## Introduction

Bode Plot deals with the frequency response of a system separately in terms of magnitude and phase. Hence there are two plots

- (i) Plot of the magnitude v/s frequency and
- (ii) Plot of phase v/s frequency

A Bode plot is a (semilog) plot of the transfer function magnitude and phase angle as a function of frequency

The format is a log frequency scale on the horizontal axis and, on the vertical axis,

- (i) magnitude in decibels and
- (ii) phase in degrees

# **Bode plot-Applications**

- For designing lead compensators
- For finding stability, gain and phase margins
- For system identification from the frequency response

## Magnitude & Phase of Open loop TF

The magnitude of the open loop transfer
 G(s)H(S)function in dB is

$$M=20\log|G(j\omega)H(j\omega)|$$

 The phase angle of the open loop transfer function in degrees is

$$\Phi = \angle G(j\omega)H(j\omega)$$

## **Basic factors**

Consider the following general transfer function

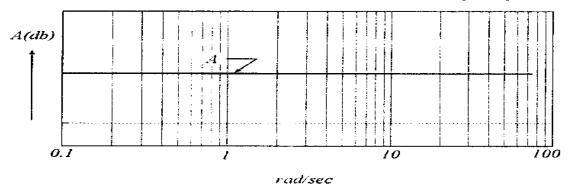
G(s) = 
$$\frac{k(1+T_a s)(1+T_b s).....}{s^r(1+T_1 s)(1+T_2 s).....(s^2+2\zeta \omega_n s+\omega_n^2)}$$

$$G(j\omega) = \frac{k(1+j\omega T_a)(1+j\omega T_b).....}{(j\omega)^r (1+j\omega T_1)(1+j\omega T_2)..\omega_n^2 \left[1+j\left(\frac{\omega}{\omega_n}\right)+\left(\frac{j}{\omega_n}\right)^2\right].}$$

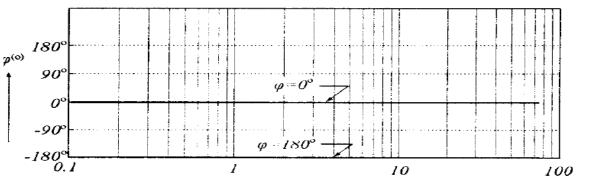
- 1. Gain k (Constant Term)
- Integral or Derivative factors (jω)<sup>±1</sup>
   (Poles or zeros at origin)
- 3. First-order factors  $(1+j\omega T)^{\pm 1}$  (poles or zeros not at origin)
- 4. Quadratic factors  $[1+2\zeta(j\omega/\omega_n)+(j\omega/\omega_n)^2]^{\pm 1}$  (Complex poles or Complex zeros)

### **Gain Factor K**

Magnitude(A)=20log | K |



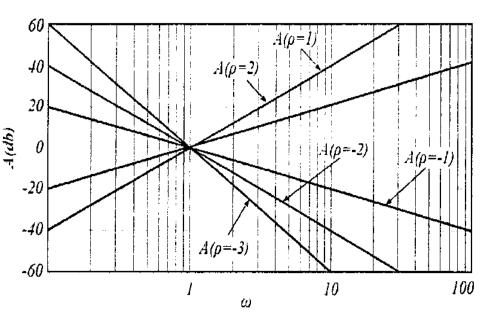
• Phase angle( $\phi$ )=K>0: 0° and K<0:  $\pm 180$ °

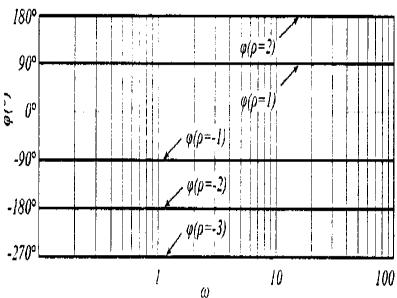


## Pole /Zero at origin $(j\omega)^{\pm\rho}$

$$A = 20 \log |(j\omega)^{\pm \rho}| = \pm 20\rho \log \omega$$

$$\varphi = /(j\omega)^{\pm \rho} = \pm 90^{\circ} \rho$$





## Poles / Zeros of the Form $(j\omega T + 1)^{\pm \rho}$

$$A = \pm 20\rho \log |(j\omega T + 1)| = \pm 20\rho \log \sqrt{\omega^2 T^2 + 1}$$
  
$$\varphi = \pm \rho \tan^{-1}(\omega T)$$

a. When  $\omega \ll 1/T$ ,

$$A = \pm 20\rho \log \sqrt{\omega^2 T^2 + 1} \simeq 20\rho \log 1 = 0$$
&  $\Phi \approx 0^\circ$ 

