

Control Systems

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CONTENTS

1	Second order System	1
1.1	Damping	1
2	State-Space Model	1
2.1	Controllability and Observability	1
2.2	Second Order System	3

Abstract—This manual is an introduction to control systems based on GATE problems. Links to sample Python codes are available in the text.

Download python codes using

```
svn co https://github.com/gadepall/school/trunk/
control/codes
```

1 SECOND ORDER SYSTEM

1.1 Damping

- 1.1.1. List the different kinds of damping for a second order system defined by

$$H(s) = \frac{\omega^2}{s^2 + 2\zeta\omega s + \omega^2} \quad (1.1.1.1)$$

where ω is the natural frequency and ζ is the damping factor.

Solution: The details are available in Table 1.1.1

Damping Ratio	Damping Type
$\zeta > 1$	Overdamped
$\zeta = 1$	Critically Damped
$0 < \zeta < 1$	Underdamped
$\zeta = 0$	Undamped

TABLE 1.1.1

- 1.1.2. Classify the following second-order systems according to damping.

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$$\begin{aligned} \text{a) } H(s) &= \frac{15}{s^2 + 5s + 15} \\ \text{b) } H(s) &= \frac{25}{s^2 + 10s + 25} \\ \text{c) } H(s) &= \frac{35}{s^2 + 18s + 35} \end{aligned}$$

Solution: For

$$H(s) = \frac{25}{s^2 + 10s + 25}, \quad (1.1.2.1)$$

$$\omega^2 = 25, 2\zeta\omega = 10 \quad (1.1.2.2)$$

$$\Rightarrow \omega = 1, \zeta = 1 \quad (1.1.2.3)$$

and the system is critically damped. Similarly, the damping factors for other systems in Problem 1.1.2 are calculated and listed in Table 1.1.2

$H(s)$	ω	ζ	Damping Type
$\frac{35}{s^2 + 18s + 35}$	$\sqrt{35}$	$\sqrt{\frac{81}{35}} > 1$	Overdamped
$\frac{25}{s^2 + 10s + 25}$	5	1	Critically Damped
$\frac{15}{s^2 + 5s + 15}$	$\sqrt{15}$	$\sqrt{\frac{5}{12}} < 1$	Underdamped

TABLE 1.1.2

- 1.1.3. By choosing an appropriate input, illustrate the effect of damping using a Python code to sketch the response.

2 STATE-SPACE MODEL

2.1 Controllability and Observability

- 2.1.1. State the general model of a state space system specifying the dimensions of the matrices and vectors.

Solution: The model is given by

$$\dot{\mathbf{x}}(t) = \mathbf{A}\mathbf{x}(t) + \mathbf{B}\mathbf{u}(t) \quad (2.1.1.1)$$

$$\mathbf{y}(t) = \mathbf{C}\mathbf{x}(t) + \mathbf{D}\mathbf{u}(t) \quad (2.1.1.2)$$

with parameters listed in Table 2.1.1.

- 2.1.2. Find the transfer function $\mathbf{H}(s)$ for the general system.

Variable	Size	Description
u	$p \times 1$	input(control) vector
y	$q \times 1$	output vector
x	$n \times 1$	state vector
A	$n \times n$	state or system matrix
B	$n \times p$	input matrix
C	$q \times n$	output matrix
D	$q \times p$	feedthrough matrix

TABLE 2.1.1

Solution: Taking Laplace transform on both sides we have the following equations

$$s\mathbf{I}X(s) - x(0) = \mathbf{A}X(s) + \mathbf{B}U(s) \quad (2.1.2.1)$$

$$(s\mathbf{I} - \mathbf{A})X(s) = \mathbf{B}U(s) + x(0) \quad (2.1.2.2)$$

$$X(s) = (s\mathbf{I} - \mathbf{A})^{-1}\mathbf{B}U(s) + (s\mathbf{I} - \mathbf{A})^{-1}x(0) \quad (2.1.2.3)$$

and

$$Y(s) = \mathbf{C}X(s) + \mathbf{D}\mathbf{I}U(s) \quad (2.1.2.4)$$

Substituting from (2.1.2.3) in the above,

$$Y(s) = (\mathbf{C}(s\mathbf{I} - \mathbf{A})^{-1}\mathbf{B} + \mathbf{D}\mathbf{I})U(s) + \mathbf{C}(s\mathbf{I} - \mathbf{A})^{-1}x(0) \quad (2.1.2.5)$$

