

# DC–AC Converters

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# Outline

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- Principle of single phase DC-AC inverters
  - Performance parameters
  - Half bridge voltage source inverter (VSI)
  - Full bridge VSI
- PWM Technique
  - SPWM – Sinusoidal PWM
- Motors
  - DC motor drives
  - AC motor drives (induction motor & synchronous motor)

# 1.0 Introduction

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- Changes DC input voltage to a symmetric AC output voltage of desired magnitude and frequency – *Inverter*
- Variable output voltage can be obtained by *varying the input dc voltage* and maintaining the gain of the inverter constant
- If the *DC input voltage is fixed*, the output voltage can be controlled using – *pulse-width-modulation (PWM)*
- The output voltage should be sinusoidal, *however*, practical inverters are non-sinusoidal and contain *certain harmonics*
- Inverters are widely used in industrial applications – inputs may be battery, fuel cell, solar cell, or other dc source
- The inverters use *fully controlled devices* – BJTs, MOSFETs

# 1.1 Performance Parameters

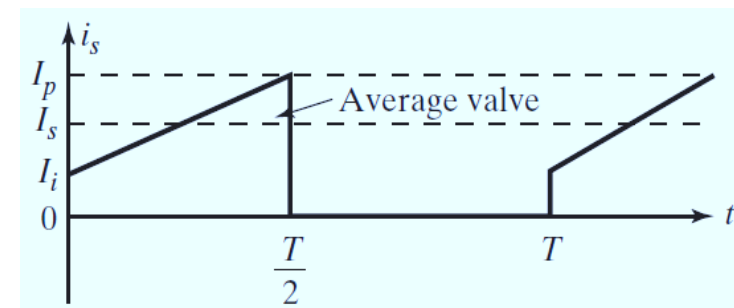
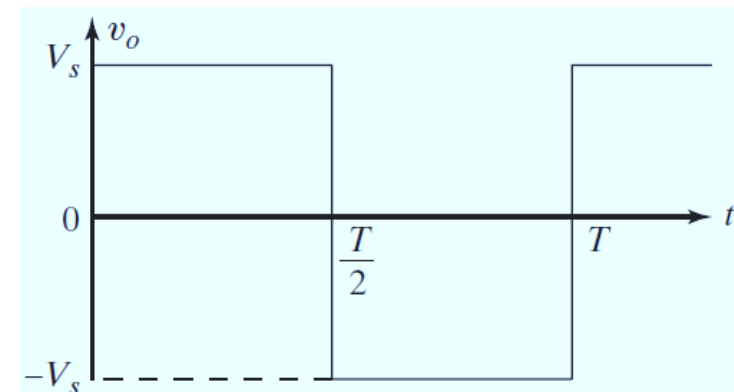
- The *input voltage* to an inverter is *dc* and the *output voltage (or current)* is *ac*.
- The *output* should ideally be an *ac of pure sine wave*, but the output voltage of a practical inverter *contains harmonics or ripples*.
- The *inverter draws current from the dc input source* only when the inverter *connects the load* to the supply source & the *input current is not pure dc*.
- Output power,  $P_{AC} = I_o^2 R$
- Input power,  $P_{DC} = V_s I_s$

$V_o$  &  $I_o$  are rms load voltage and current

$\theta$  is angle of load impedance,  $R$  is load resistance

$V_s$  &  $I_s$  are average input voltage and current

$I_i$  &  $I_s \rightarrow$  rms & average values of dc supply current



# 1.1 Performance Parameters

The output of practical inverters contain harmonics & the *quality of an inverter* is normally evaluated in terms of these parameters:

- **Harmonic factor of  $n$ th harmonic ( $HF_n$ )**: measure of an individual harmonic contribution in the output voltage, is defined as

$$HF_n = \frac{V_{on}}{V_{o1}} \quad \text{for } n > 1$$

where  $V_{o1}$  &  $V_{on}$   $\rightarrow$  rms values of fundamental &  $n$ th harmonic components.

- **Total harmonic distortion (THD)**: measure of closeness in shape between the output voltage waveform and its fundamental component, is defined as

$$THD = \frac{1}{V_{o1}} \left( \sum_{n=2,3,\dots}^{\infty} V_{on}^2 \right)^{1/2} = \frac{\sqrt{V_o^2 - V_{o1}^2}}{V_{o1}}$$

# 1.1 Performance Parameters

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- **Distortion factor (DF)**: gives total harmonic content, but does not indicate the level of each harmonic component.

$$DF = \frac{1}{V_{o1}} \left[ \sum_{n=2,3,\dots}^{\infty} \left( \frac{V_{on}}{n^2} \right)^2 \right]^{1/2}$$

