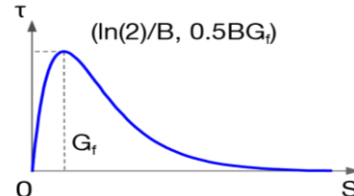
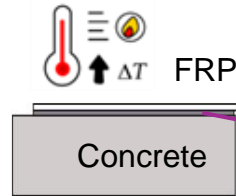


# Bond behavior of CFRP-to-concrete interface subjected to loading and elevated temperature

## Analytical solution



First stage

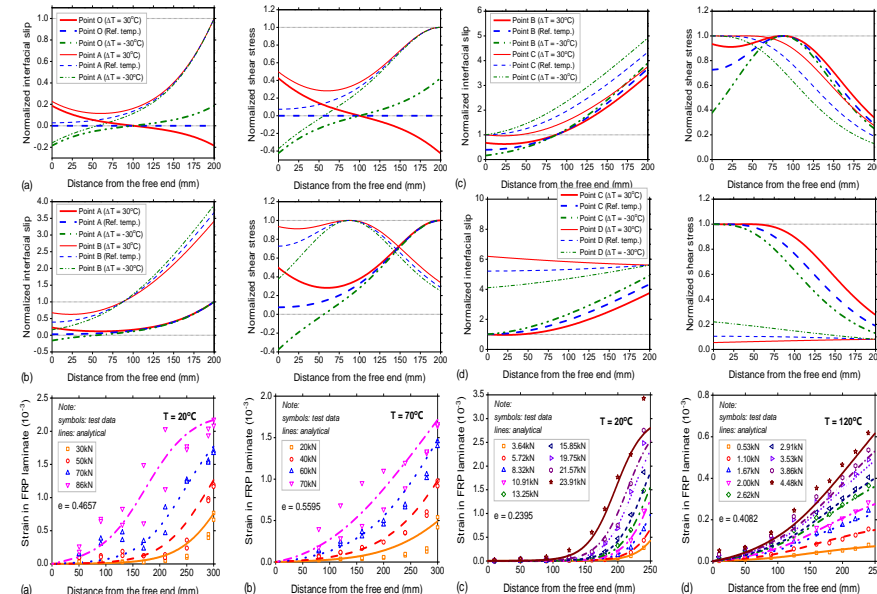
$$\tau = \begin{cases} 2BG_f \left\{ \frac{2(D+1)}{n_1 e^{-AB\sqrt{D+1}x} - n_2 D e^{AB\sqrt{D+1}x} + 2} - \left[ \frac{2(D+1)}{n_1 e^{-AB\sqrt{D+1}x} - n_2 D e^{AB\sqrt{D+1}x} + 2} \right]^2 \right\} & (x \leq x_0) \\ -2BG_f \left\{ \frac{2(D+1)}{n_3 e^{AB\sqrt{D+1}x} - n_4 D e^{-AB\sqrt{D+1}x} + 2} - \left[ \frac{2(D+1)}{n_3 e^{AB\sqrt{D+1}x} - n_4 D e^{-AB\sqrt{D+1}x} + 2} \right]^2 \right\} & (x > x_0) \end{cases}$$

Second stage

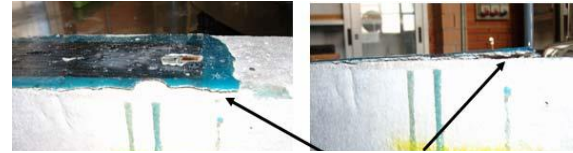
$$\tau = 2BG_f \left\{ \frac{2(D+1)}{(n_1 e^{-AB\sqrt{D+1}x} - n_2 D e^{AB\sqrt{D+1}x} + 2)} - \left[ \frac{2(D+1)}{(n_1 e^{-AB\sqrt{D+1}x} - n_2 D e^{AB\sqrt{D+1}x} + 2)} \right]^2 \right\}$$