2.1.3. Find $H(s)$ for a SISO (single input single output) system.

Solution:

$$H(s) = \frac{Y(s)}{U(s)} = C(sI - A)^{-1}B + DI \quad (2.1.3.1)$$

2.1.4. Given

$$H(s) = \frac{1}{s^3 + 3s^2 + 2s + 1} \quad (2.1.4.1)$$

$$D = 0 \quad (2.1.4.2)$$

$$\mathbf{B} = \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix} \quad (2.1.4.3)$$

find \mathbf{A} and \mathbf{C} such that the state-space realization is in *controllable canonical form*.

Solution:

$$\therefore \frac{Y(s)}{U(s)} = \frac{Y(s)}{V(s)} \times \frac{V(s)}{U(s)}, \quad (2.1.4.4)$$

letting

$$\frac{Y(s)}{V(s)} = 1, \quad (2.1.4.5)$$

results in

$$\frac{U(s)}{V(s)} = s^3 + 3s^2 + 2s + 1 \quad (2.1.4.6)$$

giving

$$U(s) = s^3V(s) + 3s^2V(s) + 2sV(s) + V(s) \quad (2.1.4.7)$$

so equation 0.1.13 can be written as

$$\begin{pmatrix} sV(s) \\ s^2V(s) \\ s^3V(s) \end{pmatrix} = \begin{pmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -1 & -2 & -3 \end{pmatrix} \begin{pmatrix} V(s) \\ s(s) \\ s^2V(s) \end{pmatrix} + \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix} U \quad (2.1.4.8)$$

So

$$\mathbf{A} = \begin{pmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -1 & -2 & -3 \end{pmatrix} \quad (2.1.4.9)$$

$$Y = X_1(s) = \begin{pmatrix} 1 & 0 & 0 \end{pmatrix} \begin{pmatrix} V(s) \\ sV(s) \\ s^2V(s) \end{pmatrix} \quad (2.1.4.10)$$

