

17/8/25

Q51

Limitations

2 terminal can't be controlled

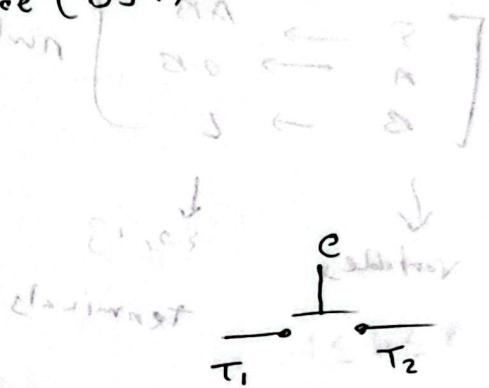
3 terminal device:

i. Linear 3 terminal device (switch)

ii. Non Linear 3 terminal device (BJT, MosFet)

AA
BB
CC
DD
EE
FF
G
H
I
J
K
L
M
N
O
P
Q
R
S
T
U
V
W
X
Y
Z
c → control

switch



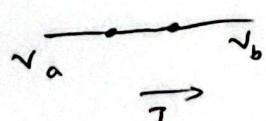
OFF = 0 = False

ON = 1 = True

c = 1 (ON)

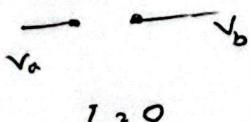
c = 0 (OFF)

c = 1;

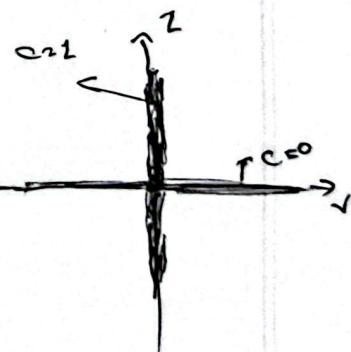


$$V = V_a - V_b = 0$$

c = 0;



$$I = 0$$



BJT

start T_{th} = instant

1. Bipolar Junction Transistor (current controlled switch)

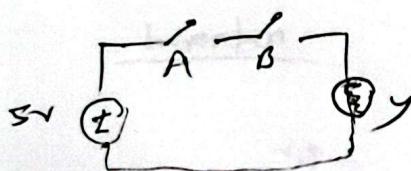
(instant) start T_{th}

2. Mosfet \rightarrow Metal oxide semiconductor field effect Effect
Transistor (voltage controlled switch)



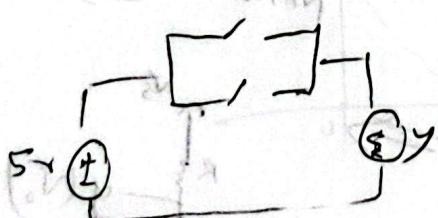
Logic gate

$I = V \propto \alpha A$



A	B	y
0	0	0
1	0	0
0	1	0
1	1	1

AND \rightarrow series



A	B	y
0	0	0
1	0	1
0	1	1
1	1	1

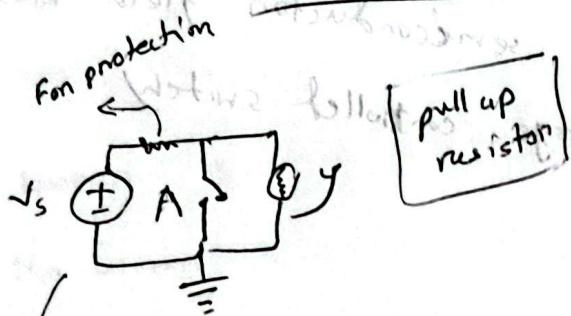
OR \rightarrow parallel

Inverter \rightarrow NOT Gate

EDA

(positive logic) not gate mit neg. output

Not Gate (Inverter)

