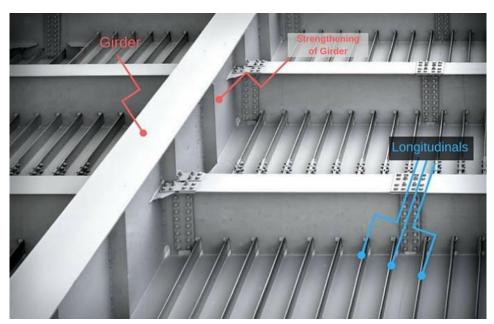
DEPARTAMENTO DE ENGEHARIA NAVAL E OCEÂNICA ESCOLA POLITÉCNICA DA USP

Análise de Vigas : δ (mm)

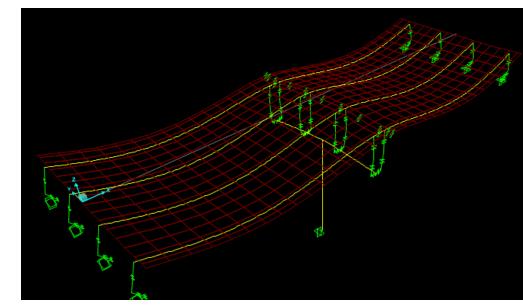


PNV 3212 – Mecânica Dos Sólidos I 2020

Deflection of beams

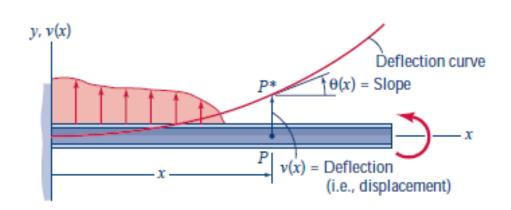


$$\delta \ll t$$



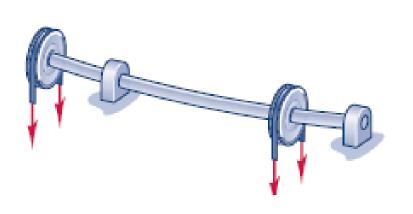
Deflection of beams

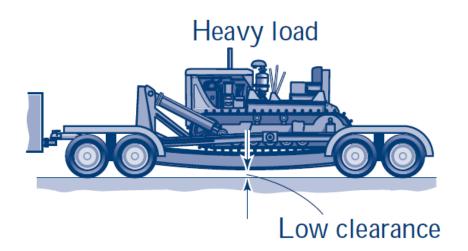
Deslocamento transversal (vertical)



$$\delta \ll t$$

$$\delta(x) \equiv v(x)$$





Hipóteses

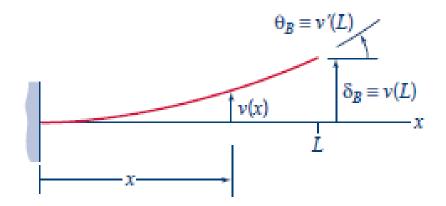
- Problema é independente do tempo.
- O formato da viga é um <u>prisma</u> reto, cujo comprimento é muito maior que as outras dimensões (Esbelta).
- A viga é constituída de um material linearmente elástico.
- O <u>efeito Poisson</u> é negligenciável.
- A seção transversal é <u>simétrica</u> em relação ao plano vertical.
- Planos perpendiculares à linha neutra permanecem quase planos e perpendiculares ao eixo deformado depois da deformação (Navier).
- O ângulo de rotação da seção transversal é muito pequeno.
- O efeitos de momento de inércia da rotação é desprezado.
- A viga é constituída de material homogêneo.
- The distribution of flexural stress on a given cross section is not affected by the deformation due to shear.
- Distorção da seção transversal é pequena o suficiente para ser desprezada!

5/14/2020

Caminho

- 1. Relação Momento- curvatura
- 2. Equação diferencial relacionando v(x) M(x)
- 3. Condições de contorno

