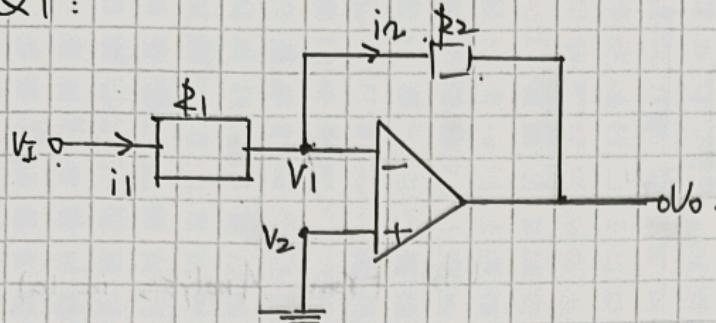


EEE 211 - Assn 3.

Q1 :



(a) i^o From the virtual short principle,

we have :

$$V_1 = V_2 \approx 0 \text{ V}.$$

\geq^o Since the current flowing into the op-amp is assumed to be zero,

we have..:

$$i_1 = i_2$$

where by ohm's law.

$$i_1 = \frac{V_I - V_1}{R_1} \text{ and } i_2 = \frac{V_1 - V_o}{R_2}.$$

Then, we have:

$$\frac{V_o}{V_I} = -\frac{R_2}{R_1}$$

That is :

$$V_o = \left(-\frac{R_2}{R_1}\right) \cdot V_I = +8.8 \text{ V}$$

(b). For an actual Op-Amp. with finite open-loop gain (that means no Virtual Short)

→ we have

$$\frac{V_I - V_1}{R_1} = \frac{V_1 - V_o}{R_2}$$

$$\text{Since } V_2 = 0.$$

$$\rightarrow \text{then } V_d = V_2 - V_1 = -V_1$$

$$\rightarrow V_o = -A_{OL} \cdot V_1$$

we find .

$$\rightarrow \frac{V_o}{V_I} = V_1 \left(\frac{1}{R_1} + \frac{1}{R_2} \right) - \frac{V_o}{R_2}$$

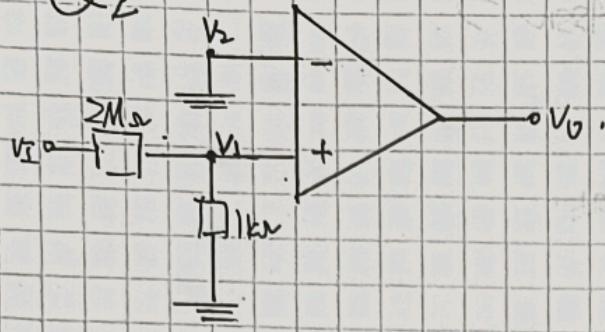
The close-loop gain is then .

$$\rightarrow A_{CL} = \frac{V_o}{V_I} = \frac{-\frac{R_2}{R_1}}{\frac{1}{A_{OL}} \left(1 + \frac{R_2}{R_1} \right) + 1}$$

$$\rightarrow A_{CL} = \frac{-\frac{22k}{1k}}{\frac{1}{5k} \left(1 + \frac{22}{1} \right) + 1} = -21.8793.$$

$$\rightarrow \text{Finally, } V_o = A_{CL} \cdot V_I = 8.7597 \text{ V}$$

Q2



(a)

From an op-amp with finite loop gain,

$$\text{we have: } V_O = A_{\text{od}} \cdot V_d$$

$$\text{Since } V_O = -2V; A_{\text{od}} = 10^4$$

$$\text{then } V_d = \frac{V_O}{A_{\text{od}}} = (-2) \times 10^{-4} V \quad \textcircled{1}$$

According to the label in schematic.

$$\Rightarrow V_d = V_L - V_2 = V_I \quad \textcircled{2}$$

Apply Ohm's Law

$$\Rightarrow V_I = \frac{1k\Omega}{1k\Omega + 2M\Omega} \cdot V_I \quad \textcircled{3}$$

