ESC201T : Introduction to Electronics

Lecture 17: LCR Filters (Resonance)

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Wireless Transmission of Speech signal

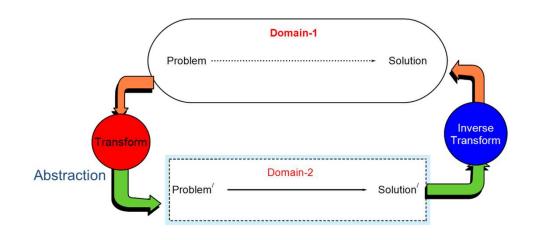
$$x(t) = x_m \sin(2\pi \times 10^3 t)$$

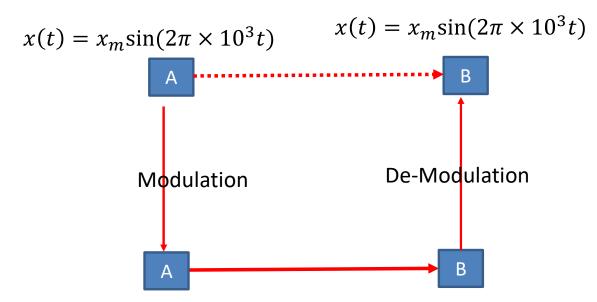




$$y(t) = y_m \sin(2\pi \times 450 \times 10^3 t)$$

Carrier wave



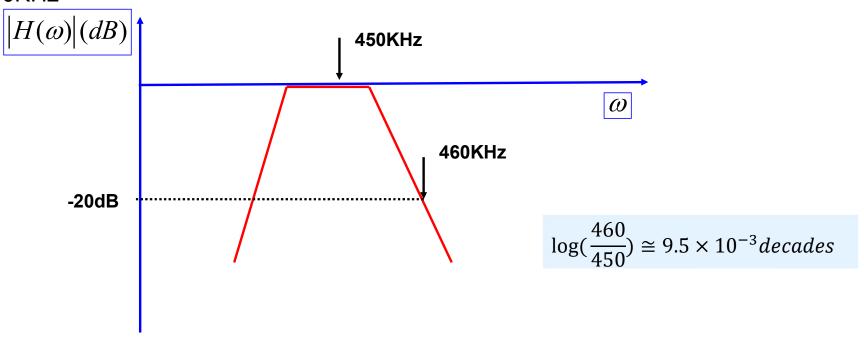


$$Z(t) = (y_m + m \times x(t))\sin(2\pi \times 450 \times 10^3 t)C$$

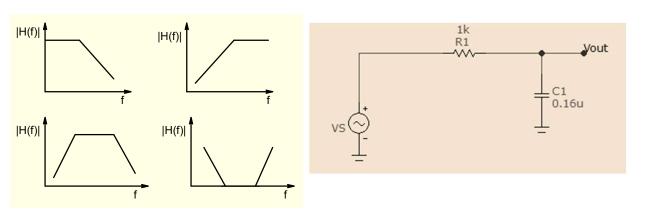
Amplitude Modulated (AM) Radio

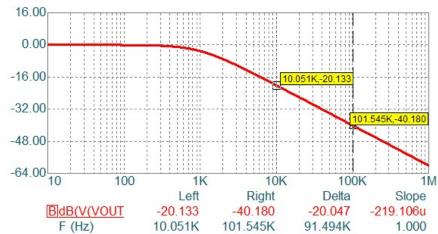
Different radio channels are separated by very narrow frequency interval.

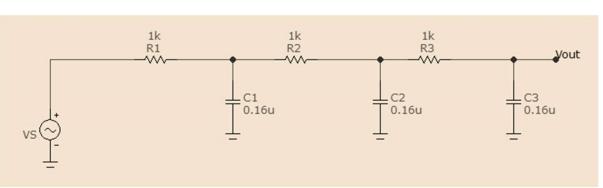
For example, one may want to receive a 450KHz signal but reject 460KHz or 440KHz

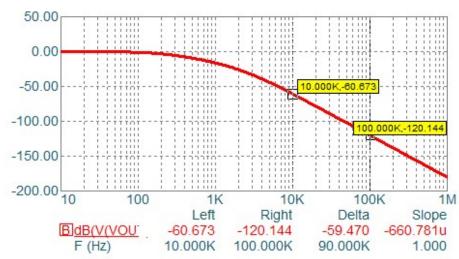


This implies an attenuation of ~ -2000 dB/decade





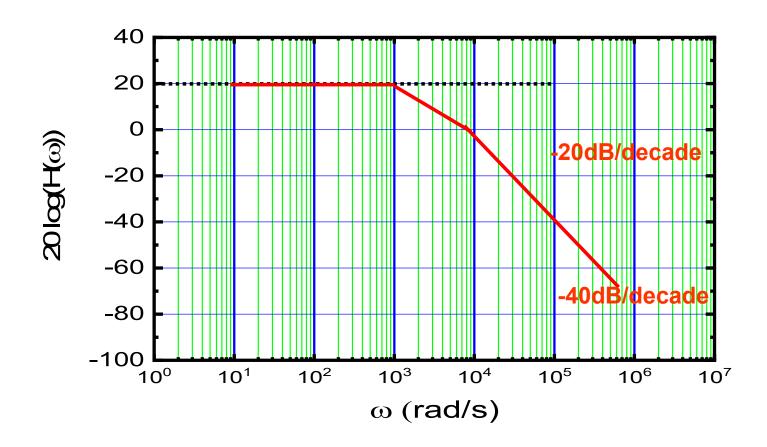




Second Order System

$$H(\omega) = \frac{10}{1+j\frac{\omega}{10^3}} \times \frac{1}{1+j\frac{\omega}{10^4}}$$