$$\mathbf{C} = \begin{pmatrix} 1 & 0 & 0 \end{pmatrix} \quad (2.1.4.11)$$

2.1.5. Obtain \mathbf{A} and \mathbf{C} so that the state-space realization is in *observable canonical form*.

Solution: Given that

$$H(s) = \frac{1}{s^3 + 3s^2 + 2s + 1} \quad (2.1.5.1)$$

$$\frac{Y(s)}{U(s)} = \frac{1}{s^3 + 3s^2 + 2s + 1} \quad (2.1.5.2)$$

$$Y(s) \times (s^3 + 3s^2 + 2s + 1) = U(s) \quad (2.1.5.3)$$

$$s^3Y(s) + 3s^2Y(s) + 2sY(s) + Y(s) = U(s) \quad (2.1.5.4)$$

$$s^3Y(s) = U(s) - 3s^2Y(s) - 2sY(s) - Y(s) \quad (2.1.5.5)$$

$$Y(s) = -3s^{-1}Y(s) - 2s^{-2}Y(s) + s^{-3}(U(s) - Y(s)) \quad (2.1.5.6)$$

let $Y = aU + X_1$

by comparing with equation 1.5.6 we get $a=0$ and

$$Y = X_1 \quad (2.1.5.7)$$

inverse laplace transform of above equation is

$$y = x_1 \quad (2.1.5.8)$$

so from above equation 1.5.6 and 1.5.7

$$X_1 = -3s^{-1}Y(s) - 2s^{-2}Y(s) + s^{-3}(U(s) - Y(s)) \quad (2.1.5.9)$$

$$sX_1 = -3Y(s) - 2s^{-1}Y(s) + s^{-2}(U(s) - Y(s)) \quad (2.1.5.10)$$

inverse laplace transform of above equation

$$\dot{x}_1 = -3y + x_2 \quad (2.1.5.11)$$

where

$$X_2 = -2s^{-1}Y(s) + s^{-2}(U(s) - Y(s)) \quad (2.1.5.12)$$

$$sX_2 = -2Y(s) + s^{-1}(U(s) - Y(s)) \quad (2.1.5.13)$$

inverse laplace transform of above equation

$$\dot{x}_2 = -2y + x_3 \quad (2.1.5.14)$$

where

$$X_3 = s^{-1}(U(s) - Y(s)) \quad (2.1.5.15)$$

$$sX_3 = U(s) - Y(s) \quad (2.1.5.16)$$

inverse laplace transform of above equation

$$\dot{x}_3 = u - y \quad (2.1.5.17)$$

so we get four equations which are

$$y = x_1 \quad (2.1.5.18)$$

$$\dot{x}_1 = -3y + x_2 \quad (2.1.5.19)$$

$$\dot{x}_2 = -2y + x_3 \quad (2.1.5.20)$$

$$\dot{x}_3 = u - y \quad (2.1.5.21)$$

sub $y = x_1$ in 1.5.19,1.5.20,1.5.21 we get

$$y = x_1 \quad (2.1.5.22)$$

$$\dot{x}_1 = -3x_1 + x_2 \quad (2.1.5.23)$$

$$\dot{x}_2 = -2x_1 + x_3 \quad (2.1.5.24)$$

$$\dot{x}_3 = u - x_1 \quad (2.1.5.25)$$

so above equations can be written as

$$\begin{pmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \end{pmatrix} = \begin{pmatrix} -3 & 1 & 0 \\ -2 & 0 & 1 \\ -1 & 0 & 0 \end{pmatrix} \begin{pmatrix} x_1 \\ x_2 \\ x_3 \end{pmatrix} + \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix} U \quad (2.1.5.26)$$

So

$$\mathbf{A} = \begin{pmatrix} -3 & 1 & 0 \\ -2 & 0 & 1 \\ -1 & 0 & 0 \end{pmatrix} \quad (2.1.5.27)$$

$$y = x_1 = \begin{pmatrix} 1 & 0 & 0 \end{pmatrix} \begin{pmatrix} x_1 \\ x_2 \\ x_3 \end{pmatrix} \quad (2.1.5.28)$$

$$\mathbf{C} = \begin{pmatrix} 1 & 0 & 0 \end{pmatrix} \quad (2.1.5.29)$$

2.1.6. Find the eigenvalues of \mathbf{A} and the poles of $H(s)$ using a python code.

Solution: The following code

```
codes/ee18btech11004.py
```

gives the necessary values. The roots are the same as the eigenvalues.

2.1.7. Theoretically, show that eigenvalues of \mathbf{A} are the poles of $H(s)$. **Solution:**

as we know that the characteristic equation is $\det(s\mathbf{I} - \mathbf{A})$

$$s\mathbf{I} - \mathbf{A} = \begin{pmatrix} s & 0 & 0 \\ 0 & s & 0 \\ 0 & 0 & s \end{pmatrix} - \begin{pmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -1 & -2 & -3 \end{pmatrix} = \begin{pmatrix} s & -1 & 0 \\ 0 & s & -1 \\ 1 & 2 & s+3 \end{pmatrix} \quad (2.1.7.1)$$

therefore

$$\det(s\mathbf{I} - \mathbf{A}) = s(s^2 + 3s + 2) + 1(1) = s^3 + 3s^2 + 2s + 1 \quad (2.1.7.2)$$

so from equation 1.6.2 we can see that characteristic equation is equal to the denominator of the transefer function