b. When  $\omega = 1/T$ ,

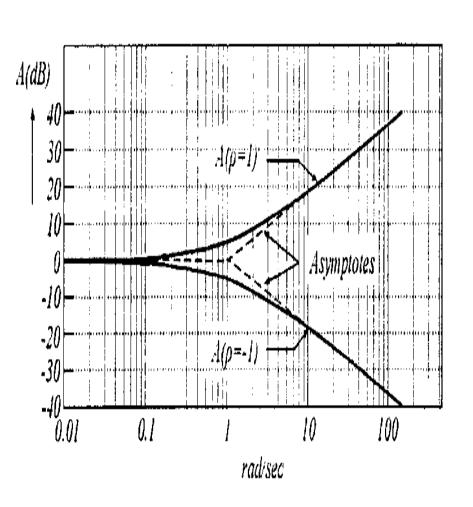
$$A = \pm 20\rho \log \sqrt{2} \simeq \pm 3\rho$$
 &  $\Phi \approx \pm 45^{\circ}\rho$ 

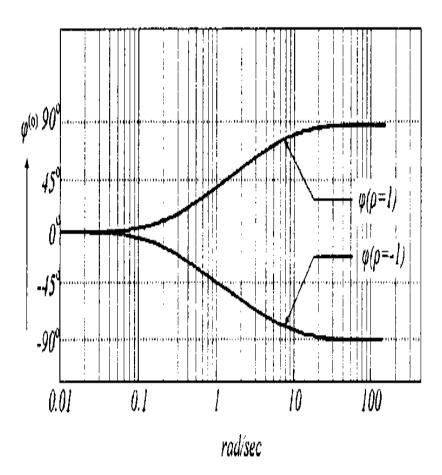
The frequency  $\omega = 1/T$  is called the *corner frequency*. Cy. c. When  $\omega \gg 1/T$ ,

$$A \simeq \pm 20 \rho \log \omega T$$
 &  $\Phi \approx \pm 90^{\circ} \rho$ 

### Poles / Zeros of the Form

$$(j\omega T + 1)^{\pm\rho}$$





### **Quadratic factor**

$$\left[\omega_n^{-2}(j\omega)^2 + 2\zeta\omega_n^{-1}(j\omega) + 1\right]^{\pm\rho}$$

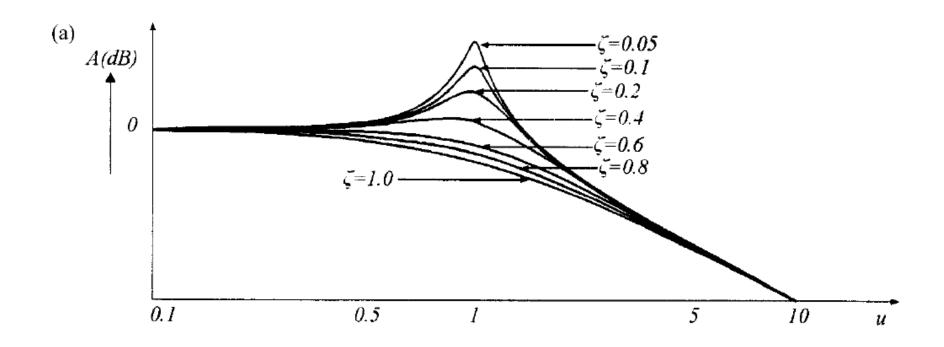
$$A = \pm 20\rho \log \sqrt{(1 - u^2)^2 + 4\zeta^2 u^2}$$

$$\varphi = \pm \rho \tan^{-1} \left[ \frac{2\zeta u}{1 - u^2} \right]$$
 where  $u = \omega/\omega_n$ .

- a. When  $u \ll 1$ , then  $A \simeq \pm 20 \rho \log 1 = 0$
- b. When  $u \gg 1$ , then  $A \simeq \pm 40\rho \log u$
- c. When  $\zeta = 1$ , then  $A = \pm 20\rho \log |1 + u^2|$
- d. When  $\zeta = 0$ , then  $A = \pm 20\rho \log |1 u^2|$ .

