

Satellite Communications

**Satellite system to provide communication services  
to polar regions in Europe and Russia**

Ana Reviejo Jiménez  
Marta Munilla Díez  
Oscar Pla Terrada  
Davide Peron  
Cristina Gava  
Javier Garcia Camin

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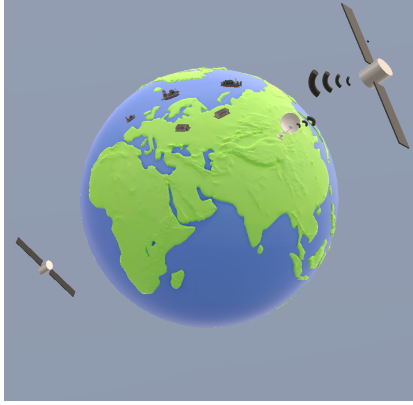


Figure 1: Scheme of the topology of the system.

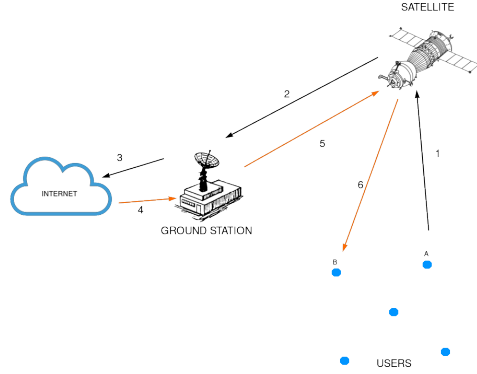


Figure 2: Typical communication path between an user A and an user B.

## 1. Problem Description

This project results from the necessity of having a good broadband coverage of polar areas and the land areas of Northern Europe and Russia: this means the coverage of latitudes over  $60^\circ$ .

The subjects interested in this kind of communication are mostly industries involved in economic sector: they need a reliable communication system able to provide a service of 50 Mbps in download and 5 Mbps in upload.

The aim is to project a system able to provide a continuous, reliable and feasible communication service, maximizing the number of users allowed to access it over  $60^\circ$  latitudes and minimizing the costs. To do that, services in narrowband communication using LEO satellites are not useful, since the broadband communication required is not feasible with this technology.

A simple representation of the system to be built is shown in Figure 1 and a communication between two users is in Figure 2.

Typically, if a user A has to communicate with user B, it sends his packets to the satellite, with the recipient address in the header. The satellite receives the packets and forwards them to the Ground Station that sends them to the proper application (Skype, Hangout, ...). These packets are sent from the application to the Ground Station, that forwards them, through the satellite, to the recipient B.

## 2. Simulator and Orbits

To guarantee the service required in section 1., different orbits have been taken in account. The most used orbit to ensure a stable and reliable satellite communication is Geostationary. Figure 3 has been taken from the Inmarsat's Website, and it shows as a Geostationary Earth Orbit (GEO) satellite can not reach the latitudes over  $75^\circ$ . For this reason a GEO does not fit our purpose.



Figure 3: Approximate coverage of GEO Satellites.

Low Earth Orbits (LEOs) has been discarded since the time of visibility for a single satellite is very low, so an high number of satellites and an accurate tracking system are required to ensure a continuous service.

Medium Earth Orbits (MEOs) suffer the same problems of LEO ones, with the addition of the proximity to the Van Allen Belt where signal degradation increases significantly.

The most suitable solution for our problem is a High Elliptical Orbit (HEO).

## 2.1 Simulator Architecture

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## 2.2 Orbit selection

# 3. Payload and Space Segment

For the space segment a payload a considerations on the transponders have been made based on the requirements that the mission has to satisfy: to be precise, the problem description requires a broadcast communication that guarantees a capacity of 5 Mbit in uplink and of 50 Mbit in downlink; moreover the communication has to allow the internet connection and video and voice call service.

