

# **TRNSYS Type 835**

**PV model for the coupling with solar thermal absorber  
and collector models as PVT model**

## **Documentation**

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This model is based on work of Manuel Lämmle, Axel Oliva, Michael Hermann, Korbinian Kramer and Wolfgang Kramer, published in Lämmle et al. 2017.

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## Disclaimer

The developers refuse to accept any liability for direct or indirect damages of any kind that may result from the use of this simulation model and its implementation in computer code.

## Nomenclature

$A_{PV}$	gross area of PV modules or PVT collector [ $m^2$ ]
$a$	model parameter a for irradiance dependence of PV efficiency calculation [ $m^2/W$ ]
$b$	model parameter b for irradiance dependence of PV efficiency calculation [-]
$b_0$	constant for incident angle modifier IAM [-]
$c$	model parameter c for irradiance dependence of PV efficiency calculation [-]
$G$	solar irradiance in PV or PVT plane [ $W/m^2$ ]
$P_{el}$	electrical power output of the PV modules or PVT collector [W]
$p_{el}$	specific electrical power output of the PV modules or PVT collector [ $W/m^2$ ]
$PR_G$	performance ratio due to loss effects of irradiance [-]
$PR_{IAM}$	performance ratio due to loss effects of incidence angle [-]
$PR_T$	performance ratio due to PV cell temperature dependence [-]
$PR_{tot}$	overall performance ratio [-]
$\dot{q}_{th}$	specific thermal power output of the PVT collector [ $W/m^2$ ]
$T_{amb}$	ambient air temperature [ $^{\circ}C$ ]
$T_{cell}$	temperature of PV or PVT cells [ $^{\circ}C$ ]
$T_{cell,ref}$	PV cell temperature at reference conditions (usually STC conditions) [ $^{\circ}C$ ]
$T_m$	mean fluid temperature of the PVT collector [ $^{\circ}C$ ]
$U_0$	coefficient for radiation dependence of PV module temperature [ $W/m^2K$ ]
$U_1$	coefficient for wind dependence of PV module temperature [ $Ws/m^3K$ ]
$U_{cell-fl}$	internal heat transfer coefficient [ $W/m^2K$ ]
$U_L$	heat loss coefficient of the PV module [ $W/m^2K$ ]
$u$	wind speed in the PV plane [m/s]
$\beta$	power temperature coefficient of the PV cells [%/K]
$\eta_{el}$	overall electrical efficiency of the PV modules or PVT collector, gross area [-]
$\eta_{el,ref}$	electrical efficiency at reference conditions (usually STC) of the PV modules or PVT collector, gross area [-]
$\theta$	incidence angle of beam radiation [ $^{\circ}$ ]
$\tau\alpha$	effective transmittance-absorptance product [-]

# 1 Overview

The main idea behind this model is to develop a PV performance model in TRNSYS, which can be coupled to existing models of solar thermal collectors or absorbers for the calculation of the electrical power output of WISC and covered PVT collectors (see Fig. 1). It is especially developed for the connection with thermal models which are based on the quasi-dynamic model of ISO 9806:2013 (ISO 9806, 2013) or ISO 9806:2017 (ISO 9806, 2017), e.g. TRNSYS Type 832 (Haller et al., 2013). As the electrical mode of operation has a significant impact on the thermal efficiency, the thermal performance coefficients for the thermal power output calculation of the PVT collector should be determined in MPP mode (Lämmle et al., 2017).

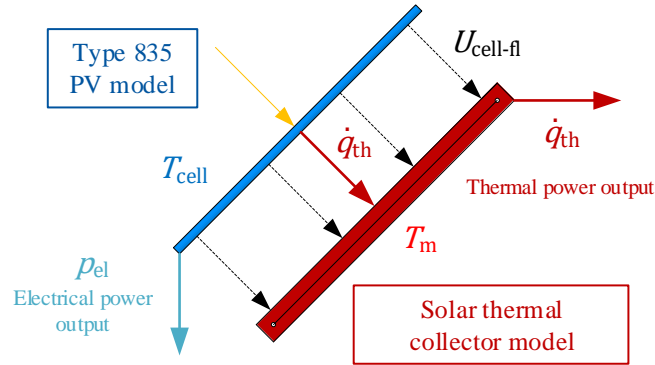


Fig. 1. Coupled PVT-model

As addition, the model includes a PV mode to simulate PV modules based on the same performance model, e.g. for a comparison of the electrical yield of a PV module and PVT collectors using identical PV cells. The major difference between the calculation of PV modules and PVT collectors in this approach results from the cell temperatures, which are determined by the fluid temperature in PVT collectors and by a steady-state module temperature in PV modules.

