Surface Gibbs Free Energy for Ternary Oxides: Alternative Derivation with B as Independent Variable

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1 Introduction

This document presents an alternative derivation of the surface Gibbs free energy for ternary oxides $A_x B_y O_z$, where the chemical potential of element B (instead of element A) is used as one of the two independent variables alongside oxygen. This formulation is particularly useful when analyzing systems like Ag_3PO_4 , where one might want to study surface stability as a function of phosphorus chemical potential ($\Delta \mu_P$) rather than silver chemical potential ($\Delta \mu_{Ag}$).

The standard derivation (e.g., as presented in the supplementary material) treats element A as the independent variable and eliminates μ_B using the bulk equilibrium condition. Here, we reverse this approach: we treat B as independent and eliminate μ_A instead.

2 General Surface Energy Expression

For a ternary oxide slab containing N_A atoms of element A, N_B atoms of element B, and N_O atoms of oxygen, with two symmetric surfaces each of area A, the surface Gibbs free energy is:

$$\gamma(T, p_{O_2}) = \frac{1}{2A} \left[E^{\text{slab}} - N_A \mu_A(T, p_{O_2}) - N_B \mu_B(T, p_{O_2}) - N_O \mu_O(T, p_{O_2}) \right]$$
(1)

where E^{slab} is the DFT total energy of the slab, and μ_i are the chemical potentials of each species.

3 Bulk Equilibrium Condition

The bulk ternary oxide $A_x B_y O_z$ must be in thermodynamic equilibrium:

$$x\mu_A + y\mu_B + z\mu_O = E_{A_xB_yO_z}^{\text{bulk}} \tag{2}$$

4 Elimination of μ_A (A as Dependent Variable)

We solve Eq. 2 for μ_A to eliminate it in favor of μ_B and μ_O :

$$\mu_A = \frac{1}{x} \left[E_{A_x B_y O_z}^{\text{bulk}} - y \mu_B - z \mu_O \right] \tag{3}$$

Substituting this into Eq. 1:

$$\gamma = \frac{1}{2A} \left[E^{\text{slab}} - N_A \cdot \frac{1}{x} \left(E^{\text{bulk}}_{A_x B_y O_z} - y \mu_B - z \mu_O \right) - N_B \mu_B - N_O \mu_O \right]$$
(4)

Expanding and rearranging:

$$\gamma = \frac{1}{2A} \left[E^{\text{slab}} - \frac{N_A}{x} E^{\text{bulk}}_{A_x B_y O_z} + \frac{N_A y}{x} \mu_B + \frac{N_A z}{x} \mu_O - N_B \mu_B - N_O \mu_O \right]$$
 (5)

Collecting terms with μ_B and μ_O :

$$\gamma = \frac{1}{2A} \left[E^{\text{slab}} - \frac{N_A}{x} E^{\text{bulk}}_{A_x B_y O_z} + \left(\frac{N_A y}{x} - N_B \right) \mu_B + \left(\frac{N_A z}{x} - N_O \right) \mu_O \right]$$
 (6)

5 Reference State and Relative Chemical Potentials

We define reference states for the chemical potentials:

$$\mu_B^{\text{ref}} = E_B^{\text{bulk}} \quad \text{(bulk elemental B)}$$
(7)

$$\mu_O^{\text{ref}} = \frac{1}{2} E_{O_2}^{\text{DFT}} \quad (O_2 \text{ gas at } 0 \text{ K})$$
(8)

The relative chemical potentials (deviations from reference) are:

$$\Delta\mu_B = \mu_B - \mu_B^{\text{ref}} = \mu_B - E_B^{\text{bulk}} \tag{9}$$

$$\Delta\mu_O = \mu_O - \mu_O^{\text{ref}} = \mu_O - \frac{1}{2}E_{O_2}^{\text{DFT}}$$
 (10)

Substituting $\mu_B = \Delta \mu_B + E_B^{\text{bulk}}$ and $\mu_O = \Delta \mu_O + \frac{1}{2} E_{\text{O}_2}^{\text{DFT}}$ into Eq. 6:

$$\gamma = \frac{1}{2A} \left[E^{\text{slab}} - \frac{N_A}{x} E^{\text{bulk}}_{A_x B_y O_z} + \left(\frac{N_A y}{x} - N_B \right) \left(\Delta \mu_B + E^{\text{bulk}}_B \right) + \left(\frac{N_A z}{x} - N_O \right) \left(\Delta \mu_O + \frac{1}{2} E^{\text{DFT}}_{O_2} \right) \right] \tag{11}$$