Feature	Value
Transponder size	72 MHz
N carriers in forward link	2
N carriers in return link	6
Amplitude carriers in fw	27.805 MHz
Amplitude carriers in rt	2,732 MHz
Tot. fw link bandwidth	55.61 MHz
Tot. rt link bandwidth	16.39 MHz
Guard-band	3.6 MHz
Tot. bandwidth used	450 MHz

Table 1: Values for the communication module

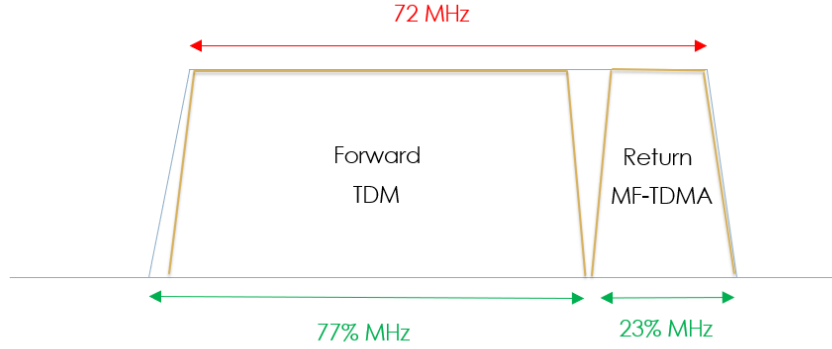


Figure 4: Representation of a transponder

### 3.1 Communication Module

The first thing to do was to select the transponder size, which we fixed at 72 MHz. After that we decided the number of carriers in for the forward and the return link and the amplitude of the guard-band between the carriers. The resulting values are listed in Table 1 and Figure 4 shows a schematic representation of a transponder.

Through these values the total number of transponder we have on the satellite is 12, 6 with horizontal polarization and 6 with the vertical one.

### 3.2 Frequency Plan

After these considerations the structure of the Frequency Plan is automatically elaborated and here it is represented in Figure 5

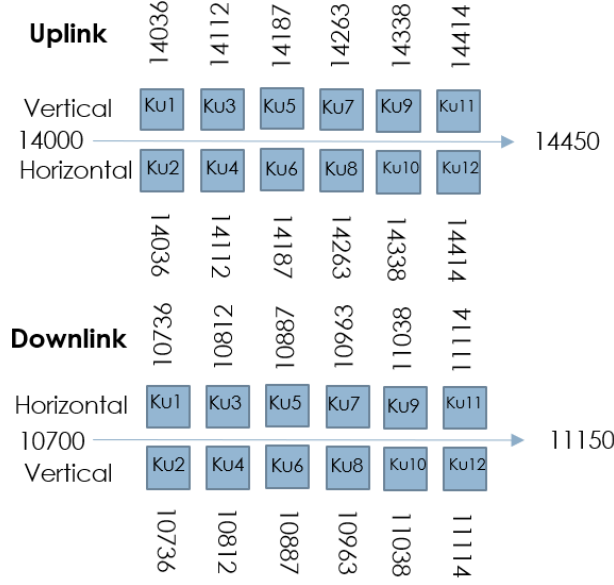


Figure 5: Frequency plan for the communication module

### 3.3 Payload

The electronic part of the payload is composed by the two main sections of the **receiver block** and **repeater block**: in the first part, the signal is received, separated in polarization, filtered and amplified so as to be ready for the repeater part, in which it is channelized and further amplified. Figure 6 shows the global representation of the payload.

#### 3.3.1 Receiver Block

The main actions in which this block is involved are the **polarization separation** and the **frequency conversion**; Figure 7 shows accurately all the fundamental components of this first part.

- (1) is the polarization diplexer, which has the role of separating the received signal depending of its polarization; Figure 7 only shows the path for one possible polarization, but in the complete payload scheme all the components that follow the diplexer have to be doubled up;
- (2) is a low noise amplifier necessary for a first recovering of the received signal; this amplifier is the main element which determines the figure of merit  $G/T$  of the transponder and thus it must have a low noise temperature (in this case is estimated of 438,45 K with a noise figure of 4 dB) and a high gain (in this case of 30 dB) in order to limit the role of the noise of subsequent stages.

