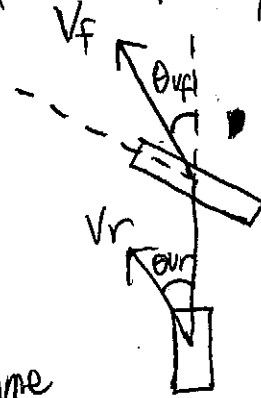
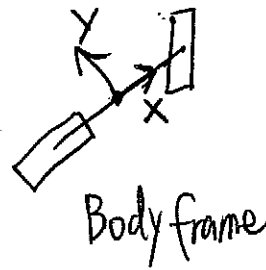
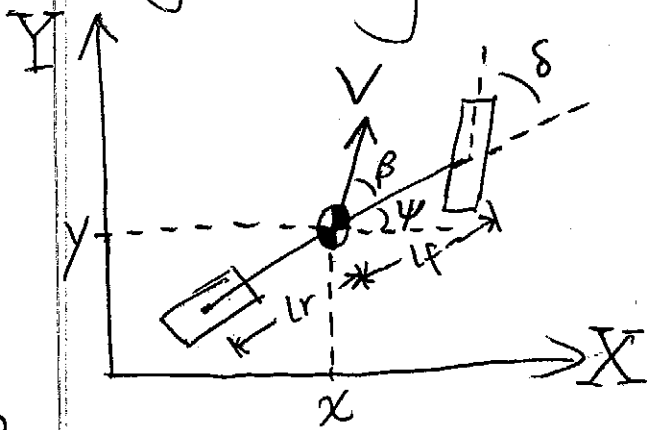


# XingYu Wang 2D Bicycle Model 7/28/2019



FBD:

$X, Y$  = Global coordinate frame

$x, y$  = body coordinate frame

$\delta$  = steering angle

$l_r, l_f$  = distance from rear/front wheel to center of mass

$\psi$  = body yaw angle

$\beta$  = velocity angle ~~with~~ w.r.t body

$\theta_{vf}, \theta_{vr}$  = ~~front/rear tire slip angle~~ front/rear ~~velocity angle~~

## Lateral Dynamics:

$$\sum F_x = 0 : m a_y = F_{yf} \cos \delta + F_{yr} \quad (1)$$

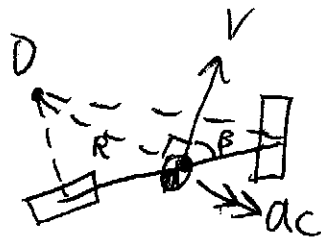
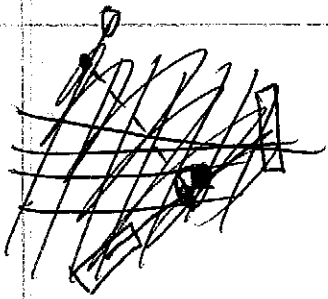
$m$  = mass of car

$a_y$  = acceleration in body  $y$  direction

$F_{yf}, F_{yr}$  = force on front/rear tire in  $y$ -direction



$$\beta = \tan^{-1} \left( -\frac{\dot{y}}{\dot{x}} \right) \quad (2)$$



O = center of rotation

$$a_c = \text{centripetal acceleration} = \frac{V^2}{R} = V \cdot \dot{\psi} \quad (3)$$

$$a_y = \ddot{y} + a_c \cos \beta = \ddot{y} + V \dot{\psi} \cos \beta = \ddot{y} + \dot{x} \dot{\psi} \quad (4)$$

$$\text{From (1) \& (4)} \Rightarrow \ddot{y} = -\dot{\psi} \dot{x} + \frac{1}{m} (F_{yf} \cos \delta + F_{yr}) \quad (5)$$

$$\ddot{\psi} I_z = l_f F_{yf} - l_r F_{yr} \quad (6), \quad I_z = \text{total moment of inertia}$$

$\alpha_f, \alpha_r = \text{front/rear tire slip angle}$

$$\alpha_f = \delta - \theta_{vf}, \quad \alpha_r = \delta - \theta_{vr}$$

~~Using small angle approximation:~~

$$\theta_{vf} = \frac{\dot{y}_f}{\dot{x}_f} = \frac{\dot{y} + l_f \dot{\psi}}{\dot{x}}, \quad \theta_{vr} = \frac{\dot{y} - l_r \dot{\psi}}{\dot{x}} \quad (7)$$

Linear approximation of tire force is:

$$F_{yf} = 2C_\alpha \left( \delta - \frac{\dot{y} + l_f \dot{\psi}}{\dot{x}} \right) \quad (8)$$

$$F_{yr} = 2C_\alpha \left( -\frac{\dot{y} - l_r \dot{\psi}}{\dot{x}} \right) \quad (9)$$

