# Investigations on Three-phase Grid-Connected Inverter using PWM Controllers

#### Abstract

In recent years, a Multilevel Inverter (MLI) topology is highly preferred in the various renewable energy applications for converting power due to their merits. In this paper, a three-phase inverter has been designed for grid-connected applications using Proportional Integral (PI) current controller scheme. To generate sequence, the Level shift (LS) and Phase Shift (PS) Pulse Width Modulation (PWM) methodologies are adapted. This topology has been designed with two stages they are DC-DC conversion stage and DC-AC conversion stage. The DC-DC conversion stage is used enrichment of input DC voltage which is obtained from the solar PV array. The PI current controller has been designed to regulate the grid current with park transformation. The performances of the inverter have been examined in terms of Total Harmonic Distortion (THD) using different PWM techniques and also investigated with existing research works. The developed results are verified using MATLAB/ Simulink.

Keywords: MLI, LS-PWM, PS-PWM, PI, THD, MLI.

## 1 Introduction

The development of high power converter topologies is growing day by day and multilevel inverters are being concentrated researchers[1]. Particularly, MLI topologies are remarkably commended for by researchers for high power applications due to their merits such modular in structure. lesser filtering requirements [2]. In [3], the authors have been investigated different types of basic MLI topologies and also discussed various hybrid MLI topologies for RES applications. The MLIs can operate both a fundamental frequency (50Hz) as well as high switching frequency (kHz ranges) [4]. Some of the few authors only concentrated and investigated the single dc source-based MLI instead of multiple dc sources and it is suitable for solar photovoltaic applications [5]. Even though, MLIs topologies are applied in various industrial and research applications and control the inverter diversified PWM controller has been applied [6]. The different types of multi-carrier PWM techniques have been applied to the five inverters and also investigated phase shift control schemes [7]. The different controllers **PWM** have investigated by the authors and also suggested to the modular MLI structure [8]. Recently, a Multi-Carrier PWM (MC-PWM) based modified MLIs have been proposed by minimizing the number of switching count [9]. In [10], 3-phase

MLI topologies have been reported for high power applications using MC-PWM. proposed topology is presented with less number of switches in comparison with CHB. The CHB has modularity in structure. In this paper, the different type of modular structure has been discussed. So, the cost of design is significantly reduced with this type of inverters [11]. This paper deals with the various types of MLIs topologies using a reduced number of switching counts and also investigated hybrid MLIs [12]. In [13] transformer based inverter has been presented for three-phase and single applications to help of the single dc sources and transformer. To inject the sinusoidal current to the grid, a different kind of closed controller are discussed [14]. In order to control the sinusoidal current, a PI-based current regulator is used in this inverter circuit. Multi-carrier PWM based modular MLI inverter for renewable energy applications is investigated using asymmetrical dc input [15]. From the discussion, it is clear that multi-carrier PWM techniques have been suitable for the characteristics control of modular MLI topologies. In this paper, different PWM controllers have been applied and tested.

## 2 Three-Phase Five-level Inverter

The Multilevel inverter is applied to control both the standalone and grid-connected applications with the help of various control methodologies. Number MLIs topologies have been discussed in the literature review and also noted limitations. The block diagram of the various PWM controlled three-phase MLI inverter is shown in Fig.1. In this research work, there are two converters have been designed to converter RES power and transferred to the grid network. The output of the PV array is connected to boost converter and it is used to match impedance to inverter network. This is work is normally achieved with the help of maximum power point tracking algorithms. In this P&O have been applied to extract the maximum power available from the Solar PV array. The second stage is used to generate a five-level output voltage of the DC bus and injected the power to the grid through a passive filtering network. The power circuit of the PWM controlled three-phase MLI and their operating modes are shown in Fig. 2 (a) and (b) respectively.

