

CAN207 Continuous and Discrete Time Signals and Systems

Lecture-12

Solving Differential Equations and Block Diagram

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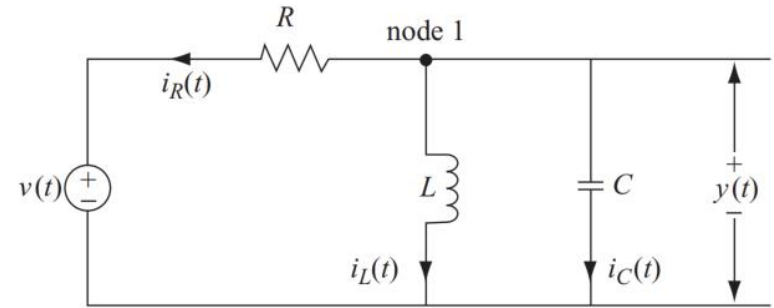
Room EE322

Content

- 1. Examples of LCCDE
 - CT examples
 - DT examples
- 2. Solving LCCDE
 - Zero-input and Zero-state response
 - Decomposing the whole response
- 3. Block diagrams of causal LTI systems
 - Block diagrams - fundamental blocks
 - Direct form I and II
 - Horizontal block diagrams (optional)

1.1 Differential equations for CT systems

- A simple electrical circuit
 - Passive components: R, L and C
 - Input: voltage signal $v(t)$
 - Output: voltage on capacitor $y(t)$



- Mathematical model

- Currents on 3 branches are:
$$i_R = \frac{y(t) - v(t)}{R}$$
$$i_L = \frac{1}{L} \int_{-\infty}^t y(\tau) d\tau$$

$$i_C = C \frac{dy}{dt}.$$

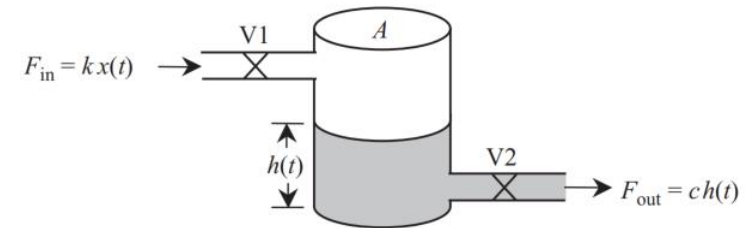
- Apply the Kurchhoff's current law:
$$\frac{y(t) - v(t)}{R} + \frac{1}{L} \int_{-\infty}^t y(\tau) d\tau + C \frac{dy}{dt} = 0,$$

- Take derivative on both sides, get:
$$\frac{d^2 y}{dt^2} + \frac{1}{RC} \frac{dy}{dt} + \frac{1}{LC} y(t) = \frac{1}{RC} \frac{dv}{dt}.$$



1.1 Differential equations for CT systems

- A mechanical water pump
 - Input: rate of flow $F_{in} = k x(t)$
 - Output: outlet flow rate $F_{out} = c h(t)$
 - Total volume of the water inside the tank is $V(t) = A h(t)$



k is the linearity constant;
 $x(t)$ is the controlling voltage;
 c is the outlet flow constant;
 $h(t)$ is the height of water level.

- Mathematical model
 - the rate of change in the volume of the stored water:

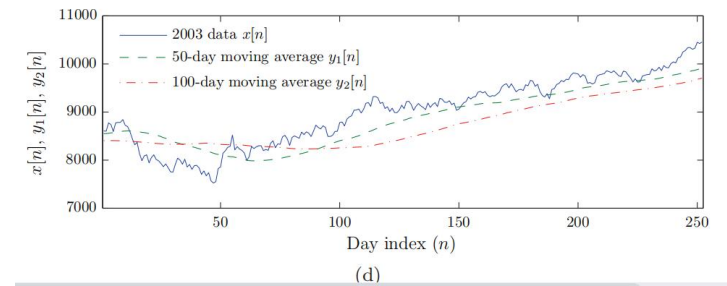
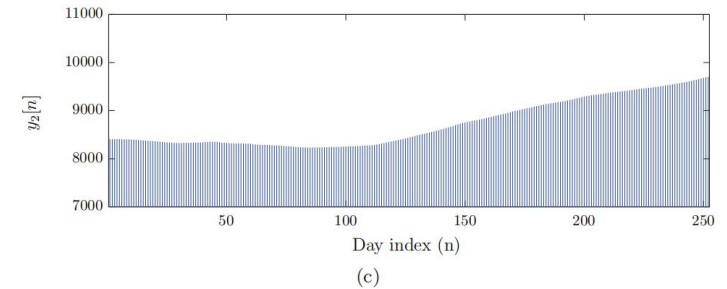
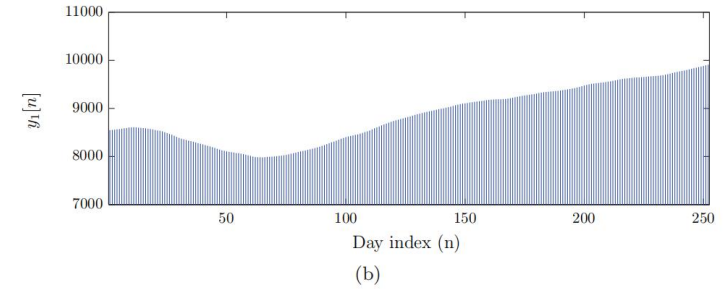
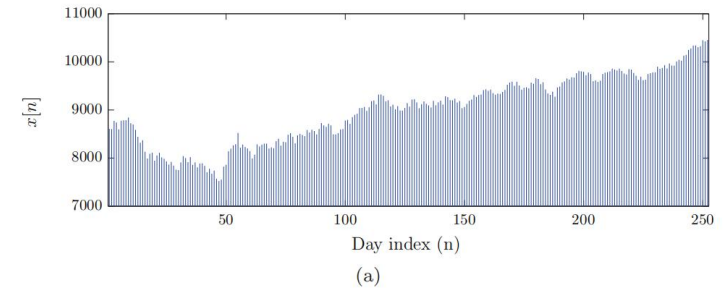
$$\frac{dV}{dt} = F_{in} - F_{out} = kx(t) - ch(t).$$