The DF of an individual (or  $n$ th) harmonic component is defined as

$$DF_n = \frac{V_{on}}{V_{o1} \times n^2} \quad \text{for } n > 1$$

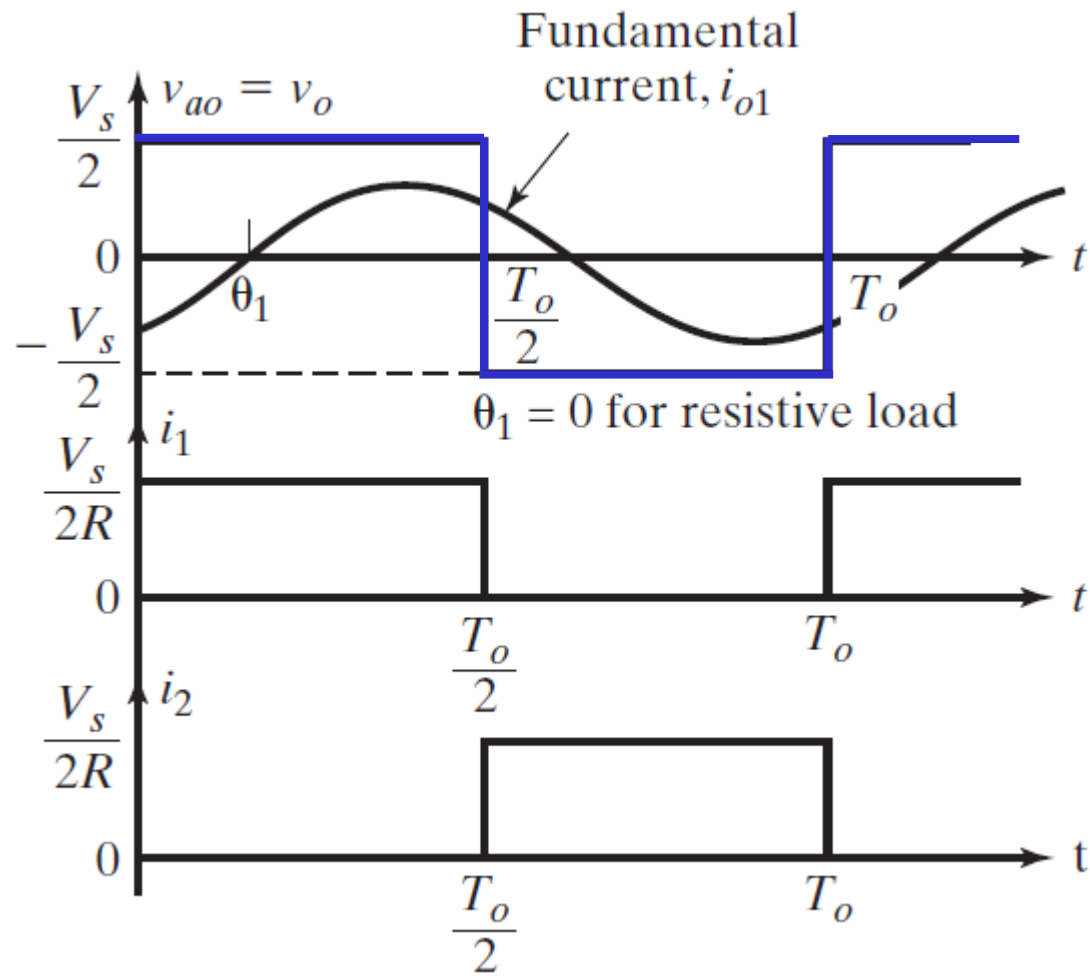
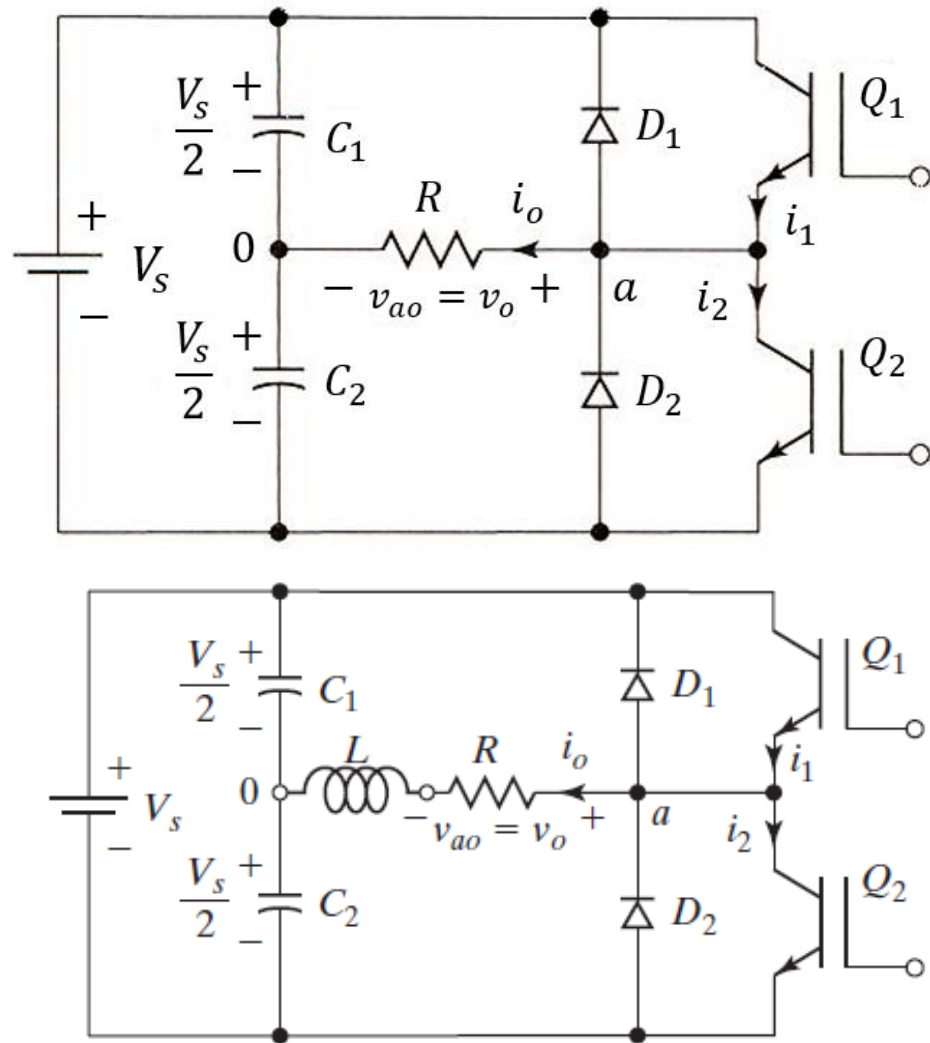
- **Lowest order harmonic (LOH)**: harmonic component whose frequency is closest to the fundamental one, and its amplitude is greater than or equal to 3% of the fundamental component.

## 1.2 Single-phase half-bridge VSI

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- Inverter consists of *two choppers* – 1) when *only*  $Q_1$  is turned ON for  $T_0/2$ , the instantaneous voltage across the load is  $V_s/2$ . 2) If *only*  $Q_2$  is turned ON for  $T_0/2$ , instantaneous voltage across load is  $-V_s/2$ .
- The logic circuit should be designed such that  $Q_1$  &  $Q_2$  *are not* turned ON at the *same time*.
- DC side is constant voltage, low impedance.
- The magnitude of output square-wave voltage is  $V_s/2$ .
- Note that the phase shift is  $\theta_1 = 0$  for a resistive load.

# 1.2 Single-phase half-bridge VSI



Waveforms of output voltage & transistor currents with resistive load



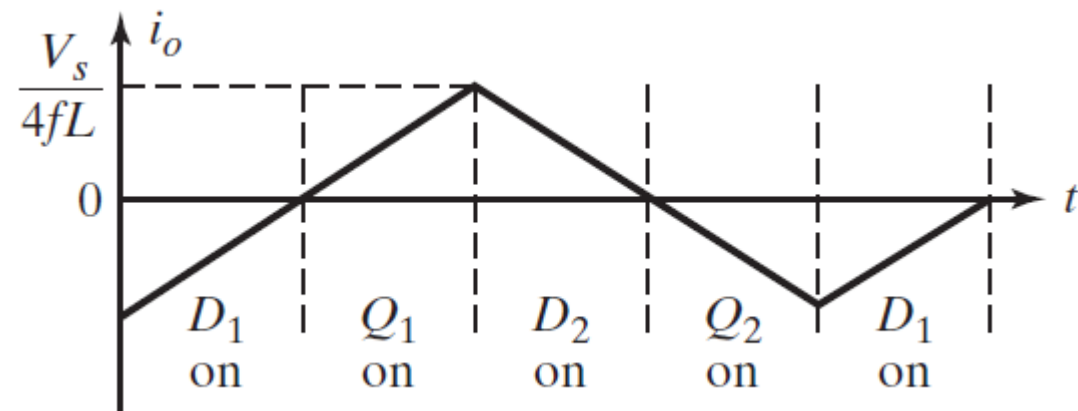
# Quantitative analysis 1

- The rms output voltage,  $V_o = \left( \frac{1}{T_o/2} \int_0^{T_o/2} \frac{V_s^2}{4} dt \right)^{1/2} = \frac{V_s}{2} \Rightarrow$  Why?
- Instantaneous output voltage can be expressed in Fourier series,  
$$v_o = \frac{a_0}{2} + \sum_{n=1}^{\infty} (a_n \cos n\omega t + b_n \sin n\omega t) = \sum_{n=1,3,5,\dots}^{\infty} \frac{2V_s}{n\pi} \sin n\omega t = 0 \text{ for } n = 2, 4, \dots$$
  - Due to the symmetry, all  $a_n$  (including  $a_0$ ) are 0 and  $b_n$  are calculated as  
$$b_n = \frac{1}{\pi} \left[ \int_{-\pi/2}^0 -\frac{V_s}{2} \sin n\omega t d\omega t + \int_0^{\pi/2} \frac{V_s}{2} \sin n\omega t d\omega t \right] = \frac{2V_s}{n\pi}$$
- The rms value of fundamental component of output is,  $V_{o1} = \frac{2V_s}{\sqrt{2}\pi} = 0.45V_s$



## 1.2.1 Inductive load

- For an inductive load, the *load current cannot* change immediately with the output voltage.
- If  $Q_1$  is turned *OFF* at  $t = T_0/2$ , the load current would continue to flow through  $D_2$ , *load, and the lower half* of the dc source until current fall to zero.
- Similarly, when  $Q_2$  is turned *OFF* at  $t = T_0$ , load current flows through  $D_1$ , *load, and the upper half* of the dc source.
- If diodes  $D_1$  or  $D_2$  conducts, energy is fed back to the dc source – *feedback diodes*
- For a purely inductive load, transistor conducts for  $T_0/4$ .



Load current with highly inductive load



# Quantitative analysis 2

- For an RL load, the instantaneous load current  $i_o$  can be found by dividing the instantaneous output voltage by the load impedance  $Z = R + jn\omega L$ , therefore

$$i_o = \sum_{n=1,3,5..}^{\infty} \frac{2V_s}{n\pi\sqrt{R^2 + (n\omega L)^2}} \sin(n\omega t - \theta_n)$$

where  $\theta_n = \tan^{-1}(n\omega L/R)$  is the phase of load impedance.