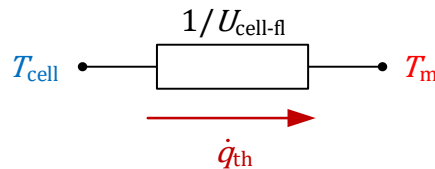


Fig. 2. Thermal network

In case of PVT collectors, the PVT cell temperature  $T_{cell}$  is calculated via an equivalent thermal network with an internal heat transfer coefficient  $U_{cell-fl}$ , which connects the PVT cell temperature with the mean fluid temperature  $T_m$  of the PVT collector (see Fig. 2), according to the electrical performance model of Lämmle et al. (2017). In case of PV modules, the PV cell temperature is calculated by the Faiman model (Faiman, 2008) or from NOCT conditions. For details see mathematical description.

## 2 Parameter, Inputs and Outputs

### Parameter

Nr.	Short	Description	Unit
1	PVTmode	mode for PVT or PV calculation 1: PVT - connection to solar thermal fluid temperature 2: PV - stand-alone calculation 3: PVT - cell temperature as input value	-
2	PVmode	mode for the irradiance dependence calculation of the PV efficiency 1: Calculation in MPP according to Heydenreich et al. 2: not defined	-
3	PVcellmode	mode for PV cell temperature calculation of stand-alone PV (only for PVT mode 2) 1: Faiman model 2: NOCT model (constant heat loss coefficient) 3: NOCT model (wind speed dependent heat loss coefficient)	-
4	Area	Area of the PVT collectors or PV modules (gross area)	m <sup>2</sup>
5	Eta_ref	electrical efficiency at reference conditions (gross area)	-
6	b0	constant for IAM	-
7	beta	temperature coefficient of solar cell efficiency	%/K
8	Tcell_ref	PV Cell temperature at reference conditions	C
9	a	model parameter a for PV efficiency (PV mode: 1)	m <sup>2</sup> /W
10	b	model parameter b for PV efficiency (PV mode: 1)	-
11	c	model parameter c for PV efficiency (PV mode: 1)	-
7	Ucellfl	internal heat transfer coefficient connecting cell and fluid temperature (PVT mode: 1)	W/m <sup>2</sup> K
12	U0	coefficient for module temperature (radiation) (PVT mode: 2, PV cell mode 1)	W/m <sup>2</sup> K
13	U1	coefficient for module temperature (wind) (PVT mode: 2, PV cell mode 1)	Ws/m <sup>3</sup> K
14	Tcell_NOCT	PV Cell temperature at NOCT conditions (PVT mode: 2, PV cell mode 2 and 3)	C
15	Tamb_NOCT	ambient temperature at NOCT conditions (PVT mode: 2, PV cell mode 2 and 3)	C
16	It_NOCT	Global radiation on PV plane at NOCT conditions (PVT mode: 2, PV cell mode 2 and 3)	W/m <sup>2</sup>
17	Taualpha	effective transmittance-absorptance product (PVT mode: 2, PV cell mode 2 and 3)	[-]

## Inputs

Nr.	Short	Description	Unit
1	It	Global radiation on PV plane	kJ/hm <sup>2</sup>
2	Theta	Incidence angle of beam radiation	degrees
3	Tm	mean fluid temperature of the PVT collector	C
4	qth	specific thermal power output of the PVT collector	kJ/hm <sup>2</sup>
5	u	wind speed in the PV plane	m/s
6	Tamb	ambient air temperature	C
t	Tcell_in	temperature of the PV cell (only for PVT mode 3)	C

## Outputs

Nr.	Short	Description	Unit
1	Pel	Electric power output	kJ/h
2	Tcell	temperature of the PV cell	C
3	EtaPV	total efficiency of PV modules (gross area)	-

### 3 Mathematical description

The PV model Type 835 can be used for the simulation of:

- 1) the electrical part of PVT collectors by coupling the PV model with models of solar thermal absorbers or collectors (PVT collector simulation, PVT mode 1 or 3), or
- 2) stand-alone PV systems (PVT mode 2).

