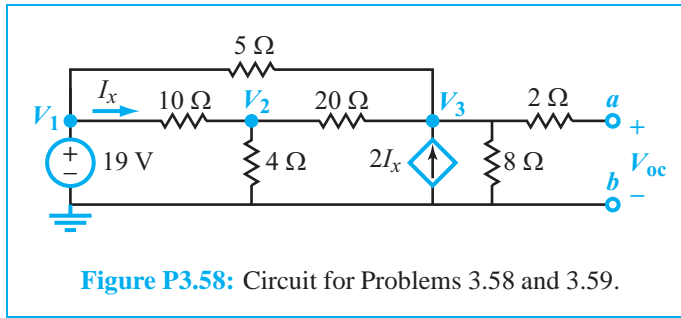


Problem 3.58 Find the Thévenin equivalent circuit at terminals (a, b) of the circuit in Fig. P3.58.



Solution:

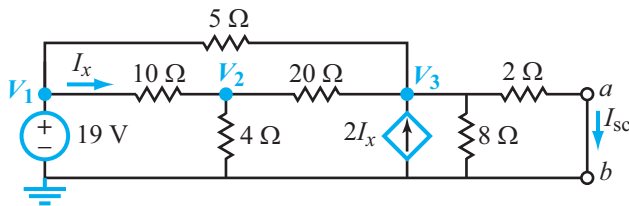
$$\begin{aligned} V_1 &= 19 \text{ V} \\ \frac{V_2 - V_1}{10} + \frac{V_2}{4} + \frac{V_2 - V_3}{20} &= 0 \\ \frac{V_3 - V_2}{20} + \frac{V_3}{8} + \frac{V_3 - V_1}{5} - 2I_x &= 0 \\ I_x &= \frac{V_1 - V_2}{10} \end{aligned}$$

Simultaneous solution of the above equations yields:

$$\begin{aligned} V_2 &= 6.94 \text{ V}, \quad V_3 = 17.49 \text{ V}. \\ V_{\text{Th}} = V_{\text{oc}} &= V_3 = 17.49 \text{ V}. \end{aligned}$$

To find R_{Th} , we calculate I_{sc} :

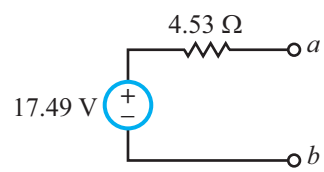
$$\begin{aligned} V_1 &= 19 \text{ V} \\ \frac{V_2 - V_1}{10} + \frac{V_2}{4} - \frac{V_2 - V_3}{20} &= 0 \\ \frac{V_3 - V_2}{20} + \frac{V_3}{8} + \frac{V_3}{2} + \frac{V_3 - V_1}{5} - 2I_x &= 0 \\ I_x &= \frac{V_1 - V_2}{10} \end{aligned}$$



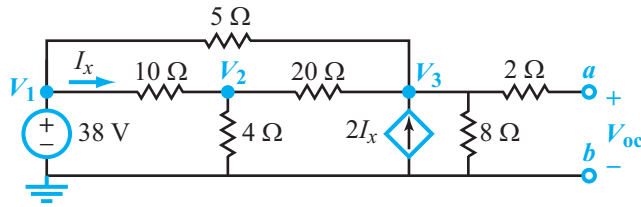
Solution is: $V_2 = 5.71 \text{ V}$, $V_3 = 7.71 \text{ V}$.

$$\begin{aligned} I_{\text{sc}} &= \frac{V_3}{2} = \frac{7.71}{2} = 3.86 \text{ A}. \\ R_{\text{Th}} &= \frac{V_{\text{oc}}}{I_{\text{sc}}} = \frac{17.49}{3.86} = 4.53 \Omega. \end{aligned}$$

Hence, the Thévenin circuit is



Problem 3.59 Find the Norton equivalent circuit of the circuit in Fig. P3.58 after increasing the magnitude of the voltage source to 38 V.



