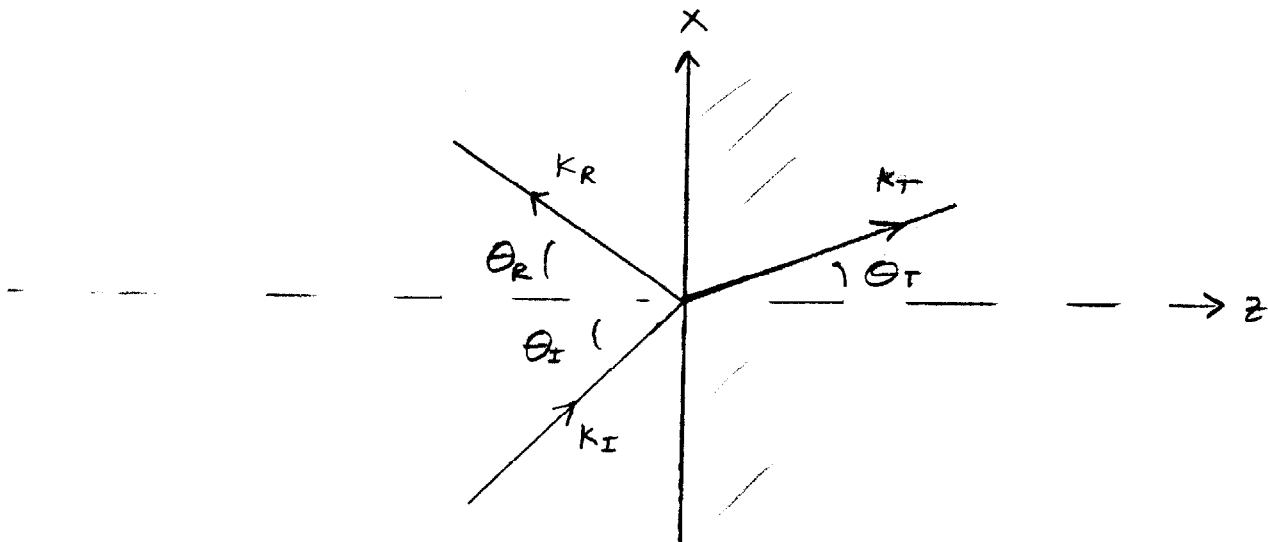


Chapter 9, lecture

Reflection and transmission of electromagnetic waves at a boundary.



We would like \tilde{E}_R , \tilde{E}_T in terms of \tilde{E}_I
To get these, along with other information,
we will do the following:

- 1) Write expressions for single frequency incident, reflected and transmitted waves
- 2) The requirement that the oscillatory portion of each wave be the same at the boundary leads to $\theta_I = \theta_R$ and Snell's law.
- 3) Apply specifically electromagnetic boundary conditions gives the desired relations for the complex amplitudes of the waves.

First, write expressions for the waves:

$$E_I = \tilde{E}_{0I} e^{i(\vec{k}_I \cdot \vec{r} - \omega t)}$$

$$E_R = \tilde{E}_{0R} e^{i(\vec{k}_R \cdot \vec{r} - \omega t)}$$

$$E_T = \tilde{E}_{0T} e^{i(\vec{k}_T \cdot \vec{r} - \omega t)}$$

Matching at the boundary:

$$\tilde{E}_{0I} e^{i(\vec{k}_I \cdot \vec{r} - \omega t)} + \tilde{E}_{0R} e^{i(\vec{k}_R \cdot \vec{r} - \omega t)} = \tilde{E}_{0T} e^{i(\vec{k}_T \cdot \vec{r} - \omega t)}$$

The exponent of each term must be the same

$$k_{Ix}x + k_{Iy}y = k_{Rx}x + k_{Ry}y = k_{Tx}x + k_{Ty}y$$

Since $z=0$

$$k_{Ix} = k_{Rx} = k_{Tx}$$

$$k_{Iy} = k_{Ry} = k_{Ty}$$

We may choose the coordinate system so that the incident wave is in the xz plane.

Then, all waves must be in the xz plane (the plane of incidence).