6 Defining the Reference Surface Energy ϕ

We define a reference surface energy ϕ as the value of γ when both $\Delta \mu_B = 0$ and $\Delta \mu_O = 0$ (i.e., at the reference state, typically the B-rich and O-poor limit):

$$\phi = \frac{1}{2A} \left[E^{\text{slab}} - \frac{N_A}{x} E^{\text{bulk}}_{A_x B_y O_z} + \left(\frac{N_A y}{x} - N_B \right) E^{\text{bulk}}_B + \left(\frac{N_A z}{x} - N_O \right) \frac{1}{2} E^{\text{DFT}}_{\text{O}_2} \right]$$
(12)

7 Final Expression with Surface Excesses

From Eq. 11 and Eq. 12, we can write:

$$\gamma(\Delta\mu_B, \Delta\mu_O) = \phi + \frac{1}{2A} \left(\frac{N_A y}{x} - N_B \right) \Delta\mu_B + \frac{1}{2A} \left(\frac{N_A z}{x} - N_O \right) \Delta\mu_O \tag{13}$$

Define the surface excesses (per unit area):

$$\Gamma_B = \frac{1}{2A} \left(\frac{N_A y}{x} - N_B \right) = \frac{1}{2A} \left(N_B^{\text{stoich}} - N_B \right)$$
 (14)

$$\Gamma_O = \frac{1}{2A} \left(\frac{N_A z}{x} - N_O \right) = \frac{1}{2A} \left(N_O^{\text{stoich}} - N_O \right)$$
 (15)

where $N_B^{\rm stoich}=\frac{N_A y}{x}$ and $N_O^{\rm stoich}=\frac{N_A z}{x}$ are the number of B and O atoms needed to maintain bulk stoichiometry with the N_A atoms of A present in the slab.

The final expression is:

$$\gamma(\Delta\mu_B, \Delta\mu_O) = \phi - \Gamma_B \Delta\mu_B - \Gamma_O \Delta\mu_O$$
(16)

Note the minus signs: when $\Gamma_B > 0$ (B-deficient surface relative to bulk stoichiometry), increasing $\Delta \mu_B$ (B-rich conditions) lowers the surface energy, which is physically intuitive.

8 Formation Energy Formulation

Using the formation energy of the bulk ternary oxide:

$$\Delta E_f(A_x B_y O_z) = E_{A_x B_y O_z}^{\text{bulk}} - x E_A^{\text{bulk}} - y E_B^{\text{bulk}} - z \cdot \frac{1}{2} E_{O_2}^{\text{DFT}}$$
(17)

The reference surface energy ϕ can be rewritten as:

$$\phi = \frac{1}{2A} \left[E^{\text{slab}} - \frac{N_A}{x} \left(\Delta E_f(A_x B_y O_z) + x E_A^{\text{bulk}} + y E_B^{\text{bulk}} + z \cdot \frac{1}{2} E_{\text{O}_2}^{\text{DFT}} \right) + \left(\frac{N_A y}{x} - N_B \right) E_B^{\text{bulk}} + \left(\frac{N_A z}{x} - N_O \right) \frac{1}{2} E_{\text{O}_2}^{\text{DFT}} \right]$$
(18)

Simplifying:

$$\phi = \frac{1}{2A} \left[E^{\text{slab}} - N_A E_A^{\text{bulk}} - N_B E_B^{\text{bulk}} - N_O \cdot \frac{1}{2} E_{O_2}^{\text{DFT}} - \frac{N_A}{x} \Delta E_f(A_x B_y O_z) \right]$$
(19)

9 Chemical Potential Limits

The allowed range of $\Delta \mu_B$ and $\Delta \mu_O$ is constrained by thermodynamic stability requirements:

9.1 Element Precipitation Limits

To prevent precipitation of pure elements:

$$\Delta \mu_B \le 0$$
 (B-rich limit) (20)

$$\Delta\mu_O \le 0$$
 (O-rich limit) (21)

9.2 Bulk Stability Constraint

From the elimination of μ_A (Eq. 3), the condition $\mu_A \leq E_A^{\text{bulk}}$ (to prevent A precipitation) gives:

$$\frac{1}{x} \left[E_{A_x B_y O_z}^{\text{bulk}} - y \mu_B - z \mu_O \right] \le E_A^{\text{bulk}} \tag{22}$$

Rearranging and using the definitions of relative chemical potentials:

$$y\Delta\mu_B + z\Delta\mu_O \ge \Delta E_f(A_x B_y O_z) \tag{23}$$

This defines the B-poor, O-poor limit.

