

# Measurement Protocol for Spiral Air-Core Electromagnets

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## 1 Preamble

Firstly, I need to make one thing clear. The described procedure is not an ideal way to measure inductance, but it is one of the two that I can think of, having current equipment. The most optimal way to measure the inductance is to use a *measuring device made for this exact purpose*, that is being an RLC meter. Chinese market offers multitude of solutions starting from several hundred euros. It's a worthy investment if STELAR wishes to standardize the measurements and create a more straightforward workflow and certification processes.

## 2 Prerequisites

In order to follow this guide, one must know how to use a VNA: calibration, measurements, data analysis. One would also benefit from understanding parallel RLC frequency response ( $Z_{11}$  parameters, phase behaviour near resonance)

## 3 Introduction

This document describes the procedure for measuring and extracting inductance values from spiral air-core multi-layer electromagnets using Vector Network Analyzer (VNA) impedance measurements. The method employs a two-step curve fitting approach that accounts for frequency-dependent skin effect in the resistance and extracts the inductance from the inductive reactance in the sub-resonant frequency regime.

### 3.1 Physical Model

The Device Under Test (DUT, air core single/multi-layer electromagnet) is modeled as a parallel RLC circuit<sup>1</sup> with the following characteristics:

- **Resistance (frequency-dependent):** The AC resistance increases with frequency due to skin effect:

$$R_{ac}(\omega) = \alpha \cdot \exp(\beta\sqrt{\omega}) \quad (1)$$

where  $\alpha \approx R_{dc}$  and  $\beta = \frac{(1+j)d}{\sqrt{2\rho}}$  - skin effect parameter (**not skin depth**  $\delta$ ).

- **Inductance:** The inductive reactance is linear with angular frequency:

$$X_L(\omega) = \omega L \quad (2)$$

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<sup>1</sup>It must be noted that the parallel RLC model works well *only* within restraints specified below. Readers are incentivized to come up with their own models if parallel RLC yields inadequate results.

- **Capacitance:** Parasitic inter-turn and layer-to-layer capacitance causes self-resonance at frequency  $f_{\text{SRF}}$ :

$$f_{\text{SRF}} = \frac{1}{2\pi\sqrt{LC}} \quad (3)$$

The complex impedance is:

$$Z(\omega) = R_{\text{ac}}(\omega) + j\omega L \quad (4)$$

valid for  $f \ll f_{\text{SRF}}$  (typically  $f < f_{\text{SRF}}/12$  to  $f_{\text{SRF}}/15$ ).

## 4 Equipment Requirements

- Vector Network Analyzer (VNA) with impedance measurement capability (e.g., S-parameter conversion to Z-parameters)
- Calibration kit appropriate for the DUT impedance range
- Measurement leads/cables with known characteristics
- Device Under Test (DUT): spiral air-core multi-layer electromagnet, or other RLC-model friendly device
- Connection fixtures for DUT mounting (crocodile)

## 5 Measurement Procedure

### 5.1 Step 1: Determine Self-Resonant Frequency (SRF)

The self-resonant frequency is the critical parameter that defines the valid measurement range. At  $f_{\text{SRF}}$ , the DUT transitions from inductive to capacitive behavior.

Connect the DUT to the VNA (initial calibration at VNA ports is sufficient for this step<sup>2</sup>).

Configure the VNA for impedance magnitude and phase measurements (or S11 with Smith chart display).

Set a wide frequency sweep covering the expected SRF range. For typical spiral air-core electromagnets, start with 100 kHz to 10 MHz.

Observe the impedance behavior:

- **Below SRF:** Impedance magnitude  $|Z|$  increases with frequency (inductive region)
- **At SRF:** Maximum impedance is reached
- **Above SRF:** Impedance magnitude decreases with frequency (capacitive region)

Identify the SRF from the VNA display:

- **Impedance magnitude:** Peak in  $|Z(f)| \rightarrow k\Omega, M\Omega, \text{etc.}$
- **Phase:** *Transition through 0° (or 180° phase flip<sup>3</sup>)*

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<sup>2</sup>that being said, one must be mindful of measurement range, i.e. the calibration must be satisfactory for selected range

<sup>3</sup>this is the most straightforward way to find SRF of parallel RLC element, prefer if possible

- **Smith chart:** Crossing from inductive (upper) to capacitive (lower) half-plane through the right-most (open circuit) point ( $|Z| \rightarrow \infty$ )

Record  $f_{\text{SRF}}$  precisely. Refine the frequency span around the resonance if needed for better resolution.

**Important:** The SRF value must be manually entered into the Python script in the variable `f_res`.

## 5.2 Step 2: VNA Calibration at DUT Plane

Proper calibration<sup>4</sup> is **critical** for accurate inductance extraction. The calibration must be performed at the DUT connection plane<sup>5</sup>, not at the VNA input ports.