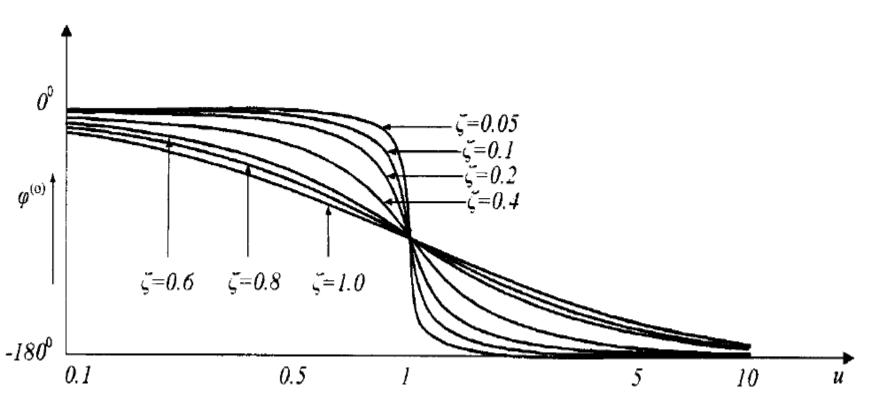
first asymptote coincides with the 0 dB-axis and the second has a slope of  $\pm 40\rho$  dB and crosses over the *u*-axis at the point u=1. In the vicinity of the point of intersection of the two asymptotes, the form of the curve of A is decisively influenced by the damping ratio  $\zeta$ .

# Magnitude plot



# Phase plot

- a. When u = 0, then  $\varphi = 0^{\circ}$
- b. When u = 1, then  $\varphi = \pm 90^{\circ} \rho$
- c. When  $u = \infty$ , then  $\varphi = \pm 180^{\circ} \rho$ .



#### Bode Plot based on Asymptotic Approximation

<u>Term</u>	<u>Magnitude</u>	<u>Phase</u>		
Constant: K	$20\log_{10}( \mathbf{K} )$	K>0: 0°		
		K<0: ±180°		
Pole at Origin	-20 dB/decade passing through	-90°		
_	$0 \text{ dB at } \omega = 1$			
(Integrator) 1/s				
Zero at Origin	+20 dB/decade passing	+90°		
	through 0 dB at $\omega$ =1	(Mirror image, around x axis, of		
(Differentiator) s	(Mirror image, around x	Integrator about )		
	axis, of Integrator)			
Real Pole	1. Draw low frequency	1. Draw low frequency		
1	asymptote at 0 dB	asymptote at $0^{\circ}$		
$\frac{s}{s}+1$	2. Draw high frequency	2. Draw high frequency		
$\frac{\overline{\omega_0}}{\omega_0}$	asymptote at -20	asymptote at -90°		
	dB/decade	3. Connect with a straight line		
	3. Connect lines at $\omega_0$ .	from $0.1 \cdot \omega_0$ to $10 \cdot \omega_0$		
Real Zero	1. Draw low frequency	Draw low frequency		
$\frac{s}{-}+1$	asymptote at 0 dB	asymptote at 0°		
$\frac{\overline{\omega_0}}{\omega_0}$	2. Draw high frequency	2. Draw high frequency		
	asymptote at +20	asymptote at +90°		
	dB/decade	3. Connect with a straight line		
	3. Connect lines at $\omega_0$ .	from $0.1 \cdot \omega_0$ to $10 \cdot \omega_0$		
	(Mirror image, around x-axis,	(Mirror image, around x-axis, of		
	of Real Pole)	Real Pole about 0°)		

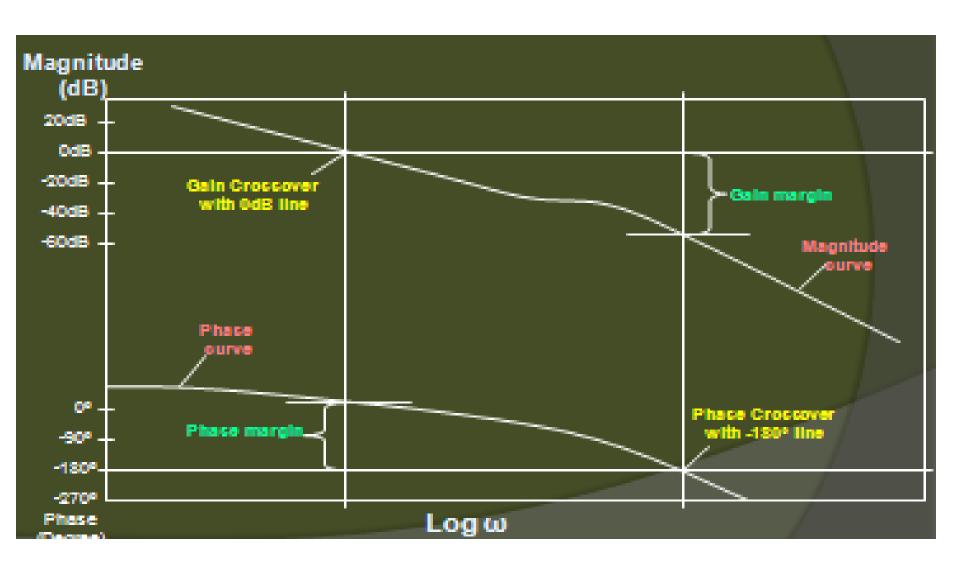
## Contd..

