

# Tutorial–2

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### Problem 6.1

Q1) An ac voltage controller has a resistive load of  $R = 10\Omega$  and rms input voltage is  $V_s = 120\text{ V}$ , 60 Hz. The thyristors switch is ON for  $n = 25$  cycles and is OFF for  $m = 75$  cycles. Determine the (a) rms output voltage,  $V_{RMS}$ ; (b) input power factor, and (c) average and rms current of thyristors.

Solution:

$$R = 10\Omega, V_s = 120\text{ V}, V_m = \sqrt{2} \times 120 = 169.7\text{ V and}$$

$$k = \frac{n}{n+m} = \frac{25}{100} = 0.25.$$

#### Solution:

a) rms output voltage,  $V_{RMS} = V_S \sqrt{k} = 120 \sqrt{\frac{25}{100}} = 60 \text{ V}$

And the rms load current is,  $I_{RMS} = \frac{V_{RMS}}{R} = \frac{60}{10} = 6 \text{ A}$

b) The load power is  $P_o = I_{RMS}^2 R = 360 \text{ W}$ . Since the input current is same as load current, the input VA is

$$VA = V_S I_S = V_S I_{RMS} = 120 \times 6 = 720 \text{ W}$$

The input power factor,  $PF = \frac{P_o}{VA} = \frac{360}{720} = 0.5$

Solution:

c) The peak thyristor current is  $I_m = \frac{V_m}{R} = 16.7 \text{ A}$ . The average current of thyristor is

$$I_A = \frac{n}{2\pi(m+n)} \int_0^\pi I_m \sin \omega t d(\omega t) = \frac{I_m n}{\pi(m+n)} = \frac{k I_m}{\pi} = 1.35 \text{ A}$$

The rms current of thyristors is

$$I_R = \left[ \frac{n}{2\pi(m+n)} \int_0^\pi I_m^2 \sin^2 \omega t d(\omega t) \right]^{1/2} = \frac{I_m}{2} \sqrt{\frac{n}{n+m}} = 4.2 \text{ A}$$

Problem 6.2

Q2) A single-phase full-wave ac voltage controller has a load of  $5\ \Omega$  and the input voltage is 230 V with 50 Hz. If the load power is 5 kW, determine (a) the firing angle, (b) input power factor, and (c) rms output voltage.

Solution:

a) The rms output voltage,  $V_{RMS} = \frac{V_m}{\sqrt{2}} \left[ \frac{1}{\pi} \left( \pi - \alpha + \frac{\sin 2\alpha}{2} \right) \right]^{1/2}$

The output power,  $P_{out} = V_{RMS} I_{RMS} = \frac{V_{RMS}^2}{R} = 5000\ W$

$$\frac{230^2}{5} \left[ \frac{1}{\pi} \left( \pi - \alpha + \frac{\sin 2\alpha}{2} \right) \right] = 5000 \rightarrow \alpha = 92.5^\circ = 1.61\ \text{rad}$$

### Problem 6.2

Solution:

b) Input power factor,  $\frac{P_{out}}{P_{in}} = \frac{5000}{V_S \times I_S} = \frac{5000}{230 \times 31.63} = 0.6871$

Input current,  $I_S = I_{RMS} = \frac{5000}{V_{RMS}} = 31.63 \text{ A}$

c) The rms output voltage,

$$V_{RMS} = \frac{V_m}{\sqrt{2}} \left[ \frac{1}{\pi} \left( \pi - \alpha + \frac{\sin 2\alpha}{2} \right) \right]^{1/2} = 158.03 \text{ V}$$

### Problem 7.1

Q3) A step-down dc-dc converter has a resistive load of  $10\ \Omega$  and input voltage of  $200\text{ V}$ . If the switching frequency is  $1\text{ kHz}$  and duty cycle is  $60\%$ , determine (a) average output voltage and current, (b) rms output voltage and current.