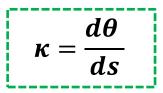
Fórmula

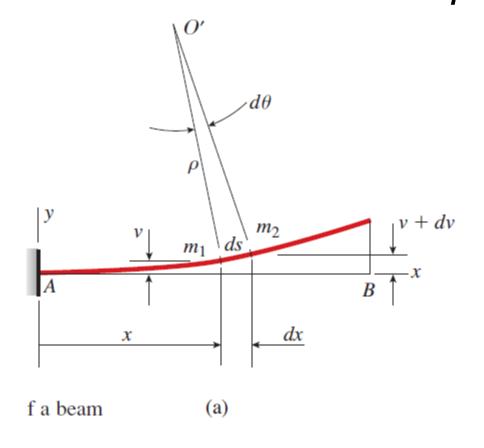


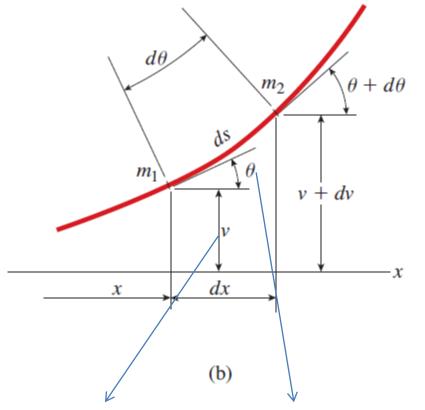
$$EI \frac{d^2v(x)}{dx^2} = M(x)$$

Curvatura

$$\kappa(x) = \frac{1}{\rho(x)}$$
$$ds = \rho d\theta$$



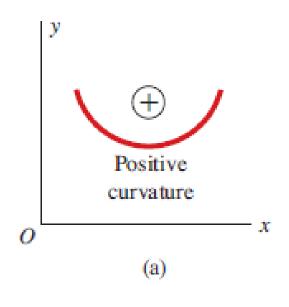




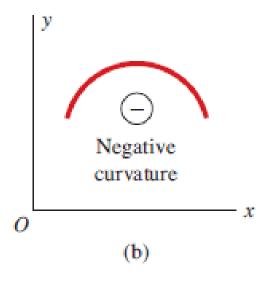
Flexão de uma viga -> deflexão vertical + rotação