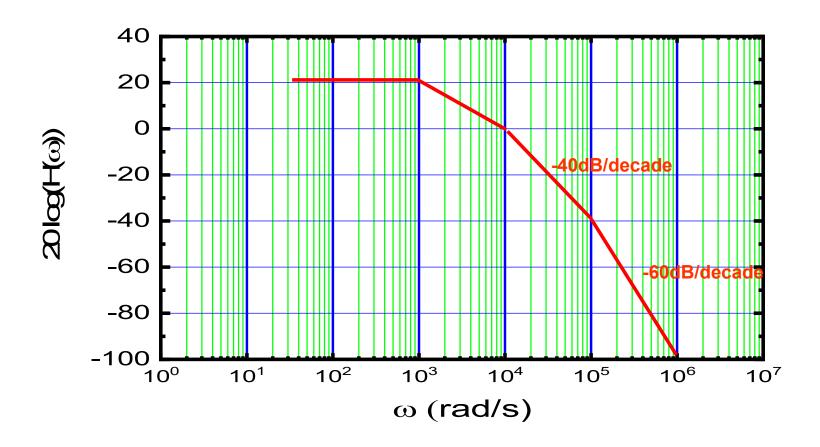
$$20\text{Log}_{10}(|H(\omega)|) = 20 - 10Log_{10}(1 + (\frac{\omega}{10^3})^2) - 10Log_{10}(1 + (\frac{\omega}{10^4})^2)$$



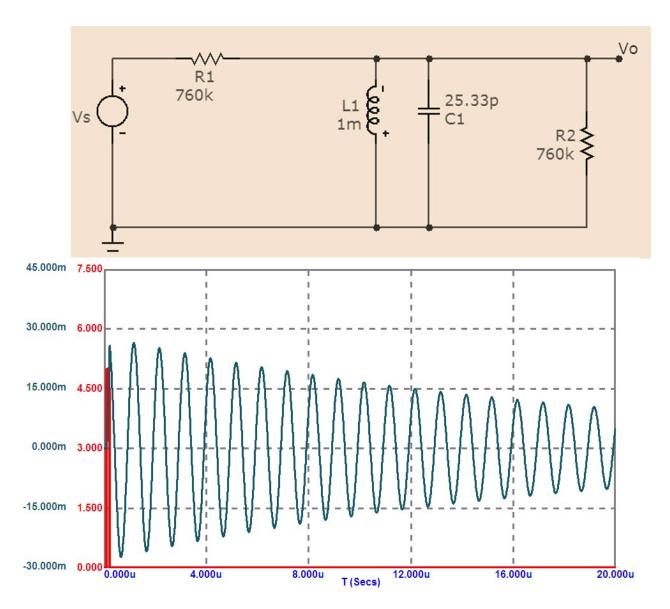
Third Order System

$$H(\omega) = \frac{10}{1 + j\frac{\omega}{10^3}} \times \frac{1}{1 + j\frac{\omega}{10^4}} \times \frac{1}{1 + j\frac{\omega}{10^5}}$$

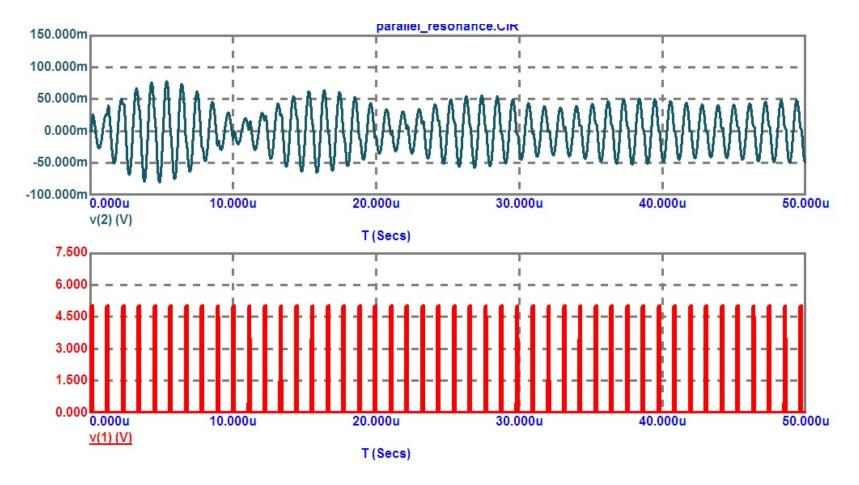
$$20\text{Log}_{10}(|H(\omega)|) = 20 - 10Log_{10}(1 + (\frac{\omega}{10^3})^2) - 10Log_{10}(1 + (\frac{\omega}{10^4})^2) - 10Log_{10}(1 + (\frac{\omega}{10^5})^2)$$



