

# The Russell Transformation

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## Abstract

This document describes the “Russell” transformation, which is used to produce a fictitious independent variable for step-size control in  $N$ -body gravitational environments.

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## 1 The Russell Transformation

The transformation takes the form

$$dt = g ds, \tag{1}$$

where

$$g = \prod_{i=1}^N \rho_i^\alpha, \tag{2}$$

where

$$\rho_i = \frac{A^2 + A}{A + \left( \frac{A(1-C)}{C+A} \right)^{\frac{r_i}{B r_{H,i}}} } - A. \tag{3}$$

Then, the equations of motion are written as

$$\mathbf{f}_s = \frac{d\mathbf{x}}{ds} \quad (4)$$

$$= \mathbf{f}_t \frac{dt}{ds} \quad (5)$$

$$= \mathbf{f}_t g \quad (6)$$

## 2 Jacobian of the Russell Transformation

We require the Jacobians  $\frac{\partial \mathbf{f}_s}{\partial \mathbf{x}}$  and  $\frac{\partial \mathbf{f}_s}{\partial s}$ .

$$\frac{\partial \mathbf{f}_s}{\partial \mathbf{x}} = \frac{\partial}{\partial \mathbf{x}} [\mathbf{f}_t g] \quad (7)$$

$$= \frac{\partial \mathbf{f}_t}{\partial \mathbf{x}} g + \mathbf{f}_t \frac{\partial g}{\partial \mathbf{x}} \quad (8)$$

$$\frac{\partial \mathbf{f}_s}{\partial s} = \frac{\partial \mathbf{f}_s}{\partial t} \frac{dt}{ds} \quad (9)$$

$$= \frac{\partial}{\partial t} [\mathbf{f}_t g] g \quad (10)$$

$$= \frac{\partial \mathbf{f}_t}{\partial t} g^2 + \mathbf{f}_t \frac{\partial g}{\partial t} g \quad (11)$$

$\frac{\partial \mathbf{f}_t}{\partial \mathbf{x}}$  and  $\frac{\partial \mathbf{f}_t}{\partial t}$  are the usual Jacobians for equations of motion when time is the independent variable, and  $\mathbf{f}_t$  are the time equations of motion. Thus, the only terms that need to be derived are  $\frac{\partial g}{\partial \mathbf{x}}$  and  $\frac{\partial g}{\partial t}$ .

## 3 Jacobian of $\rho_i$

In  $g$ , the only non-constant terms are the  $\rho_i$ . Each  $\rho_i$  is solely dependent on  $r_i$ . Using MATLAB symbolic math, we arrive at

$$\frac{\partial \rho_i}{\partial r_i} = -\frac{A \gamma^{\frac{r_i}{Br_{H,i}}} \log(\gamma) (A+1)}{Br_{H,i} \left( A + \gamma^{\frac{r_i}{Br_{H,i}}} \right)^2} \quad (12)$$

$$\gamma \triangleq \frac{A(1-C)}{C+A}, \quad (13)$$

where  $\gamma$  is a convenience function. Then,  $r_i$  is only directly dependent on  $\mathbf{r}_i$ :

$$\frac{\partial r_i}{\partial \mathbf{x}} = \frac{\partial r_i}{\partial \mathbf{r}_i} \frac{\partial \mathbf{r}_i}{\partial \mathbf{x}} \quad (14)$$

$$\frac{\partial r_i}{\partial \mathbf{r}_i} = \frac{\mathbf{r}_i^T}{r_i}. \quad (15)$$

If we call  $\mathbf{r}_i$  the vector from the spacecraft to body  $i$  and  $\mathbf{r}_{c,i}$  the vector from the central body of integration to body  $i$ , then

$$\mathbf{r}_i = \mathbf{r}_{c,i} - \mathbf{r}. \quad (16)$$

The derivatives are

$$\frac{\partial \mathbf{r}_i}{\partial \mathbf{x}} = \frac{\partial}{\partial \mathbf{x}} (\mathbf{r}_{c,i} - \mathbf{r}). \quad (17)$$

In Eq. (17),  $\mathbf{r}_{c,i}$  depends only on time, and  $\mathbf{r}$  depends only on the position state of the spacecraft. So,

$$\frac{\partial \mathbf{r}_i}{\partial t} = \mathbf{v}_{c,i} \quad (18)$$

$$\frac{\partial \mathbf{r}_i}{\partial \mathbf{r}} = -\mathbf{I} \quad (19)$$

and all other derivatives are zero.

So,

$$\frac{\partial \rho_i}{\partial \mathbf{x}} = \frac{\partial \rho_i}{\partial r_i} \frac{\partial r_i}{\partial \mathbf{x}} \frac{\partial \mathbf{r}_i}{\partial \mathbf{x}}, \quad (20)$$

where we may assume that  $t$  is part of the augmented state vector.

## 4 Jacobian of $g$

The derivative of  $g$  with respect to each of the  $\rho_i$  is

$$\frac{\partial g}{\partial \rho_i} = \alpha \rho_i^{\alpha-1} \prod_{\substack{j=1 \\ j \neq i}}^N \rho_j^\alpha. \quad (21)$$

Then, if we concatenate all  $\rho_i$  into the vector  $\boldsymbol{\rho}$ , we finally get

$$\frac{\partial g}{\partial \mathbf{x}} = \frac{\partial g}{\partial \boldsymbol{\rho}} \frac{\partial \boldsymbol{\rho}}{\partial \mathbf{x}}, \quad (22)$$

where we may assume that  $t$  is part of the augmented state vector.