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# DYNAMIQUE DES SYSTÈMES MÉCANIQUES

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## Project 1

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One degree of freedom damped system

François ROZET

University of Liège  
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# Setup

The system consists in a mass  $m$  supported by a spring of stiffness  $k$  and a viscous damper of unknown damping  $c$ .

We assume that the system has only one degree of freedom  $x$  and we know that

$$\begin{aligned} m &= 4.484 \text{ kg} \\ k &= 10\,500 \text{ N/m} \end{aligned}$$

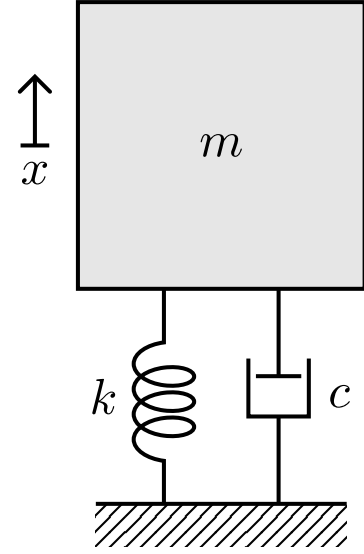


Figure 1 – System

# Computations

## 1 Natural frequency

The natural (or undamped) frequency<sup>1</sup>  $\omega_0$  of the system, which would have been the frequency of the motion if the system wasn't damped, is given by

$$\begin{aligned} \omega_0 &= \sqrt{\frac{k}{m}} \\ &= 48.3907 \text{ rad/s} \end{aligned}$$

✓

## 3 Time response

First of all, we observe that our system performs damped harmonic oscillations. It means that  $\varepsilon$ , the damping ratio of the system, is strictly between 0 and 1.

Further, to compute experimental system parameters, we have to select the 1<sup>st</sup> and the  $n^{\text{th}}$  2 maxima of the dataset<sup>3</sup> and interpolate around both peaks to obtain more accurate values of time and acceleration :

$$\begin{aligned} t_1 &= 0.1621 \text{ s} & a_1 &= 8.793 \times 10^{-2} \text{ g} \\ t_n &= 6.3645 \text{ s} & a_n &= 0.299 \times 10^{-2} \text{ g} \end{aligned}$$

<sup>1</sup>In this document, by convenience, angular frequency is shortened to frequency, despite their different units of measurement.

<sup>2</sup>In the matlab implementation, we have chosen  $n = 50$ .

<sup>3</sup>We have shrunk the dataset to the time interval  $[0.140, 9.850]$  [s] because extreme values were unreliable.

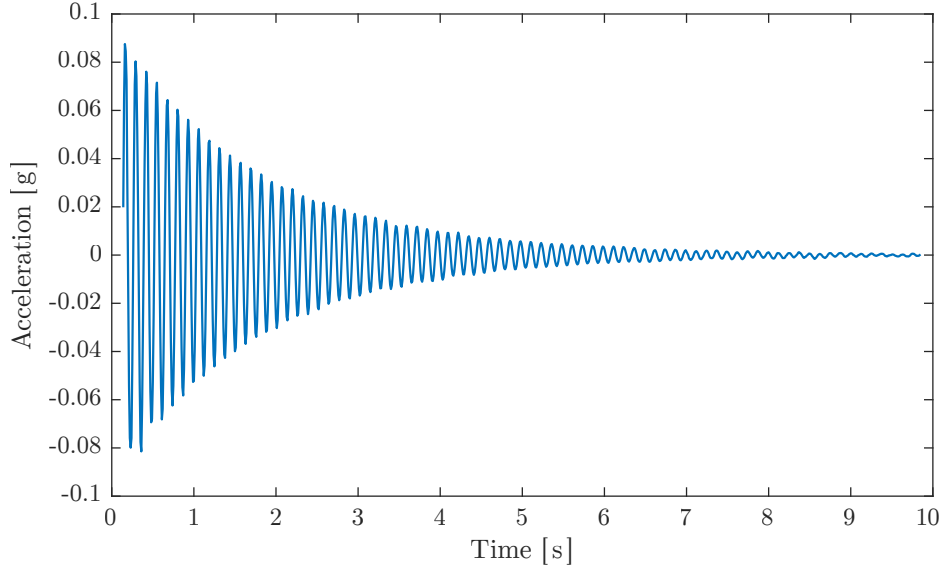


Figure 2 – Acceleration response of the system from time 0.140 s to 9.850 s.

