

# Lecture Notes

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October 26, 2025

Subject     Topics in Macroeconomics

Lecture 6   Local Linear Methods for Solving Macroeconomic Models

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# 1 A Basic RBC Model

We are going to start by the social planner problem, which is given by:

$$\max \mathbb{E}_t \left\{ \sum_{t=j}^{\infty} \beta^{t-j} \ln(c_j) \right\} \quad (1)$$

subject to:

$$c_j + k_j = z_j k_{j-1}^\alpha \quad k_j \geq 0, \quad c_j \geq 0 \quad (2)$$

$$\ln(z_{j+1}) = \rho \ln(z_j) + \eta_j, \quad \eta_j \sim N(0, \sigma_\eta^2) \quad (3)$$

In this model we have that the technology process  $\{z_t\}$  is defined as an  $AR(1)$  process.

Observe that the Lagrange of this problem is given by:

$$\mathbb{L} = \mathbb{E}_t \{ \beta^{t-j} (\ln(c_j) + \lambda_j [z_j k_{j-1}^\alpha - k_j - c_j]) \} \quad (4)$$

We have that the first order conditions of the problem are given by:

$$\frac{\partial \mathbb{L}}{\partial c_t} = \frac{1}{c_t} - \lambda_t = 0 \implies \frac{1}{c_t} = \lambda_t \quad (5)$$

$$\frac{\partial \mathbb{L}}{\partial k_t} = -\lambda_t + \beta \mathbb{E}_t [\alpha \lambda_{t+1} z_{t+1} k_t^{\alpha-1}] = 0 \quad (6)$$

The transversality condition is given by the following equation:

$$\lim_{T \rightarrow \infty} \frac{\beta^{T-j}}{c_t} k_T = 0 \quad (7)$$

Now the next step is to parametrize the model and solve the model numerically. In order to do so this method assigns parameter values based on either long-run steady state relationships of moments or moments from other studies such as microeconomic evidence:

## Step 1 - Steady State.

Now we solve the model for the non stochastic steady state in which  $z_{t+1} = z_t = 1$ . In other words  $z_t = 1 \quad \forall t$ . By the Euler equation (6) and the resource constraint represented by equation (2) we have the following equations, where the variables with overline are the variables in the steady state:

$$1 = \beta \alpha \bar{k}^{\alpha-1} \implies \bar{k} = (\beta \alpha)^{\frac{1}{1-\alpha}} \quad (8)$$

$$\bar{c} = (\beta\alpha)^{\frac{\alpha}{1-\alpha}} - (\beta\alpha)^{\frac{1}{1-\alpha}} \implies \bar{c} = (\beta\alpha)^{\frac{\alpha}{1-\alpha}}(1 - \beta\alpha) \quad (9)$$

**Step 2 - Log-linearisation.** Now we are going to define the following variables. First note that for any variable  $x$  we have that the following condition holds:

$$\hat{x} := \frac{(x - \bar{x})}{\bar{x}} \equiv \frac{\partial x}{\bar{x}} \approx \ln\left(\frac{x}{\bar{x}}\right) \quad (10)$$

The expression above is the percentage deviation of  $x$  from the point  $\bar{x}$ . By using this kind of evaluation with the variables that we have we obtain the following conditions:

$$\hat{c}_t := \ln(c_t) - \ln(\bar{c}) = \ln\left(\frac{c_t}{\bar{c}}\right) \implies c_t = \bar{c}e^{\hat{c}_t} \quad (11)$$

$$\hat{k}_t := \ln(k_t) - \ln(\bar{k}) = \ln\left(\frac{k_t}{\bar{k}}\right) \implies k_t = \bar{k}e^{\hat{k}_t} \quad (12)$$

$$\hat{\lambda}_t := \ln(\lambda_t) - \ln(\bar{\lambda}) = \ln\left(\frac{\lambda_t}{\bar{\lambda}}\right) \implies \lambda_t = \bar{\lambda}e^{\hat{\lambda}_t} \quad (13)$$

$$\hat{z}_t := \ln(z_t) - \ln(\bar{z}) = \ln\left(\frac{z_t}{\bar{z}}\right) \implies z_t = \bar{z}e^{\hat{z}_t} \quad (14)$$

By this fact and the equations that we already derived we obtain the following conditions that characterize the equilibrium conditions in this system:

**Equilibrium conditions:**

$$\lambda_t = \frac{1}{c_t} \quad (15)$$

$$\lambda_t = \beta \mathbb{E}_t[\alpha \lambda_{t+1} z_{t+1} k_t^{\alpha-1}] \quad (16)$$

$$c_t + k_t = z_t k_{t-1}^\alpha \quad (17)$$

$$\ln z_{t+1} = \rho \ln z_t + \eta_t \quad (18)$$

$$\lim_{T \rightarrow \infty} \frac{\beta^{T-j}}{c_t} k_T = 0 \quad (19)$$

Now one can observe that we have the following equation by using the kind of derivation we obtained by equation (10).

$$\bar{\lambda}e^{\hat{\lambda}_t} = \frac{1}{\bar{c}e^{\hat{c}_t}} \quad (20)$$

Now observe that a first order Taylor Expansion is given by:

$$f(x)|_{x^*} \approx f(x^*) + f'(x^*)(x - x^*) \quad (21)$$

By doing a first order Taylor approximation around the value of  $\lambda$  in the steady state we obtain the following equation:

$$\bar{\lambda} + \bar{\lambda}(\hat{\lambda}_t - \bar{\lambda}) = \frac{1}{\bar{c}} - \frac{1}{\bar{c}}(\hat{c}_t - \bar{c}) \quad (22)$$

Observe that the values of  $\bar{\lambda}$  and  $\bar{\lambda}$  are zero and that  $\bar{\lambda} = \frac{1}{\bar{c}}$ , then we get that:

$$(\hat{\lambda}_t - \bar{\lambda}) = (\hat{c}_t - \bar{c}) \quad (23)$$

The equation above lead us to the following equation:

$$\hat{\lambda}_t = -\hat{c}_t \quad (24)$$

By using equation (16) and by replacing conditions (11) to (14) in the equation (16) lead us to the following result:

$$\lambda_t = \beta \mathbb{E}_t[\alpha \lambda_{t+1} z_{t+1} k_t^{\alpha-1}] \implies \quad (25)$$

$$\lambda_t = \beta \mathbb{E}_t[\alpha (\bar{\lambda} e^{\hat{\lambda}_{t+1}}) e^{z_{t+1}} (\bar{k} e^{\hat{k}_t})^{\alpha-1}] \quad (26)$$

Now do a first order Taylor expansion around the stationary state. By using this first order Taylor expansion make us to achieve the equation below:

$$(\bar{\lambda} + \bar{\lambda} \hat{\lambda}_t) = \beta \alpha \bar{k}^{\alpha-1} \bar{\lambda} + \mathbb{E}_t \beta \alpha \bar{k}^{\alpha-1} \bar{\lambda} (\hat{z}_{t+1}) - \mathbb{E}_t \beta \alpha (1 - \alpha) \bar{k}^{\alpha-1} \bar{\lambda} \hat{k}_t + \mathbb{E}_t \beta \alpha \bar{k}^{\alpha-1} \bar{\lambda} \hat{\lambda}_{t+1} \quad (27)$$

Observe that:

$$\bar{\lambda} \hat{\lambda}_t = \beta \alpha \bar{k}^{\alpha-1} \bar{\lambda} \mathbb{E}_t \hat{z}_{t+1} - (1 - \alpha) \beta \alpha \bar{k}^{\alpha-1} \bar{\lambda} \hat{k}_t + \beta \alpha \bar{k}^{\alpha-1} \bar{\lambda} \mathbb{E}_t \hat{\lambda}_{t+1} \quad (28)$$

The equation above yield us to the following result:

$$\hat{\lambda}_t = \mathbb{E}_t \hat{z}_{t+1} - (1 - \alpha) \hat{k}_t + \mathbb{E}_t \hat{\lambda}_{t+1} \quad (29)$$

By taking expectation of the expression in (18) and inserting it into the above equation yield the following result:

$$\hat{\lambda}_t = \rho \hat{z}_t - (1 - \alpha) \hat{k}_t + \mathbb{E}_t \hat{\lambda}_{t+1} \quad (30)$$