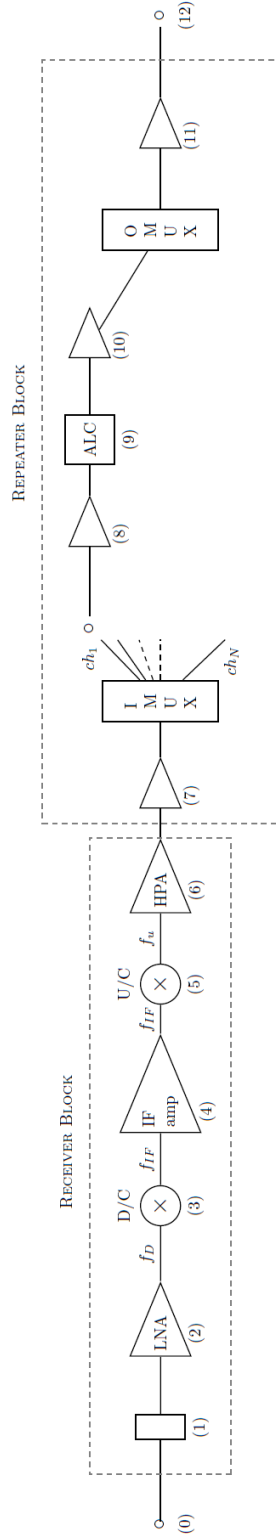


Figure 6: Payload representation

Downlink frequency	Oscillator frequency
$10.95 \leq f_d \leq 11.2$ GHz	1.5 GHz
$11.54 \leq f_d \leq 11.7$ GHz	2.58 GHz
$12.5 \leq f_d \leq 12.75$ GHz	3.8 GHz

Table 2: Oscillator frequency values depending of the Downlink frequency needed for an uplink frequency between 14 and 14.5 GHz

- (3) is the frequency oscillator: its values change with respect to the frequency we need to convert, as shown in Table 2. For the oscillator we have to monitor also other parameters like the conversion losses (normally in the order of 5 - 10 dB, we supposed the worst case of 10 dB and so a noise temperature of 2610 K) and the stability of the frequency [1];
- (4) is the High Power Amplifier (HPA) necessary to amplify the converted signal before being channelized in the repeater section;
- we also have to consider the role of the cables and the losses they bring inside the estimations; in our case we supposed a loss due to the cables of about 3 dB [2] and an associate noise temperature of 288.63 K.

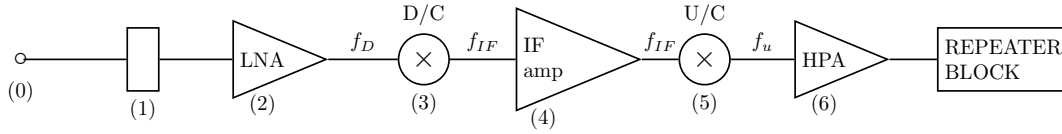


Figure 7: Payload receiver part

For this block the redundancy is of 1/2.

### 3.3.2 Repeater Block

In the repeater block the channelization part is present and, for that, the input/output multiplexers are needed. We selected 2 input and 2 output multiplexers, each one having 3 channels in order to have one channel per carrier received<sup>1</sup>. Inside the multiplexers the main elements are the band-pass filters and the circulators used to separate the frequency channels, these ones are the main cause of losses inside the multiplexers since they depend on the number of times the signal concerned passes through a circulator (the loss is in the order of 0.1 dB). [1]

In addition to this, for each channel of the multiplexers we then have:

<sup>1</sup>we remember that the path described here is still referring to one single polarization. At the end of the description, all the elements described have to be doubled up in number



- (8), a channel amplifier;
- (9), an Automatic Level Control module: a device needed to guarantee a constant power value as input of (10);
- (10), the amplifier module, composed by the EPS and the TWT sections which together form the Travelling Wave Tube Amplifier (TWTA). The output power value that we supposed for the TWTA section is 20W [1].

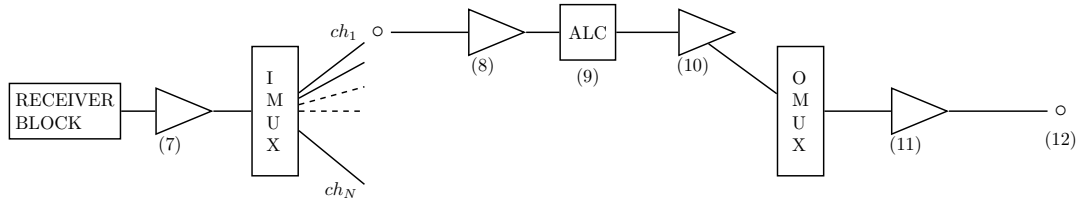


Figure 8: Payload repeater part

For this block the redundancy is a 8/12 redundancy ring.