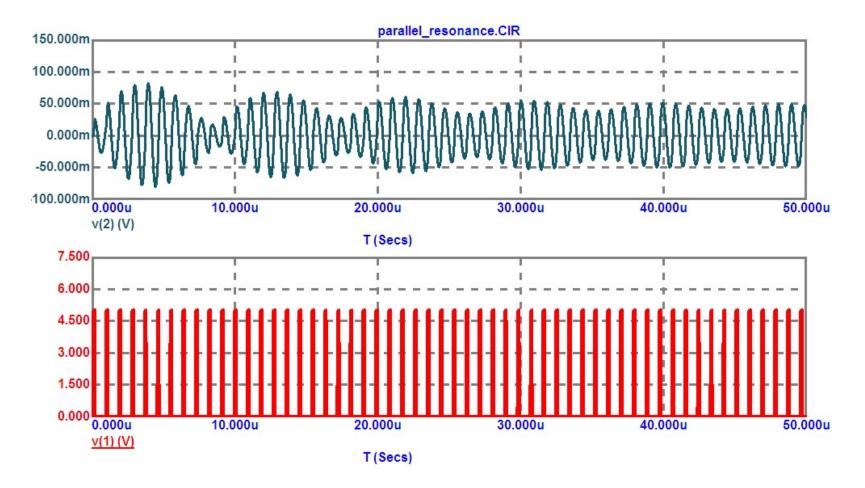
Resonance



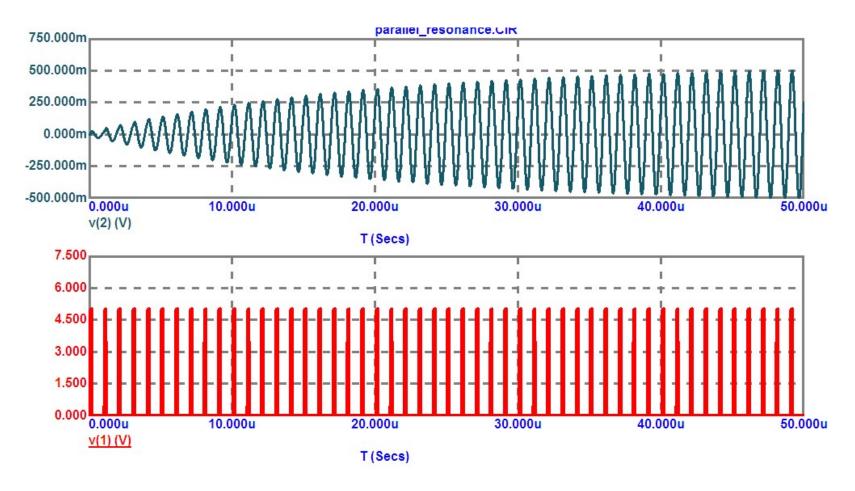
A small disturbance leads to oscillatory behavior



 $T = 1.1 \mu s$

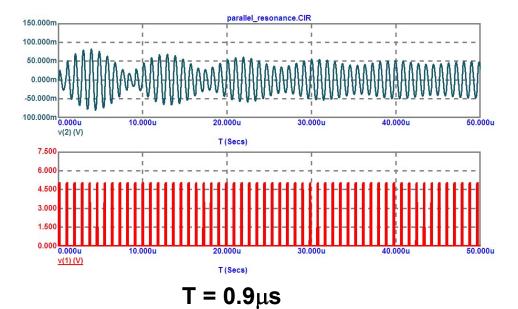


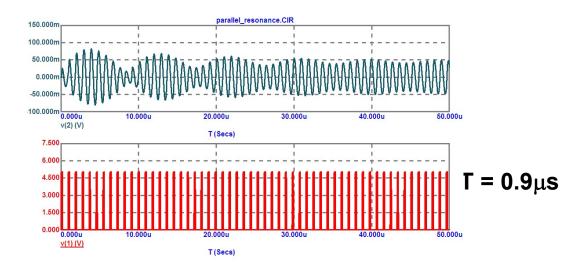
 $T = 0.9 \mu s$

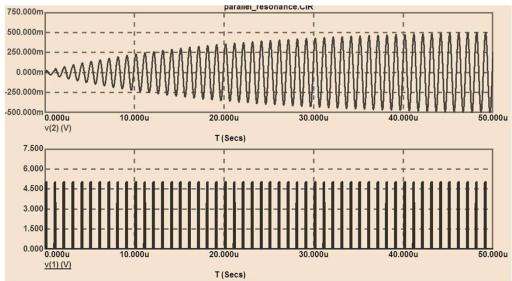


 $T = 1\mu s$

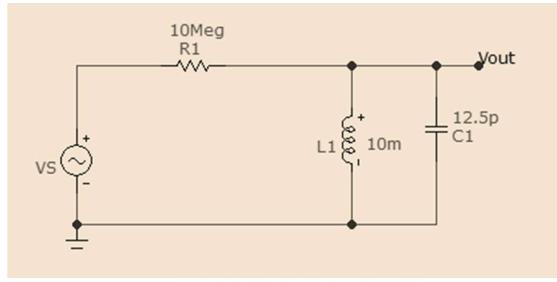
The amplitude is 10 times larger even though input magnitude is same!

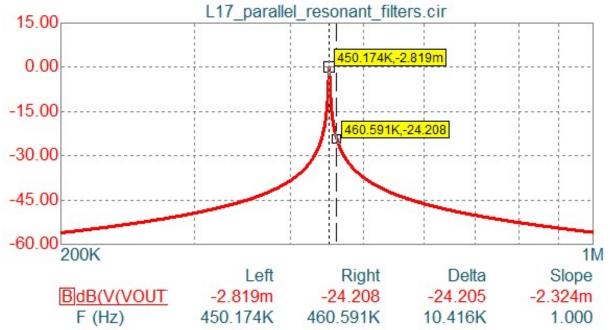


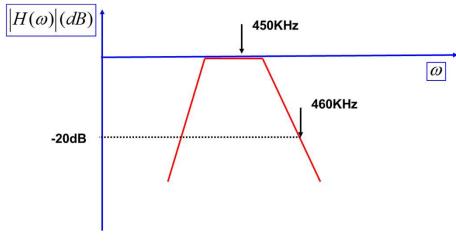


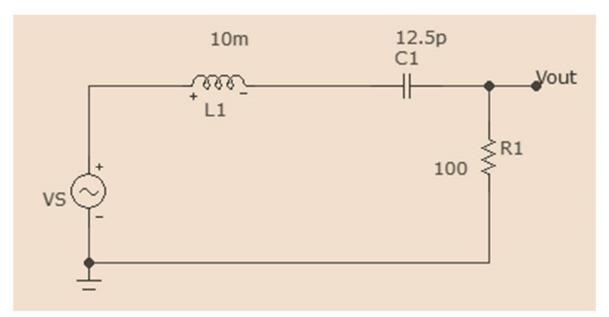


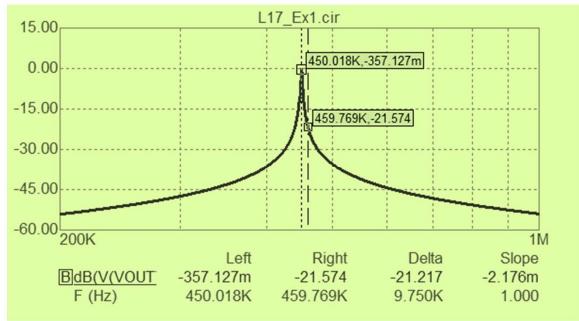
 $T = 1\mu s$





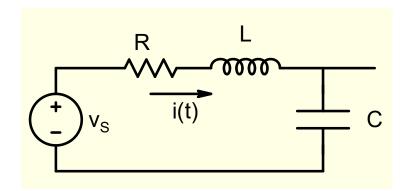






Series Resonant Circuit

In this series resonant circuit, current reaches a peak at a condition in which capacitive and inductive reactance cancel each other to give rise to a purely resistive circuit



$$Z_{eq} = R + j\omega L - j\frac{1}{\omega C}$$

Resonant frequency:
$$j\omega_{O}L - j\frac{1}{\omega_{O}C} = 0 \Rightarrow \omega_{O} = \frac{1}{\sqrt{LC}}$$

$$f_O = \frac{1}{2\pi\sqrt{LC}}$$

$$Z_{eq} = R$$

Current and voltage are in phase (power factor is unity) and current is maximum!

