

# The surface finite element method for pattern formation on evolving biological surfaces

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In this article we propose models and a numerical method for pattern formation on evolving curved surfaces. We formulate reaction-diffusion equations on evolving surfaces using the material transport formula, surface gradients and diffusive conservation laws. The evolution of the surface is defined by a material surface velocity. The numerical method is based on the evolving surface finite element method. The key idea is based on the approximation of  $S$  by a triangulated surface  $S_h$  consisting of a union of triangles with vertices on  $S$ . A finite element space of functions is then defined by taking the continuous functions on  $S_h$  which are linear affine on each simplex of the polygonal surface.

## 1. Surface gradients

We assume that  $S$  is a  $C^2$ -hyper-surface which is the zero level set of a signed distance function  $d(x)$  defined on an open subset  $\mathcal{U} \subset \mathbb{R}^3$ .  $\mathbf{n}(x) = \nabla d(x)$  is then unit outward pointing normal on  $S$ . We define the tangential gradient of a function  $\eta$  by

$$\nabla_S v = \nabla v - (\nabla v \cdot \mathbf{n})\mathbf{n} \quad x \in S$$

where  $\nabla$  denotes the usual gradient in  $\mathbb{R}^3$ .

The Laplace-Beltrami operator on  $S$  is defined as the tangential divergence of the tangential gradient:

$$\Delta_S v = \nabla_S \cdot (\nabla_S v) = \Delta v - (\nabla v \cdot \mathbf{n})(\nabla \cdot \mathbf{n}) - \mathbf{n}^t \nabla^2 v \mathbf{n}$$

where  $\nabla^2 v$  is the Hessian matrix of  $v$ .

Let  $S$  have a boundary  $\partial S$  whose intrinsic unit outer normal, tangential to  $S$ , is denoted by  $\boldsymbol{\nu}$ . Then, the formula for integration by parts on  $S$  is

$$\int_S \nabla_S v = - \int_S v H \mathbf{n} + \int_{\partial S} v \boldsymbol{\nu}$$

where  $H$  denotes the mean curvature of  $S$  with respect to  $\mathbf{n}$ , which is given by

$$H = -\nabla_S \cdot \mathbf{n}$$

Green's formula on the surface  $S$  is

$$\int_S \nabla_S u \cdot \nabla_S v = \int_{\partial S} u \nabla_S v \cdot \boldsymbol{\nu} - \int_S u \Delta_S v.$$

## 2. Reaction-diffusion systems on evolving surfaces

Let  $S(t)$  be an evolving two-dimensional hypersurface in  $\mathbb{R}^3$  bounding a time-dependent domain  $\Omega(t)$ . Let the velocity of material points on  $S(t)$  be denoted by  $\mathbf{v} := V\mathbf{n} + \mathbf{v}_T$  where  $\mathbf{n}$  is the unit outward pointing normal to  $\Omega(t)$ ,  $V$  is the normal velocity and  $\mathbf{v}_T$  is a velocity field tangential to the surface. Let  $\mathbf{u}$  be a vector of scalar concentration fields  $\{u_i\}_{i=1}^m$ . Let  $\mathcal{R}(t)$  be an arbitrary material portion of  $S(t)$  where each point moves with the material velocity. According to the mass balance conservation law:

$$\frac{d}{dt} \int_{\mathcal{R}(t)} u_i = - \int_{\partial\mathcal{R}(t)} \mathbf{q}_i \cdot \boldsymbol{\nu} + \int_{\mathcal{R}(t)} f_i(\mathbf{u}) \quad (1)$$

where, for each component  $i$ ,  $\mathbf{q}_i$  and  $f_i(\mathbf{u})$  are respectively, the surface flux through the boundary of  $\mathcal{R}(t)$  and the net production rate within the surface.

The components of  $\mathbf{q}$  normal to  $S$  do not contribute to the flux so we can assume  $\mathbf{q}$  is a tangent vector. Using integration by parts it follows that

$$\int_{\partial\mathcal{R}(t)} \mathbf{q} \cdot \mathbf{n} = \int_{\mathcal{R}(t)} \nabla_S \cdot \mathbf{q} + \int_{\mathcal{R}(t)} \mathbf{q} \cdot \mathbf{n} H = \int_{\mathcal{R}(t)} \nabla_S \cdot \mathbf{q}$$

On the other hand, for the left-hand side of (1), we use the transport formula

$$\frac{d}{dt} \int_{\mathcal{R}(t)} \eta = \int_{\mathcal{R}(t)} \partial \bullet \eta + \eta \nabla_S \cdot \mathbf{v}$$

for any material region of the surface evolving with the material velocity  $\mathbf{v}$  where

$$\partial \bullet \eta := \eta_t + \mathbf{v} \cdot \nabla \eta \quad (2)$$

denotes the material derivative.