The suggested MLI for grid-connected applications have been a less number of power switches as similar to the other existing MLI topologies. This topology is comprised of five switches per phase, hence 15-switches are required for making a three-phase system. Out of 5-switches, Sa1-Sa4 switches are forming H bridge inverter. The arrangement of Sa5 switches along with four diodes is called an auxiliary switch. In the suggested MLI switches Sa1, Sa 2, and Sa5 are operated at 20 kHz frequency, the remaining two switches Sa3 and Sa4 are operated in the 50Hz frequency. Table 1 indicates the comparison between the existing and suggested MLI topologies. Fig. 3 represents the output voltages and currents of the inverter with various Modulation Index (MI) values. Fig. 3 (a-c) are indicated the phase voltages of the inverter at MI = 1.1, 0.7, and 0.4. Fig. 3 (d-f), are indicated the phase currents of the inverter at MI = 1.1, 0.7, and 0.4. Fig. 3 (g), 3 (h), and 3 (i) are represented the three-phase load voltages of the inverter MI = 1.1,at 0.7, and

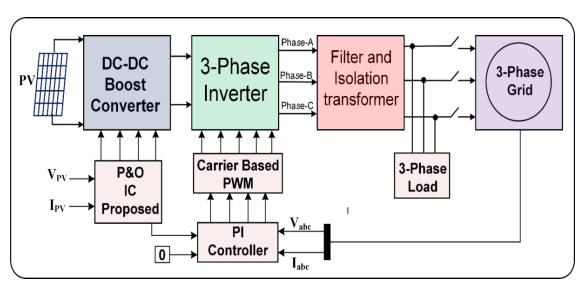
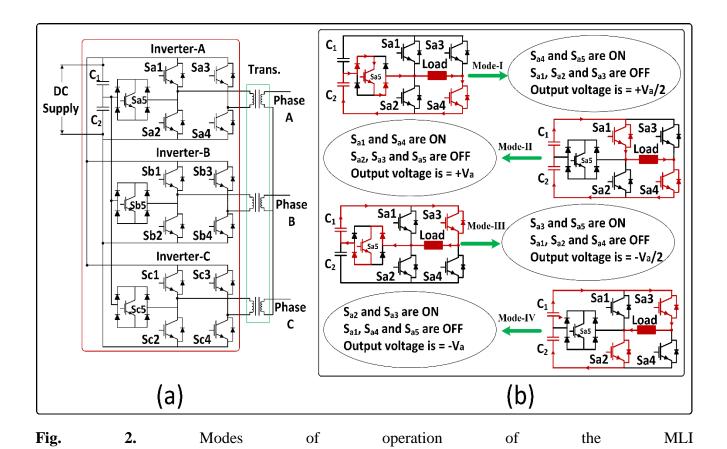


Fig. 1. Circuit diagram of the proposed MLI system



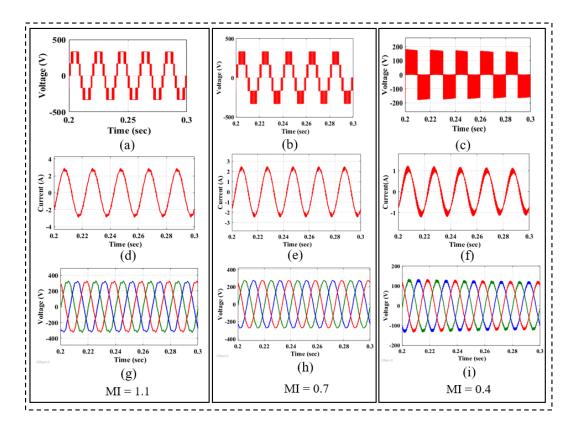


Fig. 3. Output voltages and currents of the inverter with various Modulation Index (MI) values

**Table 1.** Components required for the suggested topology and existing topologies

| Components           | Reference |      |           |
|----------------------|-----------|------|-----------|
|                      | [5]       | [11] | Suggested |
| Active<br>Switches   | 24        | 24   | 15        |
| Input DC<br>Sources  | 01        | 01   | 01        |
| DC Bus<br>Capacitors | 01        | 01   | 02        |
| Transformers         | 06        | 02   | 01        |
| Total                | 32        | 28   | 19        |

#### 3 PWM Controllers

## 3.1 Sine PWM (SPWM) Controllers

The SPWM techniques are the most familiar PWM controller for the regulation of the inverter. The SPWM is classified into two types gain (i) Phase Shift PWM (PS-PWM) and (ii) Level Shift PWM (LS-PWM). These two controllers are mainly suitable for controlling modular MLIs. In this paper, both PS-PWM and LS PWM are applied to the three-phase inverter for controlling the inverter and simulated using MATLAB/Simulink. The switching logic of the LS-PWM technique is given in Fig. 4.

