        % #node corresponding to column nn
       % From Prev Equations:
       if ii == jj
          H(mm,nn) = -Qn(ii) - imag(Ybus(ii,jj)) .* abs(V(ii,k)).^2;
          H(mm,nn) = abs(V(ii,k)) * abs(V(jj,k)) .* (...
              real(Ybus(ii,jj)) * sin( th(ii,k) - th(jj,k) ) - ...
              imag(Ybus(ii,jj)) * cos( th(ii,k) - th(jj,k) ) );
       end
   end
end
```

```
% N Matrix. N -> Dim: (nL+nG) X (nL)
% Iter over cols N matrix
    for nn = 1 : nL
        ii = x th n(mm); % #node corresponding to row mm
        jj = x_v_n(nn);  % #node corresponding to column nn
        % From Prev Equations:
        if ii == jj
           N(mm,nn) = Pn(ii) + real(Ybus(ii,jj)) .* abs(V(ii,k)).^2;
           N(mm,nn) = abs(V(ii,k)) * abs(V(jj,k)) .* (...
               real(Ybus(ii,jj)) * cos(th(ii,k) - th(jj,k)) + ...
               imag(Ybus(ii,jj)) * sin( th(ii,k) - th(jj,k) ) );
        end
    end
 end
% M Matrix. M -> Dim: (nL) X (nL+nG)
 for mm = 1 : nL
                         % Iter over rows M matrix
    % From Prev Equations:
        if ii == jj
           M(mm,nn) = Pn(ii) - real(Ybus(ii,jj)) .* abs(V(ii,k)).^2;
        else
           M(mm,nn) = -abs(V(ii,k)) * abs(V(jj,k)) .* (...
               real(Ybus(ii,jj)) * cos(th(ii,k) - th(jj,k)) + ...
               imag(Ybus(ii,jj)) * sin( th(ii,k) - th(jj,k) ) );
        end
    end
 end
% L Matrix. L -> Dim: (nL) X (nL)
 for mm = 1 : nL
                      % Iter over rows L matrix
    for nn = 1 : nL
                    % Iter over cols L matrix
        ii = x_v_n(mm); % #node corresponding to row mm
        jj = x v n(nn); % #node corresponding to column nn
       % From Prev Equations:
        if ii == jj
           L(mm,nn) = Qn(ii) - imag(Ybus(ii,jj)) .* abs(V(ii,k)).^2;
        else
           L(mm,nn) = abs(V(ii,k)) * abs(V(jj,k)) .* (...
               real(Ybus(ii,jj)) * sin( th(ii,k) - th(jj,k) ) - ...
               imag(Ybus(ii,jj)) * cos( th(ii,k) - th(jj,k) ) );
        end
    end
end
% The jacobian matrix results in:
 J = [H, N; \dots]
    M, L];
```

Se modifican los valores de J en el SVC.

$$\begin{bmatrix} \Delta P_k \\ \Delta Q_k \end{bmatrix}^{(i)} = \begin{bmatrix} 0 & 0 \\ 0 & \frac{2V_k^2}{\pi X_L} [\cos(2\alpha_{\rm SVC}) - 1] \end{bmatrix}^{(i)} \begin{bmatrix} \Delta \theta_k \\ \Delta \alpha_{\rm SVC} \end{bmatrix}^{(i)}.$$
(Eq. 5.9, Acha)