### 3.4 Power Budget

The power budget mainly depends on the power required by the TWTA amplifiers in order to transmit the signal to the Earth. As can be seen from the chart in Figure 9, the fraction of power that the communication subsystem requires is about 75 %, all the other utilities uniformly share the remaining power needed [3].

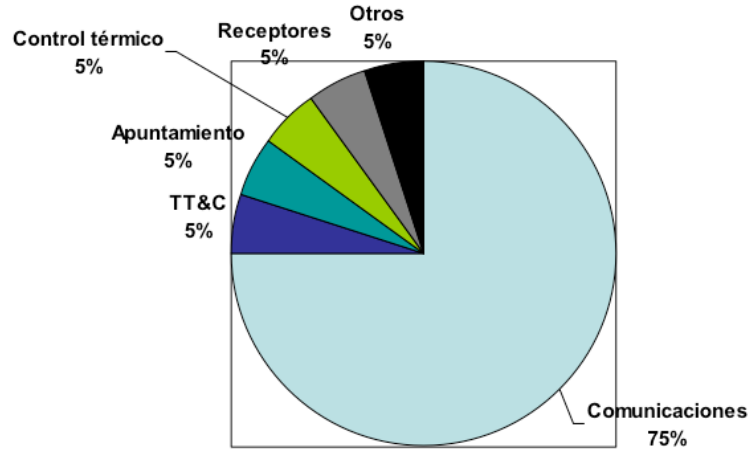


Figure 9: Power distribution among the subsystems in percentage

### 3.4.1 Required Power

To estimate the required power we supposed to be in the worst case (end of life of the satellite) and followed the steps below:

- Estimate the End Of Life (EOL) efficiency for the solar panel;
- Estimate the EOL efficiency for the TWTA module;
- Estimate the EOL efficiency for the EPC module;
- Estimate the total power required for the transponders;
- Estimate the total power required for the system;

**Solar panel efficiency** Given an expected life of 15 years, a degrading coefficient  $\frac{1}{\tau}$  of 0.043 1/s and an initial efficiency of 17 % [3], the EOL solar panel efficiency is:

$$\eta_{SP_{EOL}} = \eta_{BOL} e^{-0.043T} \rightarrow \eta_{SP_{EOL}} = \frac{17}{100} e^{-0.043 \times 15} = 8.9\% \quad (3.1)$$

**TWT efficiency** The same expression can be used to estimate the EOL efficiency for the TWTA, supposing a  $\eta_{TW_{BOL}} = 60\%$ : in particular, if we suppose that the efficiency value will be reduced of 10% after 10 years (6% of decrement) [3], we can find the degradation coefficient  $\frac{1}{\tau}$  as:

$$60\% - 6\% = 60\% e^{\frac{-10}{\tau}} \rightarrow \tau = \frac{-10}{\log_e \frac{54}{60}} = 94.91 \quad s^{-1} \quad (3.2)$$

and so the EOL efficiency:

$$\eta_{TW_{EOL}} = 60 e^{\frac{-15}{94.91}} = 51.23\% \quad (3.3)$$

**EPC efficiency** Through the same procedure we obtain also the efficiency for the EPC segment:

$$\eta_{EPC_{EOL}} = 81.2\% \quad (3.4)$$

**Total power required for the transponders** With all the efficiency values previously found we can now estimate the total power used by the satellite in the worst case, supposing an output power at saturation for the TWT module of 250 W:

$$P_{in_{TW}} = \frac{P_{out_{TW}}}{\eta_{TW_{EOL}}} = 195.198 \text{ W} \quad (3.5)$$

$$P_{in_{EPC}} = \frac{P_{in_{TW}}}{\eta_{EPC_{EOL}}} = 240.39 \text{ W} \quad (3.6)$$

$$P_{transp} = P_{in_{EPC}} \times N_{transp} = 240.39 \times 12 = 2.885 \text{ kW} \quad (3.7)$$

$$(3.8)$$

Moreover, since this power consists in the 75% of the total power necessary for the satellite, the total power for the satellite is:

$$P_{tot} = \frac{P_{transp}}{75\%} = 3.846 \text{ kW} \quad (3.9)$$

### 3.4.2 Solar Panels specifications

Once we have found the total power that the satellite needs at the worst case, the estimation of the area for the solar panels is made deploying the following expression [?]:

$$A_{panel} = \frac{P_{tot}s}{f\Phi\eta_{SP_{EOL}}s(1-l)} \quad (3.10)$$

Where:

- $s$  is the area of a single cell;
- $\Phi$  is the solar flux, supposed to be of  $1215,74 \text{ W/m}^2$  in the farthest point of the satellite orbit (based on the observation of Figure 10);
- $f$  is the filling efficiency, here of the order of 90 %;
- $l$  are general losses due to cabling and cover and typical values are 10 to 15 % (here we selected 15 % for a worst-case analysis);

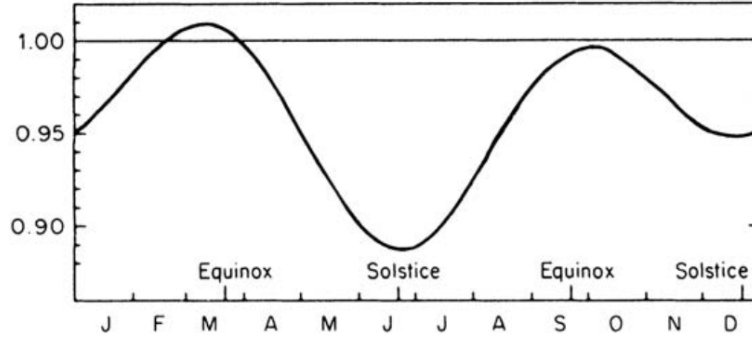


Figure 10: Combined influence of sun declination and distance variation

And from it the final value for the solar panel area of our satellite is:

$$A = 46.46 \text{ m}^2 \quad (3.11)$$

### 3.5 Weight Estimation

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## 4. Ground Segment

The ground segment is composed by a single Ground Station (GS) and all the mobile users moving around on the northern lands and seas of Russia and Europe. The reason for just one GS is that, since we do not deploy the multibeam option, there is no necessity of having more than one GS, because one is enough to correctly collect all the traffic coming from the satellite and toward it.

### 4.1 Ground Station coordinates

The coordinates of the GS are: (Cri says: Cambia valore quando Davide ha trovato un buon posto per la GS)

$$lat = 61.267865 \quad (4.12)$$

$$long = -96.608223 \quad (4.13)$$

$$(4.14)$$

These coordinates have been chosen based on the elevation values: the coordinates listed above represent a point in Russia in the surrounding area of the subsatellite point of the apogee. In this way, the values of elevation are always substantially high, guaranteeing always a good visibility. Moreover, another factor is the rain attenuation, which is not much high in this region, as we can conclude from the respective value of  $R$ : (Cri says: Cambia valore quando Davide ha trovato un buon posto per la GS)

$$R = 22.2016 \text{ mm/h} \quad (4.15)$$

### 4.2 Ground Station requirements

The requirements for the GS are substantially the following:

- the Internet connection;
- the antenna model and specifications.

The Internet connection is the most important (if not the only one) reason for the existence of the GS, since one of the problem requirements is indeed the possibility of video calls and other internet services.

For the antenna model we chose a reflector antenna with a single circular beam; the antenna parameters are listed in Table 3

(Cri says: la metto sta frase qui? a suo tempo il prof mi pare avesse detto che andava specificato, però a leggerla mi rattristo a pensare che offriamo un servizio che per 2 minuti al giorno sistematicamente non funziona)

Parameter	Value
Frequency Band	Ku Band
Dish diameter D	6 m
Efficiency	0.6
IBO	-0.5 (Cri says: può essere considerato un parametro d'antenna?)

Table 3: GS antenna specifications

### 4.3 User requirements

The user requirements are substantially the model of the antenna and the dimension of the dish: the model is identical to the ones used for the satellite and the GS, so a reflector antenna with a single beam; the dish diameter is smaller in this case, for a matter of space and feasibility, and is of 1 m (Cri says: verifica valore). There is no need, in this case, of specifying the position of the users since by definition they are mobile users.