Combining the two equations results in

$$\int_{\mathcal{R}(t)} \partial \bullet u_i + u_i \nabla_S \cdot \mathbf{v} + \nabla_S \cdot \mathbf{q}_i = \int_{\mathcal{R}(t)} f_i(\mathbf{u})$$

Since  $\mathcal{R}(t)$  is arbitrary for all time  $t$ , we conclude that

$$\partial \bullet u_i + u_i \nabla_S \cdot \mathbf{v} + \nabla_S \cdot \mathbf{q}_i = f_i(\mathbf{u}) \quad (3)$$

For the constitutive law relating the flux to the concentrations, assuming no cross-diffusion between the chemical species, we set  $\mathcal{D}$  to be a diffusivity tensor (a diagonal matrix diffusion coefficients) and assume that the chemical species diffuse according to Fick's law

$$\mathbf{q}_i = -\mathcal{D}_{ij} \nabla_S u_j \quad (4)$$

where  $\mathcal{D}_{ij} = d_i \delta_{ij}$ , with  $\delta_{ij}$  representing the usual Kronecker delta function.

Then (3) becomes

$$\partial \bullet u_i + u_i \nabla_S \cdot \mathbf{v} = \nabla_S (\mathcal{D}_{ij} \nabla_S u_j) + f_i(\mathbf{u}) \quad \text{on} \quad S(t)$$

In vector form, the system of reaction-diffusion equations on an evolving surface  $S(t)$  takes the form

$$\partial \bullet \mathbf{u} + \mathbf{u} \nabla_S \cdot \mathbf{v} = D \Delta_S \mathbf{u} + \mathbf{f}(\mathbf{u}) \quad (5)$$

where  $D = \text{diag}(d_i)$ . This system is supplemented with zero-flux boundary conditions if the boundary of  $S(t)$  is non-empty and the initial conditions

$$\mathbf{u}(\cdot, 0) = \mathbf{u}_0(\cdot) \quad \text{on} \quad S(0) \quad (6)$$

where the components of  $\mathbf{u}_0(\cdot)$  are prescribed positive bounded functions.



### 3. Surface finite element method

#### 3.1 Variational formulation

For an arbitrary  $i$

$$\partial \bullet u_i + u_i \nabla_S \cdot \mathbf{v} = d_i \Delta_S u_i + f_i(\mathbf{u}) \quad (7)$$

Let  $\varphi(\cdot, t) \in H^1(S(t))$  be a test function. Multiplying (7) by  $\varphi$  and integrating over  $S(t)$  leads to

$$\begin{aligned} \int_{S(t)} f_i(\mathbf{u}) \varphi &= \int_{S(t)} \partial \bullet u_i \varphi + u_i \varphi \nabla_S \cdot \mathbf{v} - d_i \int_{S(t)} \varphi \Delta_S u_i \\ &= \int_{S(t)} \partial \bullet u_i \varphi + u_i \varphi \nabla_S \cdot \mathbf{v} + d_i \int_{S(t)} \nabla_S u_i \cdot \nabla_S \varphi \\ &\quad - \int_{\partial S(t)} \varphi \nabla_S u_i \cdot \boldsymbol{\nu}. \end{aligned} \quad (8)$$

The last term vanishes if  $\partial S(t) = \emptyset$  or  $\partial S(t) \neq \emptyset$  but  $\varphi = 0$  or  $\nabla_S u_i \cdot \boldsymbol{\nu} = 0$  on  $\partial S(t)$ . Hence, assuming any of these conditions holds we have

$$\begin{aligned}
 \int_{S(t)} f_i(\mathbf{u})\varphi &= \int_{S(t)} \partial \bullet u_i \varphi + u_i \varphi \nabla_S \cdot \mathbf{v} + d_i \int_{S(t)} \nabla_S u_i \cdot \nabla_S \varphi \\
 &= \int_{S(t)} \partial \bullet (u_i \varphi) - u_i \partial \bullet \varphi + u_i \varphi \nabla_S \cdot \mathbf{v} + d_i \int_{S(t)} \nabla_S u_i \cdot \nabla_S \varphi \\
 &= \frac{d}{dt} \int_{S(t)} u_i \varphi - \int_{S(t)} u_i \partial \bullet \varphi + d_i \int_{S(t)} \nabla_S u_i \cdot \nabla_S \varphi \quad (9)
 \end{aligned}$$

The variational form seeks to find  $u_i \in H^1(S(t))$  satisfying

$$\begin{aligned}
 &\frac{d}{dt} \int_{S(t)} u_i \varphi - \int_{S(t)} u_i \partial \bullet \varphi + d_i \int_{S(t)} \nabla_S u_i \cdot \nabla_S \varphi \\
 &= \int_{S(t)} f_i(\mathbf{u})\varphi, \quad \forall \varphi \in H^1(S(t)) \quad (10)
 \end{aligned}$$

