Department of Computer Science and Engineering (CSE) BRAC University

Lecture 9

CSE250 - Circuits and Electronics

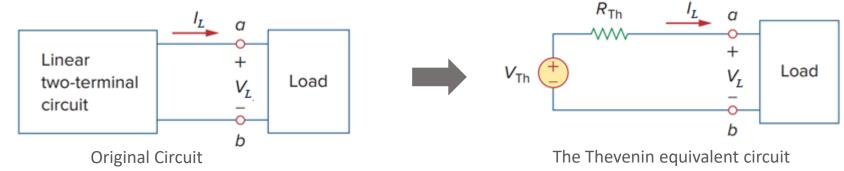
THEVENIN'S AND NORTON'S THEOREM



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Thevenin's Theorem

• Thevenin's Theorem states that a linear two-terminal circuit can be replaced by an equivalent circuit consisting of a voltage source V_{Th} in series with a resistor R_{Th} , where V_{Th} is the open-circuit voltage at the terminals and R_{Th} is the input or equivalent resistance at the terminals when the independent sources are turned off.



• Two circuits are said to be equivalent if they have the same I-V characteristics at their terminals.



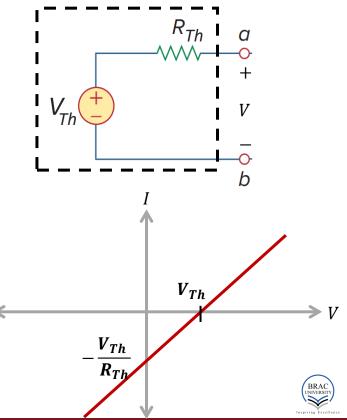
I-V of Thevenin Equivalent

- We recall that an equivalent circuit is one whose I-V characteristics are identical with the original circuit.
- Let's first find out the I-V characteristics of the reduced circuit with respect to terminals a-b.
- The configuration is a voltage source (V_{Th}) in series with a resistor (R_{Th}) . To determine the configuration's I-V characteristics, if applying a voltage V gives rise to a current I, we can write using KVL,

$$V = V_{Th} + IR_{Th}$$

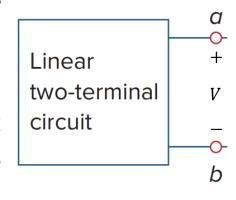
$$\Rightarrow I = \frac{1}{R_{Th}}V - \frac{V_{Th}}{R_{Th}}$$

• The equation results in a linear I vs V plot that intersects the axes at V_{Th} and $-\frac{V_{Th}}{R_{Th}}$.



I-V of Actual Circuit

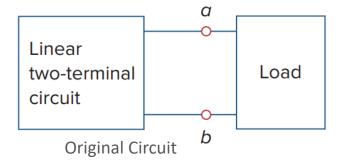
- Let's now find out the I-V characteristics of the original circuit with respect to terminals a-b.
- The circuit is a combination of linear circuit elements. We cannot theoretically derive exactly the relation between I and V unless we know the actual circuitry. However, as the circuit is linear, the I V characteristic will be a straight line and the line can be drawn if minimum two points on the line are known.

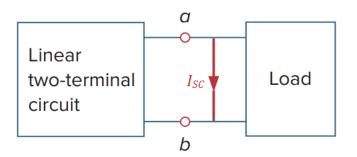


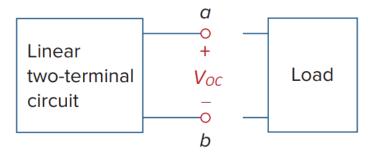
- The two points we can get are the intersecting points of x and y axis.
- To get the intersecting location on the voltage axis, current (I) at the terminals should be made equal to 0. That is, the terminals a-b must be open circuited.
- Similarly, for the intersecting location on current axis, $V_{ab}=V=0$. That is, the terminals a-b must be shorted.

OC Voltage & SC Current

- Let's denote V_{oc} be the voltage at the open terminals upon disconnecting the load
- I_{sc} be the current through the shorted terminals upon short circuiting the load.





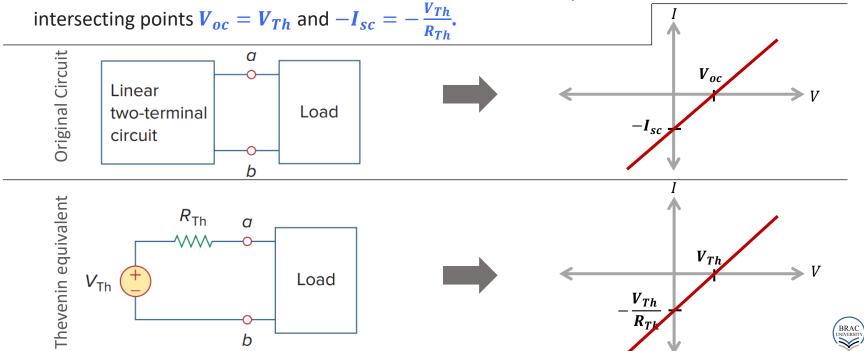


Open Circuited at the terminals

So, the I-V characteristic should be the straight line passing through the points $(V_{oc}, 0)$ and $(0, -I_{sc})$. The reason for the negative sign is that I_{sc} is opposite to the current (I) plotted along the y-axis.

Condition for Equivalence

• The original circuit and the reduced Thevenin equivalent circuit will be equivalent to each other if the I-V characteristics of the two are identical. They will indeed be identical if the



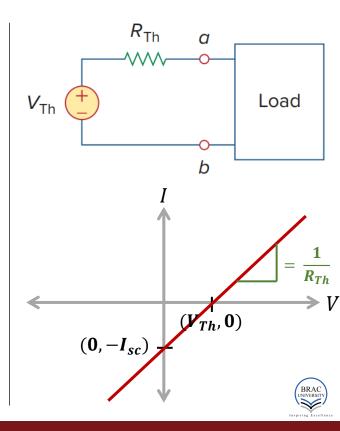
How to determine R_{Th}?

 We have seen in the previous slides that, Thevenin's conversion is valid if

i.
$$V_{oc} = V_{Th}$$
 and

ii.
$$-I_{SC} = -\frac{V_{Th}}{R_{Th}}$$
 or $I_{SC} = \frac{V_{Th}}{R_{Th}}$

- For the linear I-V characteristic, R_{Th} is the inverse of the slope of the straight line passing through the points $(V_{Th}, 0)$ and $(0, -I_{sc})$. That is,
- $Slope = \frac{\Delta I}{\Delta V} = \frac{1}{R_{Th}} = \frac{0 (-I_{SC})}{V_{Th} 0}$
- \Rightarrow $R_{Th} = \frac{V_{Th}}{I_{SC}}$
- Thus, R_{Th} may be found from this ohmic relation between V_{Th} and I_{sc} .

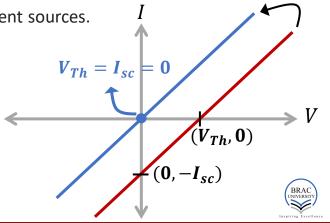


Special Case: undefined R_{Th}

- **Special Case** $(V_{Th} = 0)$: If V_{Th} is zero, $I_{SC} = \frac{V_{Th}}{R_{Th}}$ is likewise zero, and the circuit becomes resistive with respect to the terminals where Thevenin conversion is taking place. In this situation, the I V characteristic line, as shown, passes through the origin.
- This can happen in two scenarios:
- [See Example] i. if the network is erroneous in such a way that the load connected to the circuit gets no voltage and
- [See Example] ii. if the portion of the network excluding load has no independent sources.
 - This results in an undefined and indeterminant situation if we proceed to determine R_{Th} .