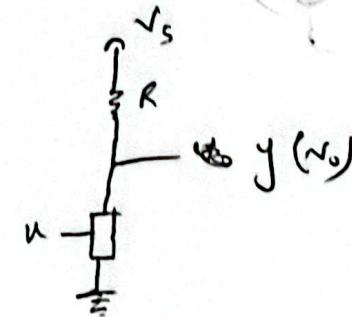


$$Y = \bar{A}$$

$$A = 0 \Rightarrow Y = 1$$

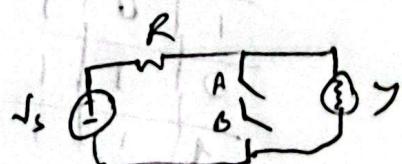
$$A = 1 \Rightarrow Y = 0$$

0	0	0
0	0	1
0	1	0

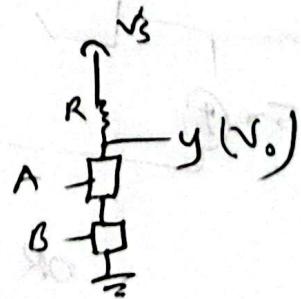


$$Y = \bar{A} \quad \text{2 inputs} \leftarrow \text{and}$$

0	0	0
0	0	1
0	1	0

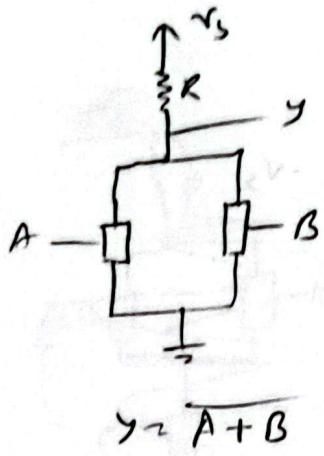


NAND - 2 \rightarrow n. - of input



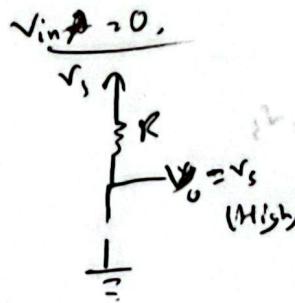
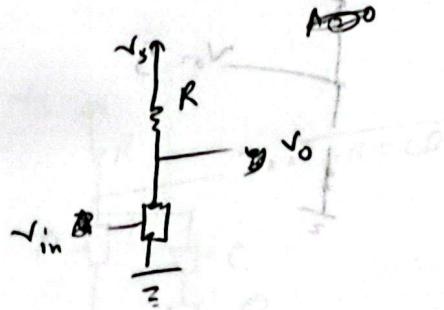
$$Y = \overline{AB} \quad \text{NAND} \leftarrow \text{and}$$

