

Model Reference Adaptive Control Design for Self Balancing Robot

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OVERVIEW

 A self-balancing robot is a type of robot that can maintain its balance on two wheels without falling over. The self-balancing feature is achieved through the use of a PID (Proportional-Integral-Derivative) controller, which is a control loop feedback mechanism widely used in control systems



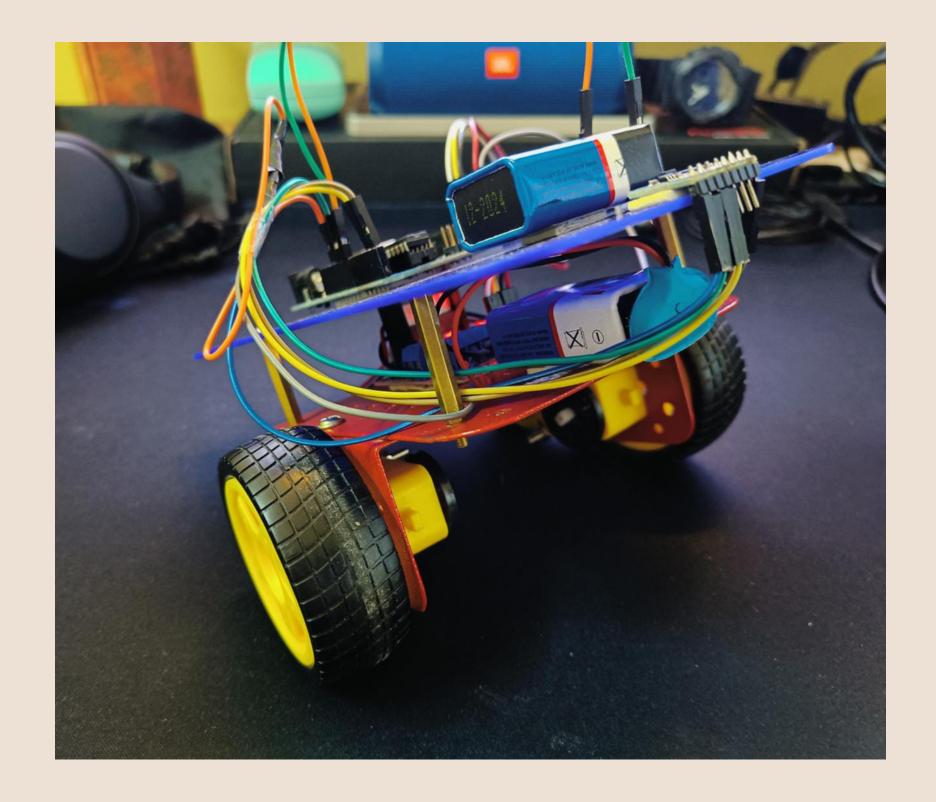
The PID controller constantly measures the robot's angle and compares it to the desired angle. If the robot's angle is not equal to the desired angle, the controller calculates an error value and adjusts the motor to correct the error. The proportional component of the PID controller adjusts the motor proportionally to the error value, the integral component accumulates the error over time, and the derivative component predicts the future error value based on the current rate of change.

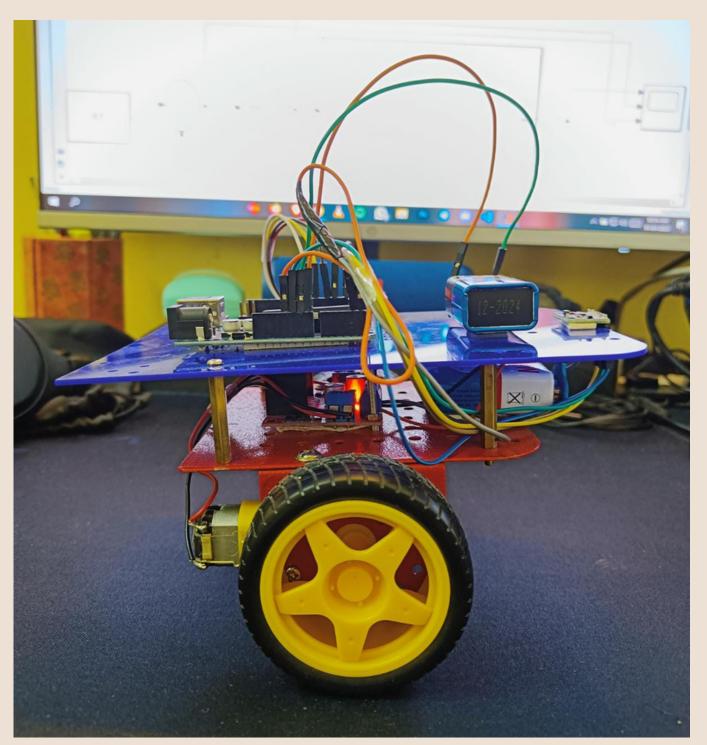
The purpose of Derivative control is to provide a "dampening" effect that can help