Curvatura

$$\kappa(x) = \frac{1}{\rho(x)}$$



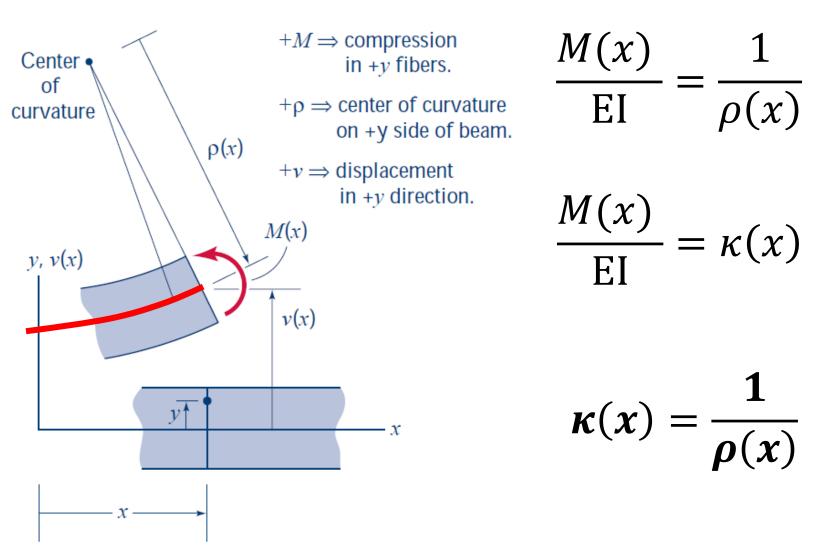
$$\kappa = \frac{d\theta}{ds}$$



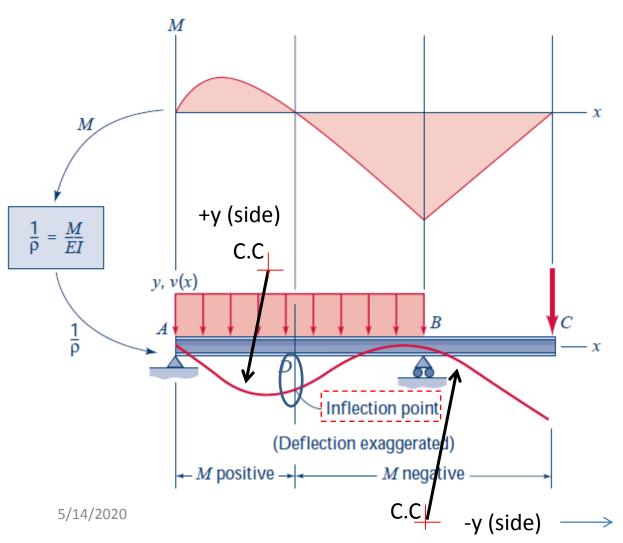
M+

M-

Momento-curvatura



Momento-curvatura

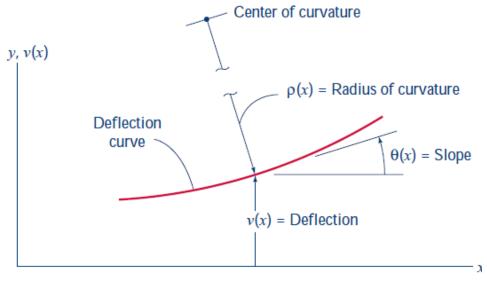


$$\frac{M(x)}{\text{EI}} = \frac{1}{\rho(x)}$$

$$\kappa(x) = \frac{1}{\rho(x)}$$

Inclinação θ

$$\kappa(x) = \frac{1}{\rho(x)}$$



$$\frac{dv(x)}{dx} = \tan \theta$$

Buildings, automobiles, aircraft, and ships, undergo relatively small changes in shape while in service

Pequenas deflexões

very small angles of rotation, very small deflections, and very small curvatures.

$$\frac{\delta}{dx}$$

5/14/2020

$$\frac{dv(x)}{dx} \cong \theta$$

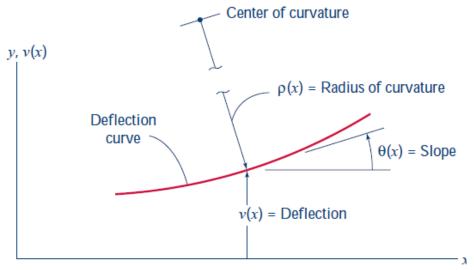
$$\frac{dv}{ds} = \sin\theta$$

$$\frac{dx}{ds} = \cos\theta$$

$$\frac{dv(x)}{dx} \ll 1$$

 $\kappa(x) = \frac{1}{\rho(x)}$

• Inclinação θ



very small angles of rotation, very small deflections, and very small curvatures.

$$\theta < 15^{\circ}$$

θ°	θ [rad]	tan θ	$\cos \theta$
5	0.087	0.087	0.996
10	0.175	0.176	0.985
15	0.262	0.268	0.966

$$\frac{M(x)}{EI} = \frac{d\theta}{dx}$$

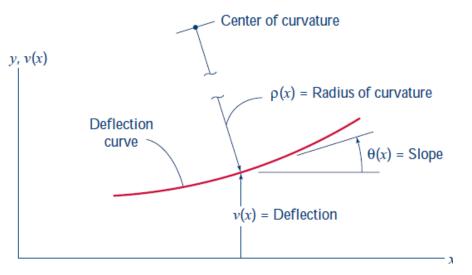
$$\kappa = \frac{d\theta}{dx}$$

$$\frac{dx}{ds} = \cos \theta$$

$$dx \approx ds$$

 $\kappa(x) = \frac{1}{\rho(x)}$

• Inclinação θ



very small angles of rotation, very small deflections, and very small curvatures.

$$\frac{M(x)}{EI} = \frac{d\theta}{dx}$$

Moment-deflection equation

$$\frac{dv}{dx} \approx \theta \longrightarrow \frac{d^2v}{dx^2} \approx \frac{d\theta}{dx}$$

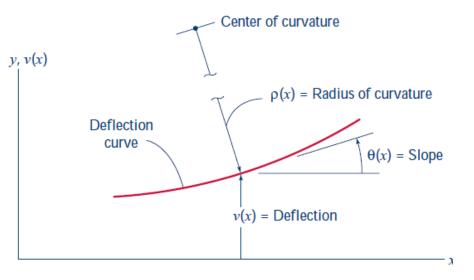
$$\frac{M(x)}{EI} = \frac{d^2v(x)}{dx^2}$$