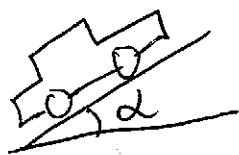
$C_\alpha$  is called cornering stiffness

# Longitudinal Dynamics

$$m\ddot{x} = F_x - F_{load} \quad (10)$$

$a_x$  = acceleration due to ~~long~~ longitudinal force

$F_x$  = tire force,  $F_{load}$  = total load force



$$F_{load} = F_{aero} + R_x + F_g$$

$$F_{aero} = \frac{1}{2} C_{aero} \rho A \dot{x}^2 = C_{aero} \dot{x}^2 \quad (\text{aerodynamic drag})$$

$$R_x \approx C_r \dot{x} \quad (\text{rolling friction})$$

$F_g$  = gravitational force from an incline at angle  $\alpha$

$$F_g = mg \sin \alpha$$

$$\Rightarrow F_{load} = C_{aero} \dot{x}^2 + C_r \dot{x} + mg \sin \alpha \quad (11)$$

Let ~~we~~  $w_e$  = engine rotational speed

$w_w$  = wheel rotational speed

$GR$  = gear ratio,  $S$  = slip ratio,

$x_\theta$  = throttle position  $\in [0, 1]$ ,  $F_{max}$  = max tire force

$T_e$  = engine torque,  $r_e$  = effective radius of tire

we have:  $w_w = (GR) w_e$

$$S = \frac{w_w \cdot r_e - \dot{x}}{\dot{x}}, \quad F_x = S \cdot F_{max} \quad (12)$$

Engine torque is computed from throttle input:

$$T_e = x_\theta (a_0 + a_1 w_e + a_2 w_e^2)$$

where  $a_0$ ,  $a_1$ , and  $a_2$  are coefficients

$$\dot{w}_e = \frac{1}{J_e} (T_e - GR \cdot r_e \cdot F_{load}) \quad (13)$$

where  $J_e$  is the combined power system inertia

From (10) ~~and~~ we have  $\ddot{x} = a_x + \dot{\psi} V \cdot \sin \theta$

$$\Rightarrow \ddot{x} = a_x + \dot{\psi} \dot{y} \quad (14)$$

From (14), (12), and (13), we have:

$$(15) \quad \ddot{x} = \dot{\psi} \dot{y} + \frac{1}{m} \left[ \frac{(GR) W_e \cdot r_e - \dot{x}}{\dot{x}} \cdot F_{max} - C_{aero} \dot{x}^2 - C_r \dot{x} - m g \sin \alpha \right]$$

$$(16) \quad W_e = \frac{1}{j_e} (X_0(a_0 + a_1 W_e + a_2 W_e^2) - (GR) \cdot r_e \cdot (C_{aero} \dot{x}^2 + C_r \dot{x} + m g \sin \alpha))$$

• Global coordinates

$$\dot{X} = \dot{x} \cos \psi - \dot{y} \sin \psi$$

$$\dot{Y} = \dot{x} \sin \psi + \dot{y} \cos \psi$$

## Complete system equation

$$\begin{cases} \ddot{y} = -\dot{\psi} \dot{x} + \frac{2C_a}{m} \left[ \cos \delta \left( \delta - \frac{\dot{y} + l_f \dot{\psi}}{\dot{x}} \right) - \frac{\dot{y} - l_r \dot{\psi}}{\dot{x}} \right] \\ \ddot{\psi} = \frac{2l_f C_a}{I_z} \left( \delta - \frac{\dot{y} + l_f \dot{\psi}}{\dot{x}} \right) - \frac{2l_r C_a}{I_z} \left( -\frac{\dot{y} - l_r \dot{\psi}}{\dot{x}} \right) \\ \ddot{X} = \dot{\psi} \dot{Y} + \frac{1}{m} \left[ \frac{(G_R) W_e \cdot r_e - \dot{X}}{\dot{X}} \cdot F_{max} - C_{aero} \dot{X}^2 - C_r \dot{X} - mg \sin \alpha \right] \\ \dot{W}_e = \frac{1}{J_e} \left[ X_\theta (a_0 + a_1 W_e + a_2 W_e^2) - (G_R) \cdot r_e \cdot (C_{aero} \dot{X}^2 + C_r \dot{X} + mg \sin \alpha) \right] \\ \dot{X} = \dot{X} \cos \psi - \dot{Y} \sin \psi \\ \dot{Y} = \dot{X} \sin \psi + \dot{Y} \cos \psi \end{cases}$$

State variables:

$X$  = ~~body~~ location in body X frame

$Y$  = location in body Y frame

$\dot{X}$  = ----- global X frame

$\dot{Y}$  = ----- global Y frame

$\psi$  = body ~~roll~~ yaw angle in global frame

$W_e$  = engine rotational speed

Controlled variables:

$\delta$  = steering angle

$X_\theta$  = throttle position

(assuming no ~~braking~~ braking)

All other variables are constants.