



## APPM2007 Lagrangian Mechanics

### Tutorial 2

#### Question 1

(5 Points)

Consider the generic point  $a \in \mathbb{R}^3$  that lies on the curve specified by the displacement vector

$$\vec{p} = \begin{pmatrix} z \\ x \\ y \end{pmatrix} = \begin{pmatrix} \rho \cos(\theta) \\ \rho \sin(\theta) \cos(\phi) \\ \rho \sin(\theta) \sin(\phi) \end{pmatrix}.$$

Perform the following construction

1. Construct the the set of unit vectors, tangent to the curve with respect to the co-ordinates  $\{\rho, \theta, \phi\}$ .
2. Show that these tangent vectors are mutually orthogonal.
3. Construct the metric  $\mathbf{g}$ .

#### Solution 1

(5 Points)

1. Construct the co-ordinate derivative of  $\vec{p}$  as follows

$$\hat{e}_\rho = \partial_\rho \vec{p} = \begin{pmatrix} \cos(\theta) \\ \sin(\theta) \cos(\phi) \\ \sin(\theta) \sin(\phi) \end{pmatrix} = \hat{\rho},$$

$$\hat{e}_\theta = \partial_\theta \vec{p} = \begin{pmatrix} -\rho \sin(\theta) \\ \rho \cos(\theta) \cos(\phi) \\ \rho \cos(\theta) \sin(\phi) \end{pmatrix} = \rho \begin{pmatrix} -\sin(\theta) \\ \cos(\theta) \cos(\phi) \\ \cos(\theta) \sin(\phi) \end{pmatrix} = \rho \hat{\theta},$$

$$\hat{e}_\phi = \partial_\phi \vec{p} = \begin{pmatrix} 0 \\ -\rho \sin(\theta) \sin(\phi) \\ \rho \sin(\theta) \cos(\phi) \end{pmatrix} = \rho \sin(\theta) \begin{pmatrix} 0 \\ -\sin(\phi) \\ \cos(\phi) \end{pmatrix} = \rho \sin(\theta) \hat{\phi}.$$

Note that,

$$\hat{e}_\rho = \hat{\rho}, \quad \hat{e}_\theta = \rho \hat{\theta} \quad \text{and} \quad \hat{e}_\phi = \rho \sin(\theta) \hat{\phi}$$

where

$$\hat{\rho} = \begin{pmatrix} \cos(\theta) \\ \sin(\theta) \cos(\phi) \\ \sin(\theta) \sin(\phi) \end{pmatrix}, \quad \hat{\theta} = \begin{pmatrix} -\sin(\theta) \\ \cos(\theta) \cos(\phi) \\ \cos(\theta) \sin(\phi) \end{pmatrix} \quad \text{and} \quad \hat{\phi} = \begin{pmatrix} 0 \\ -\sin(\phi) \\ \cos(\phi) \end{pmatrix}.$$

2. Note that

$$\hat{e}_\rho \cdot \hat{e}_\rho = \hat{\rho} \cdot \hat{\rho}, \quad \hat{e}_\theta \cdot \hat{e}_\theta = \rho^2 \hat{\theta} \cdot \hat{\theta} \quad \text{and} \quad \hat{e}_\phi \cdot \hat{e}_\phi = \rho^2 \sin^2(\theta) \hat{\phi} \cdot \hat{\phi}$$

and

$$\begin{aligned} \hat{e}_\rho \cdot \hat{e}_\theta &= \hat{e}_\theta \cdot \hat{e}_\rho = \rho \hat{\rho} \cdot \hat{\theta} \\ \hat{e}_\theta \cdot \hat{e}_\phi &= \hat{e}_\phi \cdot \hat{e}_\theta = \rho^2 \sin(\theta) \hat{\theta} \cdot \hat{\phi} \\ \hat{e}_\phi \cdot \hat{e}_\rho &= \hat{e}_\rho \cdot \hat{e}_\phi = \rho \sin(\theta) \hat{\phi} \cdot \hat{\rho}. \end{aligned}$$

It is easy to check that,

$$\hat{\rho} \cdot \hat{\rho} = \hat{\theta} \cdot \hat{\theta} = \hat{\phi} \cdot \hat{\phi} = 1 \quad \text{and} \quad \hat{\rho} \cdot \hat{\theta} = \hat{\theta} \cdot \hat{\phi} = \hat{\phi} \cdot \hat{\rho} = 0.$$