### 5.2.1 Why Calibration at DUT Plane?

Measurement leads introduce:

- Series inductance ( $L_{\text{leads}}$ )
- Series resistance ( $R_{\text{leads}}$ )
- Parasitic capacitance

These parasitic elements will be included in the measured impedance if calibration is only performed at the VNA ports, resulting in incorrect inductance values.

### 5.2.2 Calibration Procedure

- 2.1 Attach the measurement leads/cables to the VNA.
- 2.2 Perform a full 1-port calibration (OPEN, SHORT<sup>6</sup>, LOAD) at the **DUT connection plane** (i.e., at the end of the measurement leads where the DUT will connect).
- 2.3 Use calibration standards appropriate for the expected impedance range:
  - **OPEN:** Disconnect leads (open circuit)
  - **SHORT:** Short-circuit at DUT plane
  - **LOAD:**  $50 \Omega$  termination (or appropriate reference impedance)
- 2.4 Set the frequency range for calibration to cover the measurement frequencies (determined in Step 3).
- 2.5 Verify calibration quality by checking residual errors (some VNAs provide calibration verification metrics).

## 5.3 Step 3: Select Measurement Frequencies

The valid measurement range must satisfy  $f \ll f_{\text{SRF}}$  to ensure the parallel RLC model reduces to series RL behavior.

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<sup>4</sup>not to be confused with calibration from p.5.1; this calibration is actually critical and may lead to overestimation of inductance.

<sup>5</sup>what is DUT plane? it is the input point of the device under test. So the calibration **must account** for the inductance and resistance of the leads

<sup>6</sup>Good luck finding one of those, by the way. My golden coated calibration kit which came with VNA was taken for parts, I guess, so create your own shorts

### 5.3.1 Frequency Selection Criteria

$$f_{\max} < \frac{f_{\text{SRF}}}{12} \quad \text{to} \quad \frac{f_{\text{SRF}}}{15} \quad (5)$$

**Example:** If  $f_{\text{SRF}} = 4.89 \text{ MHz}$ :

- Maximum measurement frequency:  $f_{\max} \approx 408 \text{ kHz}$  (using  $f_{\text{SRF}}/12$ )
- Recommended range:  $50 \text{ kHz}^7$  to  $400 \text{ kHz}$

### 5.3.2 Number and Distribution of Points

- Use at least 7–10 frequency points for reliable curve fitting
- Distribute points logarithmically or linearly across the frequency range
- Include lower frequencies ( $\sim 50 \text{ kHz}$ ) to capture near-DC resistance
- Ensure the highest frequency is still well below  $f_{\text{SRF}}/12$

## 5.4 Step 4: Impedance Measurements

**4.1** With the VNA calibrated at the DUT plane, connect the DUT.

**4.2** Configure the VNA to measure and display:

- Real part of impedance:  $\text{Re}(Z_{11})$
- Imaginary part of impedance:  $\text{Im}(Z_{11})$

**4.3** Set the frequency points as determined in Step 3.

**4.4** For each frequency point, record:

- Frequency:  $f$  (Hz)
- Real impedance:  $\text{Re}(Z_{11})$  ( $\Omega$ )
- Imaginary impedance:  $\text{Im}(Z_{11})$  ( $\Omega$ )

**4.5** Verify measurement stability:

- Check that  $\text{Im}(Z_{11}) > 0$  (inductive behavior)
- Verify that  $\text{Im}(Z_{11})$  increases approximately linearly with frequency
- Ensure  $\text{Re}(Z_{11})$  increases with frequency (skin effect)

**4.6** Export or manually record the data.

**Caution:** If measurements show  $\text{Im}(Z_{11}) < 0$ , you are likely above the SRF (overshoot). Reduce the maximum measurement frequency.

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<sup>7</sup>lowest available frequency available with current VNA model SV4401A

## 5.5 Step 5: Data Entry into Python Script

Edit the Python script to include your measurement data:

```
# Set the SRF (from Step 1)
f_res = 4.89e6 # Hz (example: 4.89 MHz)

# Enter measurement data (from Step 4)
frequencies = np.array([477e3, 400e3, 352e3, 300e3,
                        250e3, 200e3, 150e3, 103e3,
                        50e3]) # Hz

Z_real = np.array([2.09, 1.84, 1.7, 1.52, 1.31,
                   1.15, 0.95, 0.7, 0.428]) # Ohms

Z_imag = np.array([50.2, 42.5, 37.2, 32, 26.6,
                   21.5, 16.2, 11.2, 5.33]) # Ohms
```

### Notes:

- Frequencies must be in Hz (use scientific notation, e.g., 400e3 for 400 kHz)
- Arrays must have the same length
- Order doesn't matter (script handles unsorted data)

