



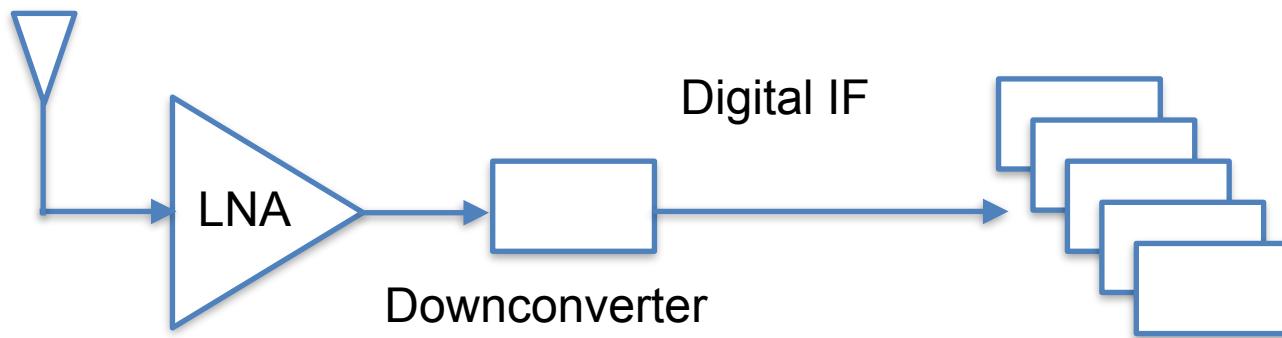
GNSS Receiver Design:

- Receiver Block diagram
- RF Frontend
- Link Budget
- Signal Tracking
- Multipath
- Signal Acquisition



Receiver Block Diagram

Antenna



RF frontend

Tracking channels



$$P_T = 27 \text{ W} = 44.3 \text{ dBm}$$

$$G_T = 10.2 - 12.3 \text{ dB}$$

$$EIRP = 240 - 470 \text{ W}$$

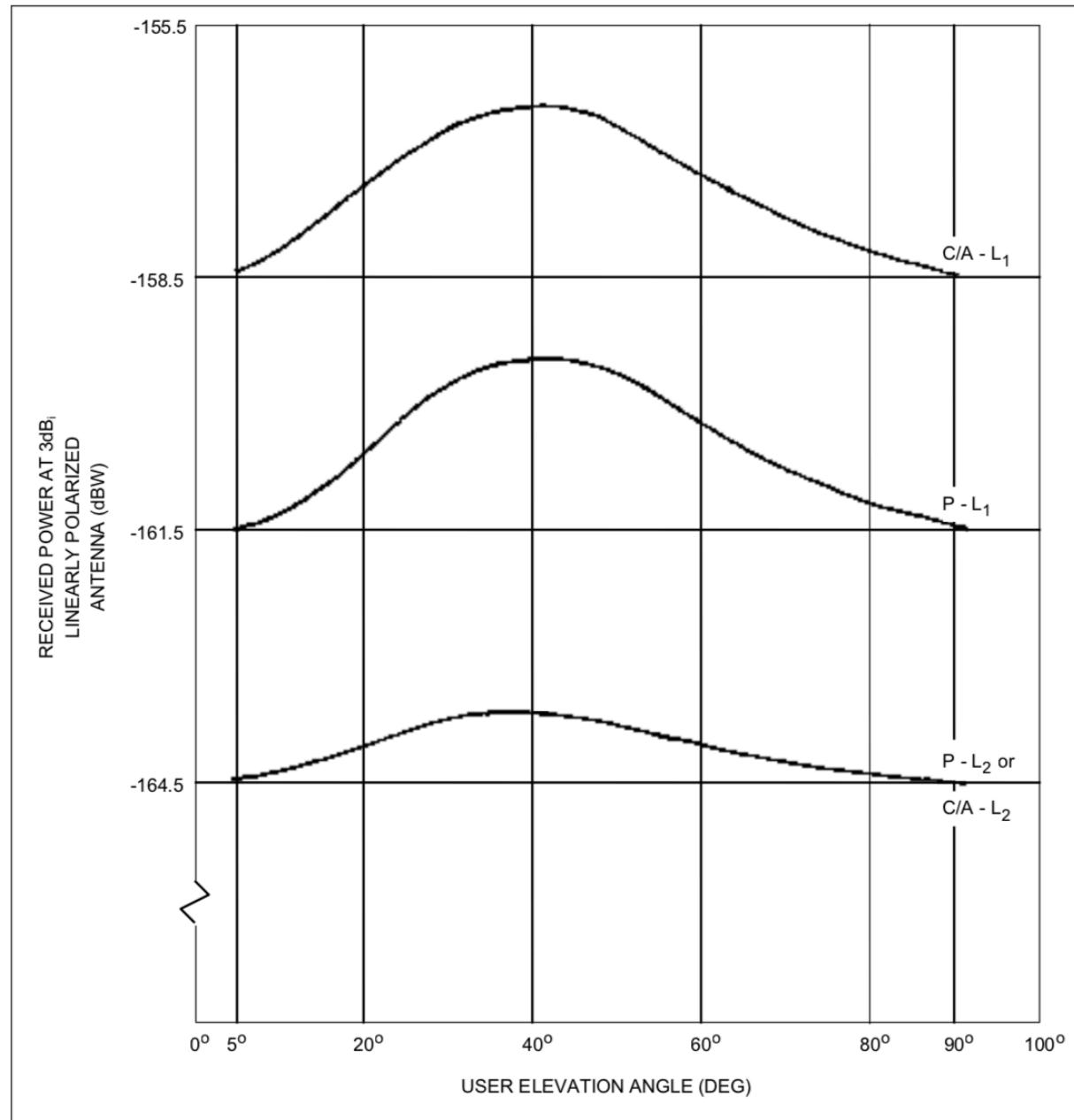
$$PL = 157 \text{ dB}$$

$$P_R = P_T + G_T + G_R - PL = 1.41 \cdot 10^{-16} \text{ W} = -128.5 \text{ dBm}$$



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Antenna Gain





$$N_0 = kT_{eq} \text{ [W/Hz]}$$

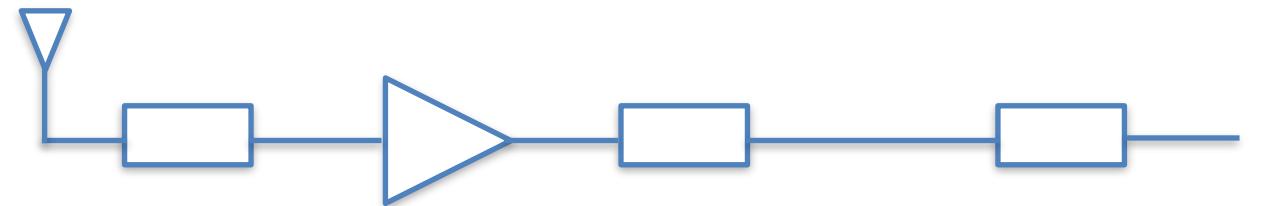
$$k = 1.38 \cdot 10^{-23} \text{ J/K}$$

$$N = N_0 B_n \text{ [W]}$$

Friis Formula

$$T_{eff} = T_a + (F_1 - 1)T + \frac{(F_2 - 1)T}{G_1} + \frac{(F_3 - 1)T}{G_1 G_2} + \frac{(F_4 - 1)T}{G_1 G_2 G_3}$$

Antenna T_a



Cable + Filter

$$G_1 = 1/F_1$$

LNA

$$G_2, F_2$$

Cable + Filter

$$G_3 = 1/F_3$$

Downconverter

$$G_4, F_4$$



$$N_0 = kT_{eq} \text{ [W/Hz]}$$

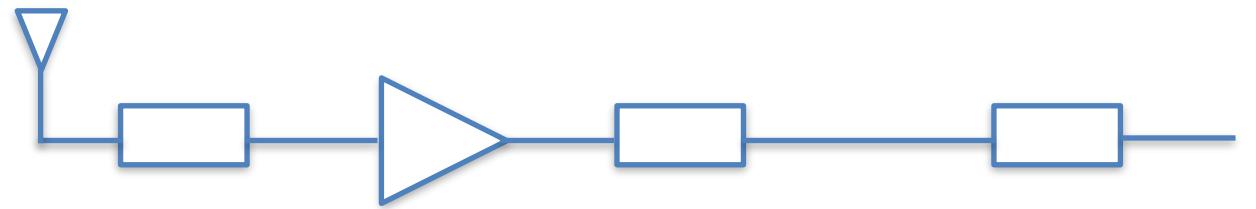
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Antenna T_a



Cable + Filter

$$G_1 = 1/F_1$$

LNA

$$G_2, F_2$$

Cable + Filter

$$G_3 = 1/F_3$$

Downconverter

$$G_4, F_4$$

$$T_a = 130 \text{ K}$$

$$G_2 = 25 \text{ dB}$$

$$T_{eff} = 296.4 \text{ K}$$

$$T = 290 \text{ K}$$

$$F_2 = 1.9 \text{ dB}$$

$$N_0 = -203.9 \text{ dBW-Hz}$$



Carrier to Noise Density Ratio

$$C/N_0 = [\text{W}] / [\text{W/Hz}] = [\text{Hz}]$$

$$10 \log_{10} C/N_0 = [\text{dB-Hz}]$$

$$C/N = \frac{C}{N_0 B_n}, \quad B_n = \text{bandwidth [Hz]}$$

$$C = -158.5 \text{ dBW}$$

$$C/N_0 = -158.5 - (-203.9) = 45.4 \text{ dBW-Hz}$$

$$B_n = 10 \text{ MHz}$$

$$SNR = 45.4 - 70 = -25.4 \text{ dB}$$



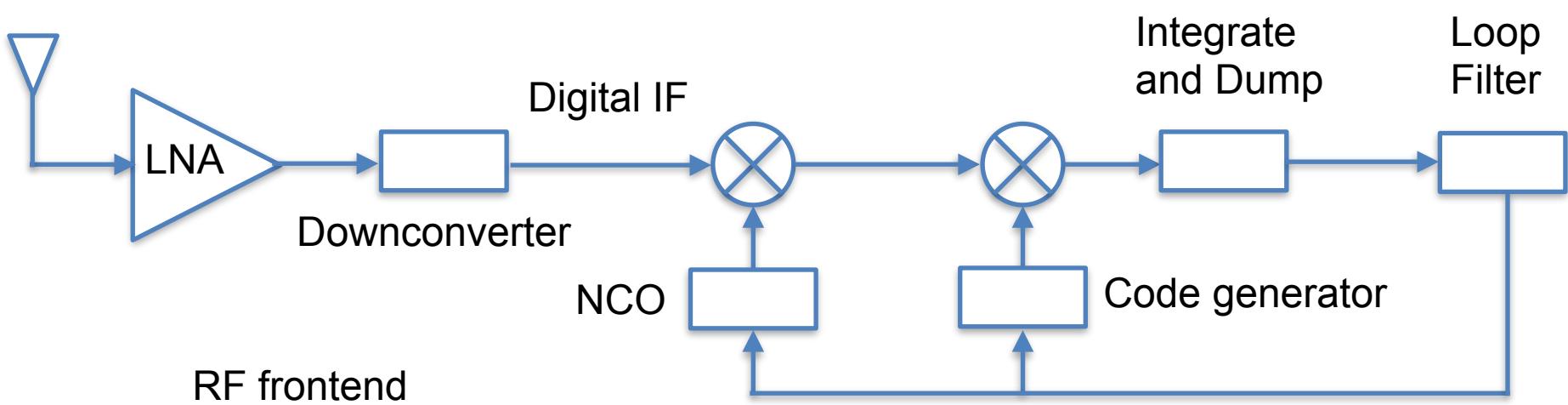
Quantization Loss

Bit number	Optimal AGC Gain	Minimum Loss (dB)
1		−1.96
2	$1/\sigma_{IF}$	−0.55 dB
3	$1.71/\sigma_{IF}$	−0.165 dB
4	$2.98/\sigma_{IF}$	−0.05 dB
5	$5.315/\sigma_{IF}$	−0.015 dB



