



DYNAMIQUE DES SYSTÈMES MÉCANIQUES

Project 1

One degree of freedom damped system

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Setup

The system consists in a mass m supported by a spring of stiffness k and a viscous damper of unknown damping c .

We assume that the system has only one degree of freedom x and we know that

$$\begin{aligned} m &= 4.484 \text{ kg} \\ k &= 10\,500 \text{ N/m} \end{aligned}$$

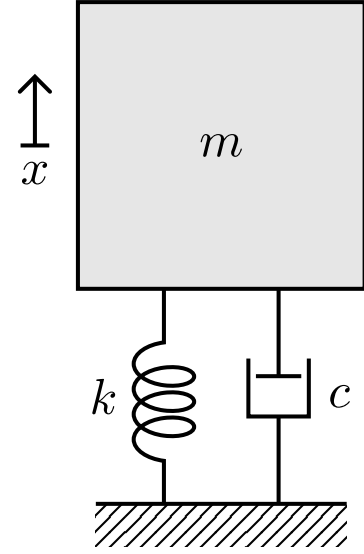


Figure 1 – System

Computations

1 Natural frequency

The natural (or undamped) frequency¹ w_0 of the system, which would have been the frequency of the motion if the system wasn't damped, is given by

$$\begin{aligned} \omega_0 &= \sqrt{\frac{k}{m}} \\ &= 48.3907 \text{ rad/s} \end{aligned}$$

3 Time response

First of all, we observe that our system performs damped harmonic oscillations. It means that ε , the damping ratio of the system, is strictly between 0 and 1.

Further, to compute experimental system parameters, we have to select the 1st and the n^{th} 2 maxima of the dataset³ and interpolate around both peaks to obtain more accurate values of time and acceleration :

$$\begin{aligned} t_1 &= 0.1621 \text{ s} & a_1 &= 8.793 \times 10^{-2} \text{ g} \\ t_n &= 6.3645 \text{ s} & a_n &= 0.299 \times 10^{-2} \text{ g} \end{aligned}$$

¹In this document, by convenience, angular frequency is shortened to frequency, despite their different units of measurement.

²In the matlab implementation, we have chosen $n = 50$.

³We have shrunk the dataset to the time interval $[0.140, 9.850]$ [s] because extreme values were unreliable.

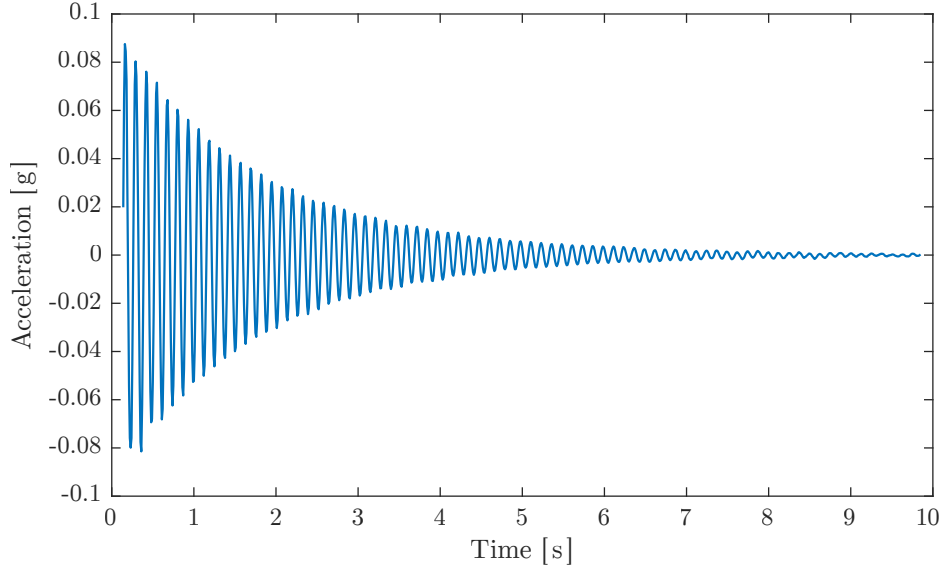


Figure 2 – Acceleration response of the system from time 0.140 s to 9.850 s.