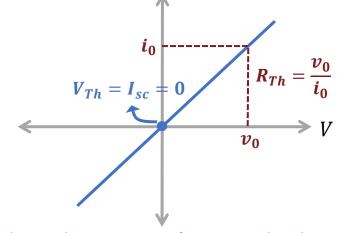
$$R_{Th} = \frac{V_{Th}}{I_{SC}} = \frac{0}{0}$$

• Let's think of a different approach to tackle this situation to determine R_{Th} .



Universal Rule to determine R_{Th}

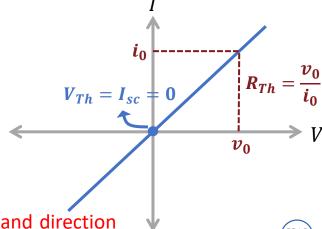
- As $V_{Th}=0$ results in a resistive I-V passing through the origin $(V_{Th},\ 0)=(0,\ -I_{SC})=(0,0)$, we may still find the value of R_{Th} by measuring the slope of the line with any other arbitrary point (v_0,i_0) on the line.
- Interestingly, we can use this technique to determine R_{Th} whether or not V_{Th} is zero. This is what the term "Universal Rule" refers to.
- So, in general (whether or not V_{Th} is zero), the strategy is to forcefully make the I-V characteristic line to go through the origin. Then calculating R_{Th} as $R_{Th} = \frac{v_0}{i_0}$.



• This can be accomplished simply by turning off all the independent sources (or equivalently replacing them with their resistances). As a result, the circuit becomes resistive, and the characteristic line will pass through the origin.

Universal Rule w/wo dependent source

- No dependent source: If a network has no dependent sources, then after turning off all the independent sources, the circuit will be a combination of resistors only. This simplifies the procedure as that, to determine R_{Th} , it is not even required to apply a voltage v_0 (or current i_0) and determine the corresponding current i_0 (or voltage v_0). Instead, use the series and/or parallel combinations of resistors to determine the equivalent resistance at the terminals, which is R_{Th} .
- **Dependent source:** However, if the network has dependent sources, then to get any point (v_0, i_0) on the line, apply a voltage source v_0 at load terminals and determine the resulting current i_0 . Then $R_{Th} = v_0/i_0$. Alternatively, insert a current source i_0 at load terminals and find the terminal voltage v_0 . Again $R_{Th} = v_0/i_0$. We call the applied source as dummy or test source. In either approach, we may assume any value of v_0 or i_0 .



Note that, for an applied dummy or test source, polarity of v_0 and direction of i_0 must be such that, the current i_0 leaves the +ve terminal of v_0 .

Methods in a nutshell

Methods to determine R_{Th}

Yes

Kill all the Method to determine V_{Th} Short the load terminals independent sources Disconnect the load (if any) Determine the current through the short circuit (I_{sc})

 $R_{Th} = \frac{V_{Th}}{I_{sc}}$

Use Ohm's Calculate the current Law to (i_0) supplied or voltage calculate (v_0) across the voltage or $R_{Th} = \frac{v_0}{c}$ current source respectively.

Determine the open circuit voltage

at the load terminals $(V_{OC} = V_{Th})$

Add a dummy voltage or current source to the load terminals

Valid only if $V_{Th} \neq 0$

No Use series-parallel combinations resistors to calculate

 $R_{ea} = R_{Th}$

Is there

anv dependent

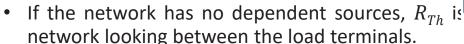
source(s)?

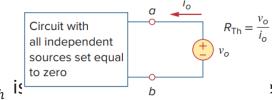
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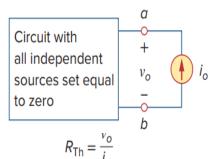
Universal Rule

Procedure to find parameters

- \blacksquare Finding $V_{oc} = V_{Th}$: Disconnect the load and use nodal/mesh or other circuit solving techniques to find the open circuit voltage at the load terminals.
- **Finding** I_{sc} : Disconnect the load, short the terminals, use nodal/mesh or other circuit solving techniques to find the short circuit current at the load terminals.
- \blacksquare Finding R_{Th}
 - Case 1: If $V_{Th} \neq 0$, Use $R_{Th} = \frac{V_{Th}}{I_{CR}}$
 - <u>Case 2</u>: If $V_{Th} = 0$, turn off all the independent sources.



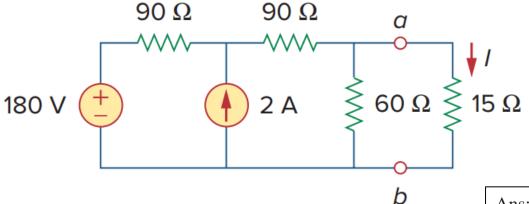




If the network has dependent sources, apply a voltage source v_0 at load terminals determine the resulting current i_0 . Then $R_{Th} = v_0/i_0$. Alternatively, we may insert a current source i_0 at load terminals and find the terminal voltage v_0 . Again $R_{Th} = v_0 / i_0$. In either approach we may assume any value of v_0 and i_0 .

Example 1

Using Thevenin's theorem, find the equivalent circuit to the left of the terminals in the circuit. Then find *I*.

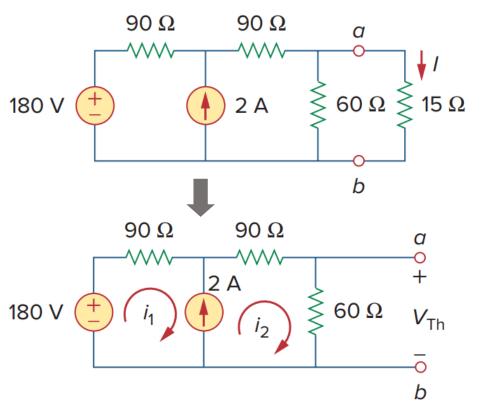


<u>Ans</u>: $V_{Th} = 90 V$; $R_{Th} = 45 \Omega$; $i_x = 1.5 A$



^{*} See solution in the next slide if necessary

Example 1: finding V_{Th}



Step 1: Disconnecting the load and finding the open circuit voltage.

Let's use mesh analysis to find the V_{Th}

KVL at mesh 1 and mesh 2 (forming supermesh),

$$-180 + 90i_1 + 90i_2 + 60i_2 = 0$$

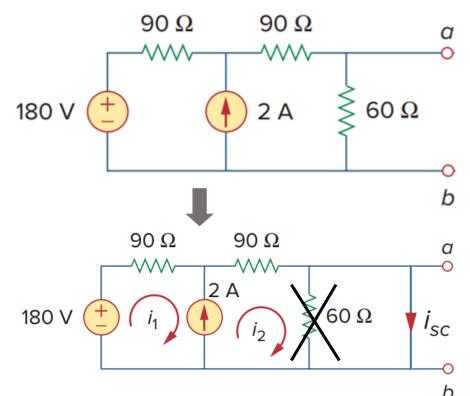
$$\Rightarrow 90i_1 + 150i_2 = 180 ------(i)$$

KCL at the supermesh, $i_1 - i_2 = -2$ --- -(ii)

Solving,
$$i_1 = -0.5 A$$
; $i_2 = 1.5 A$

So,
$$V_{Th} = 60i_2 = 60 \times 1.5 = 90 V$$

Example 1: finding R_{Th}



<u>Step 2</u>: As $V_{Th} \neq 0$, with the load disconnected, we find the short circuit current I_{sc} . The terminals a-b are shorted.

Let's use mesh analysis to find the $I_{sc.}$ Note that the 60 Ω resistance is shorted out.

