

## Teoria delle strutture - PROBLEMA 4

```
% serbatoio pieno d'acqua schematizzato come guscio sottile  
%% Clear workspace and close any open windows  
clear all  
close all
```

### SOLUZIONE PUNTO 1 & 2

% 1) Assumendo che il serbatoio possa essere schematizzato come un guscio sottile, scrivere l'equazione differenziale e le condizioni al bordo che permettono di determinare la soluzione di questo problema di equilibrio.

% 2) Determinare le espressioni dello spostamento trasversale e delle caratteristiche della sollecitazione (semplificare il problema relativamente al calcolo delle componenti flessionali della sollecitazione, assumendo nel calcolo che il guscio sia di lunghezza infinita).

#### simbolico

```
syms z A1 A2 E R nu t h gamma beta D real  
p=-gamma*(h-z) % Carico idrostatico  
  
p = -γ (h - z)
```

#### Variabili numeriche

```
R_n=1000; % raggio serbatoio [mm]  
E_n=210000; % Young's modulus steel [N/mm^2] se.. 2.1E11[N/m^2]  
nu_n=0.3; % coefficiente di Poisson acciaio  
t_n=R_n/50; %spessore serbatoio  
h_n=5*R_n; %altezza serbatoio  
gamma_n=0.000001; % acqua N/mm^3  
p_n=-gamma_n*(h_n-z); % Carico idrostatico  
D_n=(E_n*t_n^3)/(12*(1-nu_n^2)); % rigidezza  
beta_n=((E_n*t_n*R_n^2)/D_n)^(1/4);
```

#### Soluzione omogenea

```
wo=A1*exp(-(beta*z)/(R*sqrt(2)))*cos((beta*z)/(R*sqrt(2)))...  
+A2*exp(-(beta*z)/(R*sqrt(2)))*sin((beta*z)/(R*sqrt(2)))
```

$$w_0 = A_1 e^{-\frac{\sqrt{2}\beta z}{2R}} \cos\left(\frac{\sqrt{2}\beta z}{2R}\right) + A_2 e^{-\frac{\sqrt{2}\beta z}{2R}} \sin\left(\frac{\sqrt{2}\beta z}{2R}\right)$$

#### Soluzione particolare

```
wp=(p*R^2)/(E*t)
```

$$w_p = -\frac{R^2 \gamma (h - z)}{E t}$$

#### Soluzione

```
w(z)=wo+wp
```

$$w(z) =$$

$$A_1 e^{-\frac{\sqrt{2} \beta z}{2 R}} \cos\left(\frac{\sqrt{2} \beta z}{2 R}\right) + A_2 e^{-\frac{\sqrt{2} \beta z}{2 R}} \sin\left(\frac{\sqrt{2} \beta z}{2 R}\right) - \frac{R^2 \gamma (h-z)}{E t}$$

```
% Derivate
w_z(z)=diff(w,z) % derivata prima
```

$$w_z(z) = \frac{R^2 \gamma}{E t} - \frac{\sqrt{2} A_1 \beta e^{-\sigma_1} \cos(\sigma_1)}{2 R} + \frac{\sqrt{2} A_2 \beta e^{-\sigma_1} \cos(\sigma_1)}{2 R} - \frac{\sqrt{2} A_1 \beta e^{-\sigma_1} \sin(\sigma_1)}{2 R} - \frac{\sqrt{2} A_2 \beta e^{-\sigma_1} \sin(\sigma_1)}{2 R}$$

where

$$\sigma_1 = \frac{\sqrt{2} \beta z}{2 R}$$

**Applico le Condizioni al contorno:**

```
cc1=w(0)==0
```

$$cc1 = A_1 - \frac{R^2 \gamma h}{E t} = 0$$

```
cc2=w_z(0)==0
```

$$cc2 = \frac{\sqrt{2} A_2 \beta}{2 R} - \frac{\sqrt{2} A_1 \beta}{2 R} + \frac{R^2 \gamma}{E t} = 0$$