Solution:  $V_s = 200\text{ V}$ ,  $R = 10$ ,  $f = 1\text{ kHz}$ ,  $k = 60\% = 0.6$

(a) Average output voltage,  $V_o = kV_s = 0.6 \times 200 = 120\text{ V}$

Average load current,  $I_o = \frac{V_o}{R} = 12\text{ A}$

(a) RMS output voltage,  $V_{RMS} = \sqrt{k}V_s = 155\text{ V}$

RMS load current,  $I_{RMS} = \frac{V_{RMS}}{R} = 15.4\text{ A}$

Problem 7.2

Q4) A 100 V step-down dc chopper has the maximum & minimum values of inductor current as 250 A and 50 A. The ON-time and OFF-time of chopper are 20 ms and 30 ms respectively. Determine (a) ripple current, (b) chopping frequency, (c) duty cycle, and (d) output voltage.

Solution:

(a) Ripple current,  $\Delta I = I_2 - I_1 = 250 - 50 = 200 \text{ A}$

(b) Chopping frequency,  $f = \frac{1}{T_{ON} + T_{OFF}} = \frac{1}{20 \text{ ms} + 30 \text{ ms}} = 20 \text{ Hz}$

(c) Duty cycle,  $k = \frac{T_{ON}}{T_{ON} + T_{OFF}} = 0.4$

(d) Output voltage,  $V_o = kV_s = 0.4 \times 100 = 40 \text{ V}$



Problem 7.3

Q5) The buck-boost converter has an input voltage of  $V_s = 12\text{ V}$ . The duty cycle  $k = 0.25$  and the switching frequency is  $25\text{ kHz}$ . The inductance  $L = 150\text{ }\mu\text{H}$  and the filter capacitance  $C = 220\text{ }\mu\text{F}$ . The average load current  $I_a = 1.25\text{ A}$ . Determine (a) the average output voltage  $V_a$ , (b) the peak-to-peak output voltage ripple,  $\Delta V_c$ ; (c) the peak-to-peak ripple current of inductor,  $\Delta I$ , and (d) the critical values of  $L$  and  $C$ .

Solution:

$$V_s = 12\text{ V}, k = 0.25, f = 25\text{ kHz}, L = 150\text{ }\mu\text{H}, C = 220\text{ }\mu\text{F}$$

Solution:

a) The average output voltage,  $V_a = -\frac{V_s k}{1-k} = -4V$

b) The peak-to-peak ripple voltage is  $\Delta V_c = \frac{I_a k}{fC} = 56.8 \text{ mV}$

c) The peak-to-peak inductor ripple is  $\Delta I = \frac{V_s k}{fL} = 0.8 \text{ A}$

d)  $R = -\frac{V_a}{I_a} = 3.2 \Omega$

$$L_C = L = \frac{(1-k)R}{2f} = 450 \mu H$$

$$C_C = C = \frac{k}{2fR} = 1.56 \mu F$$

# Performance Parameters

The output of practical inverters contain harmonics & the quality of an inverter is normally evaluated in terms of these parameters:

- **Harmonic factor of  $n$ th harmonic ( $HF_n$ ):** measure of individual harmonic contribution, is defined as

$$HF_n = \frac{V_{on}}{V_{o1}} \quad \text{for } n > 1$$

where  $V_{o1}$  &  $V_{on}$   $\rightarrow$  rms values of fundamental &  $n$ th harmonic components.

- **Total harmonic distortion (THD):** measure of closeness in shape between a waveform and its fundamental component, is defined as

$$THD = \frac{1}{V_{o1}} \left( \sum_{n=2,3,\dots}^{\infty} V_{on}^2 \right)^{1/2} = \frac{1}{V_{o1}} (V_o^2 - V_{o1}^2)^{1/2}$$

# Performance Parameters

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- **Distortion factor (DF)**: gives total harmonic content, but does not indicate the level of each harmonic component.

$$DF = \frac{1}{V_{o1}} \left[ \sum_{n=2,3,\dots}^{\infty} \left( \frac{V_{on}}{n^2} \right)^2 \right]^{1/2}$$

The DF of an individual (or  $n$ th) harmonic component is defined as

$$DF_n = \frac{V_{on}}{V_{o1} n^2} \quad \text{for } n > 1$$

- **Lowest order harmonic (LOH)**: harmonic component whose frequency is closest to the fundamental one, and its amplitude is greater than or equal to 3% of the fundamental component.