Now we are going to do the same for the equation of consumption:

$$c_t + k_t = z_t k_{t-1}^\alpha \quad (31)$$

$$(\bar{c} e^{\hat{c}_t}) + (\bar{k} e^{\hat{k}_t}) = e^{\hat{z}_t} (\bar{k} e^{\hat{k}_{t-1}})^\alpha \quad (32)$$

$$y_t = z_t k_{t-1}^\alpha \quad \text{which implies that} \quad (33)$$

$$(\bar{c} e^{\hat{c}_t}) + (\bar{k} e^{\hat{k}_t}) = (\bar{y} e^{\hat{y}_t}) \quad (34)$$

Observe that we can write equation (34) as the following one:

$$\bar{c} + \bar{c}\hat{c}_t + \bar{k} + \bar{k}\hat{k}_t = \bar{y} + \bar{y}\hat{y}_t \quad (35)$$

The equation above implies that:

$$\bar{c}\hat{c}_t + \bar{k}\hat{k}_t = \bar{y}\hat{y}_t \implies \quad (36)$$

$$\hat{k}_t = \frac{\bar{y}}{\bar{k}}\hat{y}_t - \frac{\bar{c}}{\bar{k}}\hat{c}_t \quad (37)$$

Observe that we have that  $y_t = z_t k_{t-1}^\alpha$  and by using the conditions that characterize the equations in the steady state we obtain that:

$$(\bar{y}e^{\hat{y}_t}) = e^{\hat{z}_t}(\bar{k}e^{\hat{k}_{t-1}})^\alpha \implies \quad (38)$$

$$\bar{y} + \bar{y}\hat{y}_t = \bar{k}^\alpha + \bar{k}^\alpha \hat{z}_t + \alpha \bar{k}^\alpha \hat{k}_{t-1} \quad (39)$$

The equation that we have just written can be summarized in the equations below that characterize the equilibrium of the system:

**Equilibrium conditions of the system:**

$$\hat{\lambda}_t = -\hat{c}_t \quad (40)$$

$$\hat{\lambda}_t = \rho \hat{z}_t - (1 - \alpha)\hat{k}_t + \mathbb{E}_t \hat{\lambda}_{t+1} \quad (41)$$

$$\hat{k}_t = \frac{\bar{y}}{\bar{k}}\hat{y}_t - \frac{\bar{c}}{\bar{k}}\hat{c}_t \quad (42)$$

$$\hat{y}_t = \hat{z}_t + \alpha \hat{k}_{t-1} \quad (43)$$

$$\hat{z}_{t+1} = \rho \hat{z}_t + \eta_t \quad (44)$$

Observe that above we have 5 unknowns and 5 non linear equations, however we have a problem in solving the equation above because we still have the expectations. We have to solve this through a guess of a value for  $k_t$ . We are going to guess the value of  $k_t$  by the following expression:

$$\hat{k}_t = \phi_1 \hat{k}_{t-1} + \phi_2 \hat{z}_t \quad (45)$$

By using the five equations above we obtain that:

$$(1 + \alpha^2 \beta) \hat{k}_t = \alpha \beta \mathbb{E}_t \hat{k}_{t+1} + \alpha \hat{k}_{t-1} - (1 - \rho - \alpha \beta) \hat{z}_t \quad (46)$$

By taking expectations of equation (45) one can get the following result:

$$\mathbb{E}[\hat{k}_{t+1}] = \phi_1 \hat{k}_t + \phi_2 \rho \hat{z}_t \quad (47)$$

By replacing this value in the expression (46) yield us the following result:

$$(1 + \alpha^2 \beta) \hat{k}_t = \alpha \beta \phi_1 \hat{k}_t + \alpha \beta \phi_2 \rho \hat{z}_t + \alpha \hat{k}_{t-1} - (1 - \rho - \alpha \beta) \hat{z}_t \quad (48)$$

By isolating the value of  $\hat{k}_t$  we achieve the following equation:

$$\hat{k}_t = \frac{\alpha}{1 + \alpha^2 \beta - \alpha \beta \phi_1} + \frac{(1 + \alpha \beta \phi_2 \rho - \rho \alpha \beta)}{1 + \alpha^2 \beta - \alpha \beta \phi_1} \hat{z}_t \quad (49)$$

Observe that the value of  $\phi_1$  is given by the following expression:

$$\phi_1 = \frac{\alpha}{1 + \alpha^2 \beta - \alpha \beta \phi_1} \quad (50)$$

By isolating the value of  $\phi_1$  we get that we can have the both values listed below:

$$\phi_1 = \frac{1}{\alpha \beta} \quad \text{or} \quad \phi_1 = \alpha \quad (51)$$

