Software Requirements Specification for Solar Cooker This should be and observed he the name of your Deesha Patel

February 11, 2023

Software. Old February 17, 2023

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# Contents

1	Ref	erence Material					
	1.1	Table of Units					
	1.2	Table of Symbols					
	1.3	Abbreviations and Acronyms					
2	Intr	roduction					
	2.1	Purpose of Document					
	2.2	Scope of Requirements					
	2.3	Characteristics of Intended Reader					
	2.4	Organization of Document					
3	Ger	neral System Description					
	3.1	System Context					
	3.2	User Characteristics					
	3.3	System Constraints					
4	Spe	ecific System Description					
	4.1	Problem Description					
		4.1.1 Terminology and Definitions					
		4.1.2 Physical System Description					
		4.1.3 Goal Statements					
	4.2	Solution Characteristics Specification					
		4.2.1 Assumptions					
		4.2.2 Theoretical Models					
		4.2.3 General Definitions					
		4.2.4 Data Definitions					
		4.2.5 Instance Models					
		4.2.6 Input Data Constraints					
5	Requirements 1						
	5.1	Functional Requirements					
	5.2	Nonfunctional Requirements					
6	Like	Likely Changes					
7	Unl	Unlikely Changes					
8	Tra	ceability Matrices and Graphs					

# **Revision History**

Date	Version	Notes
02/04/2023	0.1	Initial Release
02/11/2023	0.2	Update document for first 4 issues
02/11/2023	0.3	Update document for 5 to 9 issues
02/11/2023	0.4	All changes done

## 1 Reference Material

This section records information for easy reference.

### 1.1 Table of Units

Throughout this document SI (Système International d'Unités) is employed as the unit system. In addition to the basic units, several derived units are used as described below. For each unit, the symbol is given followed by a description of the unit and the SI name.

symbol	unit	SI
m	length	metre
kg	mass	kilogram
$\mathbf{s}$	time	second
$^{\circ}\mathrm{C}$	temperature	centigrade
J	energy	joule
W	power	watt $(W = J s^{-1})$

## 1.2 Table of Symbols

The table that follows summarizes the symbols used in this document along with their units. The choice of symbols was made to be consistent with the heat transfer energy. The symbols are listed in alphabetical order.

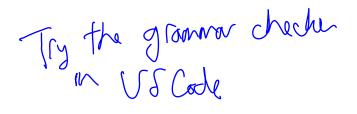
symbol	unit	description
$\overline{A_{\mathrm{g}}}$	$\mathrm{m}^2$	Area of glass
$A_{ m m}$	$\mathrm{m}^2$	Wet surface area over which heat is transferred in
$A_r$	$\mathrm{m}^2$	Area of Reflector
$A_{\mathrm{ref}}$	$\mathrm{m}^2$	Reflector area with respect to different reflectors
C	$J/(kg^{\circ}C)$	Specific Heat Capacity of material
$C_W$	$J/(kg^{\circ}C)$	Specific Heat Capacity of Water
$E_W$	J	Change in heat energy in the Water
f	-	Fluid
G	$\mathrm{W/m^2}$	Change in heat energy in the Water Fluid Incidental solar radiation Glass 2
$\sim g2$	-	Glass 2
h	$\mathrm{W/m^2K}$	Heat transfer convection coefficient
int1	_	Inner part between glass 1 and glass 2
int2	-	Inner part of the solar cooker box
` 1		

Substints who mumbers work the numbers

int3	-	Inner part of recipient
L	m	Length of box
$m_W$	kg	Mass of Water
n	-	Number of Reflector
q	$\mathrm{W}\mathrm{m}^{-2}$	Thermal flux vector
Q	(E)	Quantity of heat transfer to or from the object
r	-	Reflector
T	$^{\circ}\mathrm{C}$	Temperature
$T_W$	$^{\circ}\mathrm{C}$	Temperature of Water
t	-	Lid of recipient Emittance Transmittivity Reflector Angle Steffan-Boltzman constant Reflectivity
$\epsilon$	$\mu\mathrm{m}$	Emittance
au	$\mathrm{W}/\mathrm{m}^2\mathrm{K}$	Transmittivity
$\theta$	radians	Reflector Angle
$\sigma$	$\mathrm{W}/\mathrm{m}^2\mathrm{K}^4$	Steffan-Boltzman constant
ρ	${\rm kg/m^3}$	Reflectivity / Man down y
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# 1.3 Abbreviations and Acronyms

symbol	description
A	Assumption
DD	Data Definition
GD	General Definition
GS	Goal Statement
IM	Instance Model
LC	Likely Change
PS	Physical System Description
R	Requirement
SRS	Software Requirements Specification
Τ	Theoretical Model