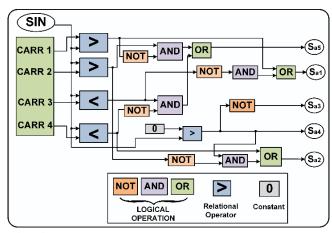


Fig. 4. Switching Logic of LS-PWM (PD)

## 3.2 Phase-Shift PWM controller

In PS-PWM all carriers are maintained equal amplitude and frequency. For the M-level inverter, M-1 carrier signals are required to generate the switching pulses. Therefore, four carriers are required for the five-level inverter and all carriers are equal magnitudes. In PS-PWM, each carrier maintains a certain phase shift with each other carrier and The phase shift angle can be calculated using the equation (1) Phase shift angle for the M level inverter is given by

$$PS = 360^{\circ}/(M-1)$$
 (1)

Where; M-number of levels. For the five-level inverter phase shift between each other must be 90°. Fig. 5 represents the Phase shift PWM technique.

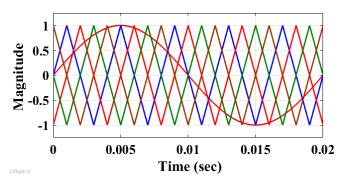


Fig. 5 PS- PWM technique

# 3.3 Level-Shift PWM Controllers

Another efficient control technique for the inverter is known as LS-PWM. For five-level inverter requires four carrier signals and one reference signal to generate the pulses to the inverter. For the M-level inverter, M-1 carriers to be considered.

$$M_{inv} = \frac{A_m}{(m-1)A_C} \tag{2}$$

Where; Am is the amplitude of the reference signal and Ac is the amplitude of the carrier signals. When the amplitude of the reference signal is greater than the carrier signal, then the only pulse was generated for inverter switches. The LS-PWM is again classified into three types those are APOD, POD, and PD. Fig. 4 represents the switching logic for the PS-PWM and LS-PWM control techniques. The frequency modulation ration of the signal is given by

$$M_f = (f_s/f_r) \tag{3}$$

Where; fs-represented the fundamental frequency, fr-represented carrier frequency. In the PD-PWM technique, four carriers are to be considered for pulse generation. Out of four carriers, the upper two carriers are positive from the reference point and the lower two carriers are negative from the reference point. Fig. 6 represents the PD-PWM technique, in this, all carriers are maintaining equal magnitude and phase shift. Fig. 7 represents the POD-PWM technique, in this, all positive carriers are maintaining equal magnitudes and phase shift. But, the negative carriers are maintaining the 180° phase shift with positive carriers. Fig. 8 represents the APOD-PWM technique, in this, all carriers are maintaining equal magnitude and each carrier maintains a 180° phase shift with other carriers.

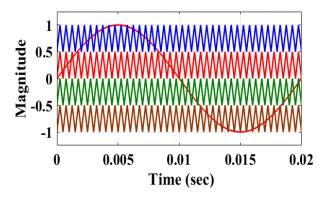


Fig. 6. PD-PWM technique

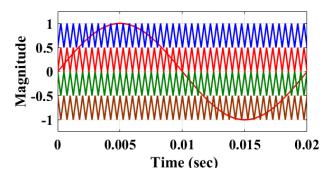


Fig. 7. POD-PWM technique

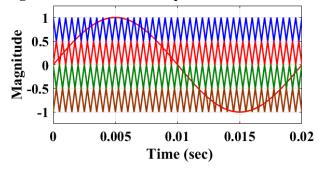


Fig. 8. APOD-PWM

## 4 PI current regulators

In order to control the grid current, PI current regulator has been used in the work. The block diagram of the closed-loop controller is shown in Fig. 9.

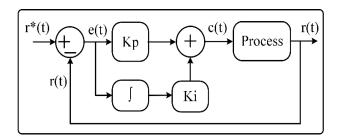


Fig. 9. Block diagram of the PI controller

$$G_c(s) = K_p \left( 1 + \frac{1}{k_i S} \right) = K_p \left( \frac{K_i S + 1}{K_i S} \right)$$
 (4)

From Fig. 9, r\*(t) - Reference value, r(t)-actual value, and e(t)-error value. The behavior of a three-phase electrical system is given by its voltage and the current equation and coefficients in this differential equation are varying with

respect to time. The mathematical modelling of such a system is very difficult. To solve such a problem through transformation techniques. The output side parameters are measured and converted from three-phase quantity to two-phase quantity for easy and fast mathematical computation of the electrical parameters. The three-phase quantity is converted into a stationary reference frame and again converted into a synchronously rotating reference frame

and it is shown in Fig.10. The direct and quadrature axis has a fundamental and oscillating component. The transformation angle for the transformation is obtained from the Phase Locked Loop (PLL) in synchronization with the grid voltage. MPPT algorithm measures the grid voltage and current and compares the output with the direct and quadrature component of the grid voltage and current.

