

Wind Turbine Electricity Generation

D. Induction Generator

DESIGN FEATURES

STATOR WITH MULTIPLE WINDINGS

ROTOR - CONDUCTING BARS

POWER EXTRACTED FROM STATOR

ALTERNATIVE DESIGNS

- ROTORS ARE WOUND ALSO

- POWER FROM BOTH ROTOR & STATOR

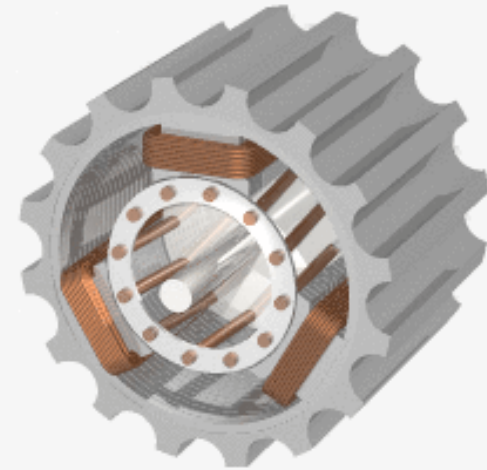
(DFIG)
↑
DOUBLY FED
INDUCTION GENERATOR

DESIGN CHALLENGES

- EXTERNAL CONSTANT FREQUENCY SOURCE TO CONTROL ROTATION SPEED
- EXTERNAL SOURCE OF REACTIVE POWER

- OFTEN OPERATE WITH POOR POWER FACTOR

→ CAN BE OVERCOME WITH CLOSER ELECTRICAL DESIGN



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INDUCTION ELECTRIC MACHINES
HAVE BEEN WIDELY USED
AS MOTORS

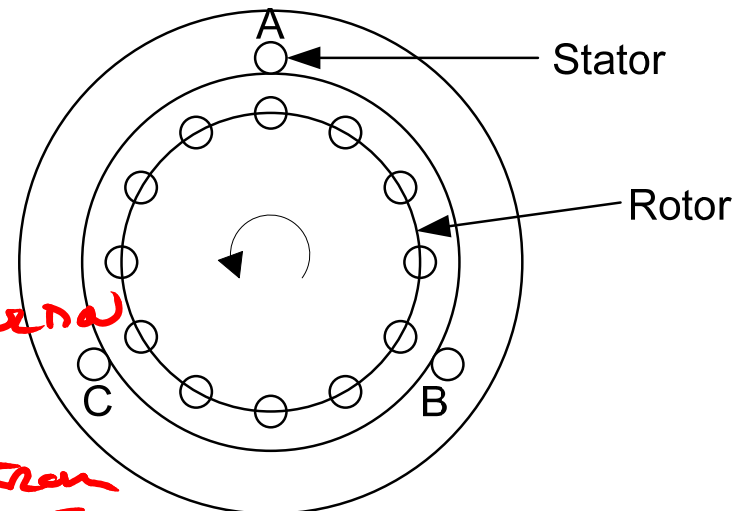
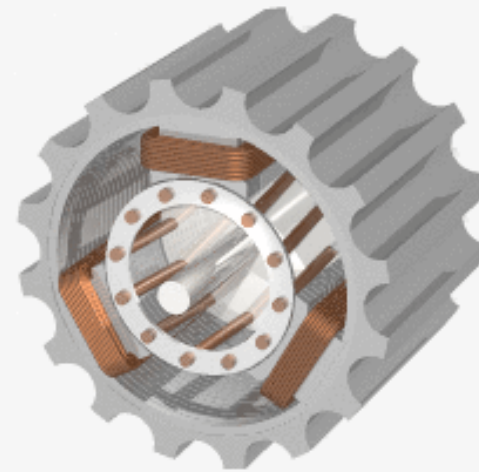
USE AS GENERATORS IS MORE
RECENT

CURRENTLY, INDUCTION GENERATOR
DESIGNS ARE MOST COMMON
GENERATOR IN WIND INDUSTRY

WHY WOULD INDUCTION MOTORS
DOMINATE IN WIND TURBINES?