#### Overall electrical efficiency and electrical power output

The overall (or total) electrical efficiency  $\eta_{el}$  is calculated with:

$$\eta_{el} = \eta_{el,ref} \cdot PR_{tot} \quad (\text{Eq. 1})$$

The electrical power output of the PV modules or PVT collector  $P_{el}$  is given by:

$$P_{el} = \eta_{el,ref} \cdot PR_{tot} \cdot G \cdot A_{PV} \quad (\text{Eq. 2})$$

and as specific electrical power output by (Lämmle et al., 2017):

$$p_{el} = \eta_{el,ref} \cdot PR_{tot} \cdot G \quad (\text{Eq. 3})$$

where  $\eta_{el,ref}$  is the electrical efficiency at reference conditions (usually STC conditions),  $PR_{tot}$  is the overall instantaneous performance ratio,  $G$  the global radiation on PV or PVT plane and  $A_{PV}$  the PV or PVT area.

The overall instantaneous performance ratio is calculated with (Lämmle et al., 2017):

$$PR_{tot} = PR_{IAM} \cdot PR_T \cdot PR_G \quad (\text{Eq. 4})$$

The electrical performance model for PV takes into account the following loss effects (performance ratios  $PR$ ):

- loss effects of incidence angle  $PR_{IAM}$
- loss effects of irradiance  $PR_G$  and
- PV cell temperature dependence of electrical efficiency  $PR_T$ .

The major difference between the calculation of PV modules as stand-alone PV system and PVT collector is given by the cell temperatures, which are determined by the fluid temperature in PVT collectors (PVT mode 1) and by the steady-state module temperature in PV modules (PVT mode 2) or set as input value from external calculation (PVT mode 3).

#### Loss effects of incidence angle

The instantaneous performance ratio due to incidence angle losses  $PR_{IAM}$  is calculated with (Duffie and Beckman, 2013):

$$PR_{IAM} = 1 - b_0 \cdot (1/\cos(\theta) - 1) \quad (\text{Eq. 5})$$

where  $b_0$  is the constant for IAM and  $\theta$  the incidence angle of beam radiation.

Tab. 1. Typical values for  $b_0$  of PV modules

Parameter	Type	Value	Reference
$b_0$	PV	0.07	Lämmle et al., 2017

### Loss effects of irradiance

The instantaneous performance ratio due to irradiance losses  $PR_G$  is calculated with (Heydenreich et al., 2008):

$$PR_G = a \cdot G + b \cdot \ln(G + 1) + c \cdot \left[ (\ln(G + e))^2 / (G + 1) - 1 \right] \quad (\text{Eq. 6})$$

with the model parameters  $a$  in  $\text{m}^2/\text{W}$ ,  $b$  and  $c$  dimensionless, the global irradiance  $G$  in  $\text{W}/\text{m}^2$  and the Euler's number  $e$ .

Tab. 2. Typical values for the parameters  $a$ ,  $b$  and  $c$  of PV modules

Parameter	Type	Value	Reference
$a$	Crystalline (c-Si)	-0.0000109 $\text{m}^2/\text{W}$	Lämmle et al., 2017
$b$	Crystalline (c-Si)	-0.047	Lämmle et al., 2017
$c$	Crystalline (c-Si)	-1.40	Lämmle et al., 2017

### PV cell temperature dependence of the electrical efficiency

The PV cell temperature dependence of the electrical efficiency is calculated with (Skoplaki and Palyvos, 2009):

$$PR_T = 1 - \beta \cdot (T_{\text{cell}} - T_{\text{cell,ref}}) \quad (\text{Eq. 7})$$

where  $\beta$  is the power temperature coefficient of the PV cells,  $T_{\text{cell}}$  the temperature of the PV cells and  $T_{\text{cell,ref}}$  the PV cell temperature at reference conditions (usually STC conditions).