Receiver block diagram

Antenna





$$I = \frac{A}{\sqrt{2}} \cdot T_{pdi} \cdot D \cdot R(\delta\hat{t}) \cdot \text{sinc}(\delta\hat{f}T_{pdi}) \cdot \cos(\delta\hat{\phi}) + \eta_I$$

$$Q = \frac{A}{\sqrt{2}} \cdot T_{pdi} \cdot D \cdot R(\delta\hat{t}) \cdot \text{sinc}(\delta\hat{f}T_{pdi}) \cdot \sin(\delta\hat{\phi}) + \eta_Q$$

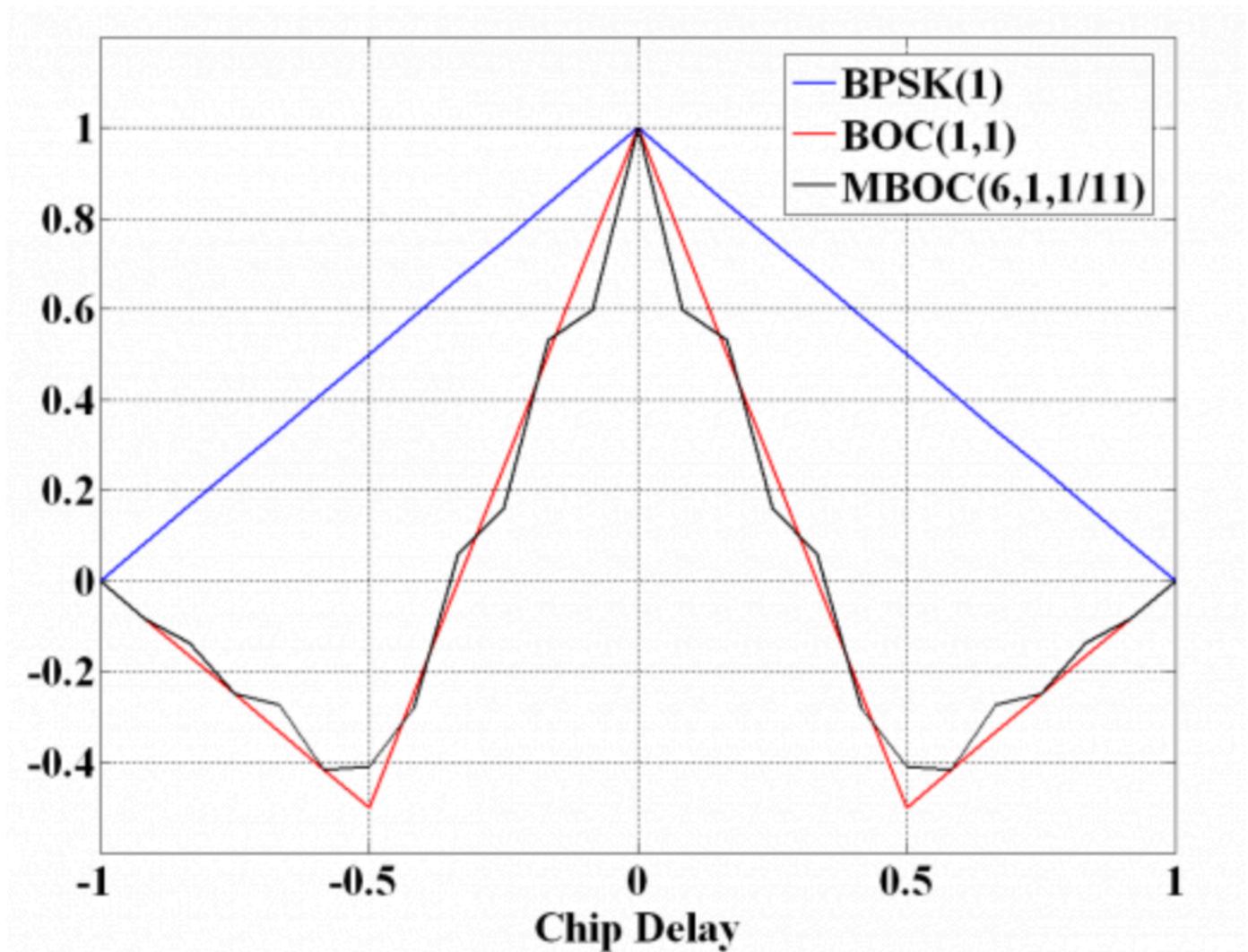
$$\mathbb{E}[\eta_i] = \mathbb{E}[\eta_Q] = 0$$

$$\mathbb{E}[\eta_i^2] = \mathbb{E}[\eta_Q^2] = N\sigma_n^2$$



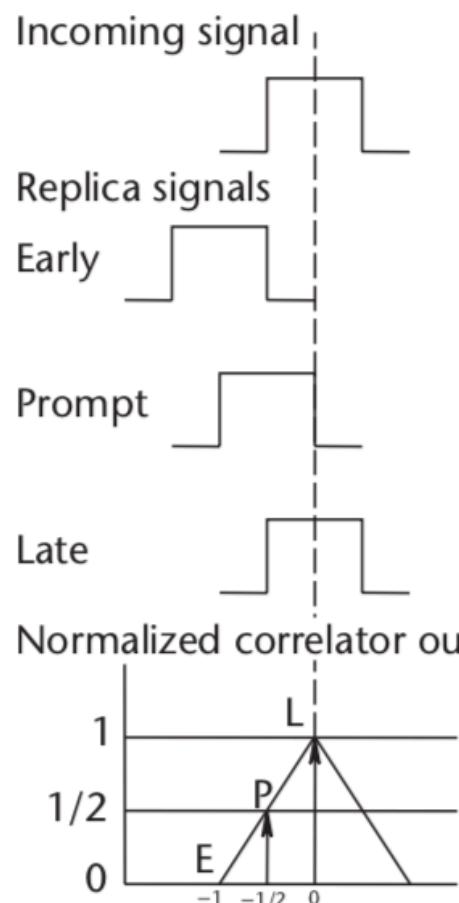
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Auto Correlation Function

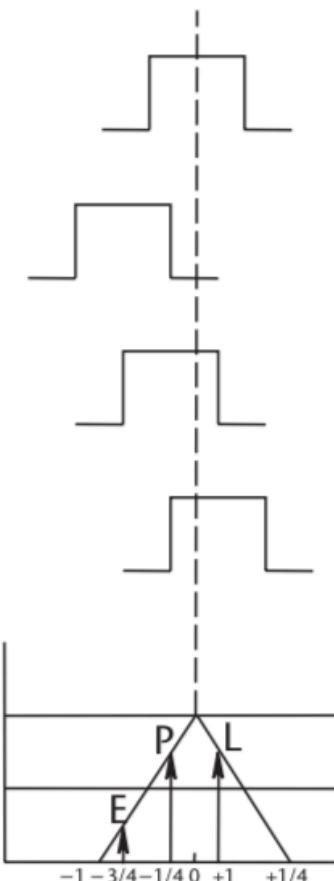




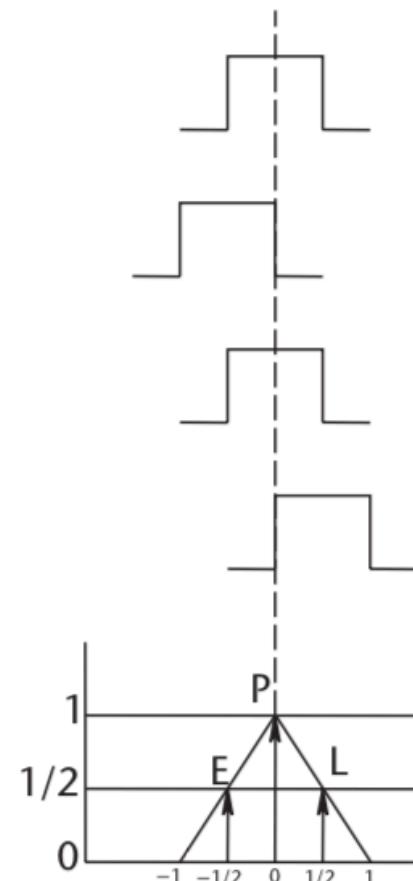
Delay Locked Loop



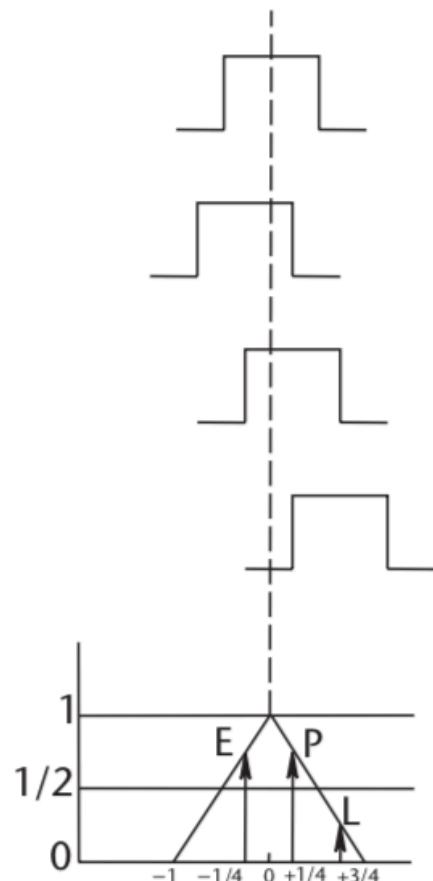
(a)



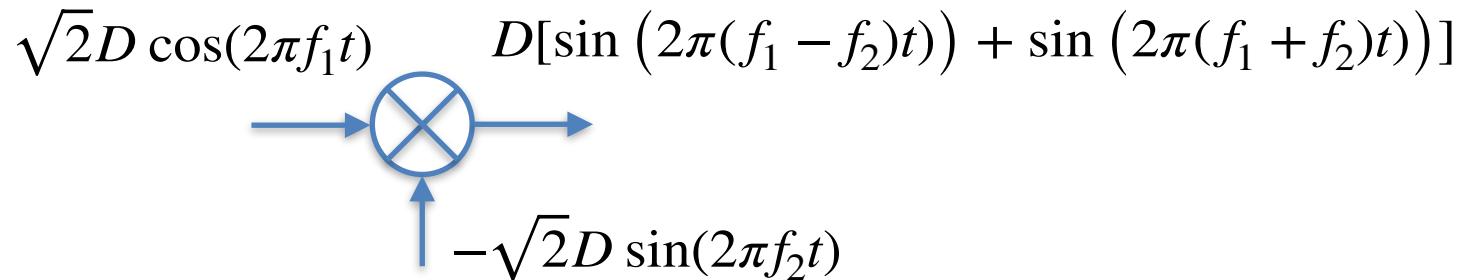
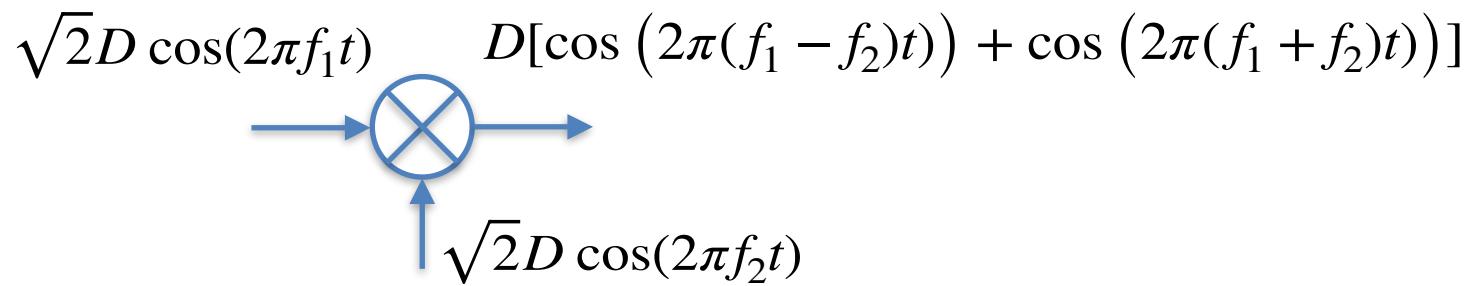
(b)



(c)



(d)

