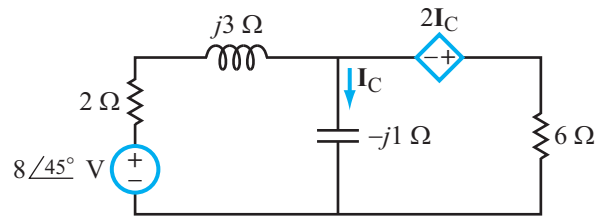
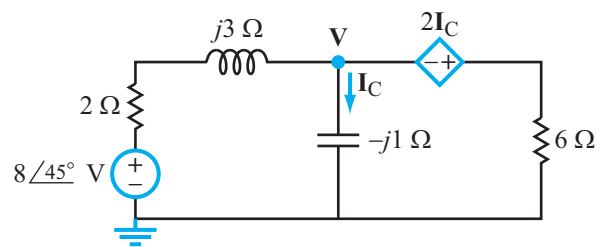


**Problem 7.51** Apply nodal analysis to determine  $\mathbf{I}_C$  in the circuit of Fig. P7.51.



**Figure P7.51:** Circuits for Problems 7.51 and 7.52.

**Solution:**



$$\frac{\mathbf{V} - 8e^{j45^\circ}}{2 + j3} + \frac{\mathbf{V}}{-j1} + \frac{\mathbf{V} + 2\mathbf{I}_C}{6} = 0$$

Also,

$$\mathbf{I}_C = \frac{\mathbf{V}}{-j1} = j\mathbf{V}.$$

Hence,

$$\mathbf{V} \left( \frac{1}{2 + j3} + j + \frac{1}{6} + \frac{j}{3} \right) = \frac{8e^{j45^\circ}}{2 + j3}$$

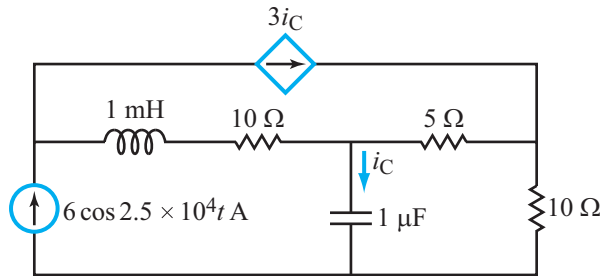
Solution gives

$$\mathbf{V} = \frac{48e^{j45^\circ}}{-(16 - j19)} = 1.93e^{-j85.1^\circ} \text{ V}$$

and

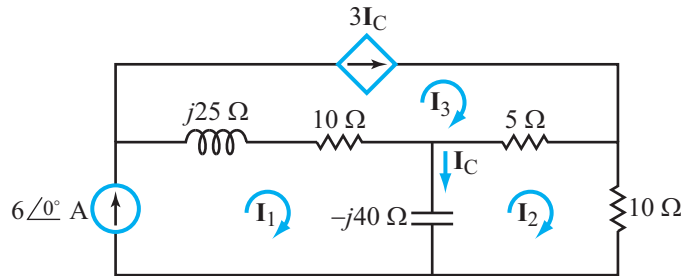
$$\mathbf{I}_C = j\mathbf{V} = 1.93e^{j4.9^\circ} \text{ A.}$$

**Problem 7.56** Use any analysis technique of your choice to determine  $i_C(t)$  in the circuit of Fig. P7-56.



**Figure P7.56:** Circuit for Problem 7.56.

**Solution:**



$$Z_L = j\omega L = j2.5 \times 10^4 \times 10^{-3} = j25 \Omega$$

$$Z_C = \frac{-j}{\omega C} = \frac{-j}{2.5 \times 10^4 \times 10^{-6}} = -j40 \Omega$$

The mesh-current method gives:

$$\begin{aligned} \text{Mesh 1:} \quad & \mathbf{I}_1 = 6 \text{ A} \\ \text{Mesh 2:} \quad & -j40(\mathbf{I}_2 - \mathbf{I}_1) + 5(\mathbf{I}_2 - \mathbf{I}_3) + 10\mathbf{I}_2 = 0 \\ \text{Mesh 3:} \quad & \mathbf{I}_3 = 3\mathbf{I}_C \\ \text{Auxiliary:} \quad & \mathbf{I}_C = \mathbf{I}_1 - \mathbf{I}_2. \end{aligned}$$

Simultaneous solution leads to

$$\mathbf{I}_1 = 6 \text{ A}, \quad \mathbf{I}_2 = (4.92 - j1.44) \text{ A}.$$

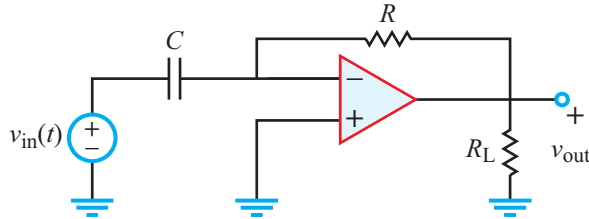
$$\begin{aligned} \mathbf{I}_C &= \mathbf{I}_1 - \mathbf{I}_2 \\ &= 1.8e^{j53.13^\circ} \text{ A}. \end{aligned}$$

$$\begin{aligned} i_C(t) &= \Re[\mathbf{I}_C e^{j\omega t}] \\ &= 1.8 \cos(2.5 \times 10^4 t + 53.13^\circ) \quad (\text{A}). \end{aligned}$$