Using $k_{Ix} = k_{Rx}$

$$k_I \sin \theta_I = k_R \sin \theta_R$$

$$\frac{\omega}{v_1} \sin \theta_I = \frac{\omega}{v_1} \sin \theta_R$$

$$\boxed{\theta_I = \theta_R}$$

{ the angle of incidence
is equal to the angle
of reflection

Also $k_{Ix} = k_{Tx}$

$$k_I \sin \theta_I = k_T \sin \theta_T$$

$$\frac{k_I}{k_T} = \frac{\sin \theta_T}{\sin \theta_I}$$

$$\boxed{\frac{v_2}{v_1} = \frac{n_1}{n_2} = \frac{\sin \theta_T}{\sin \theta_I}}$$

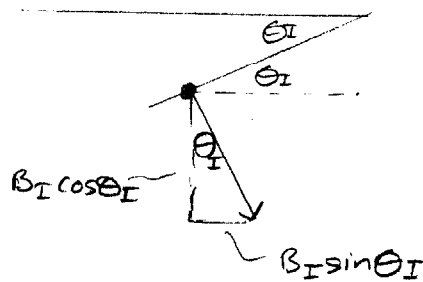
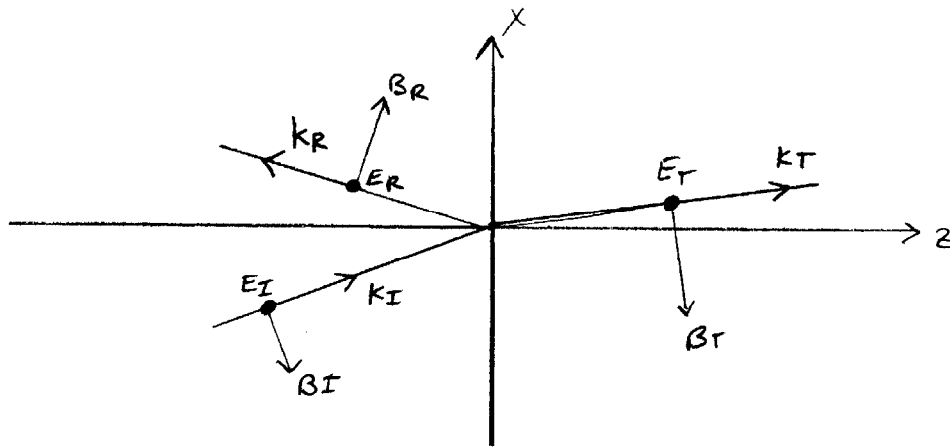
{ since $v = c/n$
Snell's Law

That's as far as we can go (pretty far!) without the specific electromagnetic boundary conditions.

$$\epsilon_1 E_{\text{Left}}^{\perp} = \epsilon_2 E_{\text{Right}}^{\perp}, \quad E_{\text{Left}}'' = E_{\text{Right}}''$$

$$B_{\text{Left}}^{\perp} = B_{\text{Right}}^{\perp}, \quad \frac{1}{\mu_1} B_{\text{Left}}'' = \frac{1}{\mu_2} B_{\text{Right}}''$$

Now, to go further, pick a specific polarization. Let's choose perpendicular, since Griffiths does the parallel case.



$$\textcircled{1} E_{\text{left}}^{\perp} = E_{\text{right}}^{\perp} = 0$$

$$\textcircled{2} B_{\text{left}}^{\perp} = B_{\text{right}}^{\perp}$$

$$\tilde{B}_{0I} \sin \theta_I + \tilde{B}_{0R} \sin \theta_R = \tilde{B}_{0T} \sin \theta_T$$

$$\text{or, } \frac{\tilde{E}_{0I}}{v_1} \sin \theta_I + \frac{\tilde{E}_{0R}}{v_1} \sin \theta_R = \frac{\tilde{E}_{0T}}{v_2} \sin \theta_T$$