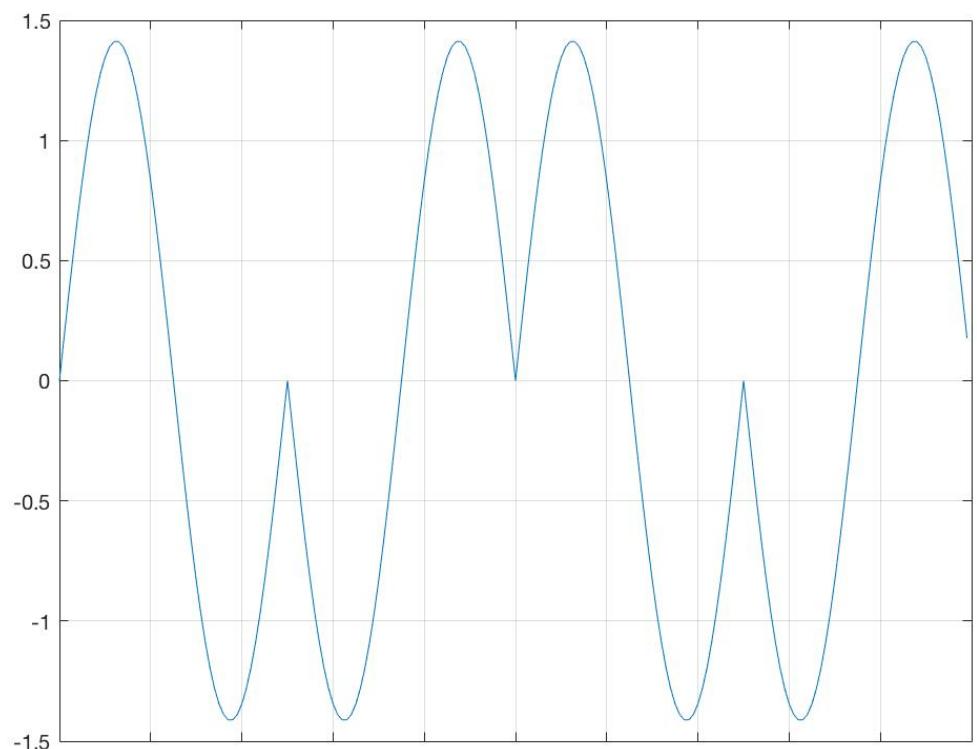




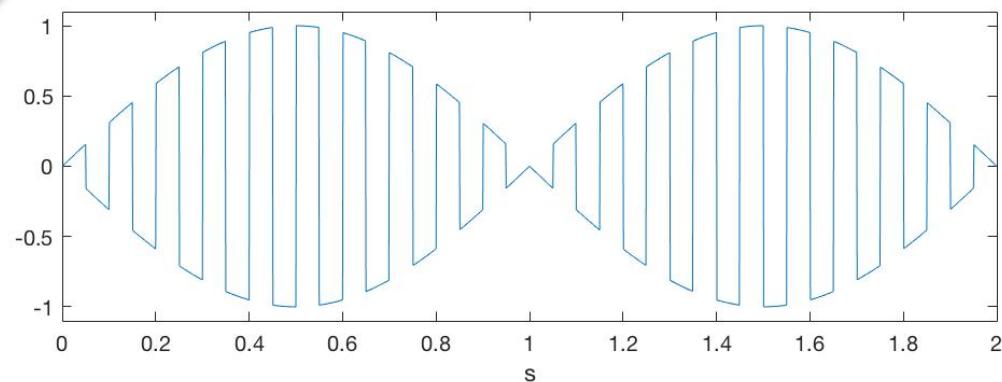
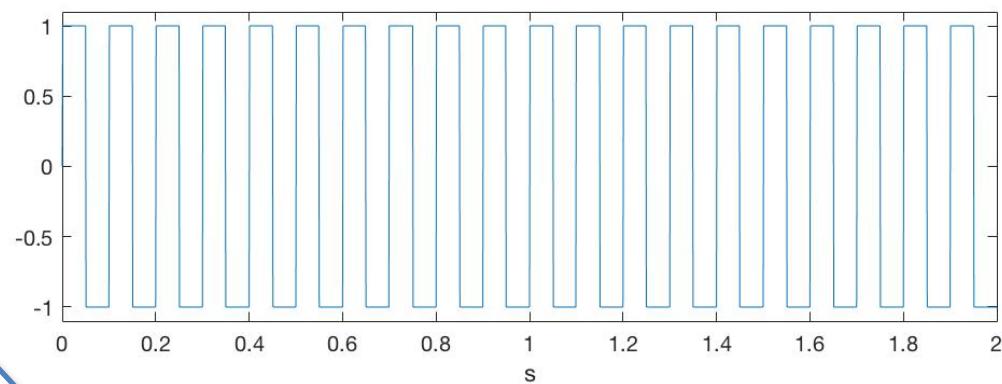
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Doppler Residual Error

Received signal



Perfect carrier wipe-off



Carrier wipe-off with
residual 0.5 Hz error



Carrier Tracking Loops

Frequency Locked Loop (FLL)

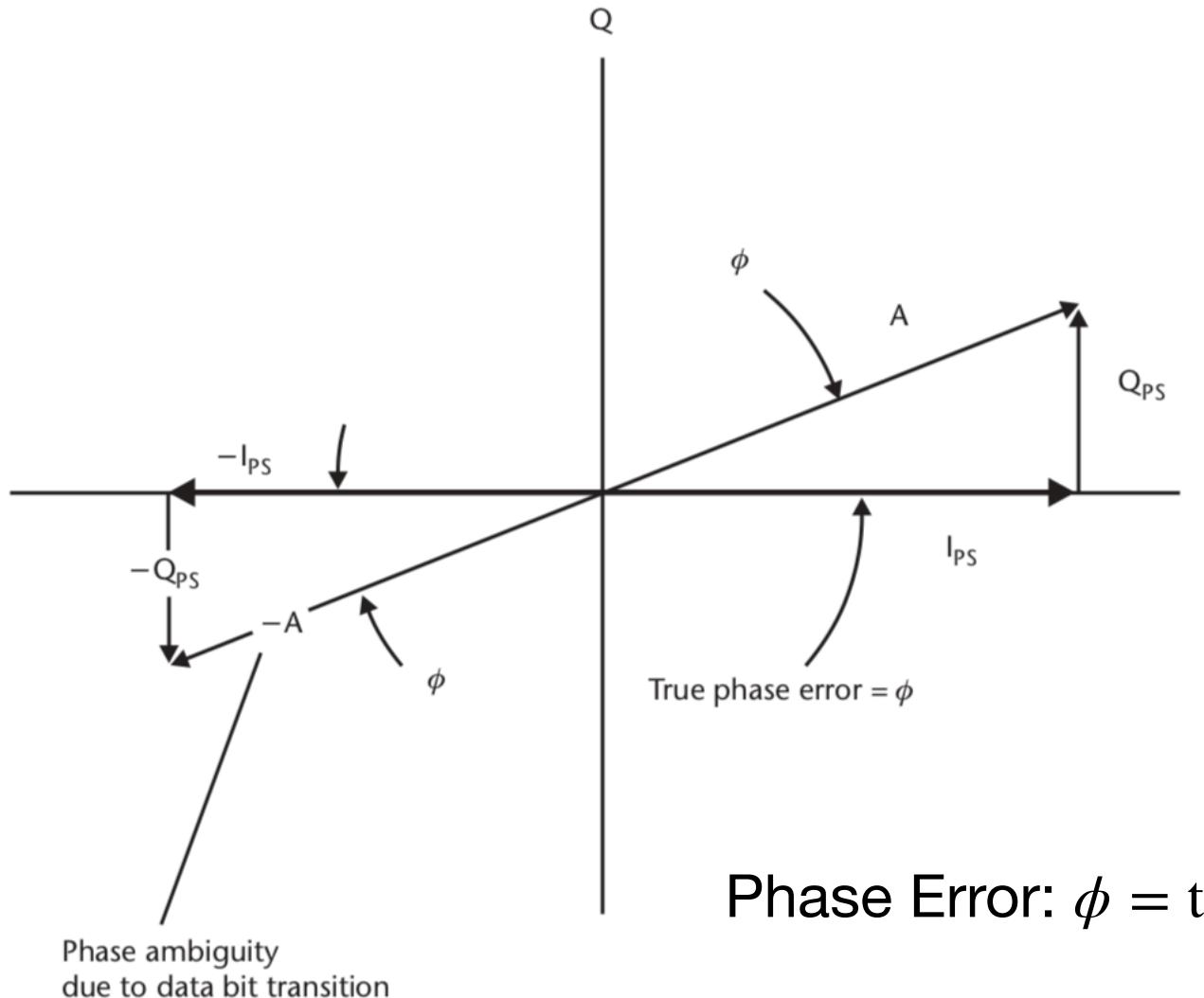
- Attempts to drive the incoming-minus-replica frequency residual to zero
- Phase is allowed to wander
- More robust than a phase-locked loop
- Produces ambiguous range measurements with decimeter-level noise

Phase Locked Loop (PLL)

- Attempts to drive the incoming-minus-replica phase residual to zero
 Incoming and replica phases are aligned
- Sensitive to dynamic stresses
- Produces ambiguous range measurements with millimeter-level noise



Phase Locked Loop



$$\text{Phase Error: } \phi = \tan^{-1} \left(\frac{Q}{I} \right)$$

$$\text{Lock Indicator: } P = I^2 + Q^2$$



Wideband Power (WBP): $WBP_m = \sum_{i=1}^M (I_i^2 + Q_i^2)$

Narrowband Power (NBP): $NBP_m = \left(\sum_{i=1}^M I_i^2 \right) + \left(\sum_{i=1}^M Q_i^2 \right)$

Normalized Power (NP): $NP_m = \frac{NBP_m}{WBP_m}$

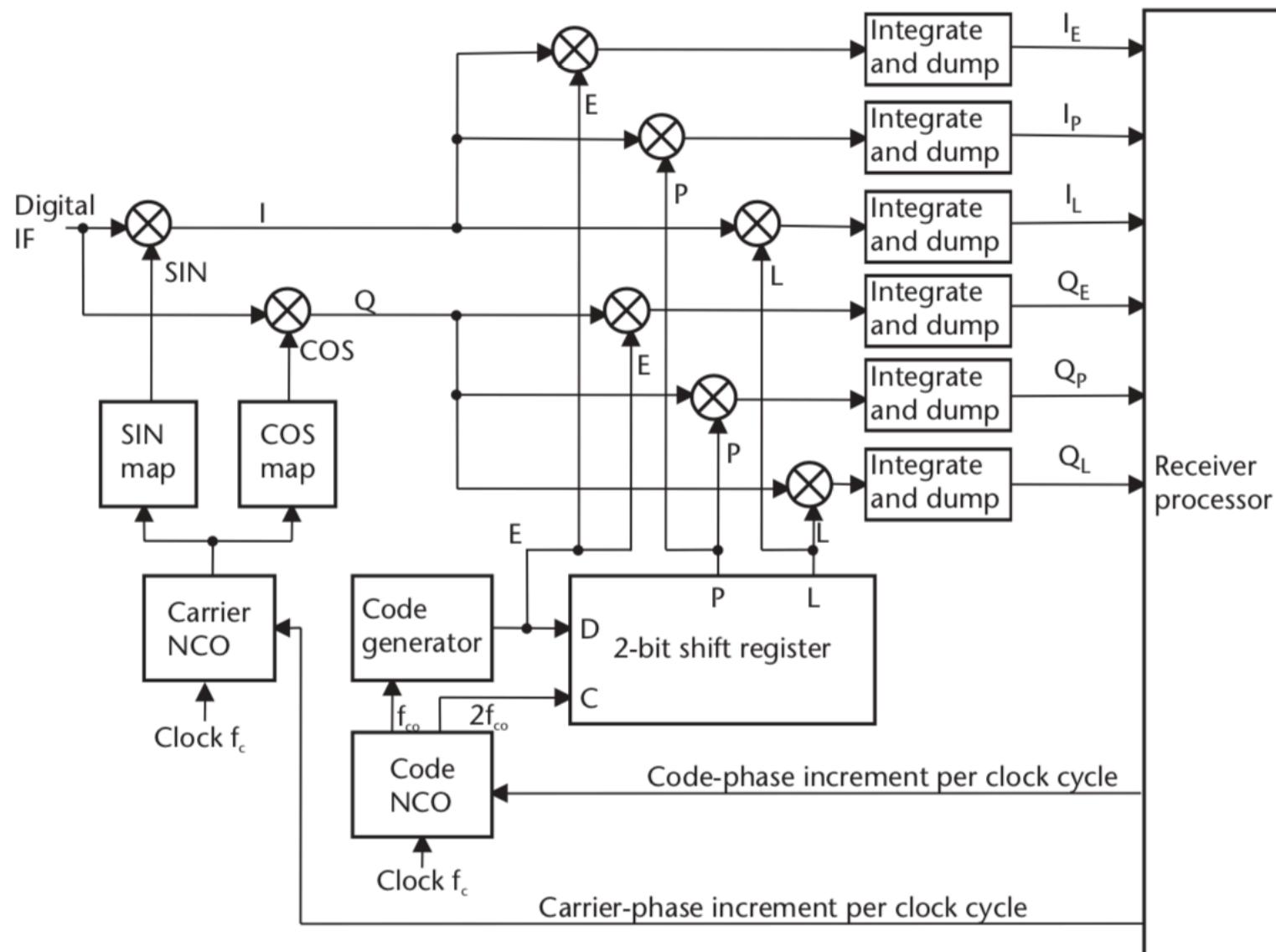
Code Lock Detector: $\mu_{NP} = \frac{1}{K} \sum_{m=1}^K NP_m$