Underdamped Poles  (Complex conjugate poles) $\frac{1}{\left(\frac{s}{\omega_0}\right)^2 + 2\zeta \frac{s}{\omega_0} + 1}$	<ol> <li>Draw low frequency asymptote at 0 dB</li> <li>Draw high frequency asymptote at -40 dB/decade</li> <li>If ζ&lt;0.5, then draw peak at ω<sub>0</sub> with amplitude  H(jω<sub>0</sub>) =-20·log<sub>10</sub>(2ζ), else don't draw peak</li> <li>Connect lines</li> </ol>	2.	Draw low frequency asymptote at $0^{\circ}$ Draw high frequency asymptote at -180° Connect with straight line from $\omega = \omega_0/10\zeta$ to $\omega_0$ · $10\zeta$
$0 < \zeta < 1$			
Underdamped zeros  (Complex conjugate zeros) $\left(\frac{s}{\omega_0}\right)^2 + 2\zeta \frac{s}{\omega_0} + 1$	<ol> <li>Draw low frequency asymptote at 0 dB</li> <li>Draw high frequency asymptote at +40 dB/decade</li> <li>If ζ&lt;0.5, then draw peak at ω<sub>0</sub> with amplitude H(jω<sub>0</sub>) =+20·log<sub>10</sub>(2 ζ), else don't draw peak</li> </ol>	<ol> <li>2.</li> <li>3.</li> </ol>	Draw low frequency asymptote at $0^{\circ}$ Draw high frequency asymptote at $+180^{\circ}$ Connect with straight line from $\omega = \omega_0/10\zeta$ to $\omega_0$ $10\zeta$
$0 < \zeta < 1$	4. Connect lines		J

# Gain Margin and Phase Margin

- GM: is the factor by which magnitude of  $G(j\omega)H(j\omega)$  at the phase crossover frequency is to be multiplied to make it unity
- The gain margin from Bode plot is the number of dB that is below 0 dB at the phase crossover frequency (ø=-180°).
- PM: is the amount of phase to be added to the phase angle at gain cross over frequency to make it -180°
- The phase margin from Bode plot is the number of degrees the phase that is above -180° at the gain crossover frequency

## **GM** and PM



- For closed loop system to be stable,
   Magnitude should be less than 0dB at phase
   cross over frequency and the phase angle
   must be greater than -180° at gain cross over
   frequency
- GM (in dB)=0-gain in dB at  $\omega_{pc}$
- PM=phase angle at  $\omega_{gc}$ +180°

## **Bode Plot: Example 1**

Draw the Bode Diagram for the transfer function:

$$H(s) = \frac{100}{s + 30}$$

#### Step 1: Rewrite the transfer function in proper form.

Make both the lowest order term in the numerator and denominator unity. The numerator is an order 0 polynomial, the denominator is order 1.

$$H(s) = \frac{100}{30} \frac{1}{\frac{s}{30} + 1} = 3.3 \frac{1}{\frac{s}{30} + 1}$$

 Step 2: Separate the transfer function into its constituent parts.

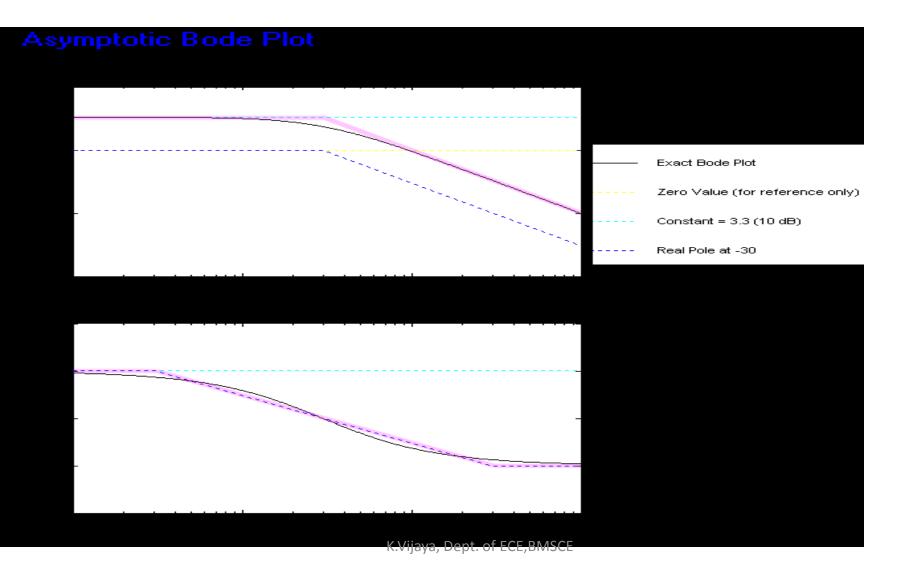
The transfer function has 2 components:

- A constant of 3.3
- A pole at s=-30
- Step 3: Draw the Bode diagram for each part.