SIMPLE DESIGN → ALLOWS
FOR RUGGED CONSTRUCTION
RELATIVELY INEXPENSIVE

CONNECTION & DISCONNECTION FROM
GRID IS RELATIVELY SIMPLE



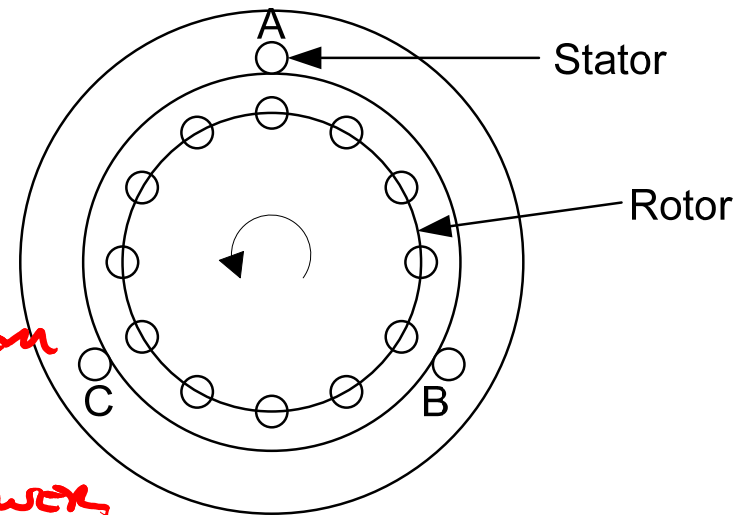
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DUE TO LIMITATIONS, APPLICATION IS PRIMARILY FOR LARGE, GRID CONNECTED SYSTEMS

AN OUTSIDE ELECTRICAL SYSTEM (GRID)

- SETS FREQUENCY
- PROVIDES REACTIVE POWER



CAN BE USED FOR DISTRIBUTED OR NON-GRID CONNECTED SYSTEMS IF ISSUES ARE ADDRESSED

- REACTIVE POWER SUPPLY
- AIDS FOR FREQUENCY STABILITY
- SPIN UP ASSISTANCE (IN SOME CASES)

START-UP OF GENERATOR

- RUN GENERATOR AS A MOTOR → USES ENERGY
- USE WIND TO START → ONLY CONNECT TO GRID WHEN IT IS GENERATING

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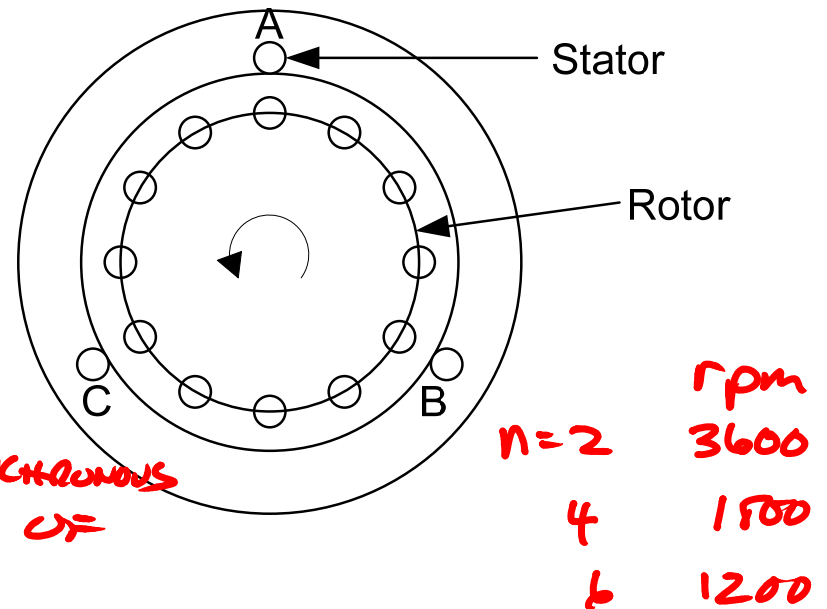
THEORY OF OPERATION