KVL at mesh 1 and mesh 2 (forming supermesh), $-180 + 90i_1 + 90i_2 = 0$

$$\Rightarrow i_1 + i_2 = 2 -----(i)$$

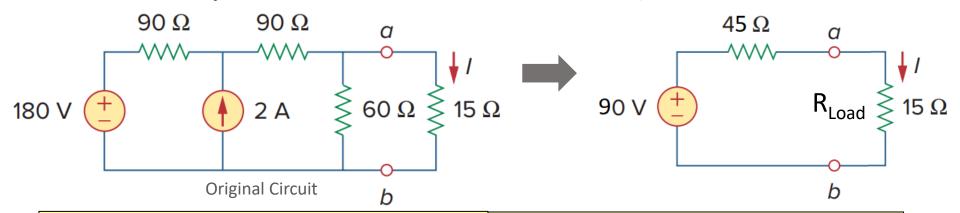
KCL at the supermesh,

$$i_1 - i_2 = -2$$
 ----(ii)

Solving,
$$i_1 = 0 A$$
; $i_2 = 2 A$

So,
$$I_{sc} = i_2 = 2 A$$

Example 1: Thevenin equivalent



Step 3: With V_{Th} and I_{sc} known, we can find R_{Th} as follows,

$$R_{Th} = \frac{V_{Th}}{I_{SC}} = \frac{90}{2} = 45 \ \Omega$$

So, the Thevenin equivalent circuit looks like the one shown above.

The load current *I* can be found as follows,

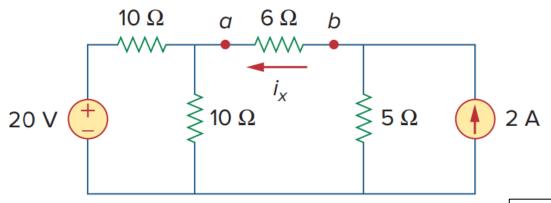
$$I = \frac{90}{45 + 15} = 1.5 A$$

[Calculate I from the original circuit and verify the Thevenin's theorem]

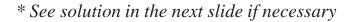


Example 2

Find the Thevenin equivalent looking into terminals a-b of the circuit and solve for i_{γ} .



$$\mathbf{A} \mathbf{0} = \mathbf{x} \mathbf{i} : \Omega \mathbf{0} \mathbf{1} = \mathbf{A} \mathbf{A} : \mathbf{V} \mathbf{0} = \mathbf{A} \mathbf{V} : \underline{\mathbf{A}} \mathbf{A} : \underline{\mathbf{A}} : \underline{\mathbf{A$$





Example 2: finding V_{Th}

Step 1: Disconnecting the load and finding the open circuit voltage.

No current flows through the open circuit. So, the voltage across the 10 Ω resistance can be found by voltage division, that is,

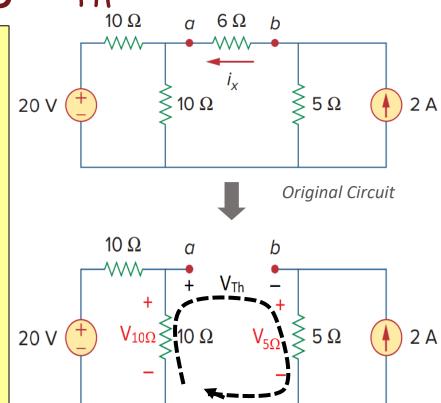
$$V_{10\Omega} = \frac{10}{10 + 10} \times 20 = 10 \, V.$$

The current 2 A flows through the 5 Ω resistor.

$$V_{5\Omega} = 5 \times 2 = 10 V$$

The voltages are indicated in the figure. V_{Th} can be found by applying KVL along the black dashed line shown. That is,

$$-10 + V_{Th} + 10 = 0$$
$$\Rightarrow V_{Th} = 0 V$$



Example 2: finding R_{Th}

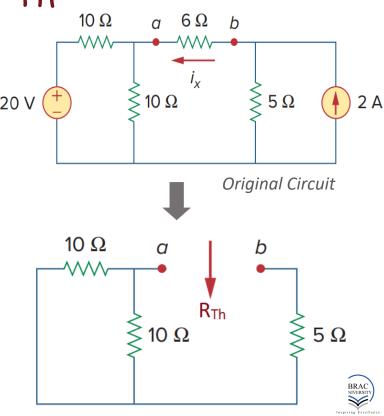
Step 2: As $V_{Th}=0$, I_{sc} will also be zero, hence, $R_{Th}=\frac{V_{Th}}{I_{sc}}$ will result in a $\frac{0}{0}$ situation. In this case we find R_{Th} by killing all the independent sources [Replace voltage sources by short circuits and current sources by open circuits].

Now check if there are dependent sources in the reduced circuit. As there is none, we simply use series-parallel combination to find the equivalent resistance seen from the load terminal. That is,

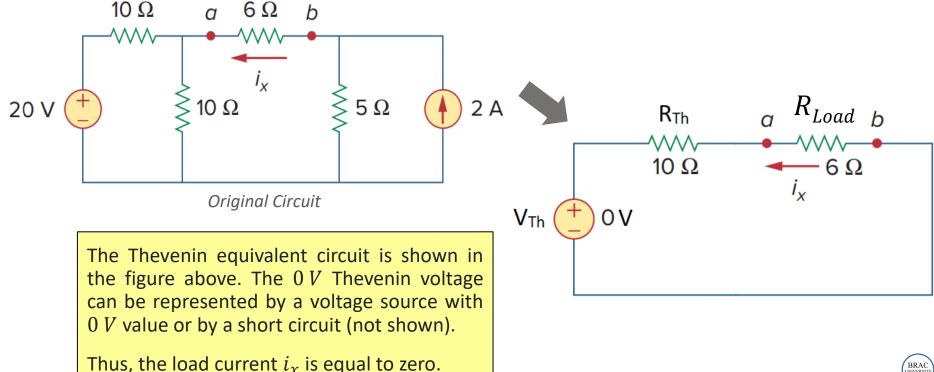
$$R_{Th} = (10 \mid \mid 10) + 5$$

$$\Rightarrow R_{Th} = 10 \Omega$$

[Keep in mind that, this method of determining R_{Th} by killing independent sources always works regardless of whether V_{Th} is equal to zero or not.]

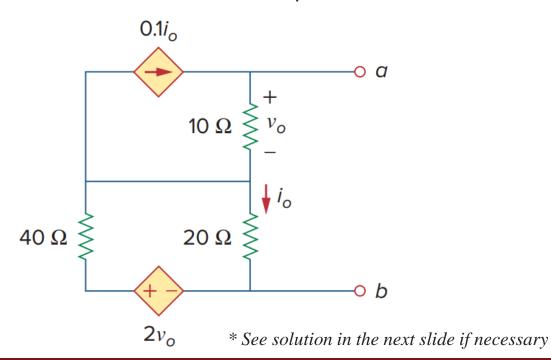


Example 2: Thevenin equivalent



Example 3

Obtain the Thevenin equivalent circuit at terminals a-b.





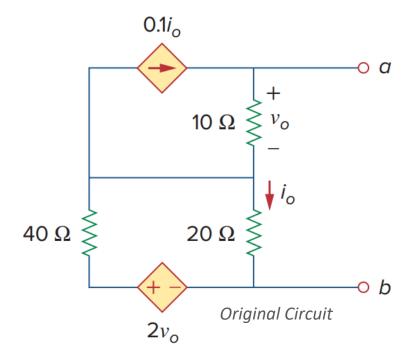
Example 2: finding V_{Th}

<u>Step 1</u>: Disconnecting the load and finding the open circuit voltage.