## 5. Link Budget

### 5.1 Parameters setting and estimation

#### 5.1.1 Antenna Parameters

#### 5.1.2 Effective Isotropic Radiated Power(EIRP)

#### 5.1.3 Losses

### 5.2 Uplink

### 5.3 Downlink

The Downlink link budget is calculated as in Equation 5.16.

$$\left(\frac{C}{N}\right)_U = EIRP_{down} - OBO - L_D + \left(\frac{G}{T}\right)_{user} - [k]_{dB} - B_{IF} \quad (5.16)$$

and

$$L_D = L_{PL} + L_{rain} + L_{pointing} + L_{gas}$$

In that equation  $EIRP_{down}$  is the Emitted Isotropic Radiated Power (EIRP) trasmitted by the gateway and  $(G/T)_{sat}$  is the *Gain-over-Temperature* ratio of the user.  $k$  and  $B_{IF}$  remain the same values we also used for the Uplink link budget, while  $L_D$  now represents the losses in the downlink segment.

$(G/T)_{user}$  is computed as the difference (in dB) between the gain of the receiving antenna and the ground station system temperature  $T_{gs}$ , as it was for the Uplink case, but this time the Friis formula involves a different antenna temperature. In fact now we are dealing with the user station antenna and this is the reason of the element  $T_A^{USER}$  in

Equation 5.17. The formula brings to a user station temperature value of  $T_{gs} = 523.94K$  and a corresponding value for the user figure of merit of  $\left(\frac{G}{T}\right)_{user} = 11.91 \text{ dB}$

$$T_{gs} = T_A^{USER} + t_{LNA} + \frac{T_{CABLE}}{G_{LNA}} + \frac{T_{DC}}{G_{LNA} \cdot G_{CABLE}} \quad (5.17)$$

## 5.4 Overall Link Budget

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## 6. Cost Estimation

### 6.1 Spacecraft cost

The spacecraft cost can be estimated depending on several parameters and criteria, such as the type of mission, the subsystem considered and the unit over which calculate the cost. In our specific case we concentrated on the cost analysis for a communication-type satellite and review it for every subsystem of the spacecraft and its launch procedure.

The subsystems analyzed are the following:

- Attitude determination and Control subsystem (ADCS)
- Communication subsystem
- Electrical power subsystem (EPS)
- Integration assembly and test (IA&T)
- Passive sensor
- Propulsion
- System engineering
- Structure
- Thermal control

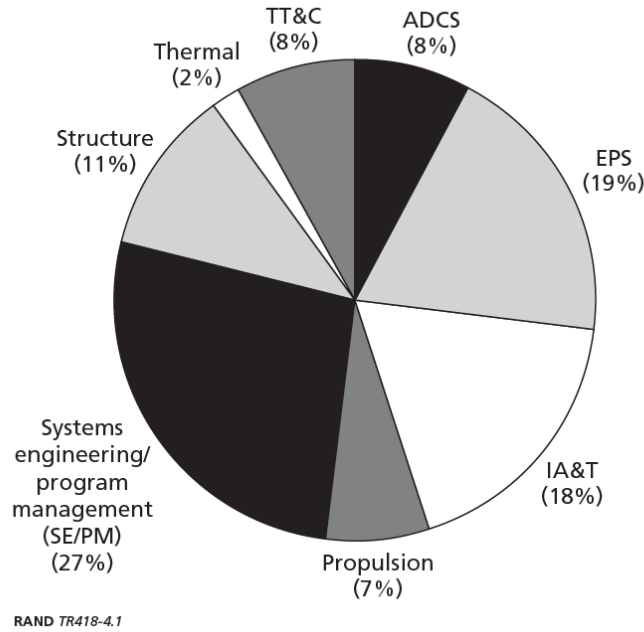


Figure 11: Communication spacecraft cost composition

- Telemetry tracking and command (TT&C)

In particular, Figure 11 shows the cost percentage that each system represents: from it we can see that the System engineering is the most important item, followed by the EPS and the IA&T subsystems. Moreover, Figure 12 lists the different sections, depending on the type of mission the satellite is intended to accomplish, with their standard deviations; tables 13 and 14, instead, show the total cost depending on the mission type and the total cost per pound [4].