**risolvo il sistema per trovare A1 e A2**

```
S=solve([cc1 cc2],[A1 A2]);
A_1=S.A1(1)
```

$$A_1 = \frac{R^2 \gamma h}{E t}$$

```
A_2=simplify(S.A2(1))
```

$$A_2 = -\frac{R^2 \gamma (\sqrt{2} R - \beta h)}{E \beta t}$$

**spostamento**

```
w1(z)=simplify(subs(w,[A1 A2],[A_1 A_2]))
```

$$w1(z) = \frac{R^2 \gamma h e^{-\sigma_1} \cos(\sigma_1)}{E t} - \frac{R^2 \gamma (h-z)}{E t} - \frac{R^2 \gamma e^{-\sigma_1} \sin(\sigma_1) (\sqrt{2} R - \beta h)}{E \beta t}$$

where

$$\sigma_1 = \frac{\sqrt{2} \beta z}{2 R}$$

**soluzione numerica**

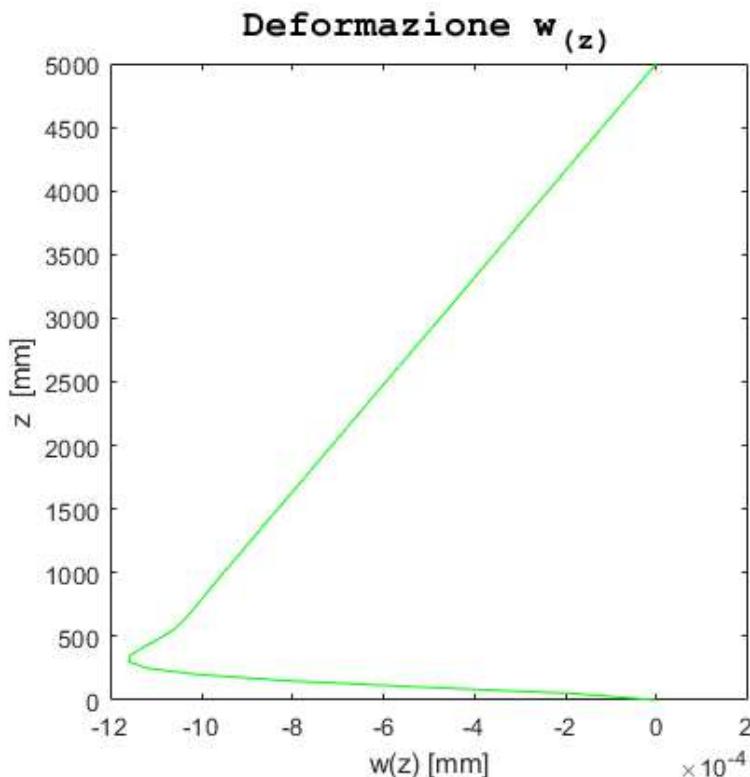
```
A_11=subs(A_1,[R gamma h E t],[R_n gamma_n h_n E_n t_n]);
```

```

A_22=subs(A_2,[R gamma h E t beta],[R_n gamma_n h_n E_n t_n beta_n]);
w_n(z)=A_11*exp(-(beta_n*z)/(R_n*sqrt(2)))*cos((beta_n*z)/(R_n*sqrt(2)))*...
+A_22*exp(-(beta_n*z)/(R_n*sqrt(2)))*sin((beta_n*z)/(R_n*sqrt(2)))*...
+(p_n*R_n^2)/(E_n*t_n);
wn_z(z)=diff(w_n,z); %derivata di w_n
wn_zz(z)=diff(wn_z,z); %derivata di wn_z

% Plot
%% Soluzione
a=0:h_n/(100-1):h_n;
figure(1)
plot(double(w_n(a)),a,'g')
title(['\fontname{Courier}\fontsize{15}Deformazione w_(z)'],'color','K');
ylabel('z [mm]');
xlabel('w(z) [mm]');
axis square