Narrowband Power Difference (NBD): $NBD_m = \left(\sum_{i=1}^M I_i^2 \right) - \left(\sum_{i=1}^M Q_i^2 \right)$

Phase Lock Detector: $PLD_m = \frac{NBD_m}{NBP_m}$

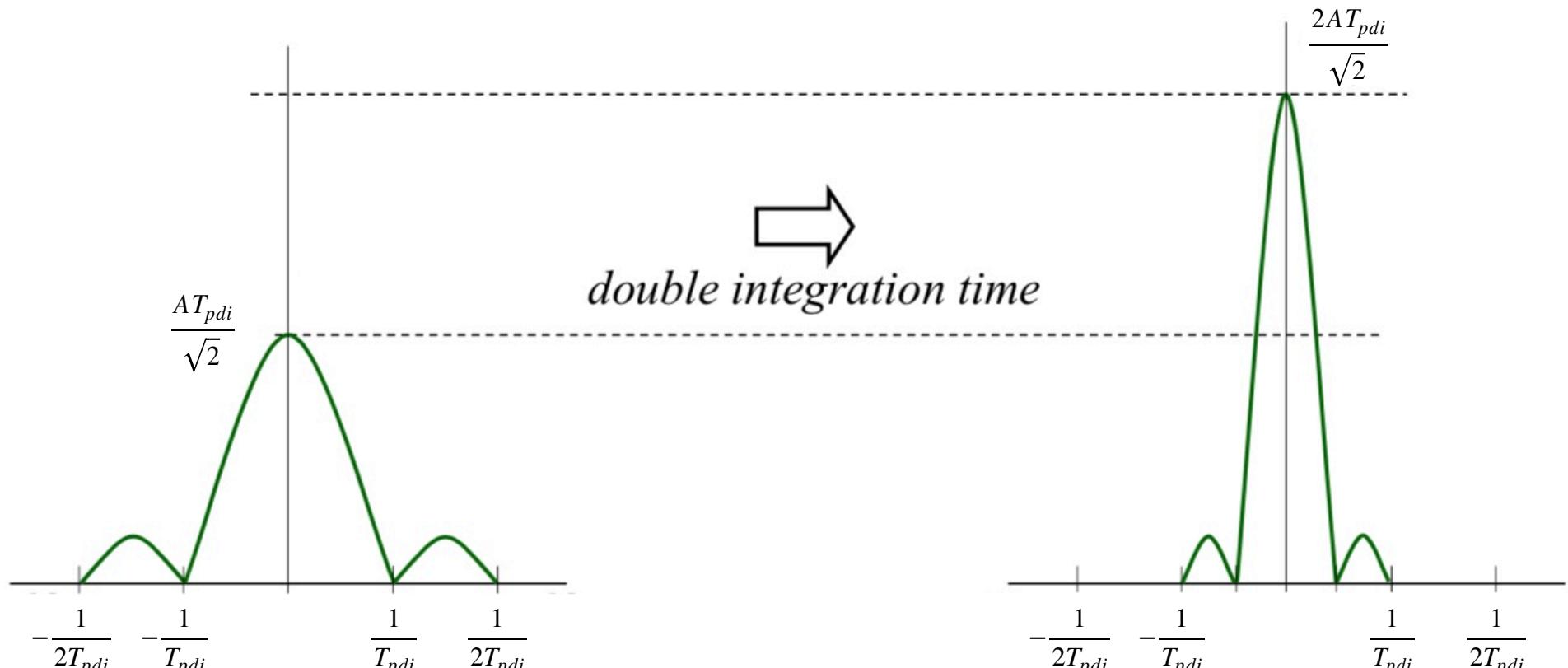


Receiver Block Diagram





Extending the Integration Time



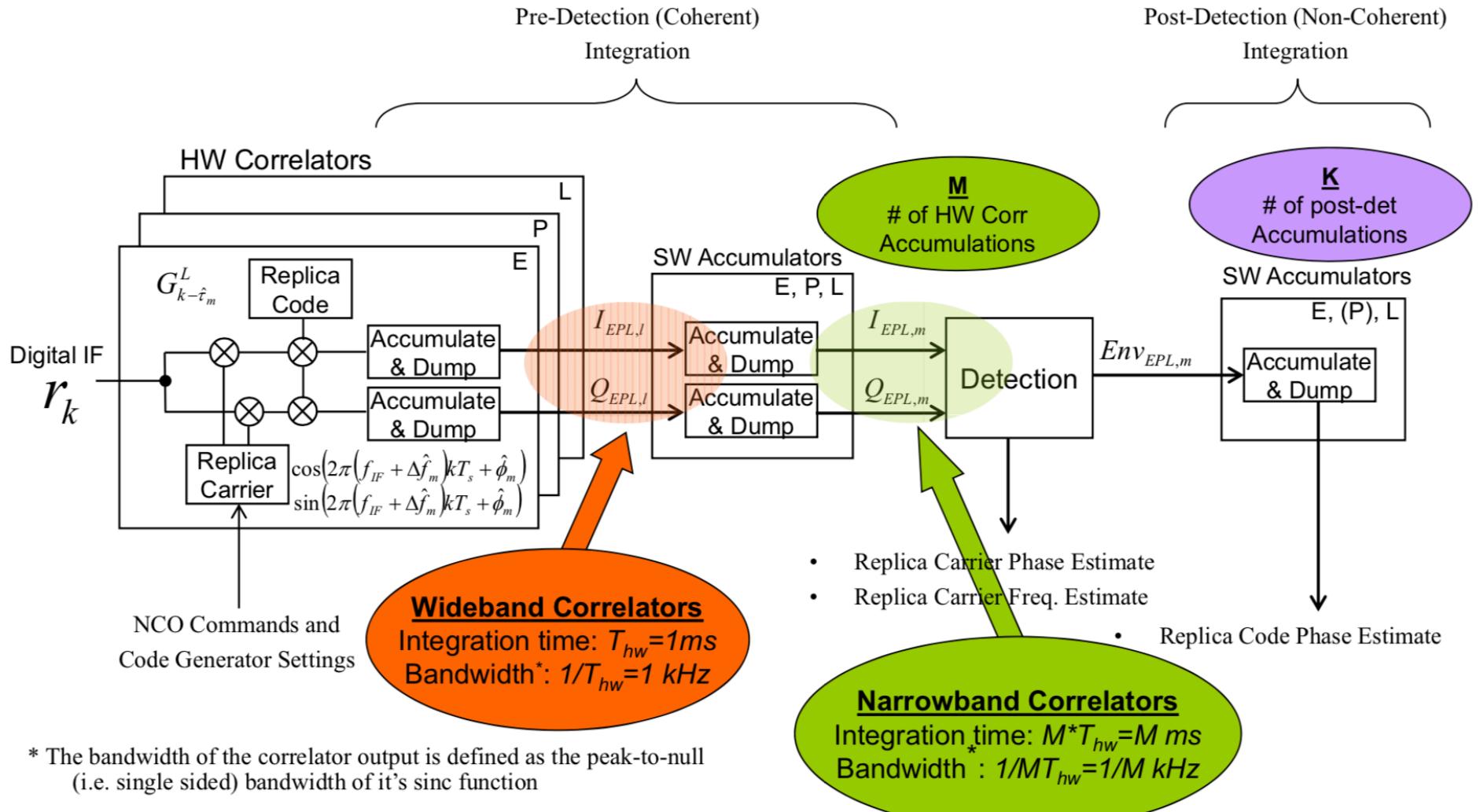
$$\text{Signal Envelope: } Z = \sqrt{I^2 + Q^2}$$

$$\text{Useful Signal Envelope: } Z_s = \frac{AT_{pdi}}{\sqrt{2}} \rightarrow \frac{2AT_{pdi}}{\sqrt{2}}$$

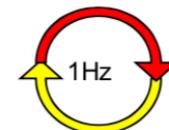
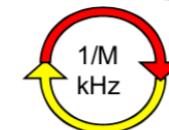
$$\text{Noise Envelope: } Z_n = \sqrt{T_{pdi}}\sigma_N \rightarrow \sqrt{2T_{pdi}}\sigma_N$$



Receiver Block Diagram



* The bandwidth of the correlator output is defined as the peak-to-null (i.e. single sided) bandwidth of its sinc function



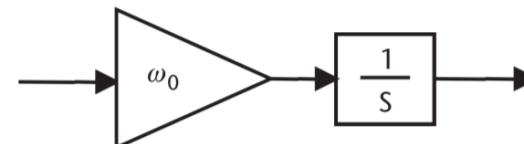


Loop Filters Order

First Order

Sensitive to velocity stress.

Unconditionally stable at all noise bandwidths.

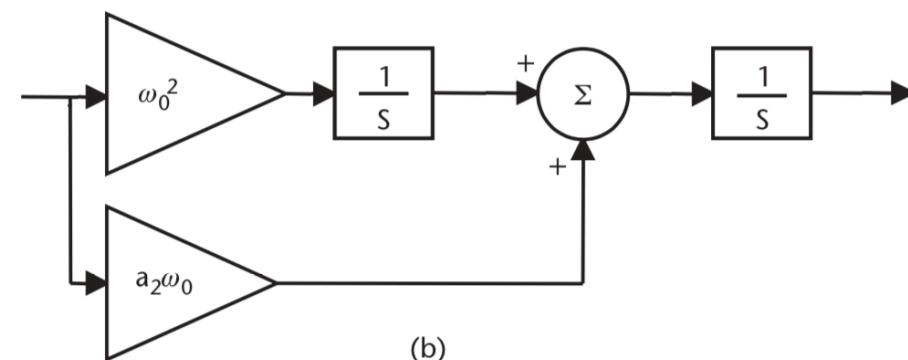


(a)

Second Order

Sensitive to acceleration stress.

Unconditionally stable at all noise bandwidths.

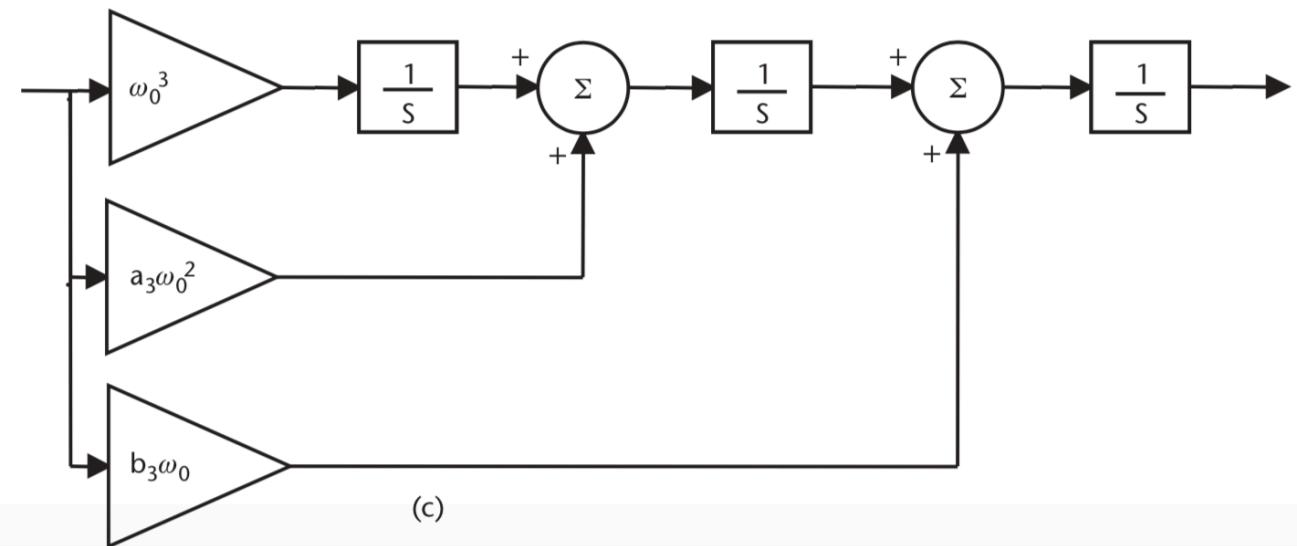


(b)

Third Order

Sensitive to jerk stress.