- STATOR PRODUCES A ROTATING MAGNETIC FIELD

→ SUPPLY AC CURRENT TO WINDINGS W/ PHASE OFFSET

→ FIELD ROTATES AT SYNCHRONOUS SPEED, DEPENDS ON # OF WINDINGS

- ROTOR SPINS AT A SPEED DIFFERENT THAN SYNCHRONOUS SPEED
 - RELATIVE MOTION BETWEEN ROTOR & STATOR FIELDS
 - SINCE ROTOR IS PASSING THROUGH A CHANGING MAGNETIC FIELD, THE BARS WILL HAVE INDUCED CURRENT
 - INDUCED CURRENT PRODUCES A MAGNETIC FIELD ASSOCIATED WITH ROTOR
 - INTERACTION BETWEEN ROTOR & STATOR FIELDS CAUSES ELEVATED VOLTAGE AT STATOR TERMINALS
 - CURRENT



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THEORY OF OPERATION

PARAMETER GOVERNING INDUCTION MACHINE OPERATION IS SLIP S

$$S = \frac{n_s - n_r}{n_s}$$

NORMALIZED
SPEED DIFFERENCE
QUOTED IN %

TYPICAL SLIP VALUES ARE $\sim 2\%$ (FOR GENERATION)

SELDOM DOES SLIP EXCEED 3% (DURING GENERATION)