Third stage

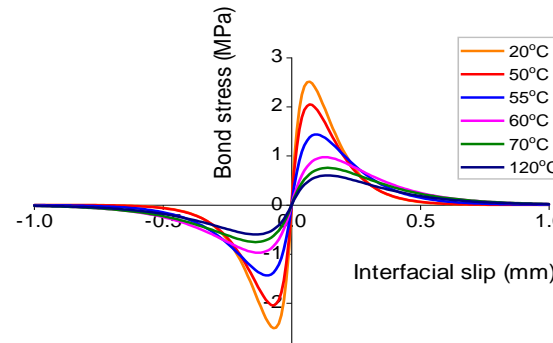
$$\tau = 2BG_f \left\{ \frac{2(D+1)}{(n_1 e^{-AB\sqrt{D+1}x} - n_2 D e^{AB\sqrt{D+1}x} + 2)} - \left[ \frac{2(D+1)}{(n_1 e^{-AB\sqrt{D+1}x} - n_2 D e^{AB\sqrt{D+1}x} + 2)} \right]^2 \right\}$$



## Temperature-dependent bond-slip model



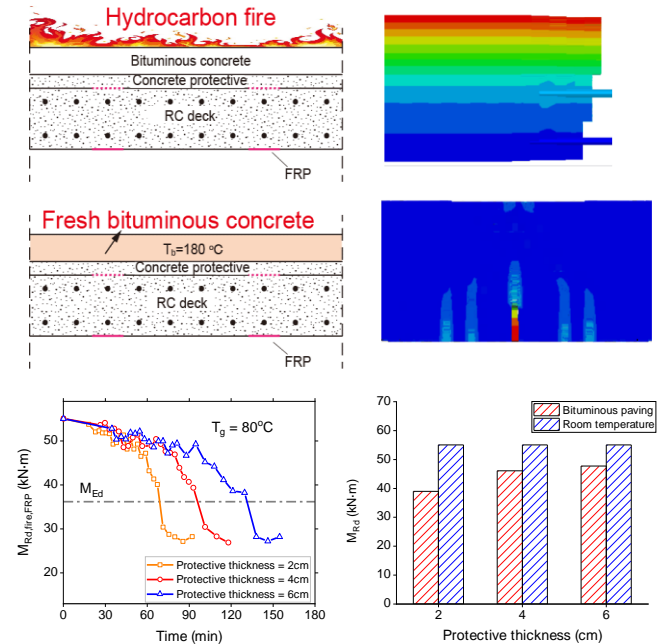
High temperature-induced bond degradation



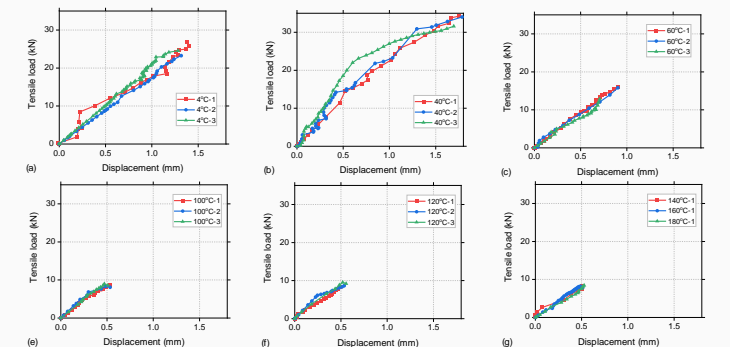
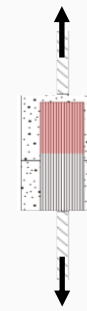
$$\frac{G_{fT}}{G_{f0}} = \left( \frac{1-a_1}{2} \right) \tanh \left[ -a_2 \left( \frac{T}{T_g} - a_3 \right) \right] + \left( \frac{1+a_1}{2} \right)$$