This is done in the diagram below.

- The constant is the cyan line (A quantity of 3.3 is equal to 10.4 dB). The phase is constant at 0 degrees.
- The pole at 30 rad/sec is the blue line. It is 0 dB up to the break frequency, then drops off with a slope of -20 dB/dec. The phase is 0 degrees up to 1/10 the break frequency (3 rad/sec) then drops linearly down to -90 degrees at 10 times the break frequency (300 rad/sec)

# Bode plot1



# Example2:GM and PM

#### Bode Plot - Example

For the following T.F draw the Bode plot and obtain Gain cross over frequency Phase cross over frequency, Gain Margin and Phase Margin.

$$G(s) = 20 / [s (1+3s) (1+4s)]$$

Term	Corner Frequency	Slope db/dB	Change in slope
20/jw		-20	
1/(1+j4w)	wc <sub>1</sub> =1/4=0.25	-20	-20-20=-40
1/(1+j3w)	wc <sub>2</sub> =1/3=0.33	-20	-40-20=-60

The sinusoidal T.F of G(s) is obtained by replacing s by jw in the given T.F

$$G(jw) = 20 / [jw (1+j3w) (1+j4w)]$$

Corner frequencies:  $wc_1 = 1/4 = 0.25 \text{ rad/sec}$ ;

$$wc_2 = 1/3 = 0.33 \text{ rad/sec}$$

Calculation of Gain (A) (MAGNITUDE PLOT)

$$A @ w_1; A=20 \log [20 / 0.025] = 58.06 dB$$

 $A @ wc_1; A = [Slope from w_1 to wc_1 x log (wc_1/w_1] + Gain (A) @ w_1$ 

$$= -20 \log [0.25 / 0.025] + 58.06$$

$$= 38.06 \, dB$$

 $A @ wc_2; A = [Slope from wc_1 to wc_2 x log (wc_2 / wc_1] + Gain (A) @ wc_1]$ 

$$= -40 \log [0.33 / 0.25] + 38$$

$$= 33 dB$$

#### Choose Whas 10Wc2

 $A @ w_h$ ;  $A = [Slope from wc_2 to w_h x log (w_h / wc_2] + Gain (A) @ wc_2$ 

$$=$$
 - 60 log [ 3.3 / 0.33 ] + 33

$$= -27 dB$$

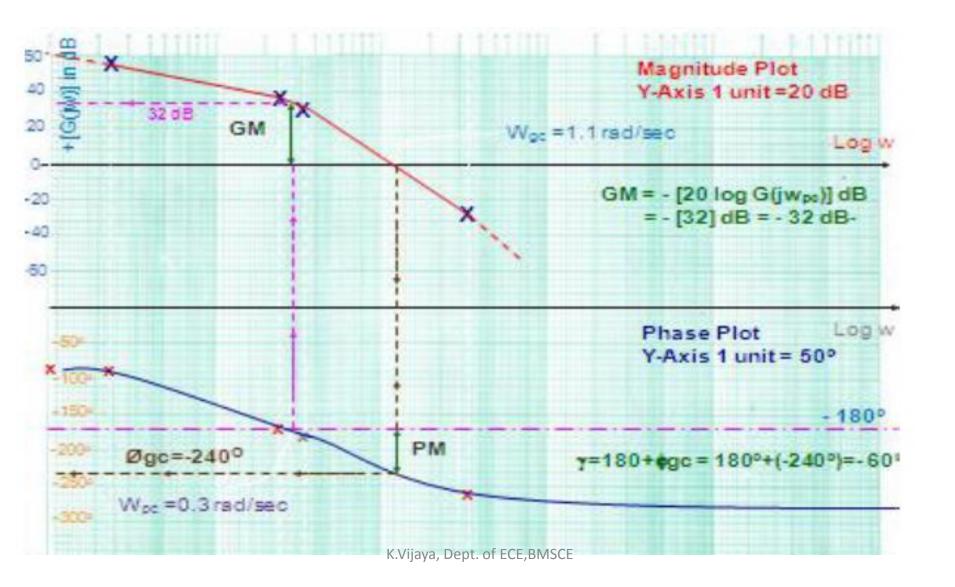
# Phase plot

$$\emptyset = -90^{\circ} - \tan^{-1} 3w - \tan^{-1} 4w$$

#### When

Frequency in rad / sec	Phase Angle in degrees
w=0	Ø= -90°
w=0.025	Ø= - 99°
w=0.25	Ø= -172°
w=0.33	Ø= -188°
w=3.3	Ø= - 259°
w=∞	Ø= - 270°