$$|I(\omega)| = \frac{V_m}{\sqrt{R^2 + (\omega L - \frac{1}{\omega C})^2}}$$

0.707 $\overline{\omega}_2$ $\dot{\omega}_{0}$

 ω_1 and ω_2 are called half power frequencies since $P \propto I^2$

$$|I(\omega_1)| = \frac{V_m}{\sqrt{R^2 + (\omega_1 L - \frac{1}{\omega_1 C})^2}} = \frac{V_m}{\sqrt{2}R}$$

$$\omega_1 = -\frac{R}{2L} + \sqrt{\left(\frac{R}{2L}\right)^2 + \frac{1}{LC}} \qquad \omega_2 = \frac{R}{2L} + \sqrt{\left(\frac{R}{2L}\right)^2 + \frac{1}{LC}}$$

 $\overline{V_M/R}$

$$\omega_2 = \frac{R}{2L} + \sqrt{\left(\frac{R}{2L}\right)^2 + \frac{1}{LC}}$$

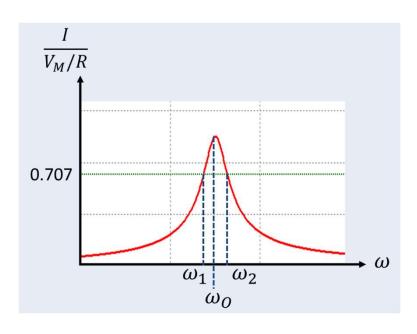
$$|I(\omega_2)| = \frac{V_m}{\sqrt{R^2 + (\omega_2 L - \frac{1}{\omega_2 C})^2}} = \frac{V_m}{\sqrt{2}R}$$

$$\omega_1 = -\frac{R}{2L} + \sqrt{\left(\frac{R}{2L}\right)^2 + \frac{1}{LC}}$$

$$\omega_2 = \frac{R}{2L} + \sqrt{\left(\frac{R}{2L}\right)^2 + \frac{1}{LC}}$$

$$\omega_O = \sqrt{\omega_1 \omega_2}$$

$$B = \omega_2 - \omega_1 = \frac{R}{L}$$



Quality (Q) factor: Sharpness of resonance

$$Q = \frac{\omega_O}{B} = \frac{\omega_O}{\Delta \omega} = \frac{\omega_O L}{R}$$

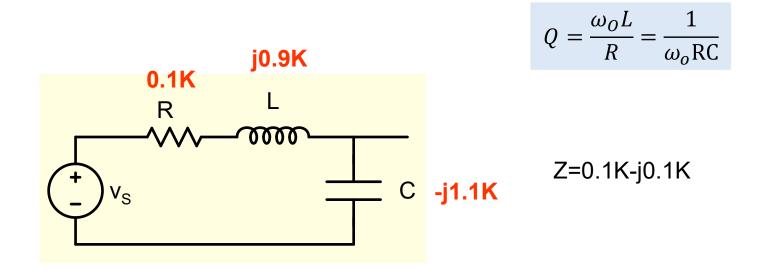
$$Q = 2\pi$$
 Peak Stored Energy

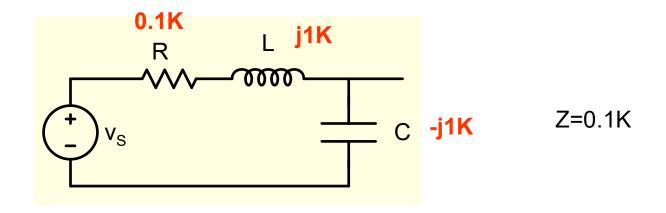
Energy dissipated in one period at resonance

$$Q = 2\pi \times \frac{\frac{1}{2}L \times I_m^2}{\frac{1}{2}I_m^2R \times T_O} = \frac{\omega_O L}{R}$$

$$\omega_O = \frac{1}{\sqrt{LC}} \Rightarrow Q = \frac{1}{\omega_O CR}$$

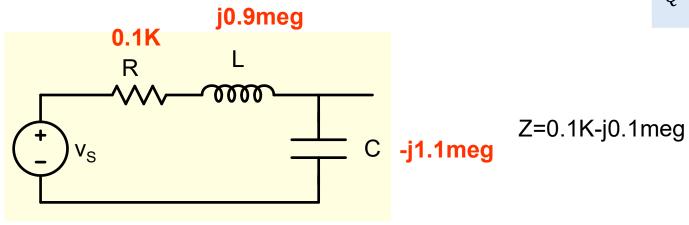
$$\omega_O = \frac{1}{\sqrt{LC}} \Rightarrow Q = \frac{1}{\omega_O CR}$$

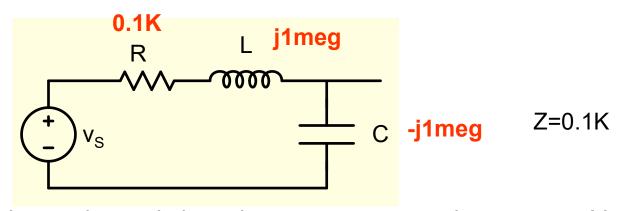




Not very large change in impedance as we approach resonance!

