# CAN102 Electromagnetism and Electromechanics

2023/24-S2

# Lecture 13 Magnetic Circuits

Jingchen Wang
SAT
jingchen.wang@xjtlu.edu.cn

#### Module information

Module teacher: Jingchen Wang

Email: <u>Jingchen.wang@xjtlu.edu.cn</u>

Location: EE226

Office hour: Thursday 13:00-15:00

Friday 13:00-15:00

Reference book:

Electric Machinery Fundamentals 5 th, by Stephen J. Chapman

Materials:

Lecture slides and recorded videos
Self-practice questions and solutions
Useful resources from external links



#### **Motivation**

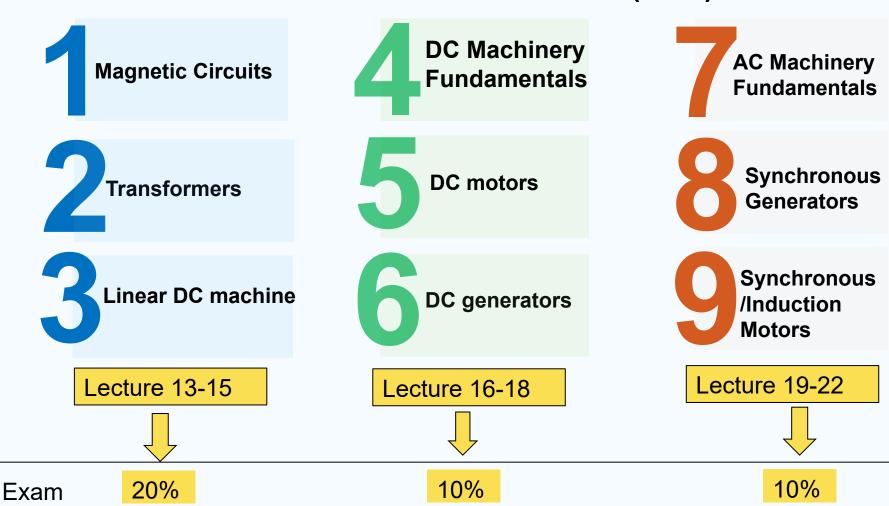


- Powering everything from industrial machinery to household appliances, such as electric motors
- Converting mechanical energy into electrical energy, such as generators
- Understanding the interplay of electrical and mechanical systems
- Design and analyzing electromechanical systems, such as robotic actuators and control systems



# Module Syllabus

# Week 8-12 Electromechanics (40%)



Consider a coil with N turns, wound onto a core carries a current I

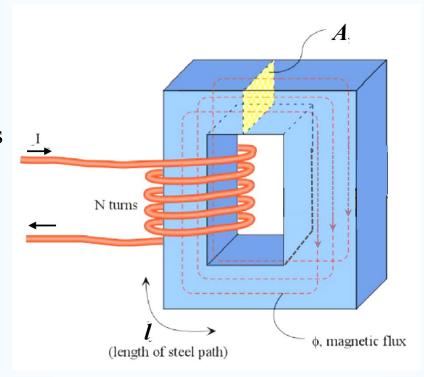
It will generate magnetomotive force (mmf/ T)

$$F = NI$$
 SI Unit: Ampere-turns

If *l* represents the length of steel path, according to Ampere's law (Lecture 9 page 24),

$$F = Hl = NI$$

Where *H* is magnetic field intensity



Ampere's circuital law (Ampere's Law):

The line integral of the magnetic field intensity  $\vec{H}$  around a closed path equals the current enclosed.

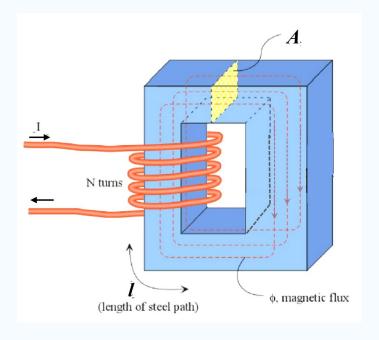
Since magnetic flux density **B** is defined as

$$B = \mu H = \mu_r \mu_0 H$$

Where  $\mu_r$  is the relative permeability of material

$$\mu_0 = 4\pi \times 10^{-7} \ H / m$$

The total flux  $\Phi$  in a given area A is provided as  $\Phi = BA$ 



$$F = Hl = \frac{B}{\mu_r \mu_0} l = \frac{\Phi}{\mu_r \mu_0 A} l = \Phi \frac{l}{\mu_r \mu_0 A} = \Phi \Re$$