#### 2 Introduction

As fossil fuels adversely affect the environment, many countries like India, where they have good Solar rays throughout the year, have started to implement devices for utilizing solar energy and transforming it into valuable energy. It includes Solar Water heaters, Solar panels, and Solar Cookers. It is indeed a fact that the demand for renewable energy has increased to deal with the problem of limited non-renewable resources. Focusing on Solar Cooker, several design such as Solar Panel Cooker, Solar Parabolic Cooker, and Solar Box Cooker has been proposed to utilize more Solar energy. Using internal reflectors, we would like to improve the utilization of Solar energy during cooking a food.

The following section provides an overview of Software Requirement Specification (SRS) for a box-type Solar Cooker. This section explains the purpose of the document, the scope of requirements, the characteristic of the intended reader, and the organization of a document.

#### 2.1Purpose of Document

We are going to use the Solar Box Cooker in this software. The main purpose of this document is to describe a mathematical model of a Solar Cooker which can provide a calculation for internal reflector in solar box that can help to improve the temperature in the box with a variety of parameters that attempts to define the intended functionality required. Thus, this document provides detailed requirements of the software which will be used in planing for design stage. Therefore, this document is intended to be used as a reference to provide ad hoc access to all information necessary to understand and verify the model. This document describes goals, assumptions, theoretical models, and important definitions to understand The algorithm duts not frequent of the Carle it just a construction. The the problem. The SRS is abstract because the content here says what the problem is. But it does not say anything related to how to solve it.

#### 2.2Scope of Requirements

Numerous algorithms have been proposed to improve the efficiency of Solar Cooker. The scope of the requirement includes a mathematical model to determine the thermal function of a box-type solar cooker with an internal reflectors. With the help of different inputs, this system calculates the achieved temperature by implementing the proposed solution. However, this project not focusing on more than one iteration for the reflections. In other words, this project focuses on the reflection from glass 2 to recipient.

#### 2.3 Characteristics of Intended Reader

Firstly, Intended Reader or Reviewer should have knowledge of heat transfer theory and radiant solar energy. A person should have completed a Heat Transfer course during their bachelor of engineering (Mechanical Engineering and Chemical Engineering expected). A reader should have knowledge about the differential equation; offered in the first year Calculus course.

1 avered or 2nd your.

### 2.4 Organization of Document

The organization of this document follows the template for an SRS for scientific computing software proposed by (2) and (3). The presentation follows the standard pattern of presenting goals, theories, definitions, and assumptions. For readers that would like a more bottom up approach, they can start reading the instance models in Section 4.2.5 and trace back to find any additional information they require. The goal statements are refined to the theoretical models, and the theoretical models to the instance models. The instance model (Section 4.2.5) to be solved is referred to as IM1.

# 3 General System Description

This section provides general information about the system. It identifies the interfaces between the system and its environment, describes the user characteristics and lists the system constraints.

### 3.1 System Context

The system context is shown in Figure 1 below. The circles represent the user, who is both responsible for handling the inputs and the outputs. The box represents the program itself, and the arrows indicate what data and information is passed between the user and the program.

Number of Reflectors and Solar Cooker Energy Value and Heat energy

Casculin Solar Cooker Energy

Figure 1: System Context

#### • User Responsibilities:

- Provide required inputs including number of reflectors, glass area, thickness, dimension and size.
- Ensure all inputs are in correct format.

### • Software Responsibilities:

- Detect data type mismatch, such as a string of characters instead of a floating point number
- Determine if the inputs satisfy the required physical and software constraints such as thickness of the glass can not be a negative value
- Calculate and plot the required outputs of temperature

### 3.2 User Characteristics

The end user of the system is expected to be familiar with undergraduate level Calculus and basic Physics. They should also know basics about the reflector angle and heat flows in solar cooker.