3. Collect these inner products together in the form of the metric tensor

$$[\mathbf{g}] = \begin{pmatrix} \hat{e}_\rho \\ \hat{e}_\theta \\ \hat{e}_\phi \end{pmatrix} \cdot \begin{pmatrix} \hat{e}_\rho & \hat{e}_\theta & \hat{e}_\phi \end{pmatrix} = \begin{bmatrix} \hat{e}_\rho \cdot \hat{e}_\rho & \hat{e}_\rho \cdot \hat{e}_\theta & \hat{e}_\rho \cdot \hat{e}_\phi \\ \hat{e}_\theta \cdot \hat{e}_\rho & \hat{e}_\theta \cdot \hat{e}_\theta & \hat{e}_\theta \cdot \hat{e}_\phi \\ \hat{e}_\phi \cdot \hat{e}_\rho & \hat{e}_\phi \cdot \hat{e}_\theta & \hat{e}_\phi \cdot \hat{e}_\phi \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \rho^2 & 0 \\ 0 & 0 & \rho^2 \sin^2(\theta) \end{bmatrix}.$$

□

## Question 2

(10 Points)

Consider the two co-ordination of  $S^2$  in  $\mathbb{R}^3$ ,

$$\vec{a}(\rho, \theta, \phi) = \begin{pmatrix} \rho \cos(\theta) \\ \rho \sin(\theta) \cos(\phi) \\ \rho \sin(\theta) \sin(\phi) \end{pmatrix}$$

where  $\{\rho, \theta, \phi\}$  are the radial, declination and azimuth positions in  $\mathbb{R}^3$ ; and

$$\vec{a}(r, s) = \begin{pmatrix} \frac{2r}{r^2+s^2+1} \\ \frac{2s}{r^2+s^2+1} \\ \frac{r^2+s^2-1}{r^2+s^2+1} \end{pmatrix}$$

where  $r, s \in \mathbb{R}^2$  are in the plane  $z = 0$ . Show that in each co-ordinate system, the length of the curve passing through the north and south poles of  $S^2$  is  $\pi$ . (Hint: construct appropriately parametrised paths  $\vec{a}(t)$  with  $t$  in the appropriate interval.)

## Solution 2

(10 Points)

For the  $(\rho, \theta, \phi)$  co-ordinate system, the curve connecting the north and south poles is that curve, parametrised by  $t$  where

$$\vec{a}(t) = \vec{a}(\rho(t), \theta(t), \phi(t)) = \begin{pmatrix} \rho(t) \cos(\theta(t)) \\ \rho(t) \sin(\theta(t)) \cos(\phi(t)) \\ \rho(t) \sin(\theta(t)) \sin(\phi(t)) \end{pmatrix}.$$

In this paramterisation, the appropriate path parametrisation is  $\rho(t) = 1$ ,  $\theta(t) = t$  and  $\phi(t) = \phi$  is a constant. Then the vector tangent to the path at each time  $t$  is

$$\partial_t \vec{a}(t) = \begin{pmatrix} -\sin(t) \\ \cos(t) \cos(\phi) \\ \cos(t) \sin(\phi) \end{pmatrix}$$

where

$$\|\partial_t \vec{a}(t)\| = 1.$$

The length of the path connecting the north and south poles of the sphere is given by the interal over the tangent vector

$$l = \int_0^\pi dt \|\partial_t \vec{a}(t)\| = \int_0^\pi dt = \pi.$$

For the  $(r, s)$  co-ordinate system, the curve connecting the north and south poles is that curve, parametrised by  $t$  where, without loss of generality, the symmetry of this co-ordinatisation allows

$$\vec{a}(t) = \vec{a}(r(t), s(t)) = \begin{pmatrix} \frac{2r(t)}{r^2(t)+s^2(t)+1} \\ \frac{2s(t)}{r^2(t)+s^2(t)+1} \\ \frac{r^2(t)+s^2(t)-1}{r^2(t)+s^2(t)+1} \end{pmatrix}.$$

In this paramterisation, the appropriate path parametrisation is  $r(t) = t$  and  $s(t) = 0$ . Then the vector tangent to the path at each time  $t$  is

$$\partial_t \vec{a}(t) = \begin{pmatrix} -2 \frac{t^2-1}{(t^2+1)^2} \\ 0 \\ 4 \frac{t^2-1}{(t^2+1)^2} \end{pmatrix}$$

where

$$\|\partial_t \vec{a}(t)\| = \frac{2}{t^2+1}.$$

The length of the path connecting the north and south poles of the sphere is given by the interal over the tangent vector

$$l = \int_0^\infty dt \|\partial_t \vec{a}(t)\| = 2 \int_0^\infty dt \frac{1}{t^2+1} = 2 \frac{\pi}{2} = \pi.$$

□

**Question 3**

(10 Points)