$$a_1 = 0.489, a_2 = 3.282, a_3 = 0.958$$

## Finite element simulation

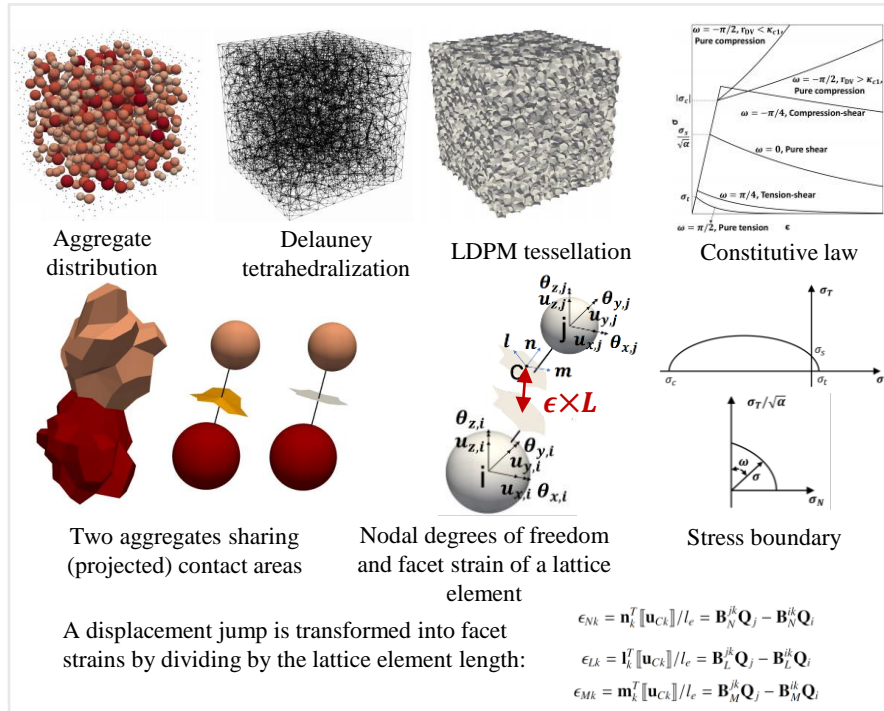


## Experimental study

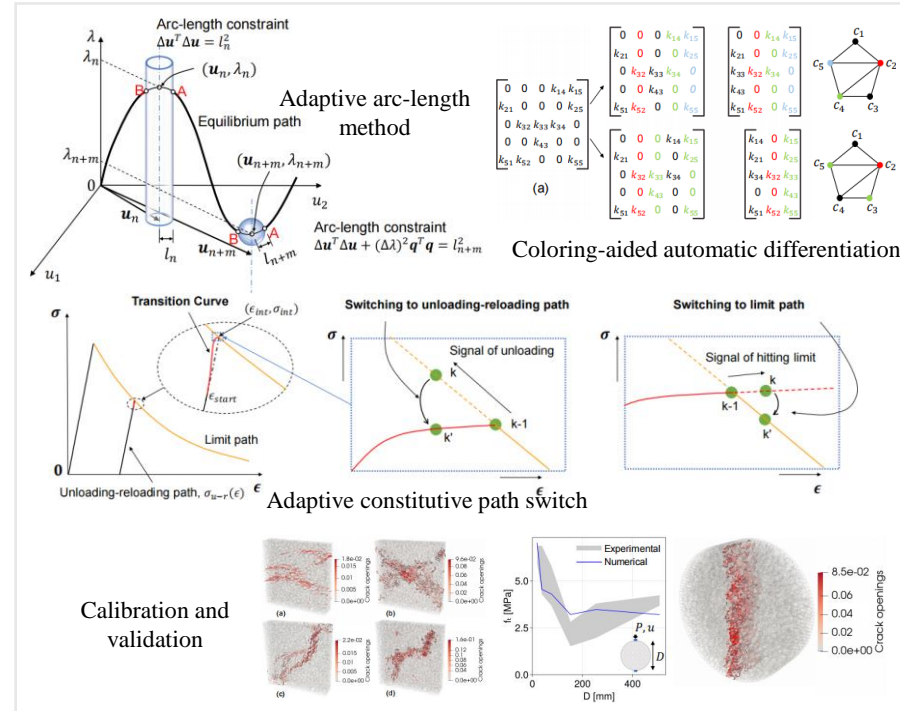


# Bond behavior of CFRP-to-concrete interface