

材料力学

第六章 强度理论





复杂应力状态下失效

最大拉应力理论(断裂)

最大拉应变理论(断裂)

最大切应力理论(屈服)

畸变能理论 (屈服)

强度理论



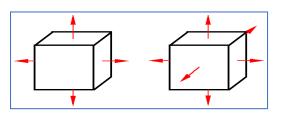
单向应力与纯剪切

T

$$\sigma_{\max} \leq \frac{\sigma_{\mathrm{u}}}{n} \quad \tau_{\max} \leq \frac{\tau_{\mathrm{u}}}{n}$$

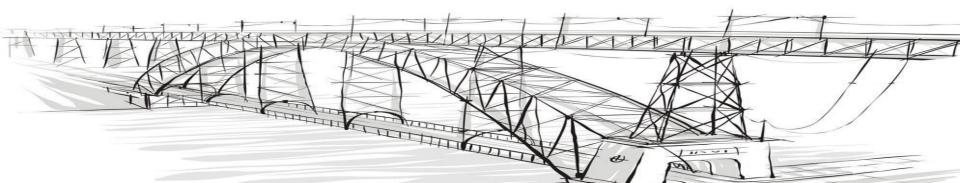
 $\sigma_{\rm u}$, $\tau_{\rm u}$ 由试验测定

一般复杂应力状态



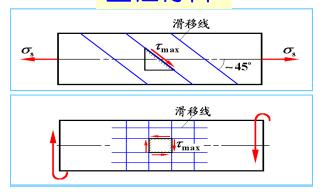
每种比值情况下的极 限应力,很难全由试 验测定

本节研究: 材料在静态复杂应力状态下的破坏或失效的规律, 及其在构件强度分析中的应用

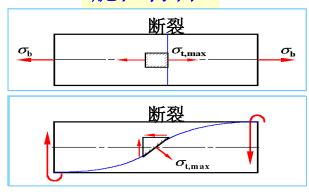


破坏形式与原图?

塑性材料



脆性材料





- ① 屈服或滑移一可能是τ_{max} 过大所引起
- 2 断裂一可能是 $\sigma_{t,max}$ 或 $\varepsilon_{t,max}$ 过大所引起

强度理论: 关于材料在静态复杂应力状态下破坏或失效规律的学说或假说



□ 最大拉应力理论 (第一强度理论)

理论要点

- ullet 引起材料断裂的主要因素一最大拉应力 $\sigma_{\!\scriptscriptstyle ullet}$
- 不论材料处于何种应力状态,只要最大拉应 力σ,达到材料单向拉伸断裂时的最大拉应力 σ_{III} (即 σ_{b}),材料即发生断裂

$$\sigma_1 = \sigma_b$$
 -材料的断裂条件

强度条件

$$\sigma_1 \leq \frac{\sigma_b}{n}$$

$$\sigma_1 \leq [\sigma]$$

$$\sigma_1 \le \frac{\sigma_b}{n}$$
 $\sigma_1 \le [\sigma]$ $[\sigma] = \frac{\sigma_b}{n}$



- $\sigma_{\rm I}$ 一构件危险点处的最大拉应力
- $[\sigma]$ 材料单向拉伸时的许用应力

最大拉应变理论 (第二强度理论)

理论要点

- ullet 引起材料断裂的主要因素一最大拉应变 $oldsymbol{arepsilon}_{oldsymbol{\iota}}$
- 不论材料处于何种应力状态,当 $\boldsymbol{\varepsilon}_1 = \boldsymbol{\varepsilon}_{1\mathrm{u}, \hat{+}\hat{\Sigma}}$ 时,材料断裂。 单向拉伸断裂时:

$$\boldsymbol{\varepsilon}_1 = \frac{1}{E} \left[\boldsymbol{\sigma}_1 - \mu (\boldsymbol{\sigma}_2 + \boldsymbol{\sigma}_3) \right]$$

 $\sigma_1 = \sigma_b \quad \sigma_2 = \sigma_3 = 0$

故
$$\boldsymbol{\varepsilon}_{1\mathrm{u}, \text{\text{\pm}}} = \frac{\boldsymbol{\sigma}_{\mathrm{b}}}{E}$$

$$\boldsymbol{\sigma}_{1} - \boldsymbol{\mu}(\boldsymbol{\sigma}_{2} + \boldsymbol{\sigma}_{3}) = \boldsymbol{\sigma}_{\mathrm{b}} - \text{材料的断裂条件}$$