Where  $\Re$  is the reluctance of the magnetic circuit

Reluctance of the magnetic circuit

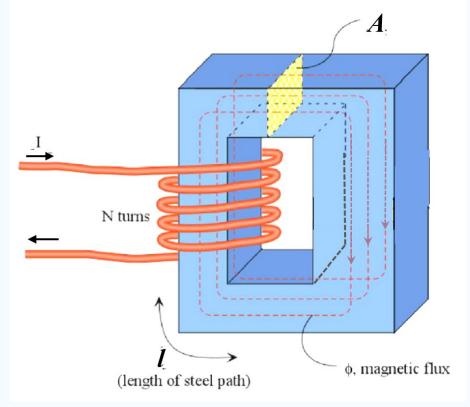
$$\Re = \frac{l}{\mu_r \mu_0 A}$$

SI unit: A · turns/Wb

*l* is the mean path length

 $\mu_r$  is the relative permeability of material

A is the perpendicular area to flux density

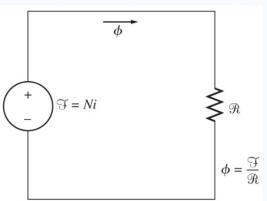


# Comparison between electric and magnetic circuit

#### Electric Circuit

# $I = \frac{V}{R}$

# Magnetic Circuit



Magnetic field intensity

Voltage Current

(V) (A) mmfFlux

(A-t)

 $(\Omega)$ 

Reluctance

Flux density

Permeability

(Wb)

Resistance Electric field intensity

(V/m)

 $(H^{-1})$ 

Current density

 $(A/m^2)$ 

(A-t/m)

Conductivity

(S/m)

(T) (H/m)

V = IR

 $J = \sigma E$ 

 $\mathcal{F} = \phi \mathcal{R}$  $B = \mu H$ 

permeance

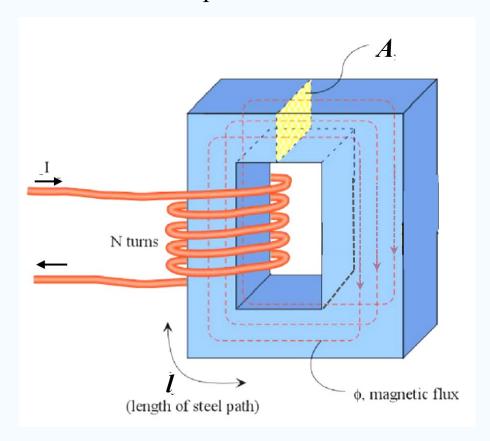
$$R = \frac{\ell}{\sigma A} = \frac{1}{G}$$

$$\Re = \frac{\ell}{\mu A} = \frac{1}{\Re}$$

Conductance

## Example

Consider a square-shaped core of cross-sectional area  $5 \times 10^{-4} \text{ m}^2$  and length 0.5m, made of steel with relative permeability of 3,500. It is wound with a coil of 250 turns that carries 2 amps. Find the flux in the core.



## Example

Consider a square-shaped core of cross-sectional area 5 x 10<sup>-4</sup> m<sup>2</sup> and length 0.5m, made of steel with relative permeability of 3,500. It is wound with a coil of 250 turns that carries 2 amps. Find the flux in the core.

#### Solution using first principles:

Ampere's Law: 
$$H \cdot l = N \cdot I$$

$$H = \frac{250 \times 2}{0.5} = 1000$$
 A/m

$$B = \mu_0 \mu_r H = 4\pi \times 10^{-7} \times 3500 \times 1000$$
  
= 4.4 Wb/m<sup>2</sup>

So the flux in the circuit is

$$\Phi = B \times A = 4.4 \times 5 \times 10^{-4}$$
  
= 2.2×10<sup>-3</sup> Wb

# Example

Consider a square-shaped core of cross-sectional area 5 x 10<sup>-4</sup> m<sup>2</sup> and length 0.5m, made of steel with relative permeability of 3,500. It is wound with a coil of 250 turns that carries 2 amps. Find the flux in the core.