**Problem 7.58** The input signal in the op-amp circuit of Fig. P7.58 is given by

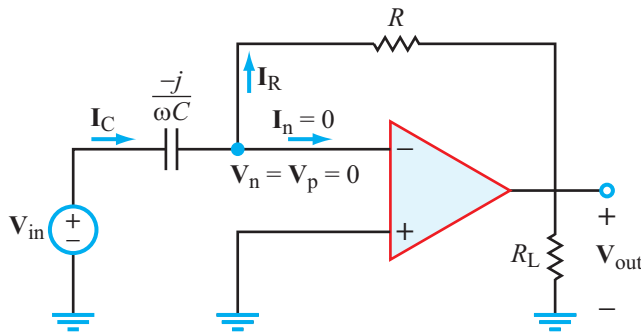
$$v_{\text{in}}(t) = V_0 \cos \omega t.$$

Assuming the op amp is operating within its linear range, obtain an expression for  $v_{\text{out}}(t)$  by applying the phasor-domain technique, and then evaluate it for  $\omega RC = 1$ .



**Figure P7.58:** Op-amp circuit for Problem 7.58.

**Solution:**



$$\mathbf{V}_{\text{in}} = V_0.$$

$$\text{Because } \mathbf{V}_n = \mathbf{V}_p = 0,$$

$$\mathbf{I}_C = \frac{\mathbf{V}_{\text{in}}}{\mathbf{Z}_C} = \frac{\mathbf{V}_{\text{in}}}{-j/\omega C} = j\omega C \mathbf{V}_{\text{in}}.$$

$$\mathbf{I}_R = \frac{\mathbf{V}_n - \mathbf{V}_{\text{out}}}{R}.$$

$$\text{Also, } \mathbf{V}_n = 0 \text{ and } \mathbf{I}_n = 0.$$

Hence

$$\begin{aligned} \mathbf{V}_{\text{out}} &= -R\mathbf{I}_R \\ &= -R\mathbf{I}_C \\ &= -j\omega RC \mathbf{V}_{\text{in}} \\ &= -j\omega RC V_0 \\ &= \omega RC V_0 e^{-j90^\circ}. \end{aligned}$$

$$\begin{aligned} v_{\text{out}}(t) &= \Re[\mathbf{V}_{\text{out}} e^{j\omega t}] \\ &= \Re[\omega RC V_0 e^{-j90^\circ} e^{j\omega t}] \\ &= \omega RC V_0 \cos(\omega t - 90^\circ) \end{aligned}$$

$$= \omega RC V_0 \sin \omega t.$$

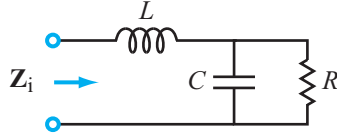
For  $\omega RC = 1$ ,

$$v_{\text{out}}(t) = V_0 \sin \omega t.$$

## CHAPTER 9

### Section 9-1: Transfer Function

**Problem 9.1** Determine the resonant frequency of the circuit shown in Fig. P9.1, given that  $R = 100\ \Omega$ ,  $L = 5\ \text{mH}$ , and  $C = 1\ \mu\text{F}$ .



**Figure P9.1:** Circuit for Problem 9.1.

**Solution:**

$$\begin{aligned} \mathbf{Z}_i &= \left( R \parallel \frac{1}{j\omega C} \right) + j\omega L \\ &= \frac{\frac{R}{j\omega C}}{R + \frac{1}{j\omega C}} + j\omega L \\ &= \frac{R}{1 + j\omega RC} + j\omega L \\ &= \frac{R(1 - \omega^2 LC) + j\omega L}{1 + j\omega RC} \times \frac{1 - j\omega RC}{1 - j\omega RC} \\ &= \frac{[R(1 - \omega^2 LC) + \omega^2 RLC] + j[\omega L - \omega R^2 C(1 - \omega^2 LC)]}{1 + \omega^2 R^2 C^2} \\ &= \frac{R + j\omega[L - R^2 C + \omega^2 R^2 LC^2]}{1 + \omega^2 R^2 C^2}. \end{aligned}$$

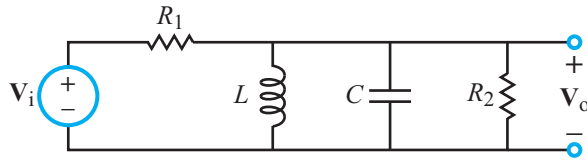
At resonance, the imaginary part of  $\mathbf{Z}_i$  is zero. Thus,

$$\omega[L - R^2 C + \omega^2 R^2 LC^2] = 0,$$

which gives two solutions, a trivial resonance at  $\omega = 0$ , and

$$\begin{aligned} \omega_0 &= \sqrt{\frac{1}{LC} - \frac{1}{R^2 C^2}} \\ &= \sqrt{\frac{1}{5 \times 10^{-3} \times 10^{-6}} - \frac{1}{10^4 \times 10^{-12}}} = 10^4 \text{ rad/s}. \end{aligned}$$

**Problem 9.4** For the circuit shown in Fig. P9.4, determine (a) the transfer function  $\mathbf{H} = \mathbf{V}_o/\mathbf{V}_i$ , and (b) the frequency  $\omega_0$  at which  $\mathbf{H}$  is purely real.