强度条件

$$|\sigma_1 - \mu(\sigma_2 + \sigma_3) \leq [\sigma]$$

 $\sigma_1, \sigma_2, \sigma_3$ 一 构件危险点处的工作应力

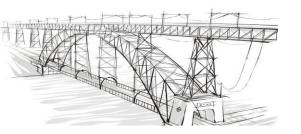
 $[\sigma]=\sigma/n$ 一 材料单向拉伸时的许用应力

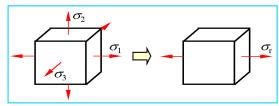
$$\sigma_{r,2} = \sigma_1 - \mu(\sigma_2 + \sigma_3)$$

 $\sigma_{\rm r}$ – 相当应力或折算应力

$$\sigma_{\mathrm{r},2} \leq [\sigma]$$

 $\sigma_{r,2} \leq [\sigma]$ $\sigma_{r,2}$ 第二强度理论的相当应力





在促使材料破坏或失效方面, 与复杂应力状态应力等效的单 向应力

□ 最大切应力理论 (第三强度理论)

理论要点

- ullet 引起材料屈服的主要因素一最大切应力 au_{max}
- 不论材料处于何种应力状态,当 $au_{max} = au_{s, mux}$ 时,材料屈服。

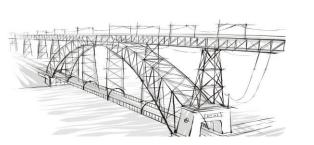
$$\tau_{\text{max}} = \frac{\sigma_1 - \sigma_3}{2}$$

$$\tau_{\text{s}, \text{\text{$\psi}$} \text{\text{$\psi}}} = \frac{\sigma_{\text{s}} - \mathbf{0}}{2} = \frac{\sigma_{\text{s}}}{2}$$

$$\sigma_1 - \sigma_3 = \sigma_s$$
 -材料的屈服条件

强度条件

$$\sigma_{\mathrm{r},3} = \sigma_1 - \sigma_3 \leq [\sigma]$$



 σ_1 , σ_3 一 构件危险点处的工作应力

 $[\sigma]$ 一材料单向拉伸时的许用应力

□ 畸变能理论 (第四强度理论)

畸变能强度理论要点

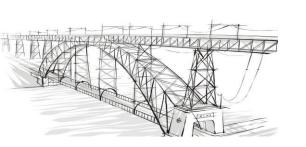
- \bullet 引起材料屈服的主要因素一畸变能,其密度为 v_d
- 不论材料处于何种应力状态,当 $v_{\mathbf{d}} = v_{\mathbf{ds}, \hat{\mu} \pm \hat{\nu}}$ 时,材料屈服

$$v_{\rm d} = \frac{1+\mu}{6E} \left[(\sigma_1 - \sigma_2)^2 + (\sigma_2 - \sigma_3)^2 + (\sigma_3 - \sigma_1)^2 \right] \quad v_{\rm ds, \not\equiv \dot{z}} = \frac{1+\mu}{3E} \sigma_{\rm s}^2$$

$$\frac{1}{\sqrt{2}}\sqrt{(\sigma_1-\sigma_2)^2+(\sigma_2-\sigma_3)^2+(\sigma_3-\sigma_1)^2}=\sigma_s$$
 -屈服条件

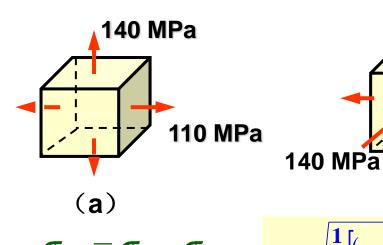
强度条件

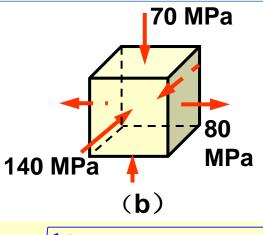
$$\sigma_{r4} = \frac{1}{\sqrt{2}} \sqrt{\left(\sigma_1 - \sigma_2\right)^2 + \left(\sigma_2 - \sigma_3\right)^2 + \left(\sigma_3 - \sigma_1\right)^2} \le \left[\sigma\right]$$

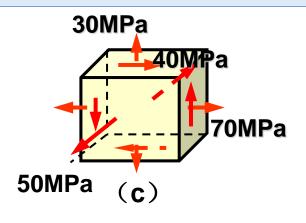


 $\sigma_1, \sigma_2, \sigma_3$ 一 构件危险点处的工作应力 $[\sigma]$ 一 材料单向拉伸时的许用应力

对于图示各单元体,试分别按第三强度理论及第四强度理论求相当应力.