$$Q = \frac{\omega_O L}{R} = \frac{1}{\omega_O RC}$$

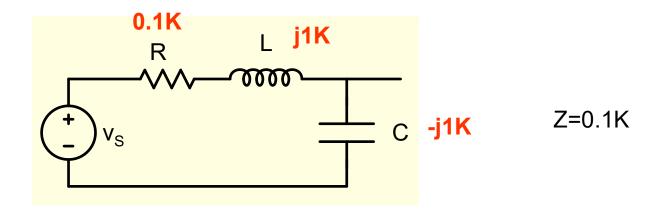


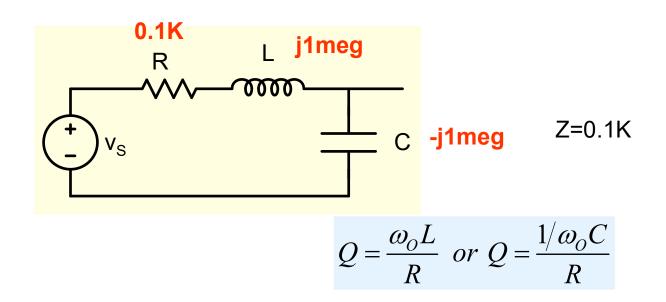


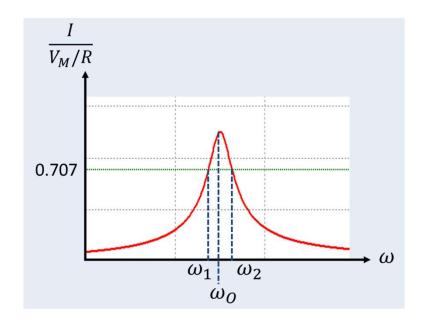
very large change in impedance as we approach resonance! Implying high quality factor



Quality factor Q







$$Q = \frac{\omega_O L}{R}$$

$$B = \omega_2 - \omega_1 = \frac{R}{L}$$

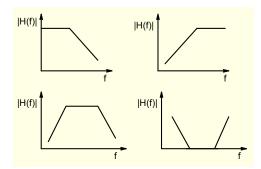
$$Q = \frac{\omega_O}{B} = \frac{\omega_O}{\Delta \omega}$$

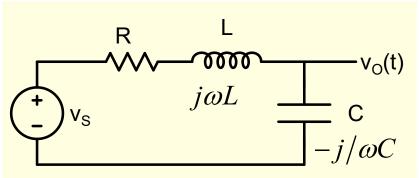
Hence Q represents sharpness of resonance

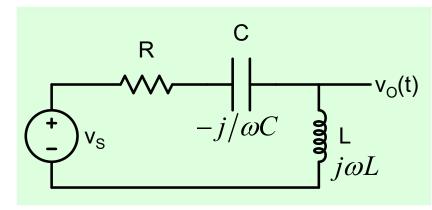
For high Q circuits:

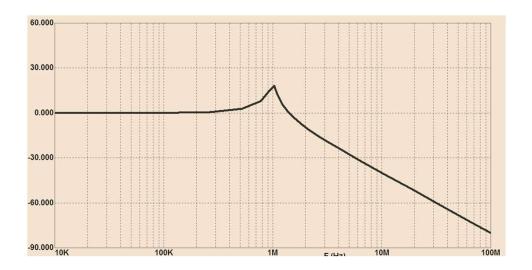
$$\omega_1 \simeq \omega_0 - \frac{B}{2}, \qquad \omega_2 \simeq \omega_0 + \frac{B}{2}$$

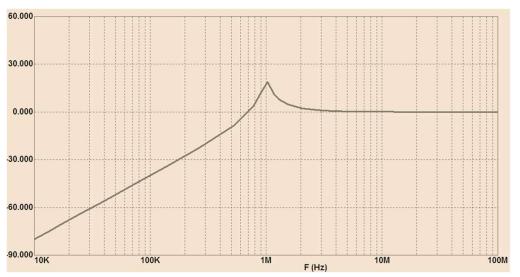
R-L-C filters

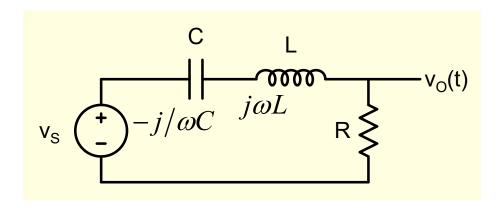


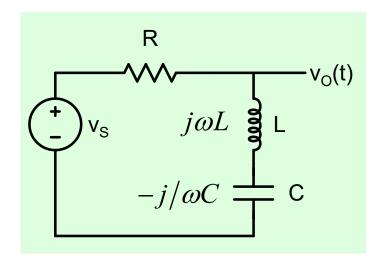


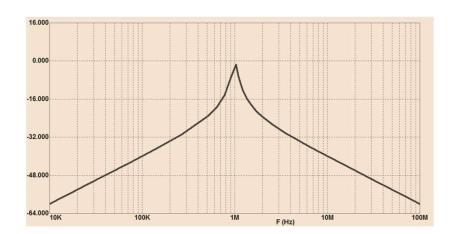


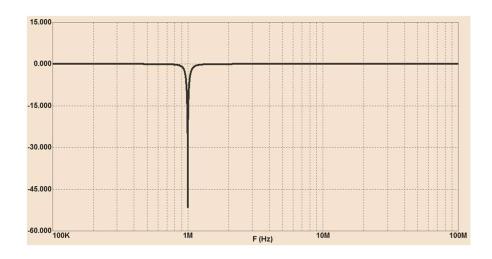


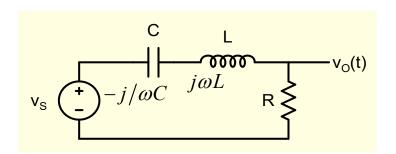


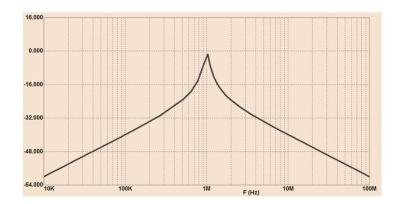












How much Q do we need to pass 450KHz but reject 460KHz by 20dB?

$$|H(\omega)| = \left| \frac{V_O(\omega)}{V_{IN}(\omega)} \right| = \frac{R}{\sqrt{R^2 + (\omega L - \frac{1}{\omega C})^2}}$$