#### Solution using circuit reluctance

$$F=NI=250 \times 2 = 500$$
 ampere-turns

$$\Re = \frac{l}{\mu_0 \mu_r A}$$

$$\frac{0.5}{4\pi \times 10^{-7} \times 3500 \times 5 \times 10^{-4}} = 2.3 \times 10^{5} \text{ A · turns/Wb}$$

So the flux in the circuit:

$$\Phi = \frac{F}{\Re} = \frac{500}{2.3 \times 10^5} = 2.2 \times 10^{-3}$$
 Wb

#### Solution using first principles:

Ampere's Law:  $H \cdot I = N \cdot I$ 

The reluctance of the circuit: 
$$\Re = \frac{l}{\mu_0 \mu_r A}$$

$$H = \frac{250 \times 2}{0.5} = 1000 \quad \text{A/m}$$

$$R = \mu_0 \mu_0 H = 4\pi \times 10^{-7} \times 3500$$

$$B = \mu_0 \mu_r H = 4\pi \times 10^{-7} \times 3500 \times 1000$$
  
= 4.4 Wb/m<sup>2</sup>

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# Magnetic Circuit with Air Gap

air gap:  $H_{g_i}B_{g_i}\Re_{g_i}l_{g_i}A_{g_i}$ 

core:  $H_{c}$ ,  $B_{c}$ ,  $\Re_{c}$ ,  $l_{c}$ ,  $A_{c}$ 

The field in the gap:  $H_g = B_g/\mu_0$ 

The field in the core:  $H_c = B_c / \mu = B_c / (\mu_n \mu_0)$ 

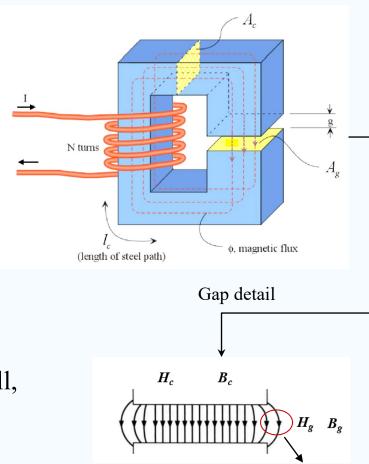
If fringing is considered as neglected and

the flux in core and air gap are same  $\Phi = BA$ 

By continuity of the magnetic flux density:

 $B_c = B_g = B$  with assuming of the gap being small, So:

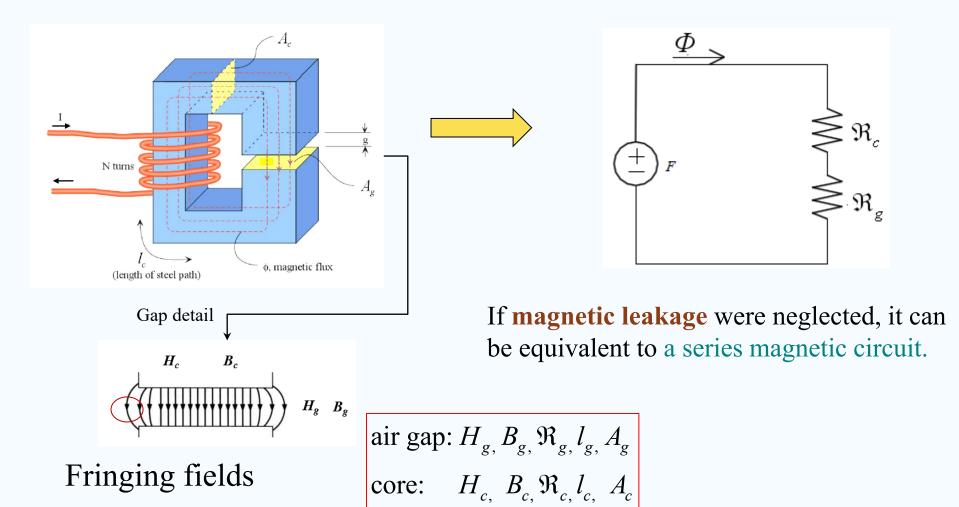
$$H_c = \frac{B}{\mu} = \frac{B}{\mu_r \mu_0} = \frac{H_g}{\mu_r} \implies \frac{H_g}{H_c} = \mu_r$$



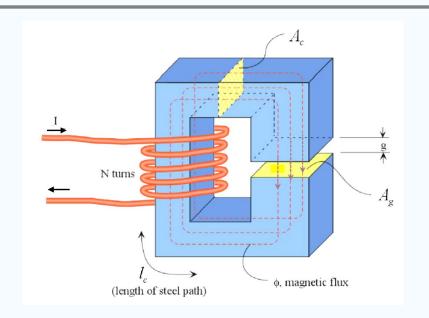
Fringing fields

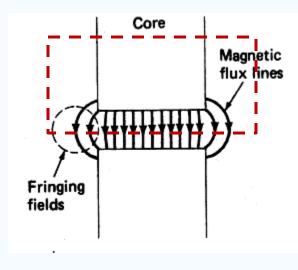
# Magnetic Circuit with Air Gap

Let a narrow air gap of thickness g be cut in the core.



