

## Teoria delle strutture - PROBLEMA 4

```
% serbatoio pieno d'acqua schematizzato come guscio sottile
%% Clear workspace and close any open windows
clear all
close all
```

### SOLUZIONE PUNTO 1 & 2

```
% 1) Assumendo che il serbatoio possa essere schematizzato come un guscio sottile, scrivere
%l'equazione differenziale e le condizioni al bordo che permettono di determinare la soluzione
%di questo problema di equilibrio.

% 2) Determinare le espressioni dello spostamento trasversale e delle caratteristiche della
%sollecitazione (semplificare il problema relativamente al calcolo delle componenti flessionali
%della sollecitazione, assumendo nel calcolo che il guscio sia di lunghezza infinita).
```

### simbolico

```
syms z A1 A2 E R nu t h gamma beta D real
```

```
p=-gamma*(h-z) % Carico idrostatico
```

$$p = -\gamma (h - z)$$

### Variabili numeriche

```
R_n=1000; % raggio serbatoio [mm]
E_n=210000; % Young's modulus steel [N/mm^2] se.. 2.1E11[N/m^2]
nu_n=0.3; % coefficiente di Poisson acciaio
t_n=R_n/50; %spessore serbatoio
h_n=5*R_n; %altezza serbatoio
gamma_n=0.000001; % acqua N/mm3
p_n=-gamma_n*(h_n-z); % Carico idrostatico
D_n=(E_n*t_n^3)/(12*(1-nu_n^2)); % rigidezza
beta_n=((E_n*t_n*R_n^2)/D_n)^(1/4);
```

### Soluzione omogenea

```
w0=A1*exp(-(beta*z)/(R*sqrt(2)))*cos((beta*z)/(R*sqrt(2)))...
+A2*exp(-(beta*z)/(R*sqrt(2)))*sin((beta*z)/(R*sqrt(2)))
```

$$w_0 = A_1 e^{-\frac{\sqrt{2}\beta z}{2R}} \cos\left(\frac{\sqrt{2}\beta z}{2R}\right) + A_2 e^{-\frac{\sqrt{2}\beta z}{2R}} \sin\left(\frac{\sqrt{2}\beta z}{2R}\right)$$

### Soluzione particolare

```
w_p=(p*R^2)/(E*t)
```

$$w_p = -\frac{R^2 \gamma (h - z)}{E t}$$

### Soluzione

```
w(z)=w0+w_p
```

$$w(z) =$$

$$A_1 e^{-\frac{\sqrt{2}\beta z}{2R}} \cos\left(\frac{\sqrt{2}\beta z}{2R}\right) + A_2 e^{-\frac{\sqrt{2}\beta z}{2R}} \sin\left(\frac{\sqrt{2}\beta z}{2R}\right) - \frac{R^2 \gamma (h-z)}{E t}$$

% Derivate

w\_z(z)=diff(w,z) % derivata prima

w\_z(z) =

$$\frac{R^2 \gamma}{E t} - \frac{\sqrt{2} A_1 \beta e^{-\sigma_1} \cos(\sigma_1)}{2 R} + \frac{\sqrt{2} A_2 \beta e^{-\sigma_1} \cos(\sigma_1)}{2 R} - \frac{\sqrt{2} A_1 \beta e^{-\sigma_1} \sin(\sigma_1)}{2 R} - \frac{\sqrt{2} A_2 \beta e^{-\sigma_1} \sin(\sigma_1)}{2 R}$$

where

$$\sigma_1 = \frac{\sqrt{2} \beta z}{2 R}$$

**Applico le Condizioni al contorno:**

cc1=w(0)==0

cc1 =

$$A_1 - \frac{R^2 \gamma h}{E t} = 0$$

cc2=w\_z(0)==0

cc2 =

$$\frac{\sqrt{2} A_2 \beta}{2 R} - \frac{\sqrt{2} A_1 \beta}{2 R} + \frac{R^2 \gamma}{E t} = 0$$

**risolvo il sistema per trovare A1 e A2**

S=solve([cc1 cc2],[A1 A2]);

A\_1=S.A1(1)