There are two dependent sources but no independent sources in this circuit. This means that all currents and voltages, including those on which dependent sources rely, will be zero. That is, $i_0=0, v_0=0$. As a result, there will be no contributions from the dependent sources. So, we can write,

$$V_{Th} = V_{ah} = 0 V.$$

[Circuit analysis can be used to confirm that $V_{Th}=0$]



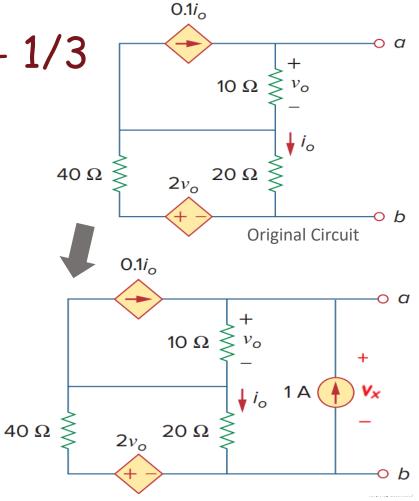


Example 3: finding R_{Th} - 1/3

Step 2: As $V_{Th}=0$, I_{SC} will also be zero, hence, $R_{Th}=\frac{V_{Th}}{I_{SC}}$ will result in a $\frac{0}{0}$ situation. In this case we find R_{Th} by killing all the independent sources.

There are no independent sources in this circuit.

There are two dependent sources. So, we must add a dummy voltage/current source between terminals a-b. Let's add a current source of 1 A between the terminals a-b. We have to find the voltage v_{χ} across the current source as shown in the circuit diagram.



Example 3: finding R_{Th} - 2/3

Let's apply mesh analysis to solve for v_0 .

It can be seen from loop 3 that,

$$i_3 = -1 A$$

Also from loop 1,

$$i_1 = 0.1i_0 = 0.1(i_2 - i_3)$$
 $[i_0 = i_2 - i_3]$
 $\Rightarrow i_1 - 0.1i_2 + 0.1i_3 = 0$

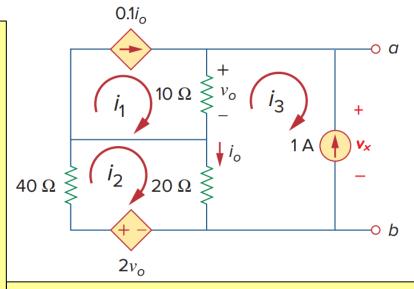
$$\Rightarrow i_1 - 0.1i_2 = 0.1 - - -(i) [i_3 = -1 A]$$

KVL at loop 2,

$$40i_2 + 20(i_2 - i_3) - 2v_0 = 0$$

$$\Rightarrow 40i_2 + 20(i_2 - i_3) - 2 \times 10(i_1 - i_3) = 0$$

$$\Rightarrow$$
 20 $i_1 - 60i_2 = 0$ -----(ii)



Solving (i) and (ii) yields,

$$i_1 = 0.103 A,$$

 $i_2 = 0.034 A.$

Let's find v_0 now!

Example 3: finding R_{Th} - 3/3

Now,

$$v_0 = 10 \times (i_1 - i_3)$$

 $\Rightarrow v_0 = 10 \times \{0.103 - (-1)\} = 11.03 V$
 $i_0 = i_2 - i_3$
 $\Rightarrow i_0 = 0.034 - (-1) = 1.034 A$

The voltage across the $20\,\Omega$ is $=20i_0=20.68\,V$.

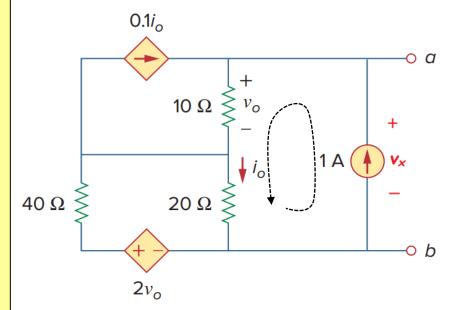
Applying KVL along the black dotted line,

$$-v_x + v_0 + 20.68 = 0$$

$$\Rightarrow v_x = 31.71 V \quad [v_0 = 11.03 V]$$

So,

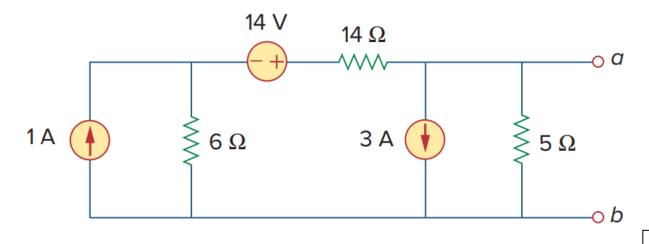
$$R_{Th} = \frac{v_x}{1} = 31.71 \,\Omega$$





Problem 1

Find the Thevenin equivalent at terminals a-b.

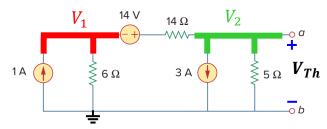


$$\Delta \mathbf{M} = \mathbf{N} : \mathbf{N}_{Th} = \mathbf{N} : \mathbf{R}_{Th} = \mathbf{A} \Omega$$



Solution to Problem 1

Finding V_{Th}



Let's use Nodal analysis to find the V_{Th} From the circuit,

$$V_2 = V_{Th}$$

Applying KCL at node 1,

$$\frac{V_1}{6} + \frac{V_1 - V_{Th} + 14}{14} - 1 = 0$$

$$\Rightarrow \frac{V_1}{6} + \frac{V_1}{14} - \frac{V_{Th}}{14} + 1 - 1 = 0$$

 $\Rightarrow \frac{5}{21}V_1 - \frac{1}{14}V_{Th} = 0 \quad(i)$

Applying KCL at node 2,

$$\frac{V_{Th}}{5} + \frac{V_{Th} - V_1 - 14}{14} + 3 = 0$$

$$\Rightarrow \frac{V_{Th}}{5} + \frac{V_{Th}}{14} - \frac{V_1}{14} - 1 + 3 = 0$$

$$\Rightarrow -\frac{1}{14}V_1 + \frac{19}{70}V_{Th} = -2 \dots (ii)$$

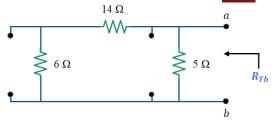
Solving (i) and (ii),

$$V_1 = -2.4 V$$

$$V_{Th} = -8 V$$

Finding R_{Th}

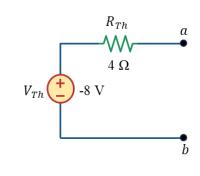
deactivate all first, let's Independent Sources. As there is no dependent sources, we simply use seriesparallel combination to find the equivalent resistance seen from the load terminal.



$$R_{Th} = 5 \mid\mid (14 + 6)$$

$$\Rightarrow R_{Th} = \frac{5 \times 20}{5 + 20} = 4 \Omega$$

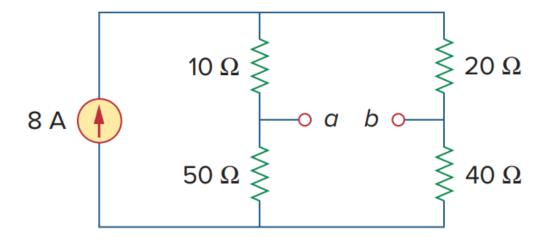
Thevenin equivalent circuit at terminals a-b





Problem 2

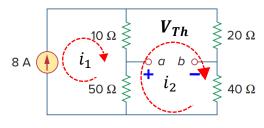
Find the Thevenin equivalent at terminals a - b.