### 3.3 System Constraints

There are no system constraints for this project.

# 4 Specific System Description

This section first presents the problem description, which gives a high-level view of the problem to be solved. This is followed by the solution characteristics specification, which presents the assumptions, theories, definitions and finally the instance models (ODE) that models the Solar Cooker Reflections.

### 4.1 Problem Description

Solar Cooker Energy Calculation is intended to investigate the temperature inside the solar cooker box with internal reflectors.

### 4.1.1 Terminology and Definitions

This subsection provides a list of terms that are used in the subsequent sections and their meaning, with the purpose of reducing ambiguity and making it easier to correctly understand the requirements:

- Reflectivity: The fraction of radiation reflected by the surface is called the reflectivity  $(\rho)$ .
- Transmittivity: The fraction of radiation transmitted is called the transmissivity  $(\tau)$ .
- Emittance: The energy radiated by the surface of a body per second per unit area  $(\epsilon)$ .
- Reflactor Angle: The angle between a reflected ray and the normal drawn at the point of incidence to a reflecting surface  $(\theta)$ .
- Heat flow Convection: Convection is the transfer of heat from one place to another due to the movement of fluid.
- Heat flow radiation: A process where heat waves are emitted that may be absorbed, reflected, or transmitted through a colder body.

- Heat Convection Coefficients: The rate of heat transfer between a solid surface and a fluid per unit surface area per unit temperature difference (h).
- Steffan-Boltzman constant: A physical constant expressing the relationship between the heat radiation emitted by a black body and its absolute temperature  $(\sigma)$ .
- Heat/Thermal Flux: The amount of heat energy passing through a certain surface.
- Heat Capacity: Heat capacity or thermal capacity is a physical property of matter, defined as the amount of heat to be supplied to an object to produce a unit change in its temperature.
- Incidental Solar Radiation: The amount of solar radiation that hits the earth's surface per unit of time and area.

### 4.1.2 Physical System Description

The physical system of Solar Cooker Energy Calculation, as shown in Figure 2, includes the following elements: PS1: A cover with two flat glasses (glass 1 and glass 2) PS2: Lead of the recipient and recipient itself PS3: Fluid inside the recipient Explain whood

Svy 1, 5, 42 int 1 g In 3 or Q7 Q8 int 2 Q11 Q15 int 3 >Q16 and advancing with the contract of the contrac Figure 2: Heat Flows in
I lime the open for almost one for the following the only had puper for ramins a, a2, ... However, mit be memoric name would bear be memoric name would be nice to have name, halpful. It would be nice to have name. → Q17 Figure 2: Heat Flows in Solar Cooker

#### 4.1.3 Goal Statements

Given the thermal attributes and solar box characteristics, the goal statements are:

and initial conditions

Colculator

GS1: predicts the Balance of temperature on the recipient

GS2: predicts the cooking energy in the recipient over time.

#### 4.2 Solution Characteristics Specification

The instance model (ODE) that governs Solar Cooker Energy Calculation is presented in Subsection 4.2.5. The information to understand the meaning of the instance model and its derivation is also presented, so that the instance model can be verified.

#### 4.2.1 Assumptions

This section simplifies the original problem and helps in developing the theoretical model by filling in the missing information for the physical system. The numbers given in the square brackets refer to the theoretical model [T], general definition [GD], data definition [DD], instance model [IM], or likely change [LC], in which the respective assumption is used.

- A1: The emissivity( $\epsilon$ ) have been considered constant [GD1, DD3, DD4, IM1]
- A2: The reflectivity  $(\rho)$  have been considered constant [DD2]
- A3: The Transmisivity  $(\tau)$  have been considered constant [DD2]
- A4: The material in the recipient (Container) is water. This implies that the temperature will not drop below melting point and not rise above the boiling point [IM1, T2]
- hate ? A5: The temperature  $T_{\text{int2}}$  are obtained in function of others temperatures by means of the consinue to Car say It in winds. following supposition: [IM1, DD1]

$$T_{
m int2} = rac{T_{
m g2} + T_t + T_r}{3}$$
 and what there when the second with the second secon

- A6: The solar radiation impact over the solar cooker occurs in perpendicular way. [IM1,  $DD_2$
- A7: The only form of energy considered in this problem is thermal energy. Other energy such as mechanical energy are assumed to be a negligible. [IM1, LC1]
- A8: The temperature of the reflector is constant over the different time. [DD6, LC2]

I had you are this to day that you are assumming no phose change. The pupilo 5 don't require this, but you can slik assume it.