```
%% SVC Jacobian Update
for ii = 1 : size(SVC_data,1)
    DQ_svc_Index= find(N_data(strcmp(N_data.type, 'PQ'),:).n==SVC_data{ii, "SVCBus"});% get F
    DP_svc_Index =find(x_th_n==SVC_data{ii, "SVCBus"});
    if (SVC_data{ii, 'Status'} == 1)
        %Delete the voltage magnitud for the SVC bus
        J(:, nL+nG+DQ svc Index) = 0; %Change DeltaV--->Delta alpha (DeltaV=0 - SVC Con
        FA=SVC_data{ii, "FA"}*pi/180;
              JAC(2*SVCsend(ii)-1,2*SVCsend(ii)-1) = ... % <- DeltaPk/Delta(Vangle)</pre>
%
              JAC(2*SVCsend(ii) - 1,2*SVCsend(ii)-1)-VM(SVCsend(ii))^2*B(ii); %¿Error?
%
        J(DP_svc_Index,DP_svc_Index)=J(DP_svc_Index,DP_svc_Index)-Vm(SVC_data{ii, "SVCBus"})
        % [deltaQk] = [Qk]*[delta(Bsvc)/Bsvc] -- k node= SVCnode
         J(nL+nG+DQ_svc_Index,nL+nG+DQ_svc_Index)=2*Vm(SVC_data{ii, "SVCBus"})^2*(cos(2*FA)
        % [deltaQk]= J(nL+nG+PQ_Index,nL+nG+PQ_Index)
    end
end
```

Se calculan los términos residuales.

$$\Delta P_i = P_i^{\text{sp}} - V_i \sum_{j=1}^n V_j (G_{ij} \cos \theta_{ij} + B_{ij} \sin \theta_{ij}) \quad i = 1, 2, \dots, n-1$$

$$Q_n$$

$$\Delta Q_i = Q_i^{\text{sp}} - V_i \sum_{i=1}^n V_j (G_{ij} \sin \theta_{ij} - B_{ij} \cos \theta_{ij}) \quad i = 1, 2, \dots, n_L$$

```
% ********************* Residual Terms Calculations

% Delta P
Dt_P=P_sp(x_th_n(1:nL+nG))-Pn(x_th_n(1:nL+nG));
% Delta Q
```

Se actualiza la solución del sistema donde:

$$\begin{bmatrix} \theta_{k+1} \\ V_{k+1} \end{bmatrix} = \begin{bmatrix} \theta_{k+1} \\ V_{k+1} \end{bmatrix} + J^{-1} \cdot \begin{bmatrix} \Delta P_k \\ \Delta Q_k \end{bmatrix}$$

$$\alpha_{\rm SVC}^{(i)} = \alpha_{\rm SVC}^{(i-1)} + \Delta \alpha_{\rm SVC}^{(i)}. \label{eq:alphaSVC}$$
 (Eq. 5.10, Acha)

```
SVC Update Adjust
   for ii = 1 : size(SVC data,1)
       if (SVC data{ii, 'Status'} == 1)
          DQ svc Index= find(N data(strcmp(N data.type, 'PQ'),:).n==SVC data{ii, "SVCBus"});% {
          % Adjust the Voltage Magnitud target
          Vm(SVC data{ii, "SVCBus"},k + 1) =SVC data{ii, "Tv"}; %Voltage at SVCnode -> Voltage
          % SVC Susceptance - Delta(Bsvc)
          value = x(nL+nG+DQ svc Index); % delta(alpha)
          %% If high or low delta(FA)
          if (value > 0.5236)
              value = 0.5236;
          elseif (value < -0.5236)</pre>
              value = -0.5236;
          end
          % Update FA
          SVC data{ii, 'FA'}=SVC data{ii, 'FA'}+ value*180/pi;
```

```
V(:,k + 1) = Vm(:,k + 1) .* exp( 1j .* th(:,k + 1) ); % Calculate phasors.

%err = max( abs( V(:,k+1) - V(:,k) ) );
err = max( abs( Dt ) ); % Calculate error

k = k + 1; % Add 1 to iterations
end
```

6) Cálculos finales:

Para el cálculo de la potencia aparente se tiene que:

$$S = \begin{bmatrix} V_1 & 0 & 0 & 0 \\ 0 & V_2 & 0 & 0 \\ 0 & 0 & \ddots & \vdots \\ 0 & 0 & \cdots & V_n \end{bmatrix} \cdot \begin{pmatrix} Y_{\text{Bus}} \cdot \begin{bmatrix} V_1 \\ V_2 \\ \vdots \\ V_n \end{bmatrix} \end{pmatrix}^* = \begin{bmatrix} V_1 & 0 & 0 & 0 \\ 0 & V_2 & 0 & 0 \\ 0 & 0 & \ddots & \vdots \\ 0 & 0 & \cdots & V_n \end{bmatrix} \cdot \begin{pmatrix} \begin{bmatrix} I_1 \\ I_2 \\ \vdots \\ I_n \end{bmatrix} \end{pmatrix}^* = \begin{bmatrix} V_1 & 0 & 0 & 0 \\ 0 & V_2 & 0 & 0 \\ 0 & 0 & \ddots & \vdots \\ 0 & 0 & \cdots & V_n \end{bmatrix} \cdot \begin{pmatrix} \begin{bmatrix} I_1^* \\ I_2^* \\ \vdots \\ I_n^* \end{bmatrix} \end{pmatrix} = \begin{bmatrix} V_1 I_1^* \\ V_2 I_2^* \\ \vdots \\ V_n I_n^* \end{bmatrix} = \begin{bmatrix} S_1 \\ S_2 \\ \vdots \\ S_n \end{bmatrix}$$