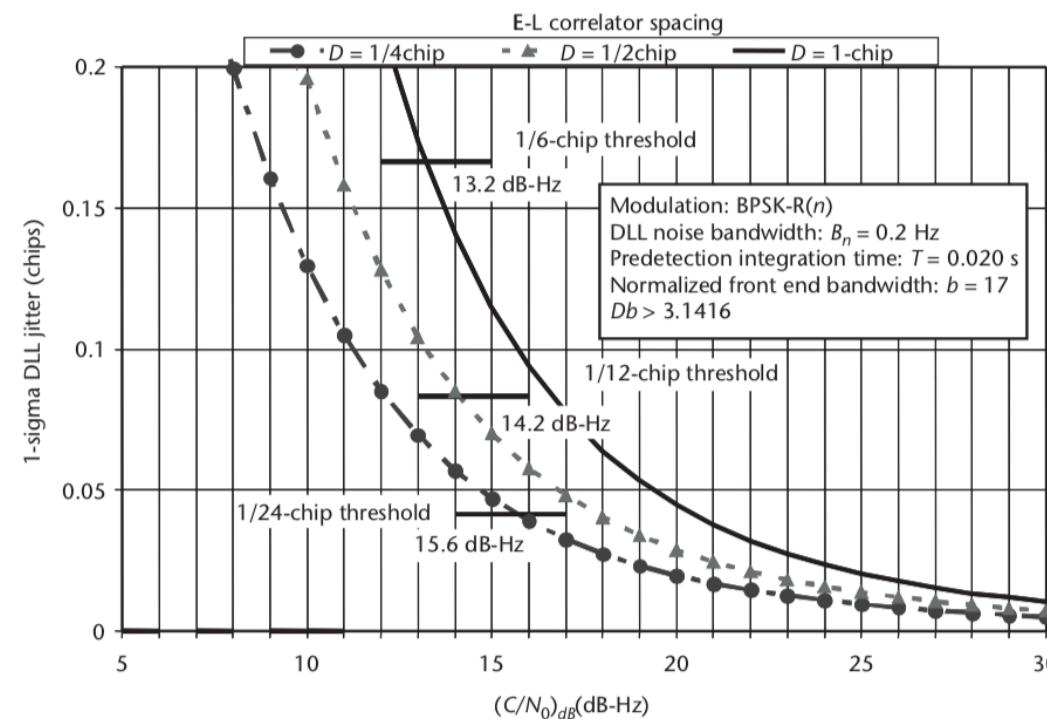
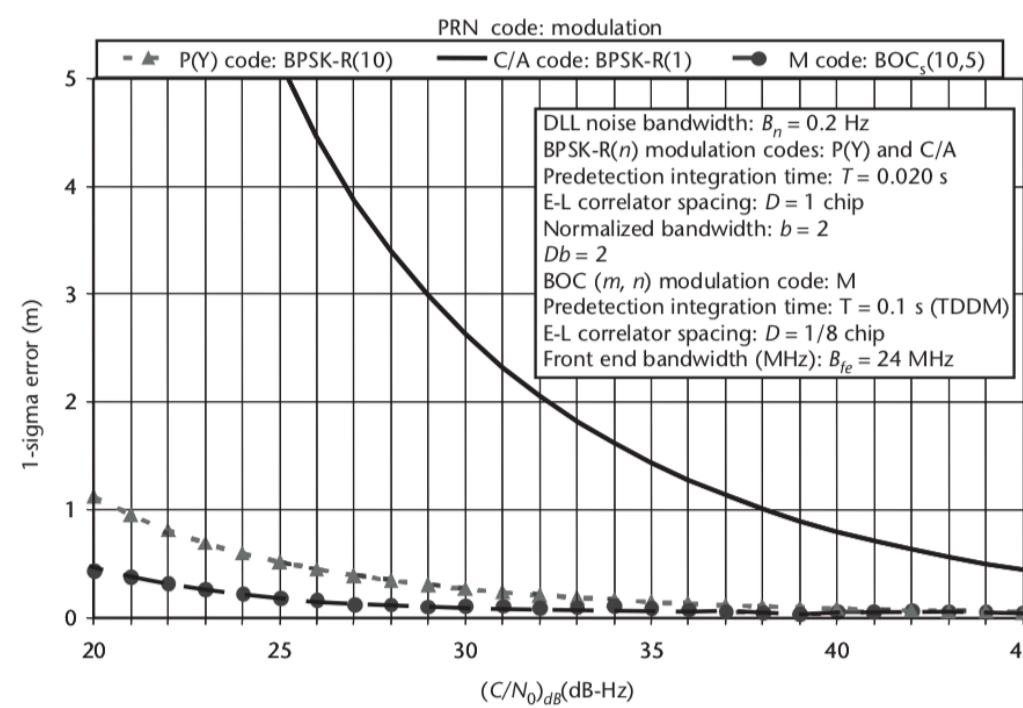
Remains stable at $B \leq 18$ Hz.



(c)

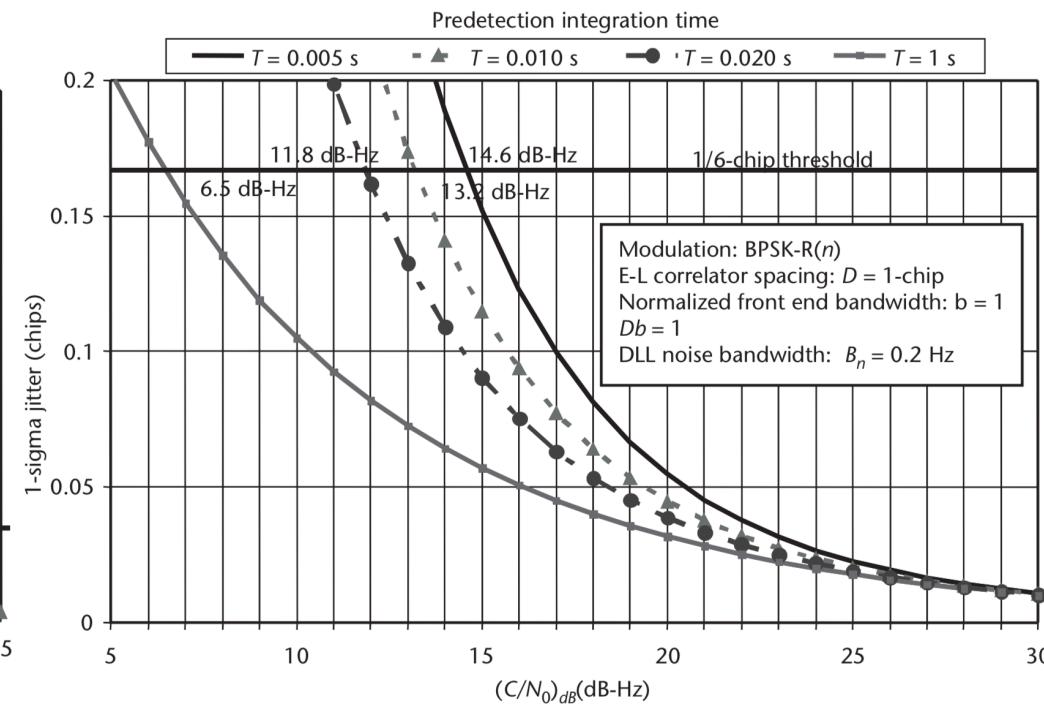
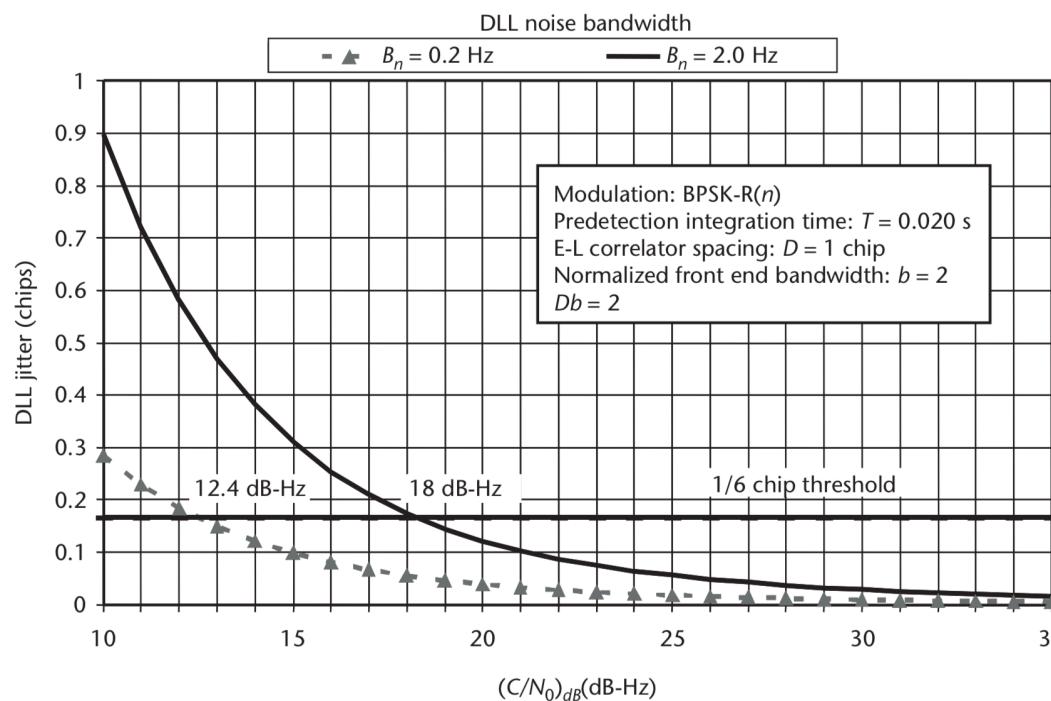