# Magnetic Circuital Laws





#### By Ampere's law

$$F = NI = H_c l_c + H_g l_g$$

where 
$$H_c l_c = \frac{B_c}{\mu_c} l_c = \frac{\Phi_c}{\mu_c A_c} l_c = \Phi_c \Re_c$$

and 
$$H_g l_g = \frac{B_g}{\mu_0} l_g = \frac{\Phi_g}{\mu_0 A_g} l_g = \Phi_g \Re_g$$

According to Gauss's law in magnetics:

$$\oint_{S} \mathbf{B} \bullet d\mathbf{A} = 0$$

We have:  $\Phi_c = \Phi_g = \Phi$ 

Therefore  $F = (\Re_c + \Re_g)\Phi$ 

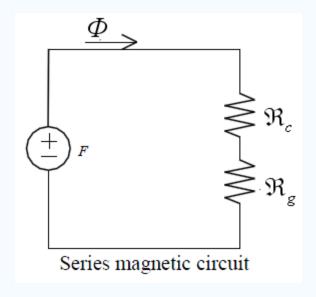
# Magnetic Circuital Laws

The magnetic circuit with an air gap is analogous to a series electric circuit.

$$F = (\mathfrak{R}_c + \mathfrak{R}_g)\Phi$$

In an electric circuit, a voltage drives a current *I* through each resistor.

In a magnetic circuit, the magnetomotive force drives a flux through each reluctance.



The equivalent total reluctance of a number of reluctances in series is just the sum of the individual reluctance:

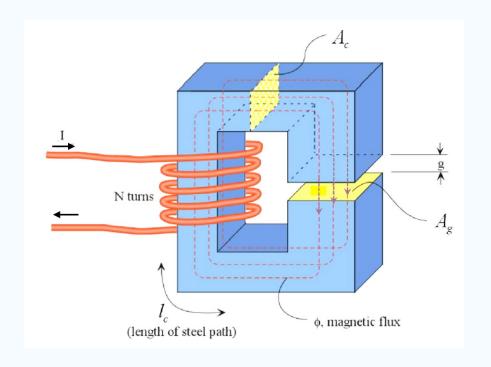
$$\mathfrak{R}_{eq} = \mathfrak{R}_1 + \mathfrak{R}_2 + \ldots + \mathfrak{R}_n = \sum_{i=1}^n \mathfrak{R}_i$$

#### **Dimensions:**

$$A_c = A_g = 9 \text{ cm}^2$$
,  $g = 0.05 \text{cm}$ 

$$l_c = 30 \text{ cm}, N = 500 \text{ turns}$$

 $\mu_r$  = 70,000 for the core and 1 for the gas. The circuit is operating with  $B_c$  = 1.0 T



#### Find:

- (a) reluctances in the core and in the gap
- (b) the flux, and
- (c) the current I

(a) The reluctances: 
$$\Re_c = \frac{l_c}{\mu_r \mu_0 A_c} = \frac{0.3}{70000(4\pi \times 10^{-7})(9 \times 10^{-4})} = 3.79 \times 10^3 \text{ A} \cdot \text{turns/Wb}$$

$$\Re_g = \frac{l_g}{\mu_r \mu_0 A_c} = \frac{5 \times 10^{-4}}{1(4\pi \times 10^{-7})(9 \times 10^{-4})} = 4.42 \times 10^5 \text{ A} \cdot \text{turns/Wb}$$

(b) The magnetic flux: 
$$\Phi = B_c A_c = 1.0(9 \times 10^{-4}) = 9 \times 10^{-4}$$
 Wb

