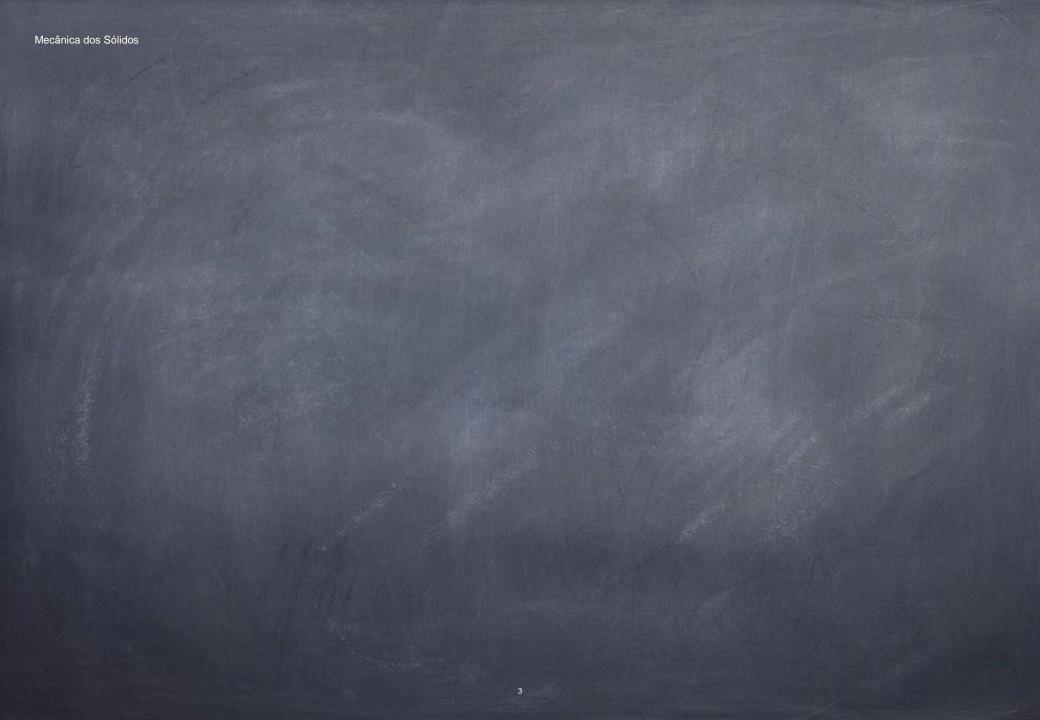
Mecânica dos Sólidos

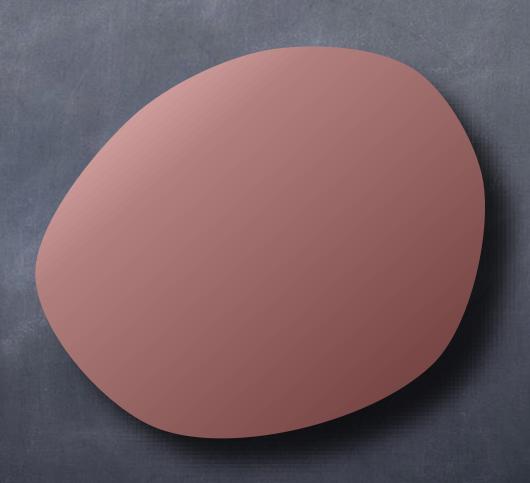
Mecânica dos Sólidos

Equilíbrio de um corpo deformável



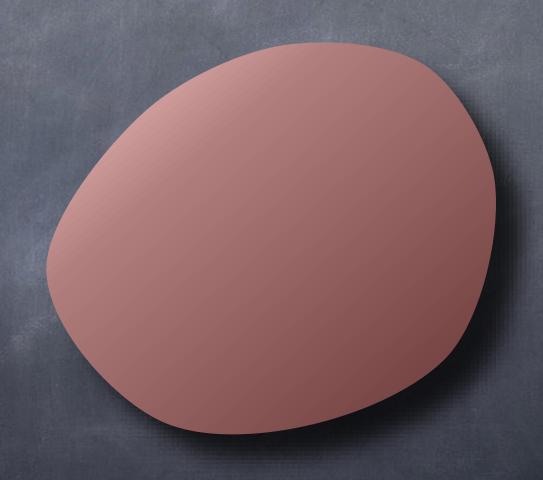
Forças externas

Forças externas

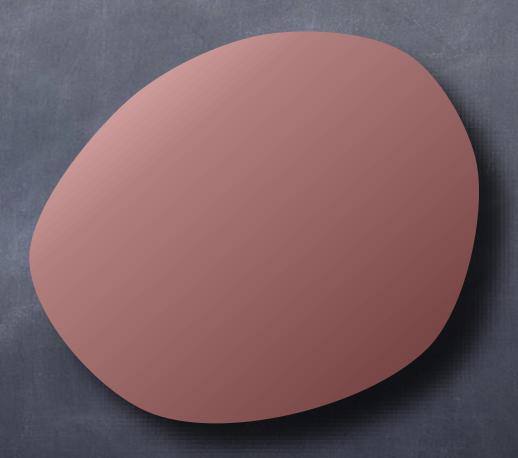


Forças externas

corpo elástico deformável

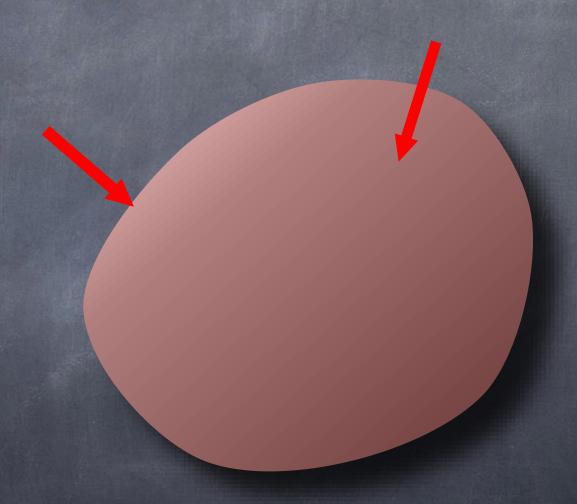


Forças externas



Forças externas

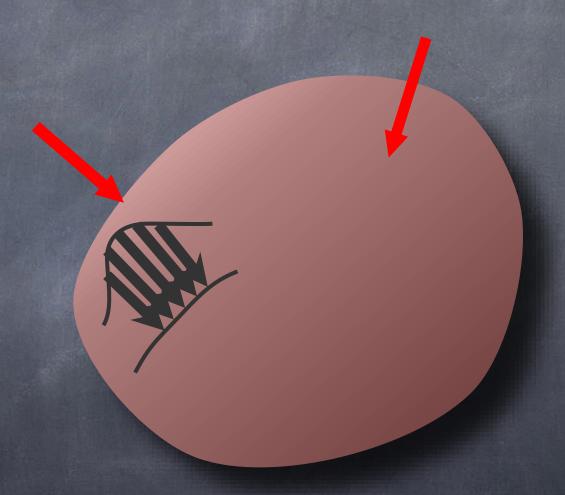
Cargas concentradas



Forças externas

Cargas concentradas

Cargas distribuídas

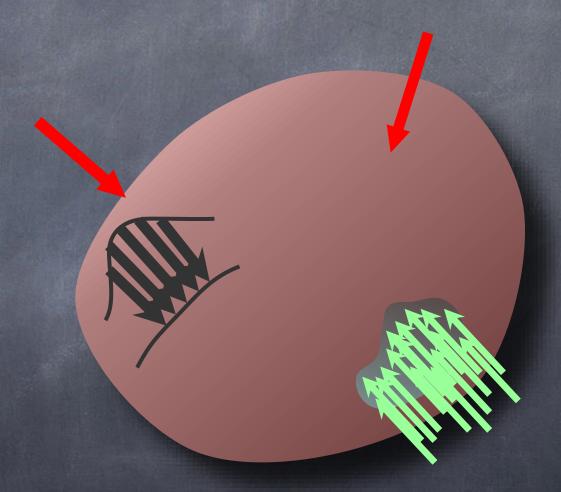


Forças externas

Cargas concentradas

Cargas distribuídas

Forças de superfície



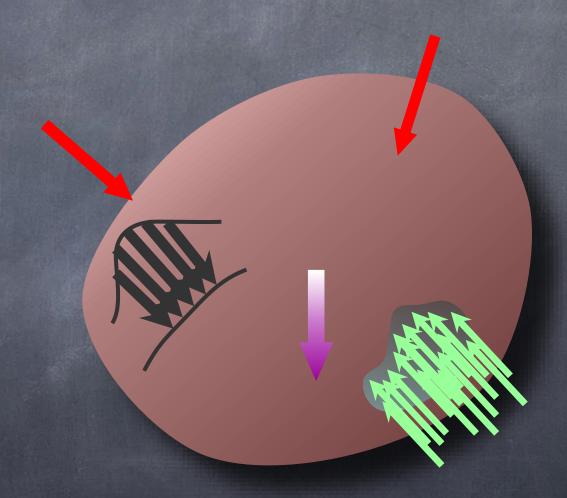
Forças externas

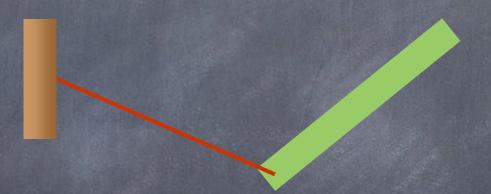
Cargas concentradas

Cargas distribuídas

Forças de superfície

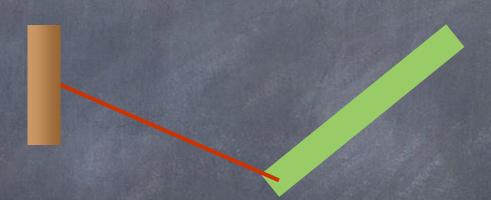
Forças de corpo





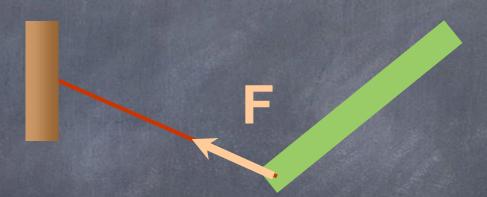
Reações de apoio

Vínculo tipo cabo



Reações de apoio

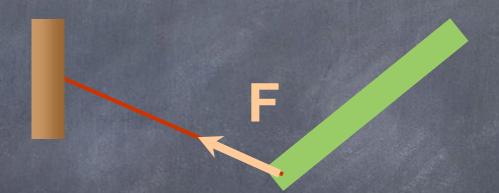
Vínculo tipo cabo



Reações de apoio

Vínculo tipo cabo

Uma incógnita (F)

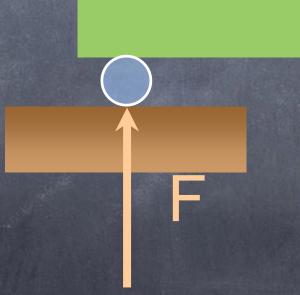


Reações de apoio

Vínculo tipo rolete

Reações de apoio

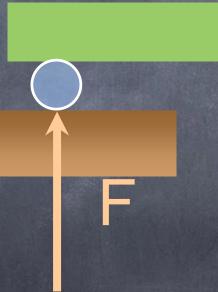
Vínculo tipo rolete



Reações de apoio

Vínculo tipo rolete

Uma incógnita (F)



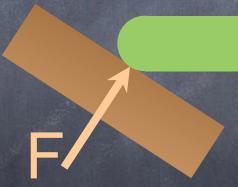


Reações de apoio

Vínculo tipo apoio simples

Reações de apoio

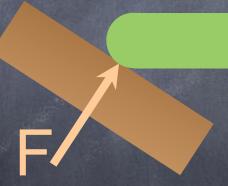
Vínculo tipo apoio simples

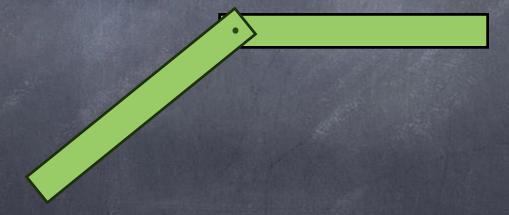


Reações de apoio

Vínculo tipo apoio simples

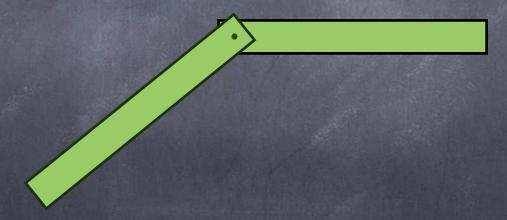
Uma incógnita (F)





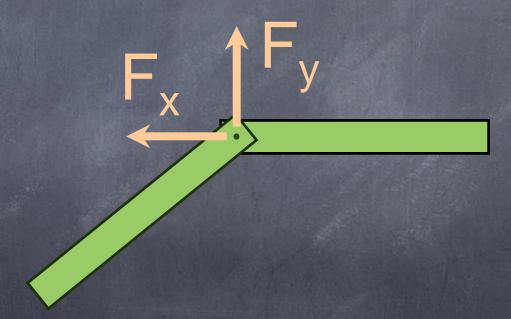
Reações de apoio

Vínculo tipo pino interno



Reações de apoio

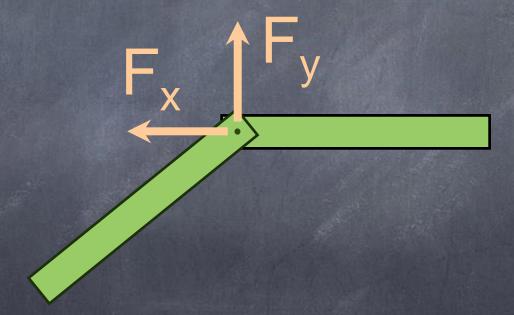
Vínculo tipo pino interno



Reações de apoio

Vínculo tipo pino interno

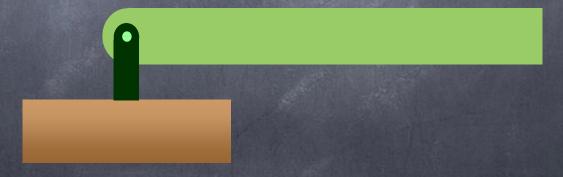
Duas incógnitas (F_x, F_y)





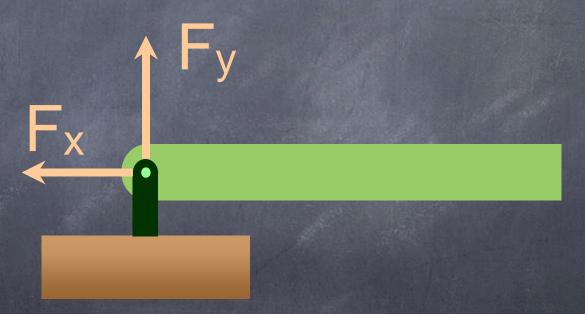
Reações de apoio

Vínculo tipo pino externo



Reações de apoio

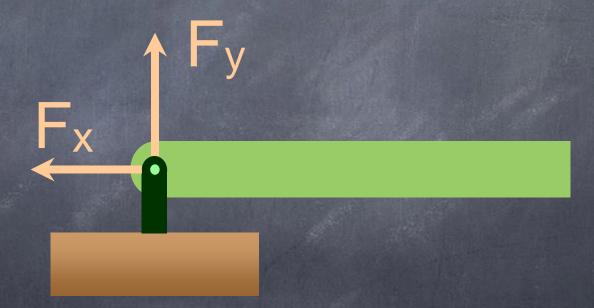
Vínculo tipo pino externo



Reações de apoio

Vínculo tipo pino externo

Duas incógnitas (Fx, Fy)

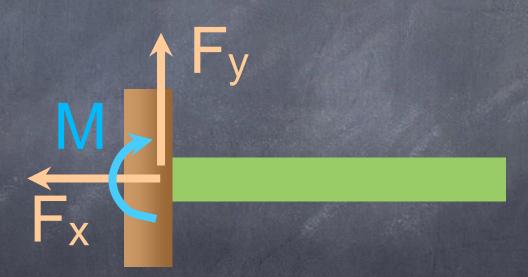


Reações de apoio

Vínculo tipo engaste

Reações de apoio

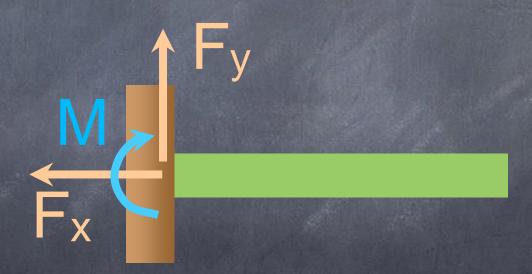
Vínculo tipo engaste

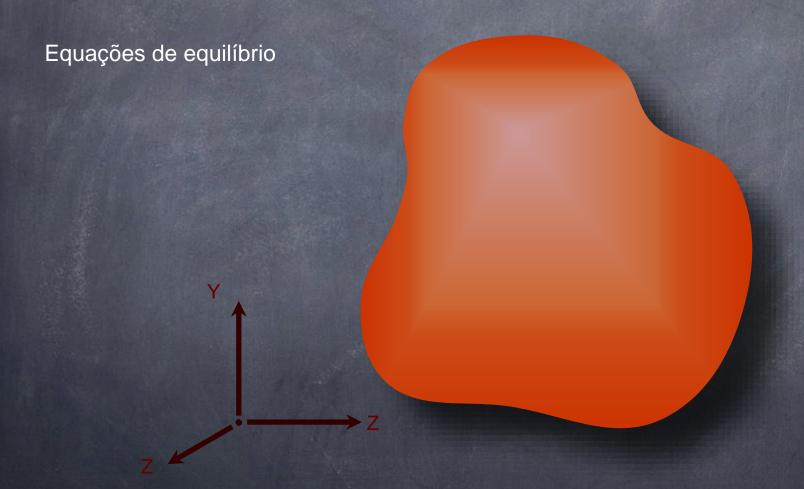


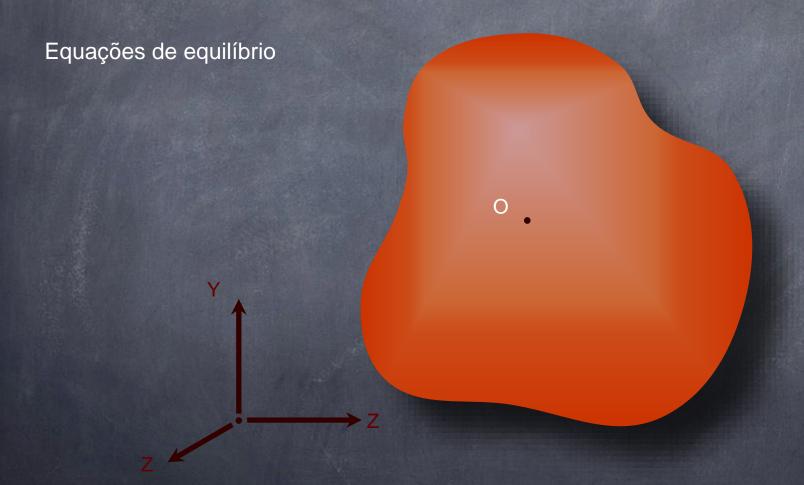
Reações de apoio

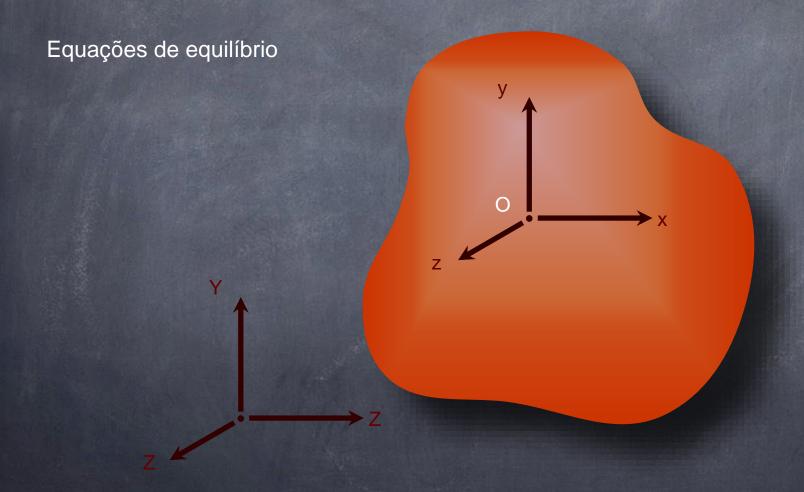
Vínculo tipo engaste

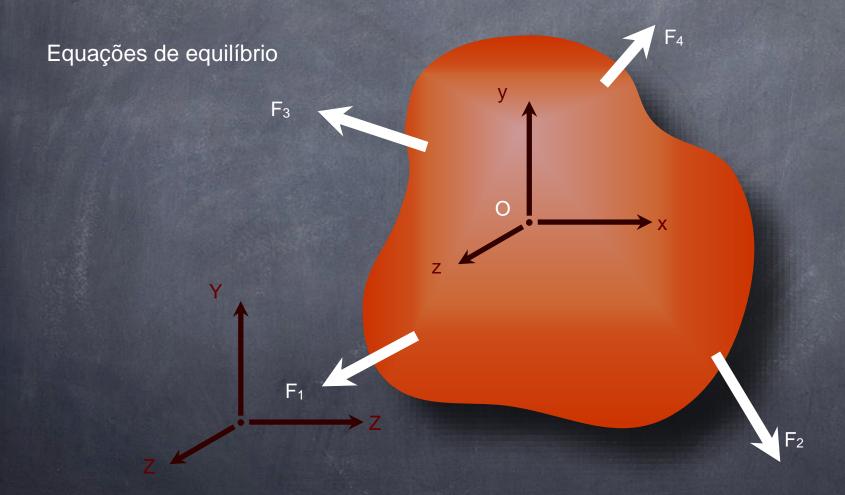
Tres incógnitas (Fx, Fy, M)