The integral component of the control algorithm can remove any steady-state error in the system

provide a "dampening" effect that can help limit overshoot and converge more quickly upon the Setpoint

II MECHANICAL STRUCTURE OF THE ROBOT

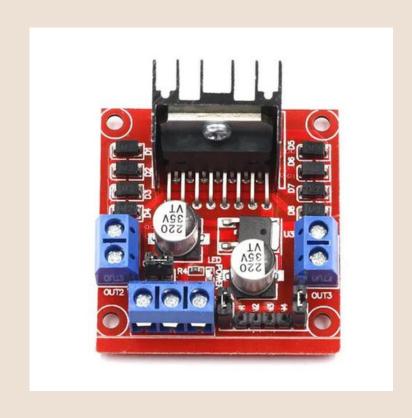




The Components used

II MECHANICAL STRUCTURE OF THE ROBOT







Arduino Uno Microcontroller L298N Motor Driver Module MPU6050 Gyroscope

II MECHANICAL STRUCTURE OF THE ROBOT



BO Motors



2 Wheel Chassis



Wheels



9V Batteries

III DESIGNING THE SYSTEM

The Transfer Function

The model is assumed to be a first order unstable system with its transfer function assumed to be :

$$G(s) = \frac{Ke^{-\theta s}}{(\tau s - 1)}$$

where, K= 800 is the Gain,

τ = 1000 is the Time Constant

 θ = 0.02. is the Delay

The Internal Model Control (IMC) Filter

We are using PID controller for our model and we have used the IMC-PID algorithm to design the PID. The IMC-PID algorithm uses the dynamics of the process being controlled to improve the performance of the PID controller. This can result in faster response times and better disturbance rejection compared to a standard PID controller.

We are using a first order IMC filter for which the transfer function is given as:

$$F(s) = \frac{\alpha s + 1}{\lambda s + 1}$$

where α is used to cancel the right half of s-plane zero and λ is the Filter Time Constant.

The Final Equation for IMC-PID Design Technique:

$$C(s) = \frac{(\alpha s + 1) (s \theta + 2)}{K s(2 \lambda - 2 \alpha + 2 \theta)}$$

The Controller can be expressed in PID form as:

$$C(s) = k_c(1 + \frac{1}{\tau_i s} + \tau_d s)$$

The values of the variables can be given as:

$$k_c = \frac{2 \alpha + \theta}{2 K (\alpha - \lambda - \theta)},$$

$$\tau_I = \alpha + \frac{\theta}{2}$$

$$\tau_D = \frac{\alpha \theta}{2 \alpha + \theta}$$

$$\alpha = \frac{2 \lambda \tau + \lambda \theta + 2 \tau \theta}{2 \tau - \theta}$$

Hence, the final PID values, viz, Kp, Ki and Kd are given by :