(c) The current: 
$$I = \frac{F}{N} = \frac{\Phi(\Re_c + \Re_g)}{N} = \frac{(9 \times 10^{-4})(4.46 \times 10^5)}{500} = 0.8028 \text{ A} \approx 0.80 \text{ A}$$

$$\Re_c = 3.79 \times 10^3 \text{ A} \cdot \text{turns/Wb}$$
  $\frac{\Re_c}{\Re_g} = 4.42 \times 10^5 \text{ A} \cdot \text{turns/Wb}$   $\frac{\Re_c}{\Re_g} = 0.00857$ 

If the reluctance in the core is negligible, then the current

$$I = \frac{F}{N} = \frac{\Phi(\Re_{c} + \Re_{g})}{N} \approx \frac{\Phi \Re_{g}}{N} = \frac{(9 \times 10^{-4})(4.42 \times 10^{5})}{500} = 0.7956 \text{ A} \approx 0.80 \text{ A}$$

$$AI = \frac{0.8028 - 0.7956}{N} \times 100\% - 0.87\%$$

$$\Delta I = \frac{0.8028 - 0.7956}{0.8028} \times 100\% = 0.87\%$$

#### Reluctance in Series

If  $\Re_c << \Re_g$ , then the reluctance of the core can be neglected. The flux or magnetic filed density B can be obtained from

$$F = (\mathfrak{R}_c + \mathfrak{R}_g)\Phi \approx \mathfrak{R}_g\Phi$$

high material permeability small core reluctance



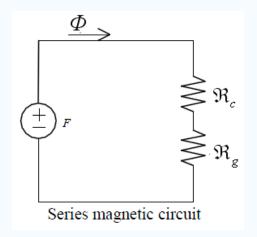
Not always ture!

 $\stackrel{(+)}{=}_{F}$   $\stackrel{\otimes}{\Longrightarrow}_{\mathcal{R}_{g}}$ 

low material permeability (2000~6000 times of air)

large core reluctance

$$F = (\mathfrak{R}_c + \mathfrak{R}_g)\Phi$$

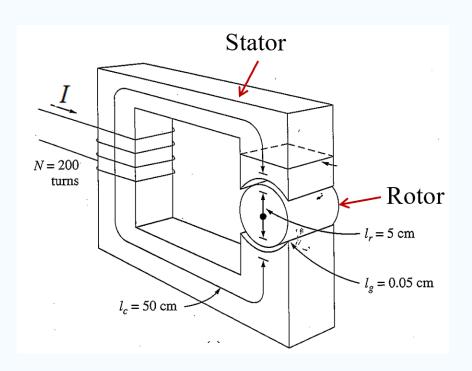


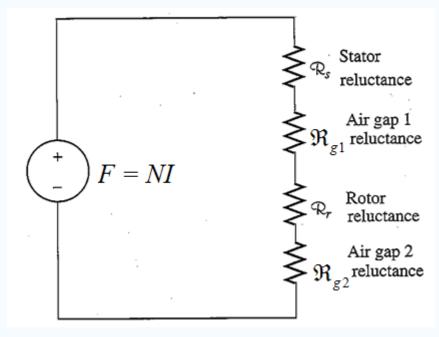
## Magnetic Circuital Laws

# Reluctance in Series Example 2

The cross-sectional area of each air gap (including fringing is 14 cm<sup>2</sup>) and the iron of the core has a relative permeability of 2000.

If the current in the wire is adjusted to be 1 A, what will the resulting flux density in the air gaps be?

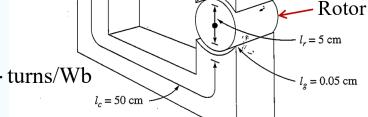




$$B_g = \Phi/A_g$$
  $A_g = 14 \text{ cm}^2$   
 $\Phi = F / \Re$ 

The reluctance of the stator:

$$\Re_s = \frac{l_s}{\mu_r \mu_0 A_s} = \frac{0.5}{(2000)(4\pi \times 10^{-7})(0.0012)} = 166000 \text{ A} \cdot \text{turns/Wb}$$



Stator

The reluctance of the rotor:

$$\Re_r = \frac{l_r}{\mu_r \mu_0 A_r} = \frac{0.05}{(2000)(4\pi \times 10^{-7})(0.0012)} = 16600 \text{ A} \cdot \text{turns/Wb}$$

The reluctance of the air gap:

$$\Re_g = \frac{l_g}{\mu_r \mu_0 A_g} = \frac{0.0005}{(1)(4\pi \times 10^{-7})(0.0014)} = 284000 \text{ A} \cdot \text{turns/Wb}$$