A\_1 =

$$\frac{R^2 \gamma h}{E t}$$

A\_2=simplify(S.A2(1))

A\_2 =

$$-\frac{R^2 \gamma (\sqrt{2} R - \beta h)}{E \beta t}$$

**spostamento**

w1(z)=simplify(subs(w,[A1 A2],[A\_1 A\_2]))

w1(z) =

$$\frac{R^2 \gamma h e^{-\sigma_1} \cos(\sigma_1)}{E t} - \frac{R^2 \gamma (h-z)}{E t} - \frac{R^2 \gamma e^{-\sigma_1} \sin(\sigma_1) (\sqrt{2} R - \beta h)}{E \beta t}$$

where

$$\sigma_1 = \frac{\sqrt{2} \beta z}{2 R}$$

**soluzione numerica**

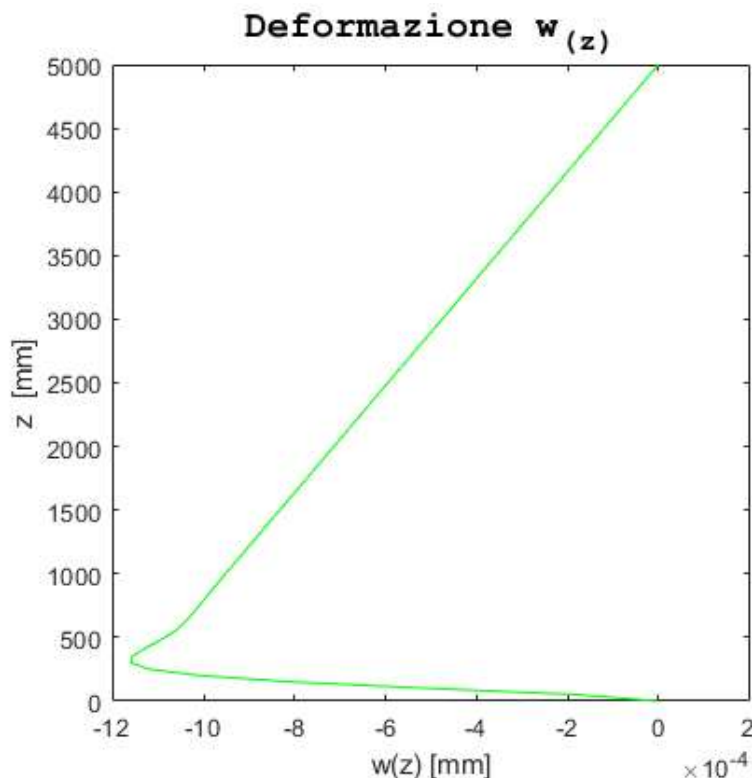
A\_11=subs(A\_1,[R gamma h E t],[R\_n gamma\_n h\_n E\_n t\_n]);

```

A_22=subs(A_2,[R gamma h E t beta],[R_n gamma_n h_n E_n t_n beta_n]);
w_n(z)=A_11*exp(-(beta_n*z)/(R_n*sqrt(2)))*cos((beta_n*z)/(R_n*sqrt(2)))+...
    +A_22*exp(-(beta_n*z)/(R_n*sqrt(2)))*sin((beta_n*z)/(R_n*sqrt(2)))+...
    +(p_n*R_n^2)/(E_n*t_n);
wn_z(z)=diff(w_n,z); %derivata di w_n
wn_zz(z)=diff(wn_z,z); %derivata di wn_z

% Plot
%% Soluzione
a=0:h_n/(100-1):h_n;
figure(1)
plot(double(w_n(a)),a,'g')
title(['\fontname{Courier}\fontsize{15}Deformazione w_(z)'], 'color','K');
ylabel('z [mm]');
xlabel('w(z) [mm]');
axis square