Combine Equation $\textcircled{1}, \textcircled{2}, \textcircled{3}$

$$\text{we have: } V_I = (-2) \times 10^{-4} \times \frac{1k\Omega + 2M\Omega}{1k\Omega}$$

$$\Rightarrow V_I = -0.40 V$$

(b) From Analysis in (a)

we are able to obtain

$$V_O = A_{\text{od}} \cdot V_d$$

$$V_d = V_I$$

$$V_I = \frac{1k}{1k+2M} \cdot V_I$$

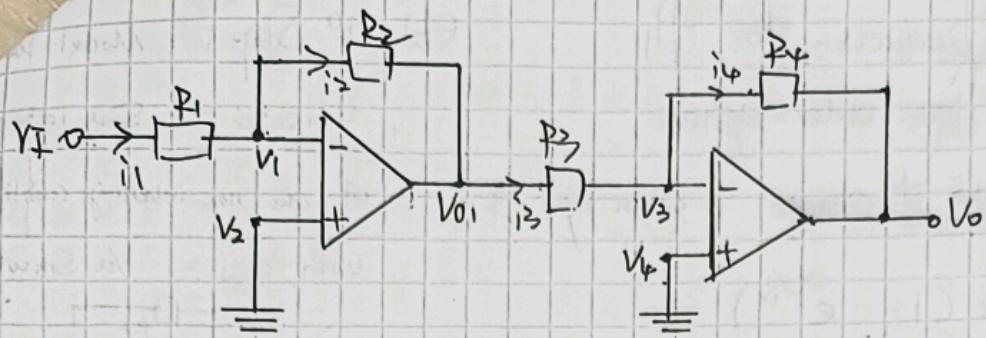
$$A_{\text{od}} = \frac{V_O}{V_I} = \frac{1k+2M}{1k}$$

$$\text{Since } V_I = 2V, V_O = 1V$$

$$\Rightarrow A_{\text{od}} = \frac{1}{2} \cdot \frac{200}{1}$$

$$\Rightarrow A_{\text{od}} = \cancel{1000.5}$$

Q3



1^o Step 1 : Find i_1 .

Assume Ideal op-amp (Left)

then we can apply "virtual short".

$$\Rightarrow \text{that is } V_{1\text{A}} = V_2 = 0 \quad (1)$$

And virtual open

$$\Rightarrow \text{we have: } i_1 = i_2. \quad (2)$$

Apply Ohm's law

$$\Rightarrow i_1 = \frac{V_1 - V_1}{R_1} = \frac{-0.15 - 0}{10k} = -15 \mu A \quad (3)$$

2^o Step 2 : Find i_2 .

Combine (2) and (3)

$$\Rightarrow i_2 = -15 \mu A \quad (4)$$

3^o Step 3 : Find V_{01}

Apply kvl

$$\Rightarrow V_{01} = V_1 - i_1 R_1 - i_2 R_2$$

$$\Rightarrow V_{01} = -0.15 - (-15\mu A) \cdot (10k + 80k)$$

$$\Rightarrow V_{01} = +1.2 V \quad (5)$$

7^o Summary

$$\left\{ \begin{array}{l} V_{01} = 1.2 V \\ V_0 = -6 V \end{array} \right. ; \quad \left\{ \begin{array}{l} i_1 = -15 \mu A \\ i_2 = -15 \mu A \end{array} \right. ; \quad \left\{ \begin{array}{l} i_3 = 60 \mu A \\ i_4 = 60 \mu A \end{array} \right.$$

4^o Step 4 : Find i_3 .

Assume Ideal op-amp (Right)

then we can apply "virtual short".

$$\Rightarrow \text{that is } V_3 = V_4 = 0 \quad (6)$$

And virtual open

$$\Rightarrow \text{we have: } i_3 = i_4. \quad (7)$$

Apply Ohm's law.

$$\Rightarrow i_3 = \frac{V_{01} - V_3}{R_3} = \frac{1.2 - 0}{20k} = 60 \mu A \quad (8)$$

5^o Step 5 : Find i_4

Combine (7) and (8)

$$\Rightarrow i_4 = +60 \mu A \quad (9)$$

6^o Step 6 : Find V_0

Apply kvl.