 $\Omega \mathbf{Z} \cdot \mathbf{Z} \mathbf{Z} = A \mathbf{V} \cdot \mathbf{R}_{Th} = \mathbf{Z} \mathbf{Z} \cdot \mathbf{Z} \mathbf{Z}$



Finding V_{Th}



Let's use mesh analysis to find the V_{Th} From the circuit,

$$V_{ab} = V_{Th}$$

Applying KVL at mesh 1,

$$i_1 = 8 A$$
(i)

Applying KVL at mesh 2,

$$50(i_2 - i_1) + 10(i_2 - i_1) + 20i_2 + 40i_2 = 0$$

$$\Rightarrow 50i_2 - 50i_1 + 10i_2 - 10i_1 + 20i_2 + 40i_2 = 0$$

$$\Rightarrow -60i_1 + 120i_2 = 0 \dots (ii)$$

Solving (i) and (ii),

$$i_1 = 8 A$$
$$i_2 = 4 A$$

Now,

$$V_a = 50(i_1 - i_2) = 50(8 - 4) = 200 V$$

$$V_b = 40i_2 = 40 \times 4 = 160 V$$

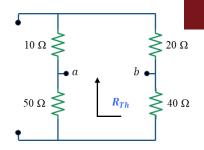
$$V_{Th} = V_{ab} = V_a - V_b$$

$$\Rightarrow V_{Th} = 200 - 160$$

$$\Rightarrow V_{Th} = 40 V$$

Finding R_{Th}

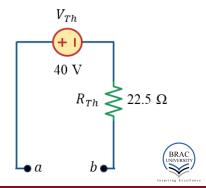
first. let's deactivate all Independent Sources. As there is no dependent sources, we simply use seriesparallel combination to find the equivalent resistance seen from the load terminal.



$$R_{Th} = (50 + 40) \mid\mid (10 + 20)$$

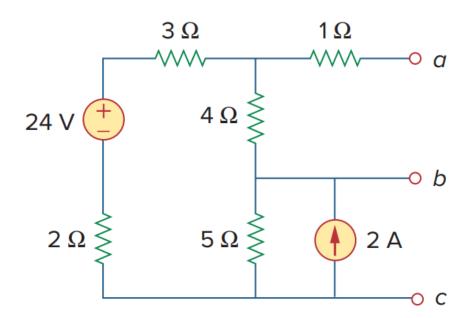
$$\Rightarrow R_{Th} = \frac{90 \times 30}{90 + 30} = 22.5 \,\Omega$$

Thevenin equivalent circuit at terminals a-b



Problem 3

Find the Thevenin equivalent as seen from terminals (i) a - b and (ii) b - c.

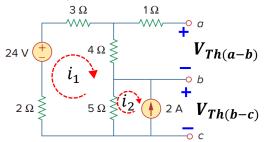


<u>Ans</u>: (i) $V_{Th} = 4 V$; $R_{Th} = 3.857 \Omega$; $(ii) V_{Th} = 15 V; R_{Th} = 3.214 \Omega;$



Solution to Problem 3

Finding V_{Th} at terminal a-b and b-c



Let's use mesh analysis to find the V_{Th} From the circuit,

$$i_2 = -2 A$$

Applying KVL at mesh 1,

$$2i_1 - 24 + 3i_1 + 4i_1 + 5(i_1 - i_2) = 0$$

$$\Rightarrow 2i_1 - 24 + 3i_1 + 4i_1 + 5(i_1 - (-2)) = 0$$

$$\Rightarrow 2i_1 - 24 + 3i_1 + 4i_1 + 5i_1 + 10 = 0$$

$$\Rightarrow i_1 = 1 A$$

Here $V_{Th(a-b)}$ is actually the voltage drop across the 4 Ω (Since no current flows through the 1 Ω)

Now,

$$V_{Th(a-b)} = V_{4\Omega} = 4i_1 = 4 \times 1 = 4 V$$

Here $V_{Th(b-c)}$ is actually the voltage drop across the 5 Ω

Now.

$$V_{Th(b-c)} = V_{5\Omega}$$

$$\Rightarrow V_{Th(b-c)} = 5(i_1 - i_2)$$

$$\Rightarrow V_{Th(b-c)} = 5(1 - (-2))$$

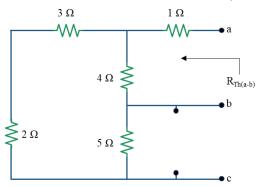
$$\Rightarrow V_{Th(b-c)} = 15 V$$

Finding R_{Th} at terminal a-b and b-c

At first, let's deactivate all the Independent Sources. As there is no dependent sources, we simply use series-parallel combination to find the equivalent resistance seen from the load terminal.



Solution to Problem 3 (Continued)



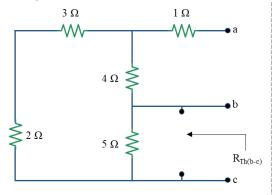
$$R_{Th(a-b)} = 1 + (4 || (3 + 2 + 5))$$

$$\Rightarrow R_{Th(a-b)} = 1 + (4 \mid\mid 10)$$

$$\Rightarrow R_{Th(a-b)} = 1 + \frac{4 \times 10}{4 + 10}$$

$$\Rightarrow R_{Th(a-b)} = 1 + 2.857$$

$$\Rightarrow R_{Th(a-b)} = 3.857 \Omega$$



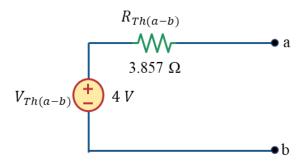
$$R_{Th(b-c)} = (5 || 2 + 3 + 4))$$

$$\Rightarrow R_{Th(b-c)} = (5 \mid\mid 9)$$

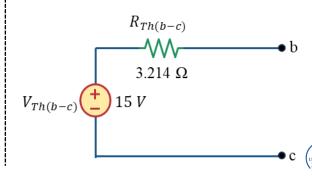
$$\Rightarrow R_{Th(b-c)} = \frac{5 \times 9}{5+9}$$

$$\Rightarrow R_{Th(b-c)} = 3.214 \Omega$$

Thevenin equivalent circuit at terminals a–b

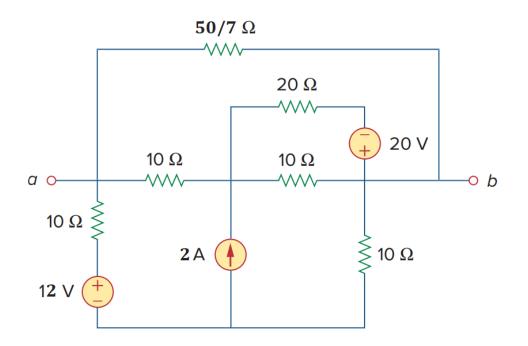


Thevenin equivalent circuit at terminals a-b



Problem 4

Find the Thevenin equivalent at terminals a-b.

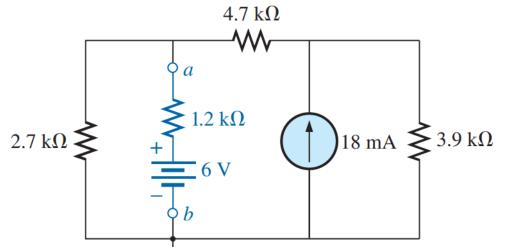


Ans: $V_{Th} = 0 V$; $R_{Th} = 4 \Omega$



Problem 5

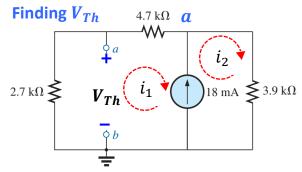
- i. Find the Thevenin equivalent circuit for the portions of the network below external to points a and b.
- ii. Redraw the network with the Thevenin circuit in place and find the current through the resistor.