```

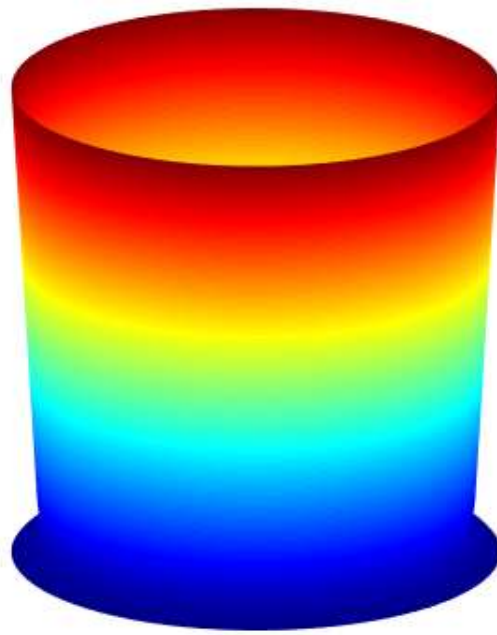


```

figure(2)
fig = gcf; % current figure handle
fig.Color = [1 1 1];
fig.ToolBar = 'none';
colormap(jet(100))
c=100000; % coefficiente che amplifica la deformazione
w1_n=R_n+(double(w_n(a))*c);
[X,Y,Z]=cylinder(w1_n,100);
s1=surface(X,Y,Z,'FaceAlpha',1,'EdgeColor','k','LineWidth',0.01);
title(['\fontname{Courier}\fontsize{15}Deformazione3D w_(z)'], 'color','K');
axis off
axis square
shading interp;
view([5.700 18.800])
rotate3d

```

## Deformazione3D $w(z)$



## Calcolo CDS

```
ns(z)=simplify(-w*E*t/R)
```

ns(z) =

$$- \frac{E t \left( A_1 e^{-\frac{\sqrt{2} \beta z}{2 R}} \cos\left(\frac{\sqrt{2} \beta z}{2 R}\right) + A_2 e^{-\frac{\sqrt{2} \beta z}{2 R}} \sin\left(\frac{\sqrt{2} \beta z}{2 R}\right) - \frac{R^2 \gamma (h - z)}{E t} \right)}{R}$$

```
%% Plot the ns(z) stresses
```

```
a=0:h_n/(200-1):h_n;
```

```
figure(3)
```

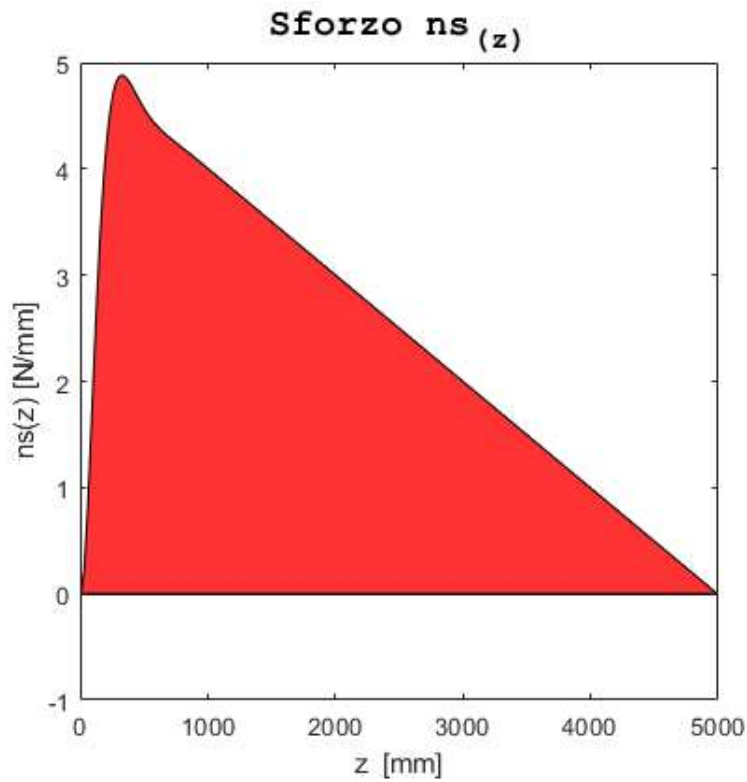
```
area(a,double(-w_n(a)*E_n*t_n/R_n),'FaceColor','r','Facealpha',0.8)
```

```
title(['\fontname{Courier}\fontsize{15}Sforzo ns(_z_)'],'color','K');
```

```
xlabel('z [mm]');
```

```
ylabel('ns(z) [N/mm]');
```

```
axis square
```