Regarding the cost per subsystem, Table 4 and Table 5 show the different cost each subsystem is intended to have:

Through this data we can make a raw hypothesis on the average total cost of the spacecraft with a summary estimation of its mass:

## 6.2 Launch cost

For the launch cost we based our considerations on the prices listed by the *SpaceX* company. Figure 15 shows the prices for different types of launches, depending on the mass of the spacecrafts and the orbits they should reach [5].

Through the considerations we have made in the previous sections we can state that around 180 Millions of dollars (151.793.055 €(**Cri says: verifica il prezzo**)) are needed for the launch: in fact each spacecraft has a total mass of about (**Cri says: mettere massa**) and the Molniya orbit is a HEO orbit; moreover, since the raans of the two

Cost	Average (%) (standard deviation)							
	ADCS	EPS	IA&T	Prop	SE/PM	Structural	Thermal	TT&C
Communication	8.0 (2.2)	19.1 (7.9)	18.0 (8.6)	6.6 (3.3)	26.8 (9.2)	11.2 (6.7)	2.3 (1.4)	8.0 (3.5)
Environmental	19.8 (6.1)	15.6 (4.2)	15.6 (9.0)	4.1 (1.9)	24.9 (6.8)	5.4 (2.4)	1.4 (0.7)	13.2 (4.3)
Navigation	13.6 (2.4)	21.0 (3.2)	16.9 (4.2)	7.7 (1.5)	20.0 (7.9)	7.6 (5.4)	3.1 (0.3)	10.1 (3.6)
Scientific/survey	11.4 (1.4)	12.3 (7.8)	22.2 (13.0)	3.6 (4.5)	25.0 (8.8)	8.2 (3.7)	1.9 (0.9)	15.4 (18.2)
Experimental	9.6 (4.8)	12.0 (2.2)	13.9 (4.6)	8.0 (9.3)	23.3 (7.3)	10.0 (5.5)	1.4 (2.6)	22.0 (4.5)
Communication/ navigation/ environmental	12.0 (6.4)	18.3 (6.8)	17.2 (8.2)	6.0 (3.0)	25.5 (8.5)	9.2 (6.1)	2.1 (1.2)	9.8 (4.3)

Figure 12: Communication spacecraft cost composition: averages and standard deviations

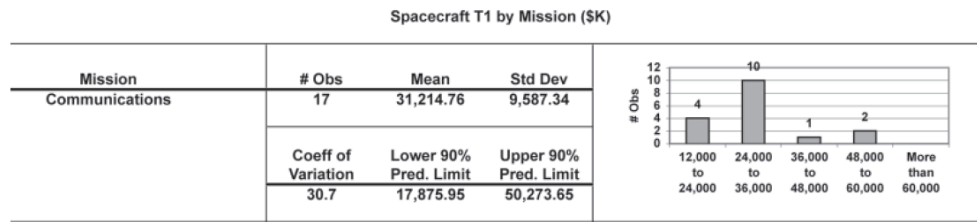


Figure 13: Total spacecraft cost

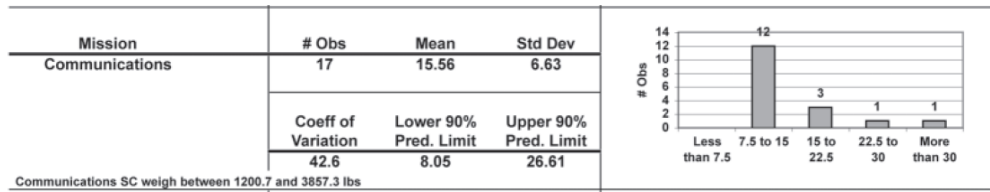


Figure 14: Total spacecraft cost per pound

Subsystem	Mean Cost (k€)	Standard deviation
IA&T	8311,49	8719,94
EPS	8441,34	5681,80
Structure	4111,49	2955,92
SEPM	12167,05	7825,63
Thermal	903,45	562,3
TT&C	4423,24	2942,24