```

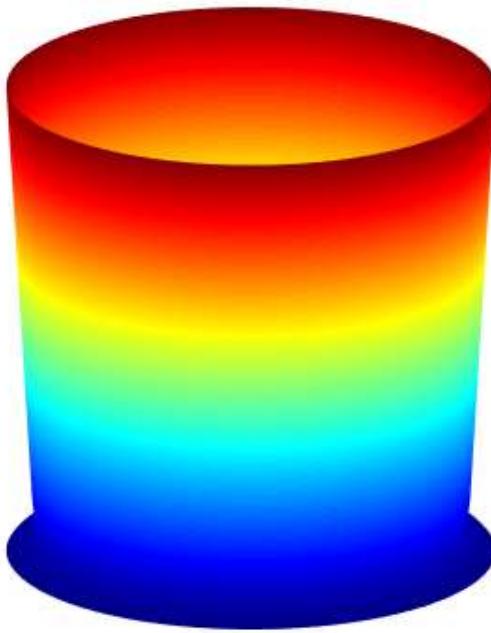


```

figure(2)
fig = gcf; % current figure handle
fig.Color = [1 1 1];
figToolBar = 'none';
colormap(jet(100))
c=100000; % coefficiente che amplifica la deformazione
w1_n=R_n+(double(w_n(a))*c);
[X,Y,Z]=cylinder(w1_n,100);
s1=surface(X,Y,Z,'FaceAlpha',1,'EdgeColor','k','LineWidth',0.01);
title(['\fontname{Courier}\fontsize{15}Deformazione3D w_(z) '],'color','K');
axis off
axis square
shading interp;
view([5.700 18.800])
rotate3d

```

### Deformazione3D w(z)

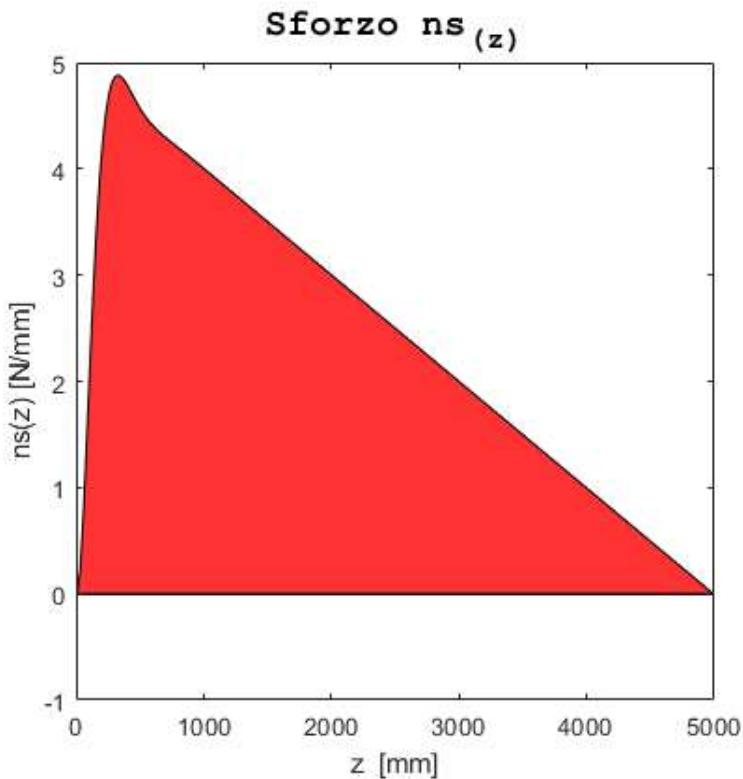


### Calcolo CDS

```
ns(z)=simplify(-w*E*t/R)
```

$$ns(z) = \frac{-Et \left( A_1 e^{-\frac{\sqrt{2}\beta z}{2R}} \cos\left(\frac{\sqrt{2}\beta z}{2R}\right) + A_2 e^{-\frac{\sqrt{2}\beta z}{2R}} \sin\left(\frac{\sqrt{2}\beta z}{2R}\right) - \frac{R^2 \gamma (h-z)}{Et} \right)}{R}$$

```
%% Plot the ns(z) stresses
a=0:h_n/(200-1):h_n;
figure(3)
area(a,double(-w_n(a)*E_n*t_n/R_n), 'FaceColor', 'r', 'Facealpha', 0.8)
title(['\fontname{Courier}\fontsize{15}Sforzo ns_(z)'], 'color', 'K');
xlabel('z [mm]');
ylabel('ns(z) [N/mm]');
axis square
```