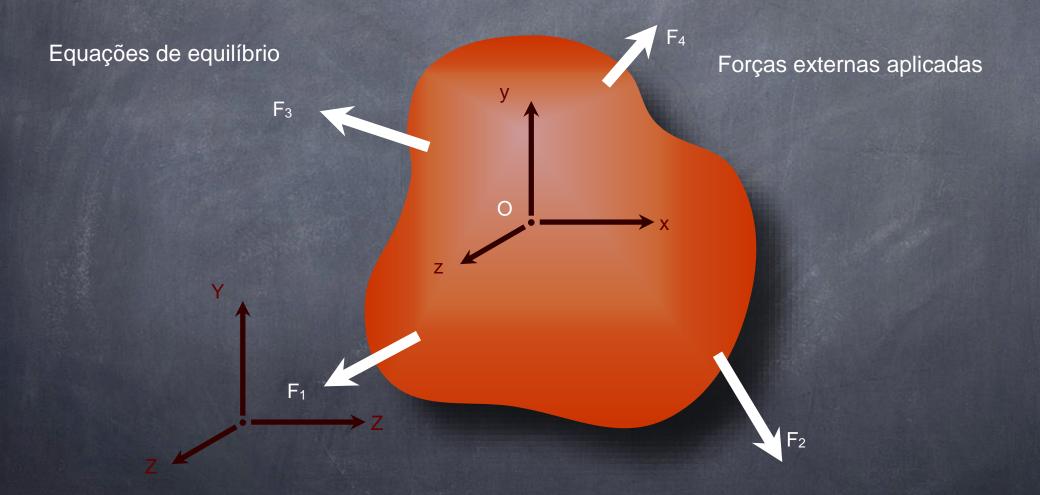


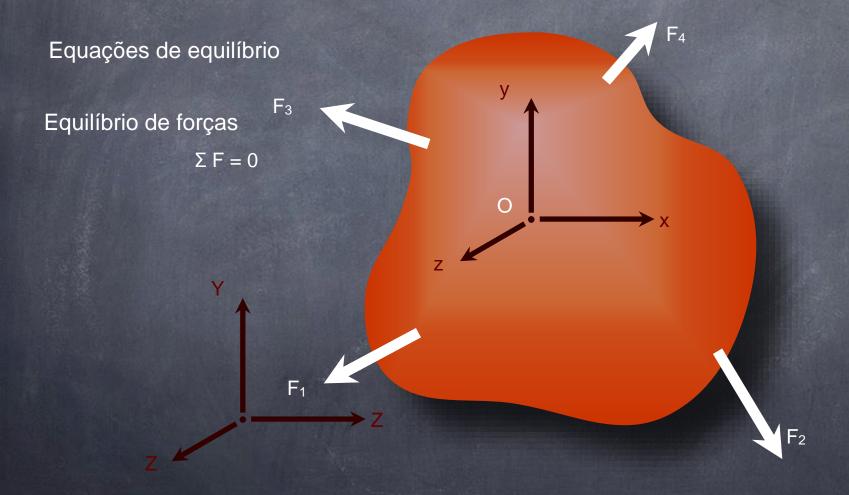


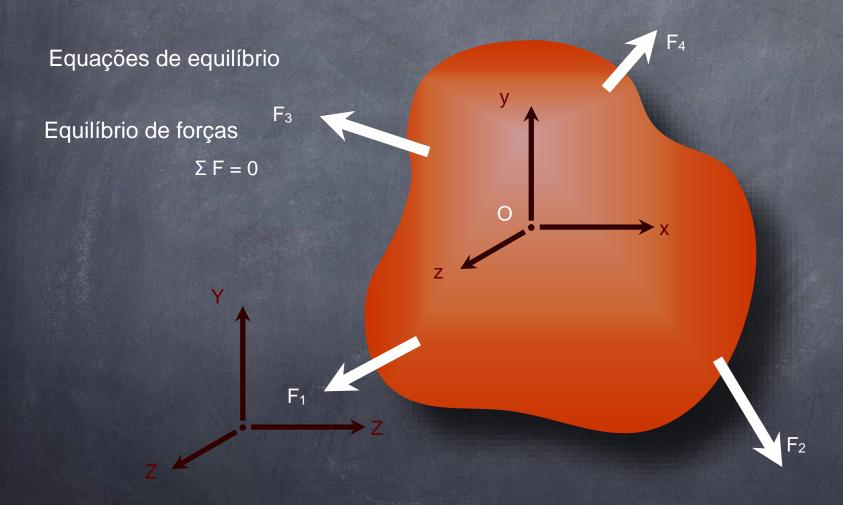








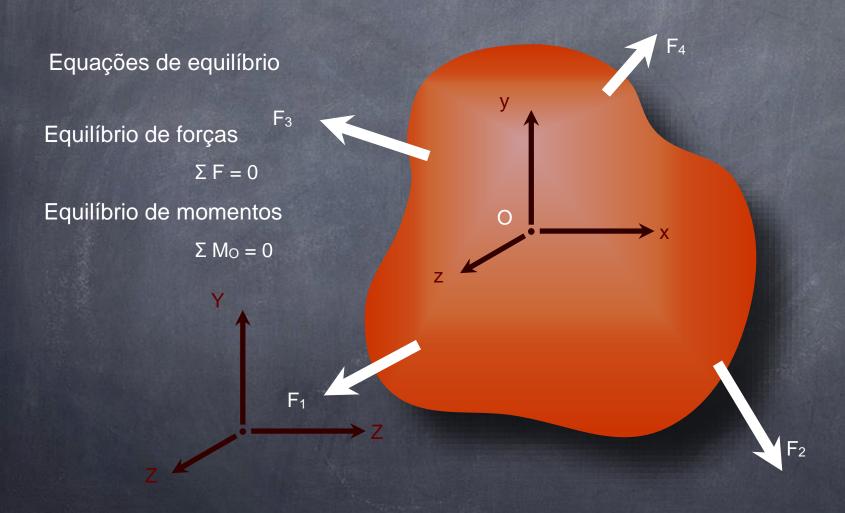




$$\Sigma\;F_x=0$$

$$\Sigma F_y = 0$$

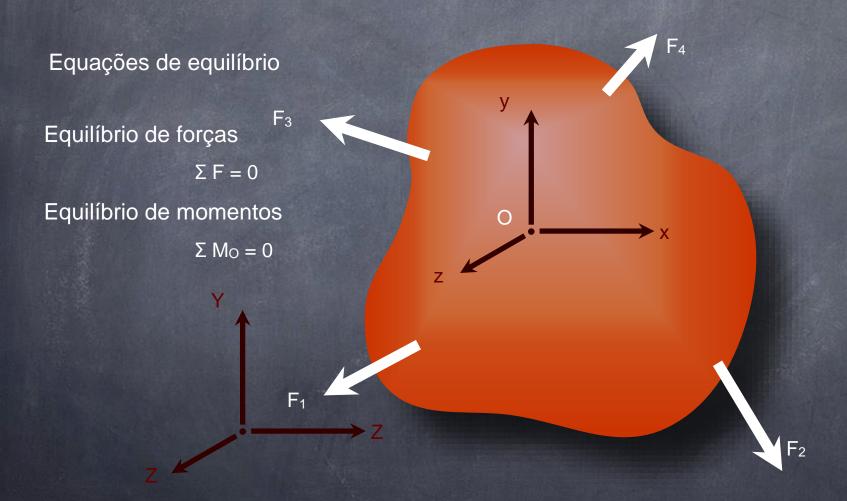
$$\Sigma F_z = 0$$



$$\Sigma F_x = 0$$

$$\Sigma F_y = 0$$

$$\Sigma\;F_z=0$$



$$\Sigma \; F_x = 0$$

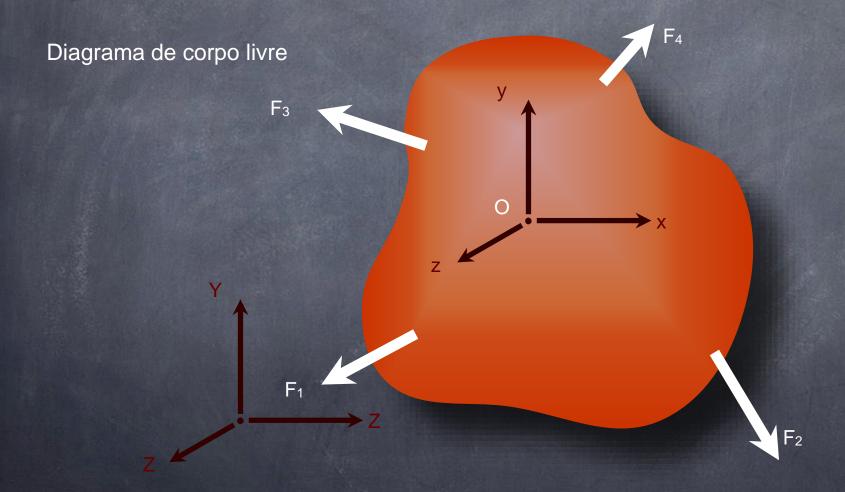
$$\Sigma F_y = 0$$

$$\Sigma F_z = 0$$

$$\Sigma\; M_x = 0$$

$$\Sigma M_y = 0$$

$$\Sigma\; M_z=0$$



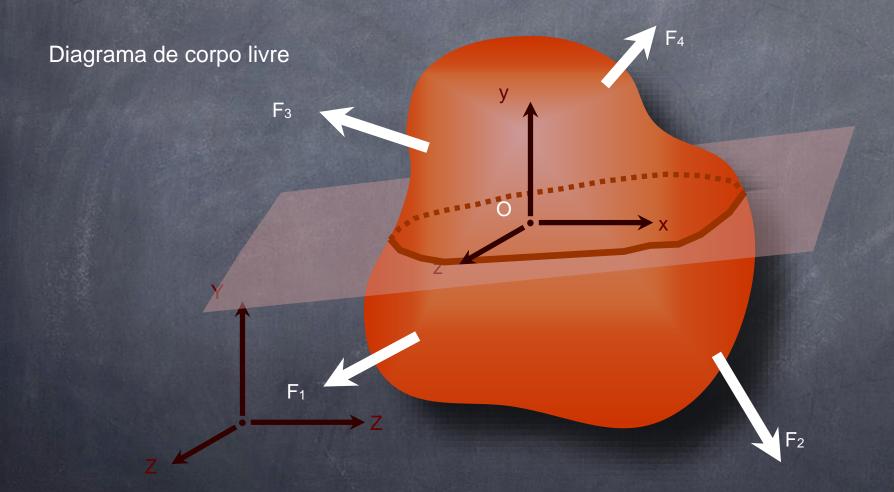
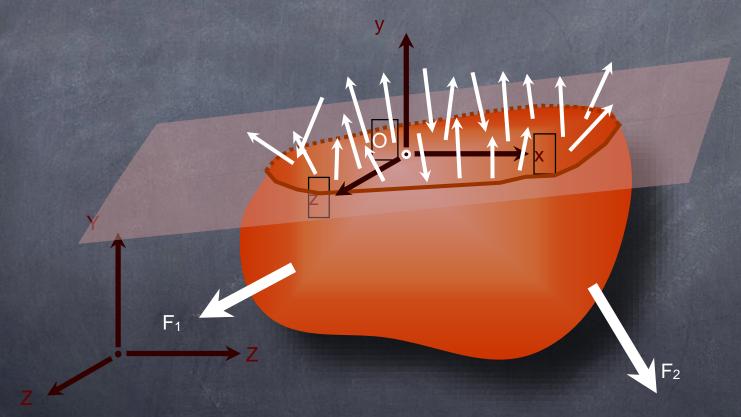
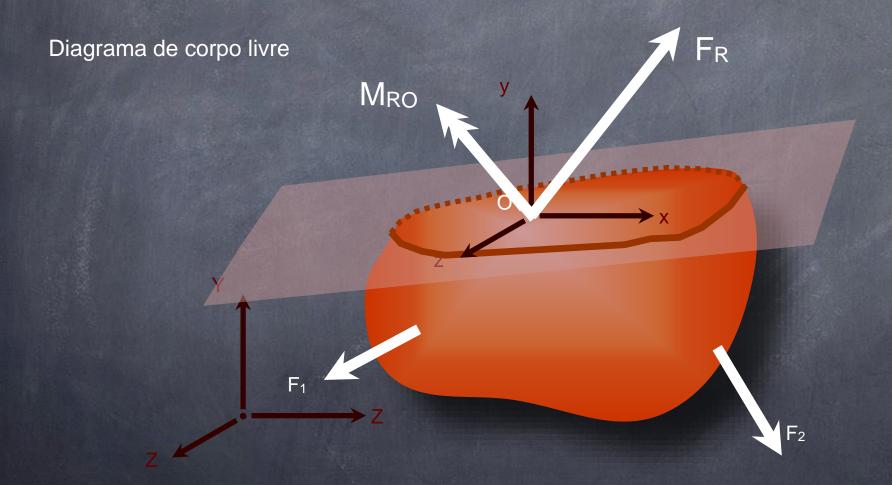
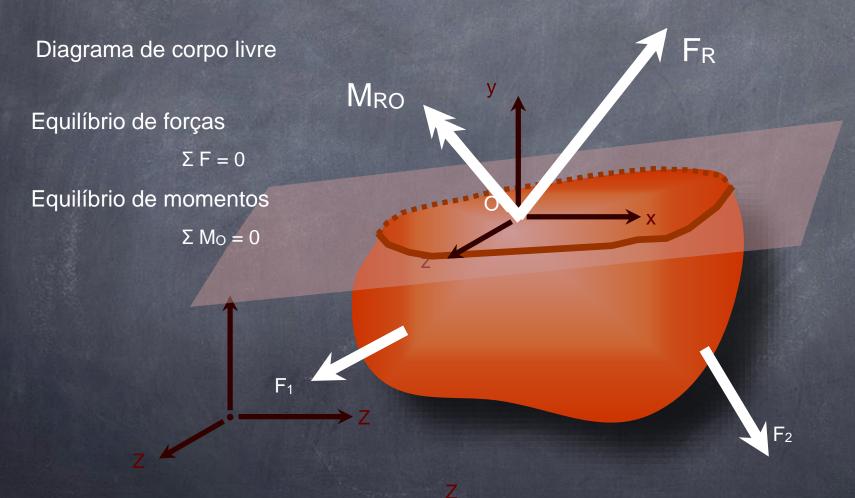
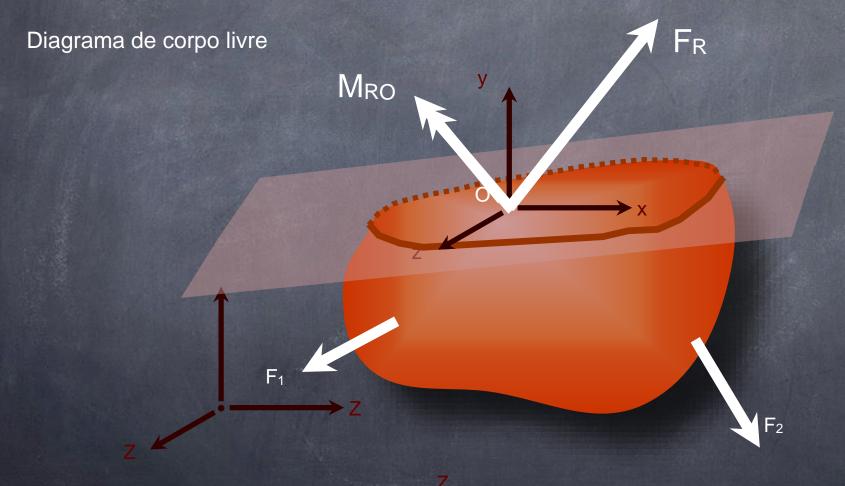


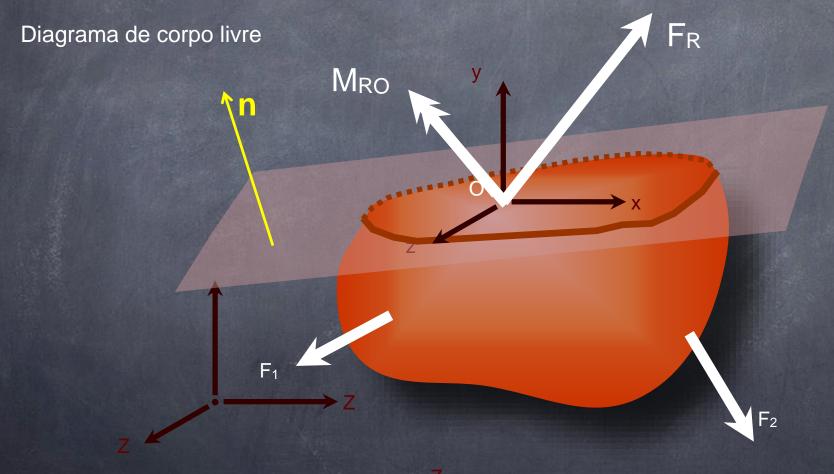
Diagrama de corpo livre

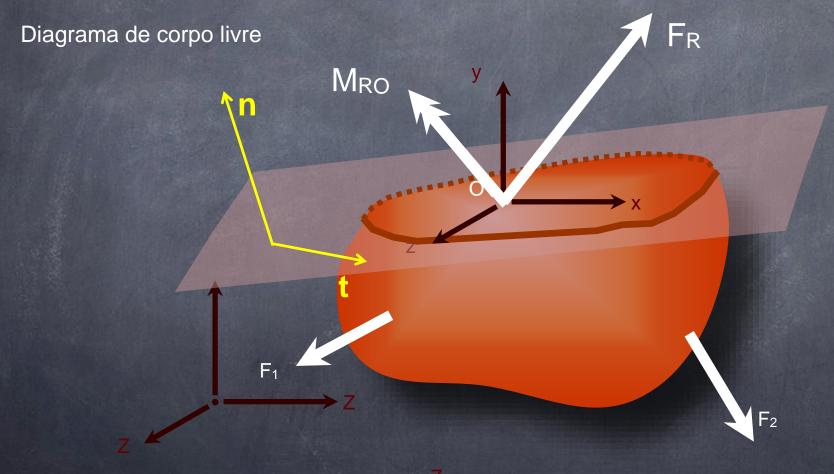


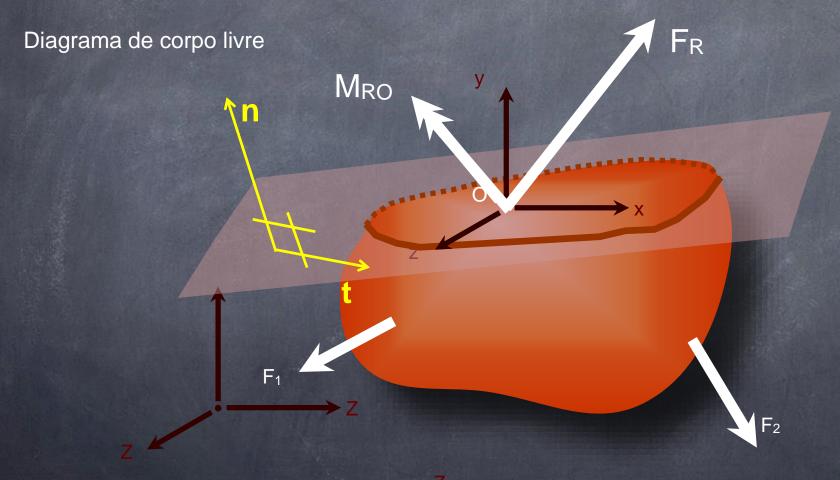


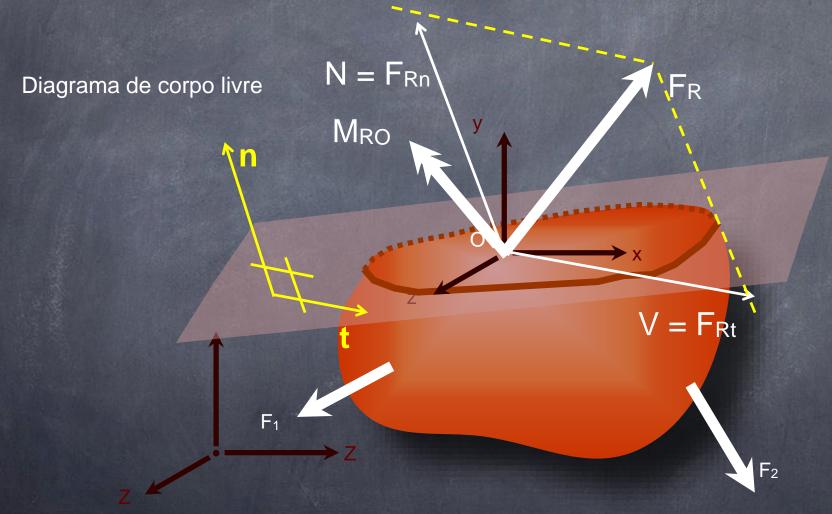


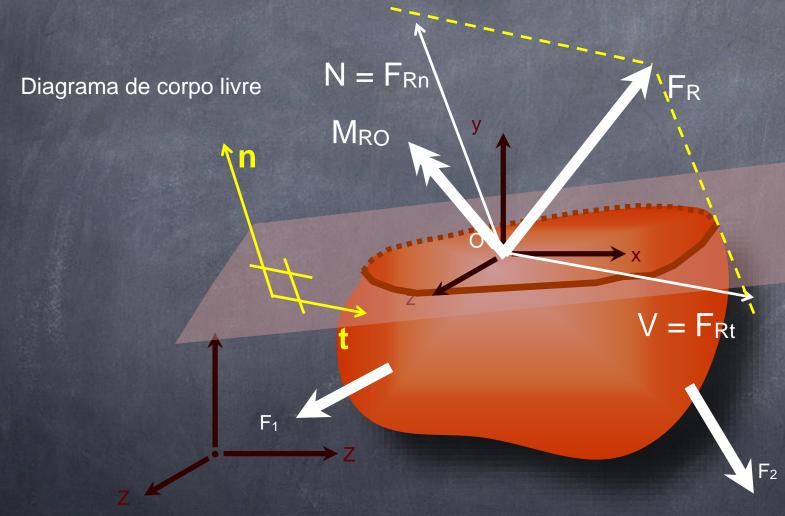






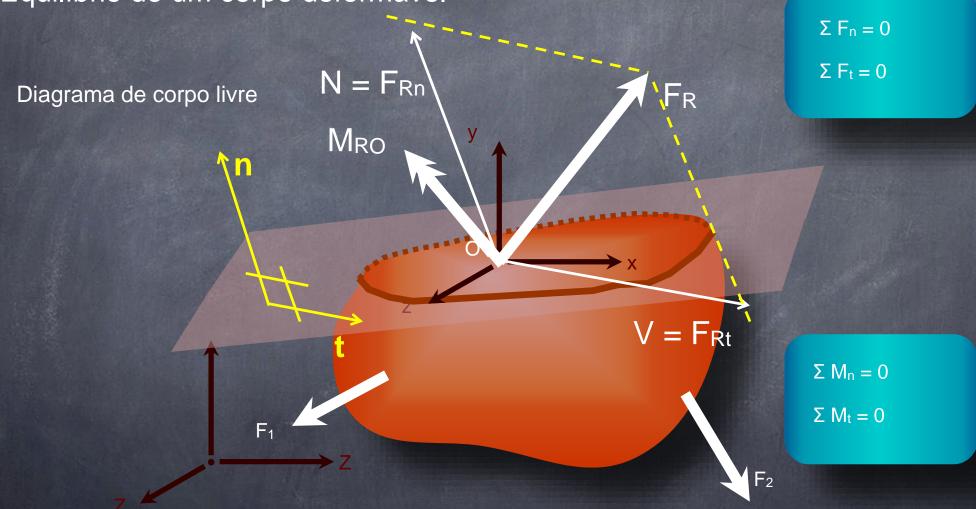






 $\Sigma F_n = 0$

 $\Sigma\; F_t = 0$



N = Força normalV = Força tangente

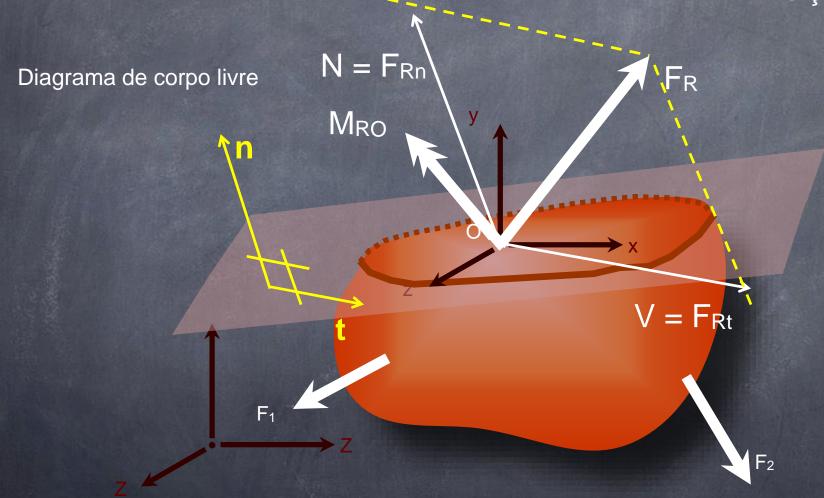


Diagrama de corpo livre

 $N = F_{Rn}$

 M_{RO}

 $V = F_{Rt}$

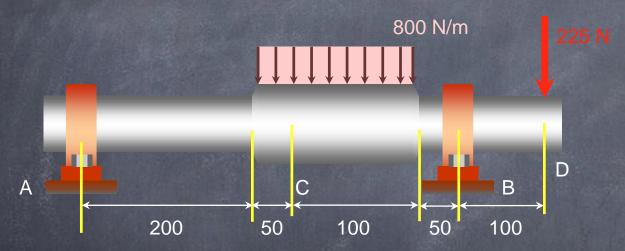
N = Força normal

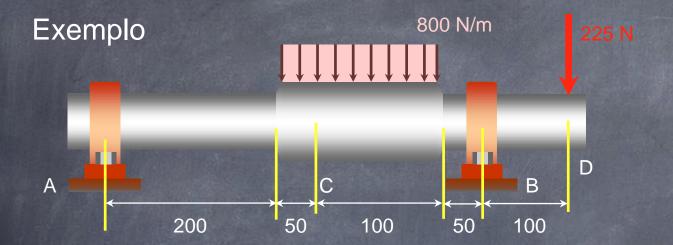
V = Força tangente

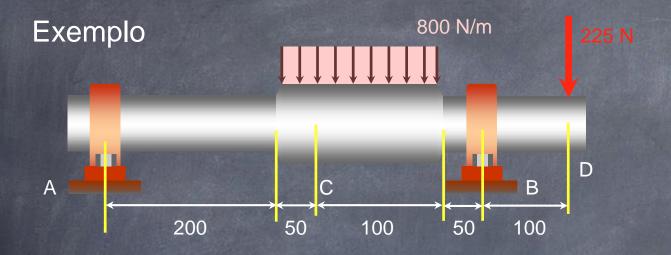
T = Momento torsor

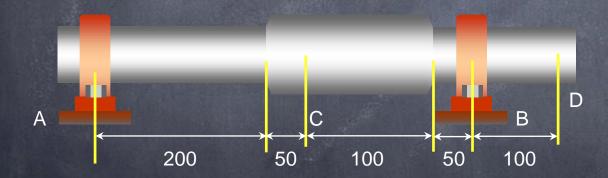
M = Momento fletor

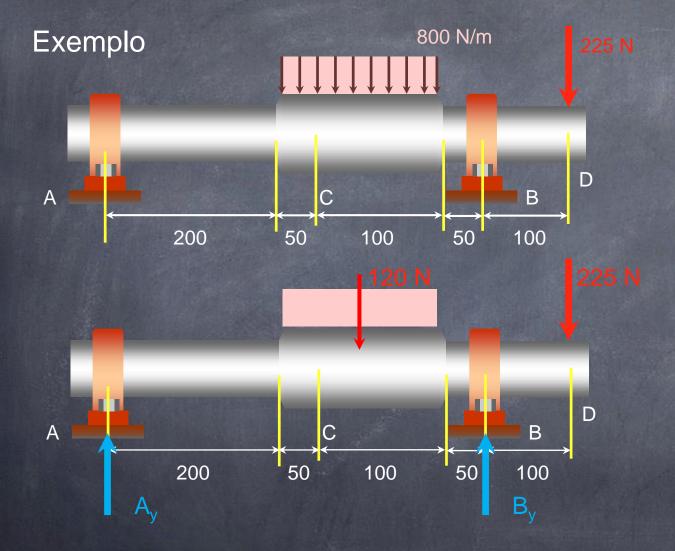
Determinar as resultantes das cargas internas que atuam na seção transversal C do eixo apoiado nos rolamentos em A e em B (transmitem apenas forças verticais).