1.
$$K_p = k_c$$

$$2. K_i = \frac{k_c}{\tau_i}$$

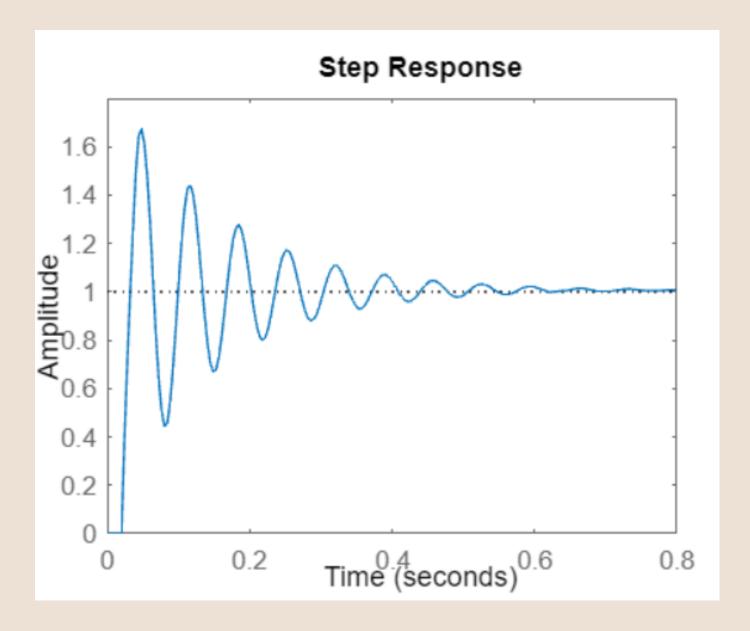
3.
$$K_d = k_c * \tau_d$$

A MatLab LiveScript is used to compute these values and is then used in the Simulink Model.

```
clear;
k = 800
tau = 1000
theta = 0.02
lambda = 0.5
alfa = (2*lambda*tau + lambda*theta + 2*tau*theta)/(2*tau-theta)
kp = (2*alfa + theta)/(2*k*(alfa-lambda-theta))
ki = kp*(alfa + (theta/2))
kd = (kp*alfa*theta)/(2*alfa + theta)
s=tf('s');
G=.8*exp(-theta*s)/s
C=pid(kp,ki,kd,0.01);
step(feedback(G*C,1))
```

The results of the LiveScript

```
k = 800
tau = 1000
theta = 0.0200
lambda = 0.5000
alfa = 0.5200
kp = 64.9516
ki = 34.4250
kd = 0.6373
G =
                 0.8
  exp(-0.02*s) * ---
                  5
Continuous-time transfer function.
```