### 3.1 Frequency

The frequency  $f$  of an harmonic motion is the ratio between the number of full oscillations performed by the system during a time period and that time period length.

$$\begin{aligned}
 f_d &= \frac{n}{t_n - t_1} \\
 &= 7.9001 \text{ Hz} \\
 \Leftrightarrow \omega_d &= 2\pi f_d = 49.6380 \text{ rad/s}
 \end{aligned}$$

✓

We see that the experimental frequency  $\omega_d$  is a bit larger than the undamped frequency  $\omega_0$ , although it should be smaller or equal given that

$$\omega_d = \omega_0 \sqrt{1 - \varepsilon^2} \leq \omega_0$$

It means that either our measures or our parameters ( $m$  or  $k$ ) are imprecise.

### 3.2 Logarithmic decrement

The logarithmic decrement  $\Delta$  is defined by the neperian logarithm of the ratio between the amplitudes of two successive maxima. That ratio, and thus  $\Delta$ , is theoretically constant all along the harmonic motion. From its definition, it is easy to show that

$$\Delta = \ln \left( \frac{a_k}{a_{k+1}} \right) = \dots = \frac{\ln \left( \frac{a_1}{a_n} \right)}{n-1} \quad \forall k > 1$$

Replacing with our computed values  $a_1$  and  $a_n$ , we obtain

$$\Delta = \frac{\ln \left( \frac{a_1}{a_n} \right)}{n-1} = 6.9002 \times 10^{-2}$$

### 3.3 Damping ratio

The value of the damping ratio  $\varepsilon$  is usually computed according to its definition :

$$\varepsilon = \frac{c}{2m\omega_0}$$

In this case, the damping  $c$  of the system is unknown. However, the damping ratio can still be estimated by the logarithmic decrement divided by  $2\pi$ .

$$\varepsilon \simeq \frac{\Delta}{2\pi} = 1.0982 \times 10^{-2}$$

## 5 Bode diagram

In the amplitude Bode diagram, we can observe a spike in amplitude near the natural frequency of the system. Searching for more accuracy, we can interpolate around the peak and obtain  $X$ , the maximum amplitude, and  $\omega_b$ , its associated frequency.

$$X = 0.8116 \text{ g/N}$$

$$\omega_b = 49.7242 \text{ rad/sec}$$

How?