Table 4: List of the costs per subsystem



Subsystem	Mean Cost/unit (k€/kg or ch)	Standard deviation
ADCS	94,70	8719,94
Communication ( $1 < ch < 10$ )	3923,19	1443,98
Communication ( $10 < ch < 25$ )	1534,45	558,37
Communication ( $25 < ch$ )	708,40	197,35
EPS	24,7	7,27
Propulsion	54,68	14,32
Structure	15,94	4,37

Table 5: List of the costs per subsystem per pound/channel

Communication spacecraft			
IA&T	8311,49 €	+	
EPS	24,7 €/Kg	$\times NCHILI$	+
Structure	15,94 €/Kg	$\times NCHILI$	+
SEPM	12167,05 €	+	
Thermal	903,45 €	+	
TT&C	4423,24 €	+	
ADCS	94,70 €/Kg	$\times NCHILI$	+
Propulsion	54,68 €/Kg	$\times NCHILI$	+
Communication ( $10 < ch < 25$ )	1534,45 €/ch	$\times 12ch$	=
Total cost:		TOT	

Table 6: List of the costs per subsystem per pound/channel

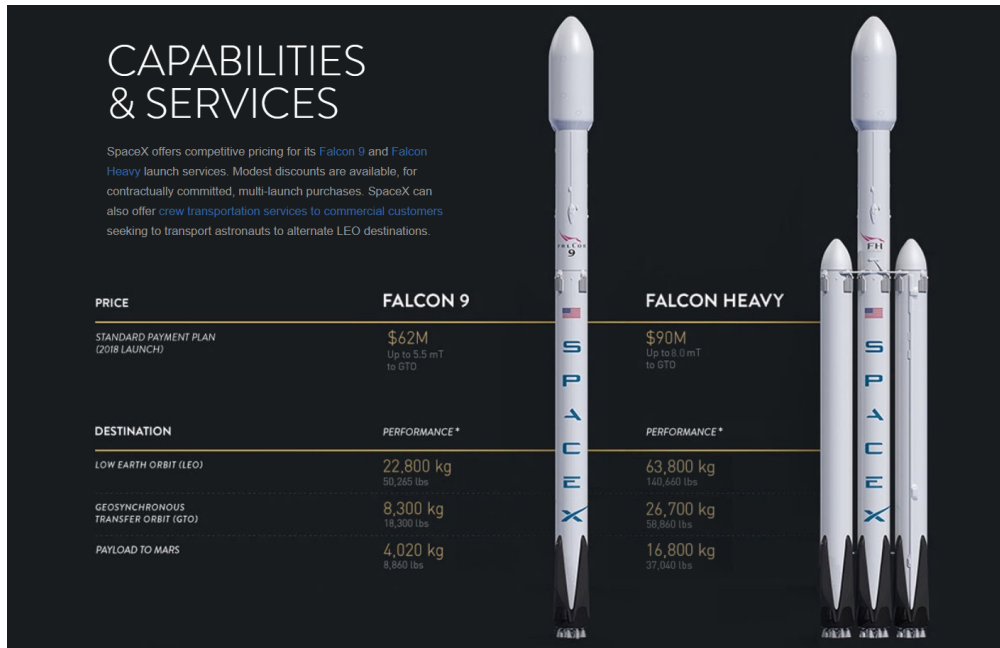


Figure 15: *SpaceX* price list

orbital planes are separated of 180 deg it is necessary to use two separate launchers, one for each spacecraft.

Through this analysis the total cost for the project is:

$$Cost_{Total} = Cost_{Launch} + Cost_{Spacecraft} = \text{(Cri says: Mettere costo finale)}\text{€} \quad (6.18)$$

## 7. Final considerations and conclusions

With this work we intended to present a communication system aimed to service the polar regions over Europe and Russia. From the previous sections the values and parameters found permitted us to establish the reliability and the feasibility of our system in terms of cost and weight. From our calculations we obtained a relatively simple system which needs 2 satellites and one ground station to supply our purpose and guarantees continuous coverage of the interested zones, moreover the link budget analysis provides us satisfactory values for the communication link, at the same time requiring a not so power-costly technology (see the modulation choice or the power for the HPA based on worst case analysis). Finally, the cost analysis outlines a project which could represent a typical market solution, even though the one presented here is just a first proposal and it could be refined with more time and a comparison to other approaches.

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