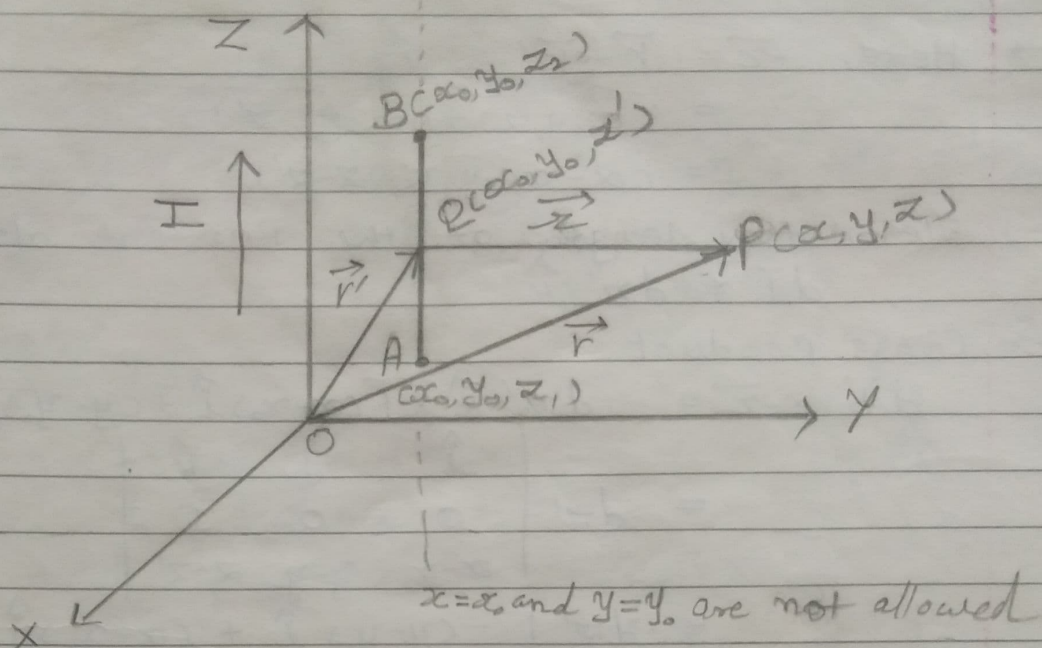


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Magnetic field due to straight conducting filament

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→ A current carrying straight filament is placed parallel to z -axis.

→ Here,

(1) source point, $Q(x_0, y_0, z')$

(2) observation point, $P(x, y, z)$

(3) lower end of the filament, $A(x_0, y_0, z_1)$

(4) upper end of the filament, $B(x_0, y_0, z_2)$

(5) The direction of current I is from A to B

→ The magnetic field \vec{B} at P can be written as,

$$\begin{aligned}\vec{B} &= \frac{\mu_0 I}{4\pi} \int_A^B \frac{d\vec{l}' \times \vec{r}}{|\vec{r}|^3} \\ &= \frac{\mu_0 I}{4\pi} \vec{H}\end{aligned}$$

→ Where,

$$\vec{H} = \int_A^B \frac{d\vec{l}' \times \vec{r}}{|\vec{r}|^3} \quad (1)$$

→ Here, $\vec{r} = \vec{r} - \vec{r}'$
 $= (x, y, z) - (x_0, y_0, z')$
 $= (x - x_0, y - y_0, z - z')$

→ Elementary length of the filament along z -axis,
 $d\vec{l}' = dz' \hat{k}$

→ Cross product,

$$d\vec{l}' \times \vec{r} = dz' \hat{k} \times [(x - x_0)\hat{i} + (y - y_0)\hat{j} + (z - z')\hat{k}]$$

$$= dz' \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ 0 & 0 & 1 \\ x - x_0 & y - y_0 & z - z' \end{vmatrix}$$

$$= dz' [-(y - y_0)\hat{i} + (x - x_0)\hat{j} + 0\hat{k}]$$

→ $|\vec{r}| = [(x - x_0)^2 + (y - y_0)^2 + (z - z')^2]^{1/2}$

→ Now, sub. all these values in eqⁿ (1)

$$\therefore \vec{H} = \int_{z_1}^{z_2} \frac{[-(y - y_0)\hat{i} + (x - x_0)\hat{j} + 0\hat{k}] dz'}{[(x - x_0)^2 + (y - y_0)^2 + (z - z')^2]^{3/2}}$$