NOR - 2

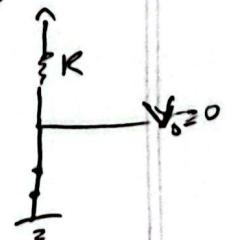


Q17A

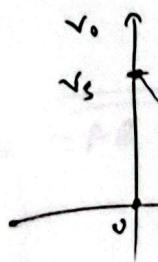
Inverten



$v_{in} = 1$

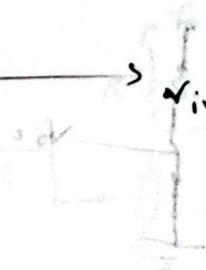


VTC

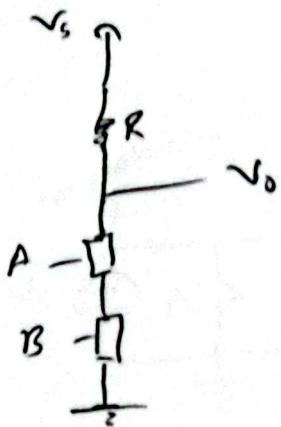


$v_{in} = 0, 1$

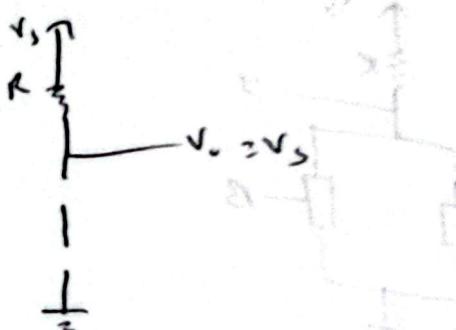
$\times \times$



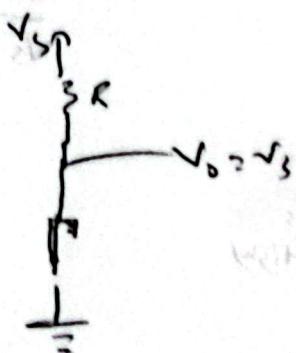
NAND - 2



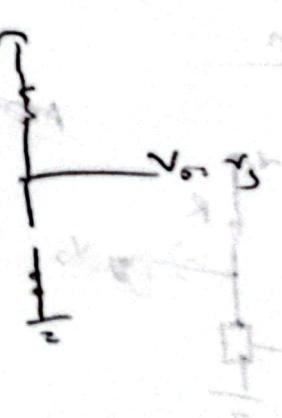
$A=0, B=0$



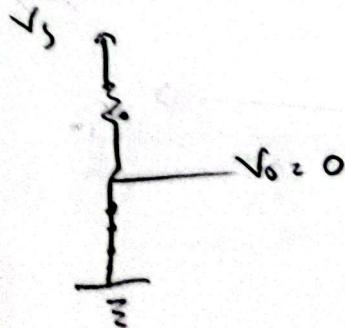
$A=1, B=0$



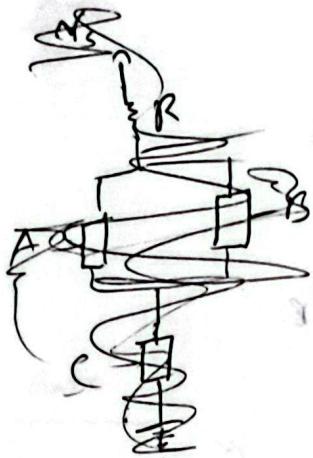
$A=0, B=1$



$A=1, B=1$

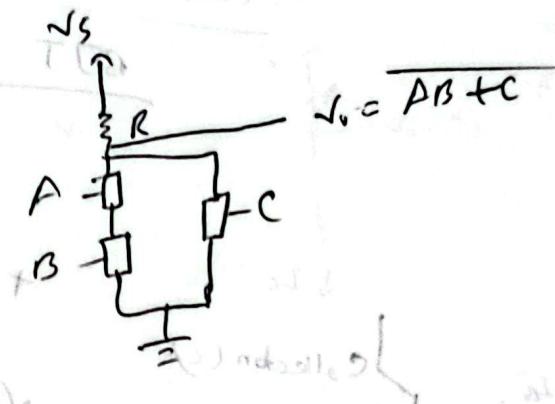


$f = \overline{AB} + C$



active behavior form

PIV

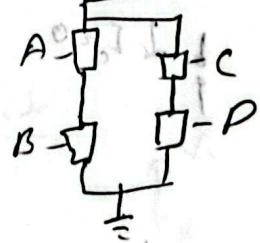


$f = \overline{AB} + CD$

no TCA to below (below)

(TCA to below not true)

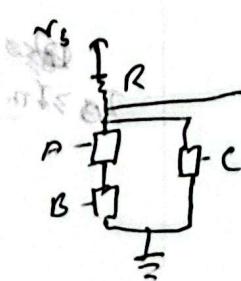
$$V_o = \overline{AB} + CD$$



no TCA

$f = AB + C = \overline{AB} + C$

or B

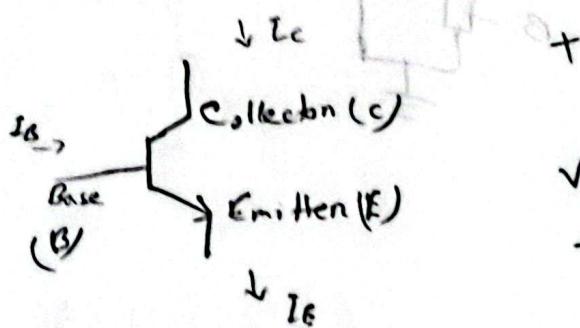


at f = BAC

$$V_o = \overline{AB} + C = AB + C$$

current controlled switch

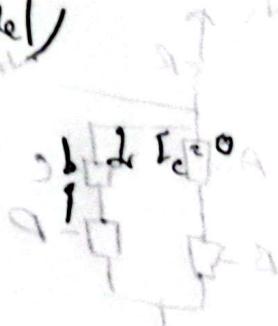
BJT



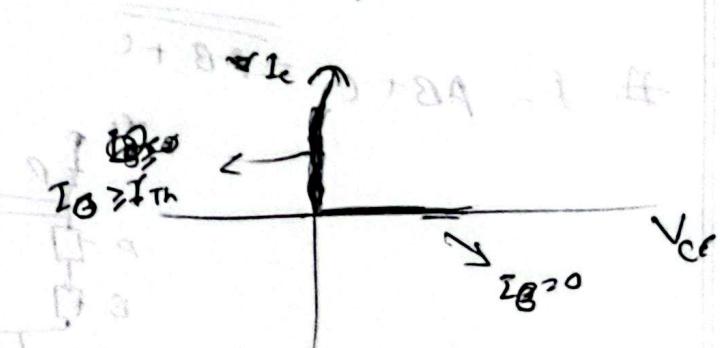
$$V_{CE} = V_C - V_E$$

Ideal model of BJT or
(switch model of BJT)
(s model)

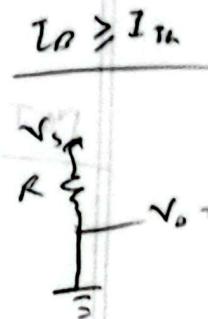
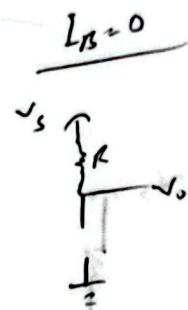
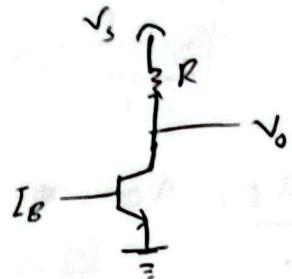
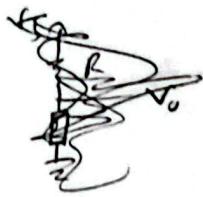
$I_B = 0$ BJT (OFF)