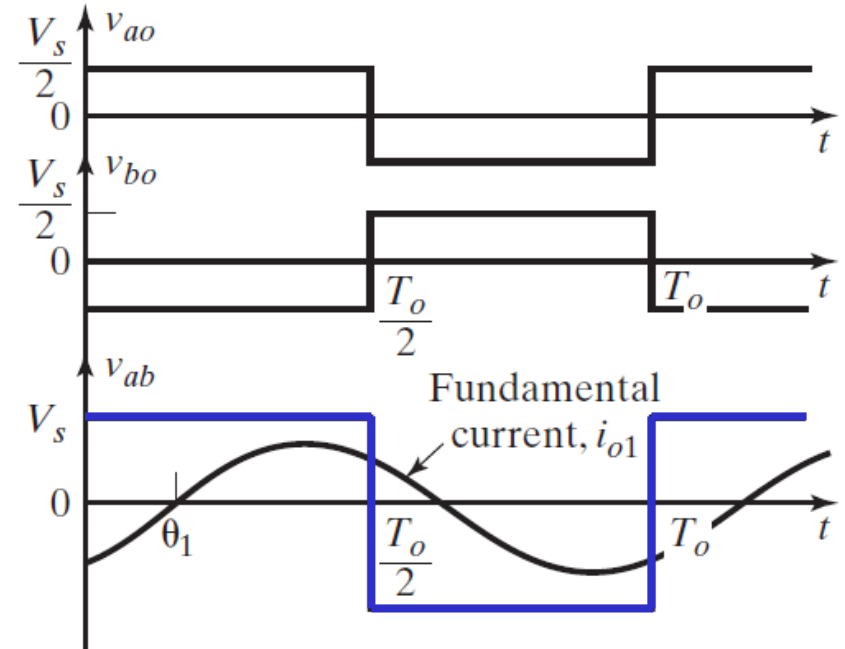
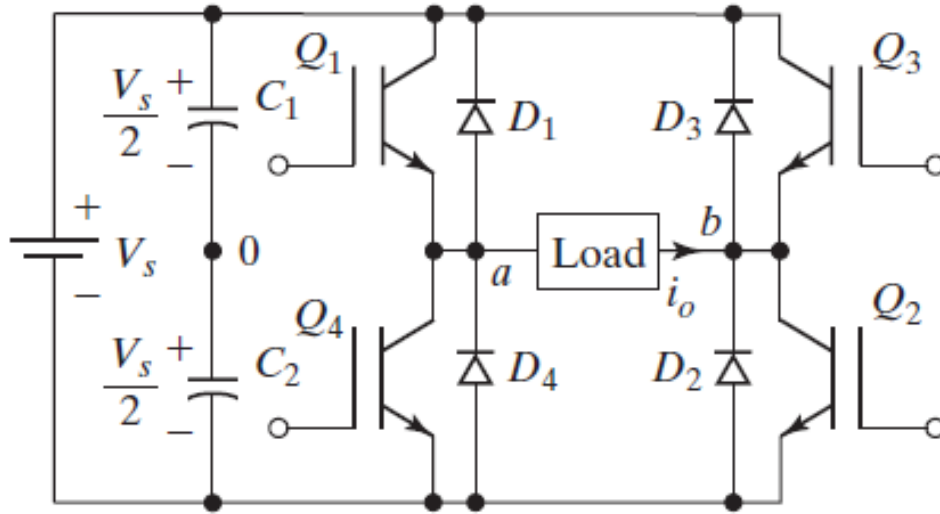
- The rms fundamental load current ( $n = 1$ ) is:

$$I_{o1} = \frac{2V_s}{\sqrt{2}\pi\sqrt{R^2 + (n\omega L)^2}}$$

- The fundamental output power ( $n = 1$ ) is,  $P_{o1} = I_{o1}^2 R$
- Power due to 1) fundamental current is the useful power, 2) harmonic currents is dissipated as heat and increases the load temperature.

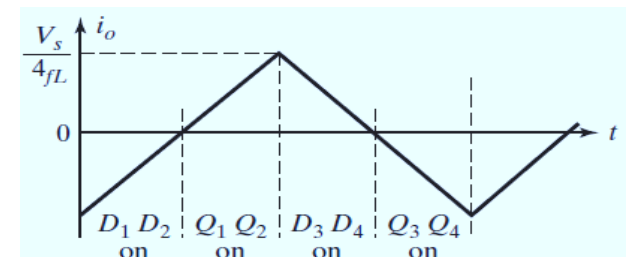


# 1.3 Single-phase full(H)-bridge VSI

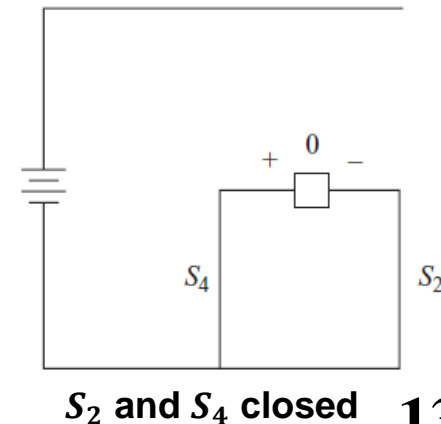
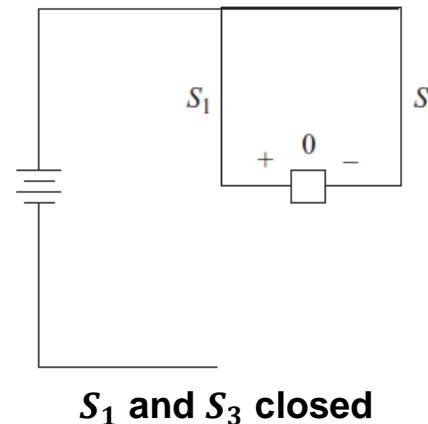
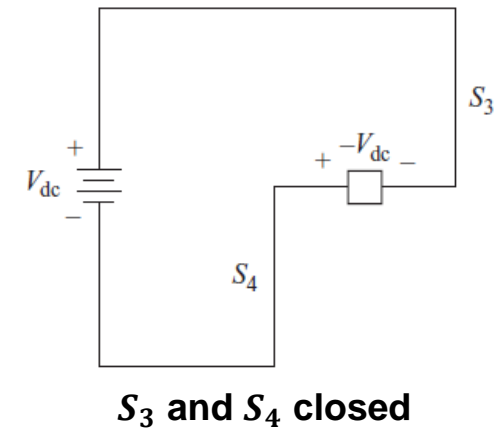
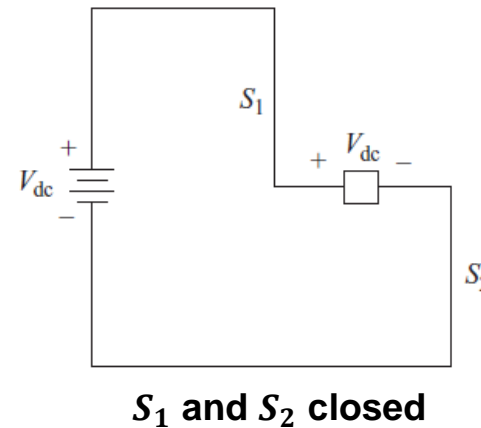
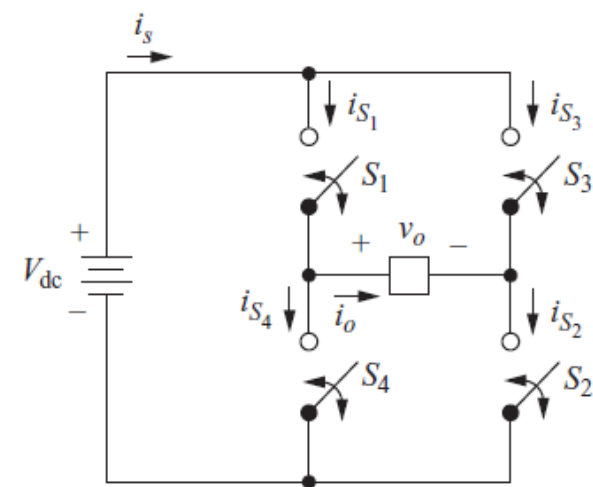