**Figure P9.4:** Circuit for Problem 9.4.

**Solution:**

**(a)** KCL at node  $\mathbf{V}_o$ :

$$\frac{\mathbf{V}_o - \mathbf{V}_i}{R_1} + \mathbf{V}_o \left( \frac{1}{j\omega L} + j\omega C + \frac{1}{R_2} \right) = 0.$$

Solution leads to

$$\mathbf{H} = \frac{\mathbf{V}_o}{\mathbf{V}_i} = \frac{jR_2\omega L}{R_1R_2(1 - \omega^2 LC) + j\omega L(R_1 + R_2)}.$$

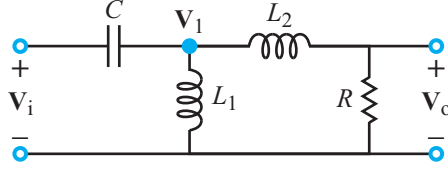
**(b)** Rationalizing the expression for  $\mathbf{H}$ :

$$\begin{aligned} \mathbf{H} &= \frac{jR_2\omega L}{R_1R_2(1 - \omega^2 LC) + j\omega L(R_1 + R_2)} \times \frac{R_1R_2(1 - \omega^2 LC) - j\omega L(R_1 + R_2)}{R_1R_2(1 - \omega^2 LC) - j\omega L(R_1 + R_2)} \\ &= \frac{\omega^2 R_2 L^2 (R_1 + R_2) + j\omega L R_1 R_2^2 (1 - \omega^2 LC)}{R_1^2 R_2^2 (1 - \omega^2 LC)^2 + \omega^2 L^2 (R_1 + R_2)^2}. \end{aligned}$$

The imaginary part of  $\mathbf{H}$  is zero when  $\omega = 0$  (trivial resonance) or when

$$\omega_0 = \frac{1}{\sqrt{LC}}.$$

**Problem 9.3** For the circuit shown in Fig. P9.3, determine (a) the transfer function  $\mathbf{H} = \mathbf{V}_o/\mathbf{V}_i$ , and (b) the frequency  $\omega_0$  at which  $\mathbf{H}$  is purely real.



**Figure P9.3:** Circuit for Problem 9.3.

**Solution:**

(a) KCL at node  $\mathbf{V}_1$  gives:

$$\frac{\mathbf{V}_1 - \mathbf{V}_i}{\mathbf{Z}_C} + \frac{\mathbf{V}_1}{\mathbf{Z}_{L_1}} + \frac{\mathbf{V}_1}{R + \mathbf{Z}_{L_2}} = 0,$$

where  $\mathbf{Z}_C = 1/j\omega C$ ,  $\mathbf{Z}_{L_1} = j\omega L_1$ , and  $\mathbf{Z}_{L_2} = j\omega L_2$ .

Also, voltage division gives

$$\mathbf{V}_o = \frac{\mathbf{V}_1 R}{R + j\omega L_2}.$$

Solving for the transfer function gives

$$\mathbf{H} = \frac{\mathbf{V}_o}{\mathbf{V}_i} = \frac{-\omega^2 R L_1 C}{R(1 - \omega^2 L_1 C) + j\omega(L_1 + L_2 - \omega^2 L_1 L_2 C)}.$$

(b) We need to rationalize the expression for  $\mathbf{H}$ :

$$\begin{aligned} \mathbf{H} &= \frac{-\omega^2 R L_1 C}{R(1 - \omega^2 L_1 C) + j\omega(L_1 + L_2 - \omega^2 L_1 L_2 C)} \\ &\quad \times \frac{R(1 - \omega^2 L_1 C) - j\omega(L_1 + L_2 - \omega^2 L_1 L_2 C)}{R(1 - \omega^2 L_1 C) - j\omega(L_1 + L_2 - \omega^2 L_1 L_2 C)} \\ &= \frac{-\omega^2 R^2 L_1 C(1 - \omega^2 L_1 C) + j\omega^3 R L_1 C(L_1 + L_2 - \omega^2 L_1 L_2 C)}{R^2(1 - \omega^2 L_1 C)^2 + \omega^2(L_1 + L_2 - \omega^2 L_1 L_2 C)^2}. \end{aligned}$$

The imaginary part of  $\mathbf{H}$  is zero if  $\omega = 0$  (trivial solution) or if

$$\omega_0 = \sqrt{\frac{L_1 + L_2}{L_1 L_2 C}}.$$