Consider the two co-ordination of  $S^2$  in  $\mathbb{R}^3$

$$\vec{a}(\rho, \theta, \phi) = \begin{pmatrix} \rho \cos(\theta) \\ \rho \sin(\theta) \cos(\phi) \\ \rho \sin(\theta) \sin(\phi) \end{pmatrix}$$

where  $\{\rho, \theta, \phi\}$  are the radial, declination and azimuth positions in  $\mathbb{R}^3$ ; and

$$\vec{a}(r, s) = \begin{pmatrix} \frac{2r}{r^2+s^2+1} \\ \frac{2s}{r^2+s^2+1} \\ \frac{r^2+s^2-1}{r^2+s^2+1} \end{pmatrix}$$

where  $r, s \in \mathbb{R}^2$  are in the plane  $z = 0$ . Show that in each co-ordinate system, the surface area of the unit sphere is  $4\pi$ .

**Solution 3**

(10 Points)

For the  $(\rho, \theta, \phi)$  co-ordinate system, the area element is at a fixed radial distance  $\rho = 1$  is given by

$$\begin{aligned} A &= \int_0^{2\pi} \int_0^\pi d\phi d\theta \|\vec{e}_\theta \times \vec{e}_\phi\| = \int_0^{2\pi} \int_0^\pi d\phi d\theta \rho^2 \sin(\theta) \\ &= 2\pi \int_0^\pi d\theta \sin(\theta) \\ &= -2\pi [\cos(\theta)]_0^\pi \\ &= -2\pi (\cos(\pi) - \cos(0)) \\ &= -2\pi (-1 - 1) \\ &= 4\pi. \end{aligned}$$

For the  $(r, s)$  co-ordinate system, the area element is computed from the cross-product of the tangent vectors,

$$\vec{e}_r = \partial_r \vec{a}(r, s) = \begin{pmatrix} -2 \frac{r^2-s^2-1}{(r^2+s^2+1)^2} \\ -4 \frac{rs}{(r^2+s^2+1)^2} \\ 4 \frac{r}{(r^2+s^2+1)^2} \end{pmatrix} \quad \text{and} \quad \vec{e}_s = \partial_s \vec{a}(r, s) = \begin{pmatrix} -4 \frac{rs}{(r^2+s^2+1)^2} \\ -2 \frac{s^2-r^2-1}{(r^2+s^2+1)^2} \\ 4 \frac{s}{(r^2+s^2+1)^2} \end{pmatrix}.$$

Note that  $\vec{e}_r \cdot \vec{e}_s = 0$ . The area element on the sphere is

$$\vec{e}_r \times \vec{e}_s = \begin{pmatrix} -8 \frac{r}{(r^2+s^2+1)^2} \\ -8 \frac{s}{(r^2+s^2+1)^2} \\ -4 \frac{r^2+s^2-1}{(r^2+s^2+1)^2} \end{pmatrix},$$

so,

$$\|\vec{e}_r \times \vec{e}_s\|^2 = \frac{16}{(r^2+s^2+1)^4} \quad \text{or} \quad \|\vec{e}_r \times \vec{e}_s\| = \frac{4}{(r^2+s^2+1)^2}.$$

Therefore the total area on the sphere is given by

$$A = \int_{-\infty}^{\infty} \int_{-\infty}^{\infty} dr ds \frac{4}{(r^2+s^2+1)^2}.$$

By noting the rotational symmetry, we may compute this integral using the trigonometric substitution,  $r = t \cos(\zeta)$  and  $s = t \sin(\zeta)$  to give

$$A = 4 \int_0^{2\pi} \int_0^{\infty} d\zeta dt \frac{t}{(t^2+1)^2} = 4 \cdot 2\pi \int_0^{\infty} dt \frac{t}{(t^2+1)^2},$$

which is again soluble by substitution  $u = t^2 + 1$  to give

$$A = 4 \cdot 2\pi \int_1^{\infty} du \frac{1}{2u^2} = 4\pi \left[ \frac{1}{u} \right]_1^{\infty} = 4\pi$$

□

**Question 4**

(10 Points)

The *Cobb-Douglas production function* is used to model the number of units produced by varying amounts of labour and capital. Let  $x$  define the units of labour and  $y$  denote the units of capital and  $C$  is a constant and  $0 < a < 1$ ,

$$f(x, y) = Cx^a y^{1-a}.$$

The Cobb-Douglas production function for a particular manufacturer is given by

$$f(x, y) = 100x^{\frac{3}{4}}y^{\frac{1}{4}}.$$

Suppose that labour is charged at R150 per unit and capital is charged at R250 per unit. Suppose that the total cost of labour and capital is limited to R50000. Find the maximum production level for this manufacturer. (Hint: relate the rate of productivity to the rate of constraint using directional derivatives.)

