

- Angles are sometimes  $\theta_1, \theta_2$  or  $\phi_1, \phi_2$  in various text books.

Let us consider three tasks

- T1: Given an arbitrary trajectory of the end effector (given  $(x, y)$  as a fn of time), make the robot follow the trajectory.
- T2: Given a location on a wall, make the robot touch the wall at that location and apply a pre-specified (constant) force at that location.
- T3: Make the robot behave like a virtual spring connected from  $E$  to a given pt.  $(x_0, y_0)$ .

Now,

$$x = l_1 \cos q_1 + l_2 \cos q_2$$

$$y = l_1 \sin q_1 + l_2 \sin q_2$$

OR

$$\begin{aligned} x &= l_1 c q_1 + l_2 c q_2 \\ y &= l_1 s q_1 + l_2 s q_2 \end{aligned} \quad \text{--- (1)}$$

Differentiating (1), we get

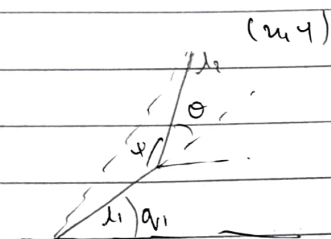
$$\dot{x} = -l_1 s q_1 \cdot \dot{q}_1 - l_2 s q_2 \dot{q}_2$$

$$\dot{y} = l_1 c q_1 \cdot \dot{q}_1 + l_2 c q_2 \dot{q}_2$$

$$\text{End effector velocity} = \begin{bmatrix} \dot{x} \\ \dot{y} \end{bmatrix} = \begin{bmatrix} -l_1 s q_1 & -l_2 s q_2 \\ l_1 c q_1 & l_2 c q_2 \end{bmatrix} \begin{bmatrix} \dot{q}_1 \\ \dot{q}_2 \end{bmatrix} \quad \text{--- (2)}$$

We will really need the ~~re~~ inverse relationship, Given  $n, y$  we need to be able to find  $q_1, q_2$ .

- Option 1: Solve numerically.
- Option 2: Derive a closed-form expression.
  - Hard in general.
  - Multiple solutions.

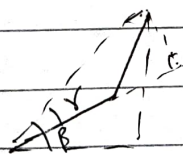


$$n^2 + y^2 = l_1^2 + l_2^2 + 2l_1l_2 \cos \theta \quad \left( \text{Using cosine rule + switching to acute angle.} \right)$$

$$\theta = \cos^{-1} \left( \frac{n^2 + y^2 - l_1^2 - l_2^2}{2l_1l_2} \right)$$

$$q_1 = \beta - \gamma = \tan^{-1} \left( \frac{y}{x} \right) - \tan^{-1} \left( \frac{l_2 \sin \theta}{l_1 + l_2 \cos \theta} \right)$$

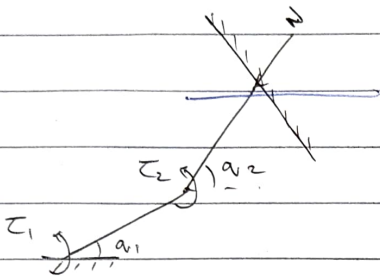
$$q_2 = q_1 + \theta.$$



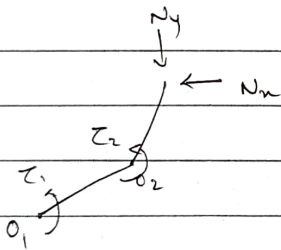
This is first level answer to  $T_1$ .

- We will later start using the notation  $u_d$  and  $y_d$ .  
(and  $q_d$  &  $\dot{q}_d$ ) here for desired values.  
(they are not necessarily actual values).

## Task 2:



FBD of entire robot.



Forces applied by the manipulator.

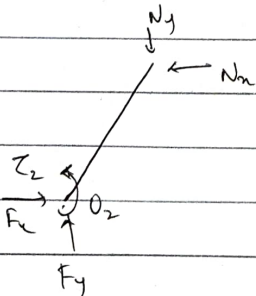
$$F_x = -N_x$$

$$F_y = -N_y$$

Neglect gravity.

Static eqbm.

FBD of each link separately.