- Expressing $V(t)$ as the product of the cross-sectional area A of the water tank and the height $h(t)$ of the water yields:

$$A \frac{dh}{dt} + ch(t) = kx(t),$$

1.2 Difference equations for DT systems

- A moving average filter
 - Input: a sequence of numbers (such as data from stock market)
 - Output: a sequence of average values of M adjacent numbers.
- Mathematical model
 - Taking average: $y[n] = \frac{1}{M} \sum_{k=0}^{M-1} x(n-k)$



1.2 Difference equations for DT systems

- A spatial averaging filter
 - Input: a 2D array $x[m, n]$ is the intensity of a monochrome image
 - Output: a 2D array $y[m, n]$ is the averaged intensity of every pixel
 - Mathematical model
 - a weighted average of the intensities of the pixels in the neighborhood
- $$y[m, n] = \frac{1}{4}(x[m, n] + x[m, n - 1] + x[m - 1, n] + x[m - 1, n - 1])$$



Original Image



Filtered Image



1.3 Summary

- Linear Constant-Coefficient Differential Equation

$$\sum_{k=0}^N a_k \frac{d^k y(t)}{dt^k} = \sum_{k=0}^M b_k \frac{d^k x(t)}{dt^k}$$

- Linear Constant-Coefficient Difference Equation

$$\sum_{k=0}^N a_k y[n - k] = \sum_{k=0}^M b_k x[n - k]$$

2.1 Differential equations

- N^{th} order differential equation

$$\sum_{k=0}^N a_k \frac{d^k y(t)}{dt^k} = \sum_{k=0}^M b_k \frac{d^k x(t)}{dt^k} \quad \dots\dots \quad (1)$$

- A more compact representation: denoting $\frac{d}{dt}$ by D :

$$\begin{aligned} & a_N D^N y(t) + a_{N-1} D^{N-1} y(t) + \dots + a_1 D y(t) + a_0 y(t) \\ &= b_M D^M x(t) + b_{M-1} D^{M-1} x(t) + \dots + b_1 D x(t) + b_0 x(t) \end{aligned}$$

- D is the differential operator, so it can be written as:

$$\underbrace{(a_N D^N + a_{N-1} D^{N-1} + \dots + a_0)}_{Q(D)} y(t) = \underbrace{(b_M D^M + b_{M-1} D^{M-1} + \dots + b_0)}_{P(D)} x(t)$$

- or simply $Q(D)y(t) = P(D)x(t) \quad \dots\dots \quad (2)$

– where $Q(D)$ is the N^{th} -order differential operator, $P(D)$ is the M^{th} -order differential operator, and the a_k and b_k are constants.

2.1 Solving differential equations

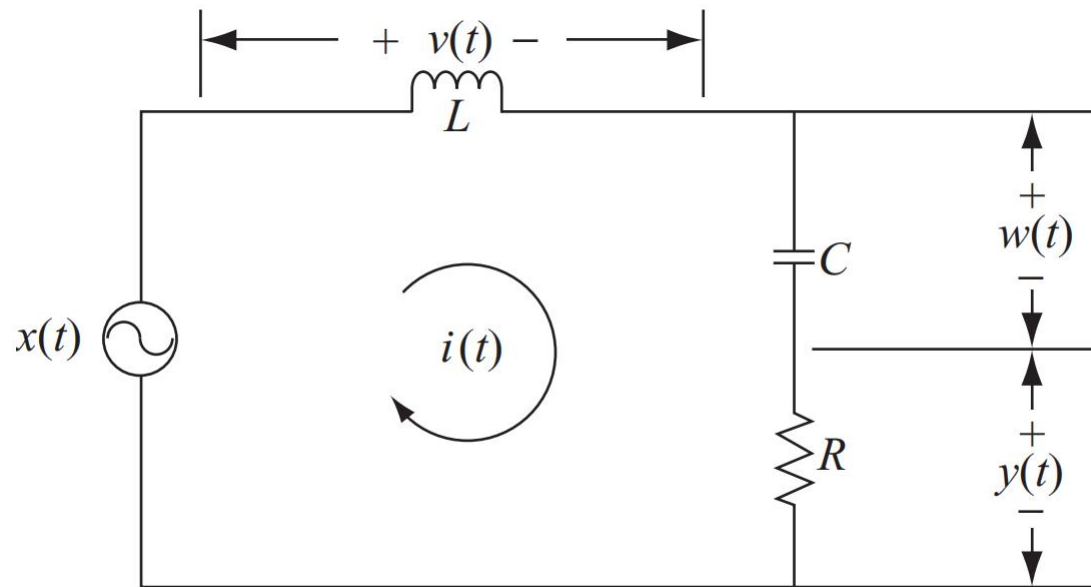
- Output $y(t)$ has two components:

$$y(t) = y_{zi}(t) + y_{zs}(t)$$

- $y_{zi}(t)$: *zero-input response* of the system
 - the response produced by the system because of **the initial conditions** (and not due to any external input);
 - evaluated by solving a homogeneous equation $Q(D)y(t) = 0$;
 - decays to zero as $t \rightarrow \infty$.
- $y_{zs}(t)$: *zero-state response* of the system
 - arises due to **the input signal** (and doesn't depend on the initial states of the system);
 - evaluated by assuming the initial states of the system to be zero;
 - defines the steady-state value of the output.