- Consists of 4 choppers – 1) When  $Q_1$  &  $Q_2$  are turned ON simultaneously,  $V_s$  appears across the load, 2) If  $Q_3$  &  $Q_4$  are turned ON simultaneously,  $-V_s$  appears across the load.
- When the load is highly inductive, the current waveform is triangular.
- The RMS output voltage is,

$$V_o = \left( \frac{2}{T_o} \int_0^{T_o/2} V_s^2 dt \right)^{1/2} = V_s$$

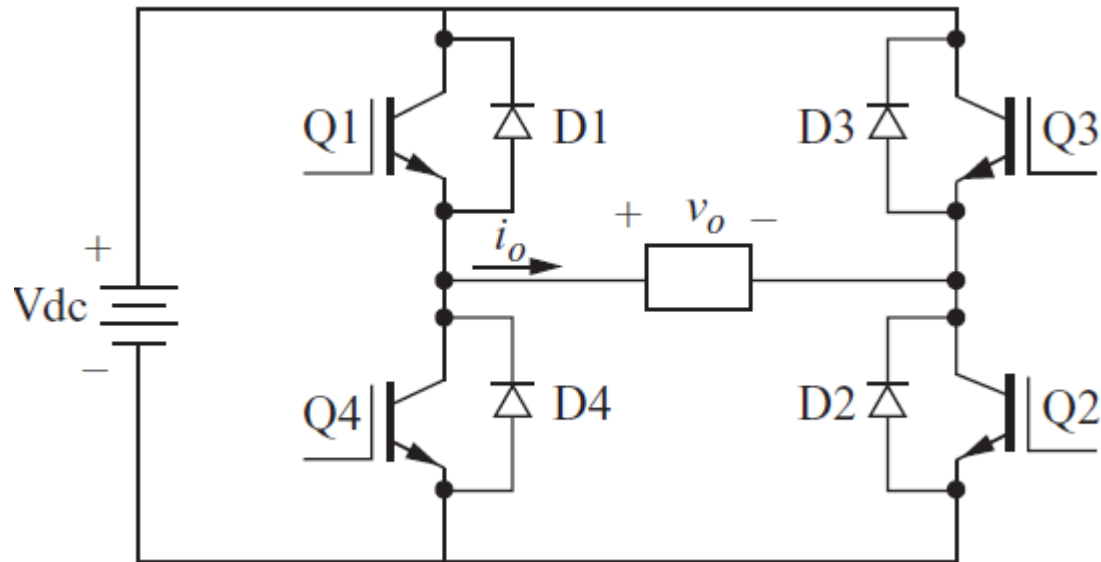


- There are four states available in the H-bridge, as shown at right.
- The voltages that can be applied to the load are  $+V_{dc}$ ,  $-V_{dc}$ , and 0.
- Notice that switches 1 and 4 should never be turned “on” simultaneously, and the same for switches 2 and 3 – *a short circuit would exist across the dc source*.
- Such a condition would be called a **shoot-through** fault.
  - To prevent shoot-through, a very short time interval called *the blanking time* must be inserted between the turning “off” of switch 1 and the turning “on” of switch 4.



# Why use diodes?

- They appear in case the load is not purely resistive. If it's inductive, which it usually is, then when switch 1 (for example) turns off, the inductive load current can commute over to the diode  $D_4$  until it goes to zero and reverses direction. Then switch  $Q_4$  can pick it up.



# Quantitative analysis 3

- The instantaneous output voltage in Fourier series form

$$v_o = \sum_{n=1,3,5,\dots}^{\infty} \frac{4V_s}{n\pi} \sin n\omega t$$

- The rms value of fundamental component of output ( $n = 1$ ) is

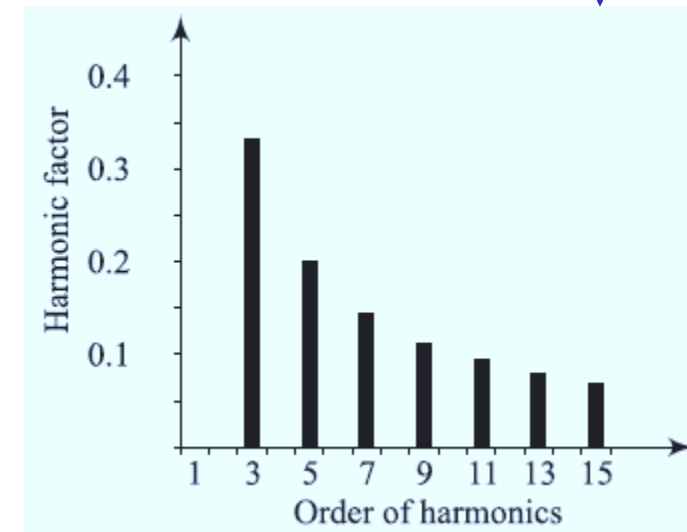
$$V_{o1} = \frac{4V_s}{\sqrt{2}\pi} = 0.9V_s$$

- The instantaneous load current  $i_o$  for an RL load becomes

$$i_o = \sum_{n=1,3,5,\dots}^{\infty} \frac{4V_s}{n\pi\sqrt{R^2 + (n\omega L)^2}} \sin(n\omega t - \theta_n)$$

## 2.0 PWM Inverters

- Usually, the output voltage of an inverter is a *square wave*. Drawbacks are:
  - 1) output voltage is constant & equal to supply voltage (cannot be controlled)
  - 2) output voltage consists of 3<sup>rd</sup> harmonic & other harmonics
- Pulse width modulation (PWM) should be used in the inverter to avoid above drawbacks – the *output pulse duration is modulated or varied* to control the output voltage. Most commonly used PWM techniques are:
  - 1) Single-pulse width modulation (SPWM)
  - 2) Multi-pulse width modulation (MPWM)
  - 3) *Sinusoidal pulse width modulation*
  - 4) Modified sinusoidal pulse width modulation