```
% Complex power calculation for each node.
Vn = V( : , k );
Vd = diag( Vn );
Sn = Vd * conj( Ybus * V( : , k ) );
Pn = real(Sn);
Qn = imag(Sn);

SGn = Sn + (PL + 1j * QL);
SLn = SGn - Sn;

% Complex Power Flow Through Branches.
```

7) Se presentan los resultados obtenidos

```
%% Results printing.
for i=1:1 % This "for" is used to display everything once.
               *********** \n')
   fprintf('
               ** Newton-Raphson Results ** \n')
   fprintf('
               ******** \n\n')
   fprintf('
   fprintf('-- Number of Iterarions: %d \n', k-1)
   fprintf('-- Error: %6.3e p.u.\n\n', err)
   VarNames = {'Node#', 'Type', 'V p.u.', ' ∠V(°)', 'PG p.u.', 'QG p.u.', 'PL p.u.', 'QL p.u.'};
   fprintf(1,'\t%s\t%s\t%s\t%s\t%s\t%s\t%s\t%s\n', VarNames{:})
   fprintf(1, '-----
                                                      ----\n')
   for ii = 1 : n
      fprintf(' \t%d\t%s\t%6.3f\t%6.3f\t%6.3f\t%6.3f\t\n', ii, char(N_data{i:
          abs(Vn(ii)), angle(Vn(ii)).*180./pi, real(SGn(ii)), imag(SGn(ii)), real(SLn(ii)), :
   end
end
```

array2table(S_pf,'VariableNames',{'FromBus','ToBus','P','Q','S'});

 Table 5.1
 Nodal voltages of modified network

	Network bus						
Nodal voltage	North	South	Lake	Main	Elm		
Magnitude (p.u.)	1.06	1	1	0.994	0.975		
Phase angle (deg)	0	-2.05	-4.83	-5.11	-5.80		

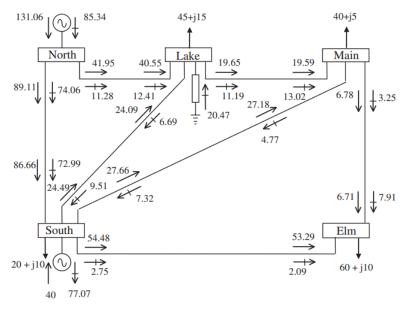


Figure 5.8 Power flow results in the five-bus network with one static VAR compensator

SVC_data

 $SVC_data = 1 \times 9 table$

	SVCBus	Xc	XL	FA	FAmax	FAmin	Tv	Status
1	3	1.0700	0.2880	132.5393	180	90	1	1

Table 5.2 Static *VAR* compensator state variables

	Susceptance model	Firing-angle model			
Iteration	B_{SVC} (p.u.)	B_{SVC} (p.u.)	$\alpha_{\rm SVC}$ (deg)		
1	0.1	0.4798	140		
2	0.1679	0.1038	130.23		
3	0.2047	0.2013	132.47		
4	0.2047	0.2047	132.55		
5	0.2047	0.2047	132.55		

Referencias:

[1] Gomez - Exposito,A. Electrica Energy Systems, Analysis and operation. 2nd Edition. Boca Raton : Taylor & Francis, CRC Press, 2018.

[2] Acha,E. FACTS Modelling and Simulation in Power Networks. 1st Edition. Boca Raton : John Wiley & Sons Inc,2004