Tab. 3. Typical values for the power temperature coefficient  $\beta$  of PV modules

Parameter	Type	Value	Reference
$\beta$	PV modules	0.43 %/K	Lämmle et al., 2017
$\beta$	Average from literature	0.45 %/K	Skoplaki and Palyvos, 2009
$\beta$	Average of Sandia and commercial cells	0.38 %/K (0.32-0.46 %/K)	Skoplaki and Palyvos, 2009
$\beta$	Monocrystalline (Mono-Si)	0.30-0.50 %/K	Skoplaki and Palyvos, 2009
$\beta$	Polycrystalline (Poly-Si)	0.40 %/K	Skoplaki and Palyvos, 2009
$\beta$	Amorphous (a-Si)	0.11-0.26 %/K	Skoplaki and Palyvos, 2009

### PV cell temperature

As described before, the main difference between the calculation of PV modules as stand-alone PV system and PVT collectors is given by the calculation of the PV cell temperatures.

In case of PVT collectors (PVT mode 1), the PVT cell temperature is calculated with a simple equivalent thermal network with an internal heat transfer coefficient  $U_{\text{cell-fl}}$ , which connects the PVT cell temperature  $T_{\text{cell}}$  with the mean fluid temperature  $T_m$  of the PVT collector. In this case, the PVT cell temperature is given by (Lämmle et al., 2016, 2017):

$$T_{\text{cell}} = T_m + \dot{q}_{\text{th}} / U_{\text{cell-fl}} \quad (\text{Eq. 8})$$

where  $\dot{q}_{\text{th}}$  is the specific thermal power output of the PVT collector.

In case of PV modules as stand-alone PV system (PVT mode 2), the PV cell/module temperature can be calculated with different models. In PV cell mode 1, the PV cell/module temperature is calculated with (Faiman, 2008):



$$T_{\text{cell}} = T_{\text{amb}} + G / (U_0 + U_1 \cdot u) \quad (\text{Eq. 9})$$

where  $T_{\text{amb}}$  is the ambient air temperature,  $U_0$  the coefficient for radiation dependence of PV module temperature,  $U_1$  the coefficient for wind dependence of PV module temperature and  $u$  the wind speed in the PV plane. At this, the PV cell temperature is assumed to be equal to the module temperature.

Tab. 4. Typical values for  $U_0$  and  $U_1$  of PV modules

Parameter	Type	Value	Reference
$U_0$	Crystalline (c-Si)	30.02 W/m <sup>2</sup> K	Koehl et al., 2011
$U_1$	Crystalline (c-Si)	6.28 Ws/m <sup>3</sup> K	Koehl et al., 2011
$U_0$	Crystalline (c-Si), combined fit	25.00 W/m <sup>2</sup> K (23.5-26.4 W/m <sup>2</sup> K)	Faiman, 2008
$U_1$	Crystalline (c-Si), combined fit	6.84 Ws/m <sup>3</sup> K (6.25-7.68 Ws/m <sup>3</sup> K)	Faiman, 2008
$U_0$	Amorphous (a-Si)	25.26-26.16 W/m <sup>2</sup> K	Koehl et al., 2011
$U_1$	Amorphous (a-Si)	4.25-10.67 Ws/m <sup>3</sup> K	Koehl et al., 2011

In PV cell mode 2 and 3, the PV cell temperature is calculated from NOCT conditions. The energy balance of a PV module per unit area can be written as (Duffie and Beckman, 2013):

$$(\tau\alpha) \cdot G = \eta_{\text{el}} \cdot G + U_L \cdot (T_{\text{cell}} - T_{\text{amb}}) \quad (\text{Eq. 10})$$

where  $\tau\alpha$  is the effective transmittance-absorptance product (usually estimate with 0.9 or 0.95) and  $U_L$  the heat loss coefficient of the PV module.