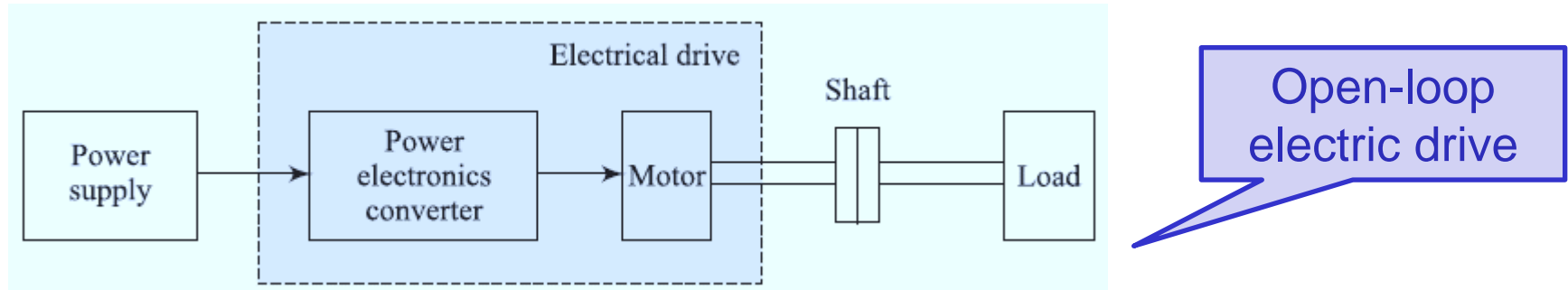
## 2.1 Other PWM Techniques

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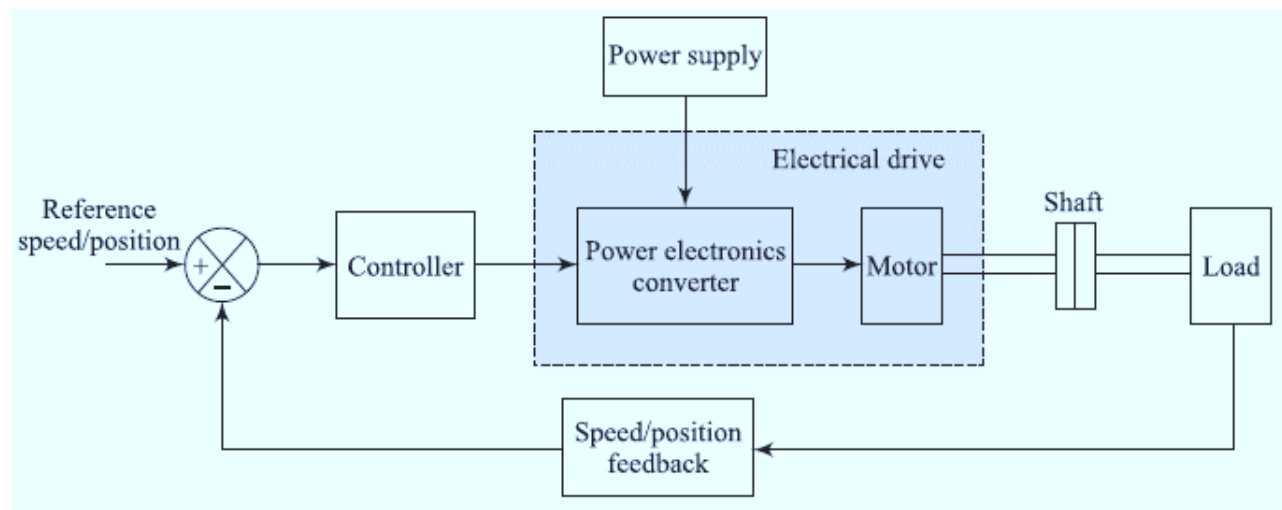
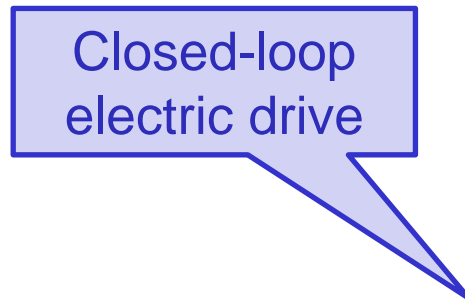
- Optimised PWM
  - PWM waveform are constructed based on certain performance criteria, e.g. THD.
- Harmonic elimination/minimisation PWM
  - PWM waveforms are constructed to eliminate some undesirable harmonics from the output waveform spectra.
  - Highly mathematical in nature
- Space-vector PWM
  - Using vectors to approximate a circle
  - Easy to generate and very commonly used

## 3.0 Electric Drives

- Electric drives are commonly used in many industrial applications
  - centrifugal pumps, robotics, elevators, conveyer belts etc.



- Power electronics converter used for interfacing between input power supply and electric motor.



## 3.0 Electric Drives

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- The *output of a power electronics converter* may be a variable dc or a variable ac with variable voltage and frequency.
- The *feedback signals* are the measured parameters of the load, i.e., speed and position.
- The *control circuit* is the heart of power electronics converter – generates triggering pulses to control thyristors of power converters.
  - low power circuit built using analog circuits, microprocessors, etc
- Electric drives are usually of mainly two types:
  - DC motor drives
  - AC motor drives  $\Longrightarrow$  1) Induction motor drives  
2) Synchronous motor drives

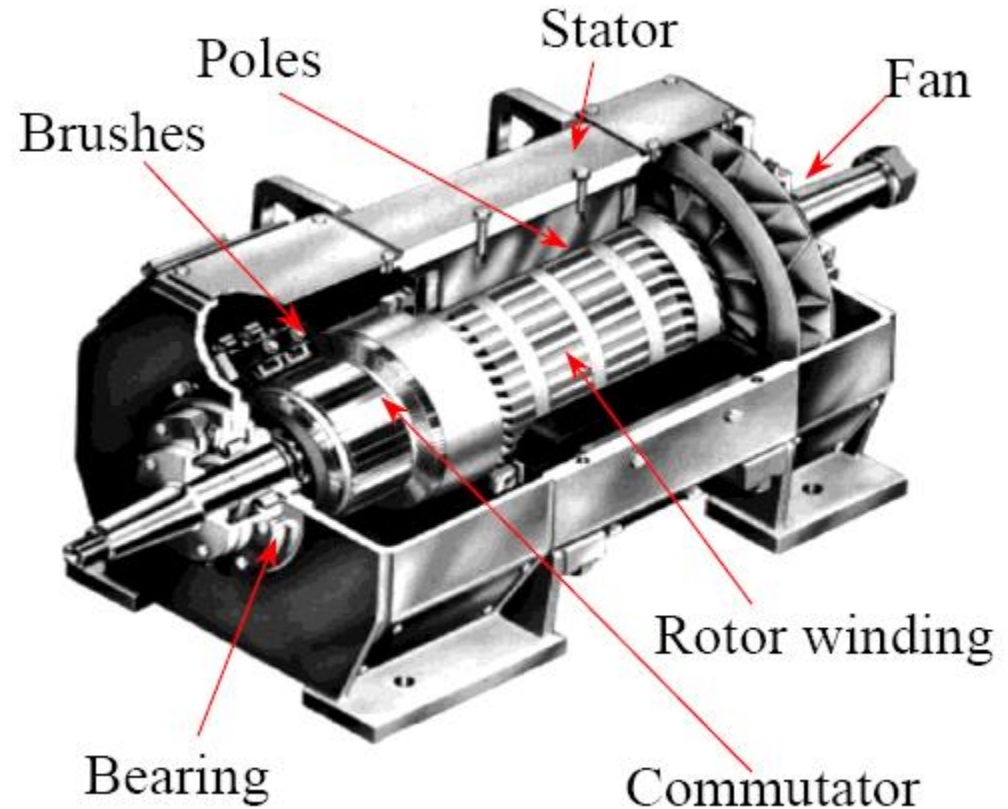
## 3.1 DC Motor Drives

### Three parts:

**Rotor (Armature)** –The rotating centre portion.

**Stator**–The static (stationary) windings around the rotor. In many small motors, the stator can be replaced with permanent magnets.

**Commutator**–The brush connection to the winding on the rotor.



## 3.1 Types of DC Motors

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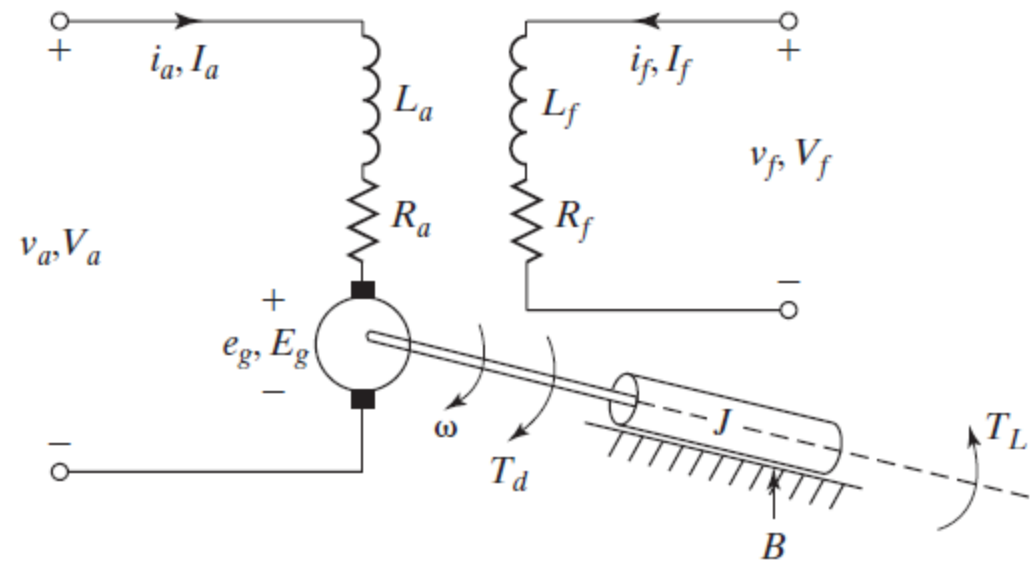
- Two types depending on type of field winding connections:
  - **Shunt:** field excitation is independent of armature circuit
    - controlled independently (*separately excited motor*)
    - armature and field currents are different
  - **Series:** the field excitation is in series with the armature
    - armature and field currents are same