subjected to loading and elevated temperature

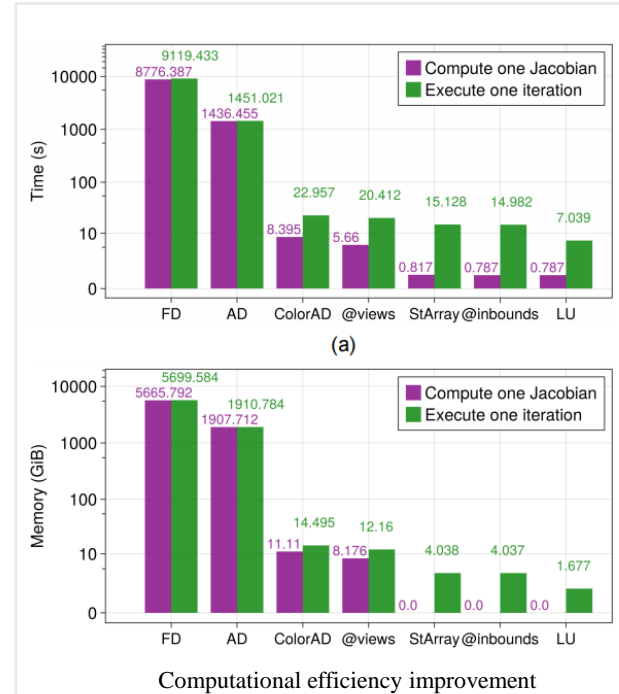
## Lattice discrete particle model (LDPM)



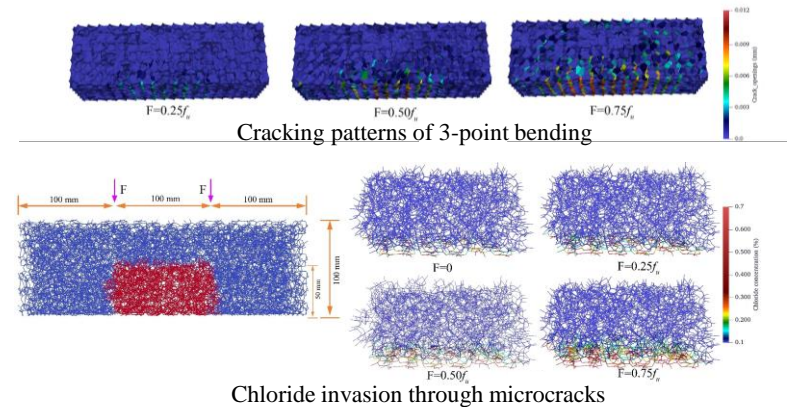
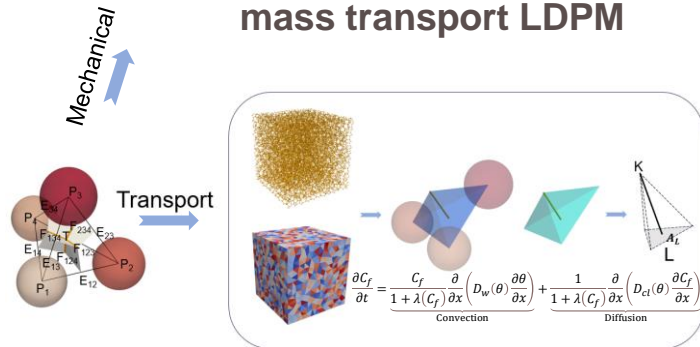
## Static solution