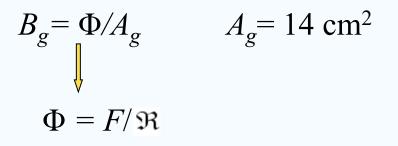
Proper units

The total reluctance of the motor:

$$\Re_{total} = \Re_s + \Re_{g1} + \Re_r + \Re_{g2} = 166000 + 284000 + 16600 + 284000 = 751000 \text{ A} \cdot \text{turns/Wb}$$

# **Magnetic Circuital Laws**

# Reluctance in Series Example 2



The total reluctance:

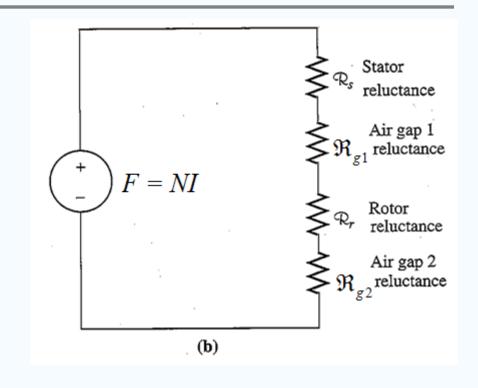
$$\Re_{total} = 751000 \text{ A} \cdot \text{turns/Wb}$$

The net magnetomotive force applied to the core:

$$F = NI = (200)(1.0) = 200$$
 (A·turns)

The total flux:

$$\Phi = \frac{F}{\Re_{total}} = \frac{200}{751000} = 0.00266 \text{ Wb}$$



Then the magnetic flux density in the gap: 
$$B = \frac{\Phi}{A_g} = \frac{0.00266}{0.0014} = 0.19$$
 T (Wb/m<sup>2</sup>)

$$\frac{\Re_s}{\Re_g} = \frac{166000}{284000} = 0.5845$$

$$\Rightarrow \Re_s(\Re_r) \text{ not } << \Re_g$$

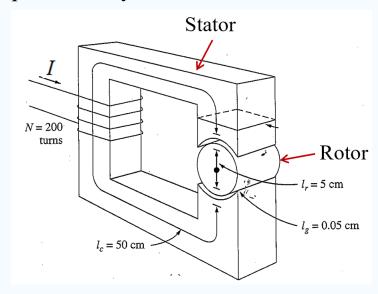
$$\frac{\Re_r}{\Re_g} = \frac{16600}{284000} = 0.05845$$

especially  $\Re_s$ 

The core has a relative permeability of 2000.

#### Two reasons:

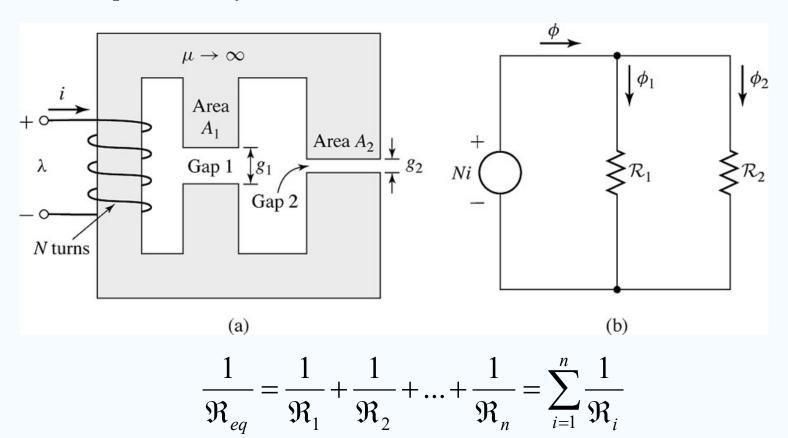
- 1.  $\mu_r$  not big enough
- 2. Length of core is much longer than that of gap



# Magnetic Circuital Laws - Reluctance in Parallel

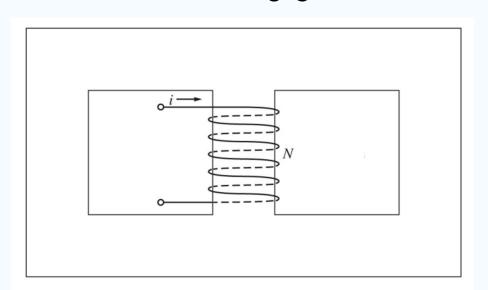
The magnetic circuits with two or more flux paths, neglecting leakage flux, are classified as parallel magnetic circuits.