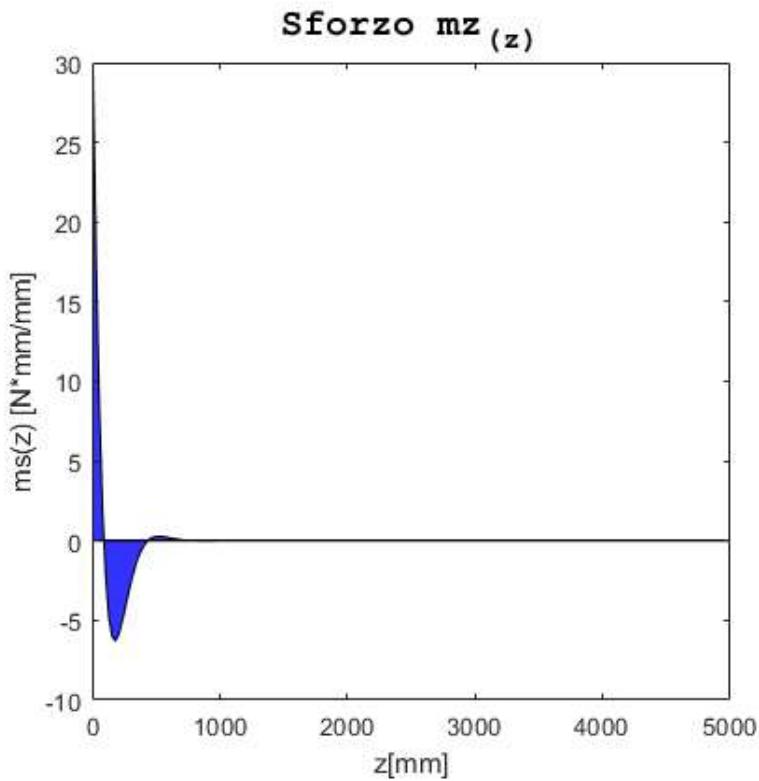
```
w_zz(z)=simplify(diff(w_z,z))
```

$$w_{zz}(z) = -\frac{\beta^2 e^{-\frac{\sqrt{2}\beta z}{2R}} \left( A_2 \cos\left(\frac{\sqrt{2}\beta z}{2R}\right) - A_1 \sin\left(\frac{\sqrt{2}\beta z}{2R}\right) \right)}{R^2}$$

```
mz(z)=simplify(-D*w_zz)
```

$$mz(z) = \frac{D \beta^2 e^{-\frac{\sqrt{2}\beta z}{2R}} \left( A_2 \cos\left(\frac{\sqrt{2}\beta z}{2R}\right) - A_1 \sin\left(\frac{\sqrt{2}\beta z}{2R}\right) \right)}{R^2}$$

```
% Plot the mz(z) stresses
figure(4)
mz_n(z)=(-wn_zz*D_n);
area(a,double(mz_n(a)), 'FaceColor', 'b', 'Facealpha', 0.8)
title(['\fontname{Courier}\fontsize{15}Sforzo mz_(z_)'], 'color', 'K');
xlabel('z[mm]');
ylabel('mz(z) [N*mm/mm]');
axis square
```



```
tz(z)=simplify(diff(mz))
```

$$tz(z) = -\frac{\sqrt{2} D \beta^3 e^{-\sigma_1} (A_1 \cos(\sigma_1) + A_2 \cos(\sigma_1) - A_1 \sin(\sigma_1) + A_2 \sin(\sigma_1))}{2 R^3}$$

where

$$\sigma_1 = \frac{\sqrt{2} \beta z}{2 R}$$

```
% Plot the ns(z) stresses
figure(5)
tz_n(z)=diff(mz_n);
area(a,double(tz_n(a)), 'FaceColor', 'g', 'Facealpha', 0.8)
title(['\fontname{Courier}\fontsize{15}Sforzo tz_(z_)'], 'color', 'K');
xlabel('z [mm]');
ylabel('tz(z) [N/mm]');
axis square
```