Problem 8.1

Q6) The single-phase half-bridge inverter has a resistive load of  $R = 2.4 \Omega$  and the dc input voltage is  $V_s = 48 V$ . Determine (a) the rms output voltage at the fundamental frequency  $V_{01}$ , (b) the output power  $P_o$ , (c) the average and peak currents of each transistor, (d) the average supply current  $I_s$ , (e) the THD, (f) the DF, (g) the HF and LOH.

Solution:

$$V_s = 48 V, R = 2.4 \Omega$$

$$\text{a) } V_{01} = \frac{2V_s}{\sqrt{2}\pi} = 0.45 \times V_s = 0.45 \times 48 = 21.6 V$$

Problem 8.1Solution:

- b) The rms output voltage,  $V_o = \frac{V_s}{2} = 24 \text{ V}$ . The output power,  $P_o = \frac{V_o^2}{R} = 240 \text{ W}$
- c) The peak transistor current  $I_p = \frac{24}{2.4} = 10 \text{ A}$ . Because each transistor conducts for a 50% duty cycle, the average current of each transistor  $I_Q = 0.5 \times 10 = 5 \text{ A}$
- d) The average supply current,  $I_s = \frac{P_o}{V_s} = \frac{240}{48} = 5 \text{ A}$
- e)  $\text{THD} = \frac{1}{V_{o1}} (V_o^2 - V_{o1}^2)^{1/2} = \frac{0.2176 V_s}{0.45 V_s} = 0.4834 = 48.34\%$

Problem 8.1Solution:

$$\begin{aligned} \text{f) } DF &= \frac{1}{V_{o1}} \left[ \sum_{n=3,5,\dots}^{\infty} \left( \frac{V_{on}}{n^2} \right)^2 \right]^{1/2} = \frac{1}{0.45V_s} \left[ \left( \frac{V_{o3}}{3^2} \right)^2 + \left( \frac{V_{o5}}{5^2} \right)^2 + \left( \frac{V_{o7}}{7^2} \right)^2 + \dots \right]^{1/2} \\ &= \frac{0.024V_s}{0.45V_s} = 5.38\% \end{aligned}$$

g) LOH is the third harmonic,  $V_{o3} = \frac{V_{o1}}{3} = 7.2 \text{ V}$  .  
 $HF_3 = \frac{V_{o3}}{V_{o1}} = \frac{1}{3} = 33.33\%$  .  $DF_3 = \frac{V_{o3}}{V_{o1} \times 3^2} = \frac{7.2}{21.6 \times 9} = 3.704$  .  
 Because harmonic factor  $V_{o3}/V_{o1}$  is 33.33%, which is greater than 3%, LOH =  $V_{o3}$ .

# Single-phase Full-converter Drives

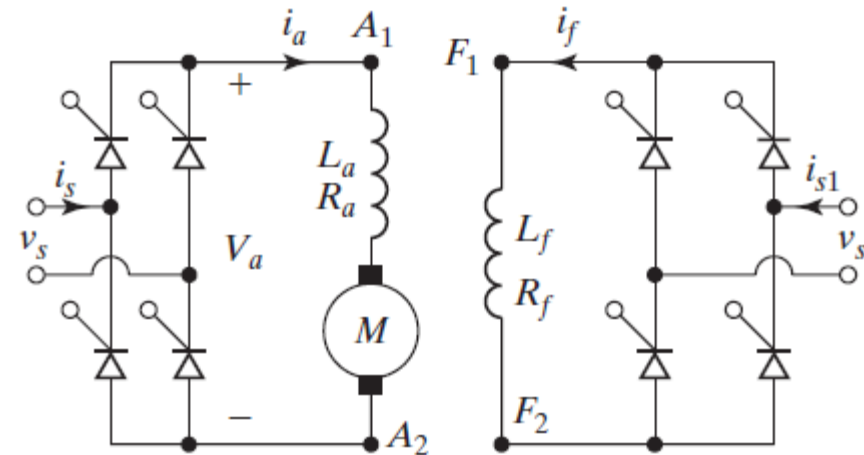
- The armature voltage is varied by a single-phase full-wave converter.
- The average armature voltage, with a single-phase full-wave converter in the armature, as