Assuming $V_{IN} = 1V$ and noting that $Q = \omega_O L/R$

$$\left|V_O(\omega)\right| = \frac{1}{\sqrt{1 + \frac{\omega_O^2}{\omega^2} Q^2 (\frac{\omega^2}{\omega_O^2} - 1)^2}}$$
 For $\omega = \omega_O$, $V_O = 1$ so the signal simply passes through!
$$\omega_O = 2 \times \pi \times 450 \times 10^3 = 2.8 \times 10^6 \, rad \, / \, s$$

$$\omega_O = 2 \times \pi \times 450 \times 10^3 = 2.8 \times 10^6 \, rad \, / \, s$$

$$\left|V_{O}(\omega)\right| = \frac{1}{\sqrt{1 + \frac{\omega_{O}^{2}}{\omega^{2}}Q^{2}(\frac{\omega^{2}}{\omega_{O}^{2}} - 1)^{2}}} \quad \left|V_{O}(\omega)\right| \cong \frac{\omega_{O}^{2}}{Q \times (\omega^{2} - \omega_{O}^{2})} \quad \left|V_{O}(\omega)\right| \cong \frac{\omega_{O}}{2Q \times (\omega - \omega_{O})}$$

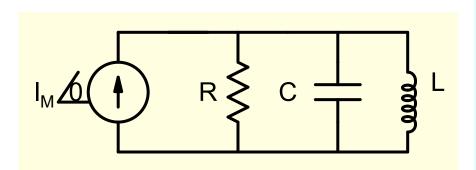
For an attenuation of -20dB or 10^{-1} at ω - ω o = 62.8 Krad/s

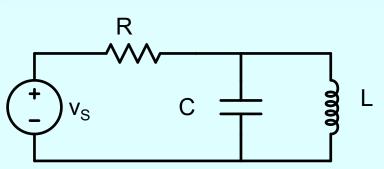
$$Q \cong 226.3$$

Example: for Q = 226.3 at 450KHz

$$Q = \frac{\omega_o L}{R}$$
 Suppose $L = 10^{-3}H$; $\Rightarrow R = 12.5 \Omega$; $\Rightarrow C = 125pF$

Parallel Resonance





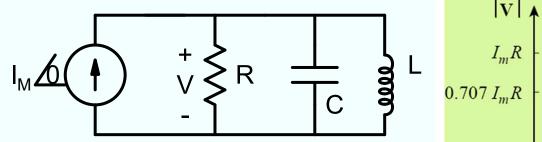
$$Y_{eq} = \frac{1}{R} + j\omega C - j\frac{1}{\omega L}$$

Resonant frequency:

$$j\omega_{O}C - j\frac{1}{\omega_{O}L} = 0 \Rightarrow \omega_{O} = \frac{1}{\sqrt{LC}}$$

$$f_O = \frac{1}{2\pi\sqrt{LC}}$$

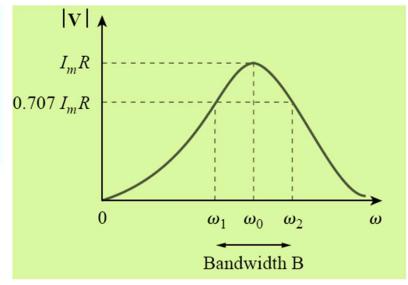
$$Z_{eq} = R$$



$$|V(\omega)| = \frac{I_m R}{\sqrt{1 + \frac{R^2 C^2}{L^2} (\omega L - \frac{1}{\omega C})^2}}$$

$$\omega_1 = -\frac{1}{2RC} + \sqrt{\left(\frac{1}{2RC}\right)^2 + \frac{1}{LC}}$$

$$\omega_2 = \frac{1}{2RC} + \sqrt{\left(\frac{1}{2RC}\right)^2 + \frac{1}{LC}}$$



$$B = \omega_2 - \omega_1 = \frac{1}{RC}$$

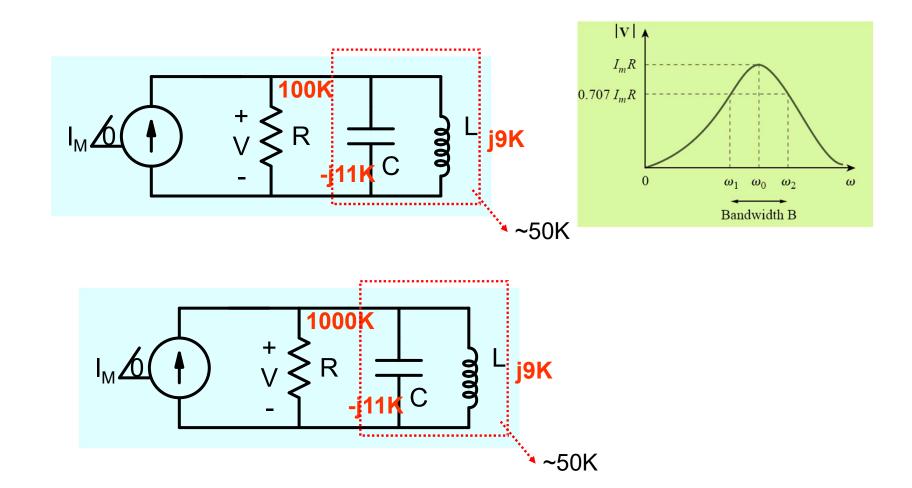
$$Q = \frac{\omega_0}{B} = \omega_0 RC = \frac{R}{\omega_0 L}$$

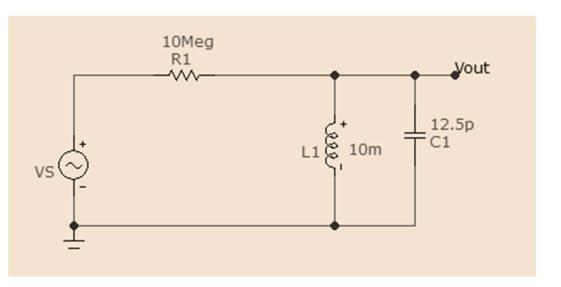
For high Q:

$$\omega_1 = \omega_0 \sqrt{1 + \left(\frac{1}{2Q}\right)^2} - \frac{\omega_0}{2Q}, \qquad \omega_2 = \omega_0 \sqrt{1 + \left(\frac{1}{2Q}\right)^2} + \frac{\omega_0}{2Q} \qquad \omega_1 \simeq \omega_0 - \frac{B}{2}, \qquad \omega_2 \simeq \omega_0 + \frac{B}{2}$$

$$\omega_1 \simeq \omega_0 - \frac{B}{2}, \qquad \omega_2 \simeq \omega_0 + \frac{B}{2}$$

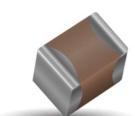
Why is
$$Q = \frac{R}{\omega L}$$
 for parallel resonance?