→ The components of \vec{H} are,

$$H_x = - \int_{z_1}^{z_2} \frac{(y - y_0) dz'}{[(x - x_0)^2 + (y - y_0)^2 + (z - z')^2]^{3/2}}$$

$$H_y = \int_{z_1}^{z_2} \frac{(x - x_0) dz'}{[(x - x_0)^2 + (y - y_0)^2 + (z - z')^2]^{3/2}}$$

$$H_z = 0$$

→ Let, $u = x - x_0$

$$v = y - y_0$$

$$w' = z - z'$$

$$\Rightarrow dw' = -dz'$$

$$\rightarrow w_1 = z - z_1$$

$$w_2 = z - z_2$$

$$\begin{aligned}
 (1) \quad H_x &= - \int_{\omega_1}^{\omega_2} \frac{V (-d\omega')}{\omega_1 [\omega^2 + V^2 + \omega'^2]^{3/2}} \\
 &= V \int_{\omega_1}^{\omega_2} \frac{d\omega'}{[a^2 + \omega'^2]^{3/2}}, \quad a^2 = \omega^2 + V^2 \text{ (constant)}
 \end{aligned}$$

→ take $\omega' = a \tan \theta$, $\Rightarrow d\omega' = a \sec^2 \theta d\theta$

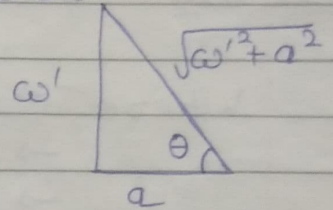
$$\int \frac{d\omega'}{[a^2 + \omega'^2]^{3/2}}$$

$$= \int \frac{a \sec^2 \theta d\theta}{[a^2 + a^2 \tan^2 \theta]^{3/2}}$$

$$= \frac{1}{a^2} \int \cos \theta d\theta$$

$$= \frac{1}{a^2} \sin \theta$$

$$= \frac{1}{a^2} \frac{\omega'}{\sqrt{\omega'^2 + a^2}}$$



$$\begin{aligned}
 \therefore H_x &= \frac{V}{a^2} \left[\frac{\omega'}{\sqrt{a^2 + \omega'^2}} \right]_{\omega_1}^{\omega_2} \\
 &= \frac{V}{a^2} \sum_{i=1}^2 \frac{(-1)^i \omega_i}{\sqrt{a^2 + \omega_i^2}}
 \end{aligned}$$

→ Similarly we can find,

$$(2) \quad H_y = -\frac{V}{a^2} \sum_{i=1}^2 \frac{(-1)^i \omega_i}{\sqrt{a^2 + \omega_i^2}}$$

$$(3) \quad H_z = 0$$

→ So, the field components for a straight current carrying filament are,

$$(1) B_x = \frac{\mu_0 I}{4\pi} \left(\frac{V}{a^2} \right) \sum_{i=1}^2 (-1)^i \frac{\omega_i}{\sqrt{a^2 + \omega_i^2}}$$

$$(2) B_y = -\frac{\mu_0 I}{4\pi} \left(\frac{U}{a^2} \right) \sum_{i=1}^2 (-1)^i \frac{\omega_i}{\sqrt{a^2 + \omega_i^2}}$$

$$(3) B_z = 0.0$$

Where, $\rightarrow a^2 = U^2 + V^2$,

$\rightarrow U = x - x_0$ $\rightarrow V = y - y_0$,

$\rightarrow \omega_1 = z - z_1$ $\rightarrow \omega_2 = z - z_2$

$\rightarrow \mu_0 = 4\pi \times 10^{-7} \text{ SI}$

$\rightarrow I$ is flowing from lower to upper end

* References :

- 1 Analytical derivation of magnetic field and vector potential due to different current carrying conducting geometries, Mrityunjay Kundu & Shishir P. Deshpande, IPR
- 2 Special thanks to Arattu Ramesh Sir.