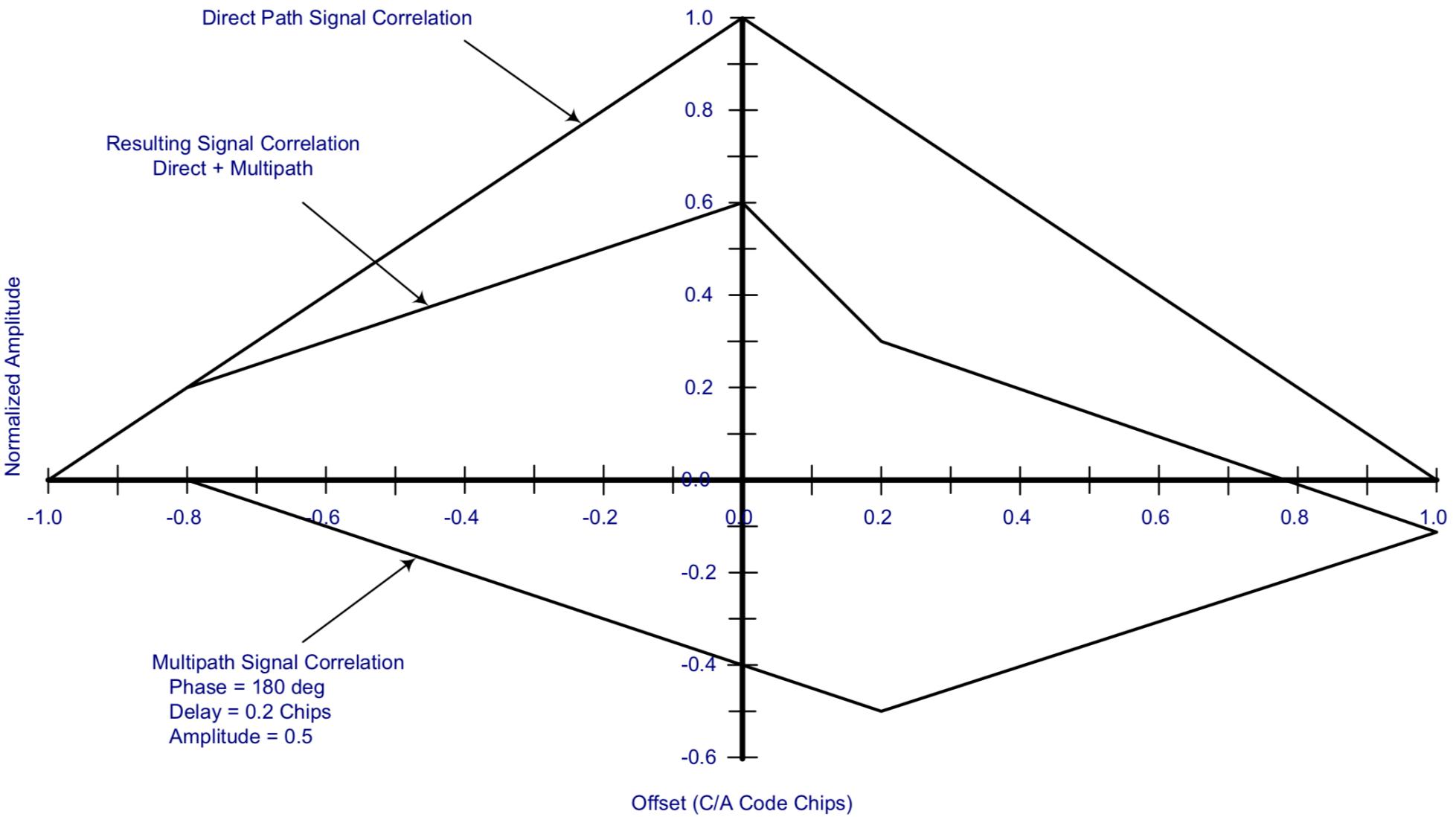
Tracking Performance





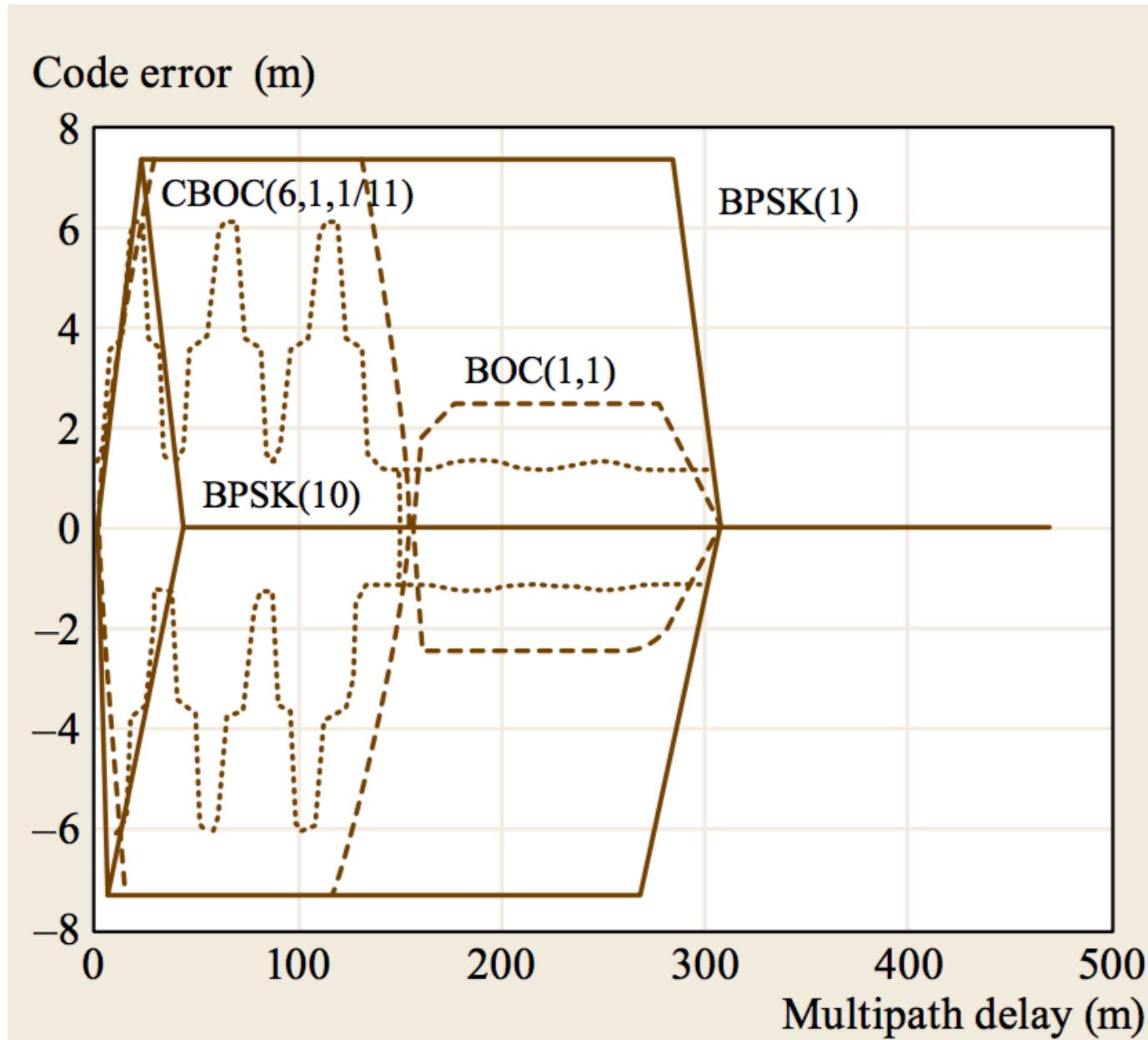
Tracking Performance





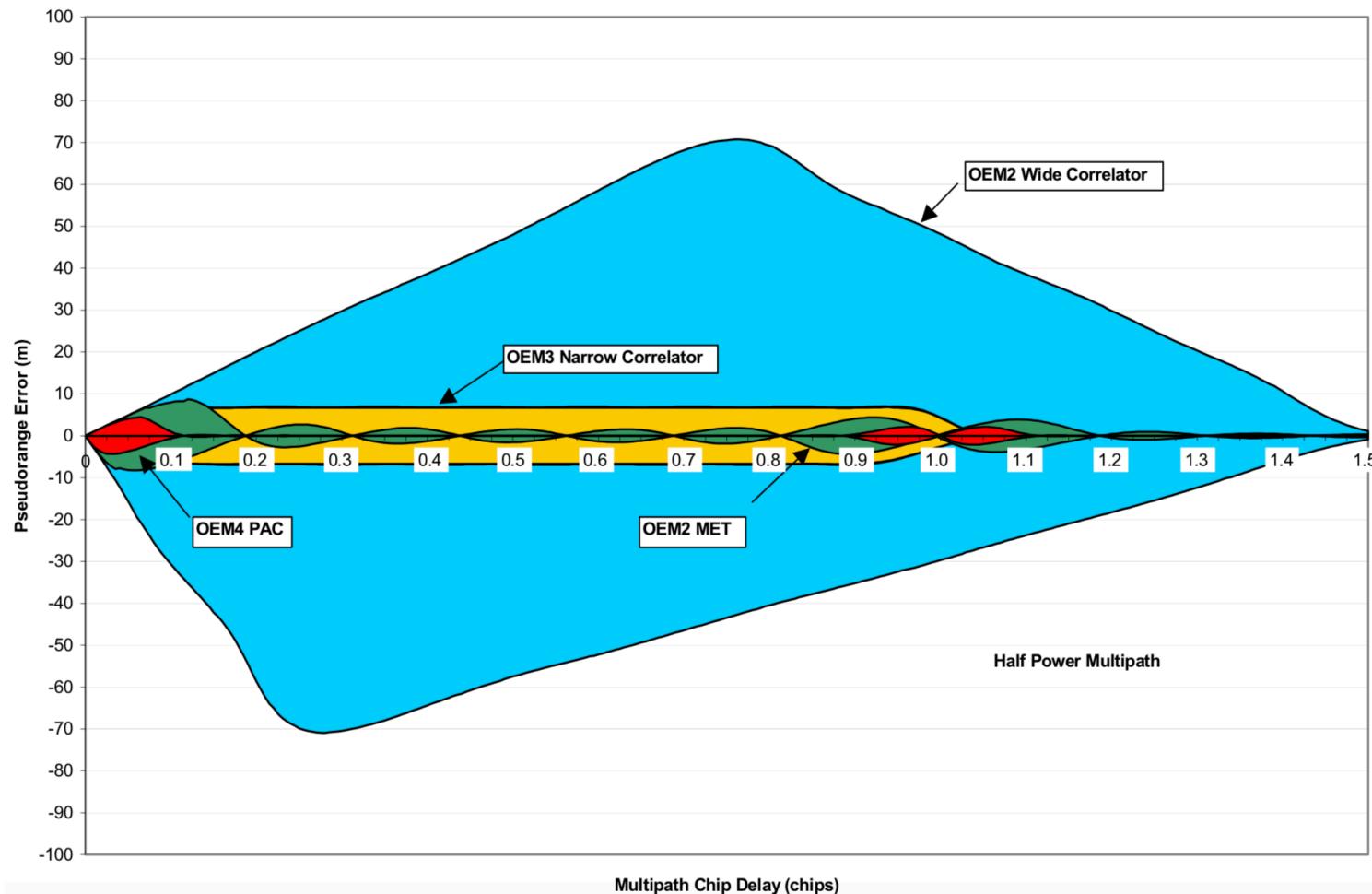


Multipath Envelopes I/II





Multipath Envelopes II/II



Example of different tracking loops performance from Novatel:

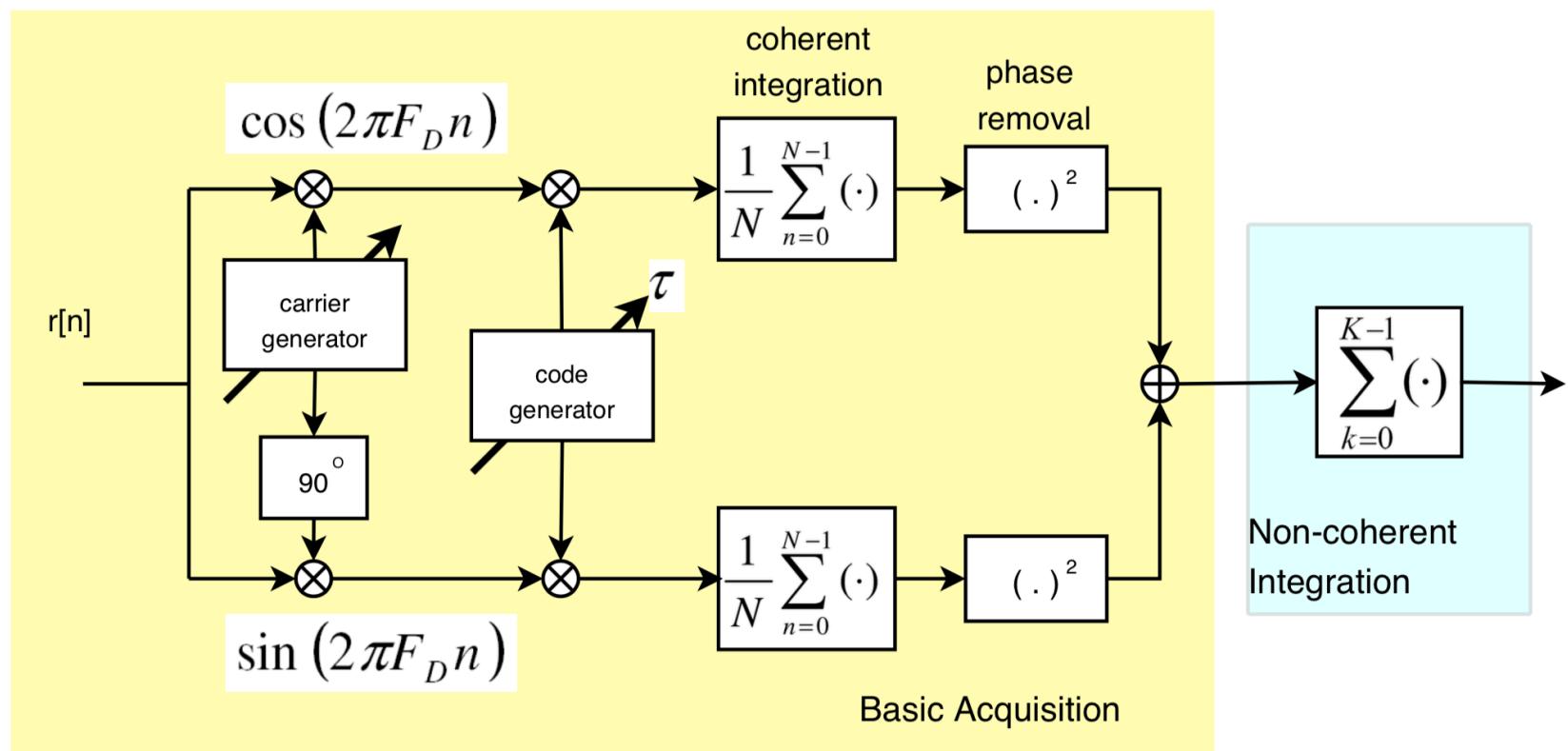
1992: Narrow Correlator

1994: Multipath Eliminating Technology (MET)