**Solution 4**

(10 Points)

The limit on the cost of labour and capital gives a constraint,

$$g(x, y) = 150x + 250y = 50000.$$

The maximum production level occurs when the constraint and production level function level sets are tangent. From the given production and constraint functions, we find tangent vectors

$$\begin{aligned}\nabla f(x, y) &= \partial_x f(x, y) \hat{x} + \partial_y f(x, y) \hat{y} \\ &= 75x^{-\frac{1}{4}}y^{\frac{1}{4}} \hat{x} + 25x^{\frac{3}{4}}y^{-\frac{3}{4}} \hat{y}\end{aligned}$$

and

$$\begin{aligned}\nabla g(x, y) &= \partial_x g(x, y) \hat{x} + \partial_y g(x, y) \hat{y} \\ &= 150\hat{x} + 250\hat{y}.\end{aligned}$$

If the tangent vectors are colinear, then  $\lambda \nabla g(x, y) = \nabla f(x, y)$  where  $\lambda$  is some constant. This gives rise to a system of equations

$$\begin{aligned}75x^{-\frac{1}{4}}y^{\frac{1}{4}} \hat{x} &= 150\lambda \\ 25x^{\frac{3}{4}}y^{-\frac{3}{4}} \hat{x} &= 250\lambda,\end{aligned}$$

subject to

$$150x + 250y = 50000.$$

Solving for  $\lambda$  yields,

$$\lambda = \frac{x^{-\frac{1}{4}} y^{\frac{1}{4}}}{2}.$$

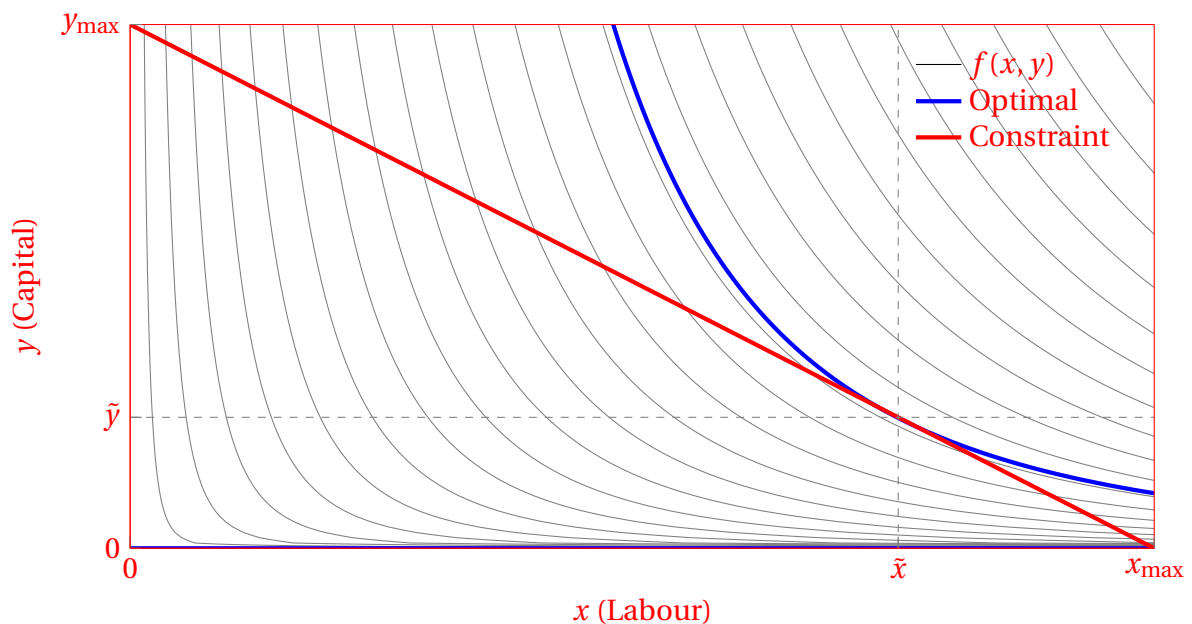
Substituting this back into the the component equations of  $\lambda \nabla g(x, y) = \nabla f(x, y)$  yields optimail values

$$\tilde{x} = 250 \quad \text{and} \quad \tilde{y} = 50.$$

The maximum production level, subject to the constraint occurs at 250 units of labour and 50 units of capital,

$$f(\tilde{x}, \tilde{y}) = 16.719 \text{ units.}$$

The Lagrange multiplier  $\lambda$  is referred to as the *marginal proctivity of money* and describes the number of addition units of production for each unit of money spent on that production.



□