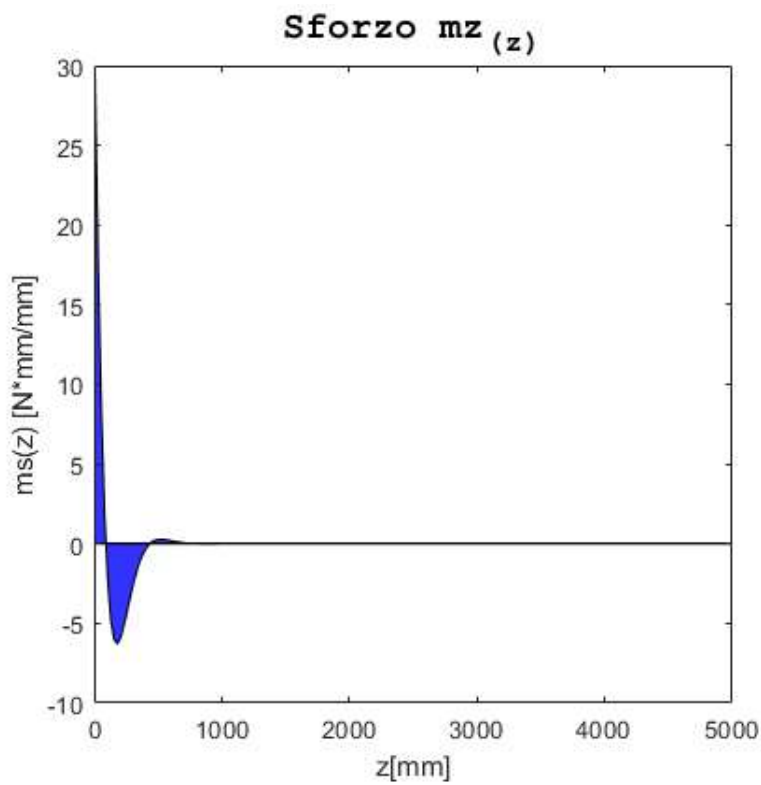
```
w_zz(z)=simplify(diff(w_z,z))
```

$$w_{zz}(z) = - \frac{\beta^2 e^{-\frac{\sqrt{2}\beta z}{2R}} \left( A_2 \cos\left(\frac{\sqrt{2}\beta z}{2R}\right) - A_1 \sin\left(\frac{\sqrt{2}\beta z}{2R}\right) \right)}{R^2}$$

```
mz(z)=simplify(-D*w_zz)
```

$$mz(z) = \frac{D \beta^2 e^{-\frac{\sqrt{2}\beta z}{2R}} \left( A_2 \cos\left(\frac{\sqrt{2}\beta z}{2R}\right) - A_1 \sin\left(\frac{\sqrt{2}\beta z}{2R}\right) \right)}{R^2}$$

```
%% Plot the mz(z) stresses
figure(4)
mz_n(z)=(-wn_zz*D_n);
area(a,double(mz_n(a)), 'FaceColor','b','Facealpha',0.8)
title(['\fontname{Courier}\fontsize{15}Sforzo mz_(z_)'], 'color','K');
xlabel('z[mm]');
ylabel('ms(z) [N*mm/mm]');
axis square
```



```
tz(z)=simplify(diff(mz))
```

tz(z) =

$$-\frac{\sqrt{2} D \beta^3 e^{-\sigma_1} (A_1 \cos(\sigma_1) + A_2 \cos(\sigma_1) - A_1 \sin(\sigma_1) + A_2 \sin(\sigma_1))}{2 R^3}$$

where

$$\sigma_1 = \frac{\sqrt{2} \beta z}{2 R}$$

```
% Plot the ns(z) stresses
figure(5)
tz_n(z)=diff(mz_n);
area(a,double(tz_n(a)), 'FaceColor','g','Facealpha',0.8)
title(['\fontname{Courier}\fontsize{15}Sforzo tz_(z_)'], 'color','K');
xlabel('z [mm]');
ylabel('tz(z) [N/mm]');
axis square
```