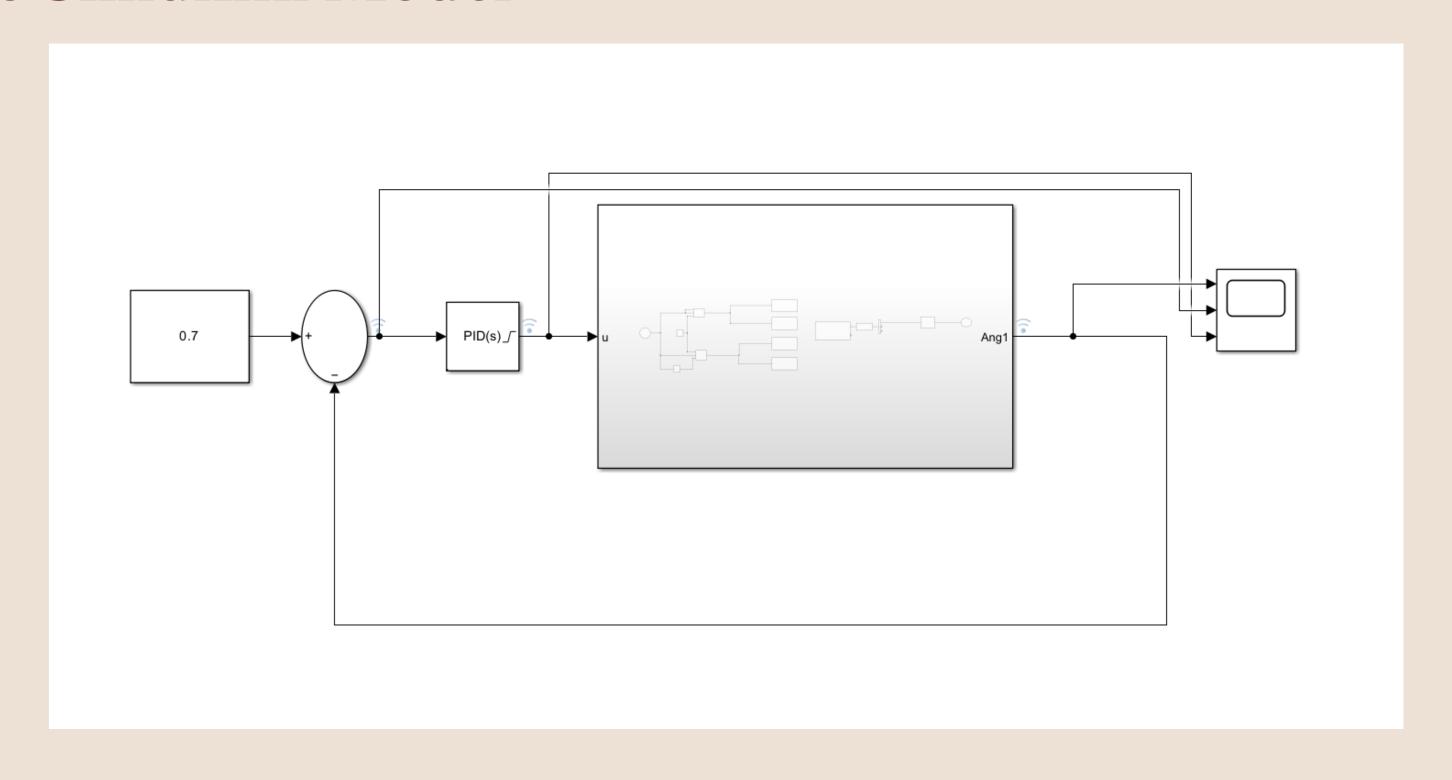


For various values of λ , the PID gains are found. These values are used to design the PID controller.

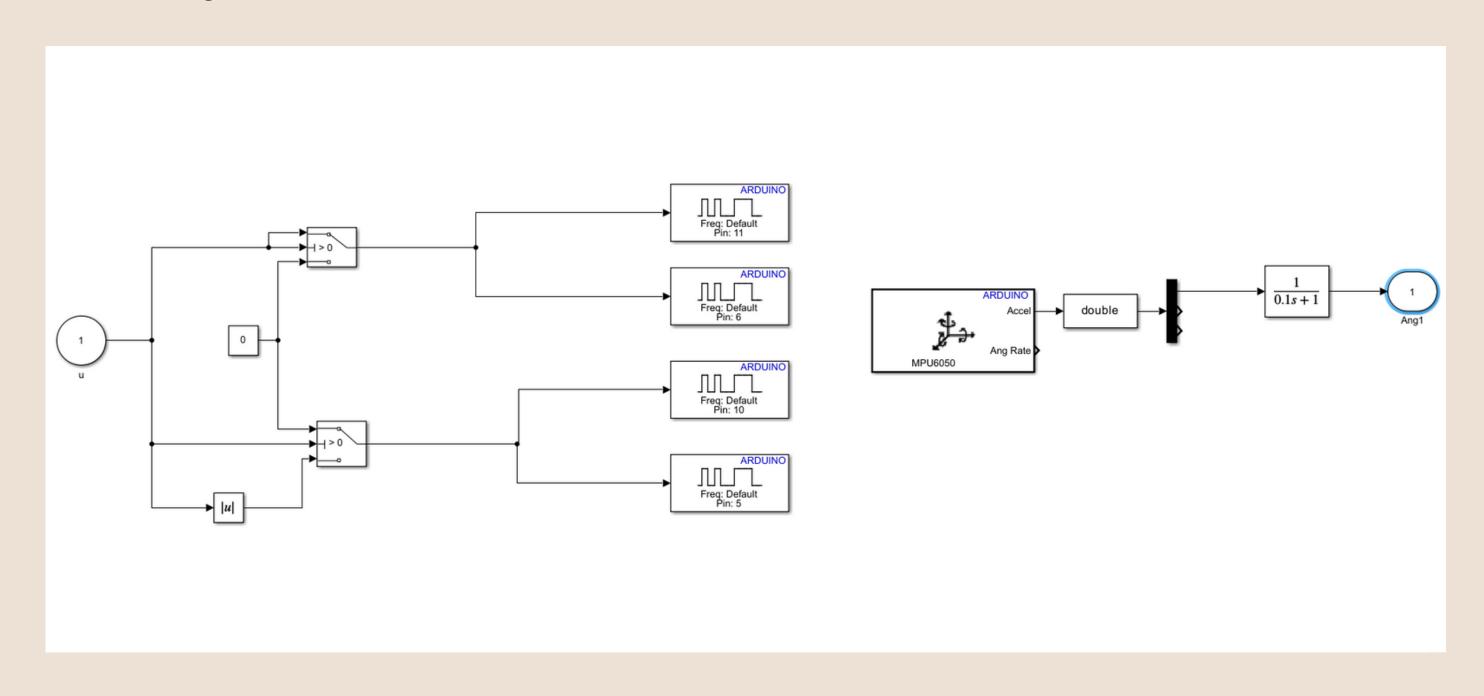
Lambda Values	Kp	Ki	Kd
0.2	104.8828	22.5520	0.5122
0.7	101.4234	72.5249	0.5036
1	101.0000	102.5251	0.5025
2	100.5037	202.5352	0.5013
4	100.2547	402.5627	0.5006