#### 4.2.2 Theoretical Models

This section focuses on the general equations and laws that Solar Cooker Energy Calculation. Me LaTex equation \$ L = Pac&q? & Delta T)

is based on.

Number	TM1
Label	Convective Heat Transfer Coefficient
Equation	$h = \frac{q}{\Delta T}$
Description	The above equation is used to calculate the heat transfer typically by convection or phase transition.
	h is the heat transfer convection coefficient (W/m <sup>2</sup> K).
	q is the thermal flux vector (W m <sup>-2</sup> ).
	$\triangle T$ is the change in temperature.
Notes	none.
Sources	https://en.wikipedia.org/wiki/Heat_transfer_coefficient
Ref. By	GD1, IM1

Number	TM2
Label	Sensible Heat energy Calculation
Equation	$Q = Cm\Delta T$
Description	This calculation occurs until the highest or lowest temperature reach, as assumed in [A4] $Q$ is the quantity of heat transferred to or from the object $M$ is the mass of the object $M$ is the specific heat capacity of the material the object is composed of $\Delta T$ is the resulting temperature change of the object
Notes	none.
Sources	https://www.physicsclassroom.com/class/thermalP/Lesson-2/ Measuring-the-Quantity-of-Heat
Ref. By	IM2

You need the hearthood store of the made energy.

You need the hearthood two of the manyle than E firm

You can borrow the consthering them E firm

It is confusing to use Q for head & Q for head Abur.

Does your original paper do this?

#### 4.2.3 General Definitions

This section collects the laws and equations that will be used in building the instance models.

(Mak could card if the		
Number	GD1	
Label	Heat Flow Convection	
SI Units	W	
Equation	$Q(t) = hA\Delta T(t)$	
Description	Heat Flow Convection is related to Newton's law of cooling describes convective cooling from a surface. The law is stated as: the rate of heat loss from a body is proportional to the difference in temperatures between the body and its surroundings.	
	Q(t) is the thermal flux (W m <sup>-2</sup> ).	
	h is the heat transfer coefficient (W m <sup>-2</sup> °C <sup>-1</sup> ).	
	A is the exposed surface area $(m^2)$ .	
	$\Delta T(t)$ is the temperature difference (°C).	
Sources	https://en.wikipedia.org/wiki/Convection_(heat_transfer)	
Ref. By	IM1	

Number	GD2
Label	Heat Flow Radiation
SI Units	J
Equation	$Q(t) = \sigma e A \triangle T^4$
Description	An object emits radiant energy in all directions unless its temperature is absolute zero. If this energy strikes a receiver, part of it may be absorbed, part may be transmitted, and part may be reflected. Heat transfer from a hot to a cold object in this manner is known as radiation heat transfer. The higher the temperature, the greater is the amount of energy radiated. $Q(t)$ is the heat flow radiation (W m <sup>-2</sup> ). $\sigma$ is the Steffan-Boltzman constant (5.669 $X$ 10 <sup>-8</sup> $W/m^2K^4$ ). $e$ is the emissivity of object(W/m). $A$ is the exposed surface area (m <sup>2</sup> )
	$\Delta T(t)$ is the temperature difference (°C).
Sources	(1)
Ref. By	IM <mark>1</mark>

### 4.2.4 Data Definitions

This section collects and defines all the data needed to build the instance models. The dimension of each quantity is also given.