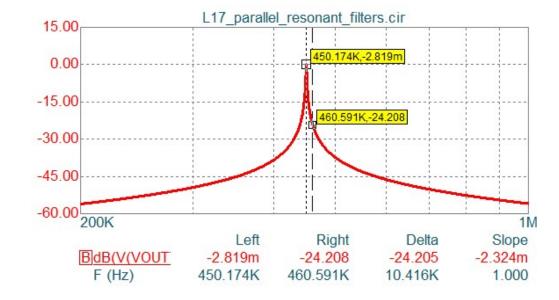
COG (NP0) Dielectric General Specifications

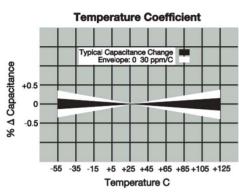


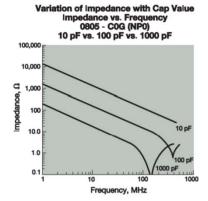


COG (NPO) is the most popular formulation of the "temperature-compensating," EIA Class I ceramic materials. Modern COG (NPO) formulations contain neodymium, samarium and other rare earth oxides.

COG (NPO) ceramics offer one of the most stable capacitor dielectrics available. Capacitance change with temperature is $0.130 \, \text{pm/}^{\circ}$ C which is less than $\pm 0.3\%$ C from -55°C to +125°C. Capacitance drift or hysteresis for COG (NPO) ceramics is negligible at less than $\pm 0.05\%$ versus up to $\pm 2\%$ for films. Typical capacitance change with life is less than $\pm 0.1\%$ for COG (NPO), one-fifth that shown by most other dielectrics. COG (NPO) formulations show no aging characteristics.



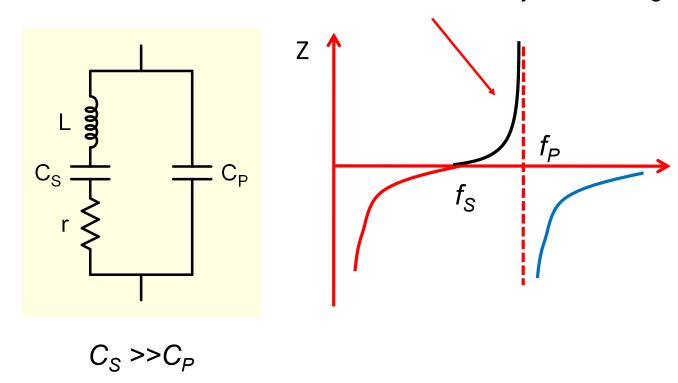




Piezoelectric Quartz Crystal

Inductive over a very narrow range

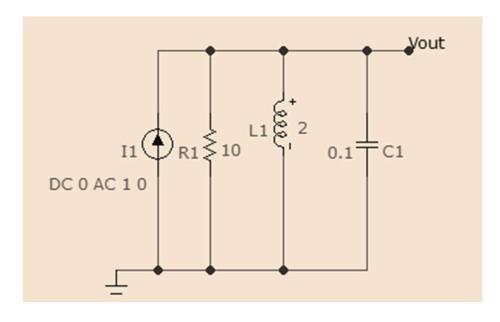




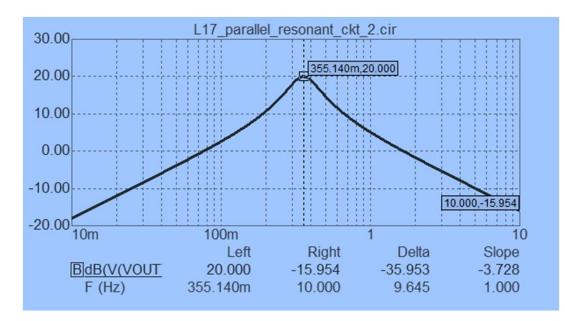
Q can be very high $^{\sim}10^4 - 10^6$

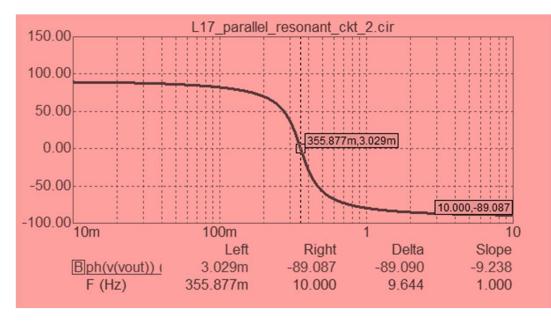
PARAMETERS	
ABRACON P/N	ABLS Series
Frequency	3.579545 MHz to 75 MHz
Operation Mode	AT cut (Fundamental or 3rd OT) or BT cut (See options) 3.579545MHz - 24.0MHz (Fundamental) (Standard) 24.01 - 75.00MHz (3rd- Overtone) (Standard) 24.01MHz - 50.00MHz (Fund. AT or BT) (Option. See 2.1)
Operating Temperature	0°C to + 70°C (see options)
Storage Temperature	- 55°C to + 125°C
Frequency Tolerance at +25°C	± 50 ppm max. (see options)
Frequency Stability over the Operating Temp. (Ref to +25°C)	± 50 ppm max. (see options)
Equivalent Series Resistance	See Table 1
Shunt Capacitance C ₀	7pF max.
Load Capacitance C _L	18pF (see options)
Drive Level	1 mW max., 100μW typical
Aging at 25°C ± 3°C Per Year	± 5ppm max.
Insulation Resistance	500 M Ω min at 100Vdc ± 15V
Spurious Responses	-3dB max.
Drive level dependency (DLD)	from 1µW to 500µW (minimum 7 points tested)

Resonant Frequency

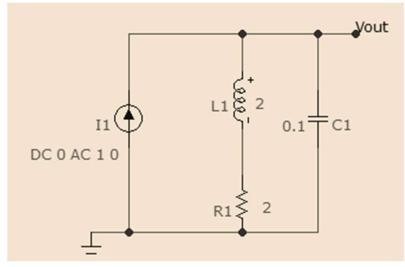


$$f_O = \frac{1}{2\pi\sqrt{LC}}$$





What is the resonant frequency (unity power factor)?