2.1 Solving differential equations - example 1

- Consider the RLC series circuit shown below. Assume that the inductance $L = 0$ H (i.e. the inductor does not exist in the circuit), resistance $R = 5 \Omega$, and capacitance $C = 1/20$ F.
- Determine the output signal $y(t)$ when the input voltage is given by $x(t) = \sin(2t)$ and the initial voltage $y(0^-) = 2$ V across the resistor.



2.1 Solving differential equations - eg.1 - solution

- Differential equation of this circuit:

$$\frac{dy}{dt} + 4y(t) = \frac{dx}{dt} = 2 \cos(2t) \quad \dots\dots\dots (3)$$

- Zero-input response is obtained by solving

$$\frac{dy}{dt} + 4y(t) = 0$$

- Characteristic equation:

- Assume $y(t) = Ae^{st}$, then $sAe^{st} + 4Ae^{st} = 0$
- $s + 4 = 0$ has a root at $s = -4$.

- The zero-input response is given by $y_{zi}(t) = Ae^{-4t}$, where A is unknown.

- Using initial condition $y(0^-) = Ae^{-4 \cdot 0} = 2$, find $A = 2$.

- So the zero-input response is $y_{zi}(t) = 2e^{-4t}$.

2.1 Solving differential equations - eg.1 - solution

- Zero-state response is obtained by solving equation (3) with a zero initial condition $y(0^-) = 0$.

- The particular component for sinusoidal input is

$$y_{zs}^{(p)}(t) = K_1 \cos(2t) + K_2 \sin(2t)$$

- The homogeneous component is similar

$$y_{zs}^{(h)}(t) = Ce^{-4t}, \text{ where } C \text{ is unknown.}$$

- Substitute $y_{zs}^{(p)}(t)$ into equation (3), get $K_1 = 0.4$ and $K_2 = 0.2$.

- The overall zero-state response:

$$y_{zs}(t) = Ce^{-4t} + 0.4 \cos(2t) + 0.2 \sin(2t)$$

- Using $y(0^-) = 0$, find $C = -0.4$, so

$$y_{zs}(t) = -0.4e^{-4t} + 0.4 \cos(2t) + 0.2 \sin(2t)$$

- Total response

$$y(t) = y_{zi}(t) + y_{zs}(t) = 1.6e^{-4t} + 0.4 \cos(2t) + 0.2 \sin(2t) \quad 12$$

2.1 Differential equations - homogeneous solution

- Homogeneous solution

- “guess” solution of the form $y_h(t) = Ae^{st}$
- Substitute back to the homogeneous equation

$$\sum_{k=0}^N a_k \frac{d^k y(t)}{dt^k} = 0$$

$$\sum_{k=0}^N a_k A s^k e^{st} = 0 \rightarrow N \text{ roots } s_i, i = 1, \dots, N$$

- Characteristic equations:

$$\sum_{k=0}^N a_k s^k = 0, \text{ solved to get } N \text{ values } s_i$$

- Homogeneous solution has the form:

$$y_h(t) = A_1 e^{s_1 t} + A_2 e^{s_2 t} + \dots + A_N e^{s_N t}$$

- Need N initial states to decide the N coefficients A_i

2.1 Differential equations - particular solution

- The zero-state response $y_{zs}(t)$ depends upon the input signal $x(t)$ subject to zero initial conditions.
- The zero-state response consists of two components:

$$y_{zs}(t) = y_{zs}^{(p)}(t) + y_{zs}^{(h)}(t)$$

- the *homogeneous component* $y_{zs}^{(h)}(t)$ is obtained by following the procedure used to solve for the zero-input response but with zero initial conditions.
- the *particular component* $y_{zs}^{(p)}(t)$ is obtained from a look-up table as shown below.
 - The constant C is determined such that $y_{zs}(t)$ satisfies the system's differential equation.

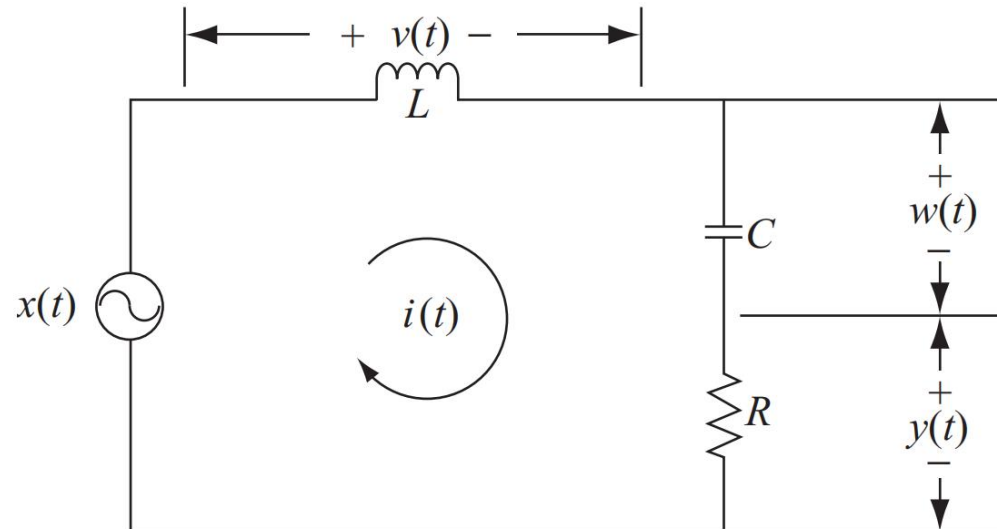
Table C.1. Zero-state response corresponding to common input signals