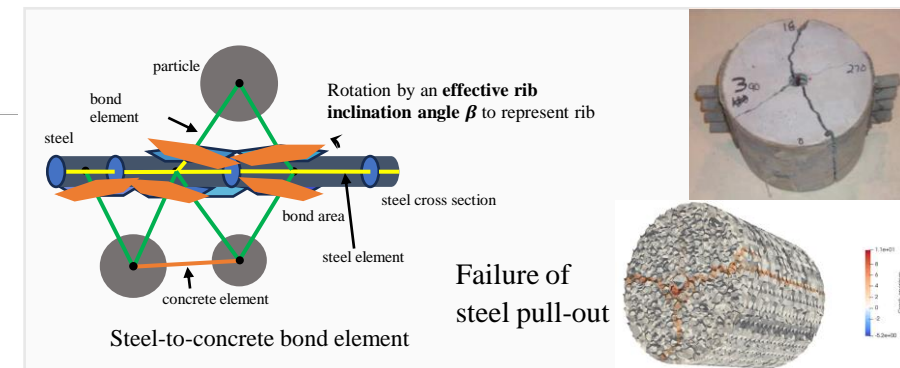
## Computational efficiency



## Coupled mechanical and mass transport LDPM



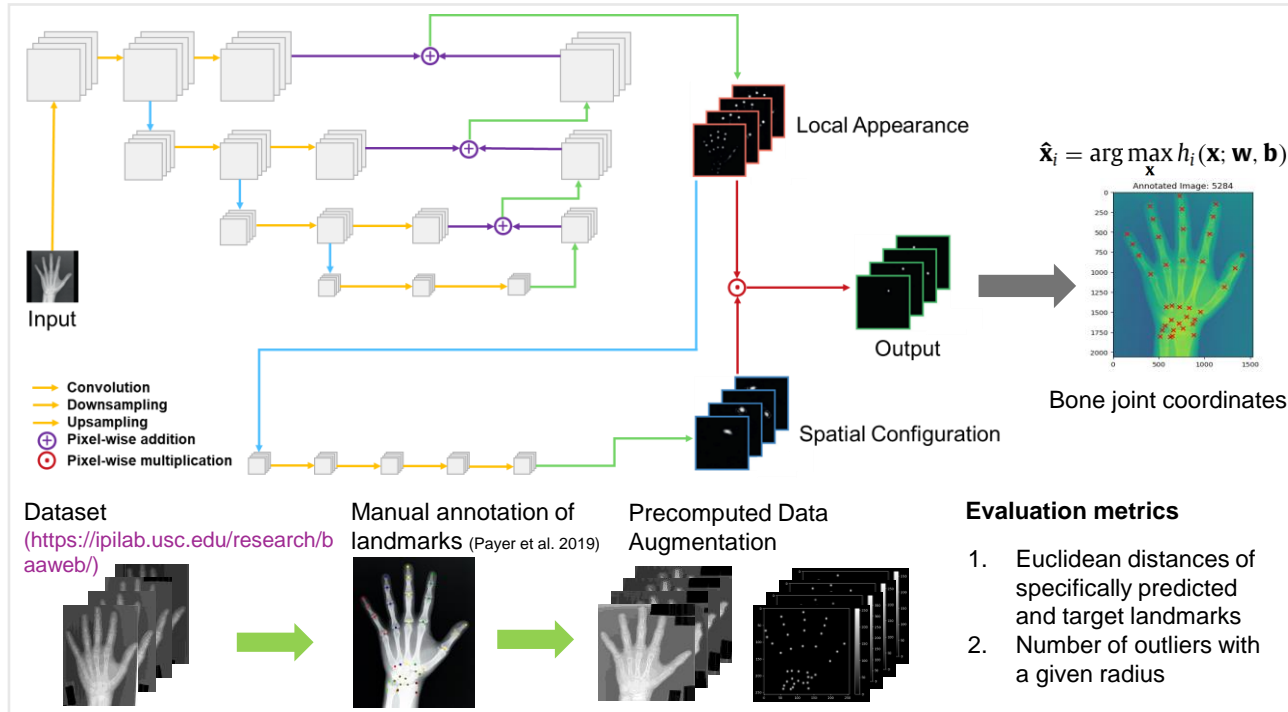
## LDPM for reinforced concrete



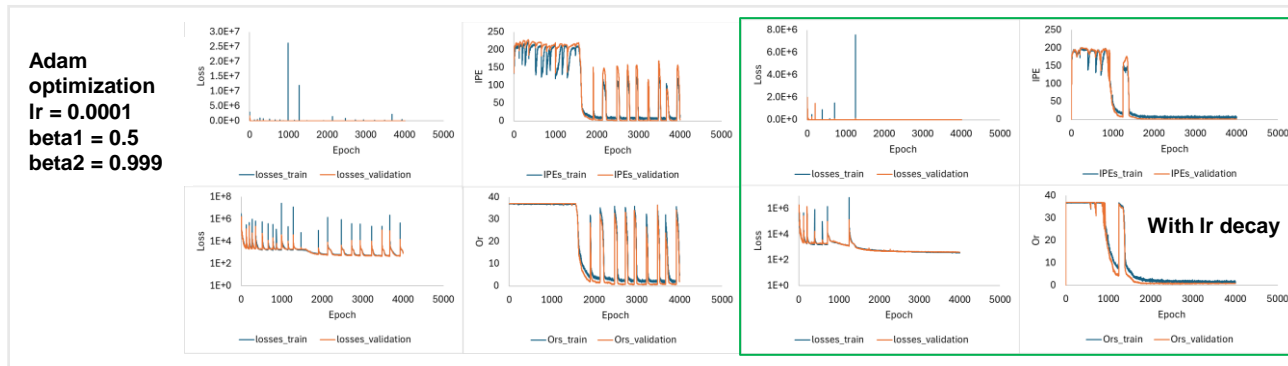


# Bond behavior of CFRP-to-concrete interface subjected to loading and elevated temperature

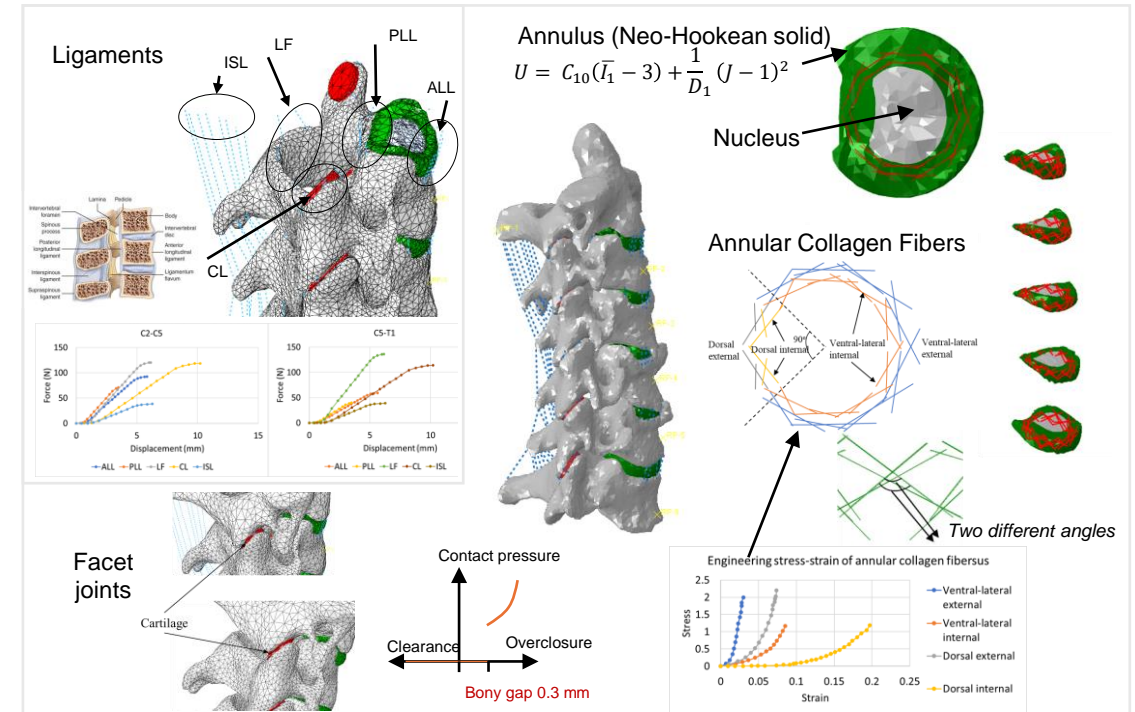