TABLE 3.1: PID values for various lambda

The Simulink Model

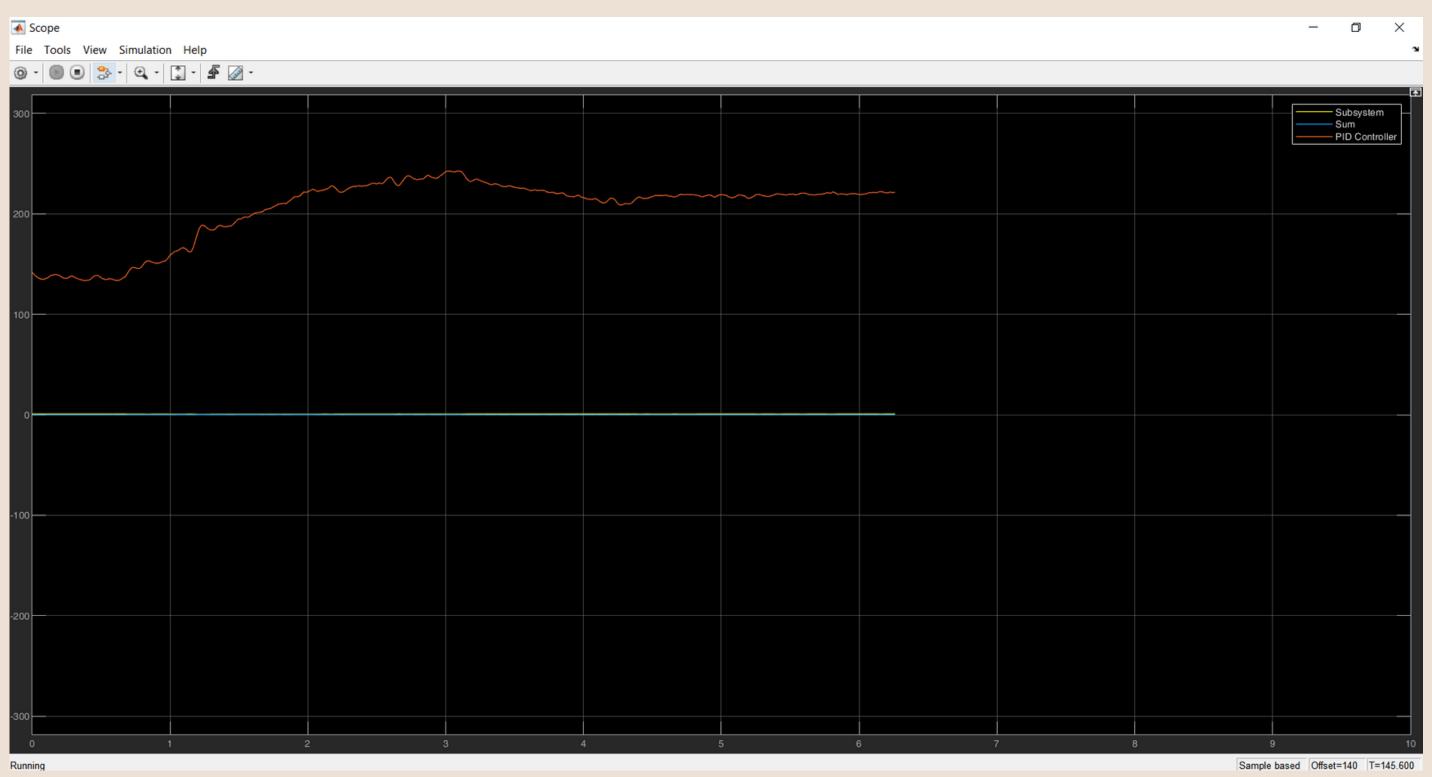


The Subsystem



IV RESULTS