### 3.2 Evolving surface finite element method

We approximate  $S(t)$  by  $S_h(t)$ , a triangulated surface whose vertices lie on  $S(t)$ , *i. e.*  $S_h(t) = \mathcal{T}_h(t) = \bigcup_k T_k(t)$ , where each  $T_k(t)$  is a triangle. The diameter of the largest triangle in the initial surface is denoted by  $h$ . We choose the vertices of the triangulation to evolve with the material velocity so that

$$\dot{X}_j(t) = \mathbf{v}(X_j(t), t) \quad (11)$$

and it is easy to see that  $X_j(t)$  lies on  $S(t)$  if  $\mathbf{v}$  is the exact material velocity. We assume  $S_h(t)$  is smooth in time. For each  $t$  we define a finite element space

$$S_h(t) = \left\{ \phi \in C^0(S_h(t)) : \phi \Big|_{T_k} \text{ is linear affine for each } T_k \in \mathcal{T}_k(t) \right\}.$$

For each  $t \in [0, T]$  we denote by  $\left\{ \chi_j(\cdot, t)_{j=1}^N \right\}$  the moving nodal basis functions and by  $X_j(t)$ ,  $j = 1, \dots, N$  the nodes. These functions will satisfy

$$\chi_j(\cdot, t) \in C^0(S_h(t)), \quad \chi_j(X_i(t), t) = \delta_{ij}, \quad \chi_j(\cdot, t) \Big|_{T_k} \text{ is linear affine}$$

and on  $T_k \in \mathcal{T}_h(t)$

$$\chi_j \Big|_e = \lambda_k, \quad \text{for each } e \in \mathcal{T}_h(t)$$

where  $k = k(T_k, j)$  and  $(\lambda_1, \lambda_2, \lambda_3)$  are the barycentric coordinates. On  $S_h(t)$  we define the discrete material velocity

$$\mathbf{v}_h = \sum_{j=1}^N \dot{X}_j(t) \chi_j \quad (12)$$

and the discrete material derivative

$$\partial_h \bullet \phi = \phi_t + \mathbf{v}_h \cdot \nabla \phi \quad (13)$$

We seek approximations  $U_i(\cdot, t) \in S_h(t)$  to  $u_i$ . Since  $\left\{ \chi_j(\cdot, t)_{j=1}^N \right\}$  is the basis of  $S_h(t)$  we know for each  $U_i(\cdot, t) \in S_h(t)$  and each  $t \in [0, T]$  that there exist unique  $\alpha_i = \left\{ \alpha_i^1(t), \dots, \alpha_i^N(t) \right\}$  satisfying

$$U_i(\cdot, t) = \sum_{j=1}^N \alpha_i^j(t) \chi_j(\cdot, t).$$

Substituting  $U_i(\cdot, t)$ ,  $S_h(t)$  and  $\phi \in S_h(t)$  for  $u_i$ ,  $S(t)$  and  $\varphi$  in (10) we obtain

$$\begin{aligned} & \frac{d}{dt} \int_{S_h(t)} \sum_{j=1}^N \alpha_i^j(t) \chi_j \phi - \int_{S_h(t)} \sum_{j=1}^N \alpha_i^j(t) \chi_j \partial_h \bullet \phi \\ & + d_i \int_{S_h(t)} \sum_{j=1}^N \alpha_i^j(t) \nabla_{S_h(t)} \chi_j \cdot \nabla_{S_h(t)} \phi = \int_{S_h(t)} f_i \phi, \end{aligned} \quad (14)$$

for all  $\phi \in S_h(t)$  and taking  $\phi = \chi_k, k = 1, \dots, N$  and using the transport property of the basis functions we obtain

$$\frac{d}{dt}(\mathcal{M}(t)\boldsymbol{\alpha}_i) + d_i\mathcal{S}(t)\boldsymbol{\alpha}_i = \mathbf{F}_i(t) \quad (15)$$

where  $\mathcal{M}(t)$  is the evolving mass matrix

$$\mathcal{M}(t)_{jk} = \int_{S_h(t)} \chi_j \chi_k$$

$\mathcal{S}(t)$  is the evolving stiffness matrix

$$\mathcal{S}(t)_{jk} = \int_{S_h(t)} \nabla_{S_h} \chi_j \cdot \nabla_{S_h} \chi_k$$

and  $\mathbf{F}_i$  is the right hand side  $\mathbf{F}_{ij} = \int_{S_h(t)} f_i(\mathbf{U}) \phi_j$