Number	DD1
Label	Data Definition of Q13
Symbol	Q13
SI Units	$ m Wm^{-2}$
Equation	$\mathbf{Q13} = A_r h_{\text{r-int2}} (T_{\text{int2}} - T_r)$
Description	Q13 calculates the Heat flow convection of recipient to inner 2
	$A_r$ is the Area of Reflector (m <sup>2</sup> ).
	$h_{ m r-int2}$ is the thermal flux difference between Reflector and Inner area inside the box
	$T_{\text{int2}}-T_r$ is the temperature difference between inner area and reflector (°C).
Sources	(5)
Ref. By	IM <mark>1</mark>

Number	DD2
Label	Data Definition of Q14
Symbol	Q14
SI Units	$ m Wm^{-2}$
Equation	$\mathbf{Q14} = \sum_{i=1}^{n} \rho A_{\text{ref,n}} G \tau_g^2 \cos(90 - \theta_{\text{ref,n}})$
Description	Q14 calculates the Heat flow reflection of incident radiation on the reflectors
	$\rho$ is the reflectivity constant (kg/m <sup>3</sup> ).
	$A_{\rm ref,n}$ is the Area of the number of reflectors
	$G$ is Incidental solar radiation taken as an input $(W/m^2)$
	$\tau_g$ is the Transmittivity constant for glass $(0 \le \tau \le 1)$
	$cos(90 - \theta_{ref,n})$ is the angle difference of reflectors.
Sources	(5)
Ref. By	IM <mark>1</mark>

Number	DD3
Label	Data Definition of Q15
Symbol	Q15
SI Units	$ m Wm^{-2}$
Equation	$\mathbf{Q15} = A_r \sigma \epsilon_r (T_r^4 - T_{g2}^4)$
Description	Q15 calculates the Heat flow radiation of recipient toward glass 2
	$A_r$ is the Area of Reflector (m <sup>2</sup> ).
	$\sigma$ is the Steffan-Boltzman constant (5.669X10^{-8}W/m^2K^4)
	$\epsilon_r$ is the Emittance of Reflector (W/m)
	$T_r - T_{\rm g2}$ is the temperature difference of reflectors and glass 2 (°C).
Sources	(5)
Ref. By	IM <mark>1</mark>

Number	DD4
Label	Data Definition of Q16
Symbol	Q16
SI Units	$ m Wm^{-2}$
Equation	$\mathbf{Q16} = A_r \sigma \epsilon_r (T_r^4 - T_f^4)$
Description	Q16 calculates the Heat flow radiation of recipient toward the fluid
	$A_r$ is the Area of Reflector (m <sup>2</sup> ).
	$\sigma$ is the Steffan-Boltzman constant (5.669X10^{-8}W/m^2K^4)
	$\epsilon_r$ is the Emittance of Reflector (W/m)
	$T_r - T_f$ is the temperature difference of reflectors and fluid(°C).
Sources	(5)
Ref. By	IM <mark>1</mark>

Number	DD5
Label	Data Definition of Q17
Symbol	Q17
SI Units	$ m Wm^{-2}$
Equation	$\mathbf{Q17} = A_m h_{\text{r-f}} (T_r - T_f)$
Description	Q17 calculates the Heat flow convection of recipient toward the fluid
	$A_m$ is the wet inside the container (m <sup>2</sup> ).
	$h_{\rm r-f}$ is the thermal flux difference between Reflector and fluid inside the container
	$T_r - T_f$ is the temperature difference between reflector and fluid (°C).
Sources	(5)
Ref. By	IM <mark>1</mark>

Number	DD6
Label	Heat flux over all different object
Symbol	q
SI Units	$ m Wm^{-2}$
Equation	$q(t) = h_r(T_r - T_W(t)), \text{ over area } A_r$
Description	It is necessary to know the thermal conductivity of a material if you want to calculate the heat energy transferred through it
	q is the heat flux
	$h_r$ is the convective heat transfer coefficient between reflector and water
	$T_r$ is the temperature of reflector °C
	$T_W(t)$ is the temperature of water °C
	t is the time (s)
Sources	https://www.omnicalculator.com/physics/thermal-conductivity
Ref. By	IM <mark>1</mark>

### 4.2.5 Instance Models

This section transforms the problem defined in Section 4.1 into one which is expressed in mathematical terms. It uses concrete symbols defined in Section 4.2.4 to replace the abstract symbols in the models identified in Sections 4.2.2.