3.1 Frequency

The frequency f of an harmonic motion is the ratio between the number of full oscillations performed by the system during a time period and that time period length.

$$\begin{aligned} f_d &= \frac{n}{t_n - t_1} \\ &= 7.9001 \text{ Hz} \\ \Leftrightarrow \omega_d &= 2\pi f_d = 49.6380 \text{ rad/s} \end{aligned}$$

We see that the experimental frequency ω_d is a bit larger than the undamped frequency ω_0 , although it should be smaller or equal given that

$$\omega_d = \omega_0 \sqrt{1 - \varepsilon^2} \leq \omega_0$$

It means that either our measures or our parameters (m or k) are imprecise.

3.2 Logarithmic decrement

The logarithmic decrement Δ is defined by the neperian logarithm of the ratio between the amplitudes of two successive maxima. That ratio, and thus Δ , is theoretically constant all along the harmonic motion. From its definition, it is easy to show that

$$\Delta = \ln \left(\frac{a_k}{a_{k+1}} \right) = \dots = \frac{\ln \left(\frac{a_1}{a_n} \right)}{n-1} \quad \forall k > 1$$

Replacing with our computed values a_1 and a_n , we obtain

$$\Delta = \frac{\ln \left(\frac{a_1}{a_n} \right)}{n-1} = 6.9002 \times 10^{-2}$$

3.3 Damping ratio

The value of the damping ratio ε is usually computed according to its definition :

$$\varepsilon = \frac{c}{2m\omega_0}$$

In this case, the damping c of the system is unknown. However, the damping ratio can still be estimated by the logarithmic decrement divided by 2π .

$$\varepsilon \simeq \frac{\Delta}{2\pi} = 1.0982 \times 10^{-2}$$

5 Bode diagram

In the amplitude Bode diagram, we can observe a spike in amplitude near the natural frequency of the system. Searching for more accuracy, we can interpolate around the peak and obtain X , the maximum amplitude, and ω_b , its associated frequency.