## 5.6 Step 6: Execute the Script

**6.1** Save the modified Python script.

**6.2** Run the script:

```
python rlc_fit.py
```

**6.3** The script will output fitting results to the console:

- Skin effect parameters:  $\alpha$  (approximate DC resistance) and  $\beta$
- Inductance:  $L$  with uncertainty
- Derived capacitance:  $C$  (from  $f_{SRF}$  and  $L$ )

**6.4** Examine the generated plots (4 subplots):

- **Top-left:** Real part fit (resistance with skin effect)
- **Top-right:** Imaginary part fit (inductive reactance)
- **Bottom-left:** Linearity check ( $\text{Im}(Z)$  vs.  $\omega$ )
- **Bottom-right:** Fit residuals<sup>8</sup>

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<sup>8</sup>the inductance fit still shows some systematic trends, the origins of which remain a mystery to the author. The magnitude of them, however, is so small, that it makes no difference **at the moment**. If you find the error in the model, feel free to e-mail me at denis.burov@proton.me

## 6 Results Interpretation and Validation

### 6.1 Expected Output

The console output provides:

```
TWO-STEP FIT: RESISTANCE + INDUCTANCE
=====
Input:
  f_resonance (known) = 4890.0 kHz
  Measurement range: 0.05 - 0.48 MHz

Step 1 - Skin effect (Re(Z) only):
  alpha = 0.XXX +/- 0.XXX Ohm
  beta = X.XXX +/- X.XXX x10^-3
  R_dc = X.XX Ohm

Step 2 - Inductance (Im(Z) only):
  L = XX.XX +/- X.XX uH
```

Derived:

```
C = XX.XX +/- X.XX nF (from f_res)
f_res (from L,C) = XXXX.X kHz (check)
R_ac(2 MHz) = XX.XX Ohm
```

### 6.2 Quality Checks

1. **Recalculated SRF:** The  $f_{\text{res}}$  calculated from fitted  $L$  and derived  $C$  should match the input  $f_{\text{SRF}}$  within a few percent. Large discrepancies indicate:
  - Measurement frequencies too close to SRF
  - Poor calibration
  - Inappropriate model (e.g., significant core losses, close to SRF)
2. **Residuals plot:** Residuals should be randomly distributed around zero<sup>9</sup> with magnitude much smaller than the measured values. Systematic trends indicate model inadequacy.
3. **Linearity check:** The  $\text{Im}(Z)$  vs.  $\omega$  plot should show excellent linearity. Deviations suggest proximity to resonance or measurement errors.
4. **Skin effect:** The real part should show exponential growth:  $e^{\sqrt{\omega}}$ . At low frequencies,  $R_{\text{ac}} \approx R_{\text{dc}} = \alpha$ .
5. **Uncertainty:** Check that parameter uncertainties are small relative to fitted values (typically < 5% for good measurements).

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<sup>9</sup>although they aren't quite random at the moment, see other footnote

### 6.3 Common Issues and Troubleshooting

| Symptom                                     | Likely Cause & Solution   |
|---|---|
| Poor fit to $\text{Im}(Z)$ (non-linear)     | Measurement frequencies too close to SRF. Reduce $f_{\text{max}}$ to $< f_{\text{SRF}}/15$ .  |
| Large residuals in $\text{Re}(Z)$           | Skin effect model may be inadequate. Check conductor geometry and consider proximity effects.   |
| Negative $\text{Im}(Z)$ values              | Above SRF or calibration error. Re-check SRF and calibration.   |
| Recalculated $f_{\text{SRF}}$ doesn't match | Model breakdown: either too close to resonance, or DUT has distributed parameter effects not captured by lumped RLC model.                      |
| Large uncertainty in $L$                    | Insufficient number of measurement points or limited frequency range. Increase number of points and expand frequency span (within valid range). |

## 7 Summary of Best Practices

- Always identify  $f_{\text{SRF}}$  first with a wide frequency sweep
- Calibrate at the DUT plane, not at VNA ports<sup>10</sup>
- Keep measurement frequencies below  $f_{\text{SRF}}/12$  (preferably  $f_{\text{SRF}}/15$ )
- Use at least 7–10 frequency points distributed across the valid range
- Verify inductive behavior:  $\text{Im}(Z) > 0$  and *increasing* with frequency
- Check fit quality through residuals and linearity plots
- Validate results by comparing recalculated  $f_{\text{SRF}}$  with measured value

## 8 References

- Skin effect in conductors: Terman, F.E., *Radio Engineers' Handbook*, McGraw-Hill (1943)
- VNA calibration techniques: Agilent Application Note 1287-3, *Exploring the Architectures of Network Analyzers*
- Self-resonance in inductors: Grandi et al., *Stray Capacitances of Single-Layer Solenoid Air-Core Inductors*, IEEE Trans. IM (1999)

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<sup>10</sup>what does "at the DUT plane" mean? Read present manual again