Input	Particular component of the zero-state response
Impulse function, $K\delta(t)$	$C\delta(t)$
Unit step function, $Ku(t)$	$Cu(t)$
Exponential, Ke^{-at}	Ce^{-at}
Sinusoidal, $A\cos(\omega_0 t + \phi)$	$C_0\cos(\omega_0 t) + C_1\sin(\omega_0 t)$



2.1 Solving differential equations - example 2

- Consider the same electrical circuit as example 1, as shown below. The values of inductance, resistance, and capacitance are set to $L = 1/12\text{H}$, $R = 7/12\Omega$, and $C = 1\text{F}$. The circuit is assumed to be open before $t = 0$, i.e. no current is initially flowing through the circuit. However, the capacitor has an initial charge of 5 V. Determine
 - the zero-input response $w_{zi}(t)$ of the system;
 - the zero-state response $w_{zs}(t)$ of the system;
 - the overall output $w(t)$;
- Notice: the input signal is given by $x(t) = 2e^{-t}u(t)$ and the output $w(t)$ is measured across capacitor C .



2.1 Solving differential equations - eg.2 - solution

- Differential equation of this circuit:

$$\frac{d^2w(t)}{dt^2} + 7\frac{dw(t)}{dt} + 12w(t) = 12x(t)$$

- Zero-input response:
 - using characteristic equation and initial conditions find:

$$w_{zi}(t) = (20e^{-3t} - 15e^{-4t})u(t)$$

- Zero-state response:
 - the homogeneous component is the same form:

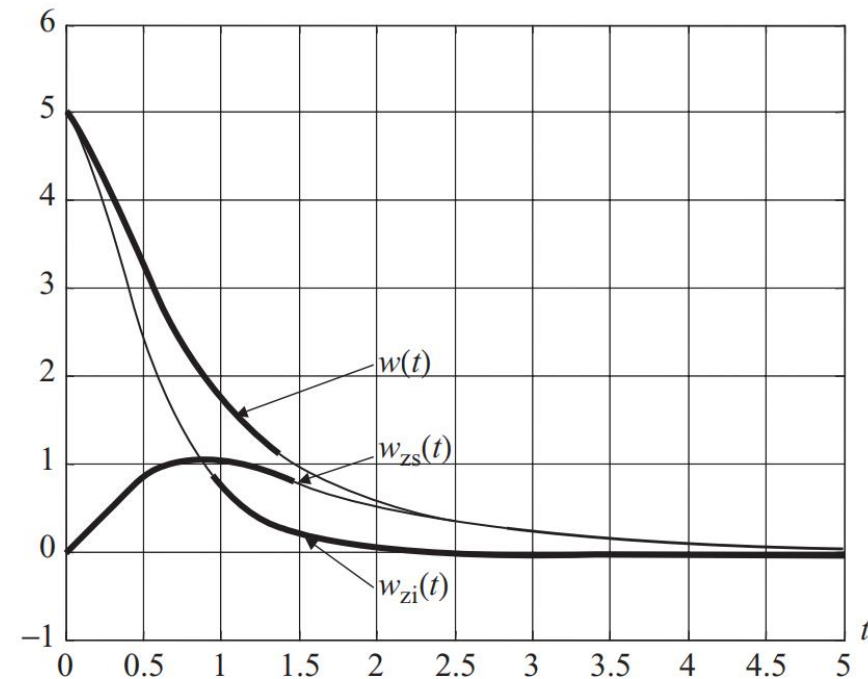
$$w_{zs}^{(h)}(t) = C_1e^{-4t} + C_2e^{-3t}$$

- the particular component for $x(t) = 2e^{-t}u(t)$ is of the form $w_{zs}^{(p)}(t) = Ke^{-t}u(t)$
- substituting back to the equation and using initial conditions to solve for C_1 , C_2 and K

$$w_{zs}(t) = w_{zs}^{(h)}(t) + w_{zs}^{(p)}(t) = (8e^{-4t} - 12e^{-3t} + 4e^{-t})u(t)$$

- The overall response is

$$w(t) = w_{zi}(t) + w_{zs}(t) = (-7e^{-4t} + 8e^{-3t} + 4e^{-t})u(t)$$



2.1 Solving differential equations - example 3

- Notice: change the input to $x(t) = 2(1 - e^{-t})u(t)$.
- Find the overall output $w(t)$.
- Differential equation of this circuit: $\frac{d^2w(t)}{dt^2} + 7\frac{dw(t)}{dt} + 12w(t) = 12x(t)$
- Zero-input response: $w_{zi}(t) = (20e^{-3t} - 15e^{-4t})u(t)$
- Zero-state response:
 - the homogeneous component: $w_{zs}^{(h)}(t) = C_1e^{-4t} + C_2e^{-3t}$
 - the particular component for $x(t) = 2u(t) - 2e^{-t}u(t)$ is of the form
$$w_{zs}^{(p)}(t) = (K_1 + K_2e^{-t})u(t)$$
 - substituting back to the equation and using initial conditions to solve:
$$w_{zs}(t) = w_{zs}^{(h)}(t) + w_{zs}^{(p)}(t) = (2 - 4e^{-t} + 4e^{-3t} - 2e^{-4t})u(t)$$
 - The overall response is
$$w(t) = w_{zi}(t) + w_{zs}(t) = (2 - 4e^{-t} + 24e^{-3t} - 17e^{-4t})u(t)$$