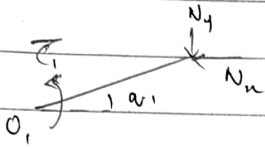


$$\sum M_{O_2} = 0$$

$$\Rightarrow \text{C.C.W is +ve}$$

$$+ N_y l_2 \cos q_2 - N_x l_2 \sin q_2 = + \tau_2$$

FBD of link 1



$$\left. \begin{aligned} N_y l_1 c q_1 - N_x l_1 s q_1 &= \tau_1 \\ N_y l_2 c q_2 - N_x l_2 s q_2 &= \tau_2 \end{aligned} \right\} \text{--- (2)}$$

$$\begin{bmatrix} \tau_1 \\ \tau_2 \end{bmatrix} = \begin{bmatrix} l_1 s q_1 & l_1 c q_1 \\ -l_2 s q_2 & l_2 c q_2 \end{bmatrix} \begin{bmatrix} N_x \\ N_y \end{bmatrix}$$

③ along with ④ solves  $\tau_2$ .

$\tau_3$  and next level answer to  $\tau_1$ :

Need to understand dynamics.

Lagrange's Equation.

Lagrangian

$$L = K - V$$

$K$  = kinetic energy

$V$  = potential energy.

$$\left[ \frac{d}{dt} \left( \frac{\partial L}{\partial \dot{q}_i} \right) - \frac{\partial L}{\partial q_i} = Q_i' \right] \quad (5)$$

$Q_i'$  are generalised forces derived using principle of virtual work.

$$K = \underbrace{\frac{1}{2} \left( \frac{1}{3} m_1 l_1^2 \right) \dot{q}_1^2}_{\text{pure rotation of } L_1} + \underbrace{\frac{1}{2} \left( \frac{1}{12} m_2 l_2^2 \right) \dot{q}_2^2 + \frac{1}{2} m_2 v_C^2}_{\text{pure rotation of } L_2}$$

$$\text{where, } v_C^2 = (l_1 \dot{q}_1)^2 + \left( \frac{l_2}{2} \dot{q}_2 \right)^2 + 2 l_1 \dot{q}_1 \frac{l_2}{2} \dot{q}_2 \cos(q_2 - q_1)$$

$$V = m_1 g \frac{l_1}{2} \sin q_1 + m_2 g \left( l_1 \sin q_1 + \frac{l_2}{2} \sin q_2 \right).$$

$$\frac{1}{3} m_1 l_1^2 \ddot{q}_1 + m_2 l_1^2 \ddot{q}_1 + \frac{m_2 l_1 l_2}{2} \ddot{q}_2 \cos(q_2 - q_1) - \frac{m_2 l_1 l_2}{2} \dot{q}_1 (\dot{q}_2 - \dot{q}_1) \sin(q_2 - q_1)$$

$$\sin(q_2 - q_1) + m_1 g \frac{l_1}{2} \cos q_1 + m_2 g l_1 \cos q_1 = \tau_1 \quad (i)$$

$$\frac{1}{3} m_2 l_2^2 \ddot{q}_2 + m_2 \frac{l_2^2}{4} \ddot{q}_2 + \frac{m_2 l_1 l_2}{2} \ddot{q}_1 \cos(q_2 - q_1) - \frac{m_2 l_1 l_2}{2} \dot{q}_1 (\dot{q}_2 - \dot{q}_1) \sin(q_2 - q_1)$$

$$\sin(q_2 - q_1) + m_2 g \frac{l_2}{2} \cos q_2 = \tau_2$$

Same this, need take.



Next, we note that (4) is valid for any forces  $F_x, F_y$  at end effector. (not just wall forces).

want,

$$\begin{aligned} F_x &= k_x \\ F_y &= k_y \end{aligned} = \begin{bmatrix} F_x = k_x (x - x_0) \\ F_y = k_y (y - y_0) \end{bmatrix}$$

from (1),

$$\begin{aligned} F_x &= k (l_1 c q_1 + l_2 c q_2) \\ F_y &= k (l_1 s q_1 + l_2 s q_2) \end{aligned}$$

from (4)

$$\Rightarrow \bullet k (l_1 s q_1 + l_2 s q_2) l_2 c q_2 - k (l_1 c q_1 + l_2 c q_2) l_2 s q_2 = \tau_{2s}$$

$$\bullet k (l_1 s q_1 + l_2 s q_2) l_1 c q_1 - k (l_1 c q_1 + l_2 c q_2) l_1 s q_1 = \tau_{1s}$$

# Set motor torques to be  $\tau_1 + \tau_{1s}$  and  $\tau_2 + \tau_{2s}$ , respectively!  
Answer to T3.

• Another way to handle  $T_1$ , is to solve for  $q_1^d$  &  $q_2^d$  from (3)

$$\begin{aligned} &\Downarrow \\ &q_1^d, q_1^{\dot{d}}, q_1^{\ddot{d}}, q_2^d, q_2^{\dot{d}}, q_2^{\ddot{d}} \\ &\downarrow \end{aligned}$$

$\tau_1, \tau_2$  from (6).

- work better when dynamic effects are significant.
- Still need feedback control.