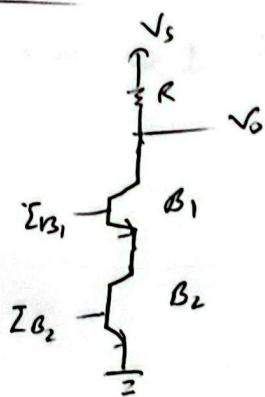
$I_B \geq I_{th}$ BJT (ON) $\{ V_{CE} = 0$



NOT Gate

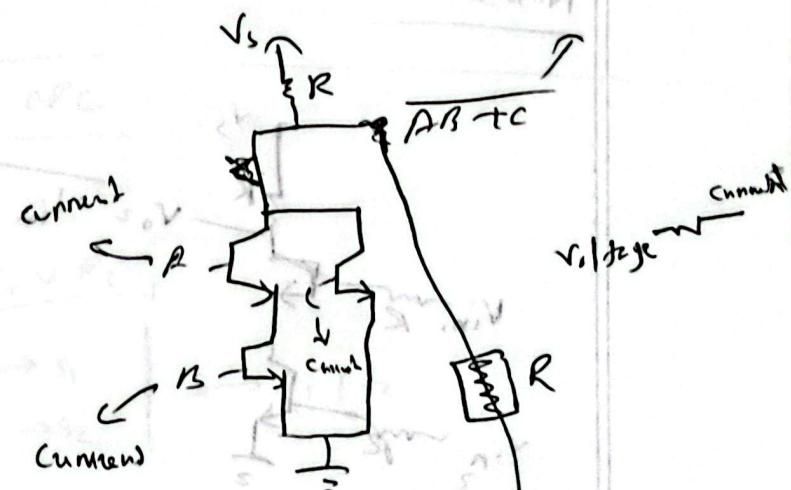


NAND Gate

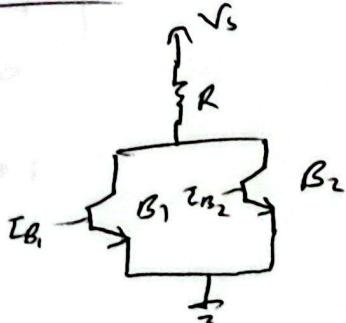


$$\# L = \overline{AB + C}$$

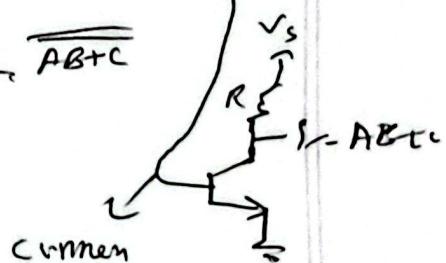
QMAN Voltage



NOR Gate

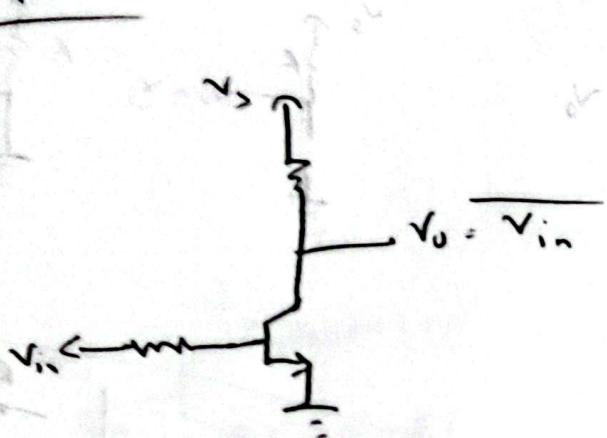


$$\# L = AB + C = \overline{\overline{AB} + C}$$



voltage controlled switch with BJT

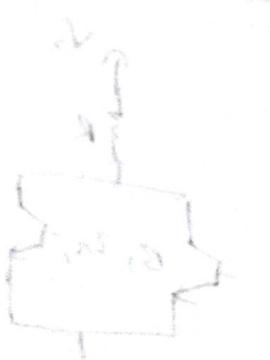