Ans: (i) $V_{Th} = 16.77 V$; $R_{Th} = 2.054 k\Omega$; (ii) $\pm 3.31 A$



Solution to Problem 5



Let's use mesh analysis to find the V_{Th} From the circuit,

$$V_{ab} = V_{Th}$$

Applying KVL at supermesh,

$$2.7i_1 + 4.7i_1 + 3.9i_2 = 0$$

$$\Rightarrow 7.4i_1 + 3.9i_2 = 0$$
(i)

Applying KCL at node a,

$$i_1 + 18 = i_2$$

$$\Rightarrow i_1 - i_2 = -18$$
 (ii)

Solving (i) and (ii),

$$i_1 = -6.21 A$$
 $i_2 = 11.78 A$

Now.

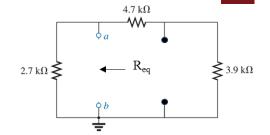
$$V_{Th} = -(i_1 \times 2.7)$$

$$\Rightarrow V_{Th} = -((-6.21) \times 2.7)$$

$$\Rightarrow V_{Th} = 16.76 V$$

Finding R_{Th}

first, let's deactivate all the Independent Sources. As there is no dependent sources, we simply use series-parallel combination to find the equivalent resistance seen from the load terminal.



$$R_{Th} = 2.7 \mid\mid (4.7 + 3.9)$$

$$\Rightarrow R_{Th} = 2.7 \mid\mid 8.6$$

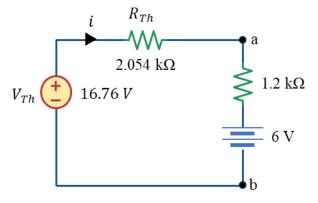
$$\Rightarrow R_{Th} = \frac{2.7 \times 8.6}{2.7 + 8.6} = 2.054 \text{ k}\Omega$$

Go to the next page



Solution to Problem 5 (Continued)

Thevenin equivalent circuit at terminals a–b



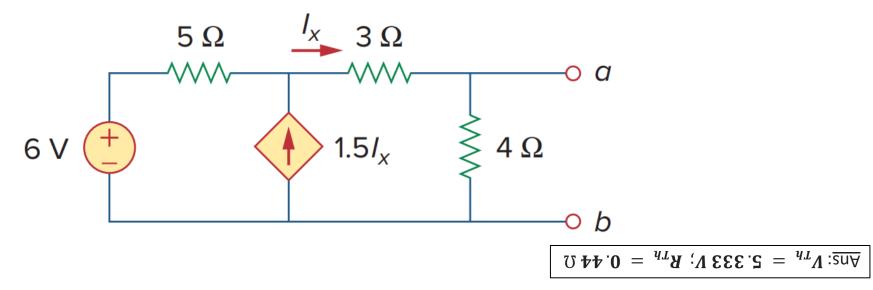
To find the current through the resistor, let us apply KVL in the circuit

$$-16.75 + 2.054i + 1.2i + 6 = 0$$

 $\Rightarrow i = 3.31 \, mA$

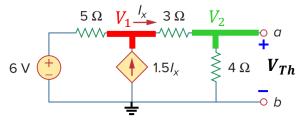


• Find the Thevenin equivalent circuit of the circuit to the left of the terminals.





Finding V_{Th}



Let's use Nodal analysis to find the V_{Th} From the circuit,

$$V_2 = V_{Th}$$

$$I_{x} = \frac{V_1 - V_{Th}}{3}$$

Applying KCL at node 1,

$$\frac{V_1 - 6}{5} + \frac{V_1 - V_{Th}}{3} - 1.5I_{\chi} = 0$$

$$\Rightarrow \frac{V_1 - 6}{5} + \frac{V_1 - V_{Th}}{3} - 1.5\frac{V_1 - V_{Th}}{3} = 0$$

$$\Rightarrow \frac{V_1}{5} - \frac{6}{5} + \frac{V_1}{3} - \frac{V_{Th}}{3} - \frac{V_1}{2} + \frac{V_{Th}}{2} = 0$$
$$\Rightarrow \frac{1}{30} V_a + \frac{1}{6} V_{Th} = \frac{6}{5} \quad \dots \dots (i)$$

Applying KCL at node 2,

$$\frac{V_{Th}}{4} + \frac{V_{Th} - V_1}{3} = 0$$

$$\Rightarrow \frac{V_{Th}}{4} + \frac{V_{Th}}{3} - \frac{V_1}{3} = 0$$

$$\Rightarrow -\frac{V_1}{3} + \frac{7}{12}V_{Th} = 0 \dots (ii)$$

Solving (i) and (ii),

$$V_1 = 9.33 V$$
$$V_{Th} = 5.33 V$$

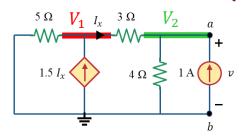
Finding R_{Th}

At first, let's deactivate all the Independent Sources. As there is dependent source. We need to use a known voltage source across the terminal a-b and find out the current through the node a-b. Alternatively, we can use a known current source across the terminal a-b and find out the voltage across the terminal.

Let's do the second type and apply 1 A at terminal a-b



Solution to Problem 6 (Continued)



We need to find the voltage vLet's use Nodal analysis to find the v

$$V_2 = v$$

$$I_x = \frac{V_1 - v}{3}$$

Applying KCL at node 1,

$$\frac{V_1}{5} + \frac{V_1 - v}{3} - 1.5I_x = 0$$

$$\Rightarrow \frac{V_1}{5} + \frac{V_1 - v}{3} - 1.5\frac{V_1 - v}{3} = 0$$

Applying KCL at node 2,

$$\frac{v}{4} + \frac{v - V_1}{3} - 1 = 0$$

$$\Rightarrow \frac{v}{4} + \frac{v}{2} - \frac{V_1}{2} - 1 = 0$$

$$\Rightarrow -\frac{V_1}{3} + \frac{7}{12}V_{Th} = 1$$
(iv)

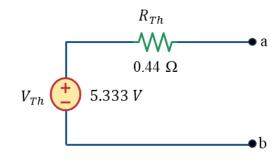
Solving (iii) and (iv),

$$V_1 = -2.22 V$$

$$v = 0.44 V$$

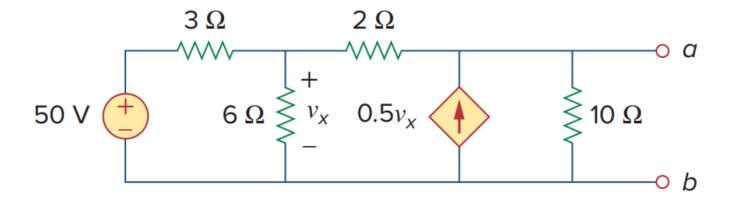
$$R_{Th} = \frac{v}{1 A} = \frac{0.44}{1} = 0.44 \Omega$$

Thevenin equivalent circuit at terminals a–b





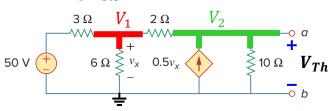
Obtain the Thevenin equivalent circuit at terminals a-b.



Ans: $V_{Th} = 166.67 V$; $R_{Th} = 10 \Omega$



Finding V_{Th}



Let's use Nodal analysis to find the V_{Th} From the circuit,

$$V_2 = V_{Th}$$
$$v_x = V_1$$

Applying KCL at node 1,

$$\frac{V_1 - 50}{3} + \frac{V_1}{6} + \frac{V_1 - V_{Th}}{2} = 0$$

$$\Rightarrow \frac{V_1}{3} - \frac{50}{3} + \frac{V_1}{6} + \frac{V_1}{2} - \frac{V_{Th}}{2} = 0$$

$$\Rightarrow V_1 - \frac{1}{2}V_{Th} = \frac{50}{3} \quad \dots \dots \dots (i)$$

Applying KCL at node 2,

Solving (i) and (ii),

$$V_1 = 100 V$$

 $V_{Th} = 166.67 V$

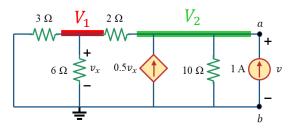
Finding R_{Th}

At first, let's deactivate all the Independent Sources. As there is dependent source. We need to use a known voltage source across the terminal a-b and find out the current through the node a-b. Alternatively, we can use a known current source across the terminal a-b and find out the voltage across the terminal.