With Eq. 10 the PV temperature difference to the ambient is given by:

$$T_{\text{cell}} - T_{\text{amb}} = G \cdot (\tau\alpha) / U_L - G \cdot \eta_{\text{el}} / U_L \quad (\text{Eq. 11})$$

or

$$T_{\text{cell}} - T_{\text{amb}} = G \cdot (\tau\alpha) / U_L (1 - \eta_{\text{el}} / (\tau\alpha)) \quad (\text{Eq. 12})$$

For NOCT conditions ( $G_{\text{NOCT}} = 800 \text{ W/m}^2$ ,  $T_{\text{amb,NOCT}} = 20^\circ\text{C}$ ,  $u_{\text{NOCT}} = 1 \text{ m/s}$ ) with no-load operation ( $\eta_{\text{el}} = 0$ ), the energy balance of Eq. 12 is given by:

$$T_{\text{cell,NOCT}} - T_{\text{amb,NOCT}} = G_{\text{NOCT}} \cdot (\tau\alpha) / U_{L,\text{NOCT}} \quad (\text{Eq. 13})$$

The PV cell temperature at any ambient temperature and global radiation is than found from:

$$(T_{\text{cell}} - T_{\text{amb}}) / (T_{\text{cell,NOCT}} - T_{\text{amb,NOCT}}) = (G / G_{\text{NOCT}}) (U_{L,\text{NOCT}} / U_L) [1 - (\eta_{\text{el}} / \tau\alpha)] \quad (\text{Eq. 14})$$

or:

$$T_{\text{cell}} = T_{\text{amb}} + (G / G_{\text{NOCT}}) (U_{L,\text{NOCT}} / U_L) (T_{\text{cell,NOCT}} - T_{\text{amb,NOCT}}) [1 - (\eta_{\text{el}} / \tau\alpha)] \quad (\text{Eq. 15})$$

With the assumption that the heat loss coefficient (PV cell mode 2) is constant, the PV cell temperature can be calculated from Eq. 15 with:

$$T_{\text{cell}} = T_{\text{amb}} + (G / G_{\text{NOCT}}) (T_{\text{cell,NOCT}} - T_{\text{amb,NOCT}}) [1 - (\eta_{\text{el}} / \tau\alpha)] \quad (\text{Eq. 16})$$

An approximation of  $U_L$  for variable wind speeds is (Duffie and Beckman, 2013):

$$U_L = 5.7 \text{ W/m}^2\text{K} + 3.8 \text{ Ws/m}^3\text{K} \cdot u \quad (\text{Eq. 17})$$

With the approximation in Eq. 17, the wind speed at NOCT  $u_{\text{NOCT}} = 1 \text{ m/s}$  and Eq. 15, the PV cell temperature for variable wind speeds (PV cell mode 3) can be calculated with:

$$T_{\text{cell}} = T_{\text{amb}} + \frac{G}{G_{\text{NOCT}}} \cdot \frac{9.5 \text{ W/m}^2\text{K}}{5.7 \text{ W/m}^2\text{K} + 3.8 \text{ W/m}^3\text{K} \cdot u} (T_{\text{cell,NOCT}} - T_{\text{amb,NOCT}}) \left[ 1 - \frac{\eta_{\text{el}}}{\tau\alpha} \right] \quad (\text{Eq. 18})$$

In addition, in PVT mode 3, the PVT cell temperature can set as input value from external calculation.

### Detailed calculation of PV cell temperature in PV cell mode 2 and 3

In PV cell mode 2 and 3, the calculation of the PV cell temperature depends on the actual overall (or total) electrical efficiency  $\eta_{\text{el}}$  of the PV modules. As  $\eta_{\text{el}}$  depends on the actual PV cell temperature, Eq. 1 has to be used in Eq. 16 / Eq. 18 and the equations has to solve for the PV cell temperature  $T_{\text{cell}}$ .