$$\Rightarrow V_0 = V_3 - i_4 R_4$$

$$\Rightarrow V_0 = 0 - 60 \mu A \cdot 100k$$

$$\Rightarrow V_0 = -6 V \quad (10)$$

Q4

(a) 1^o Step 1 : Reduction for f_H

Consider a first order system,
its maximum rate of change is given by

$$V_o(t) = V_m (1 - e^{-t/\tau_r})$$

then its derivative

$$\frac{dV_o(t)}{dt} = \frac{V_m}{\tau_r} e^{-t/\tau_r}$$

$$\Rightarrow \left. \frac{dV_o(t)}{dt} \right|_{\max} = SR = \frac{V_m}{\tau_r}$$

$$\text{Since } \tau_r = \frac{1}{2\pi f_H}$$

$$\Rightarrow \text{then } SR = V_m \cdot 2\pi f_H = 5 \text{ m-v/s}$$

$$\Rightarrow \text{that is } f_H = \frac{SR}{2\pi V_m} = \frac{5 \text{ m}}{2\pi V_m}$$

2^o Step 2 : Case 1 : $V_m = +5 \text{ V}$

$$\Rightarrow f_H = \frac{5 \text{ m}}{2\pi \times 5} = \frac{500}{\pi} \text{ kHz} = 159.15 \text{ kHz}$$

3^o Step 3 : Case 2 : $V_m = +1.5 \text{ V}$

$$\Rightarrow f_H = \frac{5 \text{ m}}{2\pi \times 1.5} = \frac{500}{3\pi} \text{ kHz} = 530.52 \text{ kHz}$$

4^o Step 4 : Case 3 : $V_m = +0.4 \text{ V}$

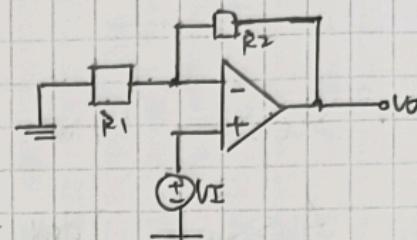
$$\Rightarrow f_H = \frac{5 \text{ m}}{2\pi \times 0.4} = \frac{5}{0.8\pi} \text{ MHz} = 1.99 \text{ MHz}$$

5^o Step 5 : Summary

$$f_H = \begin{cases} 159.15 \text{ kHz}, & \text{when } V_m = +5 \text{ V} \\ 530.52 \text{ kHz}, & \text{when } V_m = +1.5 \text{ V} \\ 1.99 \text{ MHz}, & \text{when } V_m = +0.4 \text{ V} \end{cases}$$

(b) 1^o Step 1 : Model V_o

Consider the Sine response
of an non-inverting amplifier
with $V_I = V_a \sin \omega t$



$$\Rightarrow \text{then } V_o(t) = V_a (1 + \frac{R_2}{R_1}) \sin \omega t$$

$$\text{Let } V_m = V_a \cdot (1 + \frac{R_2}{R_1})$$

$$\Rightarrow V_o(t) = V_m \sin \omega t$$

2^o Step 2 : Calculations

$$\Rightarrow \frac{dV_o(t)}{dt} = \omega V_m \cos \omega t$$

And the slew rate is

$$\Rightarrow SR = \left. \frac{dV_o(t)}{dt} \right|_{\max} = \omega V_m$$

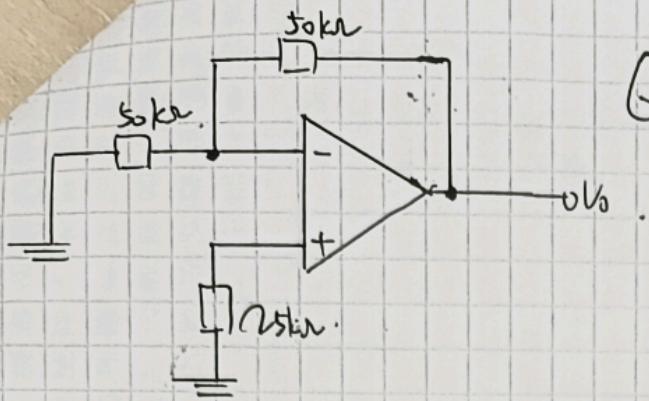
$$\Rightarrow \text{that is : } V_m = \frac{SR}{\omega} = \frac{5 \text{ m}}{\omega}$$