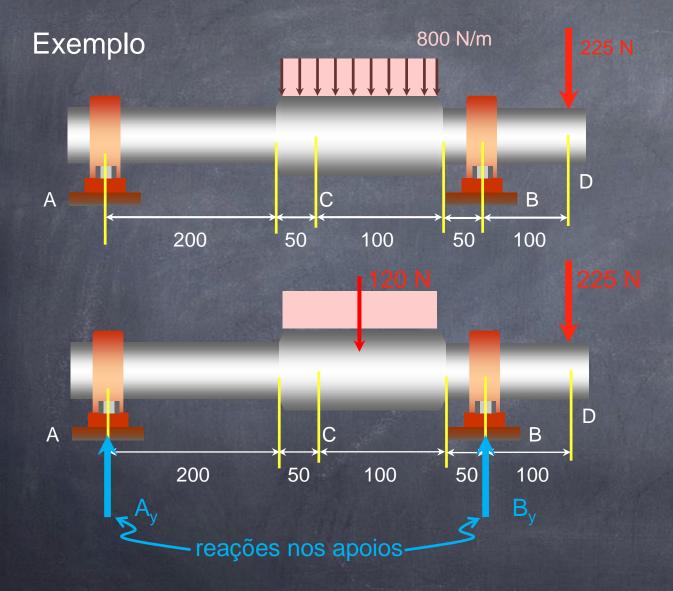


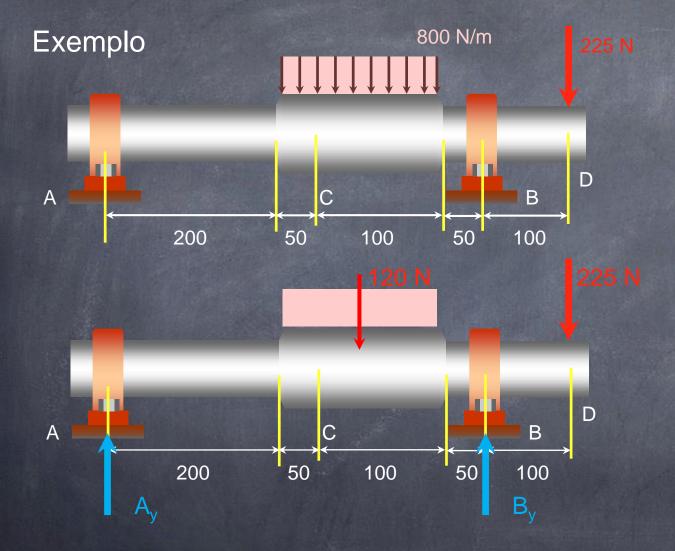


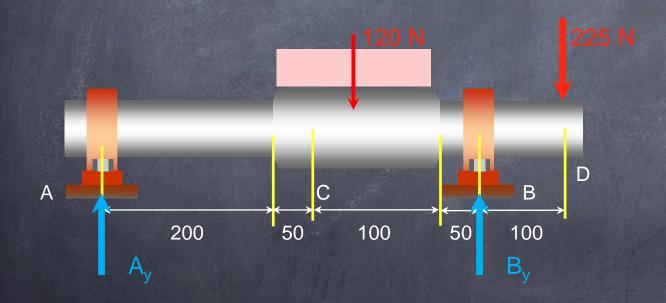


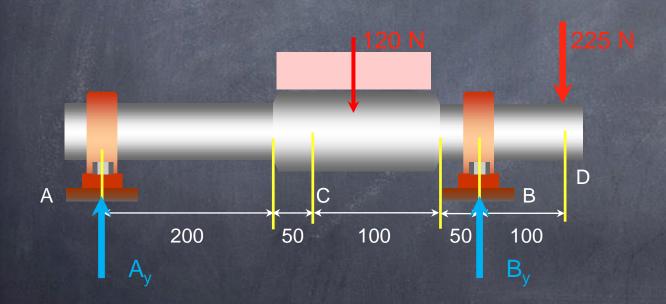




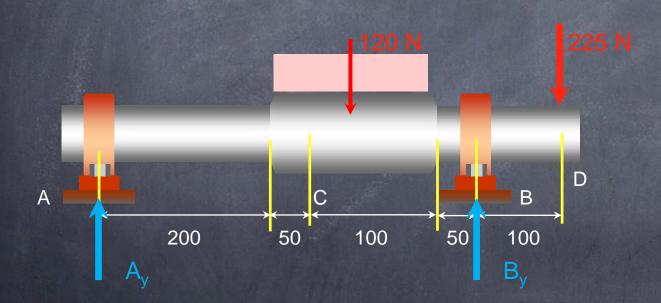




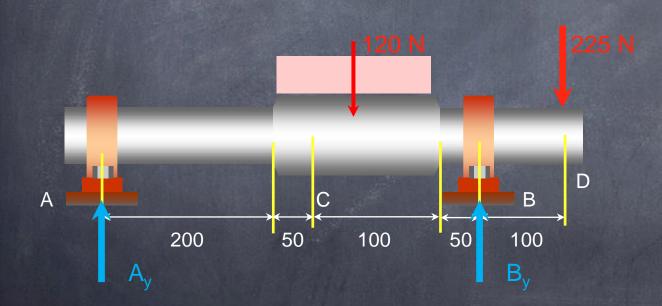




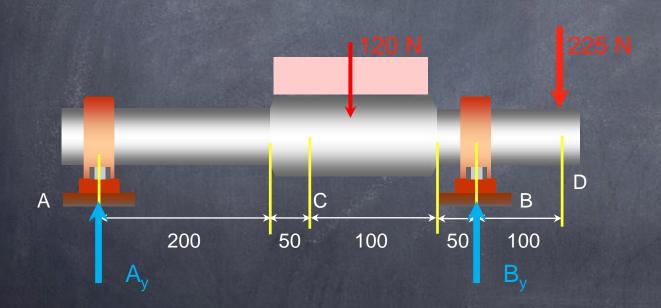
$$\Sigma M_B = 0 \implies -A_y \times (0,400) + 120 \times (0,125) - 225 \times (0,100) = 0$$



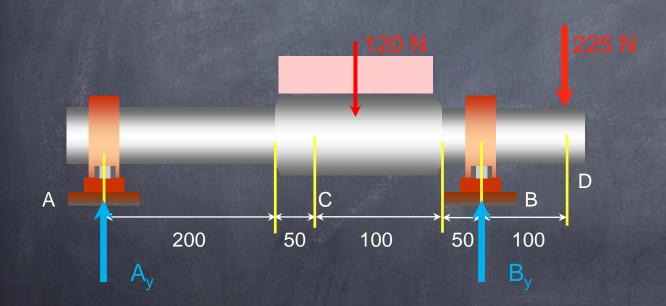
$$\Sigma M_B = 0 \implies -A_y \times (0,400) + 120 \times (0,125) - 225 \times (0,100) = 0 : A_y = -18,75 \text{ N}$$



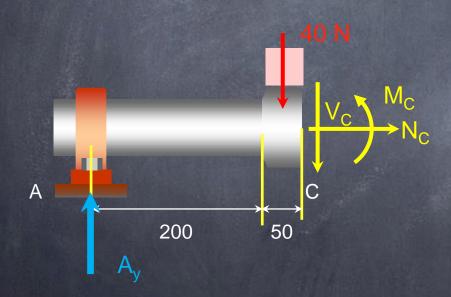
$$\Sigma M_B = 0 \implies -A_y \times (0,400) + 120 \times (0,125) - 225 \times (0,100) = 0 : A_y = -18,75 \text{ N}$$



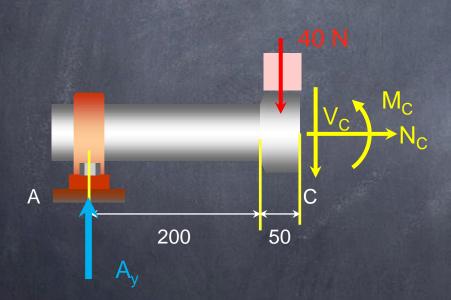
As forças internas no ponto C são mostradas no diagrama de corpo livre (DLC) abaixo.



As forças internas no ponto C são mostradas no diagrama de corpo livre (DLC) abaixo.

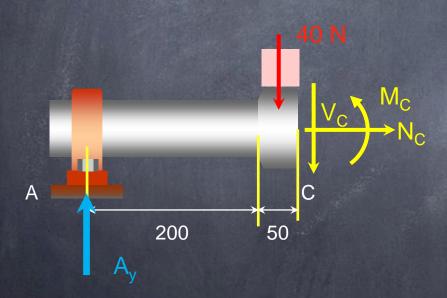


As forças internas no ponto C são mostradas no diagrama de corpo livre (DLC) abaixo. No DLC, ainda são válidas as equações de equilíbrio, i. e.



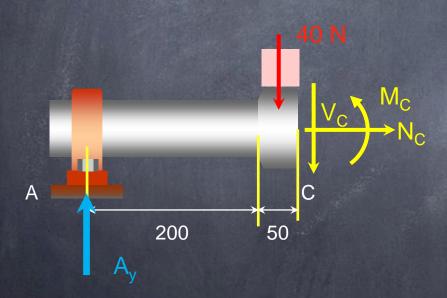
As forças internas no ponto C são mostradas no diagrama de corpo livre (DLC) abaixo. No DLC, ainda são válidas as equações de equilíbrio, i. e.

$$\Sigma F_x = 0 \Rightarrow N_C = 0$$



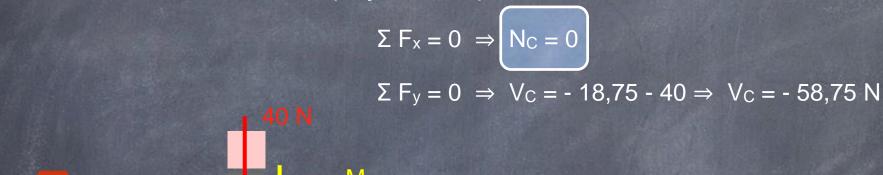
As forças internas no ponto C são mostradas no diagrama de corpo livre (DLC) abaixo.

$$\Sigma F_X = 0 \Rightarrow N_C = 0$$

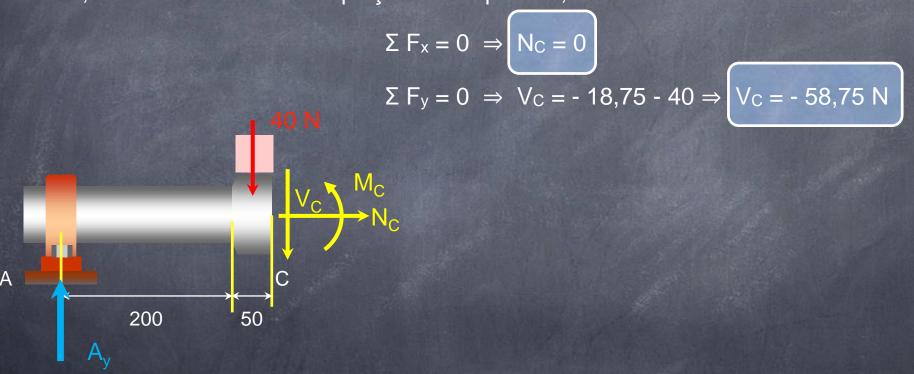


200

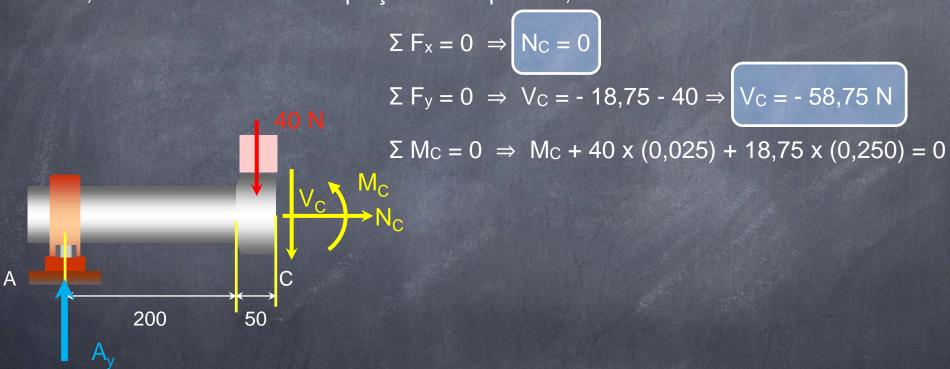
As forças internas no ponto C são mostradas no diagrama de corpo livre (DLC) abaixo.



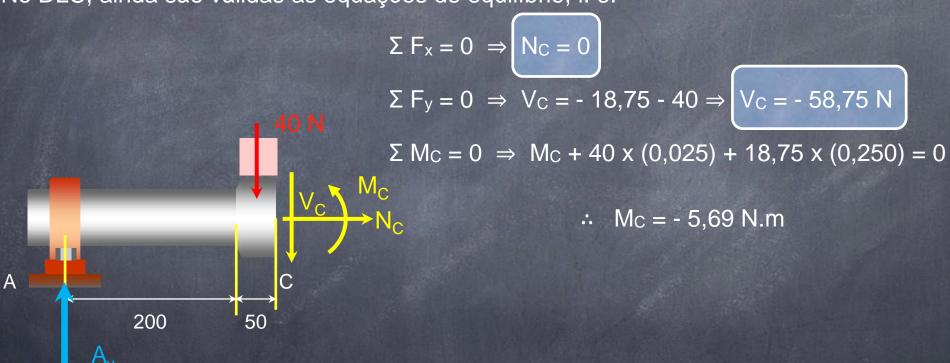
As forças internas no ponto C são mostradas no diagrama de corpo livre (DLC) abaixo.



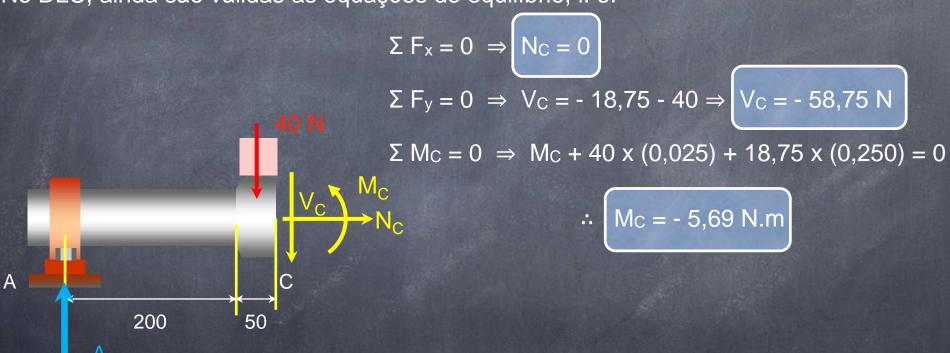
As forças internas no ponto C são mostradas no diagrama de corpo livre (DLC) abaixo.

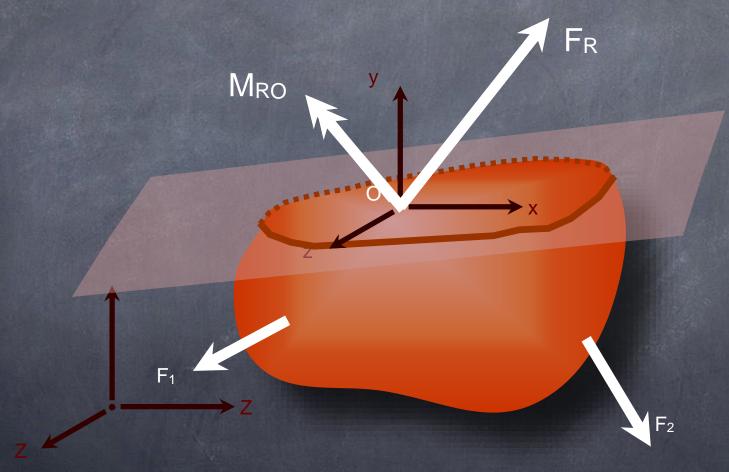


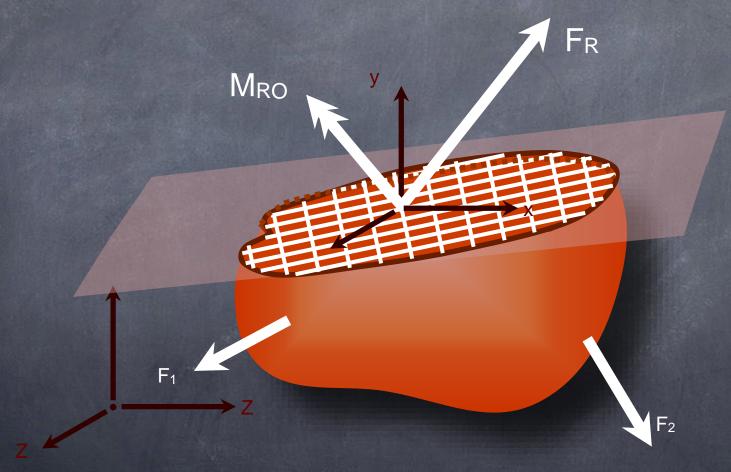
As forças internas no ponto C são mostradas no diagrama de corpo livre (DLC) abaixo.

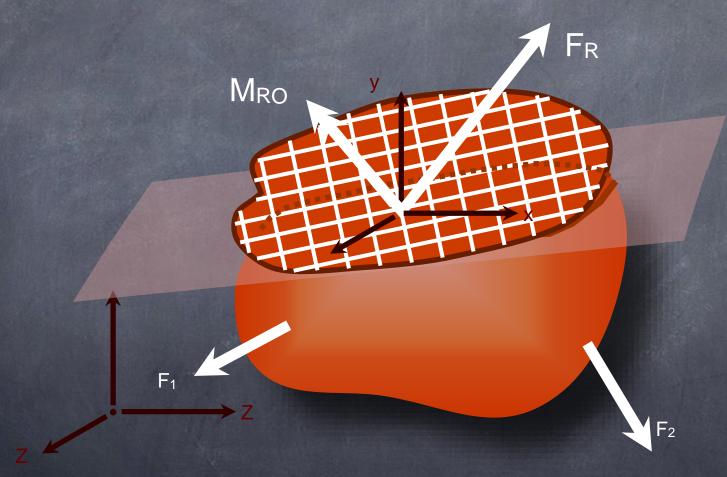


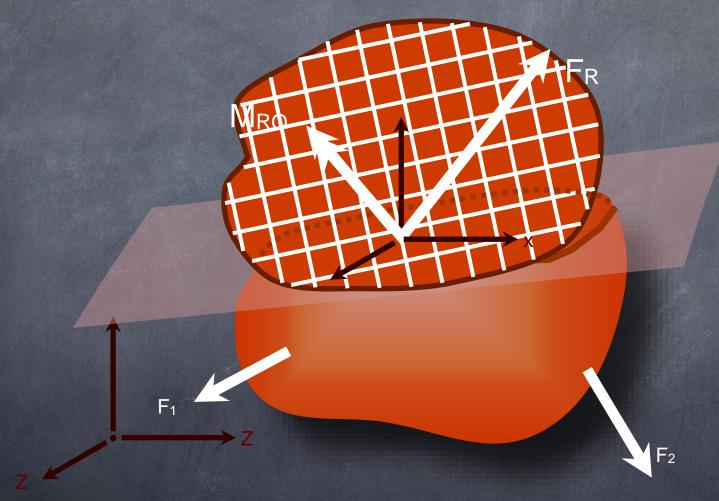
As forças internas no ponto C são mostradas no diagrama de corpo livre (DLC) abaixo.



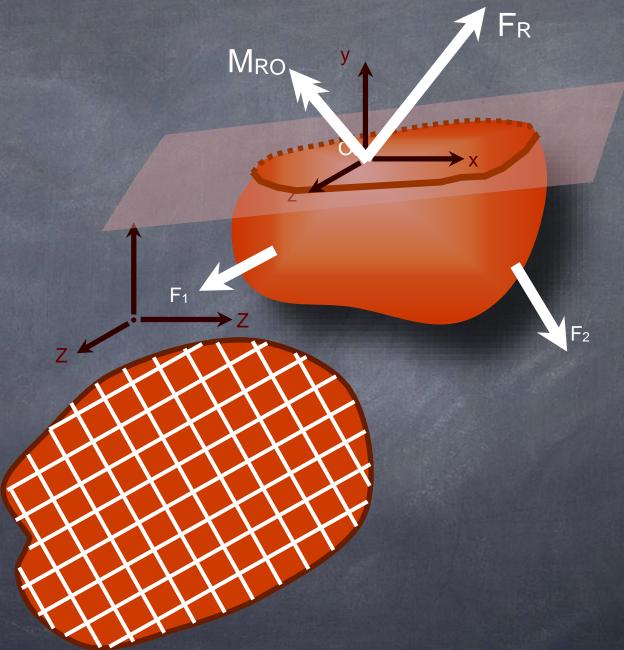








Superfície discretizada



Z

Superfície discretizada

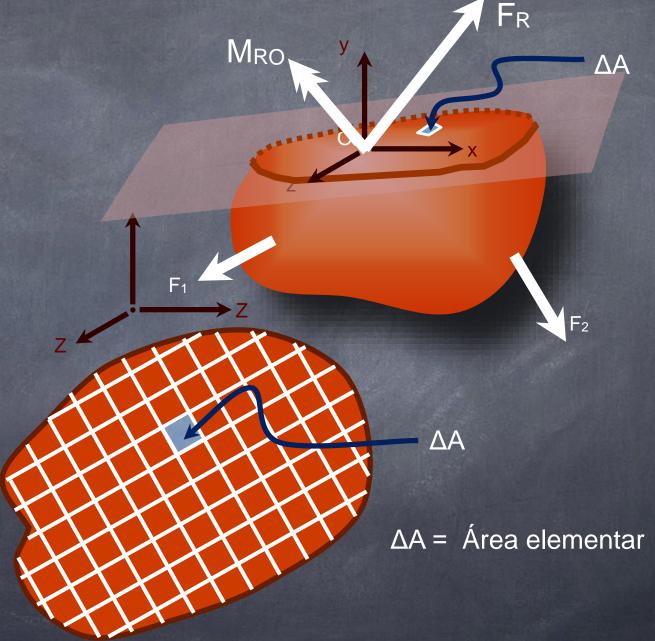
Área total -> A

 M_{RO}

7

Superfície discretizada

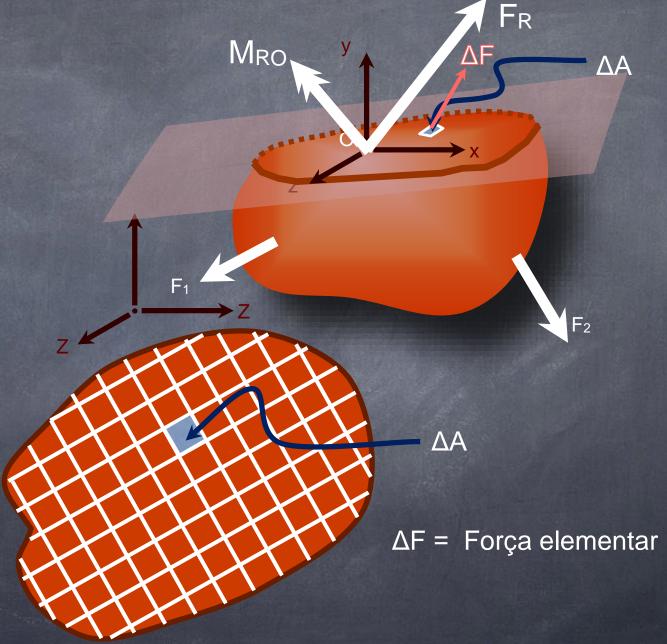
Área total -> A



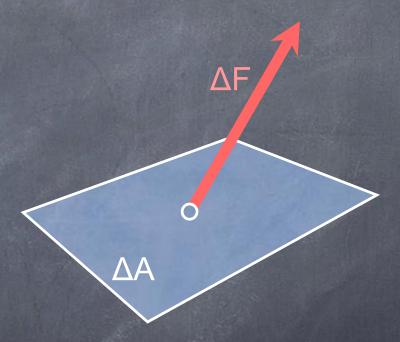
Z

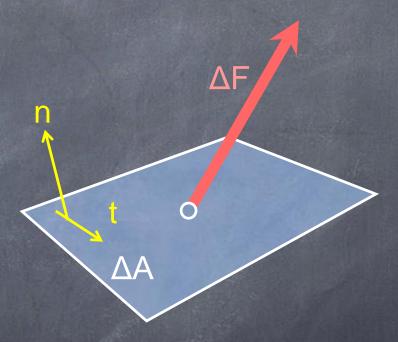
Superfície discretizada

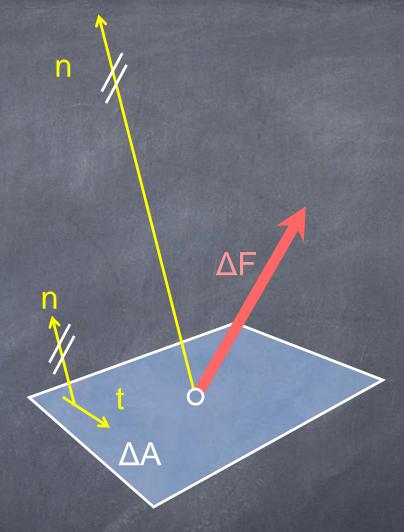
Área total -> A

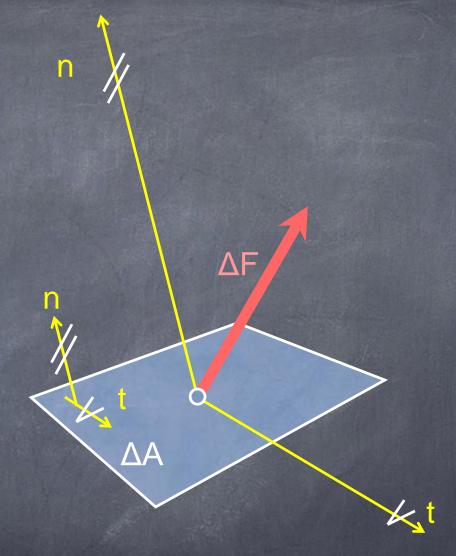


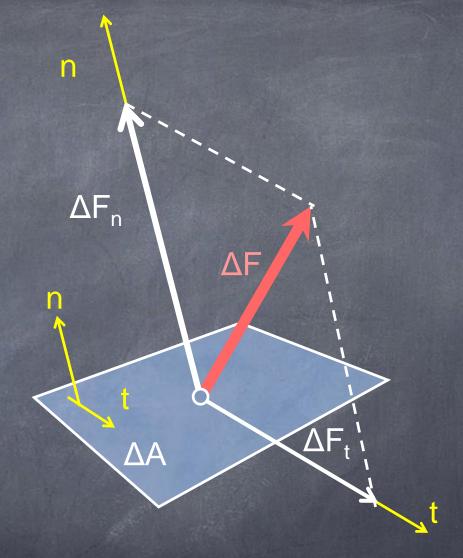
7



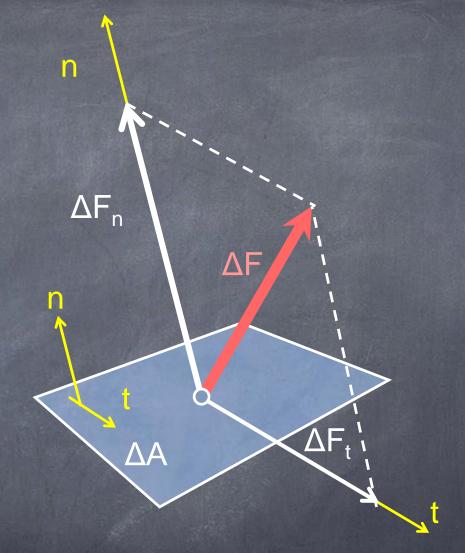






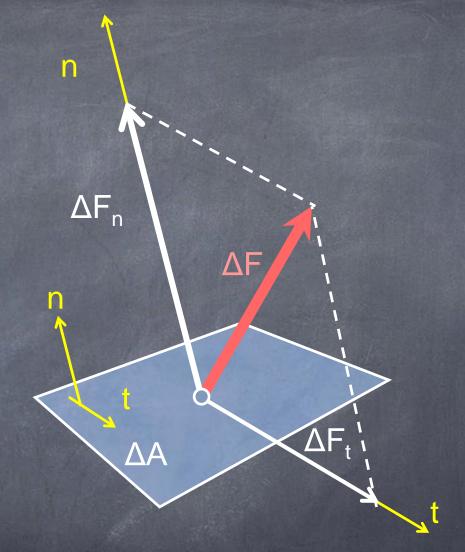


Tensão normal



Tensão normal

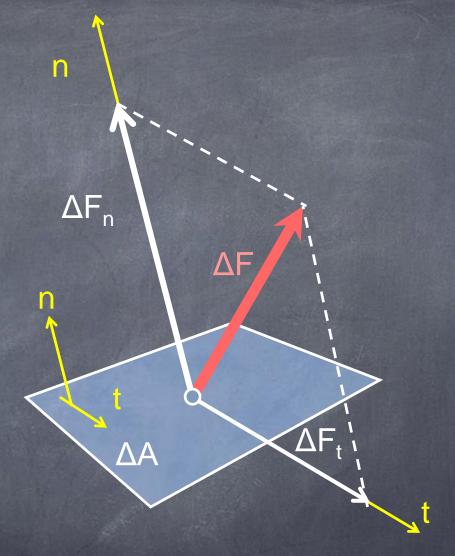
$$\sigma \equiv \Delta F_n / \Delta A$$



Tensão normal

$$\sigma \equiv \Delta F_n / \Delta A$$

Tensão tangencial (ou de cisalhamento)