$$V_a = \frac{2V_m}{\pi} \cos \alpha_a \quad \text{for } 0 \leq \alpha_a \leq \pi$$

- Similarly, the field voltage is,

$$V_f = \frac{2V_m}{\pi} \cos \alpha_f \quad \text{for } 0 \leq \alpha_f \leq \pi$$

- For three-phase full-wave converter,
  - the average armature voltage,  $V_a = \frac{3\sqrt{3}V_m}{\pi} \cos \alpha_a \quad \text{for } 0 \leq \alpha_a \leq \pi$
  - the average field voltage,  $V_f = \frac{3\sqrt{3}V_m}{\pi} \cos \alpha_f \quad \text{for } 0 \leq \alpha_f \leq \pi$





### Problem 8.2

Q7) The speed of a separately excited motor is controlled by a single-phase full-wave converter. The field circuit is also controlled by a full converter and the field current is set to the maximum possible value. The ac supply voltage to the armature and field converters is one-phase, 440 V, 60 Hz. The armature resistance is  $R_a = 0.25 \Omega$ , the field circuit resistance is  $R_f = 175 \Omega$ , and the motor voltage constant is  $K_v = 1.4 \text{ V/A rad/s}$ . The armature current corresponding to the load demand is  $I_a = 45 \text{ A}$ . If the delay angle of the armature converter is  $\alpha_a = 60^\circ$  and the armature current is  $I_a = 45 \text{ A}$ . Determine (a) the torque developed by the motor  $T_d$ , (b) the speed and (c) total input power.

Problem 8.2

Solution:

$$V_s = 440 \text{ V}, V_m = \sqrt{2} \times 440 = 622.25 \text{ V}, R_a = 0.25 \Omega, R_s = 175 \Omega, \alpha_a = 60^\circ, K_v = 1.4 \text{ V/A rad/s}.$$

a) Field voltage in a single-phase full-wave converter,

$$V_f = \frac{2V_m}{\pi} \cos \alpha_f$$

Therefore, the maximum field voltage for  $\alpha_f = 0$  is

$$V_f = \frac{2V_m}{\pi} = \frac{2 \times 622.25}{\pi} = 396.14 \text{ V}$$

$$\text{Field current, } I_f = \frac{V_f}{R_f} = \frac{396.14}{175} = 2.26 \text{ A}$$

#### Solution:

The developed torque is

$$T_d = T_L = K_v I_f I_a = 1.4 \times 2.26 \times 45 = 142.4 \text{ N.m}$$

The armature voltage is

$$V_a = \frac{2V_m}{\pi} \cos 60^\circ = \frac{2 \times 622.25}{\pi} = 198.07 \text{ V}$$

The back emf is

$$E_g = V_a - I_a R_a = 198.07 - 45 \times 0.25 = 186.82 \text{ V}$$

### Problem 8.1

Solution:

b) The speed from back EMF is,  $\omega = \frac{E_g}{K_v I_f} = 59.04$

c) Assuming lossless converters, total input power from supply is

$$P_t = V_a I_a + V_f I_f = 198.07 \times 45 + 396.14 \times 2.26 = 9808.4 \text{ W}$$

***See you in the next (**final**😊) class (May 12<sup>th</sup>)***

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➤ **Probably Revision – Don't miss!!**

➤ **Please finish MQ feedback**

**The End**