GENERATOR WILL EXPERIENCE A WIDE RANGE OF S
DURING START UP

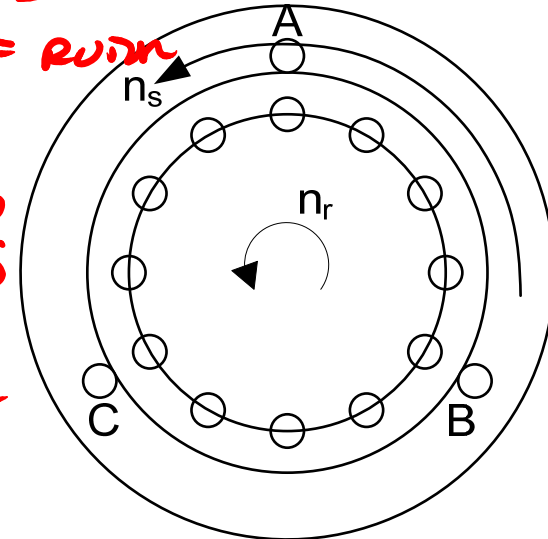
$n_r = 0$ INITIALLY

CONVENTION

$S > 0$ MOTOR - STATOR FIELD SPINS FASTER THAN ROTOR
 $S < 0$ GENERATION - ROTOR SPINS FASTER THAN THE STATOR

n_s - SPEED OF STATOR FIELD

n_r - SPEED OF ROTOR

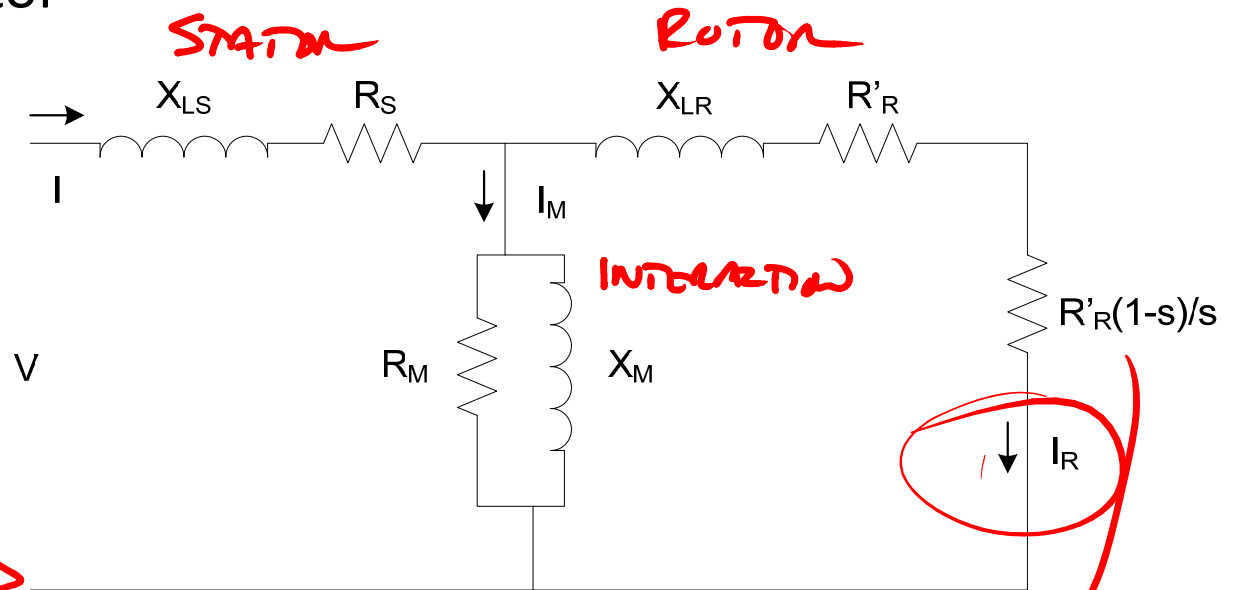


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INDUCTION GENERATOR
CAN BE REPRESENTED
BY AN EQUIVALENT
CIRCUIT

MOTOR/GENERATOR
CAN BE CHARACTERIZED
IN TERMS OF THESE
QUANTITIES

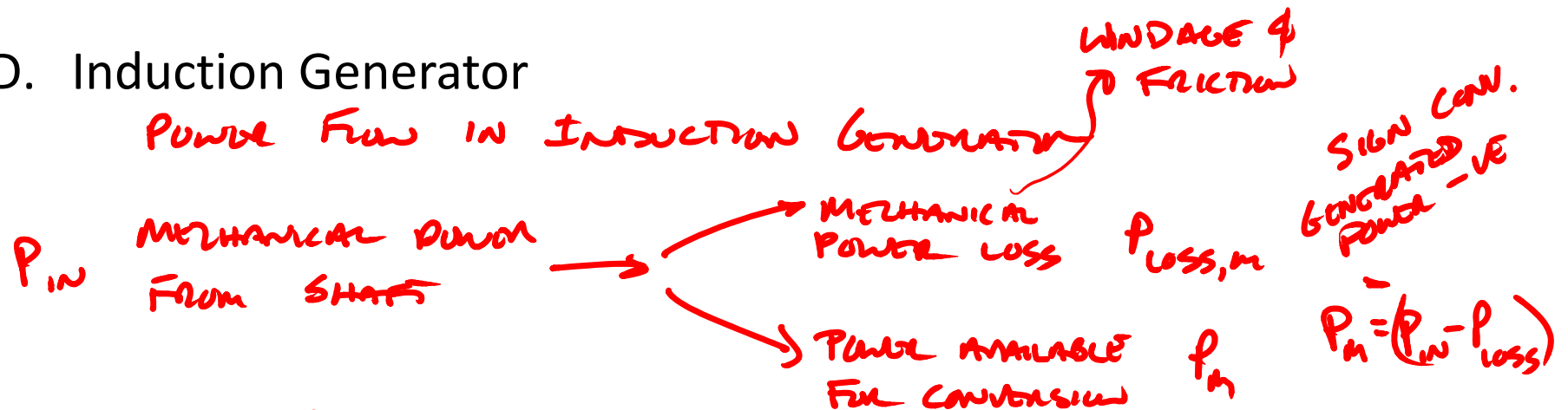


$X_m \gg X_{LS} \text{ or } X_{LR}$
 $R'_R \frac{(1-s)}{s}$ POSITIVE $s < 1$
 NEGATIVE $s > 1$
 VARIABLE RESISTOR
 CHECK!

R_m IS TYPICALLY LARGE
 → IGNORE

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THIS POWER P_m IS TRANSFORMED INTO ELECTRICAL POWER

$$P_m = I^2 R'_r \frac{1-s}{s}$$

← POWER GENERATED IN ROTOR

SOME POWER LOST IN ROTOR → NET POWER ONLY IS TRANSFERRED

$$P_g = P_m - P_{loss,r} = I^2 R'_r \frac{1-s}{s} + I_r^2 R'_r$$

SIMPLIFY $P_g = \frac{P_m}{1-s}$

SOME POWER LOST IN STATOR $I_s^2 R_s = P_{loss,s}$

SO NET POWER DELIVERED AT TERMINALS $P_{out} = P_g - P_{loss,s}$