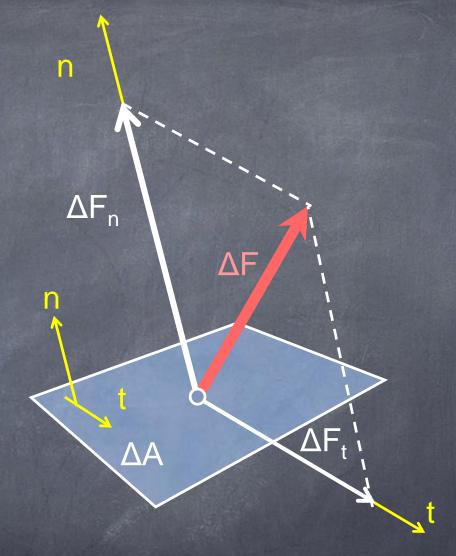


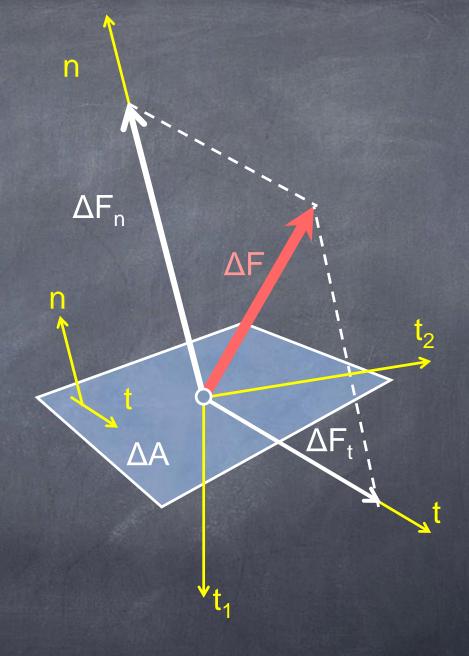
Tensão normal

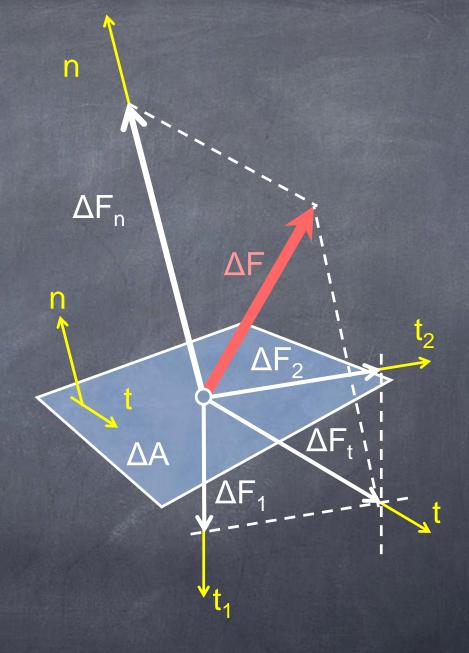
$$\sigma \equiv \Delta F_n / \Delta A$$

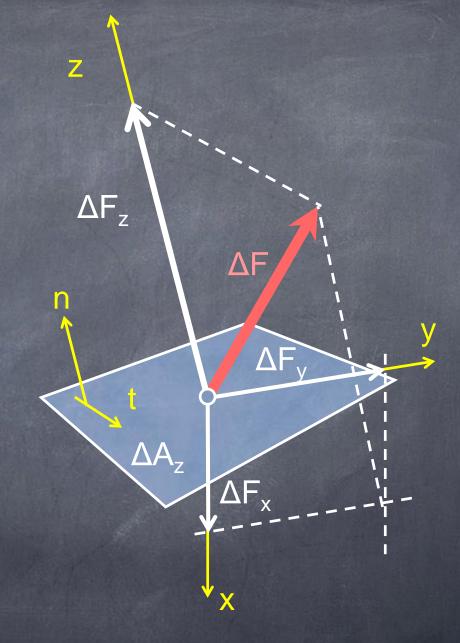
Tensão tangencial (ou de cisalhamento)

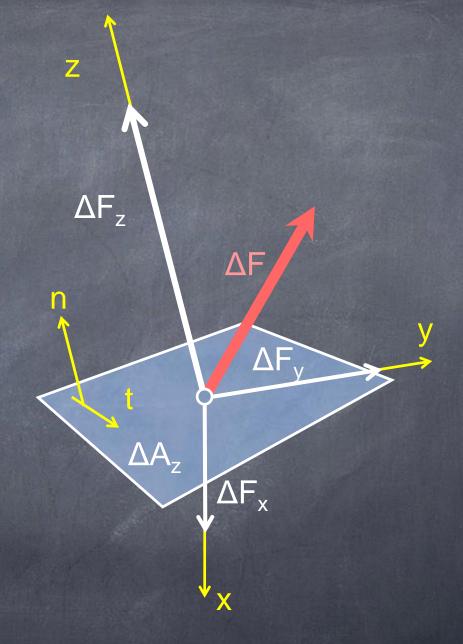
$$\tau \equiv \Delta F_t / \Delta A$$

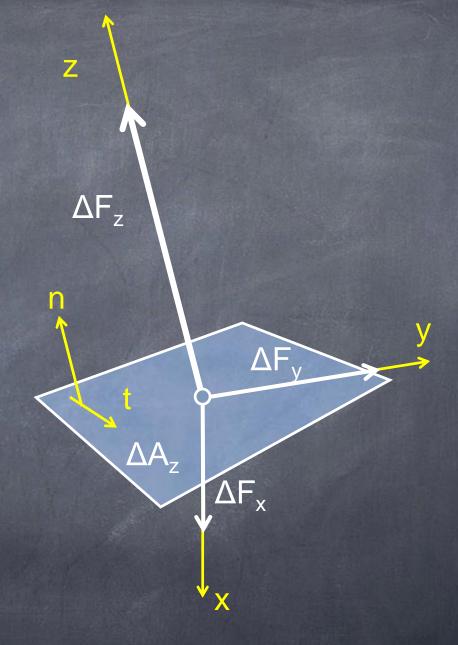




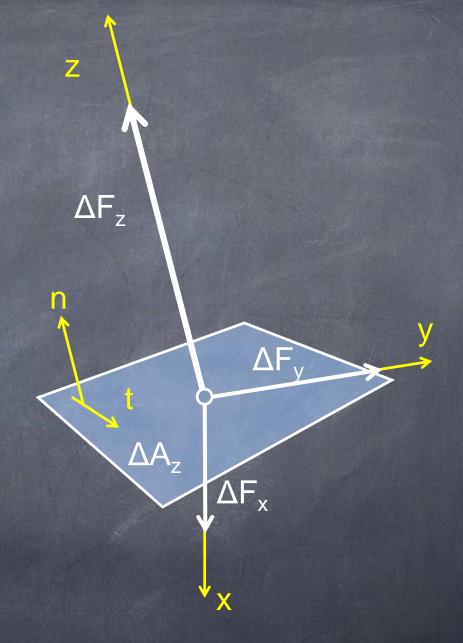




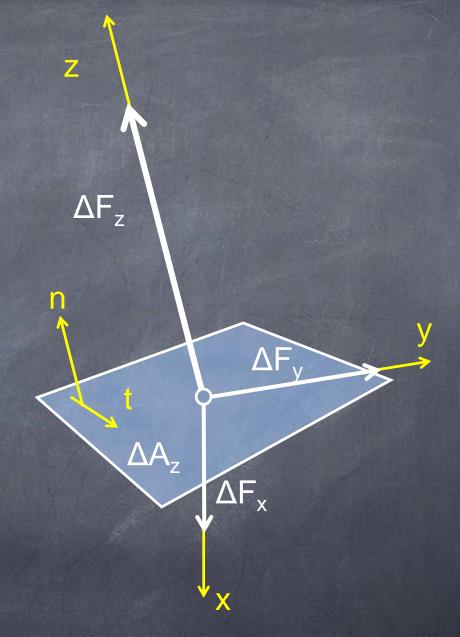




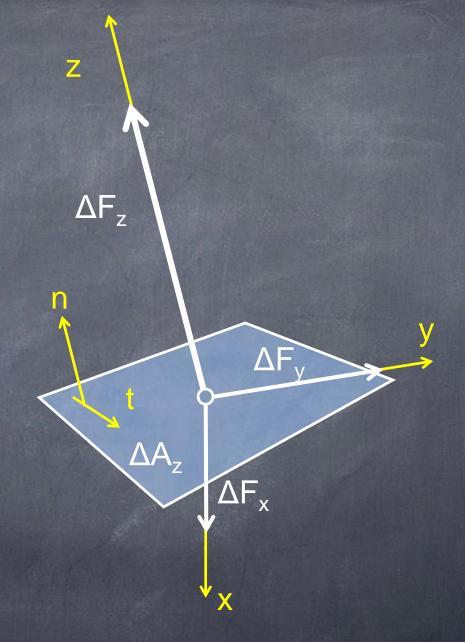
 $\begin{array}{ccc} \text{lim} & (\Delta F_x/\Delta A_z) & \rightarrow \tau_{zx} & \text{valor finito} \\ \Delta A_z \rightarrow 0 & & & \end{array}$

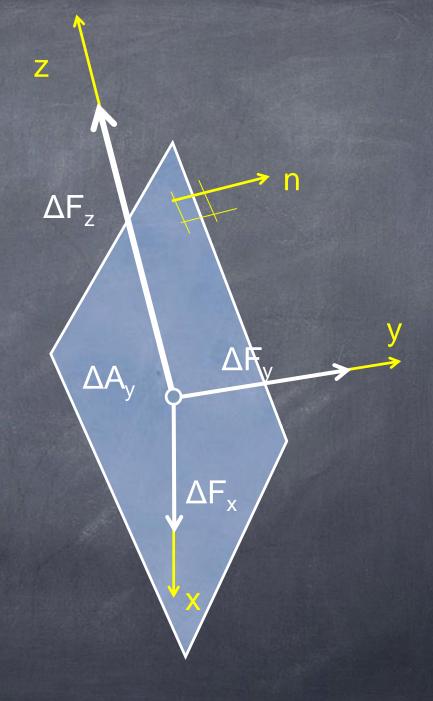


$$\begin{array}{ll} lim \;\; (\Delta F_x/\Delta A_z) \;\; \to \; \tau_{zx} & \;\; valor \; finito \\ \Delta A_z \to \; 0 & \;\; \\ lim \;\; (\Delta F_y/\Delta A_z) \;\; \to \; \tau_{zy} \\ \Delta A_z \to \; 0 & \;\; \end{array}$$

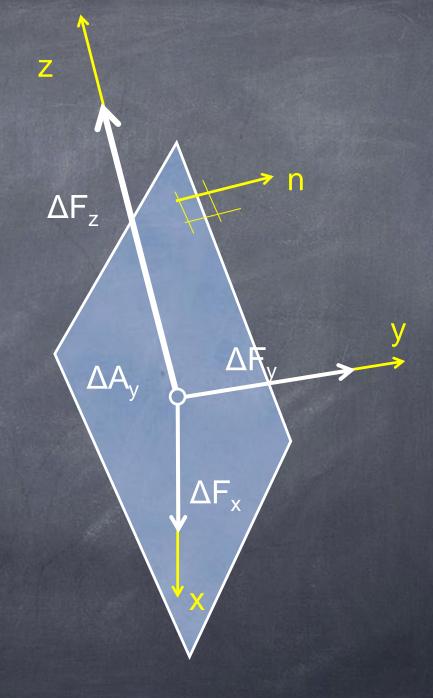


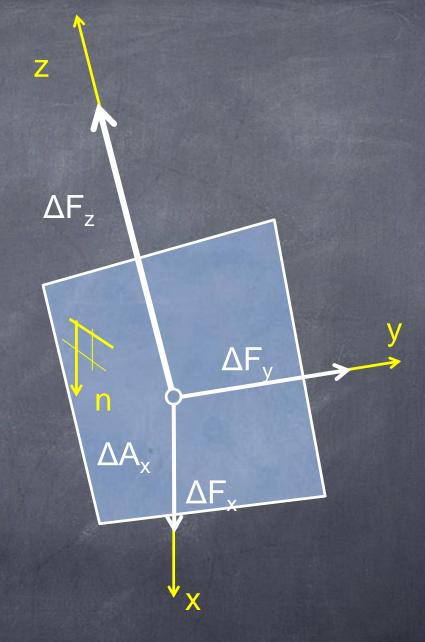
$$\begin{array}{l} lim \; (\Delta F_x/\Delta A_z) \; \to \tau_{zx} \quad \mbox{valor finito} \\ \Delta A_z \to 0 \\ lim \; (\Delta F_y/\Delta A_z) \; \to \tau_{zy} \\ \Delta A_z \to 0 \\ lim \; (\Delta F_z/\Delta A_z) \; \to \sigma_{zz} \\ \Delta A_z \to 0 \end{array}$$



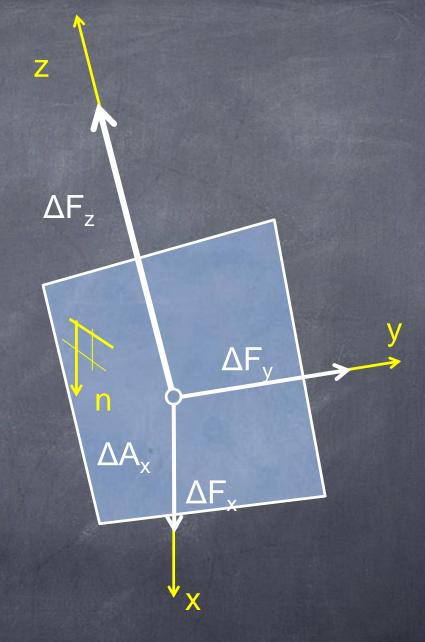


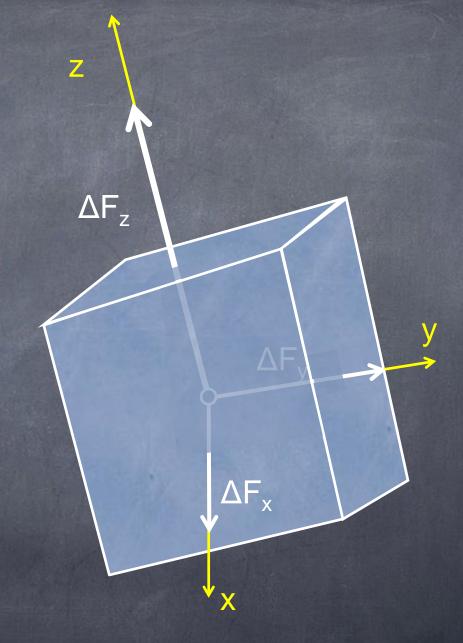
$$\begin{array}{ll} lim \;\; (\Delta F_x/\Delta A_y) \;\; \to \tau_{yx} \\ \Delta A_y \to 0 \\ \\ lim \;\; (\Delta F_y/\Delta A_y) \;\; \to \sigma_{yy} \\ \Delta A_y \to 0 \\ \\ lim \;\; (\Delta F_z/\Delta A_y) \;\; \to \tau_{yz} \\ \Delta A_y \to 0 \end{array}$$

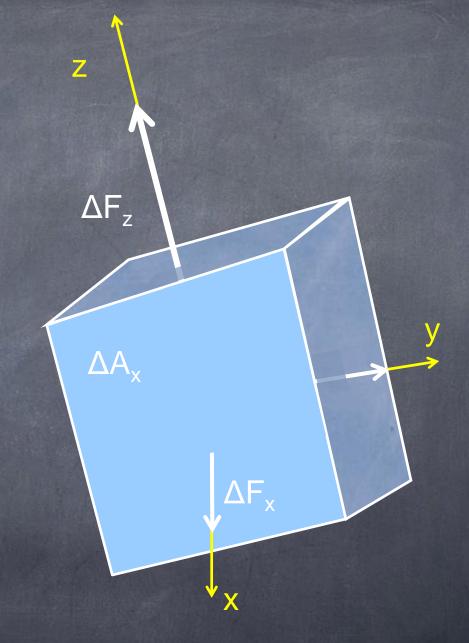


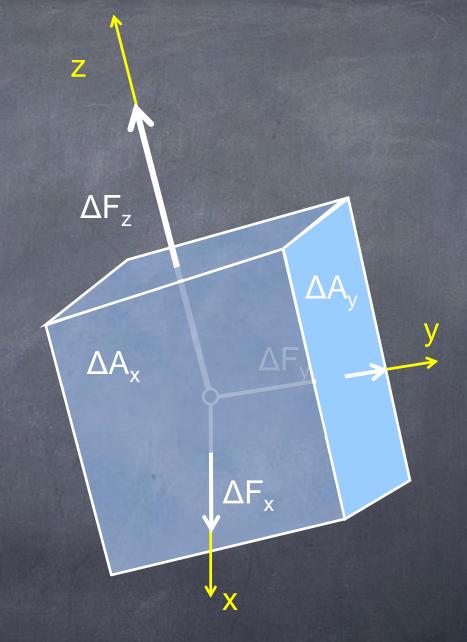


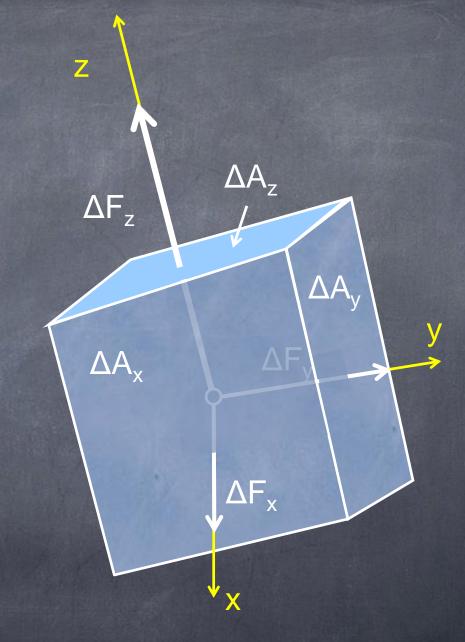
$$\begin{array}{ll} lim \;\; (\Delta F_x/\Delta A_x) \;\; \to \; \sigma_{xx} \\ \Delta A_x \to \; 0 \\ \\ lim \;\; (\Delta F_y/\Delta A_x) \;\; \to \; \tau_{xy} \\ \Delta A_x \to \; 0 \\ \\ lim \;\; (\Delta F_z/\Delta A_x) \;\; \to \; \tau_{xz} \\ \Delta A_x \to \; 0 \end{array}$$