1999: Pulsed Aperture Correlator (PAC)



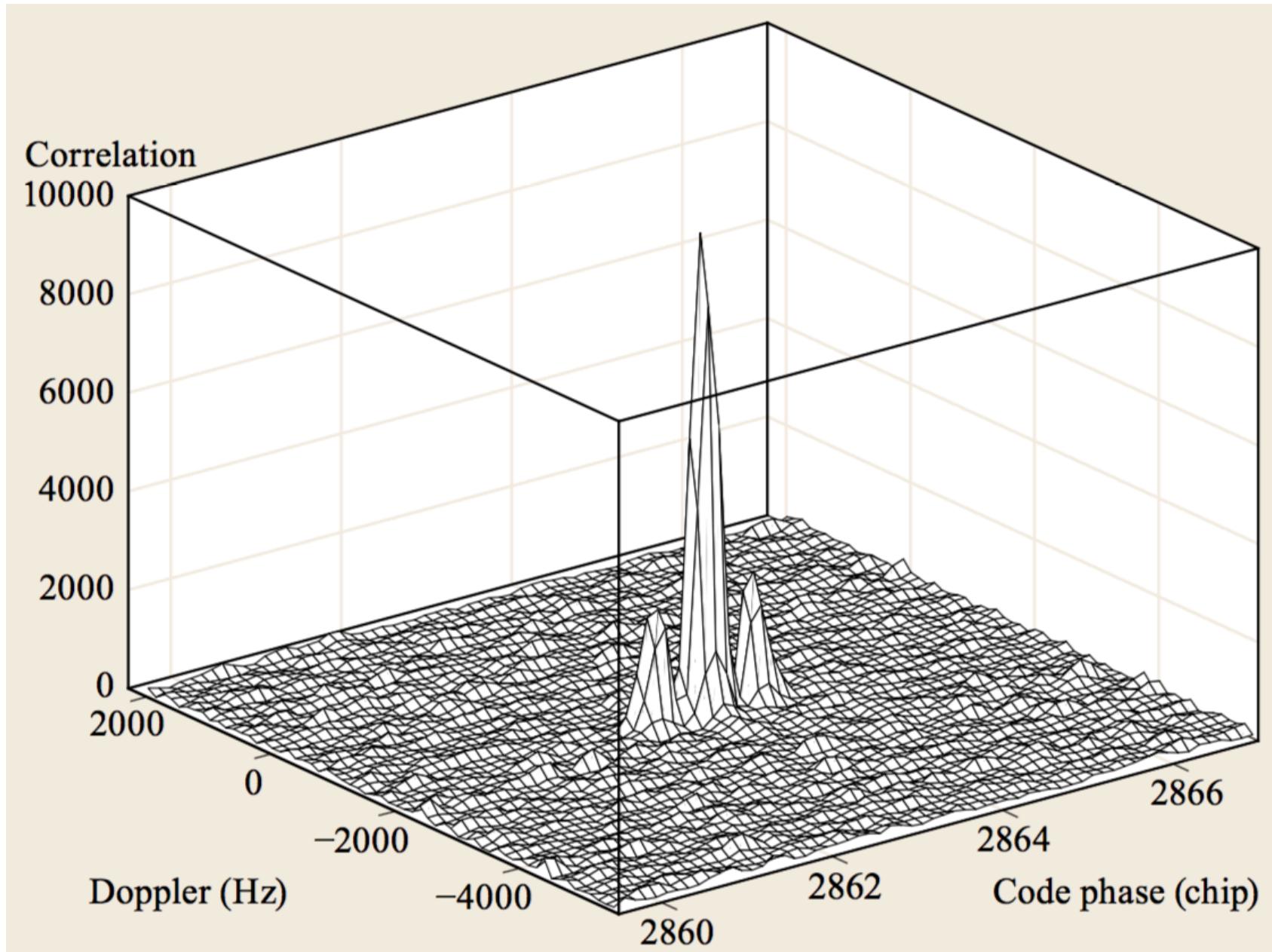
Signal Acquisition





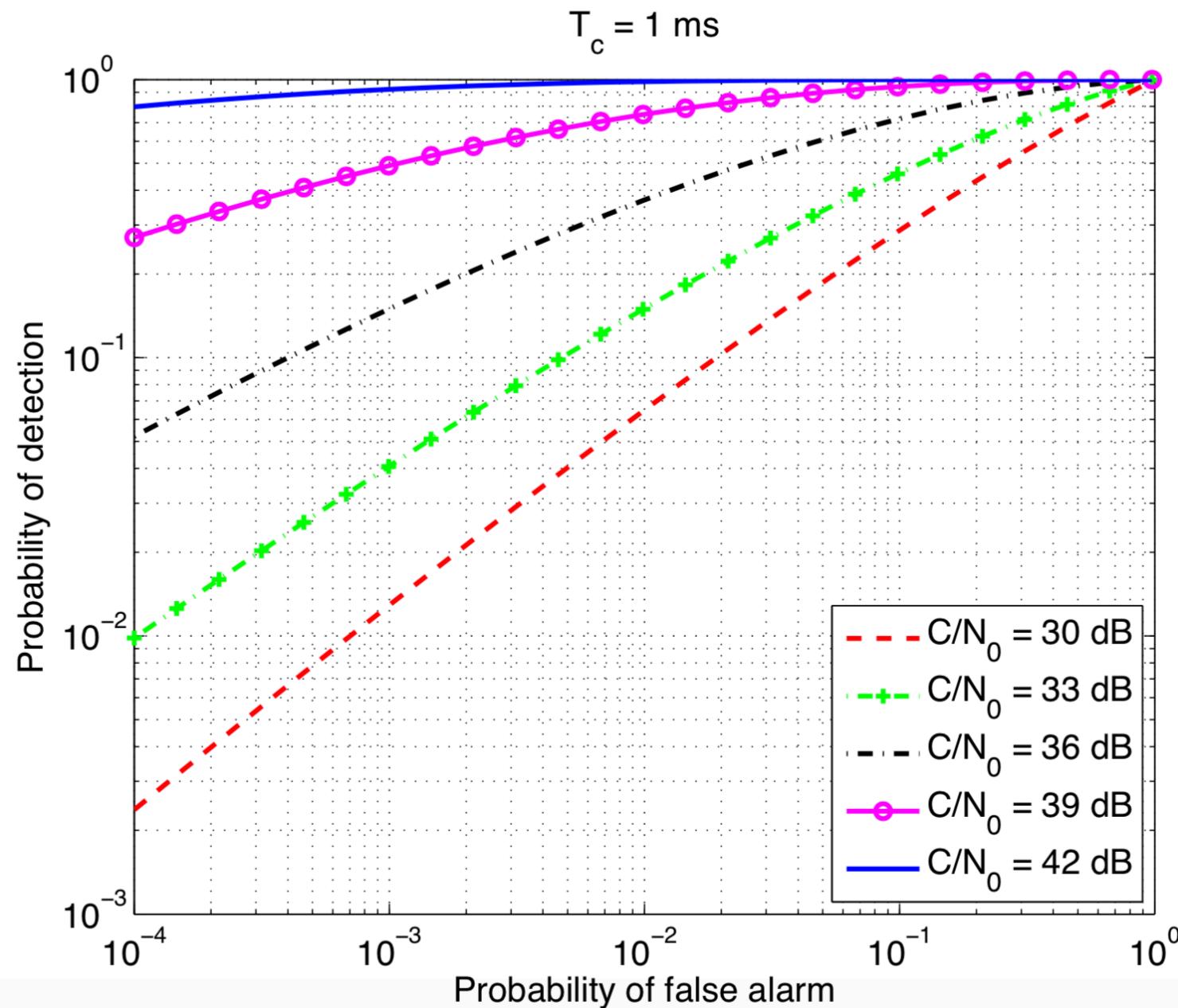
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Signal Acquisition





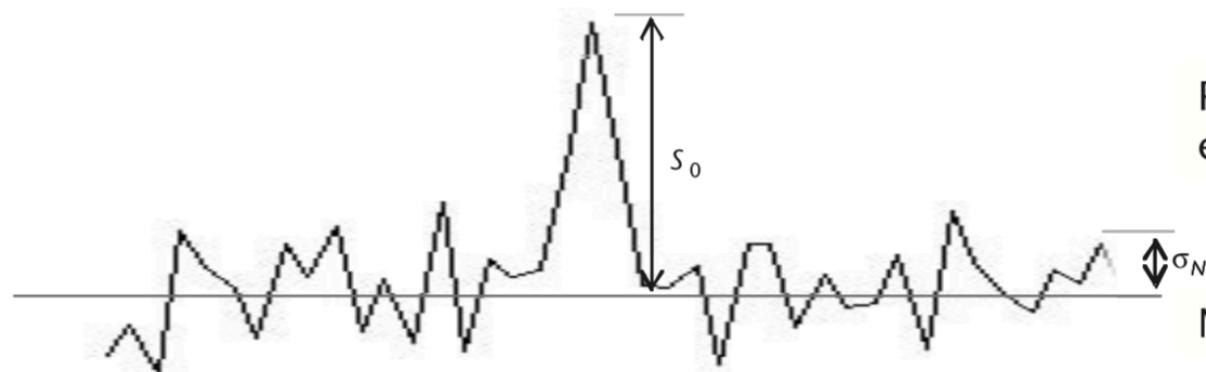
Detection Probability





Squaring Loss

I



For this example, all signal energy is shown in I channel

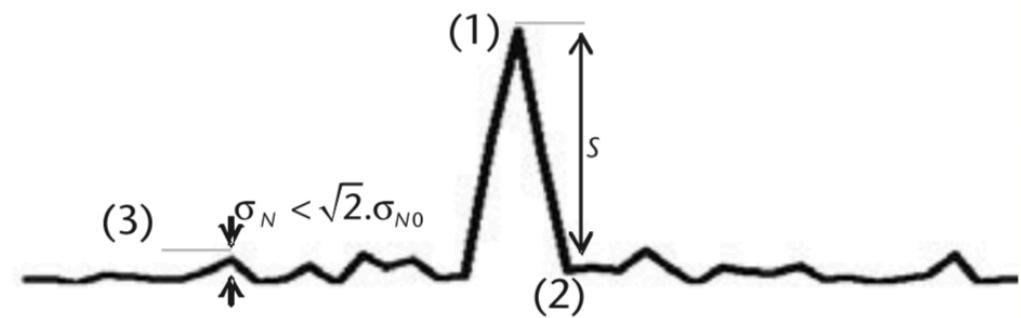
Mean I noise = 0

Q



Mean Q noise = 0

$$\sqrt{I^2 + Q^2}$$



(1) The correlation peak magnitude changes

(2) The mean value of the noise is above zero. So the effective peak magnitude, S , is reduced.