## 3.1.1 Separately Excited DC Motor

- When *excited* by a field current ( $i_f$ ) and an armature current of  $i_a$  flows in the circuit, the *motor develops* a back *EMF* & a *torque* to balance the load torque at particular speed of motor.
- The  $i_f$  is *independent* of  $i_a$  and any change in one of them would not affect other current. Normally,  $i_f \ll i_a$ .
- Instantaneous field current  $i_f$  is described as

$$v_f = R_f i_f + L_f \frac{di_f}{dt}$$

- Instantaneous armature current can be found from,  $v_a = R_a i_a + L_a \frac{di_a}{dt} + e_g$
- The motor back emf (or *speed voltage*) is,  $e_g = K_v \omega i_f$



Equivalent circuit

## 3.1.1 Separately Excited DC Motor

- The torque developed by the motor,  $T_d = K_t i_f i_a$
- The developed torque must be equal to  $T_d = J \frac{d\omega}{dt} + B\omega + T_L$
- Under steady-state conditions, the time derivatives in the above equations are zero. Therefore, the speed of a separately excited motor can be found as

$$\omega = \frac{V_a - R_a i_a}{K_v i_f}$$

where,  $B$  = viscous friction constant, N.m/rad/s;  $K_v$  = voltage constant, V/A-rad/s

$K_t$  = torque constant, same as voltage constant,  $K_v$ .

$L_a$  = armature circuit inductance, H;  $R_a$  = armature circuit resistance,  $\Omega$ .

$L_f$  = field circuit inductance, H;  $R_f$  = field circuit resistance,  $\Omega$ .

$T_L$  = load torque, N.m.

## 3.1.2 Series Excited DC Motor

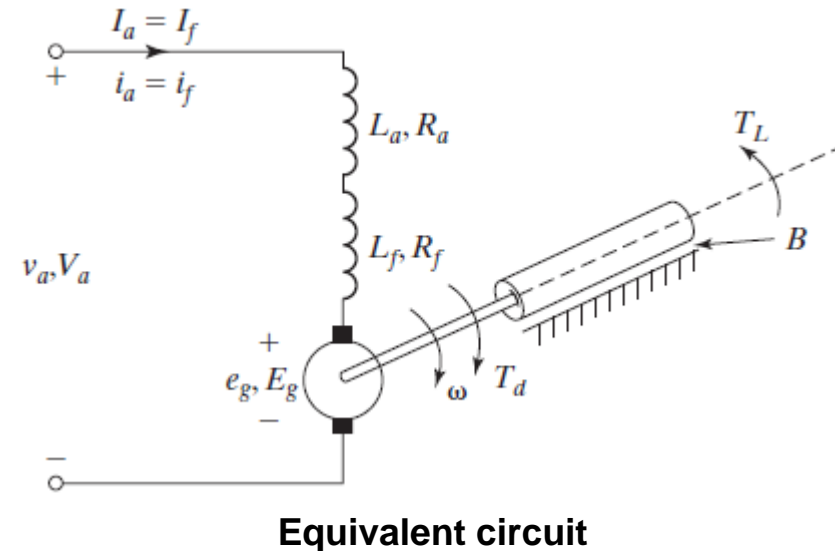
- The field circuit is designed to carry the armature current. The steady-state quantities:
- The motor back emf is,  $E_g = K_v \omega I_a$
- Instantaneous armature current can be found:  
 $V_a = (R_a + R_f)I_a + E_g = (R_a + R_f)I_a + K_v \omega I_f$
- The torque developed by the motor,

$$T_d = K_t I_f I_a = B\omega + T_L$$

- The speed of a series motor can be found as

$$\omega = \frac{V_a - (R_a + R_f)I_a}{K_v I_f}$$

- The speed can be varied by controlling the 1) armature voltage; or 2) armature current, which is a measure of the torque demand.
- Series motor can provide a high torque, especially at starting – commonly used in traction applications.





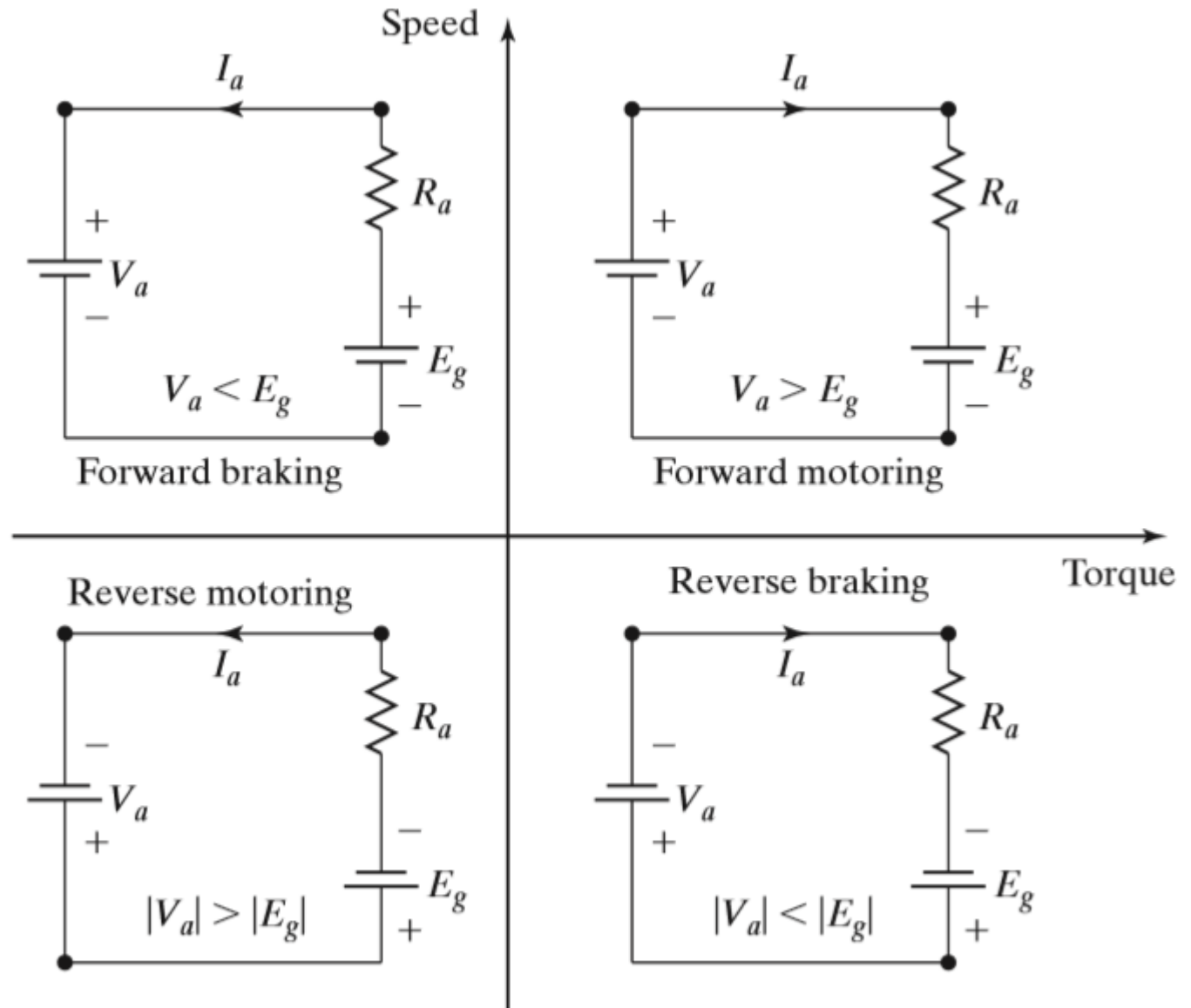
### 3.1.3 Operation Modes of a DC Motor

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In variable-speed applications, dc motor may be operating in one or more modes:

- **Motoring:**  $E_g < V_a$  and the motor drives the mechanical load.
- **Generating:** the motor is driven by a rotating machine.
- **Braking** (short-period operation):
  - Dynamic braking: re-connecting the motor as a generator by temporarily replacing the supply with a braking resistance  $R$ , and dissipating the generated power into a resistive load.
  - Regenerating braking: an extension of dynamic braking. The kinetic energy of the motor is converted into electricity and returned to the supply, which means  $E_g$  is greater than  $V_a$ .
  - Plugging: another type of braking by temporarily reversing the armature terminals to forcefully stop it.