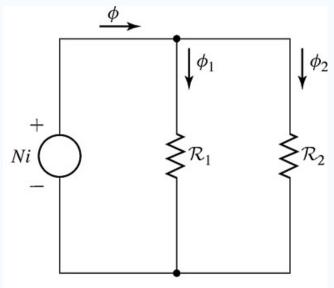
1) If the permeability of material is infinite



# Magnetic Circuital Laws - Reluctance in Parallel

2) If the permeability of material is not infinite, the reluctance of core is not considered as negligible.

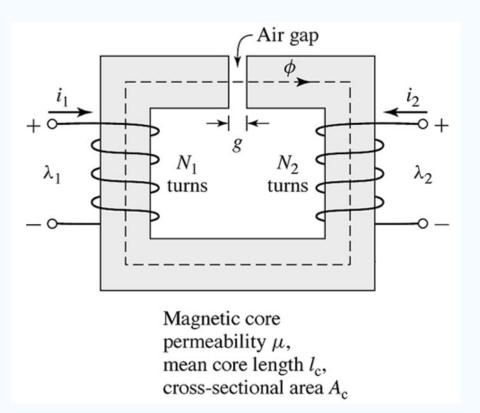




$$\Phi = \Phi_1 + \Phi_2$$

$$\frac{1}{\mathfrak{R}_{eq}} = \frac{1}{\mathfrak{R}_1} + \frac{1}{\mathfrak{R}_2}$$

# Magnetic Circuit with Two Windings



In this case, the MMF acting on the magnetic circuit is given by the total ampere-turns acting on the circuit. For the current directions shown by the Fig, the flux produced by the two windings is in the same direction. The total MMF:

$$F = N_1 i_1 + N_2 i_2$$

The total resultant core flux produced by the total magnetomotive force of the two windings with assumption of  $A_c = A_g$ :

$$\Phi = (N_1 i_1 + N_2 i_2) \frac{\mu_0 A_c}{g} \quad \text{if} \quad \mu_r \text{ is large}$$

# Summary

magnetomotive force 磁动势 F = NI

$$F = Hl = \frac{B}{\mu_r \mu_0} l = \frac{\Phi}{A \mu_r \mu_0} l$$

Flux density **B** 

磁通密度

Flux Φ

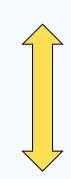
磁通量

Magnetic field intensity H

磁场强度

Magnetic reluctance R

磁阻



relative permeability  $\mu_r$ 

相对磁导率

Mean path length of the core/air gap *l* 

平均路径长度

Cross-sectional area A

横截面积

$$F = \Phi \Re = BA\Re = \mu_r \mu_0 H\Re$$

$$\Re = \frac{l}{\mu_r \mu_0 A}$$

# Summary

#### **Assumptions:**

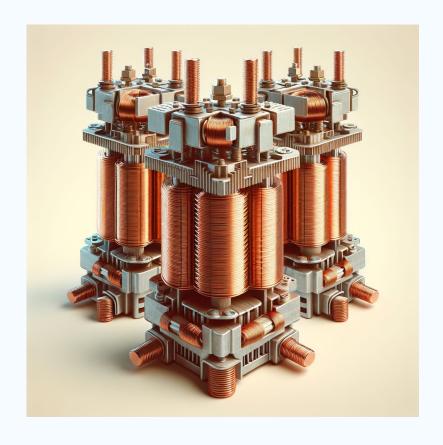
- •Constant magnetic permeability: linear relationship between B-H– gives results of acceptable engineering accuracy
- No leakage
- •Air gap is small and the fringing can be ignored:  $A_c = A_g$

Under the conditions provided, the magnetic circuit model introduced is true.

$$\mathfrak{R}_{eq} = \mathfrak{R}_1 + \mathfrak{R}_2 + \ldots + \mathfrak{R}_n = \sum_{i=1}^n \mathfrak{R}_i$$

$$\frac{1}{\Re_{eq}} = \frac{1}{\Re_1} + \frac{1}{\Re_2} + \dots + \frac{1}{\Re_n} = \sum_{i=1}^n \frac{1}{\Re_i}$$

# **Next**



**Transformers** 

# Thanks for your attention