$$X = 0.8116 \text{ g/N}$$

$$\omega_b = 49.7242 \text{ rad/sec}$$

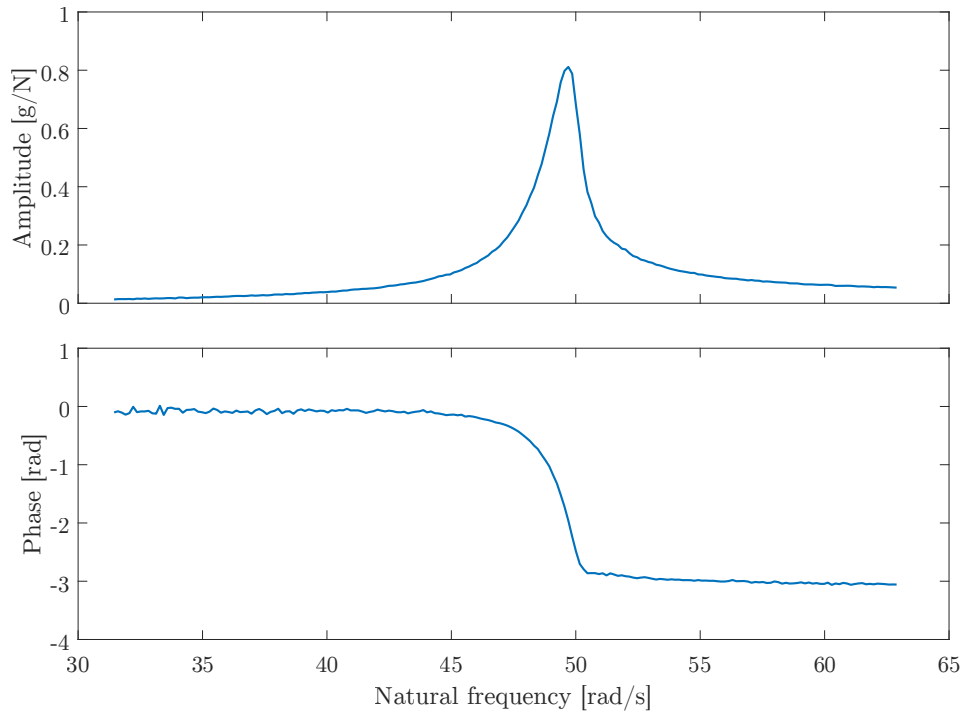


Figure 3 – Bode diagrams.

5.1 Quality factor

The half-power method's first step is to find the frequencies ω_- and ω_+ for which the amplitude is equal to $\frac{X}{\sqrt{2}}$. These can be found by interpolating separately each side of the amplitude Bode diagram's peak. In doing so, we obtain

$$\omega_- = 48.9125 \text{ rad/sec} \qquad \omega_+ = 50.1696 \text{ rad/sec}$$

We can now compute the quality factor Q of the system

$$\begin{aligned} Q &= \frac{\omega_b}{\Delta\omega} = \frac{\omega_b}{\omega_+ - \omega_-} \\ &= 38.494 \end{aligned}$$

5.2 Damping ratio

The damping ratio can be directly estimated from the quality factor.

$$\varepsilon \simeq \frac{1}{2Q} = 1.299 \times 10^{-2}$$

6 Nyquist diagram

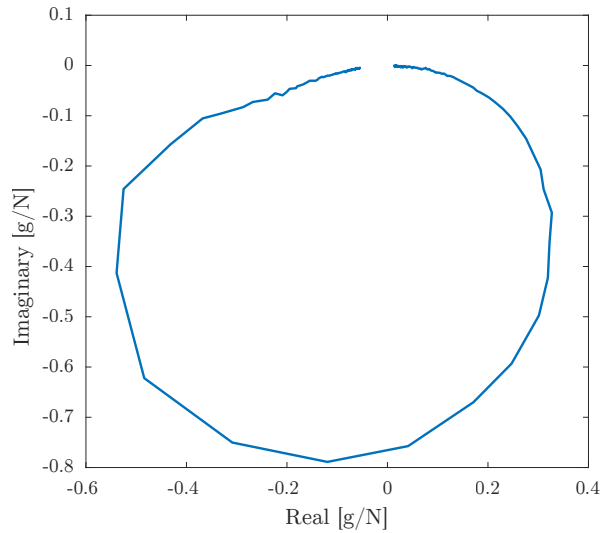


Figure 4 – Nyquist diagram.

6.1 Quality factor

The quality factor can also be estimated by the amplitude⁴ at the phase resonance, described by a null real part. Firstly, we have to find the phase resonance frequency ω_n by

⁴The amplitude has to be normed. In our case it means to multiply the amplitude by m .

interpolating around the real part root, which gives us

$$\omega_n = 49.4366 \text{ rad/sec}$$

It is now possible to determine the amplitude X_n associated to ω_n .

$$\begin{aligned} X_n &= \sqrt{\Re(\mathbf{X})^2 + \Im(\mathbf{X})^2} = |\Im(\mathbf{X})| \\ &= 0.7723 \text{ g/N} = 7.5759 \text{ m/s}^2 \cdot \text{N} \end{aligned}$$

And, therefore, the quality factor.

$$Q \simeq mX_n = 33.9704$$

6.2 Damping ratio

Finally, with the same estimation than before

$$\varepsilon \simeq \frac{1}{2Q} = 1.472 \times 10^{-2}$$

7 Conclusion

We can observe that either the time response, the Bode diagram or the Nyquist diagram gave us approximatively the same results :

$$\varepsilon \approx 1\%$$

This shows that, as expected, all these methods are effective. Therefore, the choice between one or another should be lead by its convenience which varies from case to case.