# Four-quadrant operation (conditions)



## 3.1.4 Single-phase Full-converter Drives

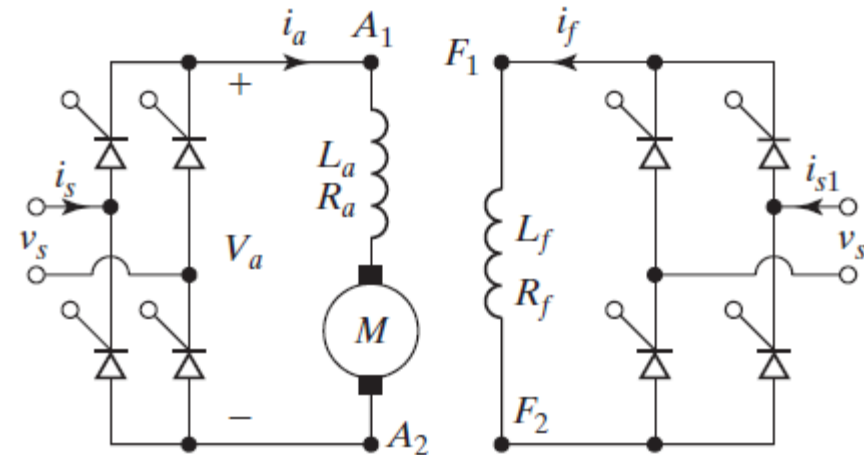
- The armature voltage is varied by a single-phase full-wave converter.
- The average armature voltage, with a single-phase full-wave converter in the armature, as

$$V_a = \frac{2V_m}{\pi} \cos \alpha_a \quad \text{for } 0 \leq \alpha_a \leq \pi$$

- Similarly, the field voltage is,

$$V_f = \frac{2V_m}{\pi} \cos \alpha_f \quad \text{for } 0 \leq \alpha_f \leq \pi$$

- For three-phase full-wave converter,
  - the average armature voltage,  $V_a = \frac{3\sqrt{3}V_m}{\pi} \cos \alpha_a \quad \text{for } 0 \leq \alpha_a \leq \pi$
  - the average field voltage,  $V_f = \frac{3\sqrt{3}V_m}{\pi} \cos \alpha_f \quad \text{for } 0 \leq \alpha_f \leq \pi$



## Example

A 15-hp, 220 V, 2000 rpm separately excited dc motor controls a load requiring a torque of  $T_L = 45 \text{ N}\cdot\text{m}$  at a speed of 1200 rpm. The field circuit resistance is  $R_f = 147\Omega$ , the armature circuit resistance is  $R_a = 0.25\Omega$ , and the voltage constant of the motor is  $K_v = 0.7032$ . The field voltage is  $V_f = 220 \text{ V}$ . The viscous friction and no-load losses are negligible. The armature current may be assumed continuous and ripple free. Determine a) the back emf  $E_g$ , b) the required armature voltage  $V_a$ , and c) rated armature current.

## Solution

$R_f = 147 \Omega$ ,  $R_a = 0.25 \Omega$ ,  $K_v = K_t = 0.7032 \text{ V/A rad/s}$ ,  $V_f = 220 \text{ V}$ ,  $T_d = T_L = 45 \text{ N}\cdot\text{m}$ ,  $\omega = 1200 \pi/30 = 125.66 \text{ rad/s}$ , and  $I_f = 220/147 = 1.497 \text{ A}$ .

# Example

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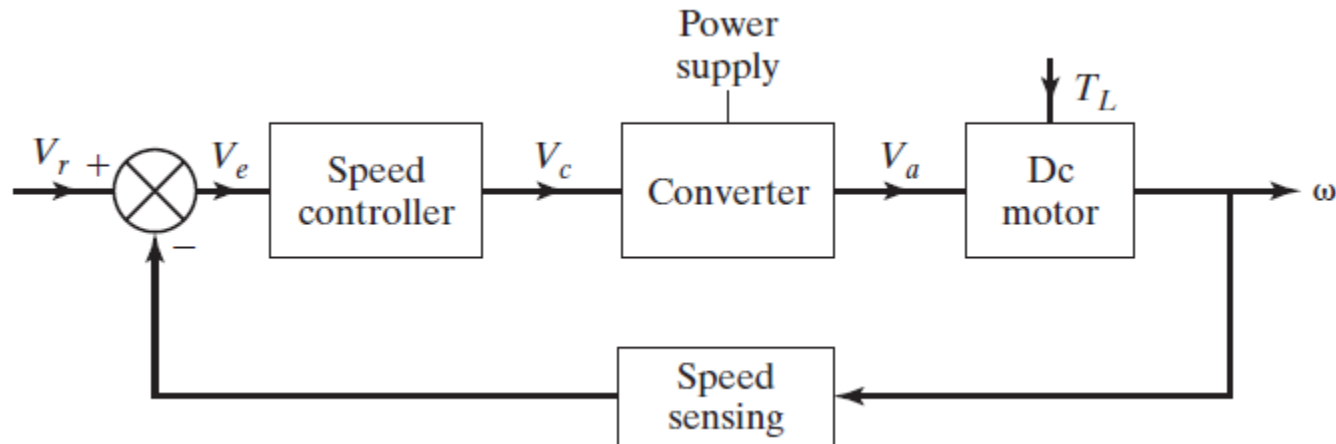
## Solution

$$a) T_d = K_t i_f i_a \Rightarrow i_a = 42.75 \text{ A}, E_g = K_v \omega I_f = 132.28 \text{ V}$$

$$b) V_a = R_a i_a + L_a \frac{di_a}{dt} + E_g \cong R_a i_a + E_g = 0.25 \times 42.75 + 132.28 = 142.97 \text{ V}$$

$$c) \text{ Because 1 hp is equal to 746 W, } I_{rated} = 15 \times 746 / 220 = 50.87 \text{ A}$$

## 3.1.5 Closed-loop Control of DC Drives



- The speed of dc motors changes with the load torque – to maintain a constant speed in practical drive systems; operate as *closed-loop feedback systems*.
- Advantages of improved accuracy, fast dynamic response, reduced effects of load disturbances and system nonlinearities.
- If the *speed of the motor decreases* due to the application of additional load torque, *the speed error  $V_e$  increases*.
- The *speed controller* response with an increased control signal to restore the motor speed to the original value.