	We the
Number	IM1
Label	Balance of energy on the recipient to find $T_W$
Input	$A_r, \epsilon_r, T_r, T_f, T_{\text{int}2}, A_m, T_f, G$
	The input is constrained so that $\epsilon_r \leq 0$
Output	$T_f(t), t \geq 0$ , such that
	$ m m_W c_W rac{dT_W}{dt} = Q13 + 4Q14 - Q15 - Q16 - Q17$
Description	$A_r$ is the Area of Reflector (m <sup>2</sup> ).
	$m_{W}c_{W}\frac{dT_{W}}{dt} = Q13 + 4Q14 - Q15 - Q16 - Q17$ $A_{r}$ is the Area of Reflector (m <sup>2</sup> ). $\epsilon_{r}$ is the Emittance of recipient (W/m). $T_{r}$ is the Reflector temperature (°C). $T_{int2}$ is a temperature inside the box (°C). $T_{int2}$ is a temperature inside the box (°C). $T_{int2}$ is the Incidental solar radiation (W/m <sup>2</sup> ).  Shape of
	$T_r$ is the Reflector temperature (°C).
	$T_{\text{int2}}$ is a temperature inside the box (°C).
	G is the Incidental solar radiation (W/m <sup>2</sup> ).
	$T_f$ is a current temperature of Fluid at the time of t (°C).
	The above equation applies as long as the fluid is in liquid form, $0 < T_f < 100^{\circ}$ C, where $0^{\circ}$ C and $100^{\circ}$ C are the melting and boiling points of water (as we are using water for testing), respectively.
Sources	(5)
Ref. By	None

You any long LC do an englan

Number	IM2
Label	Heat energy in the recipient
Input	$C_W, m_W, T_{\mathrm{init}}, T_W(t)$
Output	$E_W(t), 0 \le t \le t_{\text{final}}, \text{ such that}$
	$E_W(t) = C_W m_W (T_W(t) - T_{\text{init}})$
Description	The above equation is derived using T2. $E_W$ is the change in thermal energy of the liquid water relative to the energy at the initial temperature $(T_{\text{init}})$ . $C_W$ is the specific heat capacity of liquid water and $m_W$ is the mass of the water. The change in temperature is the difference between the temperature at time t, $T_W$ , and the initial temperature, $T_{\text{init}}$ , this equation applies as long as $0 < T_W < 100^{\circ}\text{C}$ (A4).
Sources	(4)
Ref. By	None

### 4.2.6 Input Data Constraints

Table 1 shows the data constraints on the input and output variables. The column for physical constraints gives the physical limitations on the range of values that can be taken by the variable. The column for software constraints restricts the range of inputs to reasonable values. The software constraints will be helpful in the design stage for picking suitable algorithms. The constraints are conservative, to give the user of the model the flexibility to experiment with unusual situations. The column of typical values is intended to provide a feel for a common scenario. The uncertainty column provides an estimate of the confidence with which the physical quantities can be measured. This information would be part of the input if one were performing an uncertainty quantification exercise.

# 5 Requirements

This section provides the functional requirements, the business tasks that the software is expected to complete, and the nonfunctional requirements, the qualities that the software is expected to exhibit.

# 5.1 Functional Requirements

Table 1: Input Variables

Var	Physical Constraints	Software Constraints	Typical Value	Uncertainty
L	L > 0	$L_{\min} \le L \le L_{\max}$	0.12 m	-
$C_w$	$C_w > 0$	$C_w^{\min} \le C_w \le C_w^{\max}$	$4186 \text{ J/ (kg}^{\circ}\text{C)}$	-
$ au_g$	$0 \le \tau_g \le 1$	-	$0.48 \mathrm{\ m}$	-
$A_g$	$A_g > 0$	$A_g \le A_g^{\max}$	$0.24~\mathrm{m}^2$	-
r	r > 0	$r_{\min} \le r \le r_{\max}$	1	-
$T_{\rm init}$	$0 < T_{\rm init} < 100$	-	40 °C	-
G	G > 0	$G_{\min} \le L \le G_{\max}$	$476 \mathrm{\ W/m^2}$	-
$T_{ m f}$	$0 < T_{\rm f} < 100$	-	40 °C	-

Table 2: Output Variables

	Tal	ole 2: Output Variables	I think you shill need to work and your symbs & outputs. The best way to do this would be for you to
	Var	Physical Constraints	their would be for you to
	$T_r$ $E_w$	$T_{\text{init}} \le T_r$ $E_w > 0$	write code to solve the ODE. You could use Mathab to do it rebilizely quality.
7	7 W >		reblively quelly.