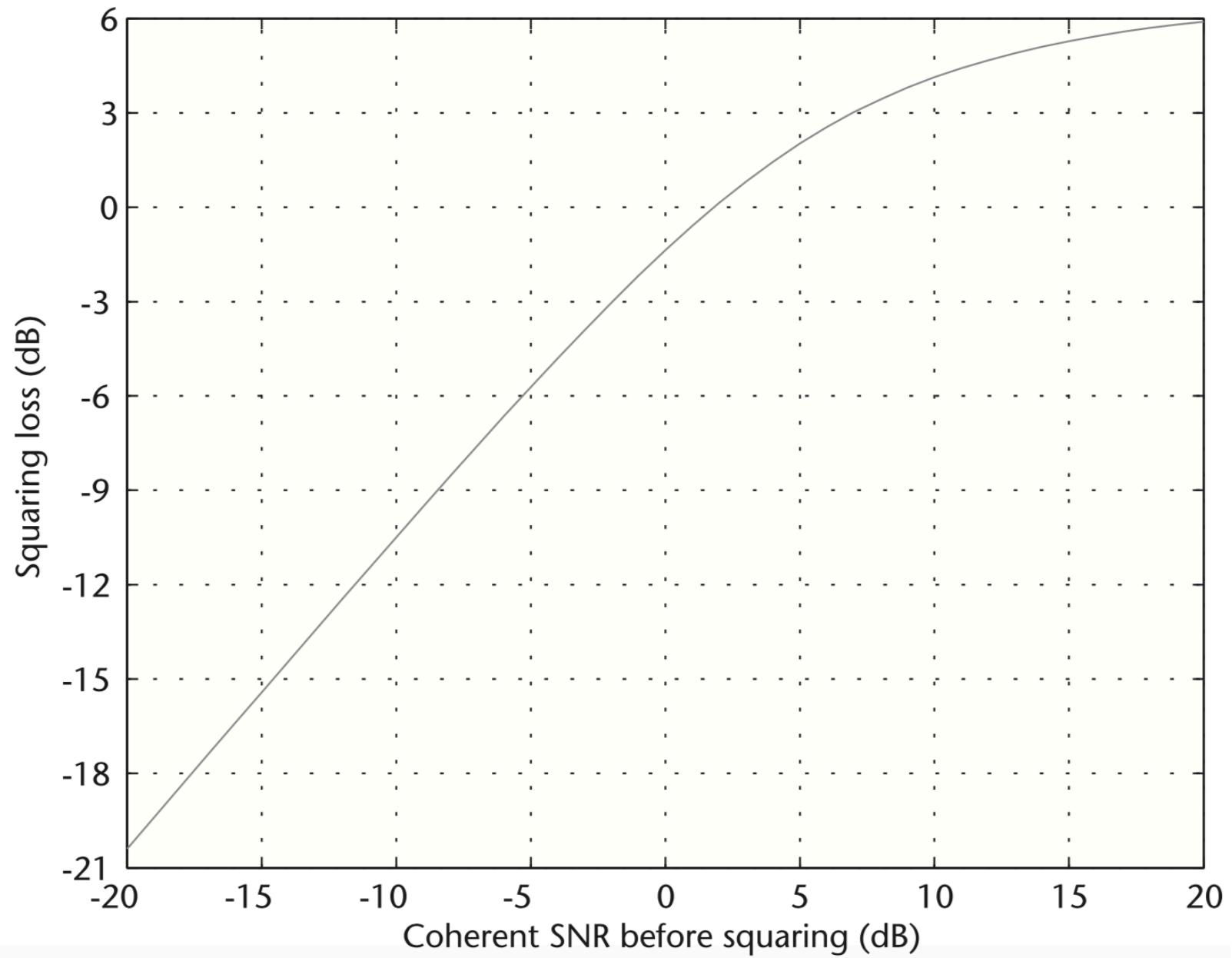
(3) The RSS operation changes the standard deviation of the noise

(1)+(2)+(3) = "squaring loss"



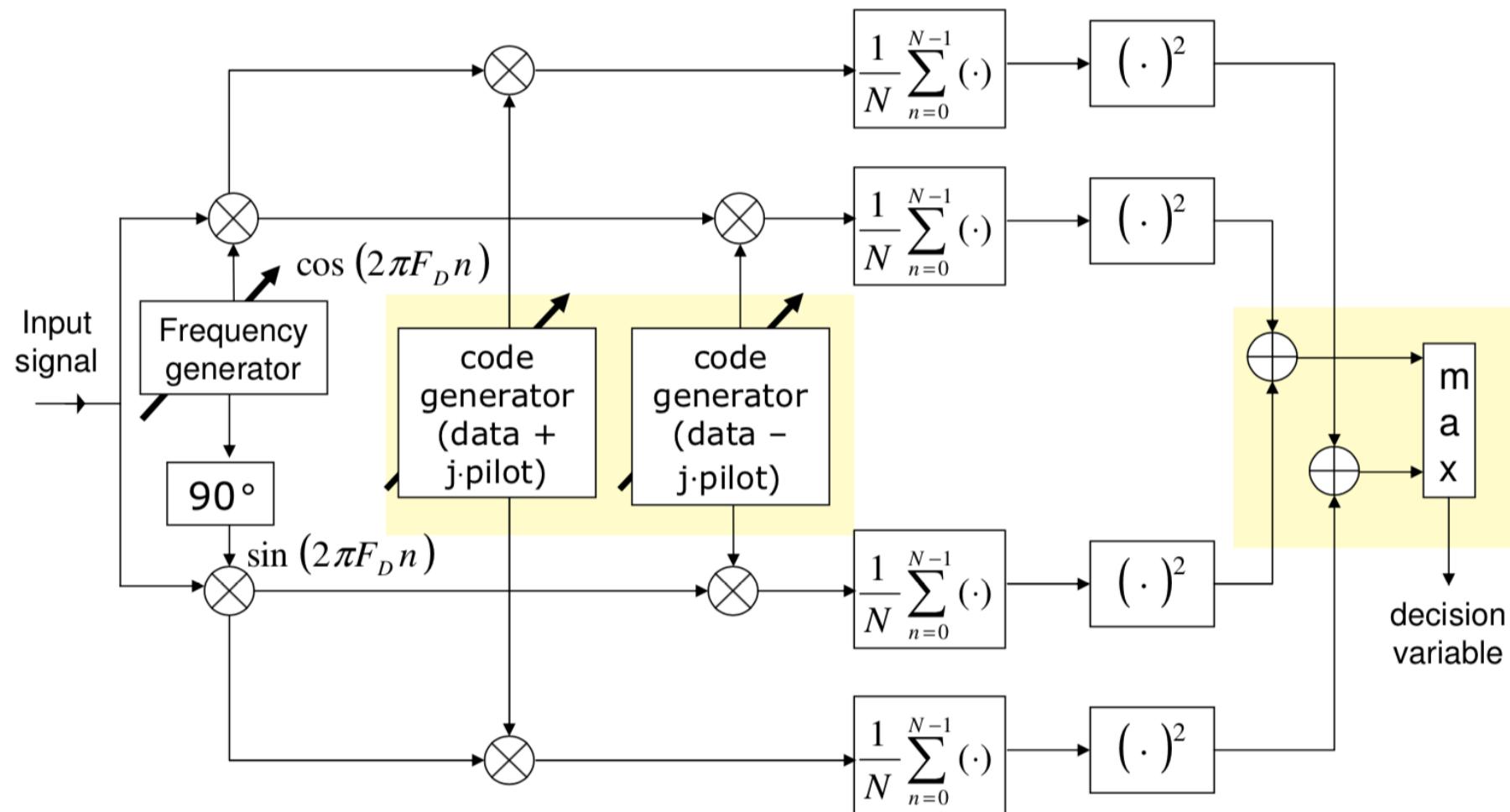
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Squaring Loss



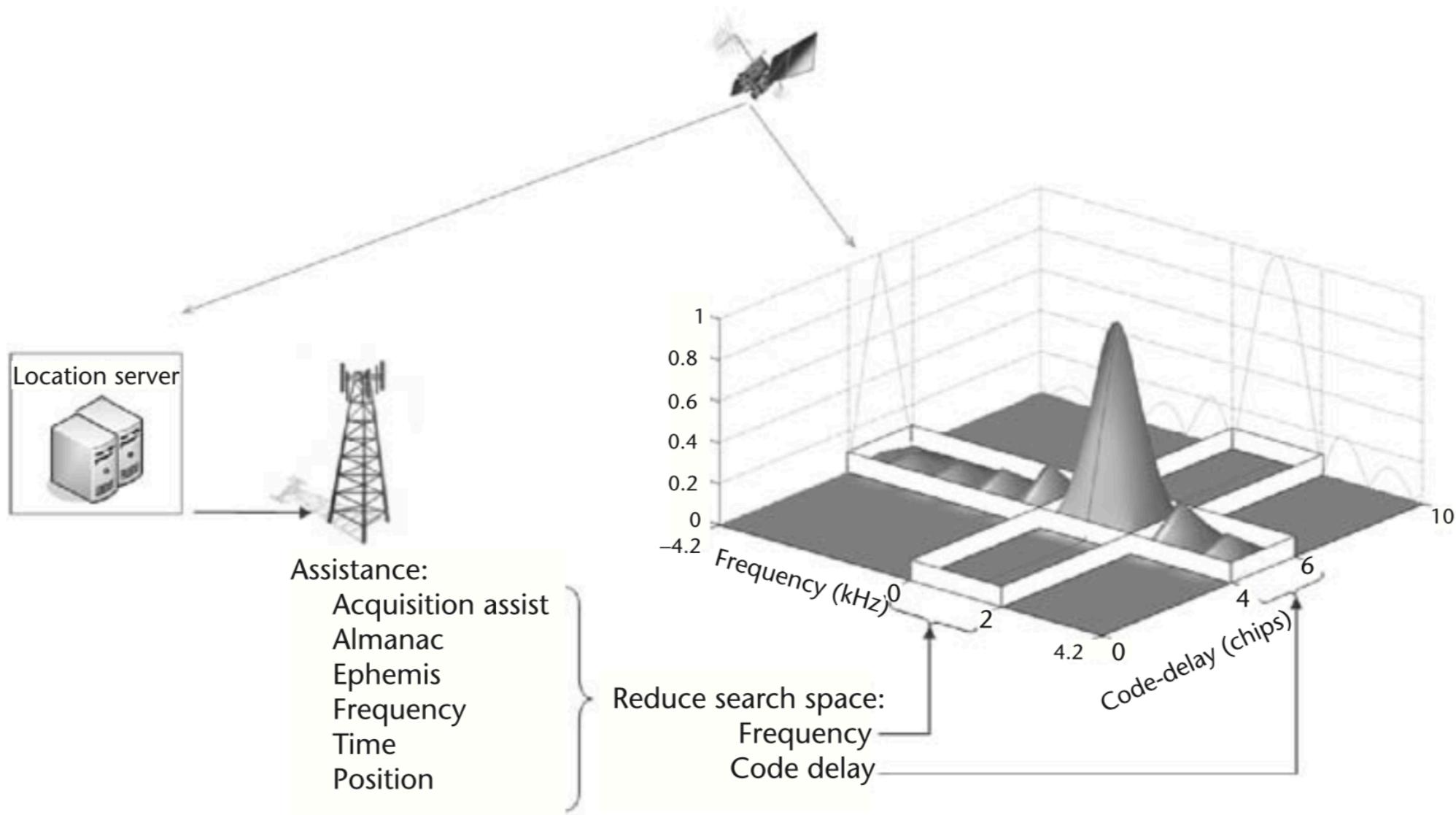


Signal Acquisition





Assisted GNSS





Autonomous	Uncertainty (+/-)	Typical
Satellite Motion	4.2 kHz	
Clock (TCXO)	1.575 kHz/ppm	3 ppm
RX speed	0.146 kHz/100 km/h	160 km/h
Total Search Space	9.2 kHz	

Assisted	Uncertainty (+/-)	Typical
Assistance Time	1.6 Hz	+/- 2 s
Assistance Position	3 Hz	3 km
Clock (TCXO)	157.5 Hz	100 ppb
RX speed	2*0.146 kHz/100 km/h	160 km/h
Total Search Space	630 Hz	