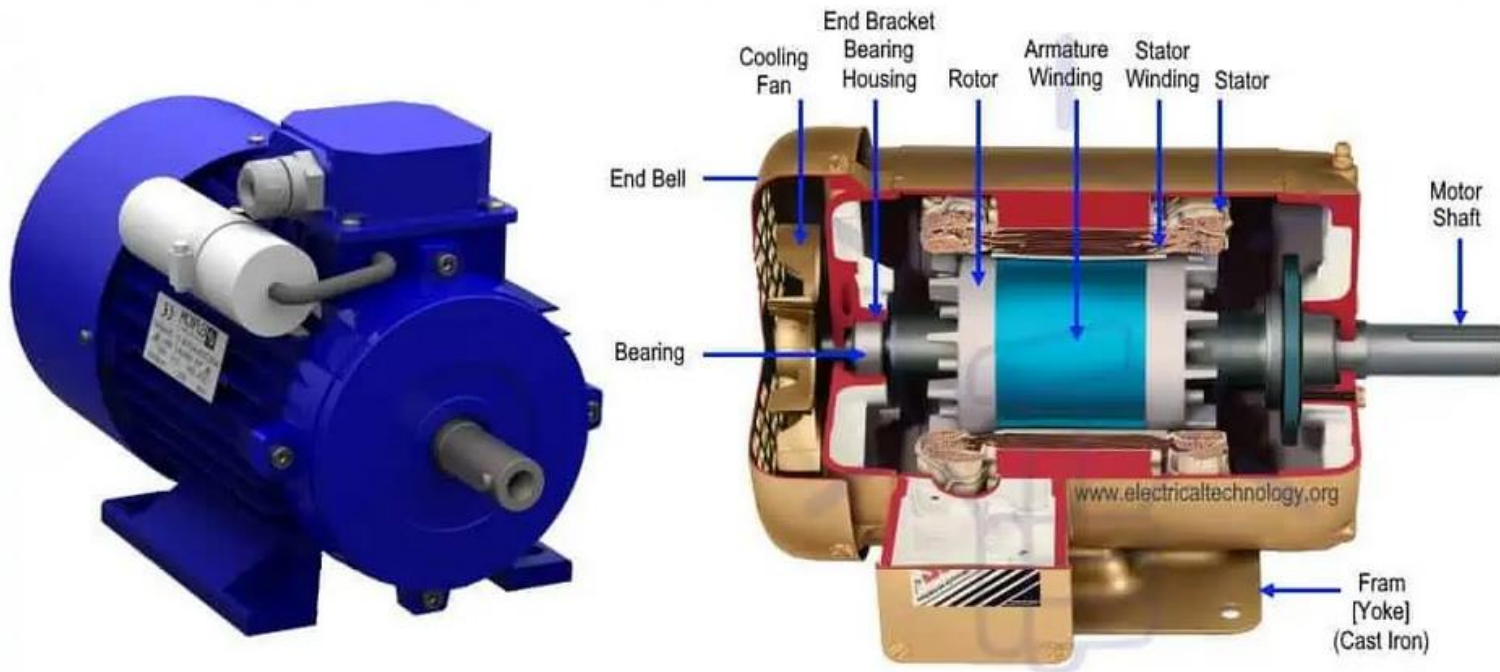


## 3.2 AC Motors

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- AC motors exhibit highly coupled, nonlinear, and multivariable structures as opposed to simple decoupled DC motors.
- Control of AC drives generally requires *complex control algorithms* that can be performed by microprocessors or microcomputers.
- AC drives are lightweight, inexpensive, low maintenance.
- Require *advanced feedback controller* such as adaptive control, sliding mode control, and field oriented control.
- **Types:** Induction motors, synchronous motors, stepper motors
- AC drives are replacing DC drives and are used in many industrial and domestic applications.

## 3.2.1 Induction Motor Drives

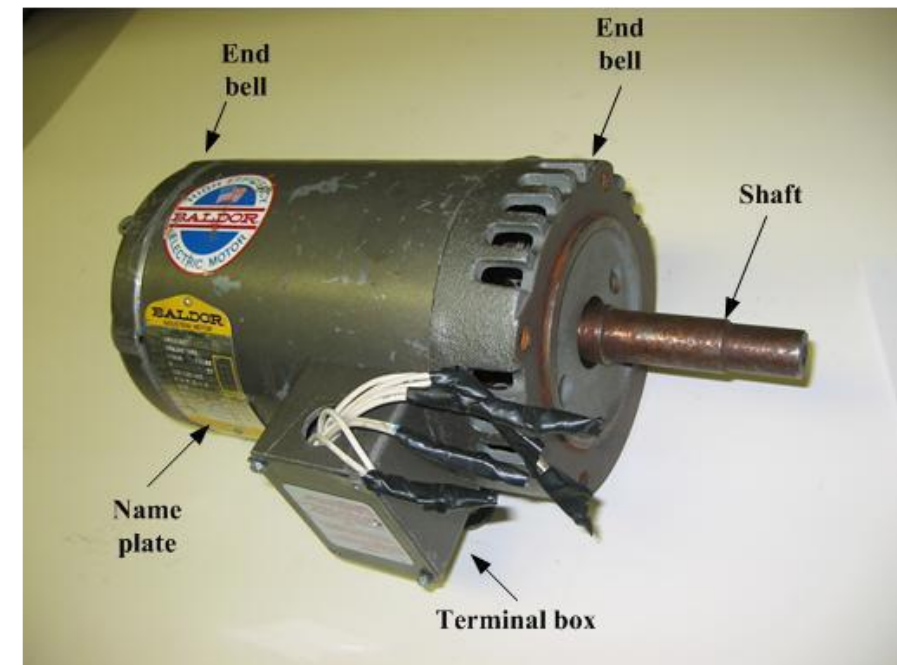
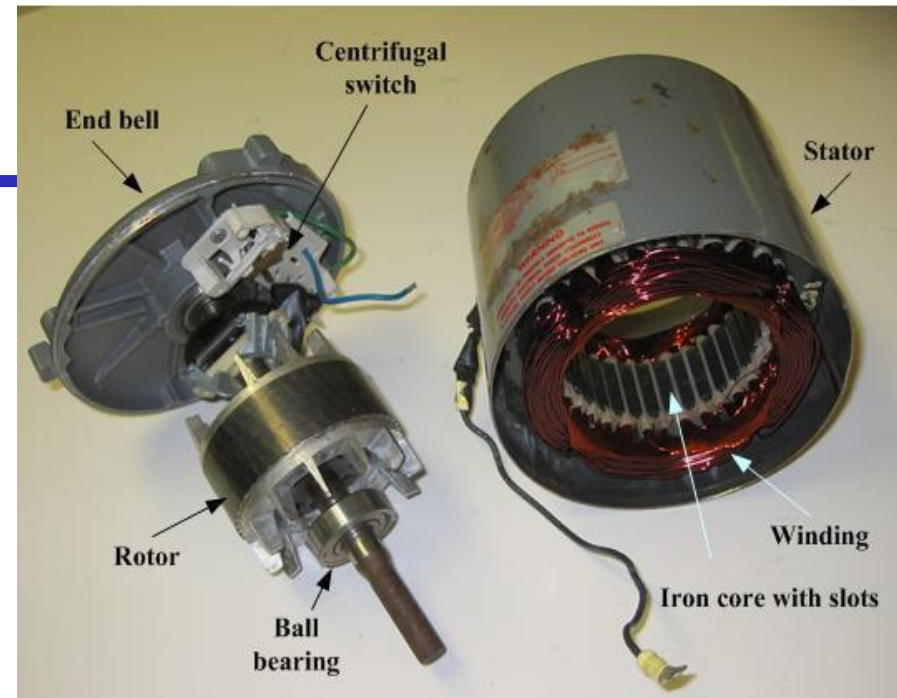


- The single-phase induction motor is the most frequently used motor in the world.
- Highly reliable and economical.
- For industrial applications, three-phase induction motors are used.



# Construction

- An induction motor consists of
  - Stator
  - Rotor
  - Housing
- The motor housing consists of
  - **Shaft:** the cylindrical middle piece that holds the stator iron core;
  - **End bell:** the two bell-shaped end covers holding the ball bearings.



## 3.2.2 Synchronous Motor Drives

- Synchronous motors have two windings: 3-phase armature winding on the stator and a field winding on the rotor.
- Always operates at synchronous speed (constant speed).
- The power factor can be controlled by varying its field current.
  - Cylindrical rotor synchronous motors
  - Salient pole synchronous motors
  - Reluctance synchronous motors
  - *Permanent magnet synchronous motors*



# Summary

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- DC-AC converters are known as *inverters*.
- *Feedback diodes* are required to transfer the energy stored in the load inductance back to the DC source.
- The most efficient method of controlling the gain is to incorporate *PWM control* in inverters.
- Electrical motors: DC and AC motor drives.
- DC drives: Shunt: field excitation is *independent* of armature circuit  
Series: field excitation is *in series* with armature circuit
- AC Motor drives: Induction motor drives, Synchronous motor drives

***See you in the next class (May 05<sup>th</sup>)***

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**The End**