With Eq. 4 and Eq. 7, Eq. 1 can be written for PV modules as:

$$\eta_{\text{el}} = \eta_{\text{el,ref}} \cdot PR_{\text{IAM}} \cdot PR_{\text{G}} \cdot [1 - \beta \cdot (T_{\text{cell}} - T_{\text{cell,ref}})] \quad (\text{Eq. 19})$$

For simplification of the following calculations, the variable  $k_1$  is introduced as:

$$k_1 = \eta_{\text{el,ref}} \cdot PR_{\text{IAM}} \cdot PR_{\text{G}} \quad (\text{Eq. 20})$$

In addition, the variable  $k_2$ , which depends on the PV cell mode (PV cell mode 2 or 3), is defined as:

$$k_2 = (G/G_{\text{NOCT}}) (T_{\text{cell,NOCT}} - T_{\text{amb,NOCT}}) \quad (\text{Eq. 21})$$

for PV cell mode 2 and

$$k_2 = \frac{G}{G_{\text{NOCT}}} \cdot \frac{9.5 \text{ W/m}^2\text{K}}{5.7 \text{ W/m}^2\text{K} + 3.8 \text{ W/m}^3\text{K} \cdot u} (T_{\text{cell,NOCT}} - T_{\text{amb,NOCT}}) \quad (\text{Eq. 22})$$

for PV cell mode 3.

With Eq. 19 – 22, Eq. 16/18 can be written as:

$$T_{\text{cell}} = T_{\text{amb}} + k_2 [1 - (k_1/\tau\alpha \cdot [1 - \beta \cdot (T_{\text{cell}} - T_{\text{cell,ref}})])] \quad (\text{Eq. 23})$$

Solving Eq. 23 for  $T_{\text{cell,PV}}$ :

$$T_{\text{cell}} = T_{\text{amb}} + k_2 \left[ 1 - \frac{k_1}{\tau\alpha} + \frac{k_1}{\tau\alpha} \cdot \beta \cdot (T_{\text{cell}} - T_{\text{cell,ref}}) \right] \quad (\text{Eq. 24})$$

$$T_{\text{cell}} = T_{\text{amb}} + k_2 - \frac{k_1 k_2}{\tau\alpha} + \frac{k_1 k_2}{\tau\alpha} \cdot \beta \cdot (T_{\text{cell}} - T_{\text{cell,ref}}) \quad (\text{Eq. 25})$$

$$T_{\text{cell}} = T_{\text{amb}} + k_2 - \frac{k_1 k_2}{\tau\alpha} + \frac{k_1 k_2}{\tau\alpha} \cdot \beta \cdot T_{\text{cell}} - \frac{k_1 k_2}{\tau\alpha} \cdot \beta \cdot T_{\text{cell,ref}} \quad (\text{Eq. 26})$$

$$T_{\text{cell}} - \frac{k_1 k_2}{\tau\alpha} \cdot \beta \cdot T_{\text{cell}} = T_{\text{amb}} + k_2 \left[ 1 - \frac{k_1}{\tau\alpha} - \frac{k_1}{\tau\alpha} \cdot \beta \cdot T_{\text{cell,ref}} \right] \quad (\text{Eq. 27})$$

$$T_{\text{cell}} \cdot \left( 1 - \frac{k_1 k_2}{\tau\alpha} \cdot \beta \right) = T_{\text{amb}} + k_2 \left[ 1 - \frac{k_1}{\tau\alpha} (1 + \beta \cdot T_{\text{cell,ref}}) \right] \quad (\text{Eq. 28})$$

the PV cell temperature can be calculated with:

$$T_{\text{cell}} = \frac{T_{\text{amb}} + k_2 [1 - k_1/\tau\alpha \cdot (1 + \beta \cdot T_{\text{cell,ref}})]}{1 - k_1 \cdot k_2 \cdot \beta / \tau\alpha} \quad (\text{Eq. 29})$$

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## Appendix: Changelog

- Version 2.0: NOCT calculation for the PV cell temperature was added (with fixed electrical efficiency)
- Version 3.0: NOCT calculation for the PV cell temperature was added with detailed calculation and use of actual electrical efficiency
- Version 3.1: Correct Calculation for Theta (Calculation in radians ( $\ast \pi / 180$ ) from input degree values and maximum as well as zero value of  $PR_{iam}$  for negative  $PR_{iam}$ 's)
- Version 3.2: Corrections in the documentation. Nomenclature "Tcell-fl" corrected in Proforma. Zero value of  $PR_g$  for negative irradiance.
- Version 3.3: zero value of  $PR_{iam}$  if the incidence angle is lower / greater than the possible acceptance angle ( $0^\circ - 90^\circ$ ) and additional parameter and input checking
- Version 3.4: Corrections in the documentation (Thermal Network).