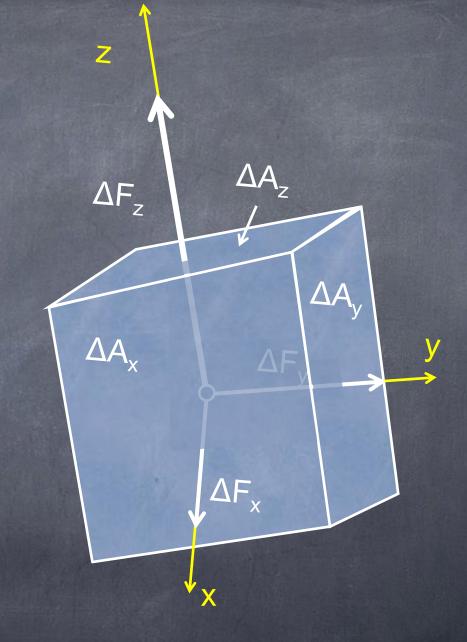


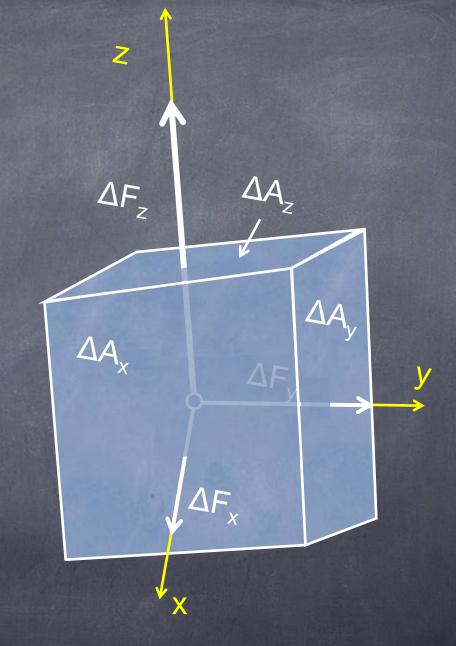


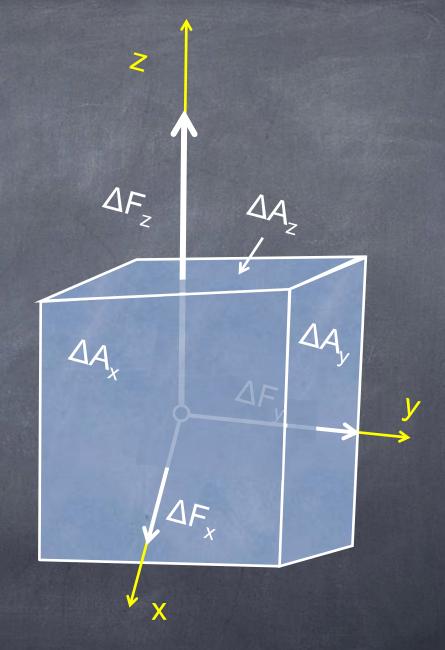


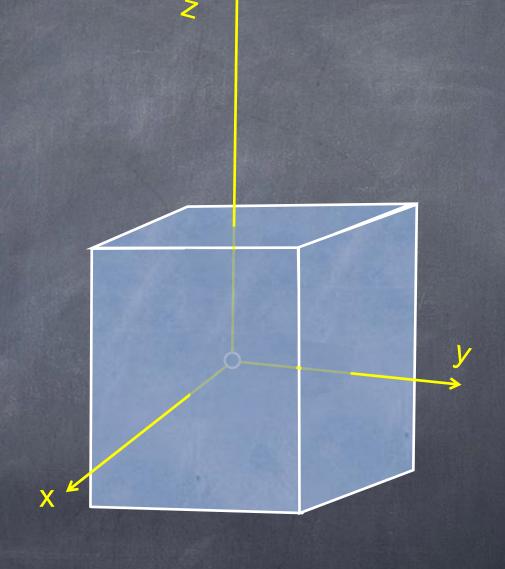


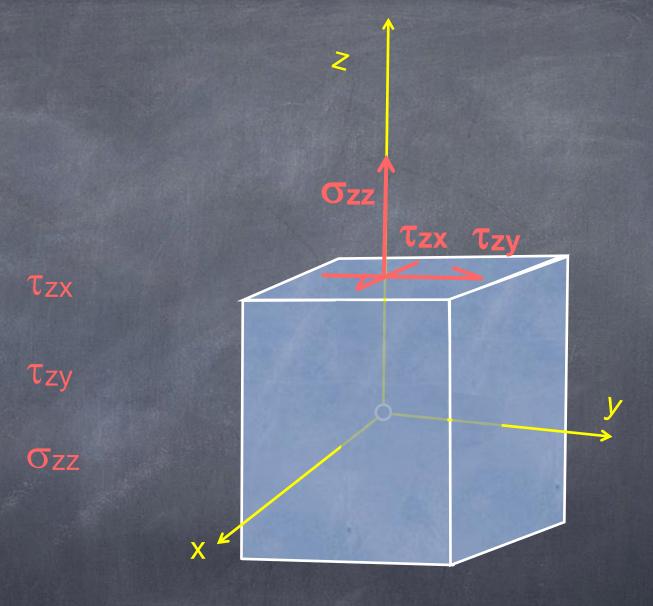








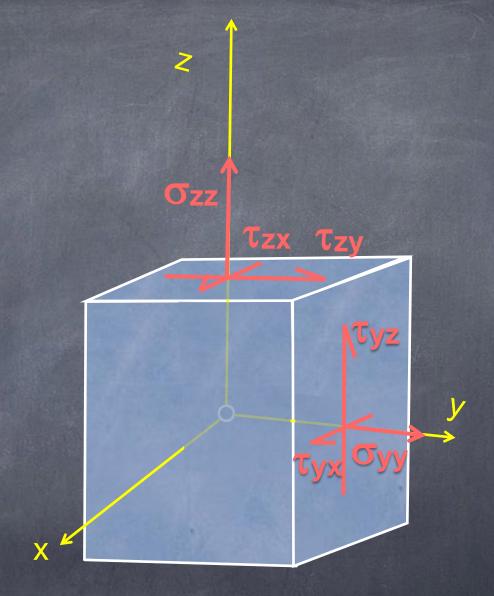




 τ_{yx} τ_{zx}

суу т у

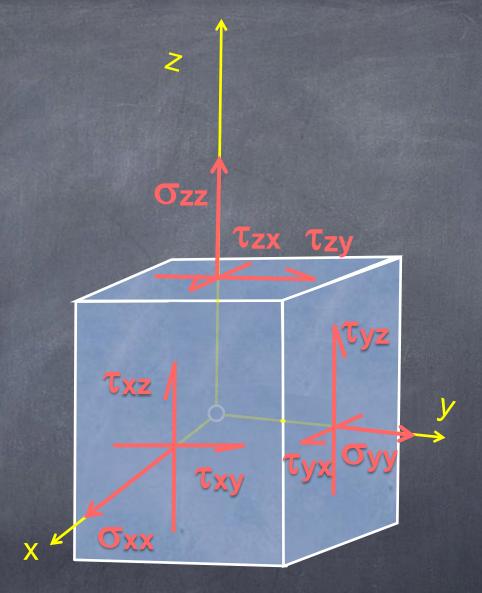
tyz Gzz



 σ_{xx} τ_{yx} τ_{zx}

 τ_{xy} σ_{yy} τ_{zy}

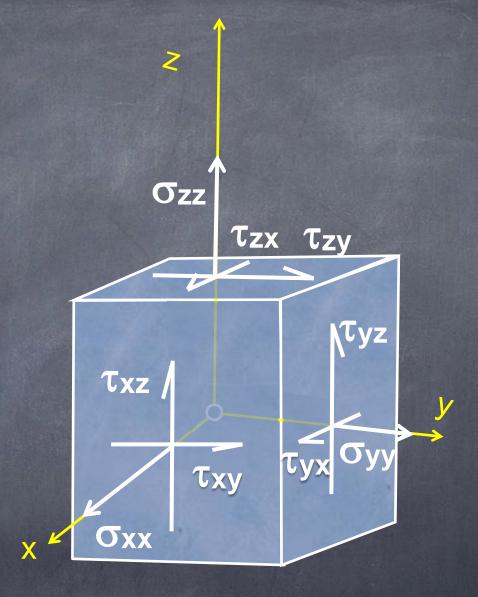
 τ_{xz} τ_{yz} σ_{zz}



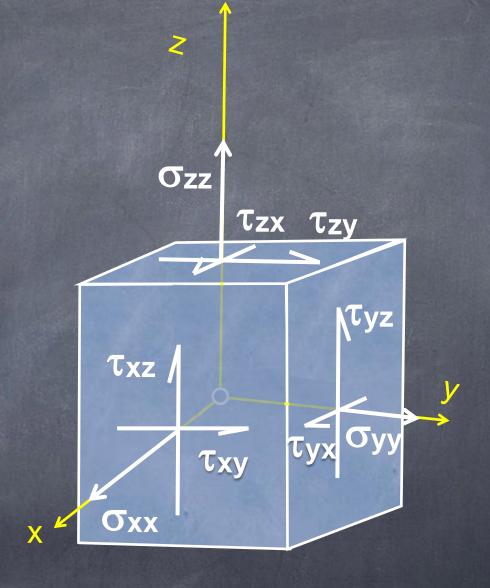
 σ_{xx} τ_{yx} τ_{zx}

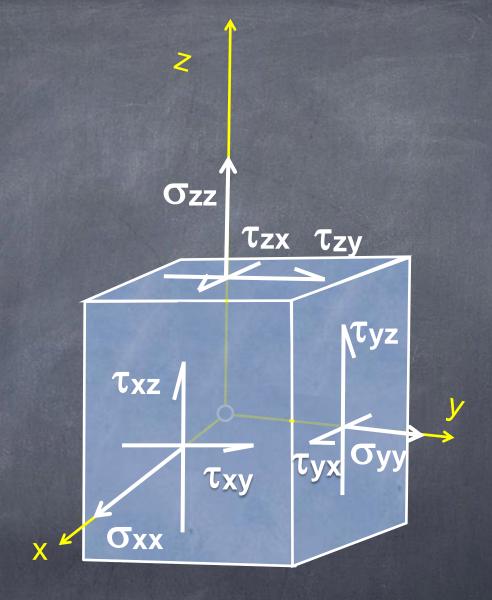
 τ_{xy} σ_{yy} τ_{zy}

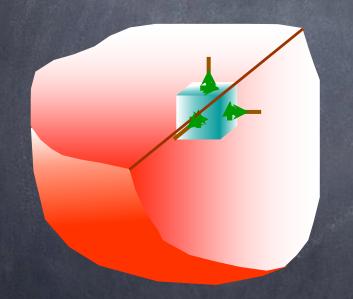
 τ_{xz} τ_{yz} σ_{zz}



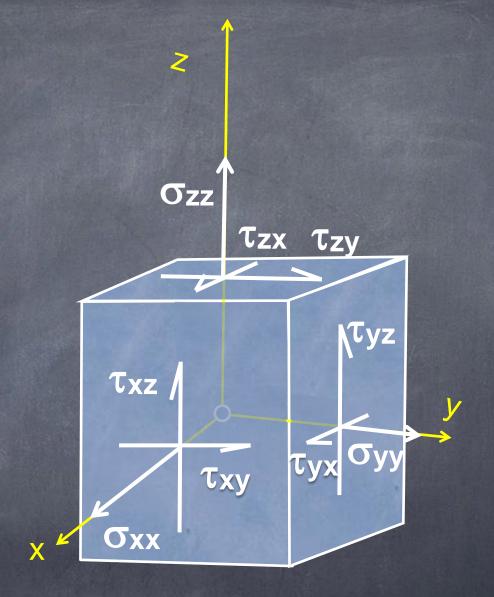
Estado geral de tensões

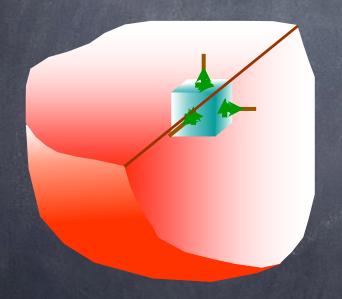


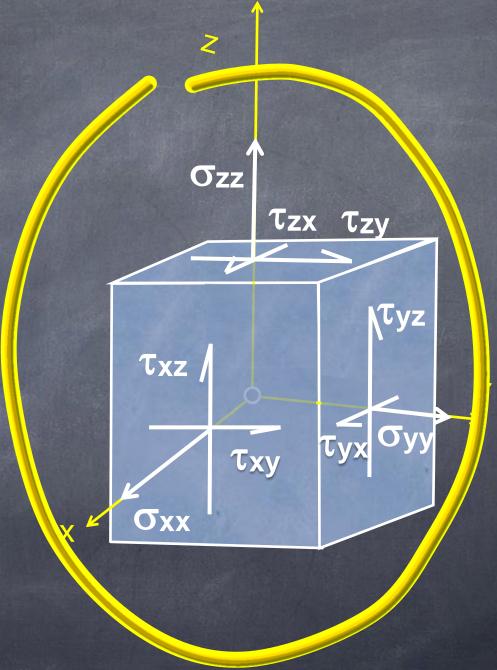




X

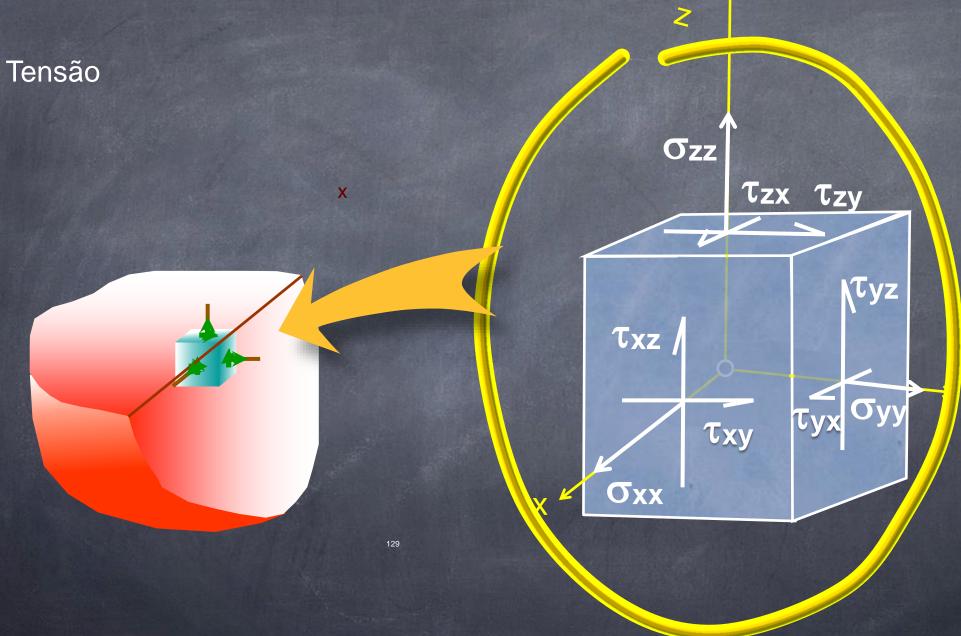






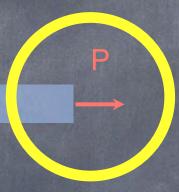
128

X

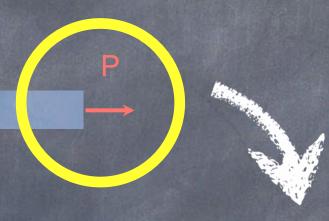


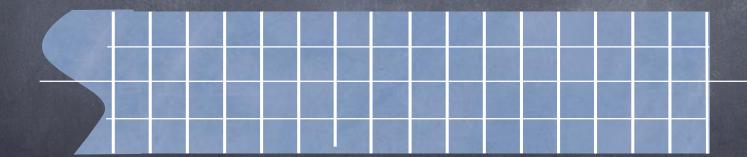




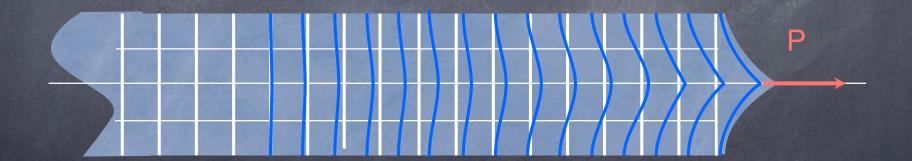


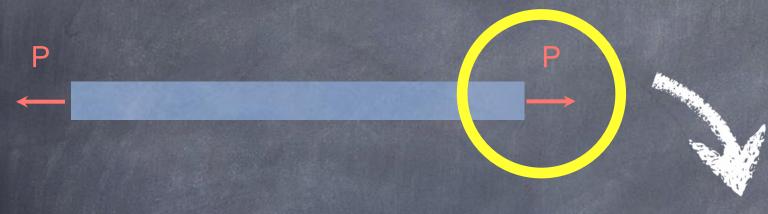
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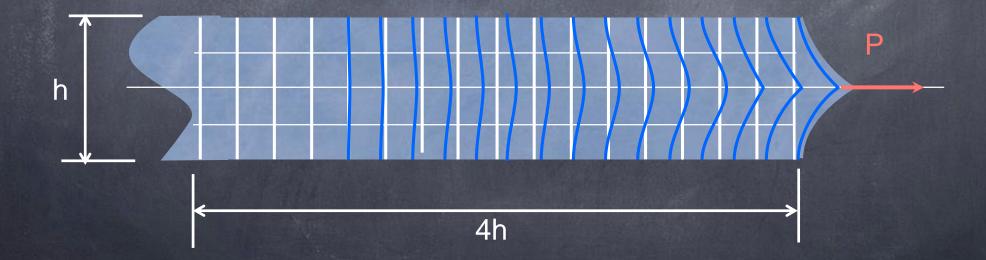


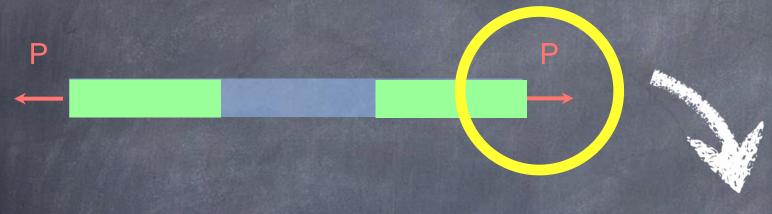


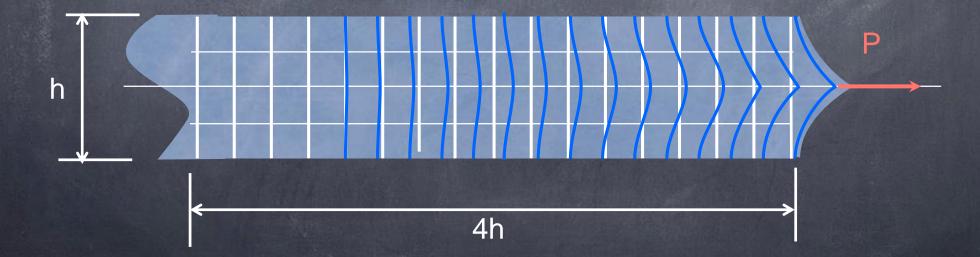
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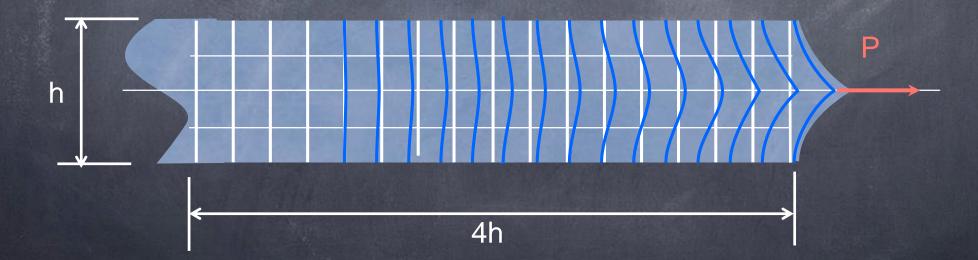




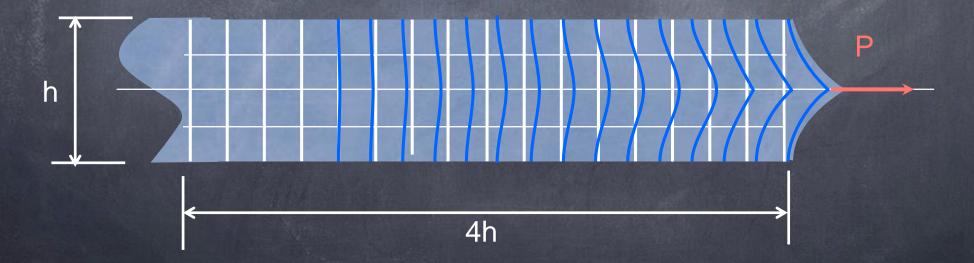








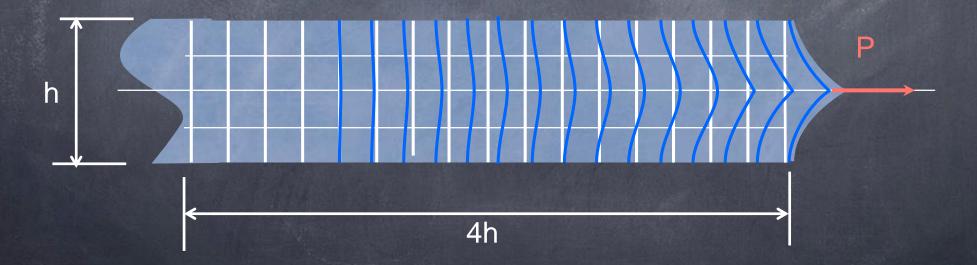




Hipóteses:

Tensão normal média

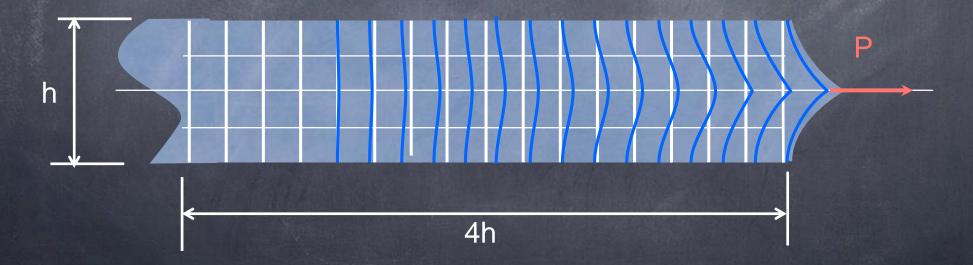




Hipóteses:

1. Deformação uniforme

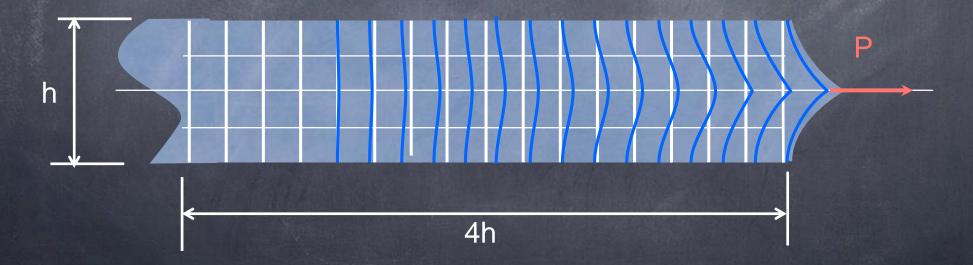




Hipóteses:

- 1. Deformação uniforme
- 2. Material homogêneo e isotrópico





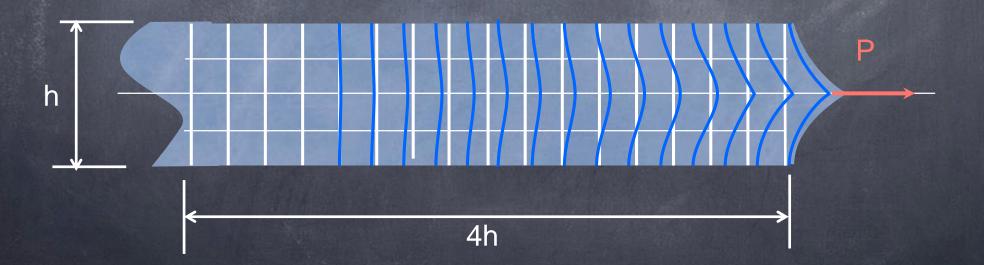
Hipóteses:

1. Deformação uniforme

2. Material homogêneo e isotrópico

mesmas propriedades em todo o volume





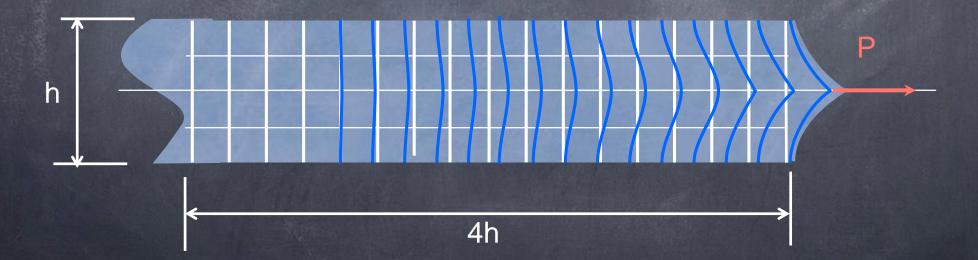
P

região considerada para análise

Hipóteses:

- 1. Deformação uniforme
- 2. Material homogêneo e isotrópico

mesmas propriedades em todas as direções



Hipóteses:

1. Deformação uniforme

2. Material homogêneo e isotrópico

des em todas as direções



barra prismática

barra prismática

carga externa P aplicada ao longo do eixo da barra

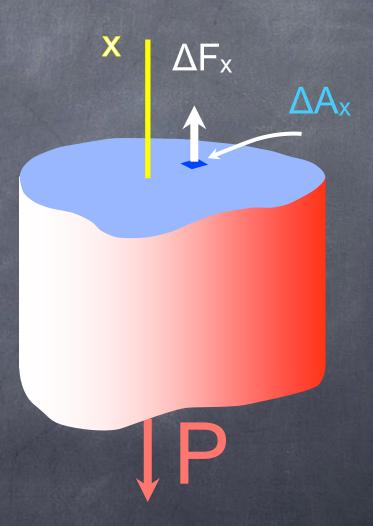


forças internas (distribuídas) que surgem na seção da barra em função da aplicação da carga externa P

barra prismática

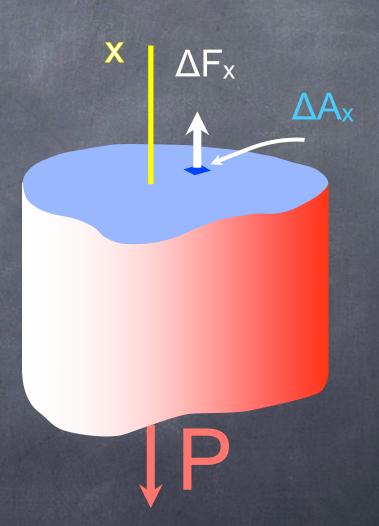
carga externa P aplicada ao longo do eixo da barra

Análise de uma das forças internas

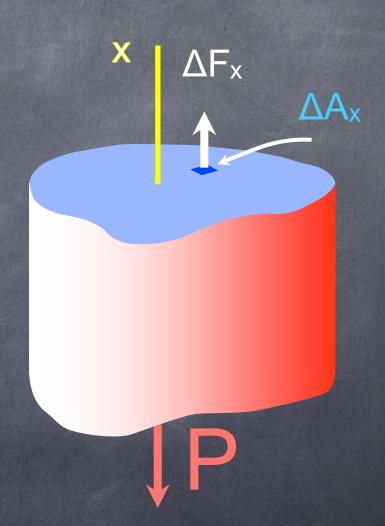


Análise de uma das forças internas

$$\overline{\sigma_x} = \frac{\Delta F_x}{\Delta A_x}$$

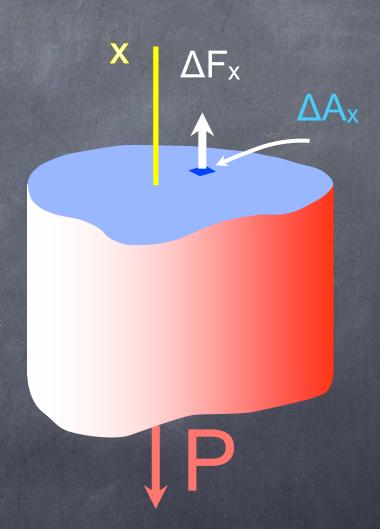


Análise de uma das forças internas



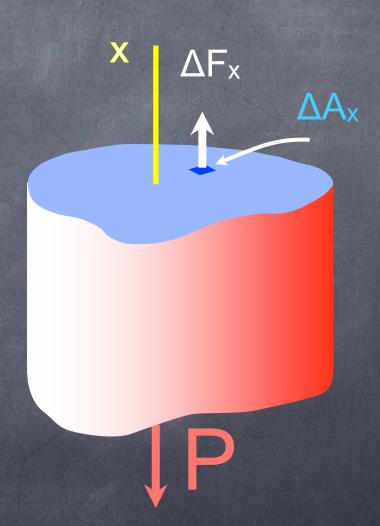
Análise de uma das forças internas

$$\frac{\Delta F_x}{\sigma_x} = \frac{\Delta F_x}{\Delta A_x} \quad \therefore \quad \Delta F_x = \sigma_x \cdot \Delta A_x$$



Análise de uma das forças internas

$$P = \int [\int (\sigma_x \cdot dz)] \cdot dy$$

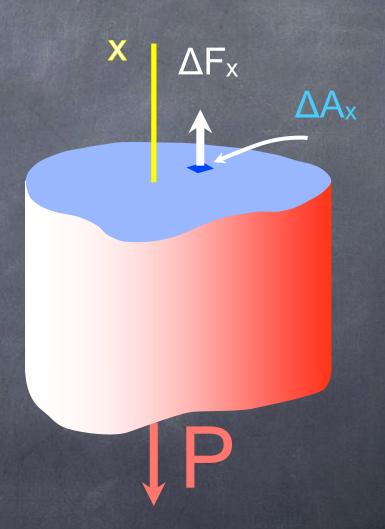


Análise de uma das forças internas

$$\frac{\sigma_{x}}{\sigma_{x}} = \frac{\Delta F_{x}}{\Delta A_{x}} \quad \therefore \quad \Delta F_{x} = \sigma_{x} . \Delta A_{x}$$

$$P = \int [\int (\sigma_x \cdot dz)] \cdot dy$$

$$P = \iint (\sigma_x) dz dy$$



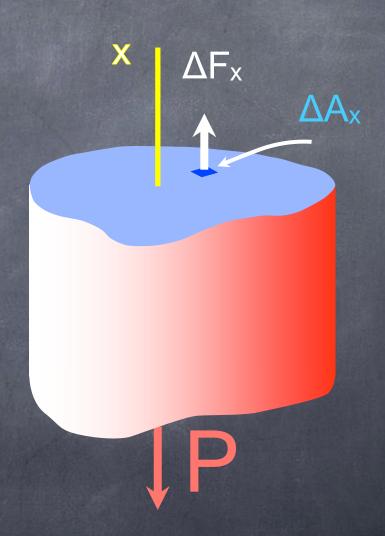
Análise de uma das forças internas

$$\frac{\sigma_{x}}{\sigma_{x}} = \frac{\Delta F_{x}}{\Delta A_{x}} \quad \therefore \quad \Delta F_{x} = \sigma_{x} \cdot \Delta A_{x}$$

$$P = \int [\int (\sigma_x \cdot dz)] \cdot dy$$

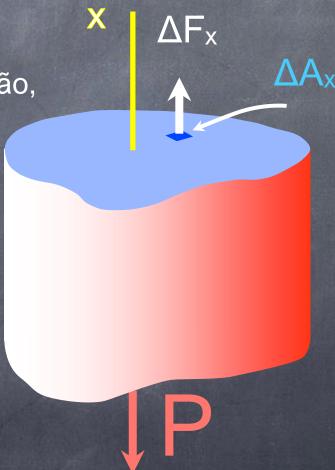
$$P = \iint (\sigma_x) dz dy$$

$$P = \int_{A} (\sigma_{x}) dA$$



Análise de uma das forças internas

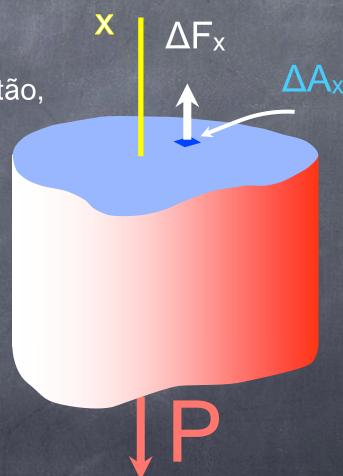
A tensão média em toda a área é dada, então, por