2.2 Decomposing the whole response

- 1. Decomposition 1:
 - Zero-input response $(20e^{-3t} - 15e^{-4t})u(t)$
 - Zero-state response $(2 - 4e^{-t} + 4e^{-3t} - 2e^{-4t})u(t)$
- 2. Decomposition 2:
 - Natural response $(20e^{-3t} - 15e^{-4t} + 4e^{-3t} - 2e^{-4t})u(t)$
 - Forced response $(2 - 4e^{-t})u(t)$
- 3. Decomposition 3:
 - Transient response $(20e^{-3t} - 15e^{-4t} - 4e^{-t} + 4e^{-3t} - 2e^{-4t})u(t)$
 - Steady-state response $2u(t)$

Quiz 1

- A first-order differential equation is given as:

$$\frac{dy(t)}{dt} + 2y(t) = x(t)$$

- where $y(t)$ denotes the output of the system and $x(t)$ is the input.
- Find $y(t)$ when the input signal is $x(t) = Ke^{3t}u(t)$ and initial rest condition with $y(0) = 0$.

Hint:

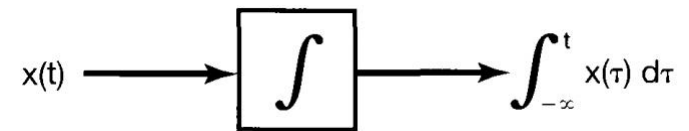
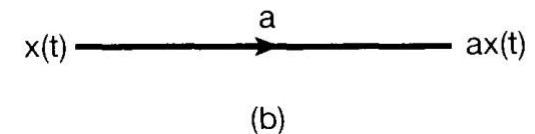
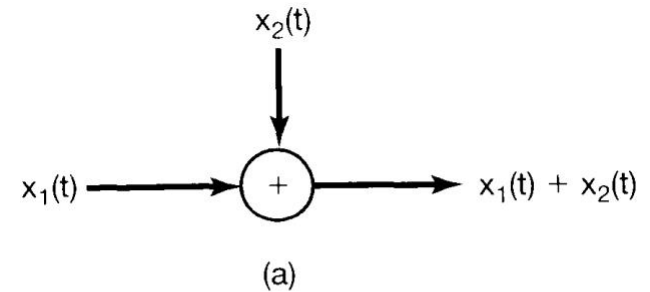
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Unit step function, $Ku(t)$	$Cu(t)$
Exponential, Ke^{-at}	Ce^{-at}
Sinusoidal, $A\cos(\omega_0 t + \phi)$	$C_0\cos(\omega_0 t) + C_1\sin(\omega_0 t)$



3.1 Block diagrams for differential equations

- Systems described by LCCDE can be represented in terms of block diagram interconnections of elementary operations.
- For CT systems, the commonly used elementary building blocks are ***adder***, ***multiplier*** and ***integrator***.
- Example 1: draw the block diagram of the 1st order LCCDE:

$$\frac{dy(t)}{dt} + ay(t) = \frac{dx(t)}{dt} + bx(t)$$



3.2 Direct form I

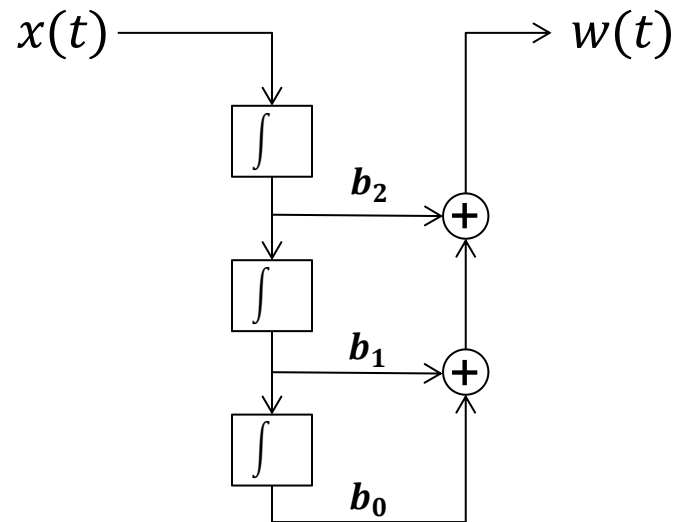
$$\frac{d^3 y}{dt^3} + a_2 \frac{d^2 y}{dt^2} + a_1 \frac{dy}{dt} + a_0 y = b_2 \frac{d^2 x}{dt^2} + b_1 \frac{dx}{dt} + b_0 x$$

- 1. Take 3 integrals on both sides

$$y(t) + a_2 \int y(t)dt + a_1 \iint y(t)dt + a_0 \iiint y(t)dt = b_2 \int x(t)dt + b_1 \iint x(t)dt + b_0 \iiint x(t)dt$$

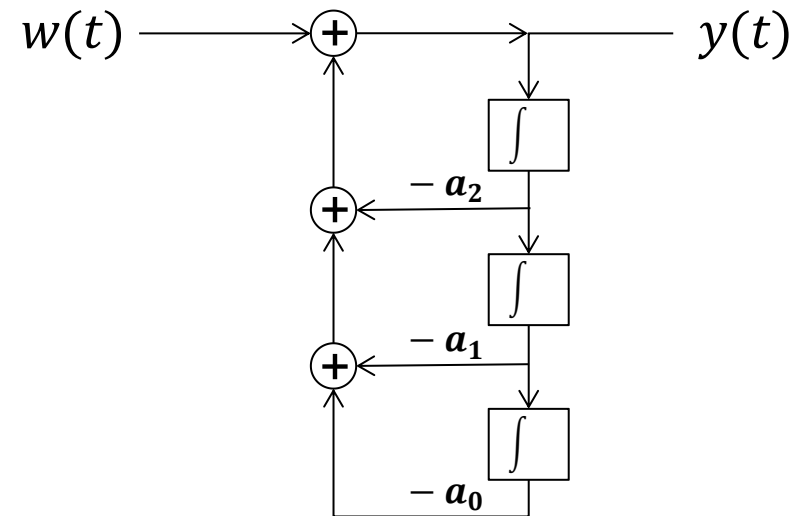
- 2. Draw the input side:

$$w(t) = b_2 \int x + b_1 \iint x + b_0 \iiint x$$

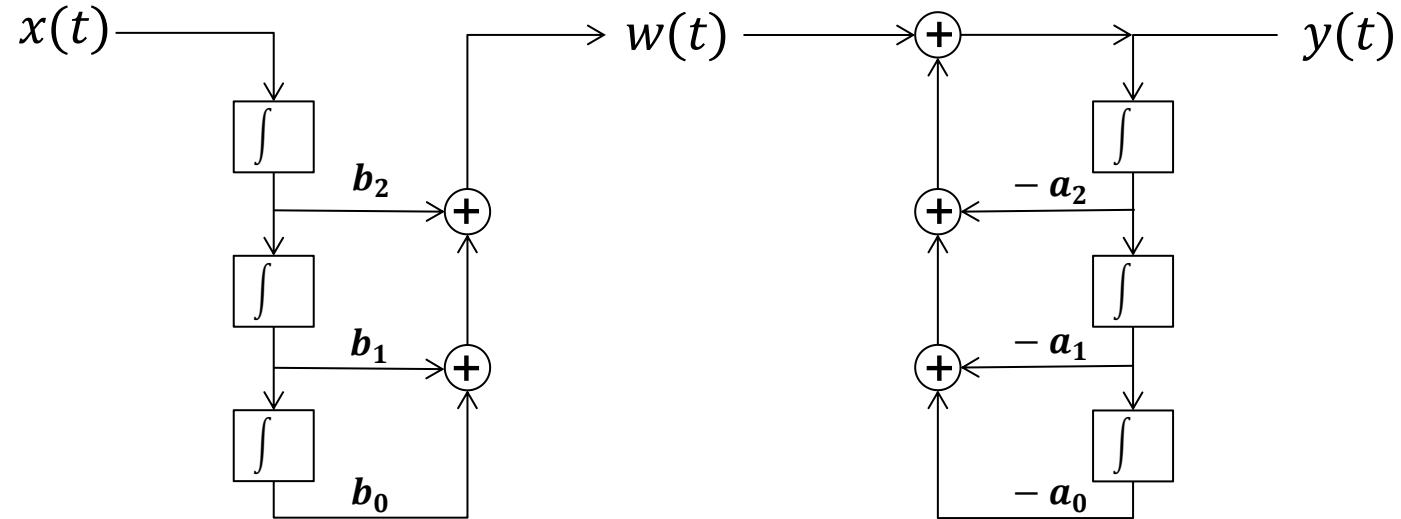


- 3. Draw the output side:

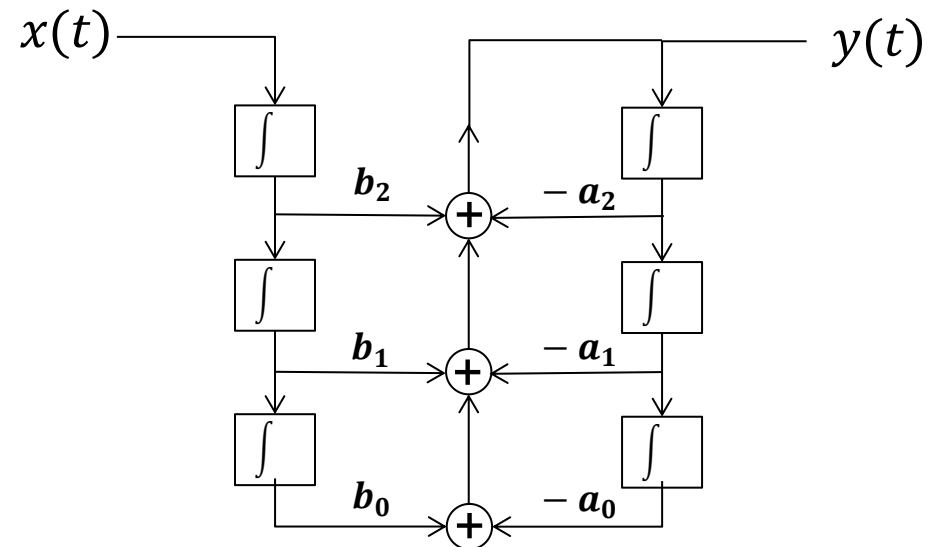
$$w(t) - a_2 \int y - a_1 \iint y - a_0 \iiint y = y(t)$$



- Connect the centre:



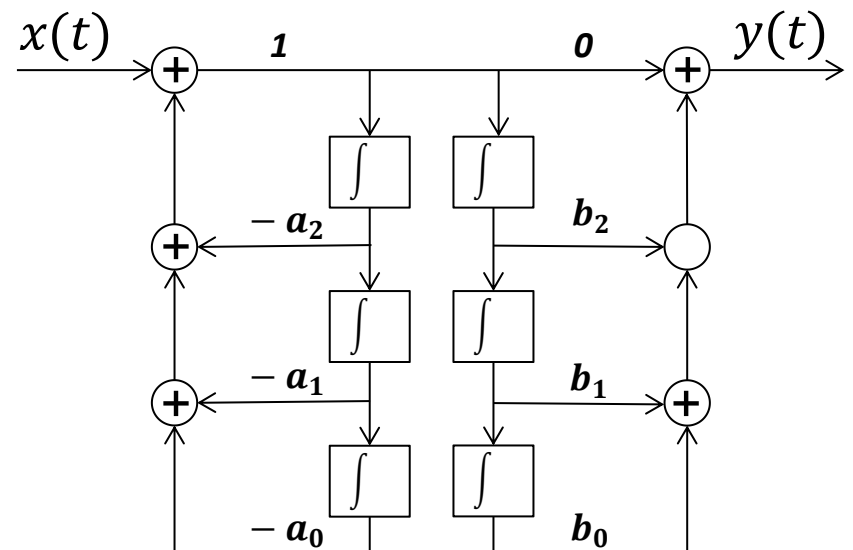
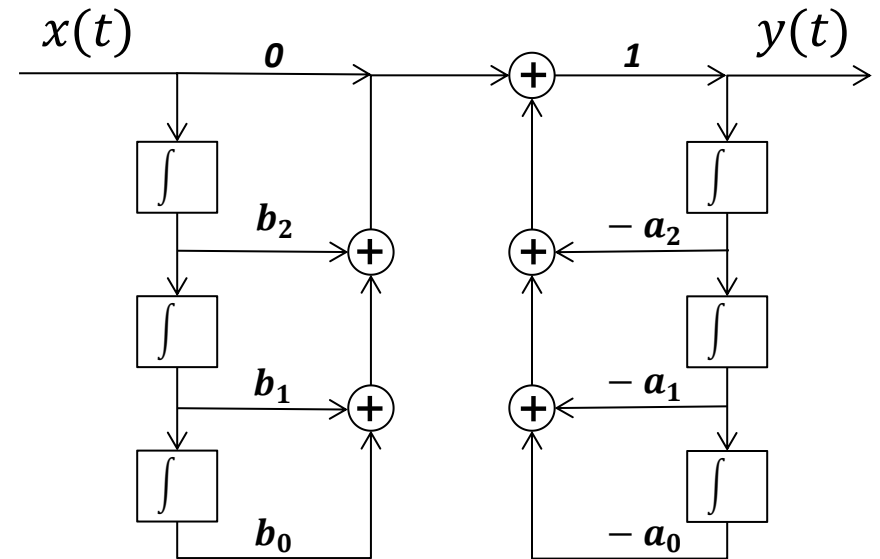
- Combine the common adders:



- This form is often referred to as the *direct form I* implementation $\Rightarrow 2N$ integrators are used.

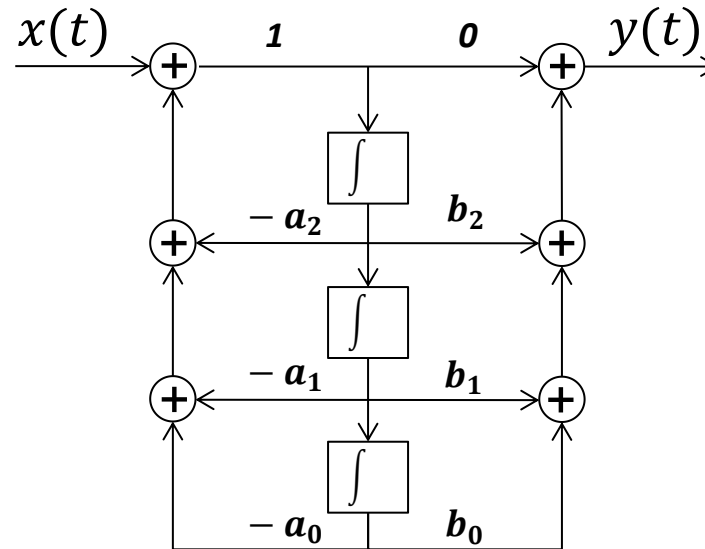
3.2 Direct form II

- To save the usage of integrator:
 - Direct form I:
 - Interchanging the order of the two segments of Direct Form I:



3.2 Direct form II

- Combining the two chains of integrators.



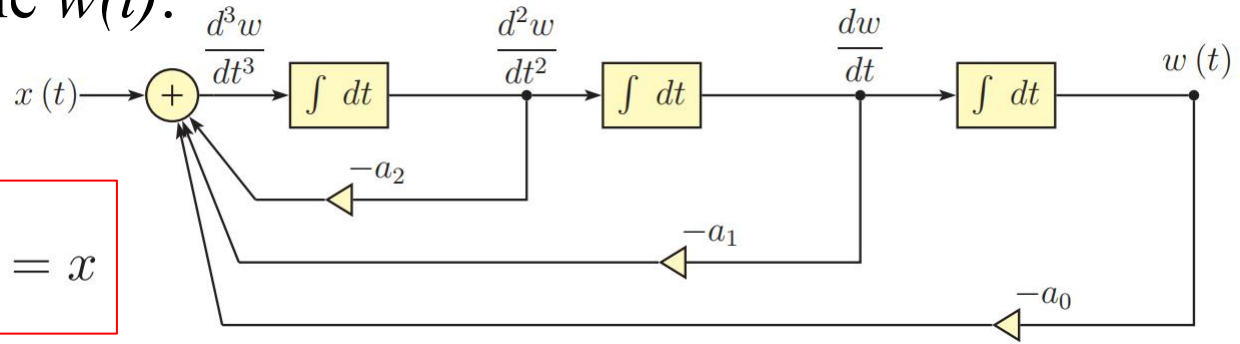
- This form is often referred to as the *direct form II* implementation \Rightarrow **N** integrators are used.
- Direct form II is also called the *Canonic form*.