Let's do the second type and apply 1 A at terminal a-b



Solution to Problem 7 (Continued)



We need to find the voltage v

Let's use Nodal analysis to find the v

$$V_2 = v$$
$$v_x = V_1$$

Applying KCL at node 1,

$$\frac{V_1}{3} + \frac{V_1}{6} + \frac{V_1 - v}{2} = 0$$

$$\Rightarrow \frac{V_1}{3} + \frac{V_1}{6} + \frac{V_1}{2} - \frac{v}{2} = 0$$

$$\Rightarrow V_1 - \frac{1}{2}v = 0 \quad \dots \dots \quad \text{(iii)}$$

Applying KCL at node 2,

$$\frac{v}{10} + \frac{v - V_1}{2} - 0.5v_x - 1 = 0$$

$$\Rightarrow \frac{v}{10} + \frac{v}{2} - \frac{V_1}{2} - 0.5V_1 - 1 = 0$$

$$\Rightarrow -V_1 + \frac{3}{5}v = 1 \dots (iv)$$

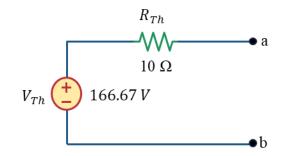
Solving (iii) and (iv),

$$V_1 = 5 V$$
$$v = 10 V$$

So,

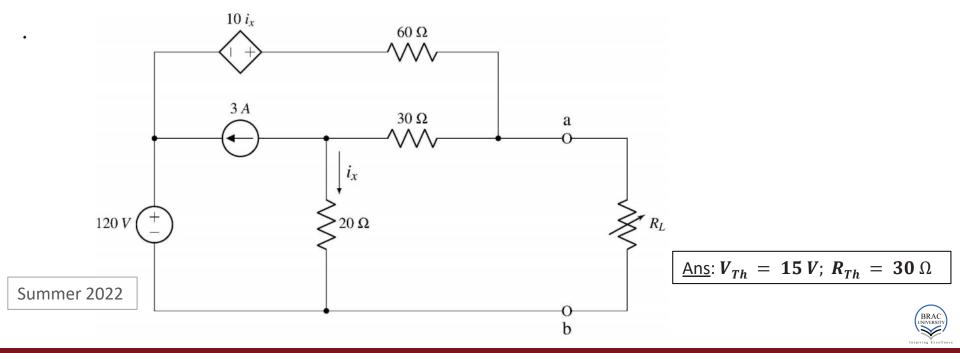
$$R_{Th} = \frac{v}{1 A} = \frac{10}{1} = 10 \Omega$$

Thevenin equivalent circuit at terminals a-b

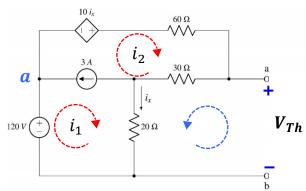




Obtain the Thevenin equivalent circuit at terminals a-b.



Finding V_{Th}



Let's use mesh analysis to find the V_{Th} From the circuit,

$$i_{x}=i_{1}$$

Applying KVL at supermesh,

$$-120 - 10i_x + 60i_2 + 30i_2 + 20i_1 = 0$$

$$\Rightarrow -120 - 10i_1 + 60i_2 + 30i_2 + 20i_1 = 0$$

$$\Rightarrow 10i_1 + 90i_2 = 120$$
(i)

Applying KCL at node a,

$$i_1 + 3 = i_2$$

 $\Rightarrow i_1 - i_2 = -3$ (ii)

Solving (i) and (ii),

$$i_1 = -1.5 A$$
 $i_2 = 1.5 A$

To find V_{Th} , let us apply KVL in the right mesh (Blue arrow)

$$-V_{Th} + 30i_2 + 20i_1 = 0$$

$$\Rightarrow -V_{Th} + 30 \times 1.5 + 20 \times (-1.5) = 0$$

$$\Rightarrow V_{Th} = 15 V$$

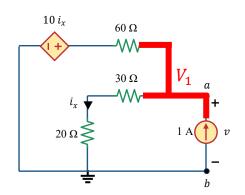
Finding R_{Th}

At first, let's deactivate all the Independent Sources. As there is dependent source. We need to use a known voltage source across the terminal a-b and find out the current through the node a-b. Alternatively, we can use a known current source across the terminal a-b and find out the voltage across the terminal.

Let's do the second type and apply 1 A at terminal a-b



Solution to Problem 8 (Continued)



Let's use Nodal analysis to find the vFrom the circuit,

$$V_1 = v$$

$$i_{x} = \frac{v}{50}$$

Applying KCL at node 1,

$$\frac{v}{50} + \frac{v - 10i_x}{60} - 1 = 0$$

$$\Rightarrow \frac{v}{50} + \frac{v}{60} - \frac{1}{6}i_x - 1 = 0$$

$$\Rightarrow \frac{v}{50} + \frac{v}{60} - \frac{1}{6} \frac{v}{50} - 1 = 0$$

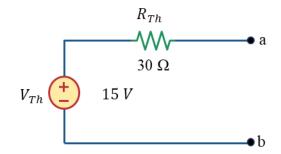
$$\Rightarrow \frac{v}{30} = 1$$

$$\Rightarrow v = 30$$

So,

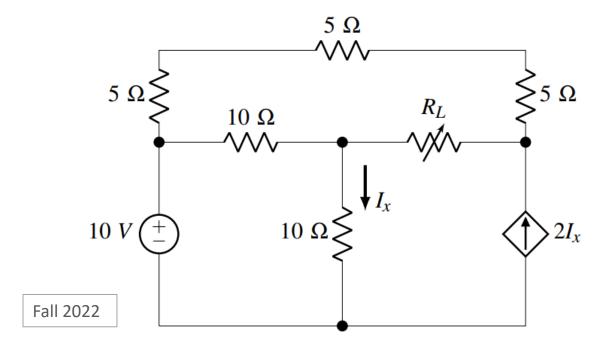
$$R_{Th} = \frac{v}{1.4} = \frac{30}{1} = 30 \Omega$$

Thevenin equivalent circuit at terminals a–b



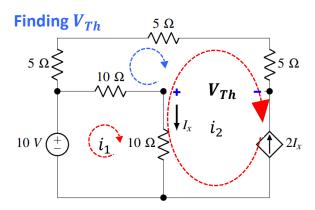


Obtain the Thevenin equivalent circuit at the load (R_L) terminals.