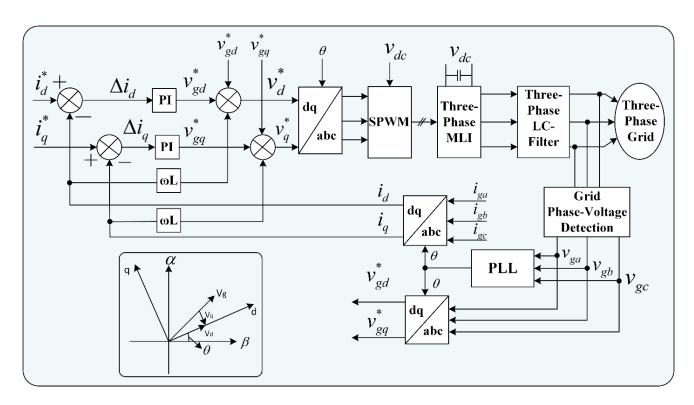


Fig. 10. Control structure of the inverter

The error signal is tuned using a PI controller and the output is given to the inverse Clarke transformation and inverse park transformation to convert the controlled quantity from two axis to three-phase quantity. The dq0-abc converter is used for driving the three-phase five-level inverter from a carrier-based PWM generator

#### 5 Simulation Results.

In this section, the simulation results of the PWM controller three-phase inverter have been discussed and verified through MATLAB/Simulink. The inverter switches are

controlled by SPWM (PS-PWM and LS-PWM) and the PI controller is used to design a current controller for a grid-connected inverter system. Fig. 11 represents the corresponding outputs of the PD-PWM. In Fig. 11(a) represents the phase voltages of the inverter for PD-PWM, Fig. 11(b) represents the three-phase load voltages and load currents of the PD-PWM, Fig. 11(c) represents the THD analysis of the inverter by using PD-PWM, by using this technique the inverter produces 1.95% THD. Fig. 12 represents the corresponding outputs of the POD-PWM. In Fig. 12(a) represents the phase voltages of the inverter for POD-PWM, Fig. 12(b) represents

the three-phase load voltages and load currents of the POD-PWM, Fig. 12(c) represents the THD analysis of the inverter by using POD-

PWM, by using this technique the inverter produces 2.00% THD.

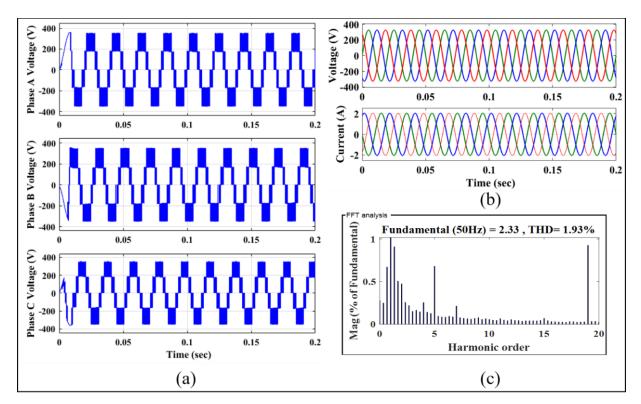


Fig. 11. PD-PWM Simulation results.