## 4. Time discretization

For simplicity we restrict the description to the two components system  $\mathbf{u} = (u, w)$  with kinetics given by

$$\mathbf{f}(\mathbf{u}) = (f_1, f_2)^T = (\gamma(a - u + u^2 w), \gamma(b - u^2 w))^T$$

and  $d_1 = 1, d_2 = d$ . We discretise in time using a uniform time step  $\tau$ . We represent by  $(U^n, W^n)$  the solution at time  $n\tau$ . Let  $U^0, W^0 \in S_h(0)$  be given. For  $n = 0, \dots, n_T$ , solve the nonlinear system

$$\begin{cases} \frac{1}{\tau} \int_{S_h^{n+1}} U^{n+1} \chi_j^{n+1} + \int_{S_h^{n+1}} \nabla_{S_h^n} U^{n+1} \cdot \nabla_{S_h^n} \chi_j^{n+1} \\ = \frac{1}{\tau} \int_{S_h^n} U^n \chi_j^n + \int_{S_h^{n+1}} f_1(U^{n+1}, W^{n+1}) \chi_j^{n+1} \\ \frac{1}{\tau} \int_{S_h^{n+1}} W^{n+1} \chi_j^{n+1} + d \int_{S_h^{n+1}} \nabla_{S_h^n} W^{n+1} \cdot \nabla_{S_h^n} \chi_j^{n+1} \\ = \frac{1}{\tau} \int_{S_h^n} W^n \chi_j^n + \int_{S_h^{n+1}} f_2(U^{n+1}, W^{n+1}) \chi_j^{n+1} \end{cases}$$

For all  $j = 1, \dots, N$ . To linearise  $f_1(U^{n+1}, W^{n+1})$  we assume slow deformation of the evolving surface which allows us to write  $(U^{n+1})^2 \approx U^n U^{n+1}$  (Madzvamuse 2006).

Using this linearisation, we can derive the following fully discrete algorithm:

Let  $U^0, W^0 \in S_h(0)$  be given. For  $n = 0, \dots, n_T$ , solve the linear system

$$\begin{cases} \left( \frac{1}{\tau} + \gamma \right) \int_{S_h^{n+1}} U^{n+1} \chi_j^{n+1} + \int_{S_h^{n+1}} \nabla_{S_h^n} U^{n+1} \cdot \nabla_{S_h^n} \chi_j^{n+1} \\ - \gamma \int_{S_h^{n+1}} U^n W^n U^{n+1} \chi_j^{n+1} = \frac{1}{\tau} \int_{S_h^n} U^n \chi_j^n + \gamma a \int_{S_h^n} \chi_j^n \\ \frac{1}{\tau} \int_{S_h^{n+1}} W^{n+1} \chi_j^{n+1} + d \int_{S_h^{n+1}} \nabla_{S_h^n} W^{n+1} \cdot \nabla_{S_h^n} \chi_j^{n+1} \\ + \gamma \int_{S_h^{n+1}} (U^{n+1})^2 W^{n+1} \chi_j^{n+1} = \frac{1}{\tau} \int_{S_h^n} W^n \chi_j^n + \gamma b \int_{S_h^n} \chi_j^n \end{cases}$$



For all  $j = 1, \dots, N$ . Using a matrix representation we have

$$\begin{cases} \left( \left( \frac{1}{\tau} + \gamma \right) \mathcal{M}^{n+1} + \mathcal{S}^{n+1} - \gamma \mathcal{M}_1^{n+1} \right) \mathbf{U}^{n+1} = \frac{1}{\tau} \mathcal{M}^n \mathbf{U}^n + \mathbf{F}_1^n \\ \left( \frac{1}{\tau} \mathcal{M}^{n+1} + d \mathcal{S}^{n+1} + \gamma \mathcal{M}_2^{n+1} \right) \mathbf{W}^{n+1} = \frac{1}{\tau} \mathcal{M}^n \mathbf{W}^n + \mathbf{F}_2^n \end{cases}$$

with

$$\mathcal{M}_{ij}^n = \int_{S_h^n} \chi_i^n \chi_j^n, \quad \mathcal{M}_{1ij}^n = \int_{S_h^n} U^n W^n \chi_i^n \chi_j^n, \quad \mathcal{M}_{2ij}^n = \int_{S_h^n} (U^{n+1})^2 \chi_i^n \chi_j^n,$$

$$\mathcal{S}_{ij}^n = \int_{S_h^n} \nabla_{S_h^n} \chi_i^n \cdot \nabla_{S_h^n} \chi_j^n, \quad \mathbf{F}_{1i}^n = \gamma a \int_{S_h^n} \chi_i^n, \quad \mathbf{F}_{2i}^n = \gamma b \int_{S_h^n} \chi_i^n$$