Análise de uma das forças internas

A tensão média em toda a área é dada, então, por

 $\sigma_x =$

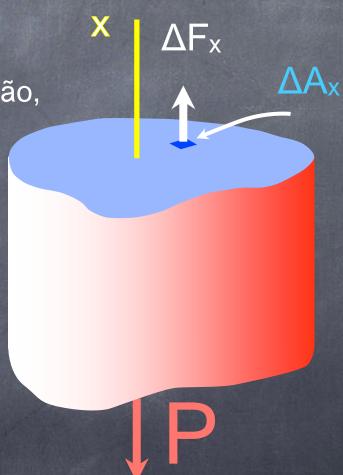


Análise de uma das forças internas

A tensão média em toda a área é dada, então,

por

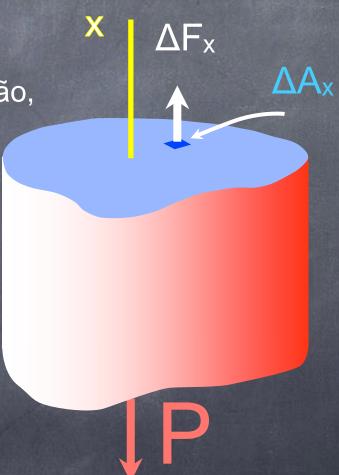
$$\frac{1}{\sigma_{x}} = \frac{\int_{A} (\sigma_{x}) dA}{\int_{A} dA}$$



Análise de uma das forças internas

A tensão média em toda a área é dada, então, por

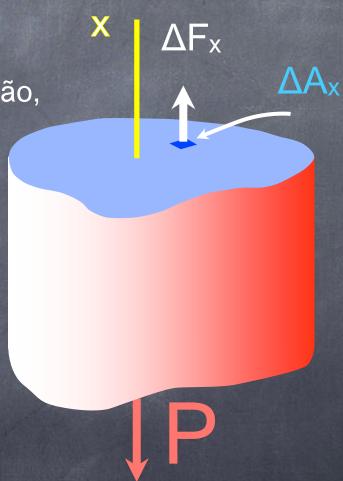
$$\frac{1}{\sigma_{x}} = \frac{\int_{A} (\sigma_{x}) dA}{\int_{A} dA} = \frac{P}{A}$$



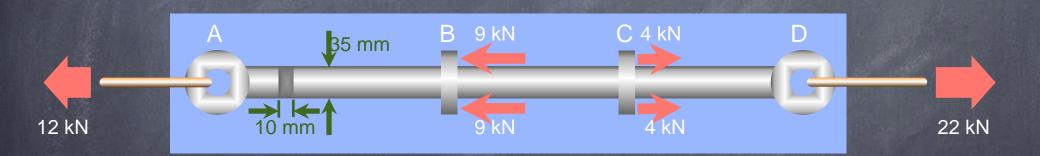
Análise de uma das forças internas

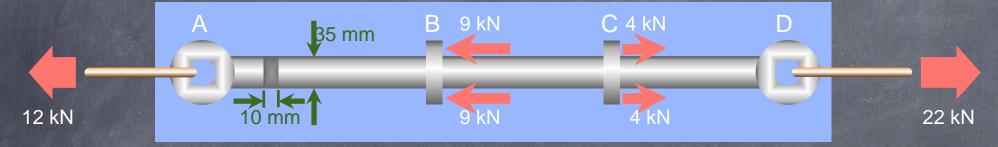
A tensão média em toda a área é dada, então, por

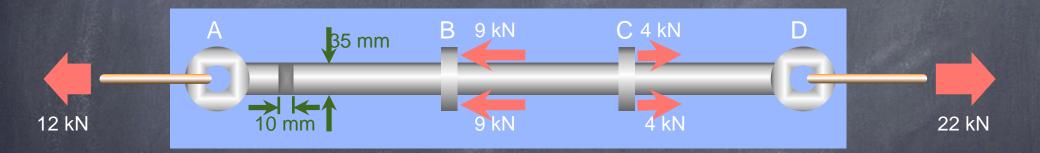
$$\frac{1}{\sigma_{x}} = \frac{\int_{A} (\sigma_{x}) dA}{\int_{A} dA} = \frac{P}{A}$$

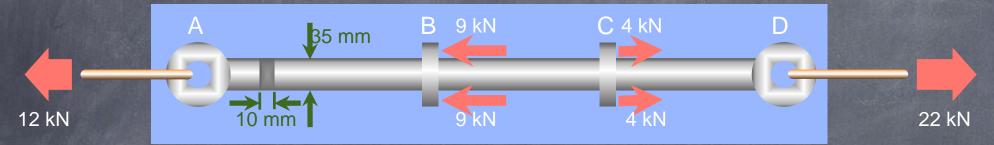


Determinar a tensão normal média máxima na barra da figura quando ela é submetida ao carregamento mostrado.

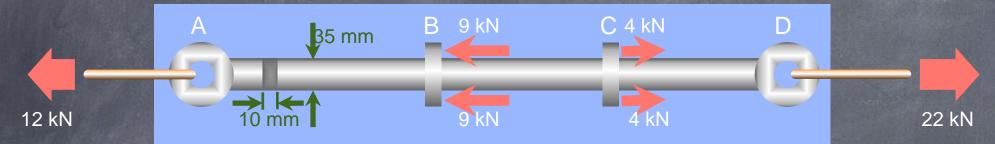


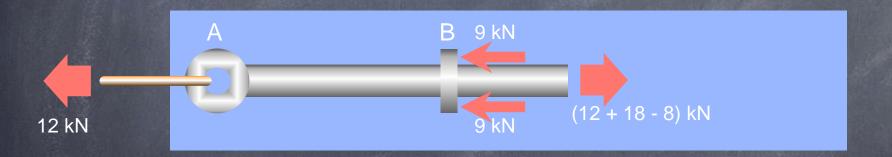


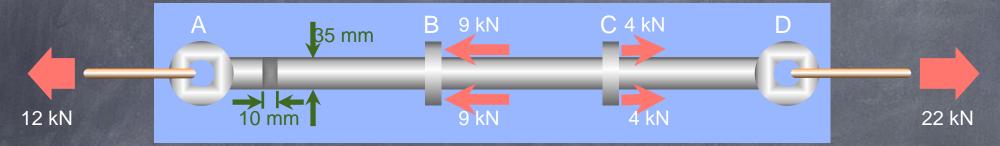


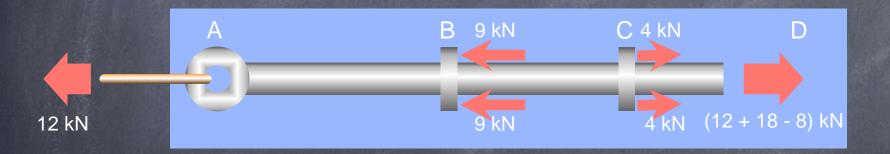


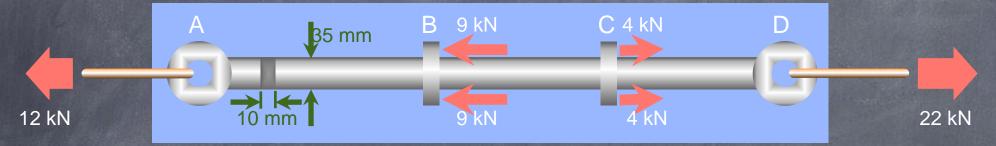


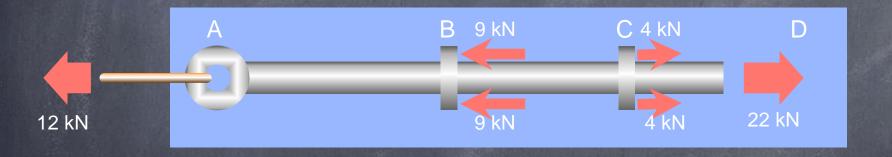


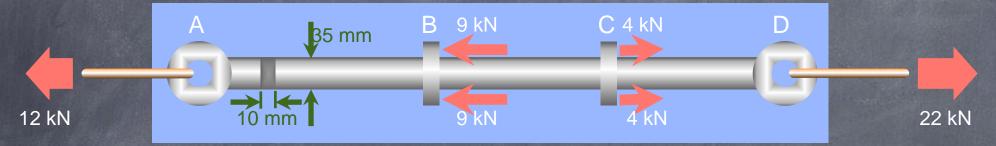












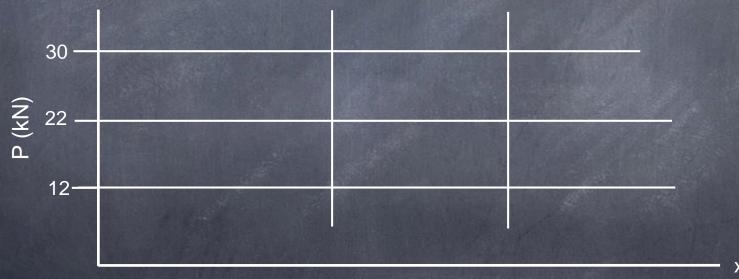
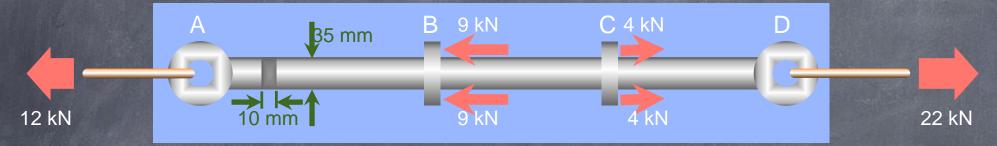
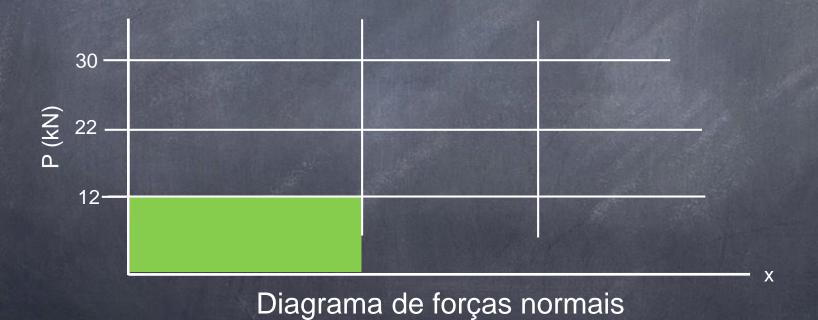
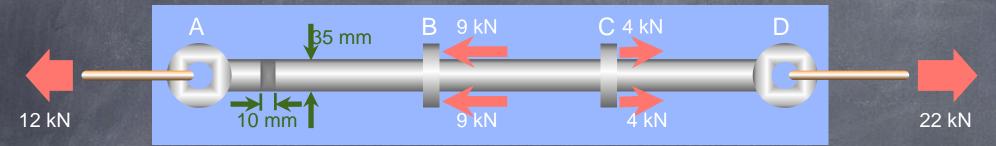
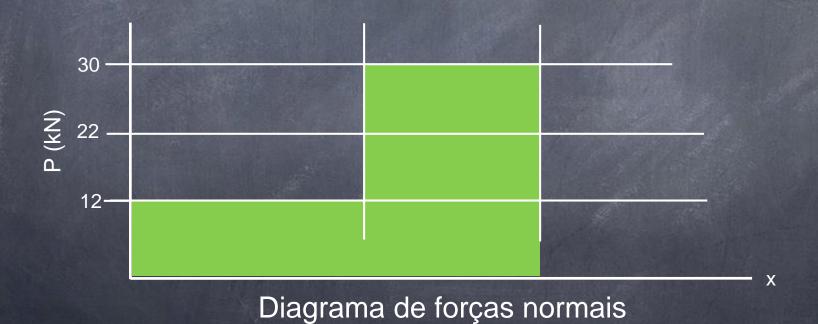


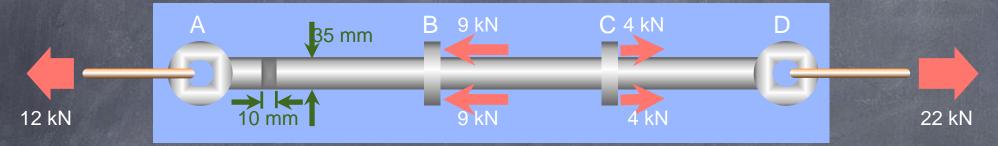
Diagrama de forças normais

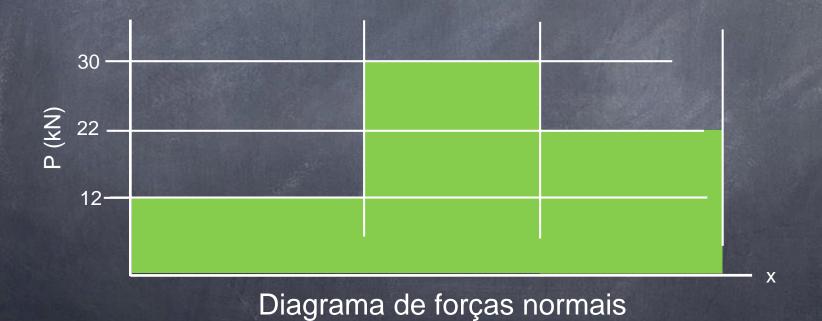


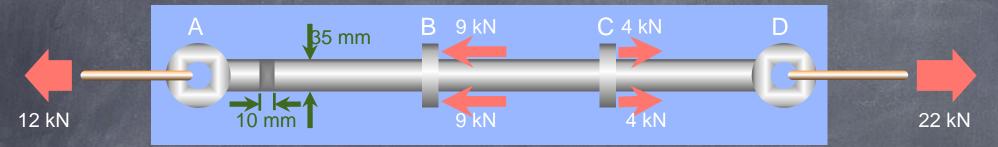


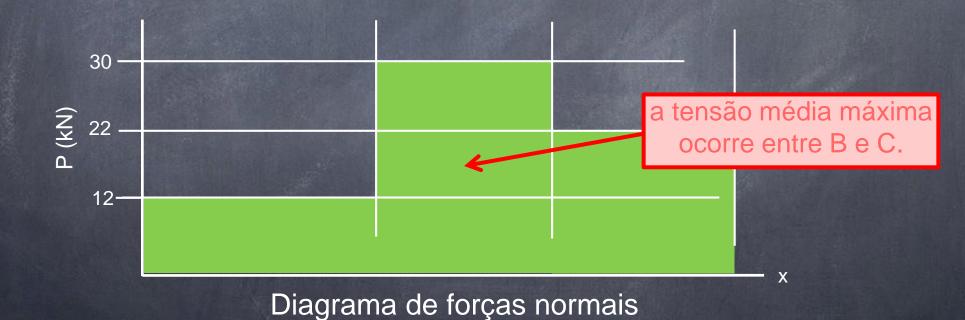


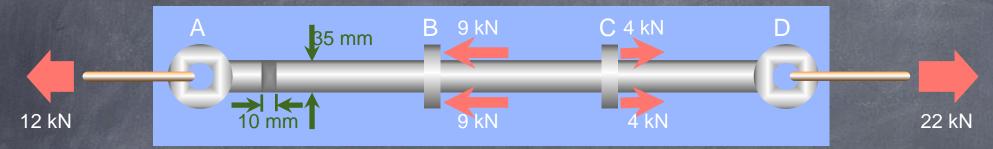




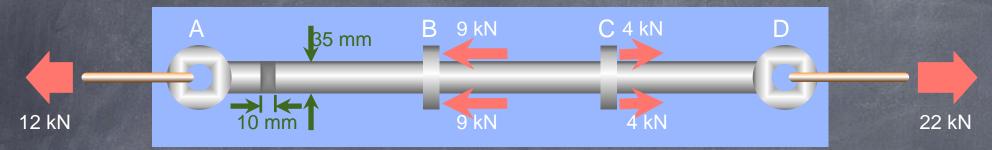






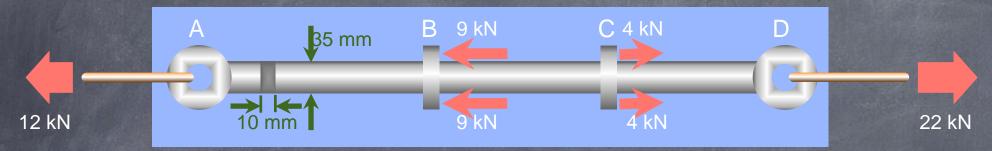


A tensão média máxima pode ser calculada por



A tensão média máxima pode ser calculada por

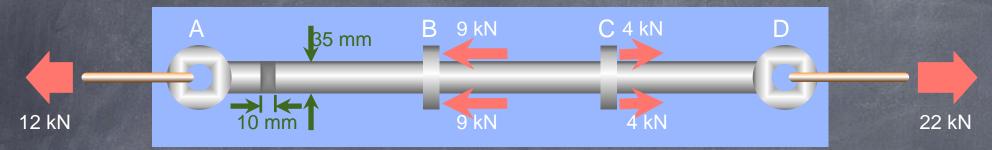
 $\sigma = 30 \text{ kN} / (0.035 \text{ m} \times 0.010 \text{ m})$



A tensão média máxima pode ser calculada por

$$\sigma = 30 \text{ kN} / (0.035 \text{ m} \times 0.010 \text{ m})$$

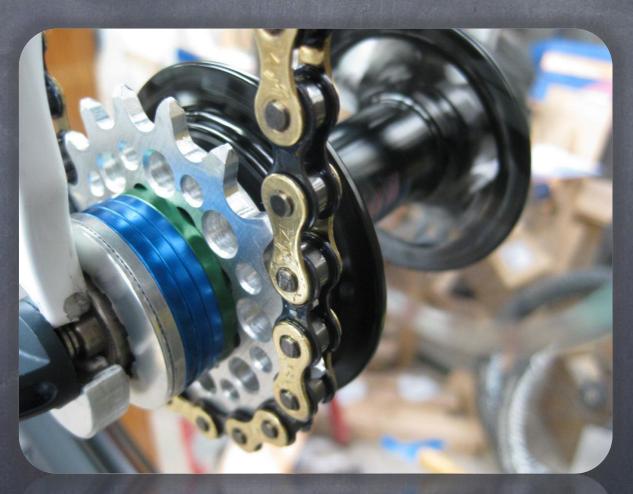
$$\sigma$$
 = 87,5 MPa

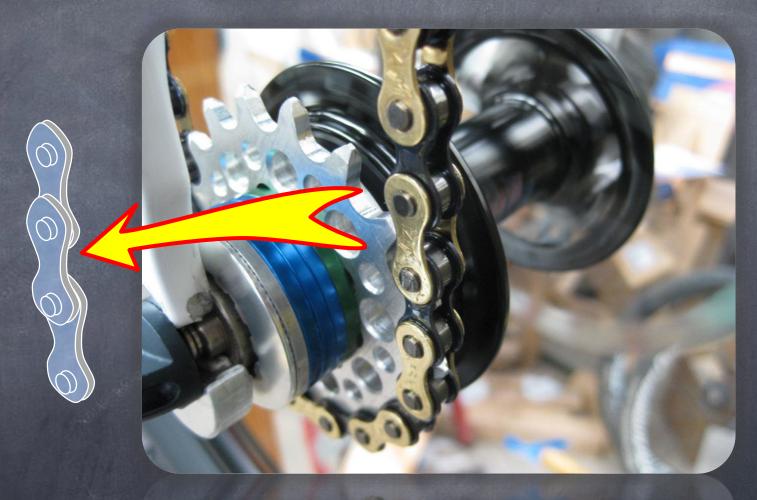


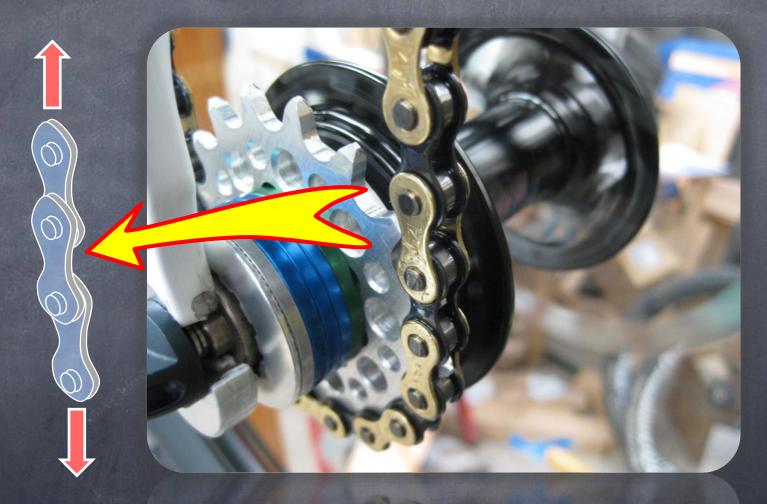
A tensão média máxima pode ser calculada por

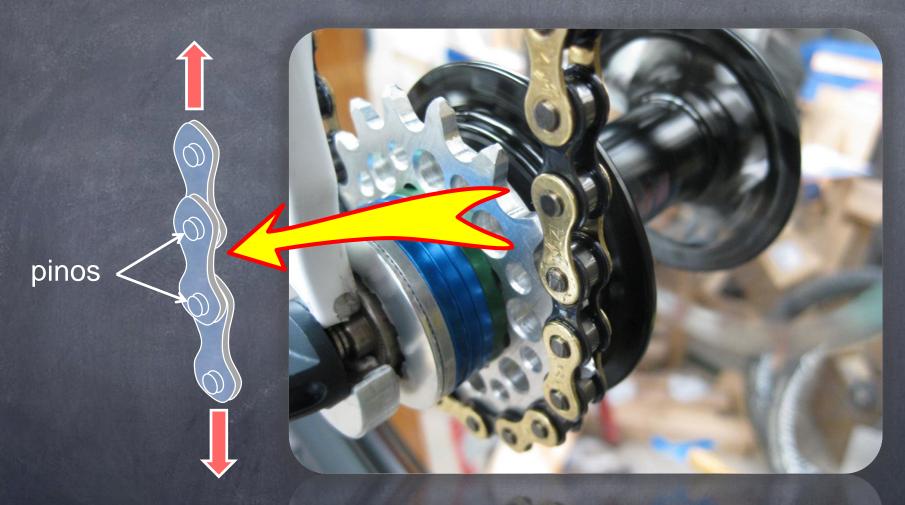
 $\sigma = 30 \text{ kN} / (0.035 \text{ m} \times 0.010 \text{ m})$