Solution:

$$V_1 = 38 \text{ V}$$

$$\frac{V_2 - V_1}{10} + \frac{V_2}{4} + \frac{V_2 - V_3}{20} = 0$$

$$\frac{V_3 - V_2}{20} + \frac{V_3}{8} + \frac{V_3 - V_1}{5} - 2I_x = 0$$

$$I_x = \frac{V_1 - V_2}{10}$$

Simultaneous solution of the above equations yields:

$$V_2 = 13.87 \text{ V}, \quad V_3 = 35.0 \text{ V}.$$

$$V_{\text{Th}} = V_{\text{oc}} = V_3 = 35.0 \text{ V}.$$

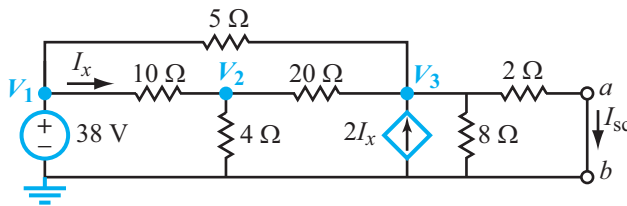
To find R_{Th} , we will calculate I_{sc} :

$$V_1 = 38 \text{ V}$$

$$\frac{V_2 - V_1}{10} + \frac{V_2}{4} + \frac{V_2 - V_3}{20} = 0$$

$$\frac{V_3 - V_2}{20} + \frac{V_3}{8} + \frac{V_3}{2} + \frac{V_3 - V_1}{5} - 2I_x = 0$$

$$I_x = \frac{V_1 - V_2}{10}$$

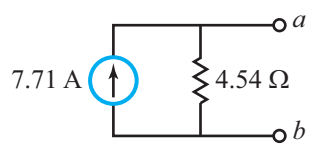


Solution is: $V_2 = 11.43 \text{ V}$, $V_3 = 15.41 \text{ V}$.

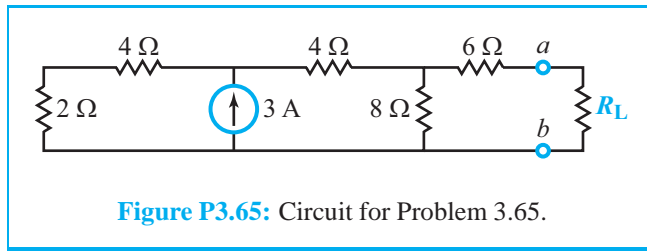
$$I_{\text{sc}} = \frac{V_3}{2} = \frac{15.41}{2} = 7.71 \text{ A}.$$

$$R_{\text{Th}} = \frac{V_{\text{oc}}}{I_{\text{sc}}} = \frac{35.0}{7.71} = 4.54 \Omega.$$

Norton equivalent circuit is



Problem 3.65 What value of the load resistor R_L will extract the maximum amount of power from the circuit in Fig. P3.65, and how much power will that be?

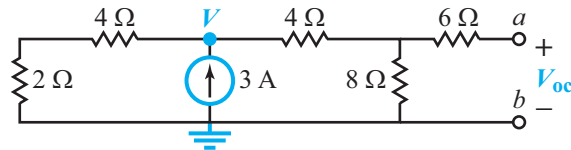


Solution: We start by obtaining the Thévenin equivalent circuit at terminals (a, b) , as if R_L were not there. We first find V_{oc} :

$$\frac{V}{6} - 3 + \frac{V}{12} = 0$$

$$V = 12 \text{ V.}$$

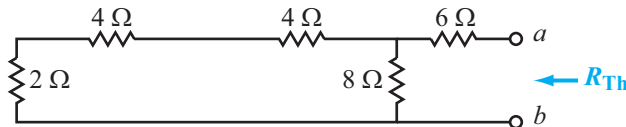
Hence,



Voltage division gives:

$$V_{Th} = V_{oc} = \left(\frac{8}{4+8} \right) V = \frac{8}{12} \times 12 = 8 \text{ V.}$$

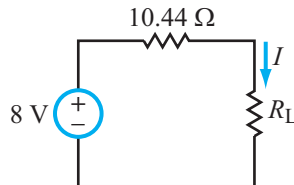
Next, we suppress the current source to find R_{Th} :



Simplification leads to:

$$R_{Th} = 10.44 \Omega.$$

Equivalent circuit:



For maximum power transfer to R_L ,

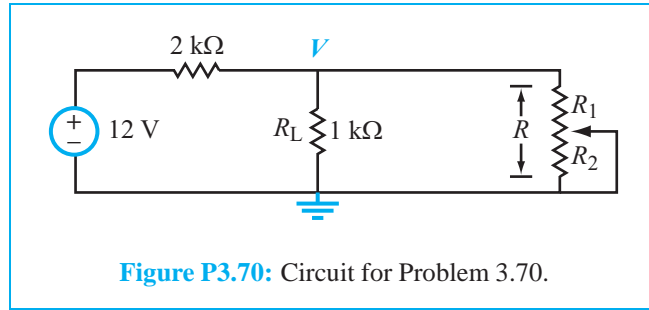
$$R_L = R_{Th} = 10.44 \Omega$$

$$I = \frac{8}{2 \times 10.44} = 0.38 \text{ A}$$

$$P_{\max} = I^2 R_L = (0.38)^2 \times 10.44 = 1.53 \text{ W.}$$

Problem 3.70 In the circuit shown in Fig. P3.70, a potentiometer is connected across the load resistor R_L . The total resistance of the potentiometer is $R = R_1 + R_2 = 5 \text{ k}\Omega$.

- (a) Obtain an expression for the power P_L dissipated in R_L for any value of R_1 .
- (b) Plot P_L versus R_1 over the full range made possible by the potentiometer's wiper.



Solution:

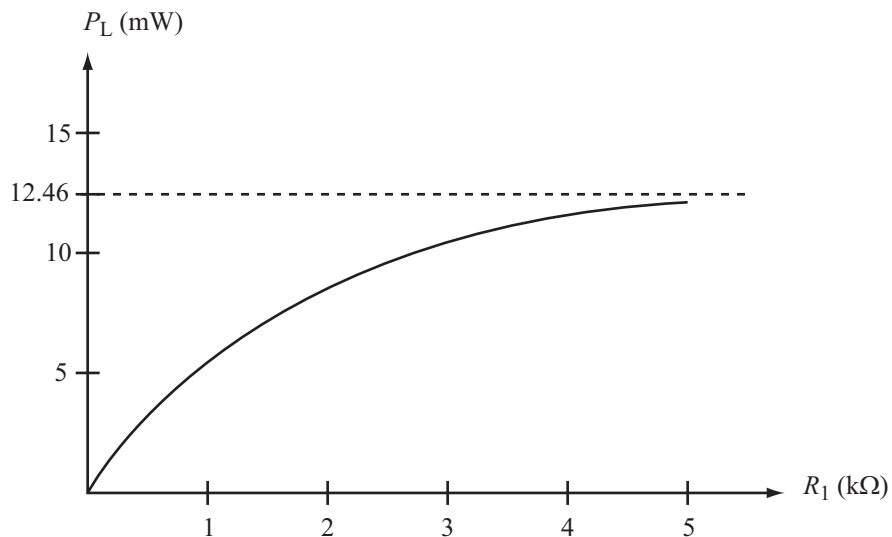
(a)

$$\frac{V - 12}{2\text{k}} + \frac{V}{1\text{k}} + \frac{V}{R_1} = 0$$

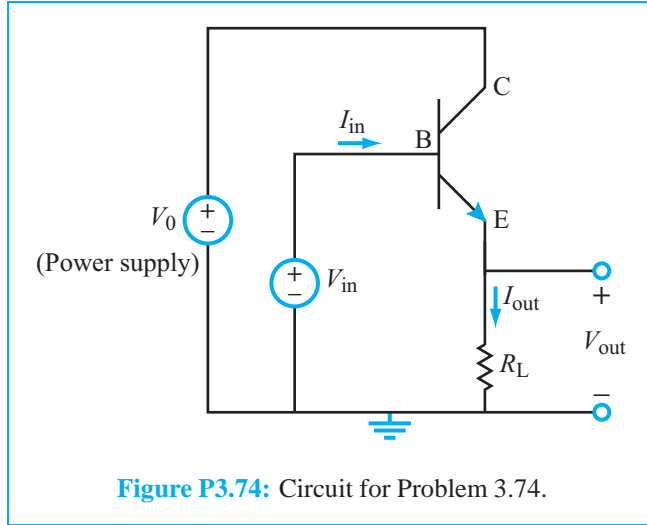
$$V = \frac{12R_1}{3R_1 + 2}, \quad \text{with } R_1 \text{ measured in k}\Omega.$$

$$P_L = \frac{V^2}{R_L} = \frac{V^2}{1\text{k}} = \left(\frac{12R_1}{3R_1 + 2} \right)^2 \times 10^{-3}$$