3.3 Horizontal Block diagrams (optional)

- Consider a third-order differential equation in the form:

$$\frac{d^3 y}{dt^3} + a_2 \frac{d^2 y}{dt^2} + a_1 \frac{dy}{dt} + a_0 y = b_2 \frac{d^2 x}{dt^2} + b_1 \frac{dx}{dt} + b_0 x$$

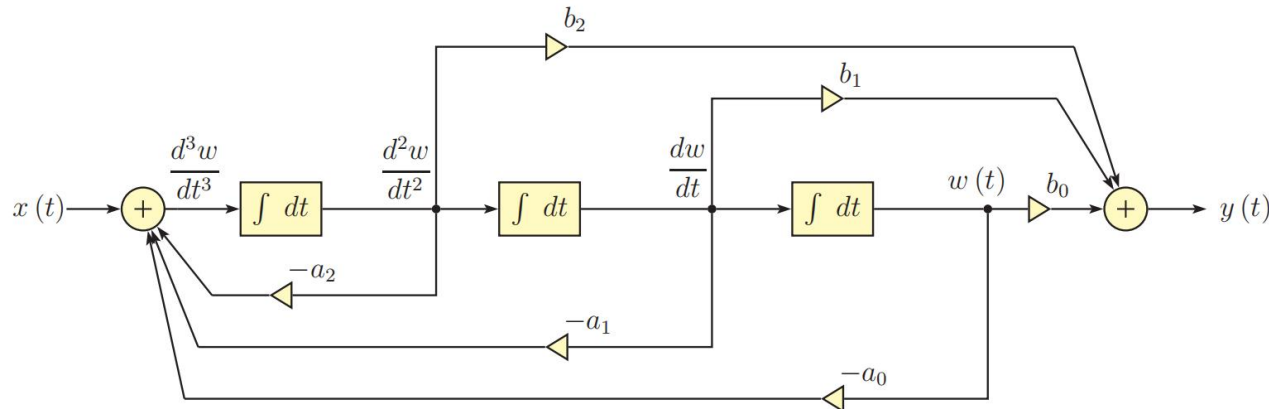
- Intermediate variable $w(t)$:



$$\frac{d^3 w}{dt^3} + a_2 \frac{d^2 w}{dt^2} + a_1 \frac{dw}{dt} + a_0 w = x$$

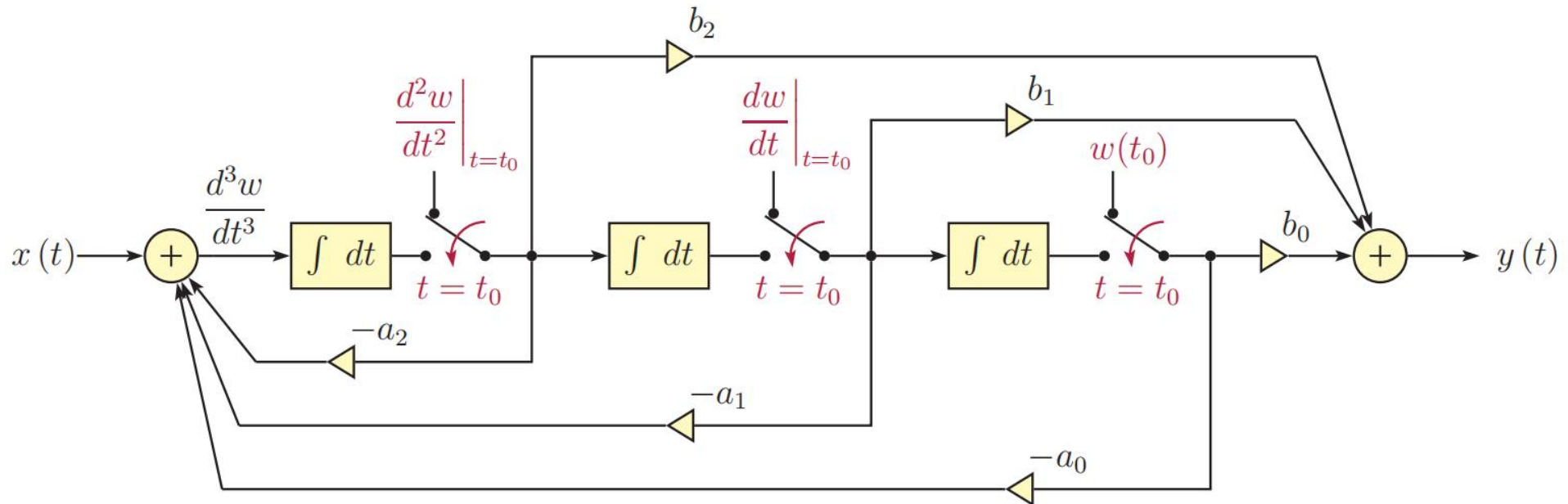
- On the other side:

$$y = b_2 \frac{d^2 w}{dt^2} + b_1 \frac{dw}{dt} + b_0 w$$



3.3 Imposing initial conditions (optional)

- Imposing initial conditions
 - initial values of $y(t)$ and its first $N-1$ derivatives need to be converted to corresponding initial values of $w(t)$ and its first $N-1$ derivatives;
 - Afterwards, appropriate initial value can be imposed on the output of each integrator



Quiz 2

- Draw block diagram for causal LTI systems described by the following difference and differential equations:

$$a) \quad y(t) = -\left(\frac{1}{2}\right) \frac{dy(t)}{dt} + 4x(t)$$

$$b) \quad \frac{dy(t)}{dt} + 3y(t) = x(t)$$

$$c) \quad \frac{d^3y}{dt^3} + 5 \frac{d^2y}{dt^2} + 17 \frac{dy}{dt} + 13y = x + 2 \frac{dx}{dt}$$

Next ...

- Unilateral Laplace Transform
- Solving LCCDE using ULT