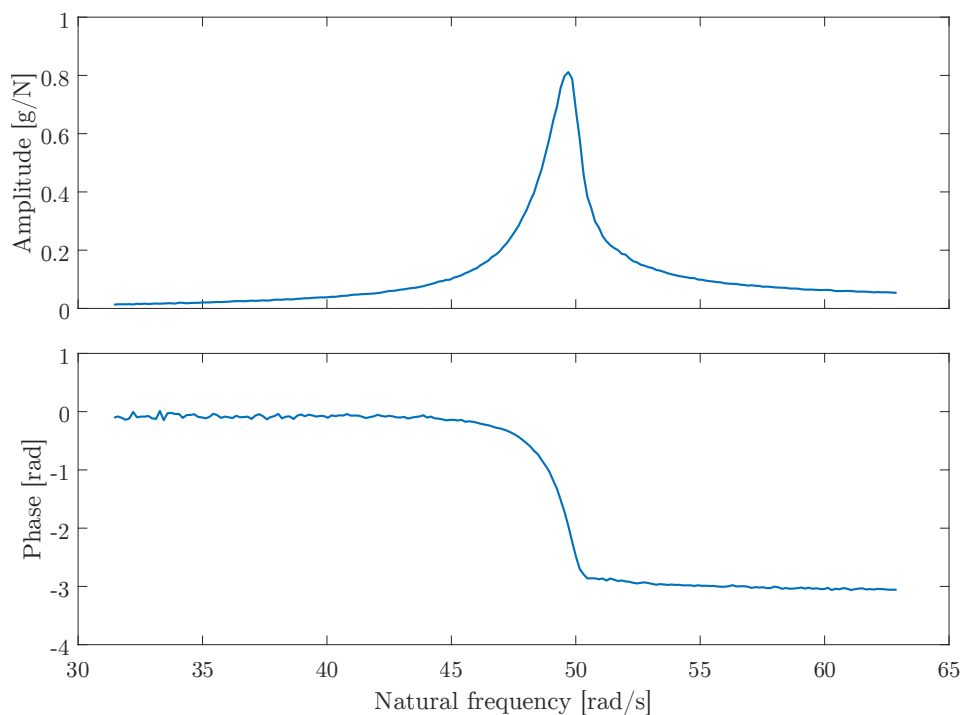


Figure 3 – Bode diagrams.

## 5.1 Quality factor

The half-power method's first step is to find the frequencies  $\omega_-$  and  $\omega_+$  for which the amplitude is equal to  $\frac{X}{\sqrt{2}}$ . These can be found by interpolating separately each side of the amplitude Bode diagram's peak. In doing so, we obtain

$$\omega_- = 48.9125 \text{ rad/sec} \qquad \omega_+ = 50.1696 \text{ rad/sec}$$

We can now compute the quality factor  $Q$  of the system

$$\begin{aligned} Q &= \frac{\omega_b}{\Delta\omega} = \frac{\omega_b}{\omega_+ - \omega_-} \\ &= 38.494 \end{aligned}$$

## 5.2 Damping ratio

The damping ratio can be directly estimated from the quality factor.

$$\varepsilon \simeq \frac{1}{2Q} = 1.299 \times 10^{-2}$$

# 6 Nyquist diagram

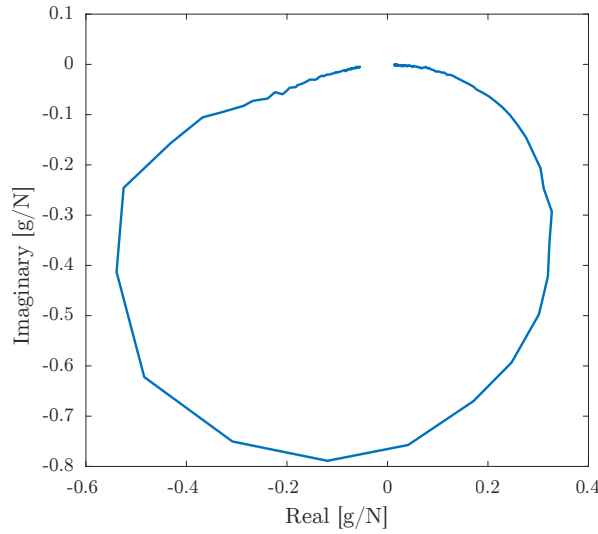


Figure 4 – Nyquist diagram.

## 6.1 Quality factor

The quality factor can also be estimated by the amplitude<sup>4</sup> at the phase resonance, described by a null real part. Firstly, we have to find the phase resonance frequency  $\omega_n$  by interpolating around the real part root, which gives us

$$\omega_n = 49.4366 \text{ rad/sec}$$

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<sup>4</sup>The amplitude has to be normed. In our case it means to multiply the amplitude by  $m$ .

It is now possible to determine the amplitude  $X_n$  associated to  $\omega_n$ .

$$\begin{aligned} X_n &= \sqrt{\Re(\mathbf{X})^2 + \Im(\mathbf{X})^2} = |\Im(\mathbf{X})| \\ &= 0.7723 \text{ g/N} = 7.5759 \text{ m/s}^2 \cdot \text{N} \end{aligned}$$

And, therefore, the quality factor.

$$Q \simeq mX_n = 33.9704$$

## 6.2 Damping ratio

Finally, with the same estimation than before

$$\varepsilon \simeq \frac{1}{2Q} = 1.472 \times 10^{-2}$$

## 7 Conclusion

We can observe that either the time response, the Bode diagram or the Nyquist diagram gave us approximatively the same results :

$$\varepsilon \approx 1\%$$

This shows that, as expected, all these methods are effective. Therefore, the choice between one or another should be lead by its convenience which varies from case to case.