## SpatialConfiguration-Net



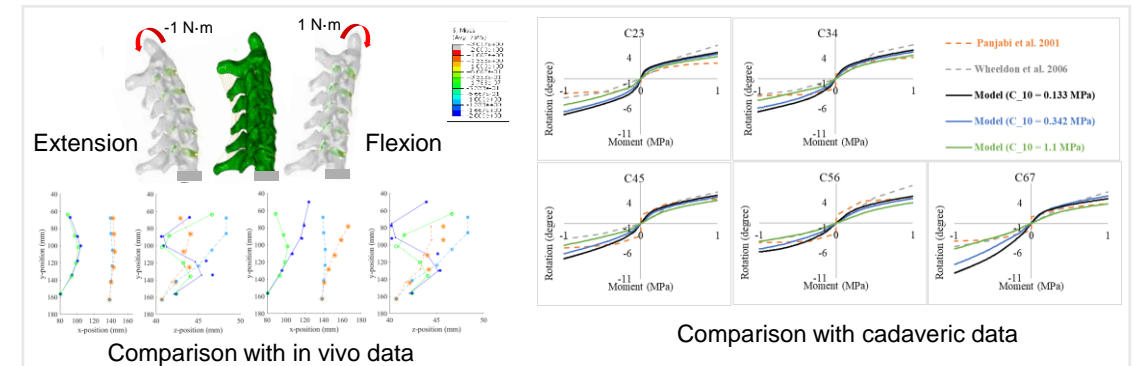
## Train and validation



## FEM spine modeling

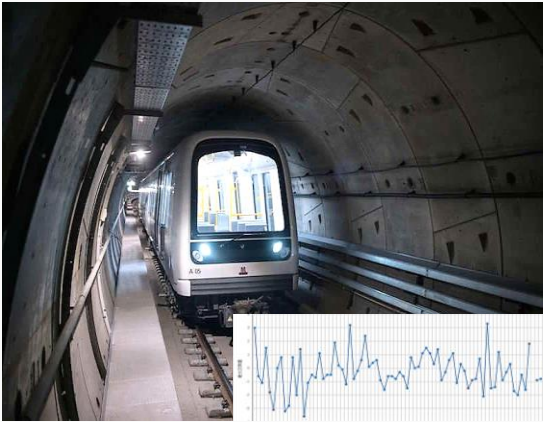


## Calibration and validation



# Deformation Characteristics of Hangzhou Soft Soil under Cyclic Loading (2017)

## Engineering problem

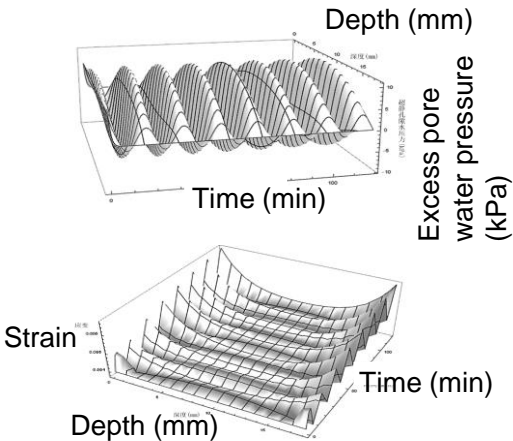


## Experiments

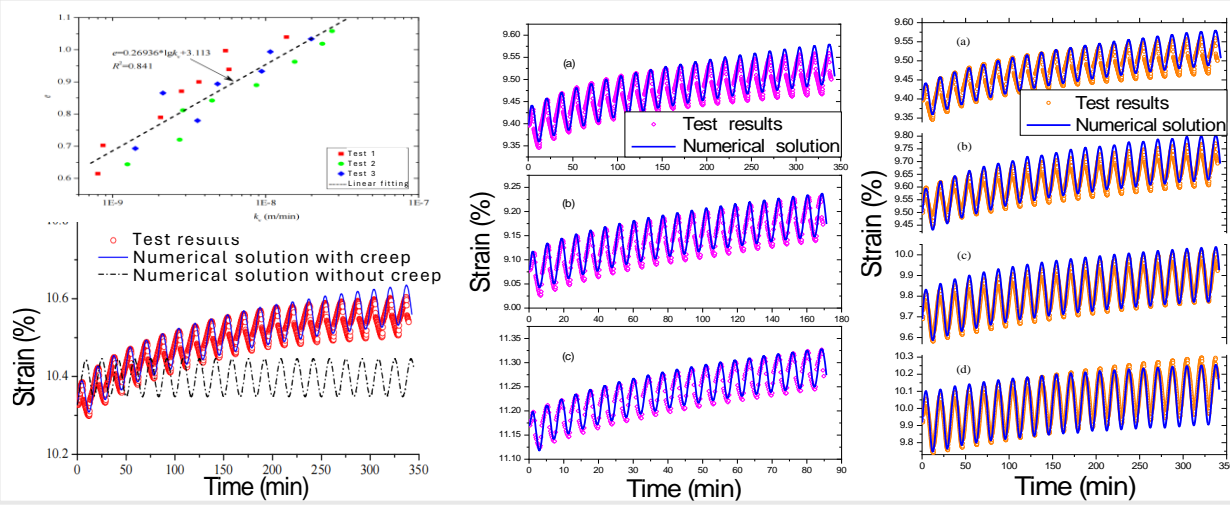


## Elastic visco-plastic consolidation model and solution

$$\left\{ \begin{aligned} & \frac{k_{vo}}{\gamma_w} \left( \frac{\sigma'_o}{\sigma'_z} \right)^{\frac{c_c}{c_k}} \left[ \frac{\partial^2 u}{\partial z^2} + \frac{c_c}{c_k} \left( \frac{1}{\sigma'_z} \right) \left( \frac{\partial u}{\partial z} \right)^2 \right] = - \frac{\partial \varepsilon_z}{\partial t} \\ & \dot{\varepsilon}_z = \frac{\kappa}{V} \frac{\dot{\sigma}'_z}{\sigma'_z} + \frac{\psi}{V t_0} \exp \left[ - \left( \varepsilon_z - \varepsilon_{z0}^{ep} \right) \frac{V}{\psi} \right] \left( \frac{\sigma'_z}{\sigma'_{z0}} \right)^{\frac{\lambda}{\psi}} \\ & u(0, t) = 0 \\ & u(H, t) = 0 \\ & u(z, 0) = \text{Initial excess pore water pressure} \\ & \varepsilon_z(z, 0) = \text{Initial strain} \end{aligned} \right.$$



## Calibration and Validation



## Calcusettlement v2.0