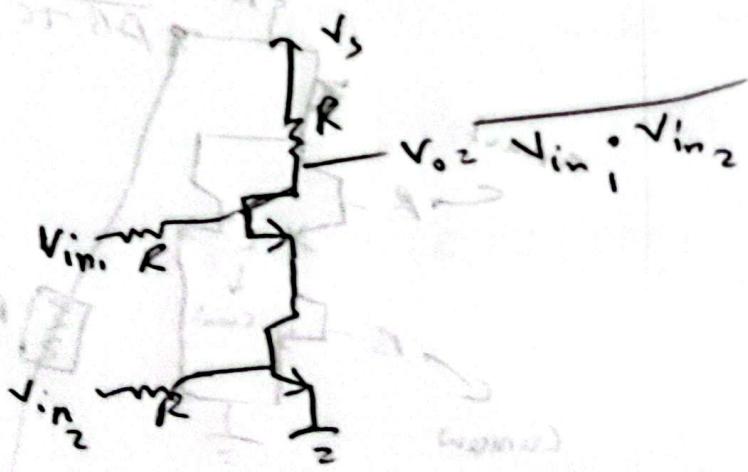
NOT



NOR



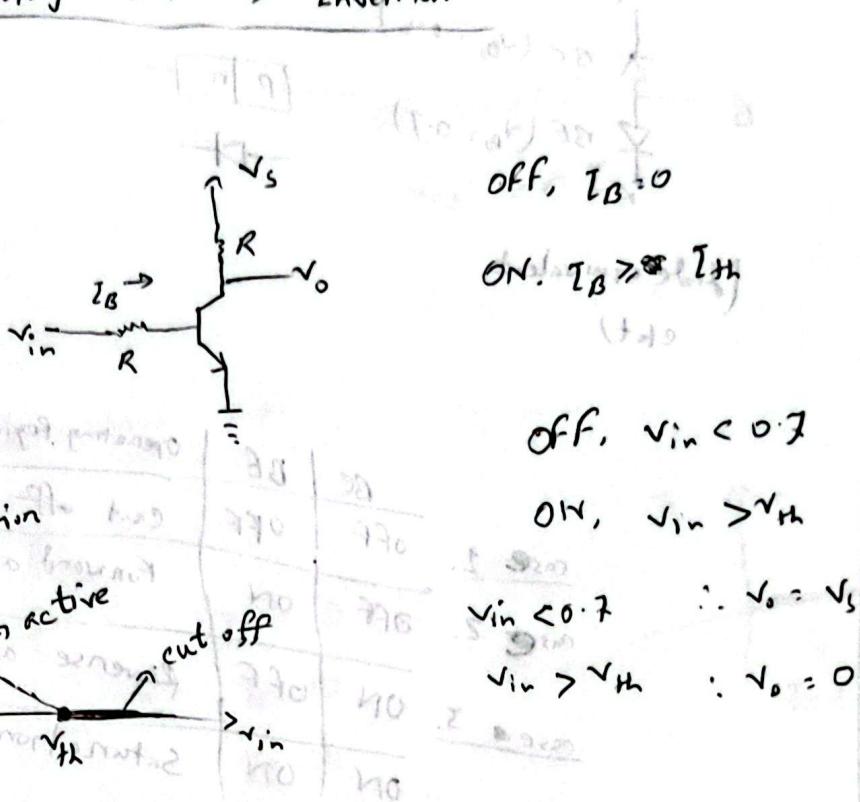
NAND



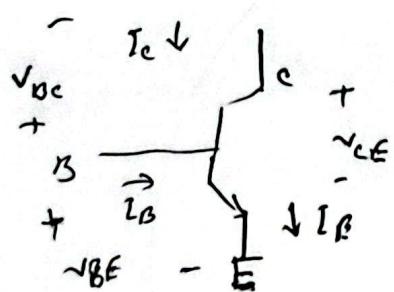
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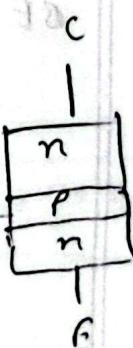
VTC of BJT (Voltage controlled) Invention:



Over simplified operation of BJT

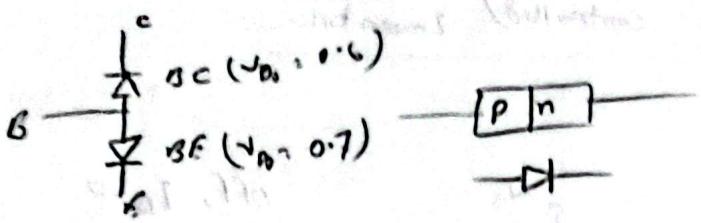


$$v_{CE} = v_C - v_E$$



$$I_E = I_B + I_C$$

Base \rightarrow less width
Emitter \rightarrow highly doped



(Node equivalent
etc)

