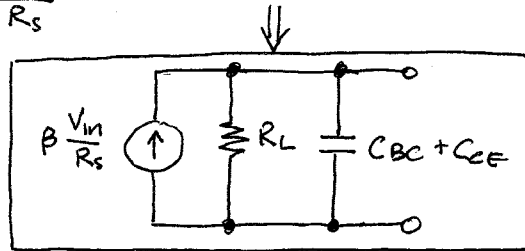
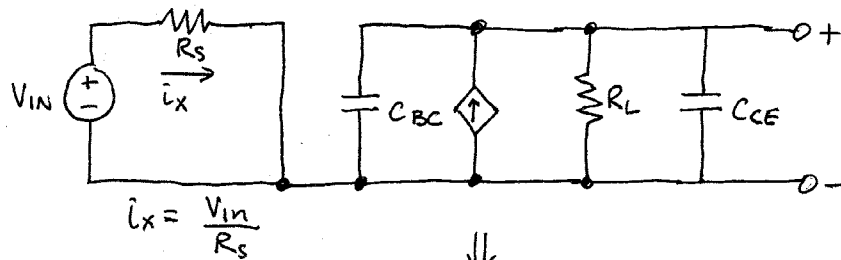
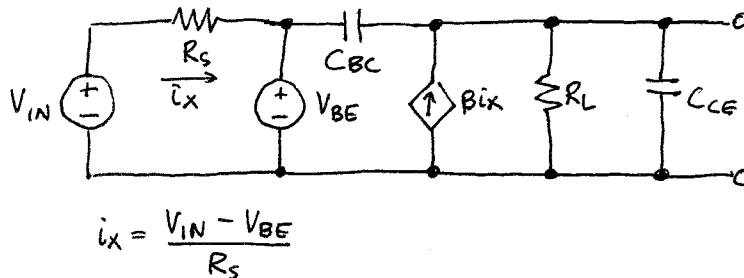


MT#2 Problem 3

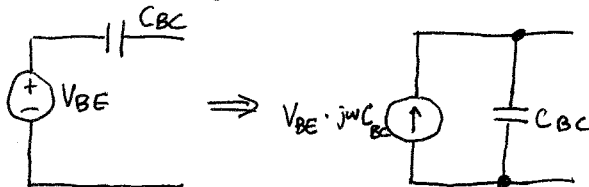
(a) assuming V_{BE} is a DC voltage: \rightarrow it becomes a short circuit



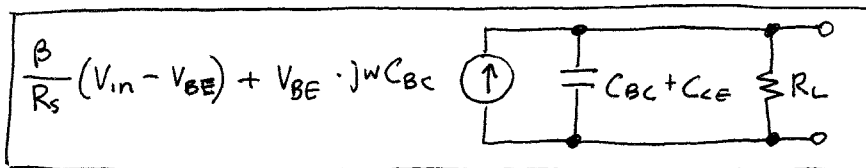
assuming V_{BE} is an AC voltage:



Thevenin to Norton:



Substitute into above ckt:



(b) V_{BE} is DC

$$V_{out} = \frac{\beta}{R_S} \cdot V_{in} \cdot \left(R_L \parallel \frac{1}{j\omega(C_{BC} + C_{CE})} \right) \Rightarrow \boxed{\frac{V_{out}}{V_{in}} = \frac{\beta}{R_S} \left[\frac{R_L}{1 + j\omega(C_{BC} + C_{CE})R_L} \right]}$$

V_{BE} is AC

$$V_{out} = \left[\frac{\beta}{R_S} \cdot V_{in} - \frac{\beta}{R_S} \cdot V_{BE} + V_{BE} \cdot j\omega C_{BC} \right] \cdot \left[\frac{R_L}{1 + j\omega(C_{BC} + C_{CE})R_L} \right]$$

In this case, the output voltage is a function of both V_{in} and V_{BE} .

By superposition, the total output is:

$$V_{out} = H_1(\omega) \cdot V_{in} + H_2(\omega) \cdot V_{BE} \quad \text{where} \quad \begin{cases} H_1(\omega) \triangleq \frac{V_{out}}{V_{in}} \Big|_{V_{BE}=0} \\ H_2(\omega) \triangleq \frac{V_{out}}{V_{BE}} \Big|_{V_{in}=0} \end{cases} \rightarrow$$

MT#2 Problem 3

(b) continued...

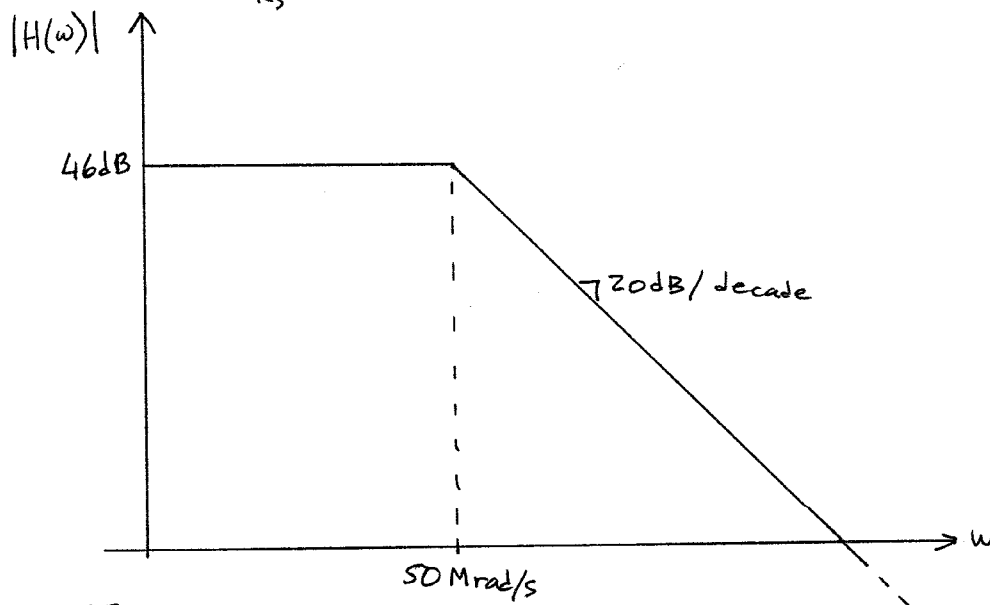
The question asked for $\frac{V_{out}}{V_{in}}$, which is $H_1(\omega)$. So, we only need to write that transfer function:

$$V_{out}|_{V_{BE}=0} = \left[\frac{\beta}{R_s} \cdot V_{in} \right] \cdot \left[\frac{R_L}{1 + j\omega(C_{bc} + C_{ce})R_L} \right]$$

$$H_1(\omega) = \frac{V_{out}}{V_{in}}|_{V_{BE}=0} = \left[\frac{\beta}{R_s} \right] \left[\frac{R_L}{1 + j\omega(C_{bc} + C_{ce})R_L} \right]$$

(this is the same as the answer in the DC case above)

(c) The transfer function is a single-pole lowpass with DC gain equal to $\frac{\beta R_L}{R_s}$ and the pole located at $\omega = \frac{1}{(C_{bc} + C_{ce})R_L}$



$$\frac{\beta R_L}{R_s} = 200$$

$$20 \log(200) = 46 \text{ dB}$$

$$\frac{1}{(C_{bc} + C_{ce})R_L} = 50 \text{ Mrad/s} = 8 \text{ MHz}$$