$$\sigma_{\rm r3} = \sigma_1 - \sigma_3$$

$$oldsymbol{\sigma}_{\mathrm{r}3} = oldsymbol{\sigma}_{1} - oldsymbol{\sigma}_{3} \qquad eta_{\mathrm{r}4} = \sqrt{rac{1}{2} ig[(\sigma_{1} - \sigma_{2})^{2} + (\sigma_{2} - \sigma_{3})^{2} + (\sigma_{3} - \sigma_{1})^{2} ig]}$$

(1) 单元体 (a)

$$\sigma_1 = 140 \text{MPa}$$
 $\sigma_2 = 110 \text{MPa}$ $\sigma_3 = 0$

$$\sigma_{r3} = \sigma_1 - \sigma_3 = 140 \text{MPa}$$

$$\sigma_{r4} = \sqrt{\frac{1}{2}[30^2 + 110^2 + (-140)^2]} = 128 \text{MPa}$$

(2) 单元体(b)

$$\sigma_1$$
 = 80MPa σ_2 = -70MPa σ_3 = -140MPa
$$\sigma_{r3}$$
 = 220MPa σ_{r4} = 195MPa

(3) 单元体(c)

$$\frac{\sigma_{\text{max}}}{\sigma_{\text{min}}} = \frac{70 + 30}{2} + \sqrt{\left(\frac{70 - 30}{2}\right)^2 + 40^2} = \frac{94.72}{5.28}$$

$$\sigma_1 = 94.72 \text{MPa}$$
 $\sigma_2 = \sigma_z = 50 \text{MPa}$ $\sigma_3 = 5.28 \text{MPa}$

$$\sigma_{\rm r3} = 89.44 \rm MPa$$

$$\sigma_{\rm r4} = 77.5 {\rm MPa}$$

□ 强度理论的选用

● 一般情况

脆性材料:抵抗断裂的能力 < 抵抗滑移的能力

塑性材料:抵抗滑移的能力 < 抵抗断裂的能力

第一与第二强度理论,一般适用于脆性材料

第三与第四强度理论,一般适用于塑性材料

● 全面考虑

材料的失效形式,不仅与材料性质有关,而且与应力状态形式、 温度与加载速率等有关

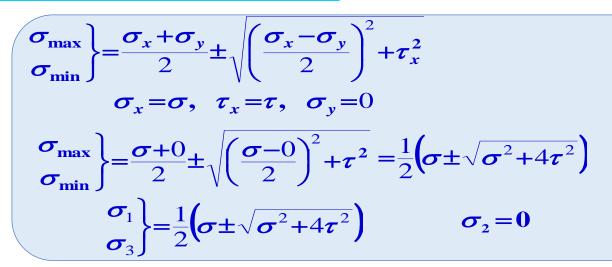
低碳钢, 三向等拉, $\tau_{\text{max}} = (\sigma_1 - \sigma_3)/2 = 0$ 低碳钢, 低温断裂

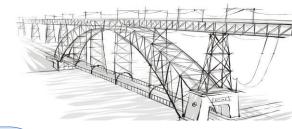
. 断裂

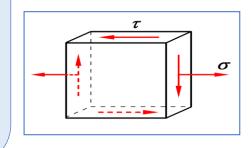


□ 一种常见应力状态的强度条件

单向、纯剪切联合作用







塑性材料:
$$\sigma_{r3} = \sqrt{\sigma^2 + 4\tau^2} \leq [\sigma]$$

$$\sigma_{\rm r4} = \sqrt{\sigma^2 + 3\tau^2} \leq [\sigma]$$

□ 纯剪切许用应力

纯剪切情况下($\sigma = 0$)

$$\sigma_{r3} = 2\tau \leq [\sigma]$$

$$\tau \leq \frac{[\sigma]}{2}$$

$$[\tau] = \frac{[\sigma]}{2}$$

塑性材料:

$$\sigma_{r4} = \sqrt{3}\tau \leq [\sigma]$$

$$\tau \leq \frac{[\sigma]}{\sqrt{3}}$$

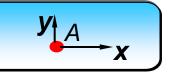
$$[\tau] = \frac{[\sigma]}{\sqrt{3}}$$

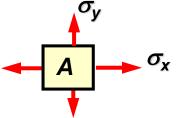
$$[\tau] = (0.5 \sim 0.577)[\sigma]$$

$$\sigma_{r3} = \sigma_1 - \sigma_3 \le [\sigma]$$

例题14 薄壁圆筒受最大内压时,测得 ε_x =1.88×10⁻⁴, ε_y =7.37×10⁻⁴,已知钢的 E=210GPa,[σ]=170MPa,泊松比 μ =0.3,试用第三强度理论校核其**强度**.