 σ = 87,5 MPa



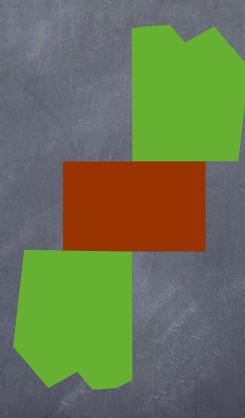


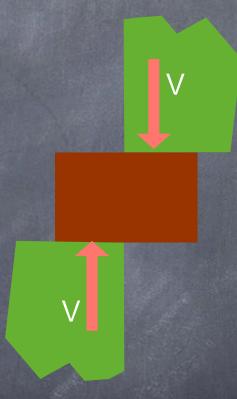


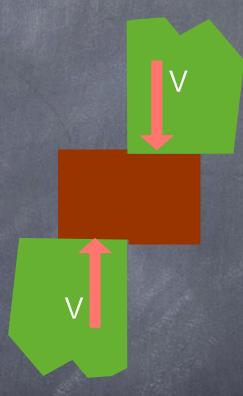


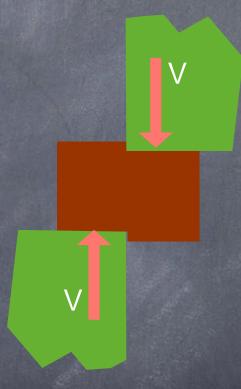
pino

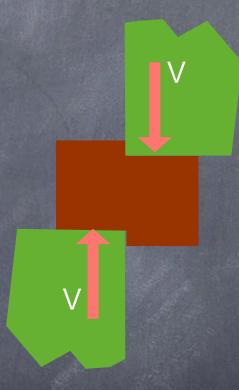


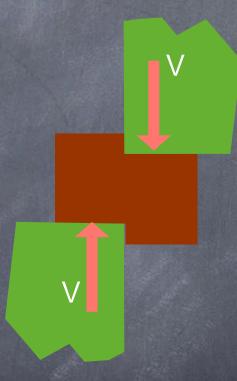


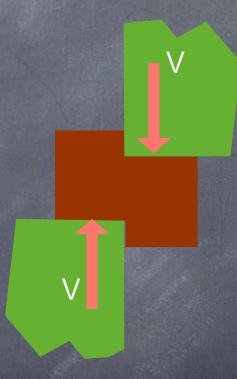


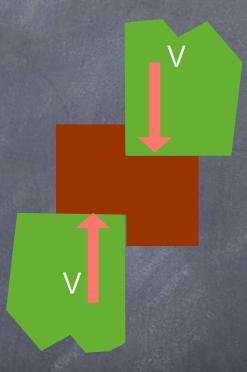


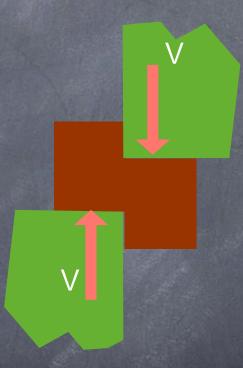


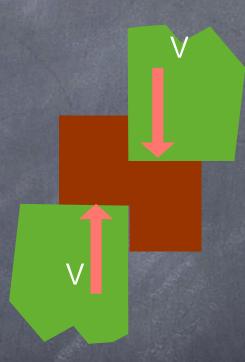


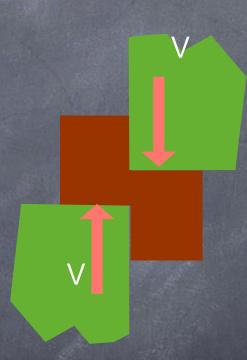


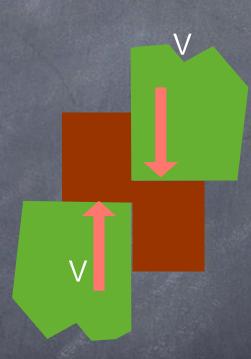


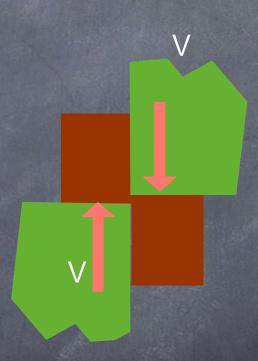


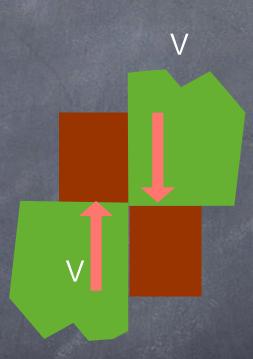






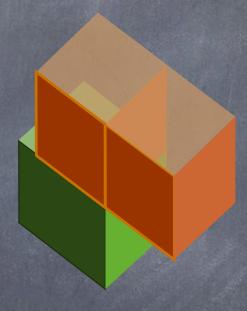


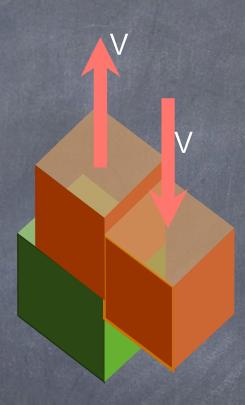


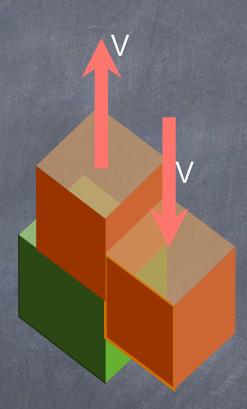


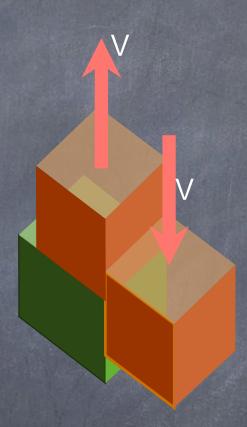


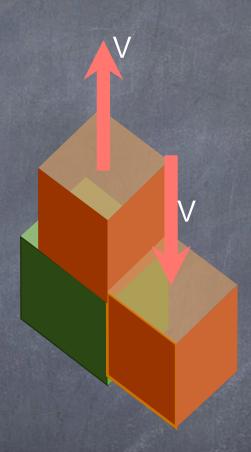


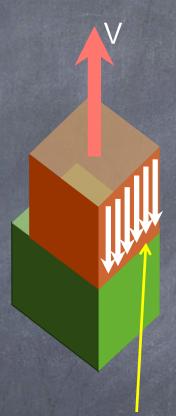






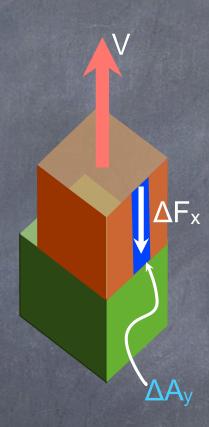




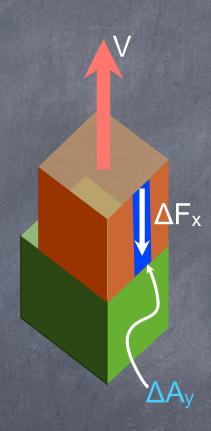


força distribuída tangente à superfície

$$\tau_{xy} = \frac{\Delta F_x}{\Delta A}$$



$$\tau_{xy} = \frac{\Delta F_x}{\Delta A} = \Delta F_x = \tau_{xy} \cdot \Delta A_y$$



$$\tau_{xy} = \frac{\Delta F_x}{\Delta A} = \Delta F_x = \tau_{xy} \cdot \Delta A_y$$

$$V \cong \sum \Delta F_x = \sum \tau_{xy} \cdot \Delta A_y = \sum \tau_{xy} \cdot \Delta z \cdot \Delta x$$

$$\tau_{xy} = \frac{\Delta F_{x}}{\Delta A} = \cdot \Delta F_{x} = \tau_{xy} \cdot \Delta A_{y}$$

$$V \cong \sum \Delta F_{x} = \sum \tau_{xy} \cdot \Delta A_{y} = \sum \tau_{xy} \cdot \Delta z \cdot \Delta x$$

$$V \cong \lim_{\Delta x \to 0} [\lim_{\Delta z \to 0} (\sum \tau_{xy} \cdot \Delta z) \cdot \Delta x]$$

$$\tau_{xy} = \frac{\Delta F_{x}}{\Delta A} = \cdot \cdot \Delta F_{x} = \tau_{xy} \cdot \Delta A_{y}$$

$$V \cong \sum \Delta F_{x} = \sum \tau_{xy} \cdot \Delta A_{y} = \sum \tau_{xy} \cdot \Delta z \cdot \Delta x$$

$$V \cong \lim_{\Delta x \to 0} [\lim_{\Delta z \to 0} (\sum \tau_{xy} \cdot \Delta z) \cdot \Delta x]$$

$$V = \int [\int (\tau_{xy} \cdot dz)] \cdot \Delta x = y$$

$$\tau_{xy} = \frac{\Delta F_{x}}{\Delta A} = \Delta F_{x} = \tau_{xy} \cdot \Delta A_{y}$$

$$V \cong \sum \Delta F_{x} = \sum \tau_{xy} \cdot \Delta A_{y} = \sum \tau_{xy} \cdot \Delta z \cdot \Delta x$$

$$V \cong \lim_{\Delta x \to 0} \left[\lim_{\Delta z \to 0} (\sum \tau_{xy} \cdot \Delta z) \cdot \Delta x \right]$$

$$V = \int \left[\int (\tau_{xy} \cdot dz) \right] \cdot \Delta x = \lambda$$

$$V = \int \left[\int (\tau_{xy} \cdot dz) \right] \cdot dx = \int (\tau_{xy} \cdot dz) dz$$

$$\tau_{xy} = \frac{\Delta F_{x}}{\Delta A} = \cdot \cdot \Delta F_{x} = \tau_{xy} \cdot \Delta A_{y}$$

$$V \cong \sum \Delta F_{x} = \sum \tau_{xy} \cdot \Delta A_{y} = \sum \tau_{xy} \cdot \Delta z \cdot \Delta x$$

$$V \cong \lim_{\Delta x \to 0} \left[\lim_{\Delta z \to 0} (\sum \tau_{xy} \cdot \Delta z) \cdot \Delta x \right]$$

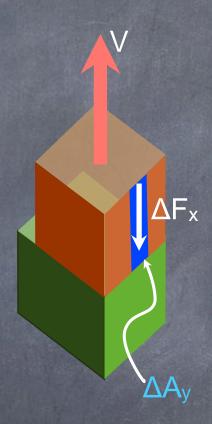
$$V = \int \left[\int (\tau_{xy} \cdot dz) \right] \cdot \Delta x = 0$$

$$V = \int \left[\int (\tau_{xy} \cdot dz) \right] \cdot dx = \int (\tau_{xy} \cdot dz) dz$$

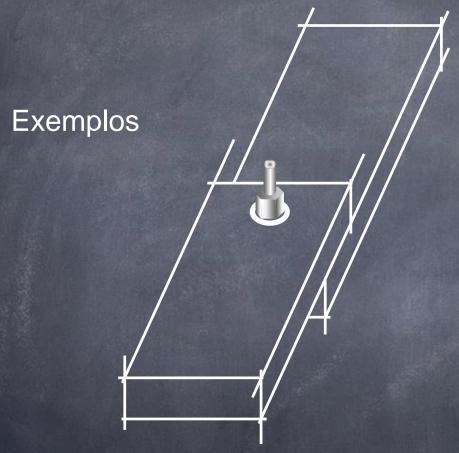
$$V = \int \left[\int (\tau_{xy} \cdot dz) \right] \cdot dx = \int (\tau_{xy} \cdot dz) dz$$

A tensão tangencial média é dada por

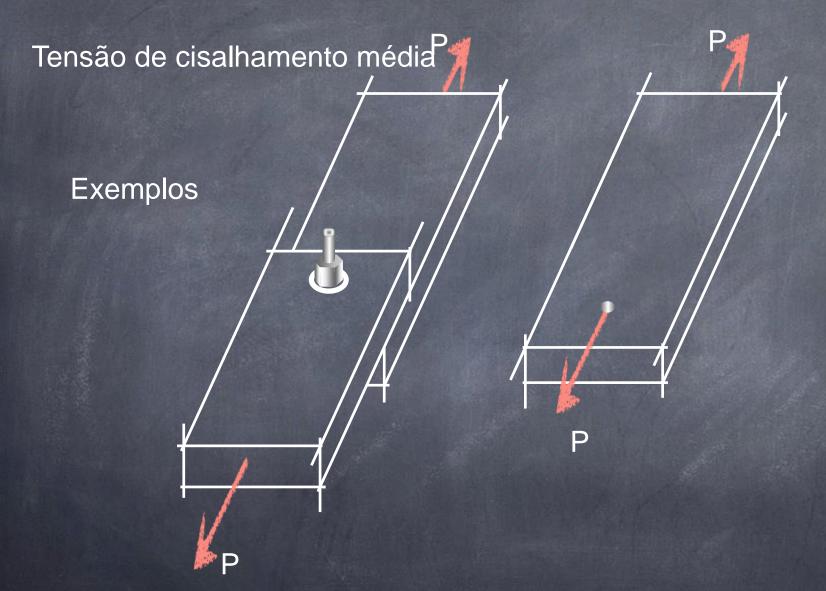
$$\frac{\int_{A}^{C} (T_{xy}) dA}{T_{xy}} = \frac{\int_{A}^{C} (T_{xy}) dA}{\int_{A}^{C} dA} = \frac{V}{A}$$

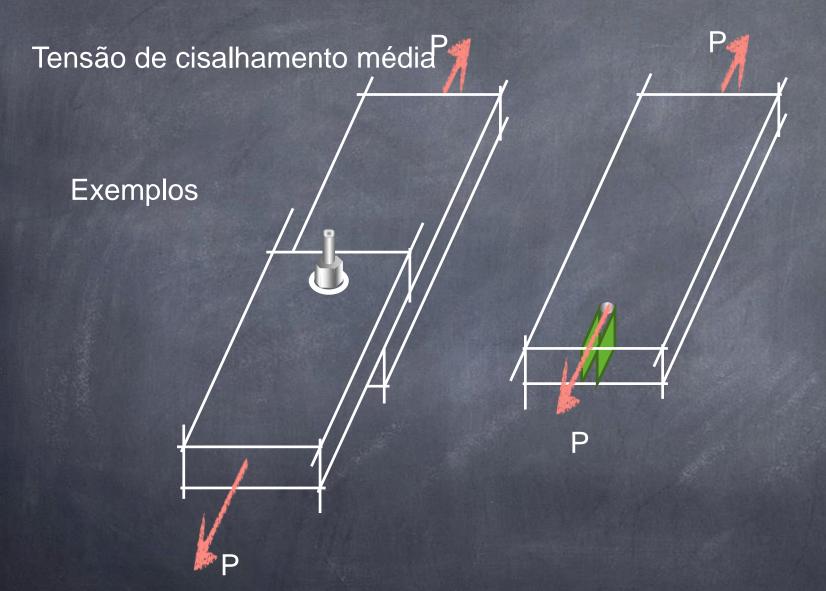


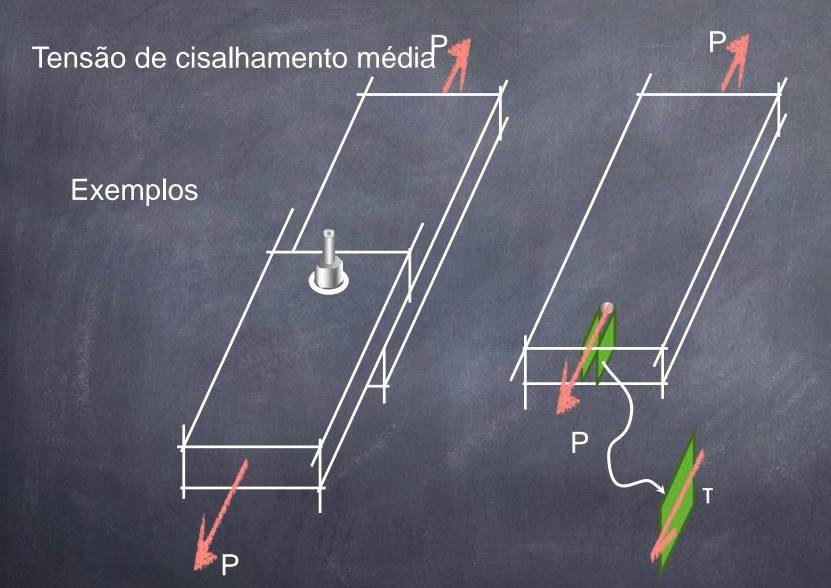
Exemplos

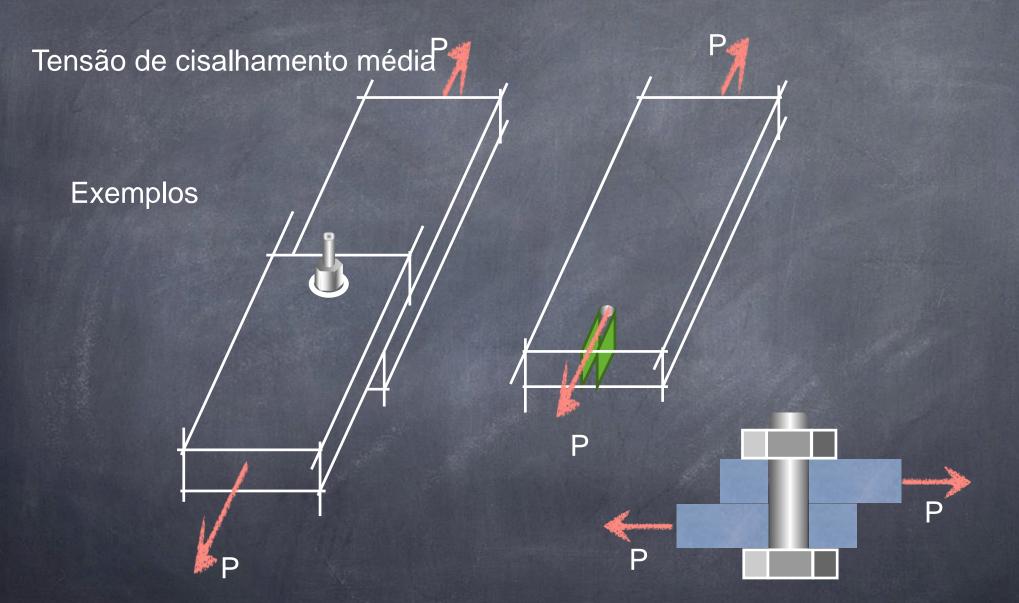


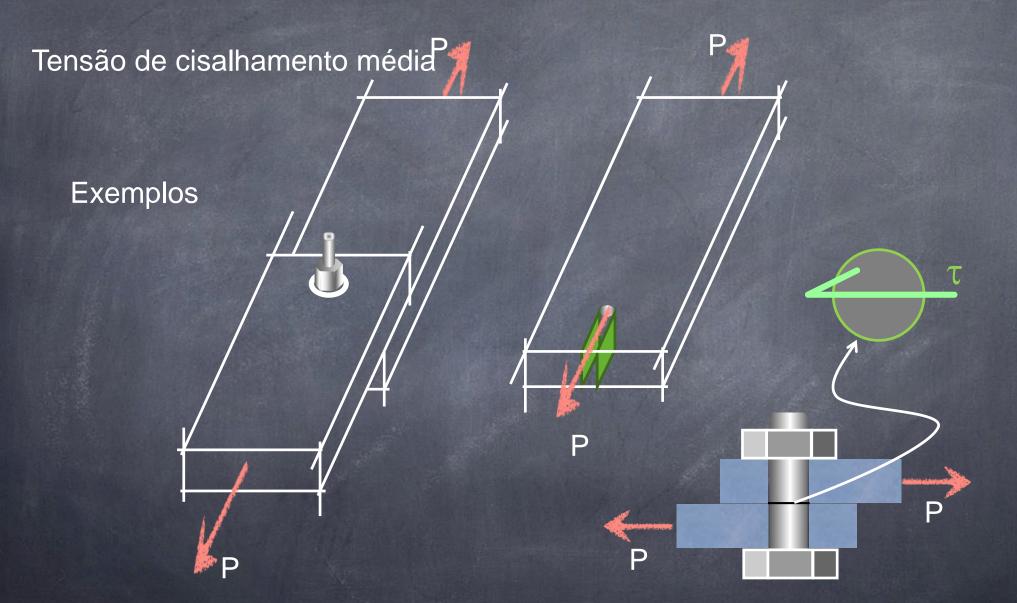
Tensão de cisalhamento média Exemplos

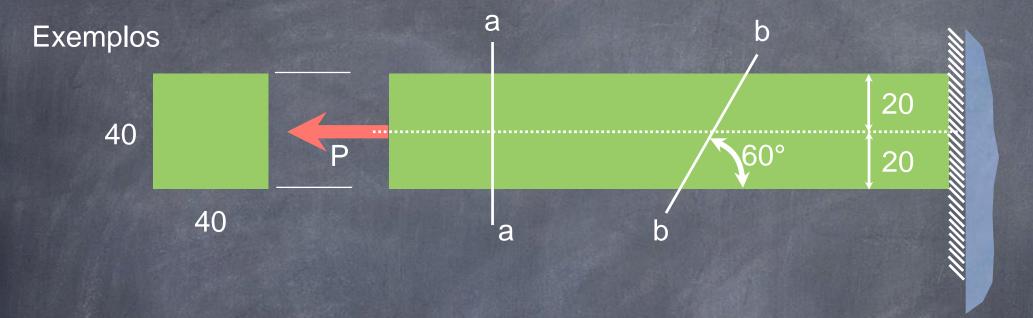




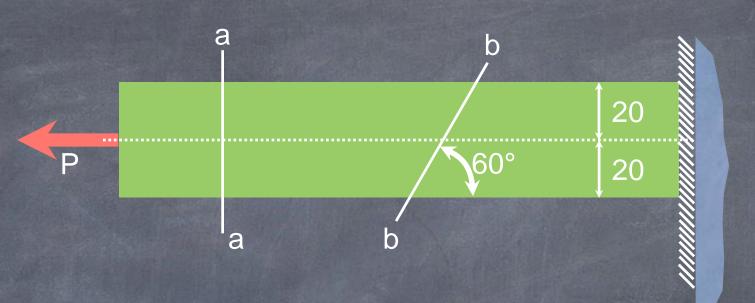




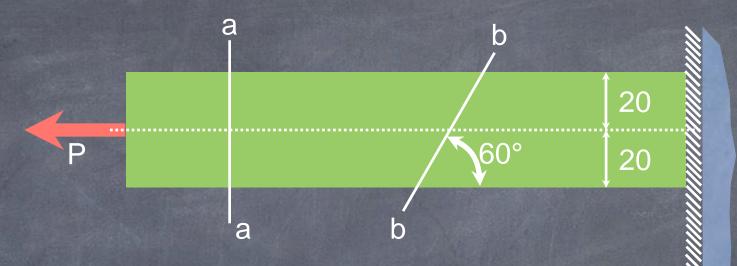




A barra de seção quadrada da figura é submetida a uma força axial P = 800 N. Determinar a tensão normal média e a tensão cisalhante média que atuam nos planos a-a e b-b.

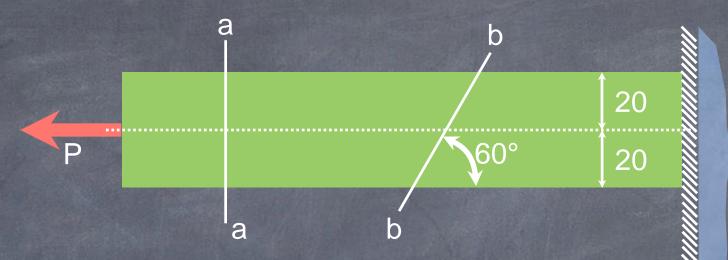






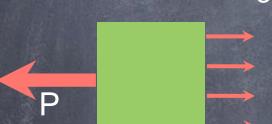
Na seção a-a

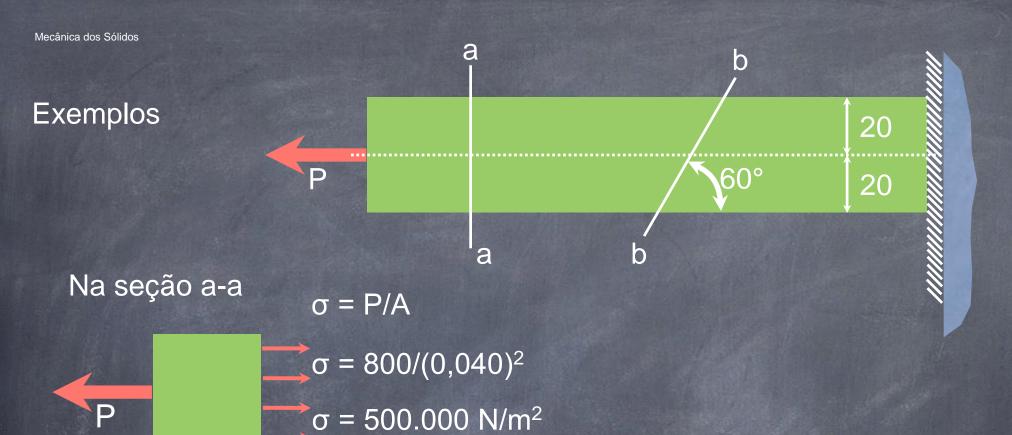




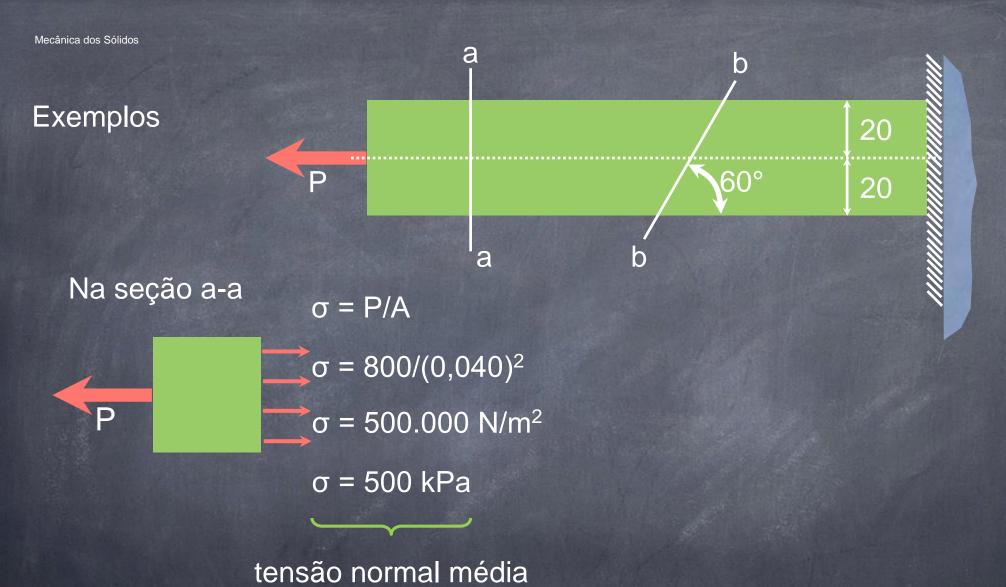
Na seção a-a

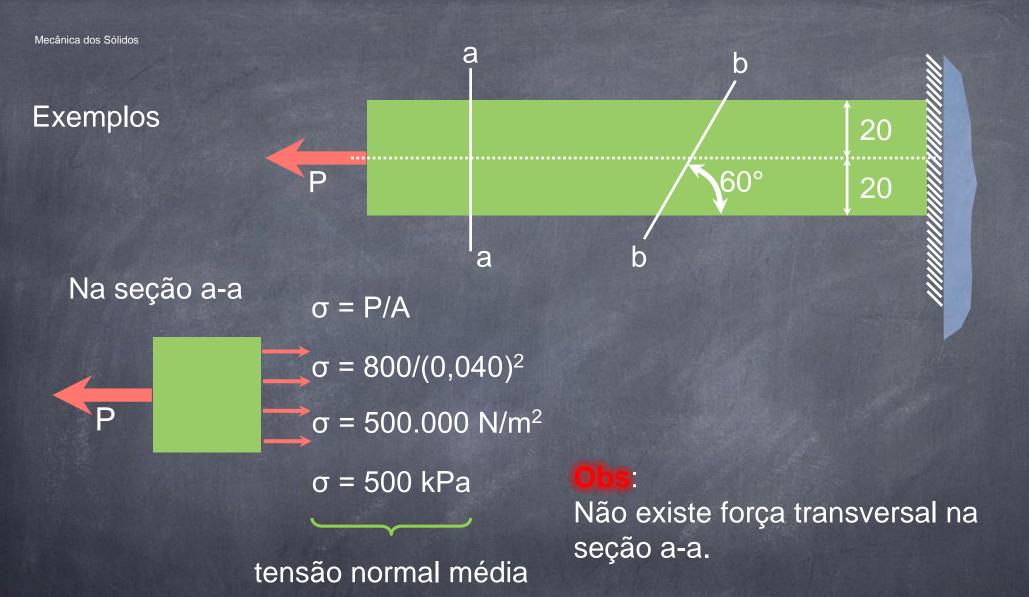


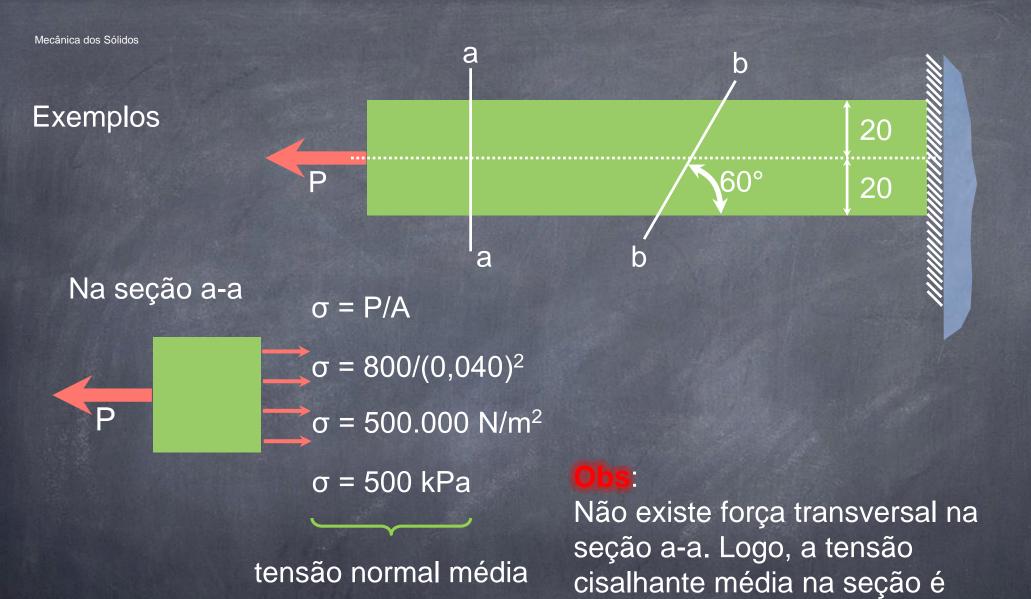




 $\sigma = 500 \text{ kPa}$



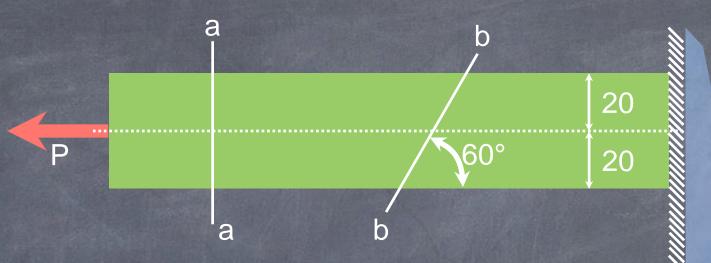




$$\tau = 0$$
.