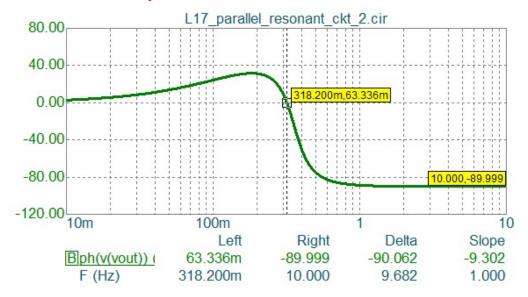


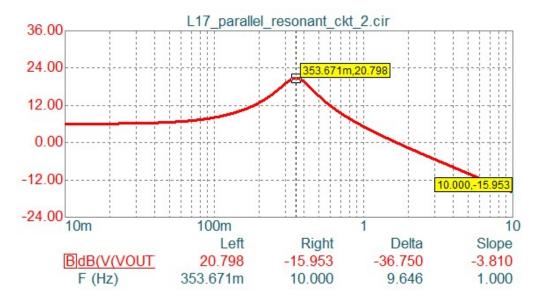
$$Y = j\omega 0.1 + \frac{1}{2 + j2\omega}$$

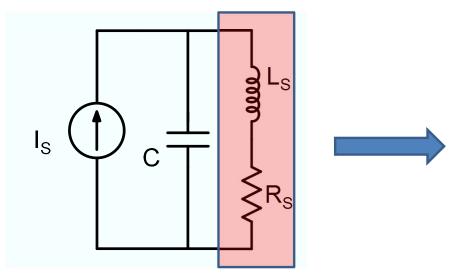
For unity power factor, imaginary part = 0

$$Y = \frac{2}{4 + 4\omega^2} + j\omega 0.1 - \frac{j2\omega}{4 + 4\omega^2}$$

$$0.1\omega_O - \frac{2\omega_O}{4 + 4\omega_O^2} = 0 \Rightarrow \omega_O = 2 \, rad/s$$







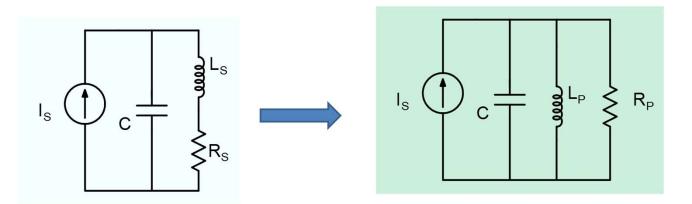
$$R_P = R_S + \frac{\omega^2 L_S^2}{R_S}$$

$$Y_S = \frac{1}{Z_S} = \frac{1}{R_S + j\omega L_S}$$

 $Z_S = R_S + j\omega L_S$

$$L_P = L_S + \frac{R_S^2}{\omega^2 L_S}$$

$$Y_{S} = \frac{R_{S} - j\omega L_{S}}{R_{S}^{2} + \omega^{2} L_{S}^{2}} = \frac{R_{S}}{R_{S}^{2} + \omega^{2} L_{S}^{2}} + \frac{1}{j\omega} \times \frac{\omega^{2} L_{S}}{R_{S}^{2} + \omega^{2} L_{S}^{2}} = \frac{1}{R_{P}} + \frac{1}{j\omega L_{P}}$$



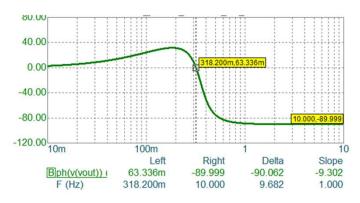
unity power factor frequency : $\omega_P L_P = \frac{1}{\omega_P C}$

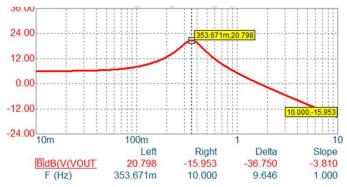
$$Y = \frac{1}{R_P} + j\omega C - \frac{j}{\omega_P L_P}$$

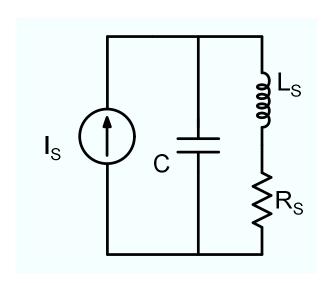
 Y_{min} is reached at a higher frequency than f_P

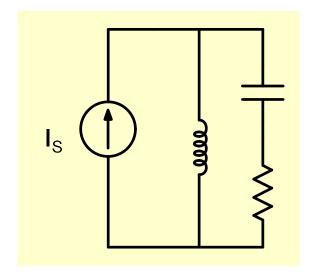
$$R_P = R_S + \frac{\omega^2 L_S^2}{R_S}$$

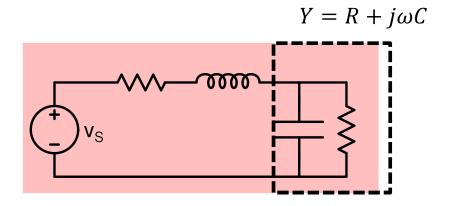
$$L_P = L_S + \frac{R_S^2}{\omega^2 L_S}$$











$$Z_S = \frac{1}{Y} = \frac{1}{R + j\omega C} = \frac{R - j\omega C}{R^2 + \omega^2 C^2}$$