$$\sigma_x = \frac{pD}{4\delta}$$





 $\sigma_{\rm t} = \frac{pD}{2\delta}$

解:由广义胡克定律

$$\sigma_{x} = \frac{E}{1 - \mu^{2}} (\varepsilon_{x} + \mu \varepsilon_{y}) = \frac{2.1}{1 - 0.3^{2}} (1.88 + 0.3 \times 7.37) \times 10^{7} = 94.4 \text{MPa}$$

$$\sigma_{y} = \frac{E}{1 - \mu^{2}} (\varepsilon_{y} + \mu \varepsilon_{x}) = \frac{2.1}{1 - 0.3^{2}} (7.37 + 0.3 \times 1.88) \times 10^{7} = 183.1 \text{MPa}$$

$$\stackrel{\stackrel{\cdot}{=}}{=} \stackrel{\cdot}{=} \stackrel{\cdot}{=} \frac{1}{1 - 0.3^{2}} (7.37 + 0.3 \times 1.88) \times 10^{7} = 183.1 \text{MPa}$$

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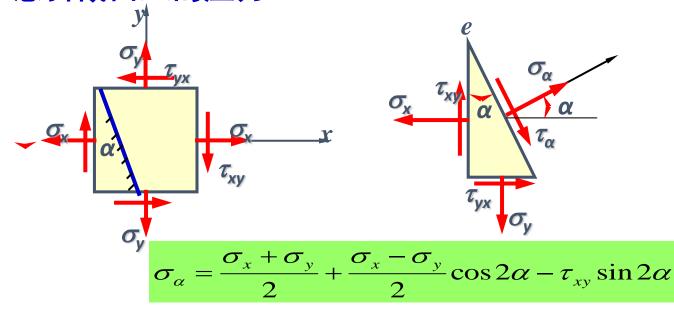
不安全





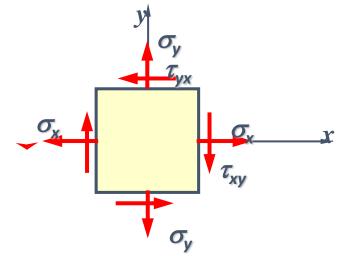
1任意斜截面上的应力:





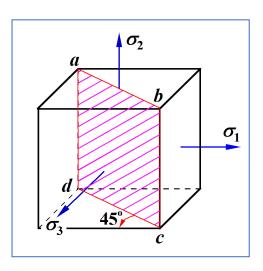
$$\tau_{\alpha} = \frac{\sigma_{x} - \sigma_{y}}{2} \sin 2\alpha + \tau_{xy} \cos 2\alpha$$

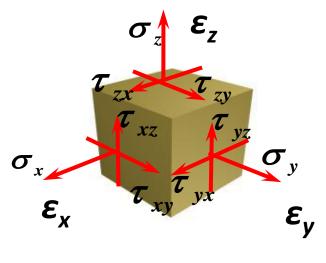
2 主应力、主平面:



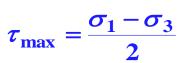
$$\sigma_{\max_{\min}} = \frac{\sigma_x + \sigma_y}{2} \pm \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2}$$

$$\tan 2\alpha_0 = -\frac{2\tau_{xy}}{\sigma_x - \sigma_y} \qquad \alpha_0 \quad \alpha_0 + 90^0$$





3. 最大切应力



最大切应力截面位置:

与 σ_2 所在平面垂直 与 σ_1 及 σ_3 所在平面均成45°

4. 广义胡克定律

$$\varepsilon_{x} = \frac{1}{E} \left[\sigma_{x} - \mu (\sigma_{y} + \sigma_{z}) \right]$$

$$\varepsilon_{y} = \frac{1}{E} \left[\sigma_{y} - \mu (\sigma_{x} + \sigma_{z}) \right]$$

$$\varepsilon_{z} = \frac{1}{E} \left[\sigma_{z} - \mu (\sigma_{x} + \sigma_{y}) \right]$$

$$\gamma_{xy} = \frac{\tau_{xy}}{G}$$
 $\gamma_{xz} = \frac{\tau_{xz}}{G}$ $\gamma_{yz} = \frac{\tau_{yz}}{G}$