	BE	BE	Operating Region
case 1.	OFF	OFF	cut off
case 2.	OFF	ON	Forward active/active
case 3.	ON	OFF	reverse active
	ON	ON	Saturation (Rare case)

$$V_{BC} \rightarrow OFF, \quad V_{BC} \leq 0.6$$

$$V_{BE} \rightarrow OFF, \quad V_{BE} \leq 0.7$$

$$V_{BC} = V_B - V_C$$

$$= V_B + V_E - V_E - V_C$$

$$= (V_B - V_E) - (V_C - V_E)$$

$$\approx V_{BE} - V_{CE}$$

$$\therefore V_{BE} - V_{CE} \leq 0.6 \Rightarrow V_C \geq V_{BE} - 0.6$$

~~case - 1~~

case - 2

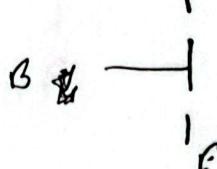
(cut off) $BC \Rightarrow OFF$.

$$V_{CE} \geq V_{BE} - 0.6$$

$BE \Rightarrow OFF$

$$V_{BE} \leq 0.7$$

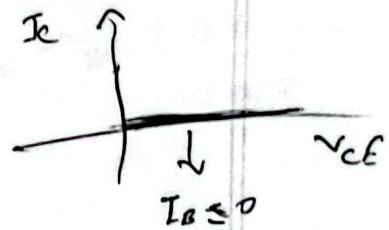
diode equivalent ckt



$$I_B = 0$$

$$I_C = 0$$

$$I_E = 0$$



$$V_{CE} = V_{BE} - 0.6 \approx 0.7 - 0.6 = 0.1$$

case - 2

(Forward active)

$BC \Rightarrow OFF$

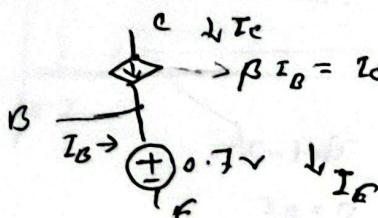
$BE \Rightarrow ON$

$$I_{BE} > 0$$

$$V_{CE} \geq V_{BE} - 0.6$$

$$\therefore V_{CE} = 0.7 - 0.6 = 0.1$$

diode equivalent ckt



$$I_C \propto I_B$$

$$\Rightarrow I_C = \beta I_B$$

$\beta \Rightarrow 50 \text{ to } 200$

$$I_C = I_B + I_E$$

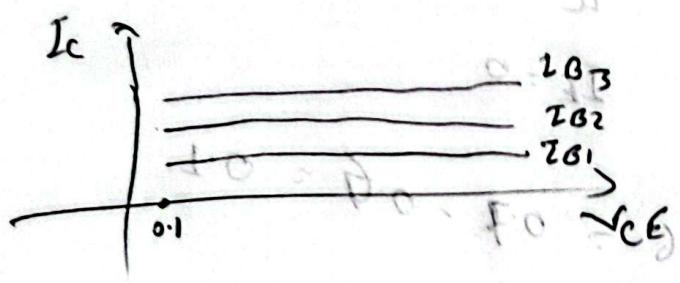
$$\alpha \rightarrow 0.9999.$$

$$= \frac{I_C}{\beta} + I_C$$

$$= I_C \left(\frac{1}{\beta} + 1 \right)$$

$$= I_C \left(\frac{1+\beta}{\beta} \right)$$

$$I_C = \left(\frac{\beta}{1+\beta} \right) I_E = \alpha I_E - \left[\alpha^2 \frac{\beta}{1+\beta} \right]$$

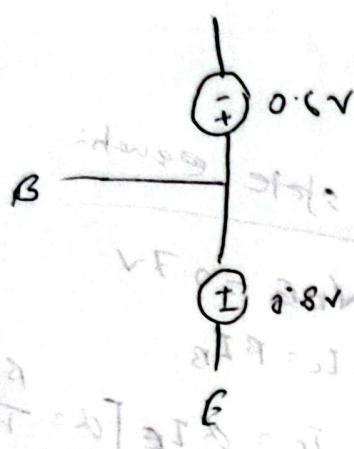


$$I_{B_3} > I_{B_2} > I_{B_1}$$

case-3:
(saturation)