$$SR = 5 \text{ V/μs}$$

$$\omega = 2\pi f$$

$$\Rightarrow V_m = \frac{8 \text{ m}}{2\pi \cdot 250 \text{ kHz}}$$

$$\Rightarrow V_m = +5.09 \text{ V}$$



Q5. 2^o Step 2: I_{Bn} Contribution

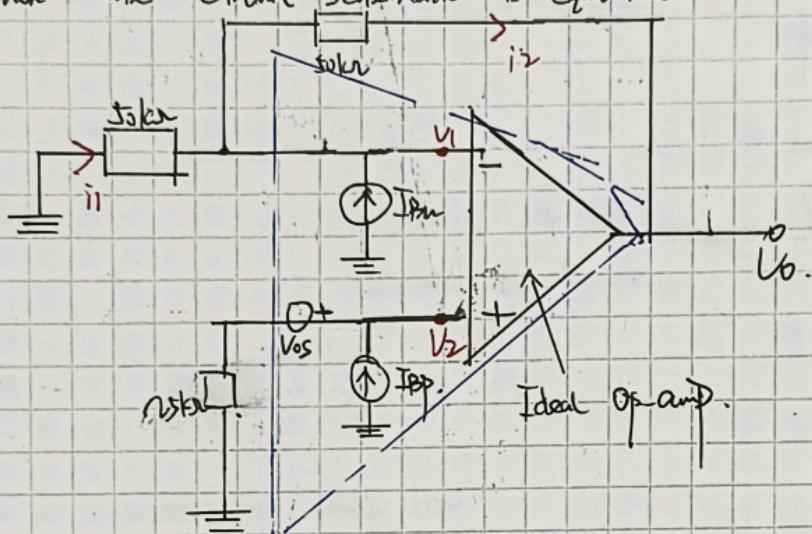
Assume ideal op-amp and apply similar analysis in Step 1

$$\Rightarrow \text{we have: } V_{Bn} = I_{Bn} \cdot 50k \text{ V.}$$

1^o Step 1: Modelling

Since we have to consider input offset current,

then the circuit schematic is equivalent to:



2^o Step 2: I_{Bp} Contribution

Apply Superposition Principle.

\Rightarrow Close / turn off the sources I_{Bn} and V_{os}

$$\text{and we have: } V_2 = -I_{Bp} \cdot (25k).$$

Since it is an ideal op-amp

\Rightarrow then apply Virtual Short principle

$$\left\{ \begin{array}{l} V_1 = V_2 = -I_{Bp} \cdot 25k \\ i_1 = i_2 \end{array} \right.$$

Apply Ohm's Law

$$\Rightarrow V_{Bp} = \frac{50k + 30k}{50k} \cdot V_1 = (-I_{Bp}) \cdot 50k \text{ V.}$$

3^o Step 3: Total Offset Contribution

From the question,

$$\left\{ \begin{array}{l} I_B = 0.8 \text{ mA} \\ I_{os} = 0.2 \text{ mA} \end{array} \right.$$

And we know that

$$\left\{ \begin{array}{l} I_B = \frac{I_{Bp} + I_{Bn}}{2} \\ I_{os} = |I_{Bp} - I_{Bn}| \end{array} \right.$$

then combine ①, ②, ③, ④

$$\Rightarrow \left\{ \begin{array}{l} I_{Bp} = 0.9 \text{ mA} \\ I_{Bn} = 0.7 \text{ mA} \end{array} \right. \quad \text{or} \quad \left\{ \begin{array}{l} I_{Bp} = 0.7 \text{ mA} \\ I_{Bn} = 0.9 \text{ mA} \end{array} \right.$$

We also know that

$$\left\{ \begin{array}{l} V_{Bp} = (-I_{Bp}) \cdot 50k \\ V_{Bn} = I_{Bn} \cdot 50k \end{array} \right.$$

$$\Rightarrow V_{0,\text{tot}} = V_{Bp} + V_{os}$$

$$\Rightarrow V_{0,\text{tot}} = 50k (I_{Bn} - I_{Bp})$$

Thus, consider the two solutions,

$$\Rightarrow V_{0,\text{tot}} = \pm 0.01 \text{ V}$$