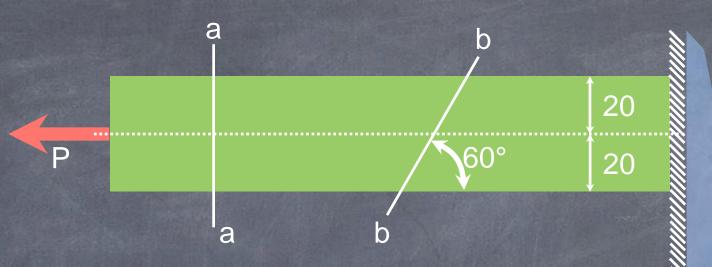
P sen 60°





$$V = P \cos 60^{\circ}$$



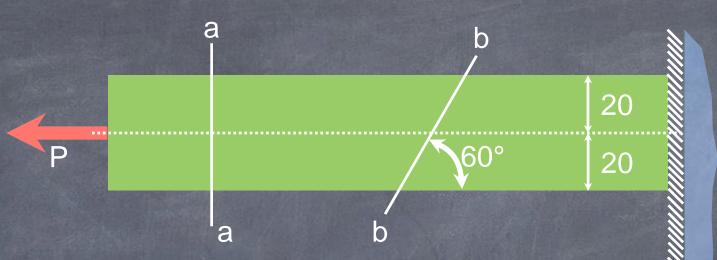


$$V = P \cos 60^{\circ}$$



$$N = P sen 60^{\circ}$$

$$\Sigma F_n = 0$$



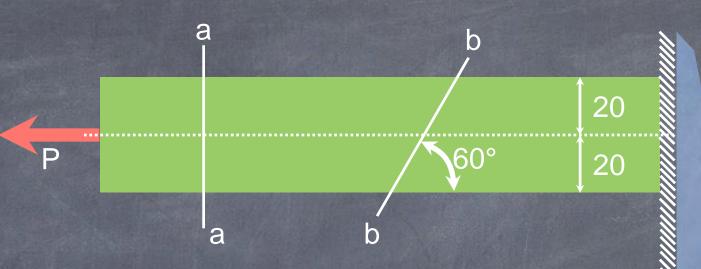
Na seção b-b

$$V = P \cos 60^{\circ}$$



$$\Sigma F_n = 0$$

N - P sen $60^{\circ} = 0$



Na seção b-b

$$V = P \cos 60^{\circ}$$

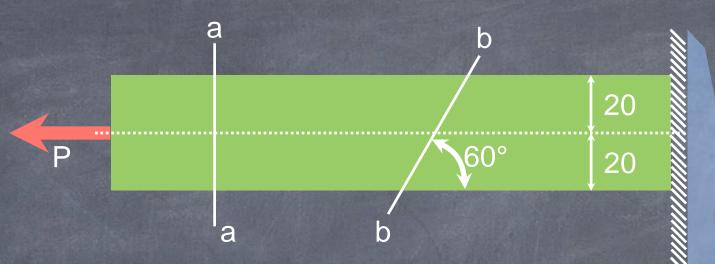


 $N = P sen 60^{\circ}$

$$\Sigma F_n = 0$$

N - P sen
$$60^{\circ} = 0$$

$$N = 692,8 N$$



Na seção b-b

$$V = P \cos 60^{\circ}$$



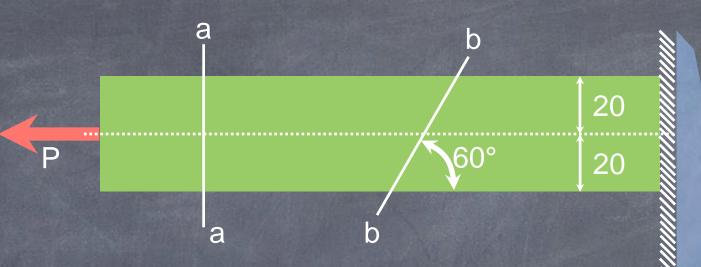
$$\Sigma F_n = 0$$

$$N = P sen 60^{\circ}$$

N - P sen $60^{\circ} = 0$

$$\Sigma F_t = 0$$

N = 692,8 N



Na seção b-b

$$V = P \cos 60^{\circ}$$



 $\Sigma F_n = 0$

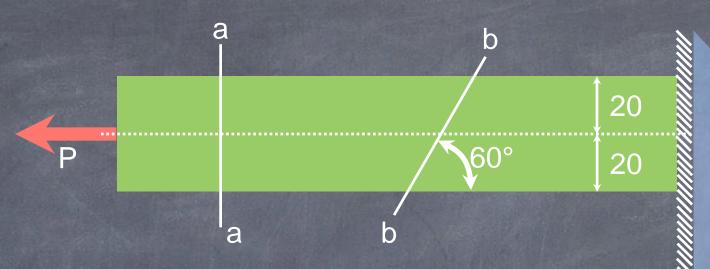
N - P sen $60^{\circ} = 0$

N = 692,8 N

$$N = P sen 60^{\circ}$$

$$\Sigma F_t = 0$$

$$V - P \cos 60^{\circ} = 0$$



$$V = P \cos 60^{\circ}$$



$$\Sigma F_n = 0$$

N - P sen
$$60^{\circ} = 0$$

$$N = 692,8 N$$

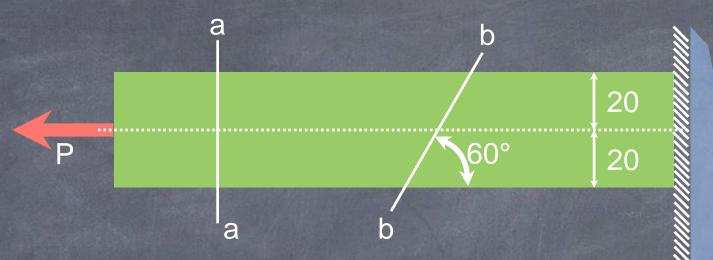
$$N = P sen 60^{\circ}$$

$$\Sigma F_t = 0$$

$$V - P \cos 60^{\circ} = 0$$

$$V = 400,0 N$$





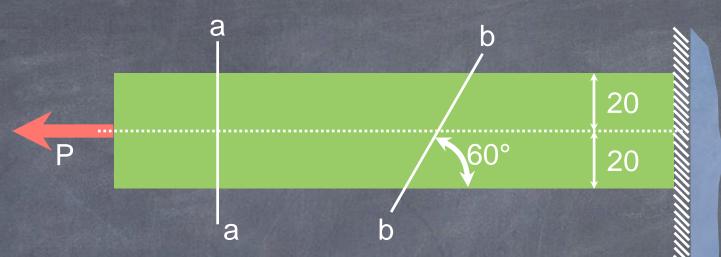
$$V = P \cos 60^{\circ}$$



tensão normal média

 $N = P sen 60^{\circ}$





Na seção b-b

$$V = P \cos 60^{\circ}$$

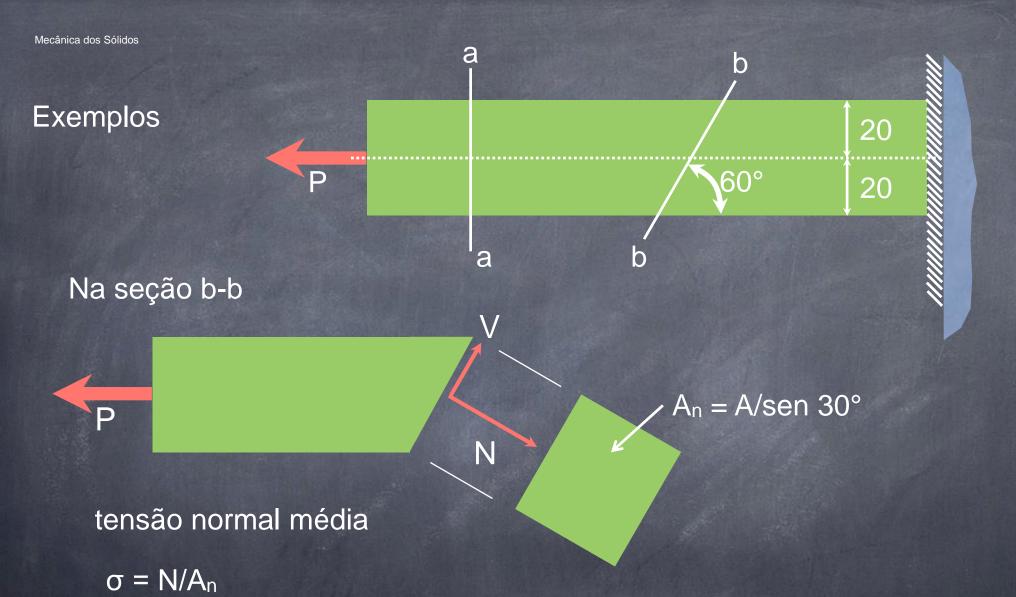
P

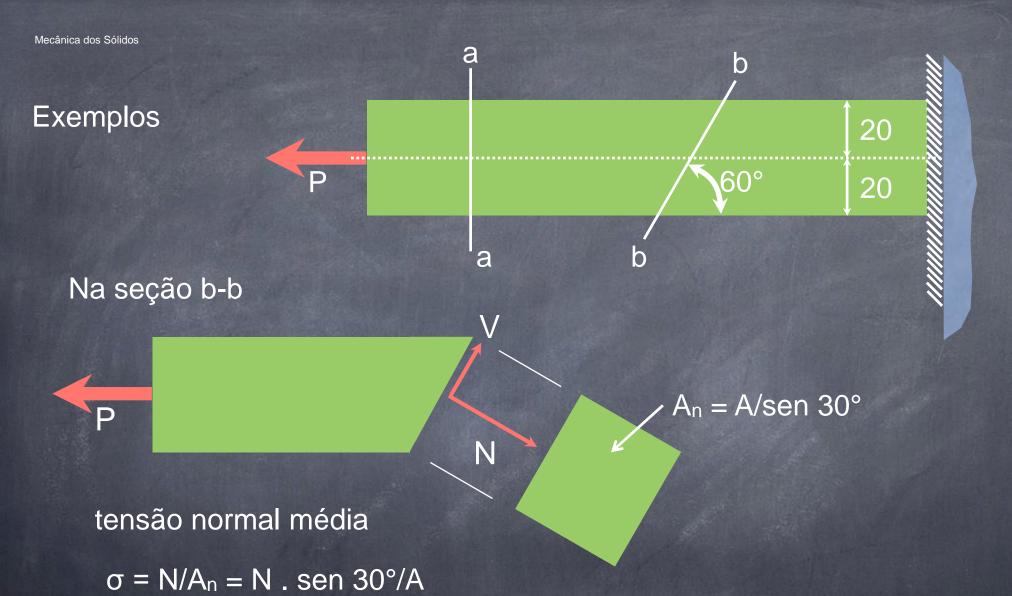
tensão normal média

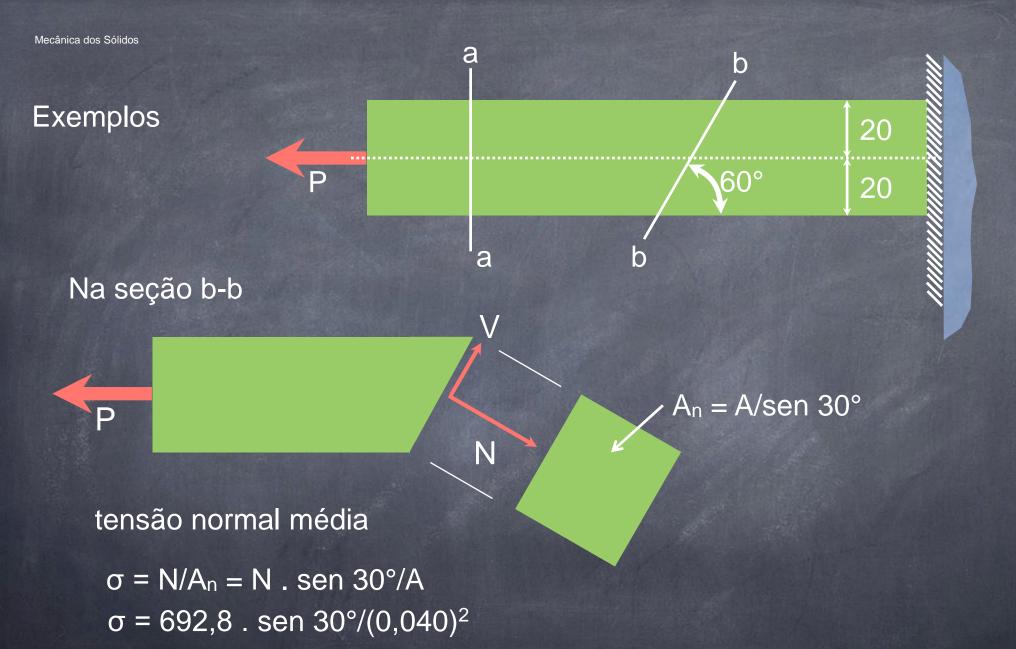
$$\sigma = N/A_n$$

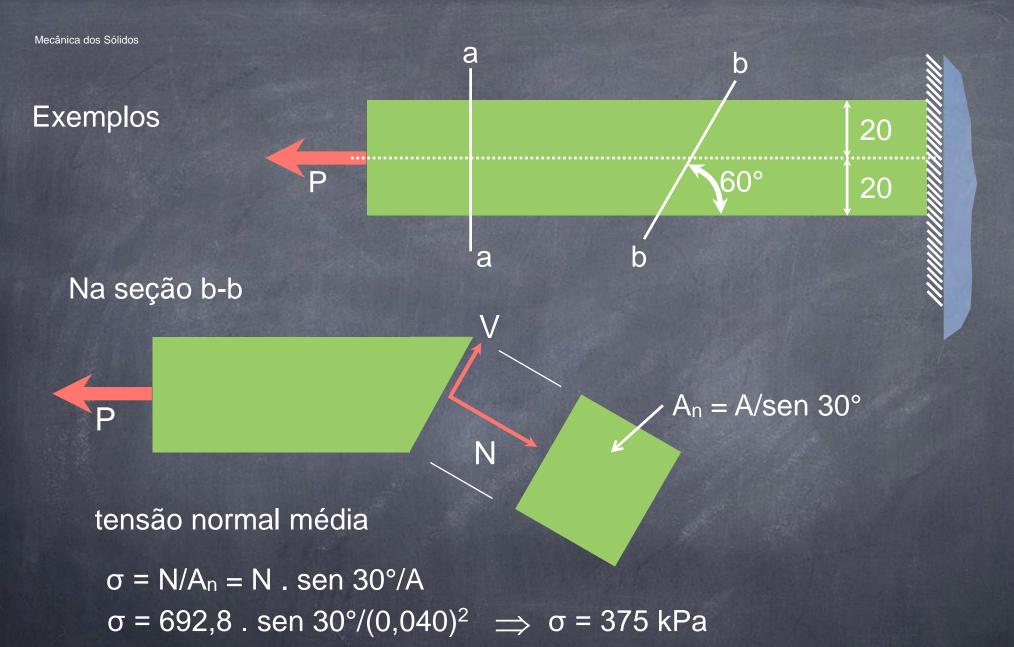
tensão normal média

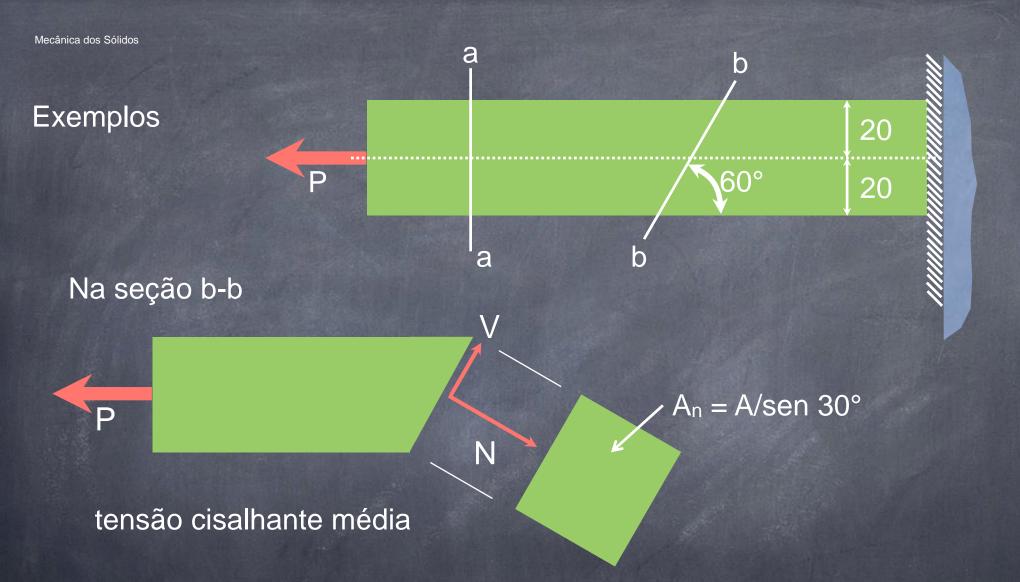
$$\sigma = N/A_n$$











tensão cisalhante média

$$\tau = V/A_n$$

tensão cisalhante média

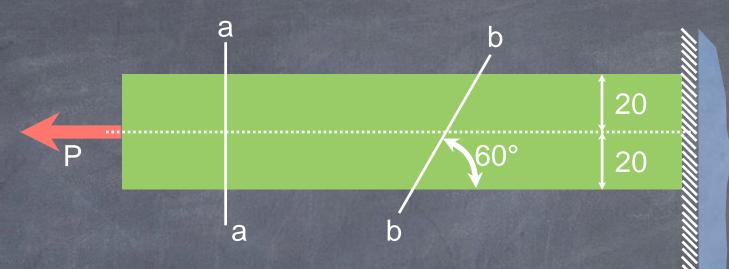
$$\tau = V/A_n = V \cdot sen 30^{\circ}/A$$

tensão cisalhante média

$$\tau = V/A_n = V \cdot sen 30^{\circ}/A$$

$$\tau = 400 \text{ . sen } 30^{\circ}/(0,040)^{2}$$





Na seção b-b

P

tensão cisalhante média

$$\tau = V/A_n = V$$
 . sen 30°/A

$$\tau = 400 \text{ . sen } 30^{\circ}/(0,040)^{2} \implies \tau = 217 \text{ kPa}$$

$$A_n = A/sen 30^\circ$$

$$\Rightarrow \tau = 217 \text{ kPa}$$

N

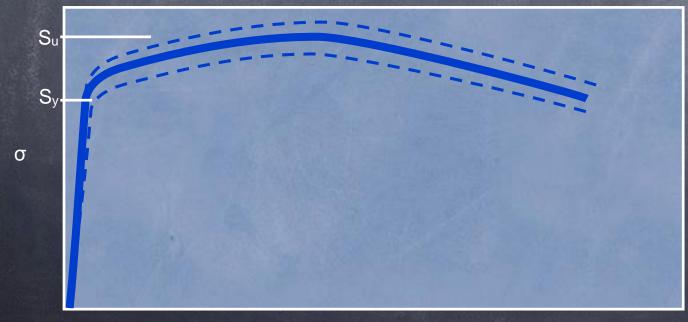
Segurança no dimensionamento de peças e componentes exige uma garantia mínima de que não ocorrerá falha (σ ≤ tensão limite);

Segurança no dimensionamento de peças e componentes exige uma garantia mínima de que não ocorrerá falha (σ ≤ tensão limite);

Impossível assegurar que os materiais atendam as mesmas propriedades;

Segurança no dimensionamento de peças e componentes exige uma garantia mínima de que não ocorrerá falha (σ ≤ tensão limite);

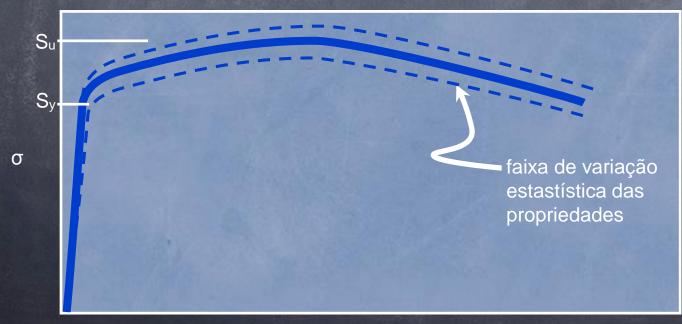
Impossível assegurar que os materiais atendem as mesmas propriedades;



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Segurança no dimensionamento de peças e componentes exige uma garantia mínima de que não ocorrerá falha (σ ≤ tensão limite);

Impossível assegurar que os materiais atendem as mesmas propriedades;



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Segurança no dimensionamento de peças e componentes exige uma garantia mínima de que não ocorrerá falha (σ ≤ tensão limite);

Impossível assegurar que os materiais atendem as mesmas propriedades;

Difícil prever a aplicação de cargas excessivas, ou uso inapropriado do componente;

Segurança no dimensionamento de peças e componentes exige uma garantia mínima de que não ocorrerá falha (σ≤S_y, S_u);

Impossível assegurar que os materiais atendem as mesmas propriedades;

Difícil prever a aplicação de cargas excessivas, ou uso inapropriado do componente;

Uso de um fator de segurança nas propriedades.

Fator de segurança

Fator de segurança

tensão normal

- no escoamento:
$$FS = \frac{S_y}{\sigma_{adm}}$$

Fator de segurança

tensão normal tensão cisalhante

- no escoamento:

$$FS = \frac{S_y}{\sigma_{adm}}$$

$$FS = \frac{S_{sy}}{\tau_{adm}}$$

$$FS = \underbrace{S_u}_{\sigma_{adm}}$$

$$FS = \frac{S_{su}}{\tau_{adm}}$$

Fator de segurança

tensão normal tensão cisalhante

- no escoamento:

$$FS = \frac{S_y}{\sigma_{adm}}$$

$$FS = \frac{S_{sy}}{\tau_{adm}}$$
 >

$$FS = \frac{S_u}{\sigma_{adm}}$$

$$FS = \frac{S_{su}}{\tau_{adm}} > 1$$

Fator de segurança

tensão normal

tensão cisalhante

- no escoamento:

$$FS = \frac{S_y}{\sigma_{adm}}$$

$$FS = \frac{S_{sy}}{\tau_{adm}}$$

> 1 padronizado por norma técnica

- na tração:

$$FS = \frac{S_u}{\sigma_{adm}}$$

$$FS = \frac{S_{su}}{\tau_{adm}}$$

> 1 padronizado por norma técnica

Fim do Cap. 1