By transversality condition we eliminate the solution  $\phi_1 = \frac{1}{\alpha \beta}$ , since in this case the process would be explosive. Therefore given the value of  $\phi_1 = \alpha$  then we have the value of  $\phi_2 = 1$  and equation (45) becomes:

$$\hat{k}_t = \alpha \hat{k}_{t-1} + \hat{z}_t \quad (52)$$

Observe also that we can obtain the following equations:

$$\hat{y}_t = \alpha \hat{k}_{t-1} + \hat{z}_t \quad (53)$$

$$\hat{c}_t = \alpha \hat{k}_{t-1} + \hat{z}_t \quad (54)$$

## 2 A generic DSGE model

We first begin by defining the model of the problem:

$$U = \max_{x_t, y_t} \mathbb{E}_0 \sum_{t=0}^{\infty} \beta^t u(x_t, y_t) \quad (55)$$

subject to

$$x_t = g(x_{t-1}, y_t, z_t) \quad (\text{or} \quad x_{t+1} = g(x_t, y_t, z_t)) \quad (56)$$

$$z_t = f(z_{t-1}, \epsilon_t), \quad \epsilon_t \sim iid(0, \Sigma) \quad (57)$$

$$x_{-1} \quad (\text{or} \quad x_0) \quad \text{and} \quad z_0 \quad \text{given} \quad (58)$$

Observe that:

1. The vector of endogenous state variables is given by  $x_t$ , which is a  $m \times 1$  vector;
2. The vector of exogenous state variables (stochastic shocks) is given by:  $z_t$ ;
3. The vector of all other endogenous variables (including control variables) is given by  $y_t$ , which is a  $n \times 1$  vector. In order to solve the model we have to do the following steps:
  1. Write the Lagrangian;
  2. Take first order conditions;
  3. Collect all other equations that come from market clearing, policy rules etc;
  4. Equilibrium conditions: a system of  $v$  (first-order) difference equations o  $v$  variables.

In general we have that DSGE models have large number of variables and large numbers of state variables  $\implies$  very complicated to solve with Global Methods.



### 3 Blanchard-Kahn Method

Write the system of linear difference equations as

$$A \begin{bmatrix} \hat{x}_t \\ \mathbb{E}_t \hat{y}_{t+1} \end{bmatrix} = B \begin{bmatrix} \hat{x}_{t-1} \\ \hat{y}_t \end{bmatrix} + C \hat{z}_t \quad (59)$$

In order to solve the system above we assume that  $z_t$  is a stable stochastic process. Moreover two issues are important for solving equation above:

- (a) The matrix A may not be singular;
- (b) Some components of  $x_t$  are predetermined and others are non-predetermined.

The method of Blanchard and Kahn (1980) assume that A is non singular. As a result, we define  $F = A^{-1}B$  and apply the Jordan decomposition to F. Therefore by assuming that A is invertible, we transform to:

$$\begin{bmatrix} \hat{x}_t \\ \mathbb{E}_t \hat{y}_{t+1} \end{bmatrix} = F \begin{bmatrix} \hat{x}_{t-1} \\ \hat{y}_t \end{bmatrix} + G \hat{z}_t \quad (60)$$

where we have that  $F = A^{-1}B$  is a  $(n+m) \times (n+m)$  and  $G = A^{-1}C$ .

By applying the Jordan decomposition to F lead us to the following:

$$F = H J H^{-1} = \begin{bmatrix} v_1 & \dots & v_{n+m} \end{bmatrix} \begin{bmatrix} \lambda_1 & \dots & 0 \\ \vdots & \ddots & \vdots \\ 0 & \dots & \lambda_{n+m} \end{bmatrix} \begin{bmatrix} v_1 & \dots & v_{n+m} \end{bmatrix}^{-1} \quad (61)$$

where the eigenvalues are ordered such that  $|\lambda_1| < |\lambda_2| < \dots < |\lambda_{n+m}|$  and  $v_i$  are their corresponding eigenvectors. Let  $h$  be the number of eigenvalues of J that are outside the unit circle,  $|\lambda_i| > 1$ .

#### Proposition Blanchard-Kahn, 1980

- (a) If  $h = n$ , the system of stochastic difference equations has a unique solution.
- (b) If  $h > n$ , the system of linear stochastic difference equations has no solutions.
- (c) If  $h < n$ , the system of linear stochastic difference equations has infinite solutions.