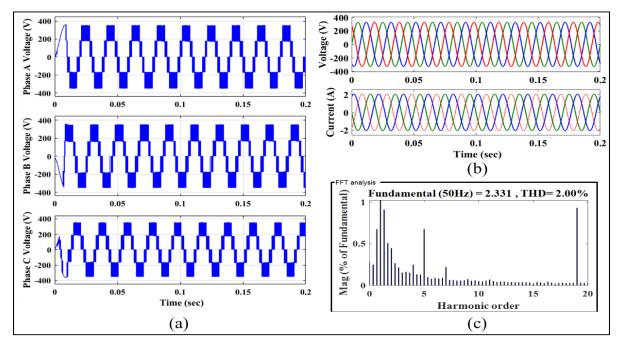


Fig. 12. POD-PWM simulation results

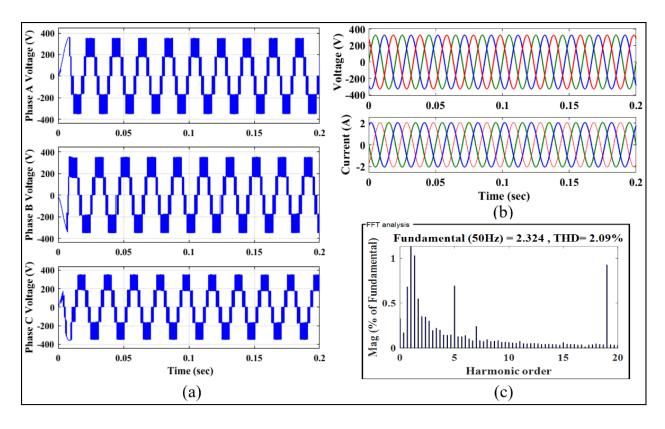


Fig. 13. APOD-PWM Simulation results.

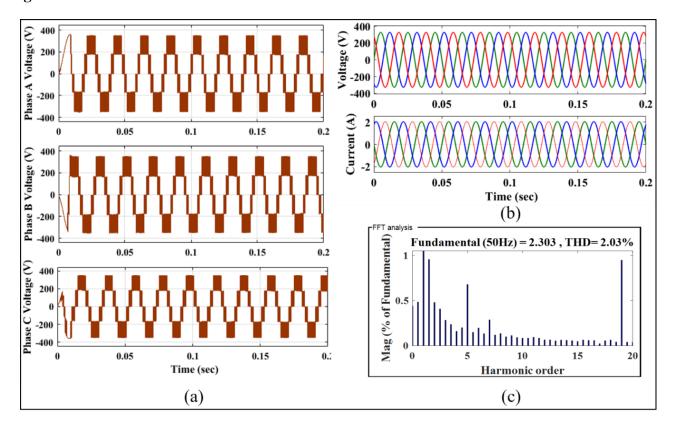
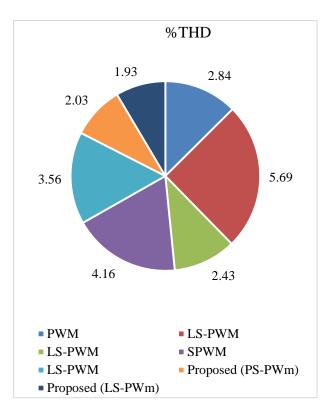


Fig. 14. PS-PWM Simulation results.

Fig. 13 represents the corresponding outputs of the APOD-PWM. In Fig. 13(a) represents the phase voltages of the inverter for APOD-PWM, Fig. 13(b) represents the three-phase load voltages and load currents of the APOD-PWM, Fig. 13(c) represents the THD analysis of the inverter by using APOD-PWM, by using this technique the inverter produces 2.09% THD. Fig. 14 represents the corresponding outputs of the PS-PWM. In Fig. 14(a) represents the phase voltages of the inverter for PS-PWM, Fig. 14(b) represents the three-phase load voltages and load currents of the PS-PWM, Fig. 14(c) represents the THD analysis of the inverter by using PS-PWM, by using this technique the inverter produces 2.03% THD. The proposed PWM controlled three-phase system has produced 1.93% of THD using an LS PWM technique whereas 2.03 % of THD using PS PWM techniques in Table 2.

**Table 2.** Comparison of % THD with the proposed system and existing systems

| Reference | %THD | PWM technique |
|-----------|------|---------------|
| [2]       | 2.84 | PWM           |
| [6]       | 5.69 | LS-PWM        |
| [7]       | 2.43 | LS-PWM        |
| [9]       | 4.16 | SPWM          |
| [15]      | 3.56 | LS-PWM        |
| Proposed  | 1.93 | LS-PWM        |
| Proposed  | 2.03 | PS-PWM        |



**Fig. 15.** Flow chart of % THD with the proposed system and existing system

# 6 Conclusion

A three phase grid connected inverter using different PWM controllers has been investigated in this article. The PI current control regulator has been applied to control the grid current. The inverter switches are controlled by SPWM techniques. In this observe the framework execution regarding THD and the proposed current controller generated less THD when contrasted with the current strategies. The proposed system with the PI controller produces 1.93% THD, the produced THD is within the IEE standards. The entire work is done in MATLAB/Simulink tool.

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