9.3 Binary Oxide Competition

The ternary oxide must also be stable against decomposition into binary oxides. For example:

$$p\Delta\mu_B + q\Delta\mu_O \le \Delta E_f(B_pO_q)$$
 (for competing B_pO_q) (24)

$$r\Delta\mu_A + s\Delta\mu_O \le \Delta E_f(A_rO_s)$$
 (for competing A_rO_s) (25)

Note that for Eq. 25, we need to express $\Delta \mu_A$ in terms of $\Delta \mu_B$ and $\Delta \mu_O$ using the bulk equilibrium condition.

10 Comparison with Standard A-Based Formulation

10.1 Standard Formulation (A as independent)

In the standard formulation where A is the independent variable and B is eliminated:

$$\gamma(\Delta\mu_A, \Delta\mu_O) = \phi_A - \Gamma_A \Delta\mu_A - \Gamma_O^{(A)} \Delta\mu_O \tag{26}$$

with:

$$\Gamma_A = \frac{1}{2A} \left(\frac{N_B x}{y} - N_A \right) \tag{27}$$

$$\Gamma_O^{(A)} = \frac{1}{2A} \left(\frac{N_B z}{y} - N_O \right) \tag{28}$$

10.2 Current Formulation (B as independent)

In our new formulation:

$$\gamma(\Delta\mu_B, \Delta\mu_O) = \phi_B - \Gamma_B \Delta\mu_B - \Gamma_O^{(B)} \Delta\mu_O \tag{29}$$

with:

$$\Gamma_B = \frac{1}{2A} \left(\frac{N_A y}{x} - N_B \right) \tag{30}$$

$$\Gamma_O^{(B)} = \frac{1}{2A} \left(\frac{N_A z}{x} - N_O \right) \tag{31}$$

10.3 Relation Between Formulations

Both formulations describe the same physical surface and must give identical surface energies for equivalent thermodynamic conditions. The chemical potentials are related through the bulk equilibrium condition:

$$x\Delta\mu_A + y\Delta\mu_B + z\Delta\mu_O = \Delta E_f(A_x B_y O_z) \tag{32}$$

This allows conversion between $(\Delta \mu_A, \Delta \mu_O)$ and $(\Delta \mu_B, \Delta \mu_O)$ coordinate systems.

11 Application to Ag₃PO₄

For the specific case of Ag_3PO_4 (x = 3, y = 1, z = 4):

- Element A = Ag (silver)
- Element B = P (phosphorus)
- Element O = O (oxygen)

11.1 Surface Excesses

$$\Gamma_P = \frac{1}{2A} \left(\frac{N_{Ag}}{3} - N_P \right) \tag{33}$$

$$\Gamma_O = \frac{1}{2A} \left(\frac{4N_{Ag}}{3} - N_O \right) \tag{34}$$

11.2 Surface Energy

$$\gamma(\Delta\mu_P, \Delta\mu_O) = \phi - \Gamma_P \Delta\mu_P - \Gamma_O \Delta\mu_O \tag{35}$$

11.3 Chemical Potential Limits

$$\Delta \mu_P \le 0 \tag{36}$$

$$\Delta\mu_O \le 0 \tag{37}$$

$$\Delta\mu_P + 4\Delta\mu_O \ge \Delta E_f(\text{Ag}_3\text{PO}_4) \tag{38}$$

Plus constraints from competing binary oxides:

$$\Delta\mu_P + \frac{5}{2}\Delta\mu_O \le \Delta E_f(P_2O_5)/2 \tag{39}$$

$$2\Delta\mu_{Ag} + \Delta\mu_O \le \Delta E_f(Ag_2O) \tag{40}$$

where $\Delta \mu_{Ag}$ must be expressed in terms of $\Delta \mu_P$ and $\Delta \mu_O$ using:

$$3\Delta\mu_{Ag} = \Delta E_f(Ag_3PO_4) - \Delta\mu_P - 4\Delta\mu_O \tag{41}$$

12 Implementation Notes

To implement this B-based formulation in the code:

- 1. Identify elements A, B, and O from the bulk structure
- 2. Choose B as the independent variable (instead of A)
- 3. Calculate Γ_B and Γ_O using $N_B^{\rm stoich} = N_A y/x$
- 4. Compute ϕ using Eq. 19
- 5. Define the stability region in $(\Delta \mu_B, \Delta \mu_O)$ space
- 6. Calculate $\gamma(\Delta\mu_B, \Delta\mu_O)$ on a 2D grid

The key difference from the standard implementation is simply swapping which element is treated as independent (the "M" element) versus which is used as reference (the "N" element) before applying the same mathematical framework.