# Bode plot



## GM and PM

Calculations of Gain cross over frequency

The frequency at which the dB magnitude is Zero  $w_{gc} = 1.1 \text{ rad} / \text{sec}$ 

Calculations of Phase cross over frequency

The frequency at which the Phase of the system is  $-180^{\circ}$  wpc = 0.3 rad / sec

Gain Margin

The gain margin in dB is given by the negative of dB magnitude of G(jw) at

GM = - { 
$$20 \log [G(jw_{pc})] = - {32} dB$$

• Phase Margin

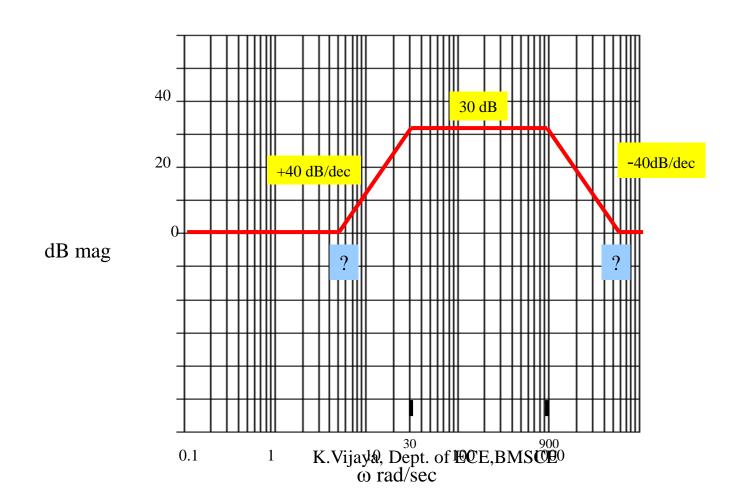
$$I' = 180^{\circ} + \varnothing_{gc} = 180^{\circ} + (-240^{\circ}) = -60^{\circ}$$

Conclusion

For this system GM and PM are negative in Values. Therefore the system is unstable in nature.

# Example3: TF from Bode plot

#### Obtain the TF from the given Bode Plot



Procedure:

The two break frequencies need to be found. Recall:

$$\#dec = log_{10}[w_2/w_1]$$

Then we have:

$$(\#dec)(40dB/dec) = 30 dB$$

$$log_{10}[w_1/30] = 0.75$$
  $\underline{w_1} = 5.33 \text{ rad/sec}$ 

Also

$$log_{10}[w_2/900] (-40dB/dec) = -30dB$$

This gives  $\underline{w}_2 = 5060 \text{ rad/sec}$ 

$$G(s) = \frac{(1+s/5.3)^2 (1+s/5060)^2}{(1+s/30)^2 (1+s/900)^2}$$

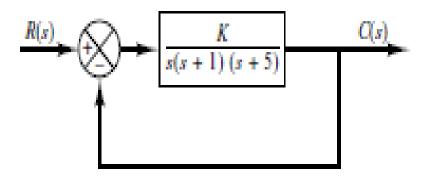
Clearing:

$$G(s) = \frac{(s+5.3)^2(s+5060)^2}{(s+30)^2(s+900)^2}$$

## <u>Tutorials</u>

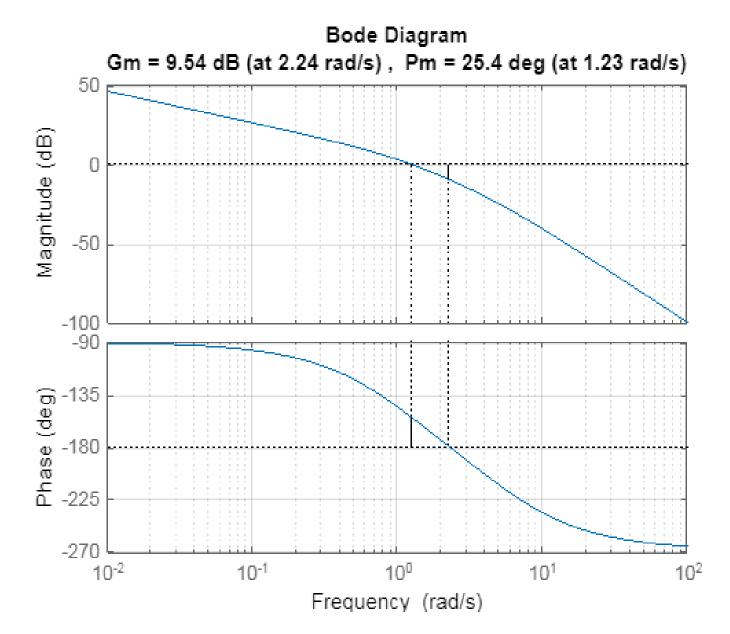
Problem 1

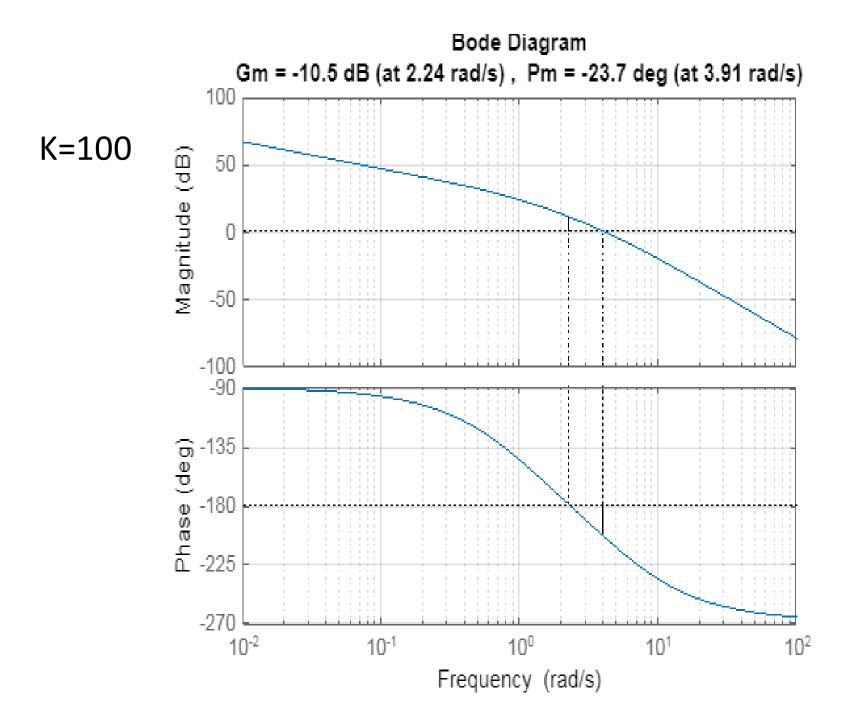
Obtain the phase and gain margins of the system shown in Figure for the two cases where K=10 and K=100



ANS:

K=10





### Problem 2

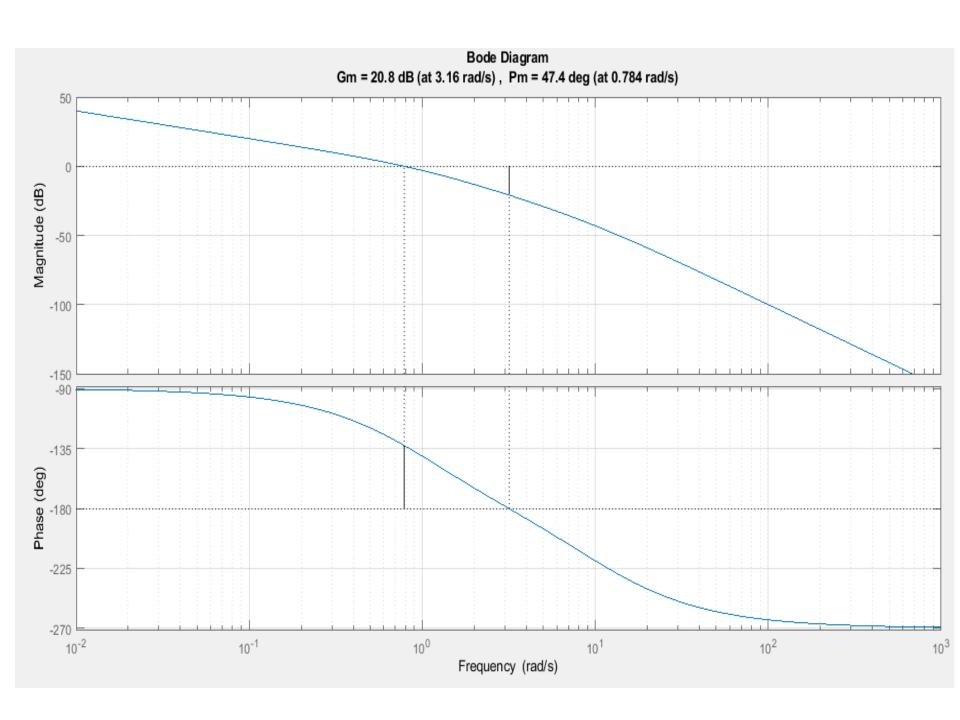
The system has an open loop transfer function  $G(s) = \frac{k}{s(1+s)(1+0.1s)}$ . Find the gain k such that