2.2 Second Order System

2.2.1. Consider a state-variable model of a system

$$\begin{pmatrix} \dot{x}_1 \\ \dot{x}_2 \end{pmatrix} = \begin{pmatrix} 0 & 1 \\ -\alpha & -2\beta \end{pmatrix} \begin{pmatrix} x_1 \\ x_2 \end{pmatrix} + \begin{pmatrix} b_1 \\ b_2 \end{pmatrix} r \quad (2.2.1.1)$$

$$y = \begin{pmatrix} 1 & 0 \end{pmatrix} \begin{pmatrix} x_1 \\ x_2 \end{pmatrix} \quad (2.2.1.2)$$

where y is the output, and r is the input.

2.2.2. List the various state matrices in (2.2.1.1)

Solution: The state space model is given by

$$\dot{X} = AX + BU \quad (2.2.2.1)$$

$$Y = CX + DU \quad (2.2.2.2)$$

Comparing this with (2.2.1.1) we get the state matrices as,

$$A = \begin{pmatrix} 0 & 1 \\ -\alpha & -2\beta \end{pmatrix} \quad (2.2.2.3)$$

$$B = \begin{pmatrix} b_1 \\ b_2 \end{pmatrix} \quad (2.2.2.4)$$

$$C = \begin{pmatrix} 1 & 0 \end{pmatrix} \quad (2.2.2.5)$$

$$D = 0 \quad (2.2.2.6)$$

2.2.3. Find the the system transfer function $H(s)$.

Solution: From (2.1.1.1) and , (2.1.3.1), the transfer function for the state space model is

$$H(s) = C(sI - A)^{-1}B + D \quad (2.2.3.1)$$

$$= \frac{\begin{pmatrix} 1 & 0 \end{pmatrix} \begin{pmatrix} s + 2\beta & 1 \\ -\alpha & s \end{pmatrix} \begin{pmatrix} b_1 \\ b_2 \end{pmatrix}}{s(s + 2\beta) + \alpha} \quad (2.2.3.2)$$

$$= \frac{b_1(s + 2\beta) + b_2}{s^2 + 2s\beta + \alpha} \quad (2.2.3.3)$$

$$\Rightarrow H(s) = \frac{b_1 s}{s^2 + 2s\beta + \alpha} + \frac{2b_1\beta + b_2}{s^2 + 2s\beta + \alpha} \quad (2.2.3.4)$$

2.2.4. Find the Damping ratio ζ and the Undamped natural frequency ω_n of the system.

Solution: Generally for a second order system the transfer function is given by 1.1.1.1

$$H(s) = \frac{\omega_n^2}{s^2 + 2s\zeta\omega_n + \omega_n^2} \quad (2.2.4.1)$$

Comparing the denominator of the above with (2.2.3.4),

$$2\zeta\omega_n = 2\beta, \quad (2.2.4.2)$$

$$\omega_n^2 = \alpha \quad (2.2.4.3)$$

$$\Rightarrow \zeta = \frac{\beta}{\sqrt{\alpha}}, \omega_n = \sqrt{\alpha} \quad (2.2.4.4)$$

2.2.5. Using Table 1.1.1, explain how the damping conditions depend upon α and β .

Solution: Using Table 1.1.1, and equation (2.2.4.4) we can say the following things about system,

$$\beta > \sqrt{\alpha} \Rightarrow \text{Overdamped} \quad (2.2.5.1)$$

$$\beta = \sqrt{\alpha} \Rightarrow \text{Critically Damped} \quad (2.2.5.2)$$

$$0 < \beta < \sqrt{\alpha} \Rightarrow \text{Underdamped} \quad (2.2.5.3)$$

$$\beta = 0 \Rightarrow \text{Undamped} \quad (2.2.5.4)$$