This is

$$\tilde{E}_{0I} + \tilde{E}_{0R} = \frac{v_1}{v_2} \frac{\sin \theta_T}{\sin \theta_I} \tilde{E}_{0T}$$

$$\uparrow n_1/n_2 = \frac{c/v_1}{c/v_2}$$

$$\tilde{E}_{0I} + \tilde{E}_{0R} = \tilde{E}_{0T}$$

$$(3) E''_{\text{left}} = E''_{\text{right}}$$

$$\tilde{E}_{0I} + \tilde{E}_{0R} = \tilde{E}_{0T} \quad \text{same as above}$$

$$(4) \frac{1}{\mu_1} B''_{\text{left}} = \frac{1}{\mu_2} B''_{\text{right}}$$

$$-\frac{1}{\mu_1} \tilde{B}_{0I} \cos \theta_I + \frac{1}{\mu_1} \tilde{B}_{0R} \cos \theta_I = -\frac{1}{\mu_2} \tilde{B}_{0T} \cos \theta_T$$

$$-\tilde{E}_{0I} + \tilde{E}_{0R} = -\frac{\mu_1 v_1}{\mu_2 v_2} \frac{\cos \theta_T}{\cos \theta_I} \tilde{E}_{0T}$$

$$= -\beta \alpha \tilde{E}_{0T}$$

using the book definitions $\alpha \equiv \frac{\cos \theta_T}{\cos \theta_I}$, $\beta \equiv \frac{\mu_1 v_1}{\mu_2 v_2}$

combining 3 & 4

$$-\tilde{E}_{OI} + \tilde{E}_{OR} = -\beta\alpha E_{OI} - \beta\alpha E_{OR}$$

$$\tilde{E}_{OR} = \left(\frac{1 - \beta\alpha}{1 + \beta\alpha} \right) \tilde{E}_{OI}$$

$$\tilde{E}_{OT} = \left(\frac{2}{1 + \beta\alpha} \right) \tilde{E}_{OI}$$

Reflection coefficient $\equiv \frac{\text{Reflected intensity}}{\text{Incident intensity}}$

$$R \equiv \frac{I_R}{I_I} = \left(\frac{E_{OR}}{E_{OI}} \right)^2 = \left(\frac{1 - \beta\alpha}{1 + \beta\alpha} \right)^2$$

$$\text{Since } I_I = \langle S \rangle \cdot \hat{z} = \frac{1}{2} \epsilon_1 \nu_1 E_{OI}^2 \cos \theta_I$$

$$I_R = \langle S \rangle \cdot \hat{z} = \frac{1}{2} \epsilon_1 \nu_1 E_{OR}^2 \cos \theta_R$$

$$\text{and } \theta_R = \theta_I$$

Similarly,

$$T \equiv \frac{I_T}{I_I} = \frac{\epsilon_2 \nu_2}{\epsilon_1 \nu_1} \left(\frac{E_{OT}}{E_{OI}} \right)^2 \frac{\cos \theta_T}{\cos \theta_I}$$

This is:

$$\frac{\epsilon_2 \mu_2 v_2}{\epsilon_1 \mu_1 v_1} \frac{\mu_1}{\mu_2} \left(\frac{2}{1 + \beta \alpha} \right)^2 \propto$$

$$= \frac{v_1 \cancel{v_2}}{v_2 \cancel{v_1}} \frac{\cancel{v_2}}{\cancel{v_1}} \frac{\mu_1}{\mu_2} \propto \left(\frac{2}{1 + \beta \alpha} \right)^2$$

$$T = \beta \alpha \left(\frac{2}{1 + \beta \alpha} \right)^2$$

using definitions of α , β and

$$I_T = \langle S \rangle \cdot \hat{z} = \frac{1}{2} \epsilon_2 v_2 E_{0T}^2 \cos \theta_T$$

$$R + T = \frac{4\beta\alpha}{(1+\beta\alpha)^2} + \frac{(1-\beta\alpha)^2}{(1+\beta\alpha)^2} = \frac{1 - 2\beta\alpha + (\beta\alpha)^2 + 4\beta\alpha}{(1+\beta\alpha)^2}$$

$$= \frac{1 + 2\beta\alpha + (\beta\alpha)^2}{(1+\beta\alpha)^2} = \frac{(1+\beta\alpha)^2}{(1+\beta\alpha)^2} = 1$$