(i) GM = 10dB(ii) GM = 30dB

Assume K=1,

Draw the Bode plot

$$\begin{aligned} \mathsf{M}_{\mathsf{db}} &= 20 log \ 1 - 20 log \ \omega - 20 log \ \sqrt{1 + \omega^2} \, - 20 log \ \sqrt{1 + (0.1\omega)^2} \\ \emptyset &= 0 - 90 \, - \, tan^{-1} \ \omega \, - \, tan^{-1} \ (0.1\omega) \end{aligned}$$



(i) For k = 1, the GM = 20 dB

In order to get GM = 10dB the magnitude diagram at  $\omega = \omega_p$  must be pushed by 10dB. This means that k must be increased by 10dB

Hence  $20\log k = 10$ 

$$k = 3.162$$

(ii) To get GM = 30dB the magnitude diagram at  $\omega = \omega_p$  must be pushed down by 10dB.

This means that k must be decreased by 10dB

Hence  $20\log k = -10$ 

$$k = 0.3162$$

(iii) On the phase diagram locate margin of 24 deg.

In order to get the PM of 24°, the magnitude diagram must intercept the zero dB axis at  $\omega = 1.55$  rad/sec.

For this to happen, the magnitude must be pushed up by 8.2 dB. This means that gain must be increased by 8.2dB

$$20\log k = 8.2$$
  
 $k = 2.57$ 

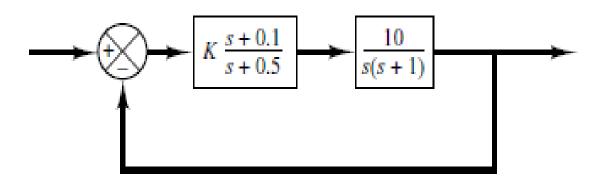
(iv) For the closed loop system to be stable the PM should be positive. For PM to be positive the gain cross over frequency should occur before  $\omega_p = 3.16$  rad/sec

As a limiting case, for PM to be zero the gain cross over should be at  $_{\rm p}$  = 3.16 rad/sec. For this to happen, the magnitude plot should be pushed up by 20 dB

$$20 \log k = 20$$
  
 $k = 10$ 

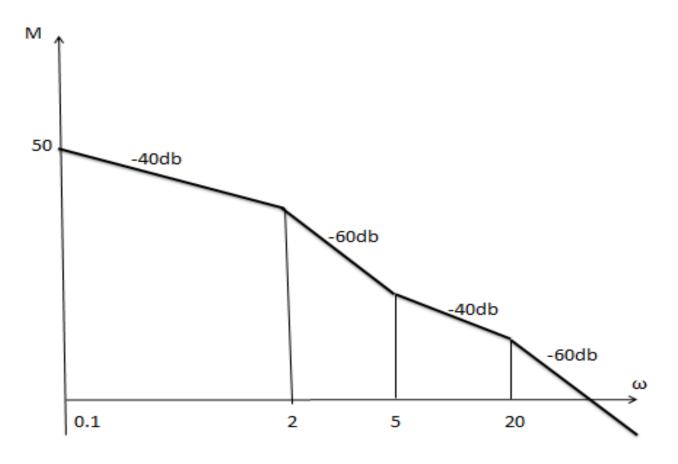
# Assignment

Consider the system shown in Figure. Draw a Bode diagram of the open-loop transfer function, and determine the value of the gain K such that the phase margin is 50°. What is the gain margin of this system with this gain K?



## Problem 3

Find the transfer function for the given Bode plot



$$G(s) = \frac{k(1 + \frac{s}{5})}{s^2 \left(1 + \frac{s}{2}\right)(1 + \frac{s}{20})}$$

At  $\omega = 0.1$ , M = 50db

$$20 \log(\frac{k}{\omega^2}) = 50$$

$$20\log k + 20\log(\frac{1}{\omega^2}) = 50$$

$$20\log k - 40\log \omega = 50$$

$$20\log k - 40\log (0.1) = 50$$

$$20\log k + 40 = 50$$

$$20\log k = 10$$
,  $K = 10^{10/20} = 3.16$ 

$$G(s) = \frac{3.16(\frac{5+s}{5})}{s^2(\frac{2+s}{2})(\frac{20+s}{20})} = \frac{25.28(s+5)}{s^2(2+s)(20+s)}$$