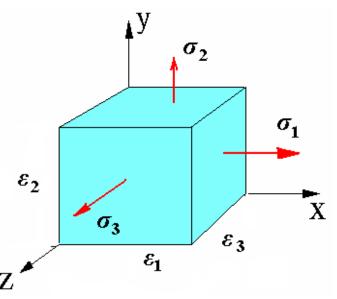


$$\varepsilon_1 = \frac{1}{E} \left[\sigma_1 - \mu (\sigma_2 + \sigma_3) \right]$$

$$\varepsilon_2 = \frac{1}{E} \left[\sigma_2 - \mu (\sigma_1 + \sigma_3) \right]$$

$$\varepsilon_3 = \frac{1}{E} \left[\sigma_3 - \mu (\sigma_1 + \sigma_2) \right]$$

一广义胡克定律



5. 强度理论

$$\sigma_{
m r} \leq [\sigma]$$
 $\sigma_{
m r}$ - 相当应力或折算应力

$$\sigma_{r,1} = \sigma_1$$

$$\sigma_{\mathrm{r},2} \equiv \sigma_{\mathrm{l}} - \mu(\sigma_{2} + \sigma_{3})$$

$$\sigma_{r,3} = \sigma_1 - \sigma_3$$

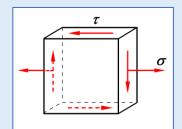
$$\sigma_{r4} = \frac{1}{\sqrt{2}} \sqrt{(\sigma_1 - \sigma_2)^2 + (\sigma_2 - \sigma_3)^2 + (\sigma_3 - \sigma_1)^2}$$

第一与第二强度理论,一般适用于脆性材料第三与第四强度理论,一般适用于塑性材料

6.一种常见应力状态的强度条件

单向、纯剪切联合作用

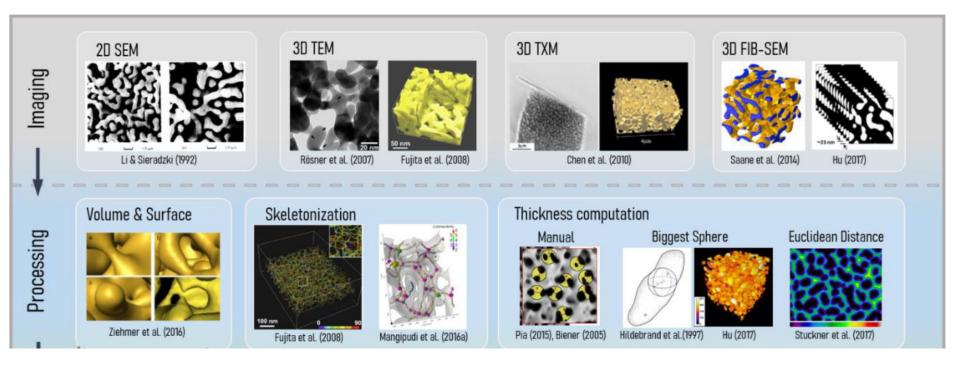
塑性材料:



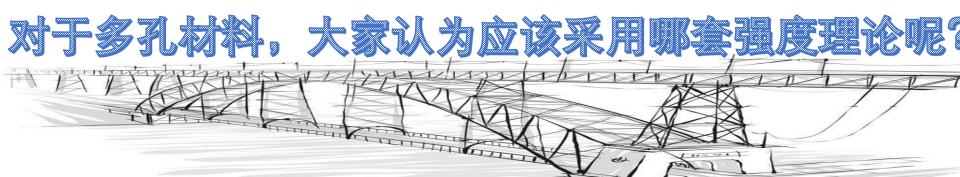
$$\sigma_{r3} = \sqrt{\sigma^2 + 4\tau^2} \leq [\sigma]$$

$$\sigma_{r4} = \sqrt{\sigma^2 + 3\tau^2} \le [\sigma]$$

纳米多孔金属微机械模型



Claudia Richert, Norbert Huber. A Review of Experimentally Informed Micromechanical Modeling of Nanoporous Metals: From Structural Descriptors to Predictive Structure—Property Relationships[J]. Materials 2020, 13, 3307; doi:10.3390/ma13153307



谢谢大家!