R1: Provide the inputs specific to Solar Box (Area of glass, Current Temperature of reflector/fluid/glass, Area of reflector) and other parameters (Incidental Solar Radiation, Reflectors angle, and number of reflectors)

R2: Verify the given inputs are in correct form and satisfy the required physical constraints given in the table 1

R3: Calculate and output the balance of energy on recipient  $T_W(t)$  over the simulation - Sous It is the origina? time(from IM1)

R4: Calculate and output the energy in the water (fluid - recipient)  $E_W(t)$  over the simulation time(from IM2)

#### 5.2 Nonfunctional Requirements

This problem is small in size and relatively simple, so performance is not a priority. Any reasonable implementation will be very quick and use minimal storage. Rather than performance, the non-functional requirement priorities are

rol værifiable

NFR1: Correctness: The calculated temperature should be correct and behave the same in all different use-cases. Not a reg.

NFR2: Verifiability: The result will be verifiable using the VnV plan.

NFR3: Understandability: The system accepts the simple inputs from the user and then user will gets the temperature value as a output. So, this will be easy for any new user to Cambagnoss understand the system.

NFR4: Reusability: The system only focuses on the temperature inside the box. But we can extend it to calculate the temperature at different points in Solar cooker where we can reuse this system. Raps are not arguments by why a quality is achieved, his should NFR5: Maintainability: The traceability between requirements, assumptions, theoretical models, general definition and the state of the state of

els, general definitions, data definitions, instance models, likely changes, and unlikely don't say how you will ashieve normalist shilling, say what you require changes is completely recorded in traceability matrices.

#### Likely Changes 6

LC1: A7 The other form of energy such as Mechanical energy may apply as a part of energy consideration.

Wic is whitely. The initial energy to the leave of the reflector will change over the different time during the day

which is totally based on the sun rays.

#### Unlikely Changes 7

UC1: A5 The given calculation for the inner temperature for the box(int2) in the assumption will not change throughout the whole process.

#### 8 Traceability Matrices and Graphs

The purpose of the traceability matrices is to provide easy references on what has to be additionally modified if a certain component is changed. Every time a component is changed, the items in the column of that component that are marked with an "X" may have to be modified as well. Table 5 shows the dependencies of theoretical models, general definitions, data definitions, and instance models with each other. Table 3 shows the dependencies of instance models, requirements, and data constraints on each other. Table 4 shows the dependencies of theoretical models, general definitions, data definitions, instance models, and likely changes on the assumptions.

	IM1	IM2	4.2.6	R1	R2	R3	R4
IM1		X				X	
IM2	X						X
R1							
R2			X				
R3	X						
R4		X					

Table 3: Traceability Matrix Showing the Connections Between Requirements and Instance Models

	A1	A2	A3	A4	A5	A6	A7	A8
T1								
T2				X				
GD1	X							
GD2		X	X					
DD1					X			
DD2						X		
DD3	X							
DD4	X							
$DD_5$								
DD6								X
IM1	X			X	X	X	X	
IM2								
LC1							X	
LC2								X

Table 4: Traceability Matrix Showing the Connections Between Assumptions and Other Items

	T1	T2	GD1	GD2	DD1	$DD_2$	$DD_3$	DD4	$DD_{5}$	$DD_6$	IM1	IM2
T1			X		X						X	
T2												X
GD1	X				X				X			
$GD_2$							X	X				
DD1	X		X								X	
$DD_2$											X	
$DD_3$				X							X	
DD4				X							X	
$DD_{5}$	X		X								X	
DD6	X										X	
IM1	X				X	X	X	X	X	X		
IM2		X										

Table 5: Traceability Matrix Showing the Connections Between Items of Different Sections

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