Ans: $V_{Th} = \pm 20 V$; $R_{Th} = 5 \Omega$





Let's use mesh analysis to find the V_{Th} From the circuit,

$$I_{x}=i_{1}-i_{2}$$

Applying KVL mesh 2,

$$i_2 = -2I_x$$

 $\Rightarrow i_2 = -2(i_1 - i_2)$
 $\Rightarrow 2i_1 - i_2 = 0$ (i)

Applying KVL mesh 1,

$$-10 + 10(i_1 - i_2) + 10(i_1 - i_2) = 0$$

$$\Rightarrow -10 + 20i_1 - 20i_2 = 0$$

$$\Rightarrow 20i_1 - 20i_2 = 10$$
(ii)

Solving (i) and (ii),

$$i_1 = -0.5 A$$

$$i_2 = -1 A$$

To find V_{Th} , let us apply KVL in the upper mesh (Blue arrow)

$$-V_{Th} + 10(i_2 - i_1) + 5i_2 + 5i_2 + 5i_2 = 0$$

$$\Rightarrow -V_{Th} + 10i_2 - 10i_1 + 5i_2 + 5i_2 + 5i_2 = 0$$

$$\Rightarrow V_{Th} = -10i_1 + 25i_2$$

$$\Rightarrow V_{Th} = -10 \times (-0.5) + 25 \times (-1)$$

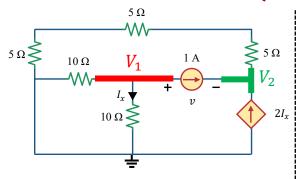
$$\Rightarrow V_{Th} = -20 V$$

Finding R_{Th}

At first, let's deactivate all the Independent Sources. As there is dependent source. We need to use a known voltage source across the terminal a-b and find out the current through the node a-b. Alternatively, we can use a known current source across the terminal a-b and find out the voltage across the terminal.

Let's do the second type and apply 1 A at terminal a-b

Solution to Problem 9 (Continued)



Let's use Nodal analysis to find the vFrom the circuit,

$$V_1 - V_2 = v$$

$$I_{x} = \frac{V_{1}}{10}$$

Applying KCL at node 1,

$$\frac{V_1}{10} + \frac{V_1}{10} + 1 = 0$$

$$\Rightarrow \frac{1}{5}V_1 = -1 \dots (iii)$$

Applying KCL at node 2,

Solving (iii) and (iv),

$$V_1 = -5 V$$

$$V_2 = 0 V$$

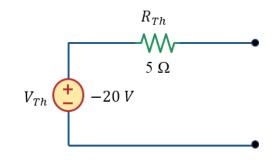
So,
$$v = V_1 - V_2 = -5 - 0 = -5 V$$

So,

$$R_{Th} = \frac{v}{1 A} = \frac{-5}{1} = 5 \Omega$$

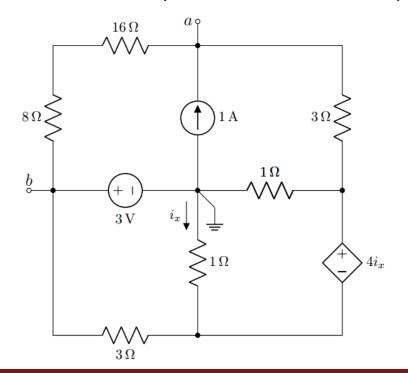
Ignoring the negative sign

Thevenin equivalent circuit at terminals a-b





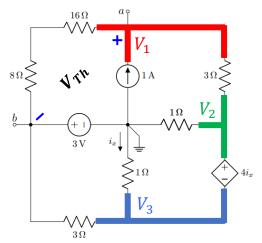
• Obtain the Thevenin equivalent circuit with respect to terminals a-b.



Ans: $V_{Th} = 3 V$; $R_{Th} = 4 \Omega$



Finding V_{Th}



Let's use Nodal analysis to find the V_{Th} From the circuit,

$$V_{Th} = V_1 - 3$$

$$i_{x}=-\frac{V_{3}}{1}$$

Applying KCL at node 1,

$$\frac{V_1 - 3}{24} + \frac{V_1 - V_2}{3} - 1 = 0$$

$$\Rightarrow \frac{V_1}{24} - \frac{3}{24} + \frac{V_1}{3} - \frac{V_2}{3} - 1 = 0$$

$$\Rightarrow \frac{3}{8}V_1 - \frac{1}{3}V_2 = \frac{9}{8} \quad \dots \dots \dots (i)$$

Applying KCL at supernode 2 and 3,

$$\frac{V_2 - V_1}{3} + \frac{V_2}{1} + \frac{V_3}{1} + \frac{V_3 - 3}{3} = 0$$

$$\Rightarrow \frac{V_2}{3} - \frac{V_1}{3} + \frac{V_2}{1} + \frac{V_3}{1} + \frac{V_3}{3} - 1 = 0$$

$$\Rightarrow -\frac{1}{3}V_1 + \frac{4}{3}V_2 + \frac{4}{3}V_3 = 1 \quad (ii)$$

Applying KVL at supernode 2 and 3,

$$V_2 - V_3 = 4i_x$$

$$\Rightarrow V_2 - V_3 = 4(-\frac{V_3}{1})$$

$$\Rightarrow V_2 + 3V_3 = 0$$
(iii)

Solving (i), (ii) and (iii),

$$V_1 = 6 V$$

 $V_2 = 3.375 V$
 $V_3 = -1.125 V$

So, $V_{Th} = V_1 - 3$

$$\Rightarrow V_{Th} = 6 - 3$$

$$\Rightarrow V_{Th} = 3 V$$

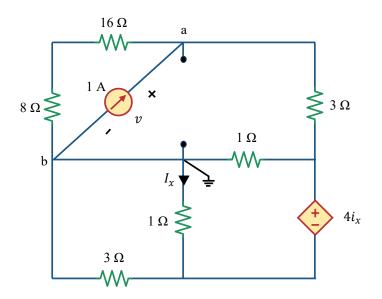


Solution to Problem 10 (Continued)

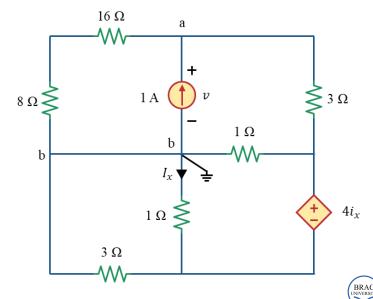
Finding R_{Th}

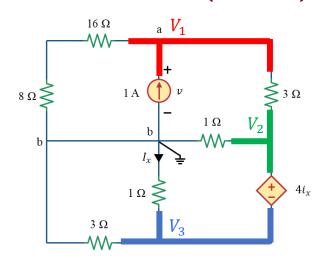
At first, let's deactivate all the Independent Sources. As there is dependent source, we need to use a known current source across the terminal a-b and find out the voltage across the terminal.

Let's do the second type and apply $1\,A$ at terminal a-b



Rearranging the circuit by just moving the 1A current source





Let's use Nodal analysis to find the vFrom the circuit,

$$v = V_1$$

$$i_x = -\frac{V_3}{1}$$

Applying KCL at node 1,

$$\frac{v}{24} + \frac{v - V_2}{3} - 1 = 0$$

$$\Rightarrow \frac{v}{24} + \frac{v}{3} - \frac{V_2}{3} - 1 = 0$$

$$\Rightarrow \frac{3}{8}v - \frac{1}{3}V_2 = 1 \dots \text{(iv)}$$

Applying KCL at supernode 2 and 3,

$$\frac{V_2 - v}{3} + \frac{V_2}{1} + \frac{V_3}{1} + \frac{V_3}{3} = 0$$

$$\Rightarrow \frac{V_2}{3} - \frac{v}{3} + \frac{V_2}{1} + \frac{V_3}{1} + \frac{V_3}{3} = 0$$

$$\Rightarrow -\frac{1}{3}v + \frac{4}{3}V_2 + \frac{4}{3}V_3 = 0 \dots (v)$$

Applying KVL at supernode 2 and 3,

$$V_2 - V_3 = 4i_x$$

Solving (iv), (v) and (vi),

$$V_1 = 4 V$$

$$V_2 = 1.5 V$$

$$V_3 = -0.5 V$$

So,

$$R_{Th} = \frac{v}{1A} = \frac{4}{1} = 4 \Omega$$

$$V_{Th} \stackrel{P}{\longrightarrow} 3V$$