**Uniqueness:** For every free variable, you need one eigenvalue that is larger than one (saddle path stability).

**Multiplicity:** Not enough eigenvalues larger than one (indeterminacy).

Now suppose that the solution is unique.

In order to solve the system of difference equations:

$$\begin{bmatrix} \hat{x}_t \\ \mathbb{E}_t \hat{y}_{t+1} \end{bmatrix} = F \begin{bmatrix} \hat{x}_{t-1} \\ \hat{y}_t \end{bmatrix} + G \hat{z}_t \quad (62)$$

we do a change of variables according to:

$$\begin{bmatrix} \tilde{x}_{t-1} \\ \tilde{y}_t \end{bmatrix} = H^{-1} \begin{bmatrix} \hat{x}_{t-1} \\ \hat{y}_t \end{bmatrix} \quad \text{and} \quad \begin{bmatrix} \tilde{x}_t \\ \mathbb{E}_t \tilde{y}_{t-1} \end{bmatrix} = H^{-1} \begin{bmatrix} \hat{x}_t \\ \mathbb{E}_t \hat{y}_{t+1} \end{bmatrix} \quad (63)$$

which implies that:

$$\begin{bmatrix} \tilde{x}_t \\ \mathbb{E}_t \tilde{y}_{t+1} \end{bmatrix} = J \begin{bmatrix} \tilde{x}_{t-1} \\ \tilde{y}_t \end{bmatrix} + V \hat{z}_t \quad (64)$$

where  $V = H^{-1}G$ .

The matrix  $J$  is diagonal, with the eigenvalues in the diagonal ordered from smallest to largest. By partitioning the matrix we can obtain that:

$$\begin{bmatrix} \tilde{x}_t \\ \mathbb{E}_t \tilde{y}_{t+1} \end{bmatrix} = \begin{bmatrix} J_1 & 0 \\ 0 & J_2 \end{bmatrix} \begin{bmatrix} \tilde{x}_{t-1} \\ \tilde{y}_t \end{bmatrix} + \begin{bmatrix} V_1 \\ V_2 \end{bmatrix} \hat{z}_t \quad (65)$$

Therefore we have the following equation:

$$\tilde{x}_t = J_1 \tilde{x}_{t-1} + V_1 \hat{z}_t \quad (66)$$

The system above is a system of uncoupled difference equations which is stable, since all eigenvalues in  $J_1$  are inside the unit circle. Moreover we also have that:

$$\mathbb{E}_t \tilde{y}_{t+1} = J_2 \tilde{y}_t + V_2 \hat{z}_t \implies \tilde{y}_t = J_2^{-1} \mathbb{E}_t \tilde{y}_{t+1} - J_2^{-1} V_2 \hat{z}_t \quad (67)$$

By doing the iteration of the expression (67) and taking expectations we achieve that:

$$\tilde{y}_{t+1} = J_2^{-1} \mathbb{E}_{t+1} \tilde{y}_{t+2} - J_2^{-1} V_2 \hat{z}_{t+1} \quad (68)$$

$$\mathbb{E}_t \tilde{y}_{t+1} = J_2^{-1} \mathbb{E}_t \mathbb{E}_{t+1} \tilde{y}_{t+2} - J_2^{-1} V_2 \mathbb{E}_t \hat{z}_{t+1} = J_2^{-1} \mathbb{E}_t \tilde{y}_{t+2} \quad (69)$$

After many iterations we achieve that:

$$\tilde{y}_t = -J_2^{-1} V_2 \hat{z}_t \quad (70)$$

Then we have that:

$$\tilde{x}_t = J_1 \tilde{x}_{t-1} + V_1 \hat{z}_t \quad (71)$$

$$\tilde{y}_t = -J_2^{-1} V_2 \hat{z}_t \quad (72)$$

This system can be solved with known methods for uncoupled difference equations, and we recover the original variables from using the above solutions and the change of variables

$$\begin{bmatrix} \hat{x}_{t-1} \\ \hat{y}_t \end{bmatrix} = \begin{bmatrix} H_{11} & H_{12} \\ H_{21} & H_{22} \end{bmatrix} \begin{bmatrix} \tilde{x}_{t-1} \\ \tilde{y}_t \end{bmatrix} \quad (73)$$