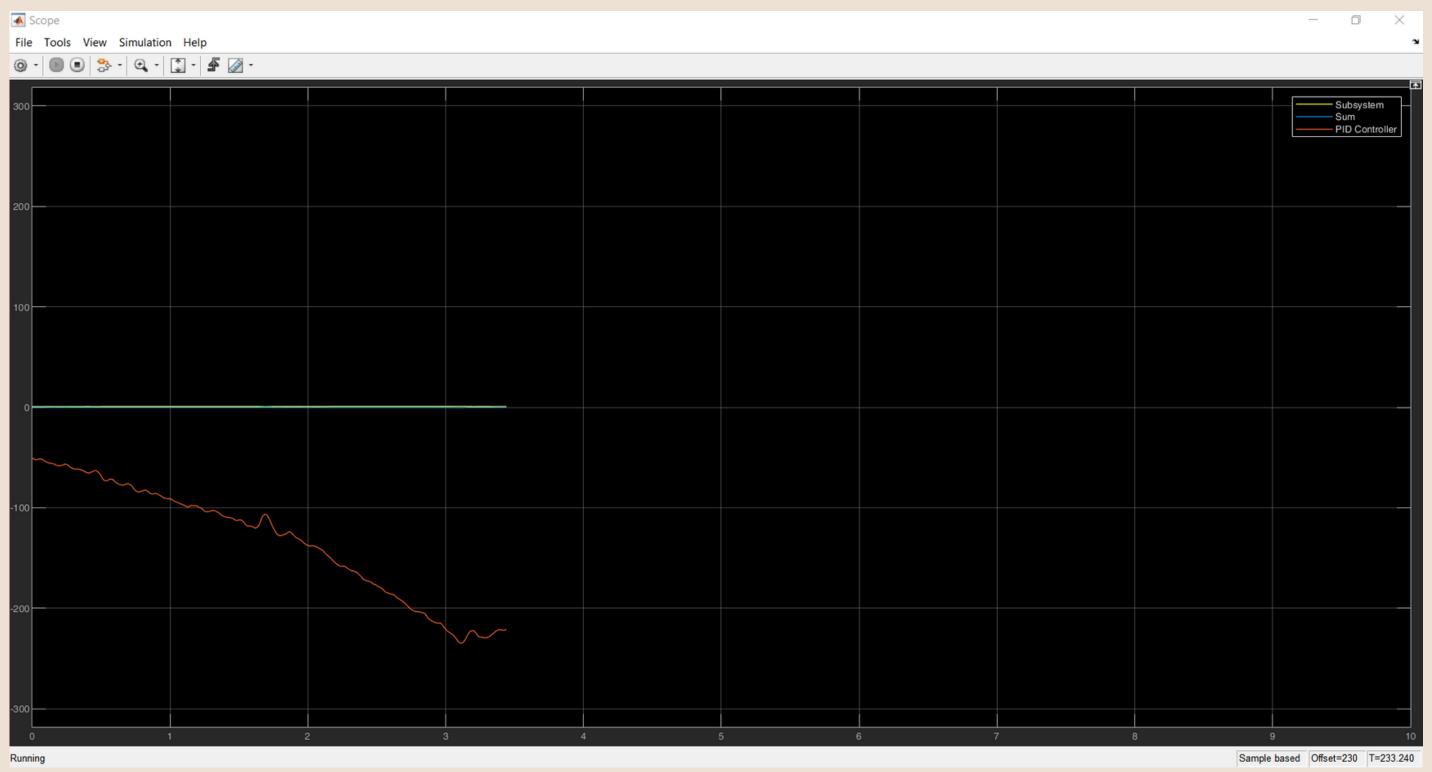
The following graph shows the control action depending on the values of the gyroscope:



When the model falls forward

IV RESULTS

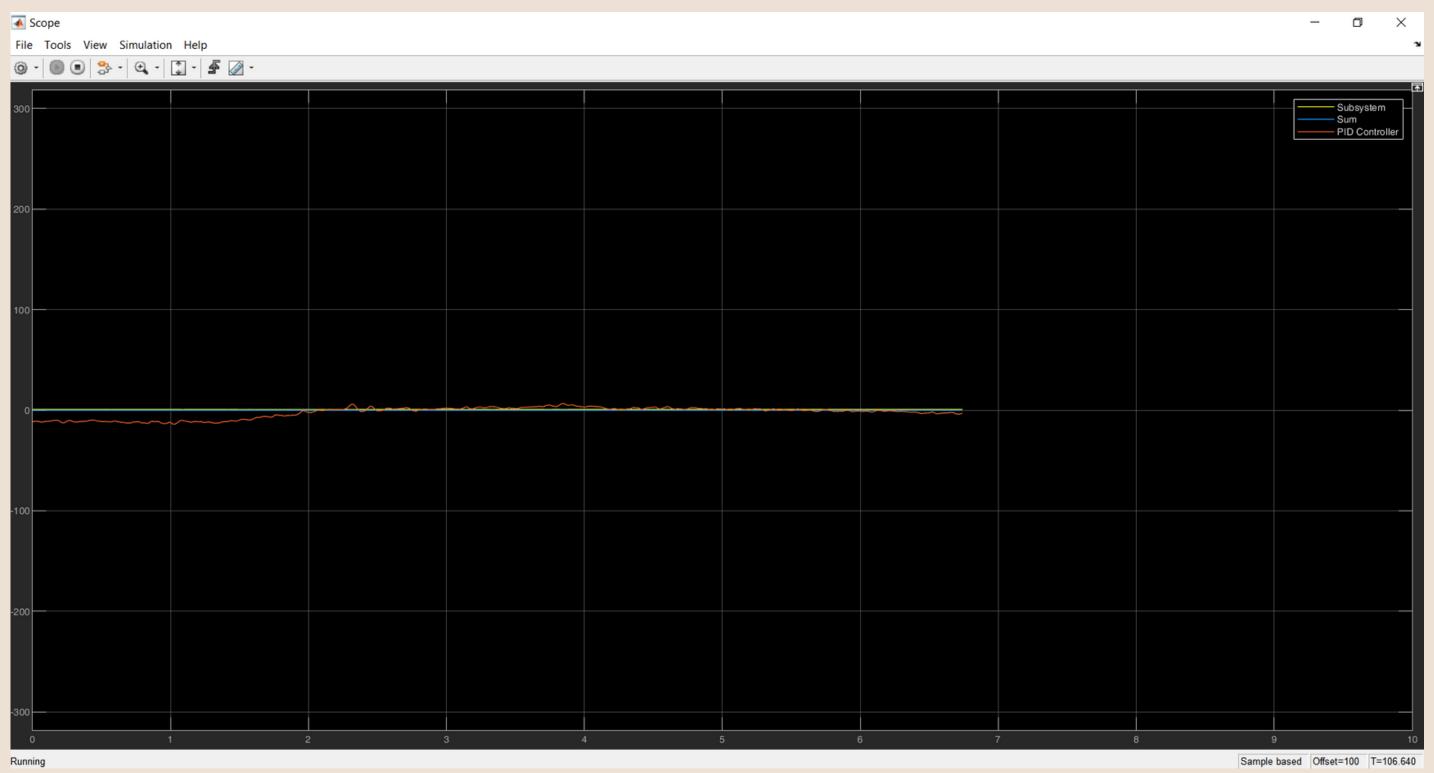
The following graph shows the control action depending on the values of the gyroscope:



When the model falls backward

IV RESULTS

The following graph shows the control action depending on the values of the gyroscope:



When the model is at equilibrium position

Conclusion:

• We were able to design the PID controller that provides the required control action to drive the motors which should balance the motors.

Future Work Required:

- Further Tuning of the PID controller for smoother working of the model and removal of the jerking action.
- Using Model Reference Adaptive Control to make the system adjust the controller in real-time.
- Adjust the chassis so that the centre of mass falls at the centre of the body.
- Adding an algorithm that stops the motor when the model gets in an irrecoverable state.
- Adding a LiPo Battery Source to provide a stable power supply to the model.



Thank you!

Supervisor

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