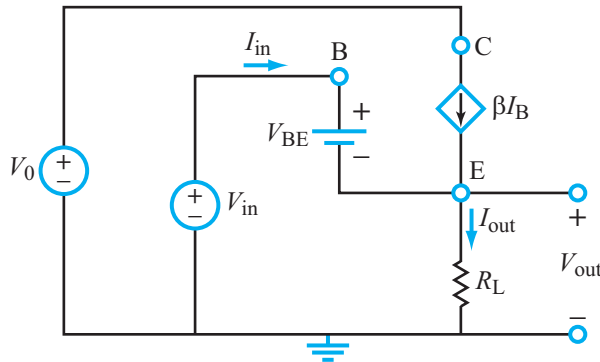
(b)



Problem 3.74 The circuit in Fig. P3.74 is a BJT *common collector amplifier*. Find both the voltage gain ($A_V = V_{out}/V_{in}$) and the current gain ($A_I = I_{out}/I_{in}$). Assume $V_{in} \gg V_{BE}$.



Solution: Upon replacing the BJT with its equivalent circuit model, we obtain the circuit shown in Fig. P3.74(b).



From

$$V_{out} = V_{in} - V_{BE},$$

$$A_V = \frac{V_{out}}{V_{in}} = 1 - \frac{V_{BE}}{V_{in}} \simeq 1 \quad (\text{since } V_{BE} \ll V_{in}).$$

Also,

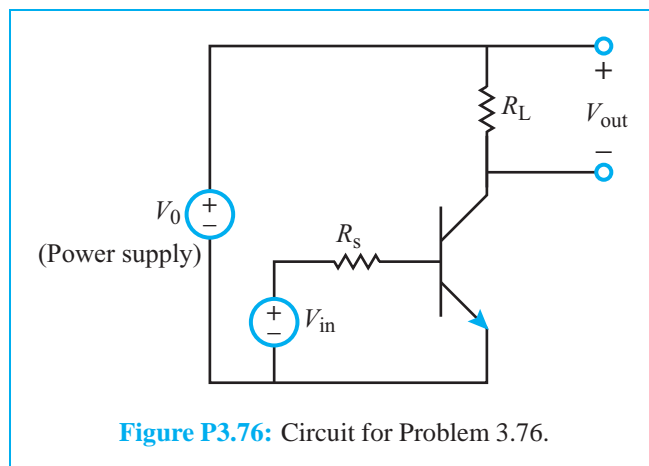
$$I_{in} = I_B,$$

$$I_{out} = I_{in} + \beta I_B = I_{in}(1 + \beta).$$

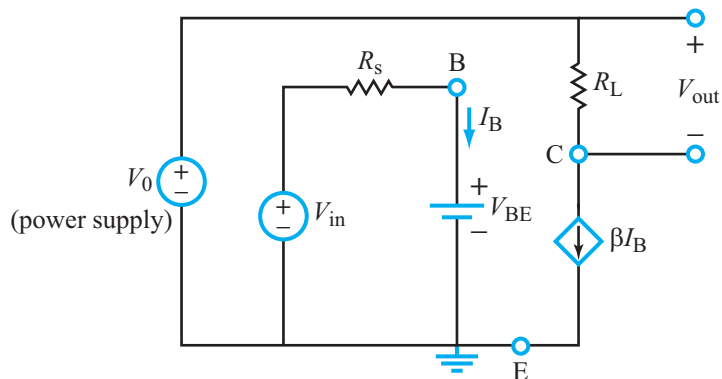
Hence,

$$A_I = \frac{I_{out}}{I_{in}} = 1 + \beta \simeq \beta \quad (\text{since } \beta \gg 1).$$

Problem 3.76 The circuit in Fig. P3.76 is a BJT *common emitter amplifier*. Find V_{out} as a function of V_{in} .



Solution: Upon replacing the BJT with its equivalent circuit model, we obtain the circuit in Fig. 3.76(b).



$$V_{\text{out}} = \beta I_B R_L,$$

$$I_B = \frac{V_{\text{in}} - V_{\text{BE}}}{R_s}.$$

Hence,

$$V_{\text{out}} = \beta \left(\frac{R_L}{R_s} \right) (V_{\text{in}} - V_{\text{BE}}) \simeq \left(\beta \frac{R_L}{R_s} \right) V_{\text{in}} \quad (\text{if } V_{\text{in}} \gg V_{\text{BE}}).$$