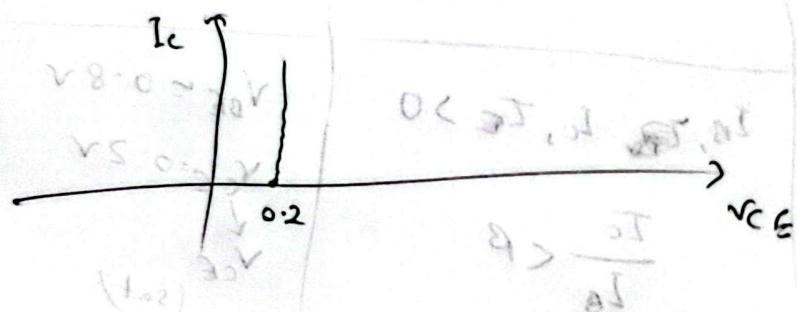
$BC \rightarrow ON$

$BE \rightarrow ON$

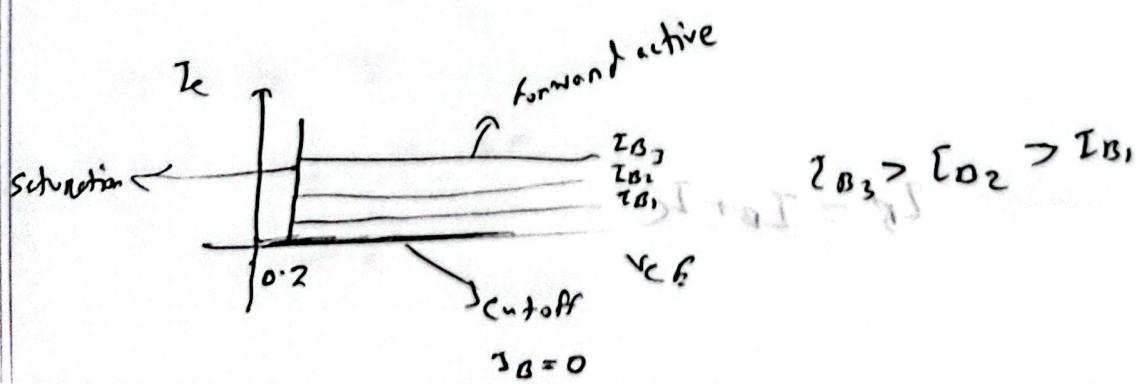


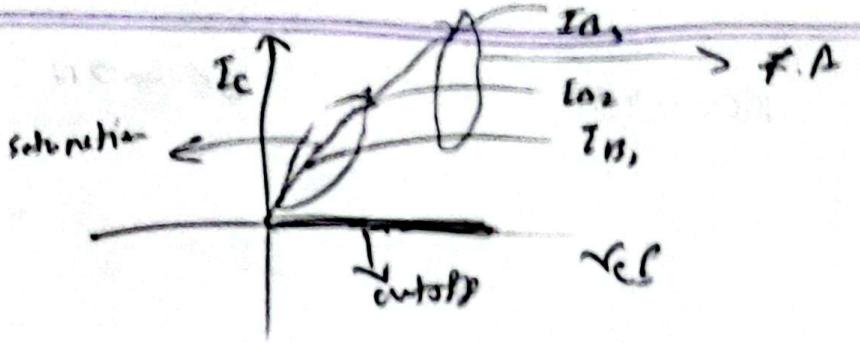
$$V_{BE} = 0.8V$$

$$\sqrt{V_{BC}} = 0.6V \quad \text{and} \quad \frac{\sqrt{V_{BE}} - \sqrt{V_{BC}}}{\sqrt{V_{BC}}} = 0.2$$



$$\text{Over simplified } \frac{I_C}{V_{CE}}$$

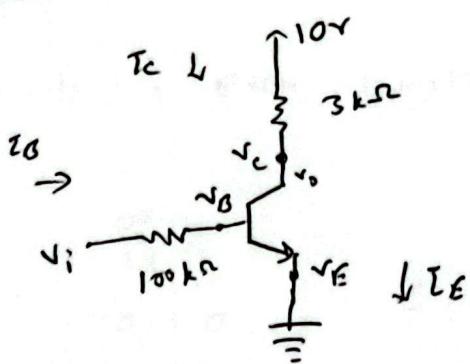




<u>Operating Region</u>	<u>Condition</u>	<u>State equations</u>
forward Active	$V_B > V_{B_0}, I_E > 0$ $V_{C_E} > 0.2V$	$V_{BE} = 0.7V$ $I_E = \beta I_B$ $I_C = \alpha I_E [\alpha = \frac{\beta}{1 + \beta}]$
saturation	$I_B, V_B, I_E, I_C > 0$ $\frac{I_C}{I_B} < \beta$	$V_{BE} \approx 0.8V$ $V_{C_E} \approx 0.2V$ $V_{C_E} (\text{sat})$
cutoff	$V_{BE} \leq 0.7V$ $V_{BC} \leq 0.6V$	$I_B = I_C = I_E = 0$

$$I_B = I_B + I_C$$

E'n-1:



find v_o . when $v_i = 2V$, $\beta = 100$.

sol:

Assuming,

$\beta_1 \rightarrow$ forward active

$$v_{BE} = 0.7$$

$$I_{C1} = \beta I_B$$

$$\alpha = \frac{\beta}{1 + \beta}$$

$$\sqrt{V_E} = V_B - V_E$$

$$\Rightarrow 0.7 = \sqrt{B} - 0.7^2$$

$$\therefore \sqrt{B} = 0.7^2 + 0.7 = 2.0V$$

Pleas note that $v_o = 2V$

$$\frac{2V - v_o}{3k\Omega} = \frac{2V}{3k\Omega}$$

$$\frac{2V - v_o}{3k\Omega} = 0.01$$

$$2V - v_o = 0.03V$$

$$v_o = 2V - 0.03V = 1.97V$$

$$v_o = 1.97V$$

Ohms law on $100\text{k}\Omega$,

$$I_B = \frac{V_{in} - V_B}{100}$$

$$\therefore \frac{1 - 0.7}{100}$$

$$= 0.003 \text{ mA}$$

$$I_C = \beta I_B \cdot 100 \times 0.003 = 0.3 \text{ mA}$$

$$I_E = I_B + I_C = 0.003 + 0.3 = 0.303 \text{ mA}$$

Ohms law on 3Ω ,

$$\therefore I_C = \frac{10 - V_C}{3}$$

$$\Rightarrow 0.3 = \frac{10 - V_C}{3}$$

$$\therefore V_C = 9.1 \text{ V}$$

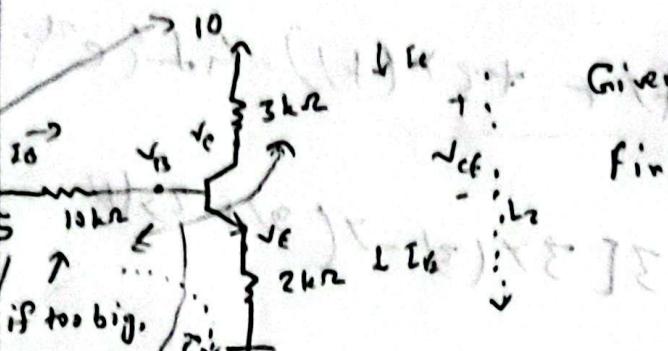
$$V_{CE} = V_C - V_E = 9.1 - 0 = 9.1 \text{ V}$$

Verification

$$I_C, I_B, I_E > 0 \quad \left. \right\} \text{connected}$$

$$V_{CE} = 9.1 > 0.2 \text{ V} \quad \text{Assumption}$$

$$V_o = V_C = 9.1 \text{ V}$$

E_{H2} :Given $\beta = 100$ Find I_B, I_C, I_E Ans:Assumption: $B \rightarrow$ Active

$$V_{BE} = 0.7V$$

$$I_C < \beta I_B$$

$$I_C < \alpha I_E$$

$$\therefore \frac{\beta}{1+\beta} = \frac{100}{101}$$

$$I_E = I_B + I_C$$

need to show $I_B, I_C, I_E > 0$

$$V_{CE} > 0.2$$

KVL along L_1 ,

$$5 - 0 = 10I_B + V_{BE} + 2I_E$$

$$\Rightarrow 5 = 10I_B + 0.7 + 2I_E$$

$$I_C = \beta I_B$$

$$\therefore I_E = \beta I_B$$

$$\therefore I_E = \frac{\beta}{\alpha} I_B$$

$$\Rightarrow 5 = 10I_B + 0.7 + 2 \times \frac{\beta}{\alpha} I_B$$

$$\therefore I_B = 0.02 \text{ mA}$$

$$I_C = 2 \text{ mA}$$

$$I_E = 0.02 + 2 \\ \approx 2.02$$

KVL along L_2 ,

$$10 - 0 = 3I_C + V_{CE} + 2I_E \Rightarrow 10 = 3 \times 2 + V_{CE} + 2 \times 2.02 \Rightarrow V_{CE} = -0.04$$

Verification:

$$I_B, I_C, I_E > 0$$

$$V_{CE} = -0.04 \neq 0.2$$

Assumption wrong.

Assumption-2:

$B \rightarrow$ saturation

$$V_{BE} = 0.8$$

$$V_{CE} = 0.2$$

Now need to show

$$\frac{I_C}{I_B} < \beta$$

KVL along L_1 ,

$$10 - 0 = 10I_B + V_{BE} + 2I_E$$

$$10I_B + 2I_E - 4.2 = 0 \dots (i)$$

KVL along L_1 ,

$$10 - 0 = 3I_C + V_{CE} + 2I_E$$

$$3I_C + 2I_E - 9.8 = 0 \dots (ii)$$

$$I_E = I_B + I_C$$

$$I_B + I_C - I_E = 0 \dots (iii)$$

$$I_B = 0.025$$

$$I_C = 1.95$$

$$I_E = 1.975$$

$$\frac{I_C}{I_B} = 78 < \beta = 100$$

Assumption correct