$$\frac{dV}{dx} = -q(x)$$

$$\frac{dM}{dx} = -V(x)$$

 $\kappa(x) = \frac{1}{\rho(x)}$

• Inclinação θ



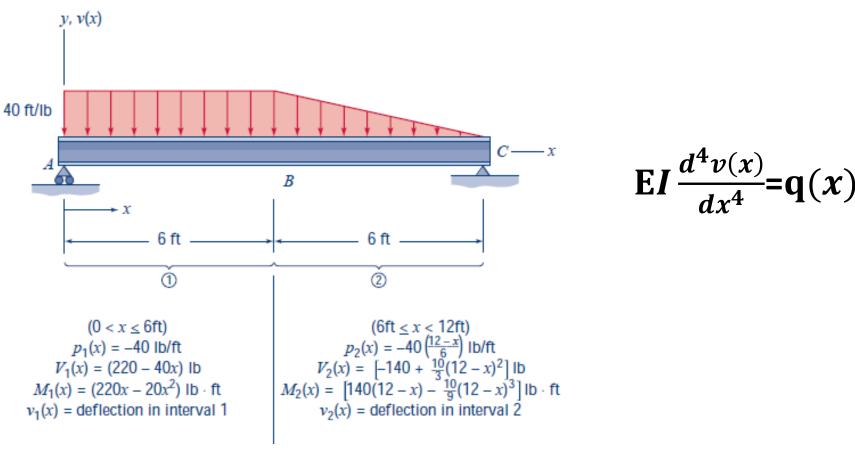
very small angles of rotation, very small deflections, and very small curvatures.

Load-deflection equation

$$\mathbf{E}I \frac{d^{2}v(x)}{dx^{2}} = M(x) \longrightarrow \mathbf{E}I \frac{d^{3}v(x)}{dx^{3}} = V(x) \longrightarrow \mathbf{E}I \frac{d^{4}v(x)}{dx^{4}} = \mathbf{q}(x)$$

$$\frac{dM}{dx} = -V(x)$$

$$\frac{dV}{dx} = -q(x)$$



Boundary Conditions and Continuity Conditions

$$v_1(0) = v_2(12) = 0$$

$$v_1(6) = v_2(6)$$

$$\theta_1(6) = \theta_2(6)$$

Boundary Conditions and Continuity Conditions

TAI	TABLE 7.1 Boundary Conditions							
	Туре	Symbol*	2nd Order	4th Order				
	Fixed end		$ \begin{aligned} v &= 0 \\ v' &= 0 \end{aligned} $	$ \begin{aligned} \mathbf{v} &= 0 \\ \mathbf{v}' &= 0 \end{aligned} $				
	Simple support		v = 0	v = 0 $M = 0$				
ВС	Free end		No BC	V = 0 $M = 0$				
	Concentrated force	P ₀	No BC	$V = P_0$ $M = 0$				
	Concentrated couple	$\bigcap^{M_0} \square$	No BC	$V = 0$ $M = -M_0$				
	*These boundary conditions also apply if the boundary under consideration the other end of the beam (i.e., $x = L$).							

$$\mathbf{E}I\frac{d^4v(x)}{dx^4}=\mathbf{q}(x)$$

5/15/2020

Boundary Conditions and Continuity Conditions

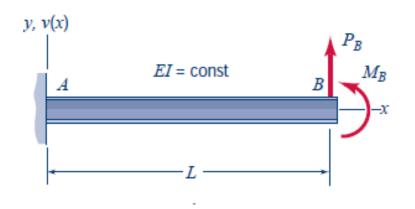
TABLE 7.2 Continuity Conditions*

	Туре	Symbol	2nd Order	4th Order
CC	Roller	① → ②	$v_1 = v_2 = 0$ $v_1' = v_2'$	$ v_1 = v_2 = 0 v'_1 = v'_2 M_1 = M_2 $
	Discontinuity in load function	<u>+11111</u>	$v_1 = v_2$ $v'_1 = v'_2$	$egin{aligned} v_1 &= v_2 \ v_1' &= v_2' \ V_1 &= V_2 \ M_1 &= M_2 \end{aligned}$
	Concentrated force	P ₀	$v_1 = v_2 v_1' = v_2'$	$v_1 = v_2, v'_1 = v'_2$ $V_2 - V_1 = P_0$ $M_1 = M_2$
	Concentrated couple	$\stackrel{M_0}{\longmapsto}$	$v_1 = v_2 \\ v_1' = v_2'$	$v_1 = v_2, v'_1 - v'_2$ $V_1 = V_2$ $M_2 - M_1 = -M_0$
	Pin, with force	$\stackrel{P_0}{\longleftarrow}$	$v_1 = v_2$	$v_1 = v_2$ $V_2 - V_1 = P_0$ $M_1 = M_2 = 0$

^{*}The displacement (v) and slope (v') continuity conditions that are listed in Table 7.2 are obtained by inspection, that is, by simply looking at the figures in the "Symbol" column. The continuity conditions on shear force (V) and bending moment (M) are obtained by taking a local free-body diagram of the "joint" that is common to beam segments (1) and (2).

$$EI\frac{d^4v(x)}{dx^4}=q(x)$$

Exemplo 1



$$\frac{M(x)}{EI} = \frac{d^2v(x)}{dx^2}$$