

Circuit Theory and Electronics Fundamentals

Lecture 14: Diode circuits

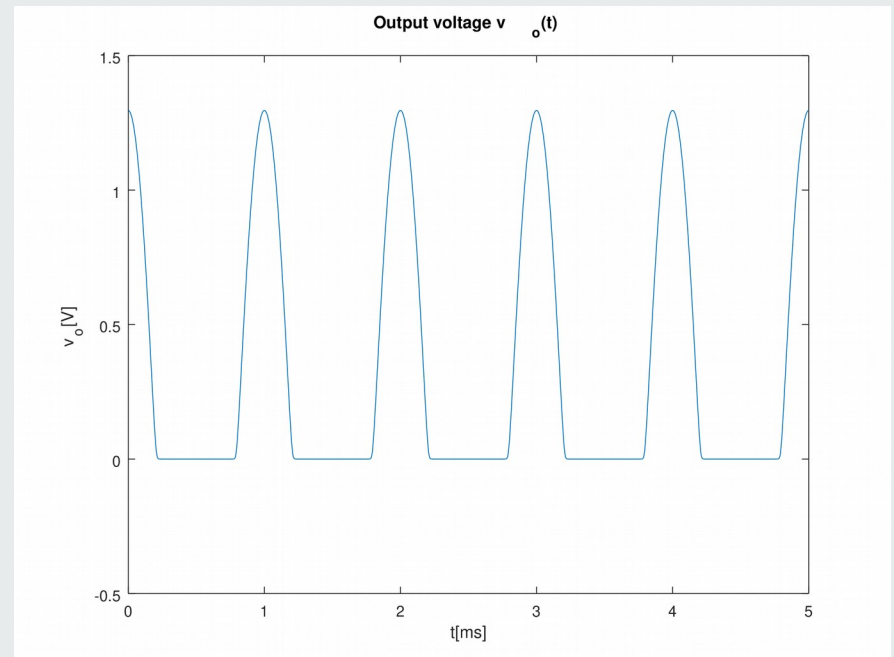
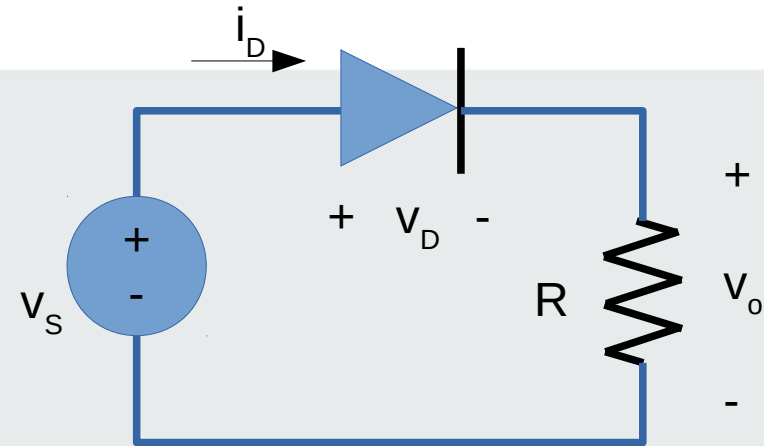
- **AC/DC converter**
 - Half-wave rectifier circuit revisited
 - Full-wave rectifier circuit
 - Limiter circuit
 - Envelope detector circuit
 - Voltage regulator circuit

Half-wave rectifier revisited

$$v_s(t) = A \cos(\omega t)$$

$$v_o = \begin{cases} v_s - v_D, & D_{ON} \\ 0, & D_{OFF} \end{cases}$$

$$i_D = \begin{cases} \frac{v_o}{R}, & D_{ON} \\ 0, & D_{OFF} \end{cases}$$



Octave script l11.m solves 1 non-linear equation for v , for each time instant t

HALF WAVE RECTIFIER CIRCUIT

Full-wave bridge rectifier circuit

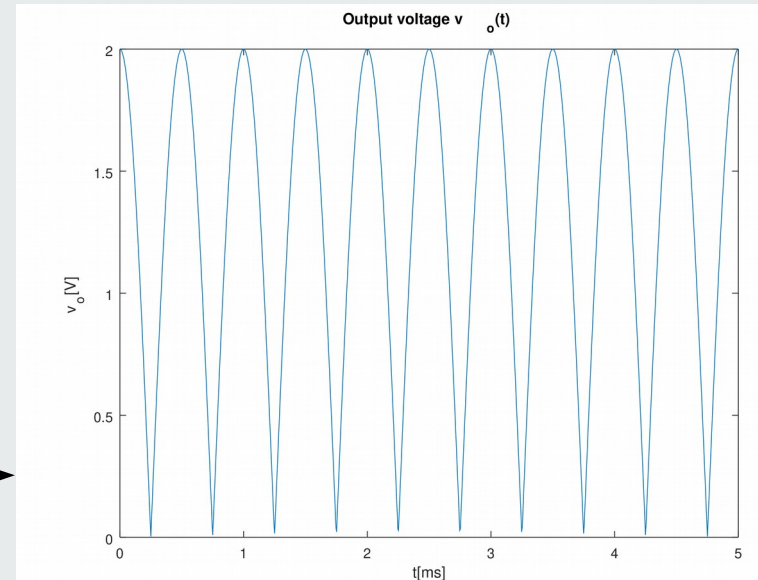
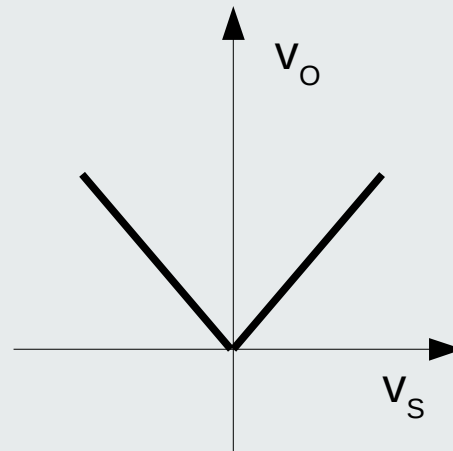
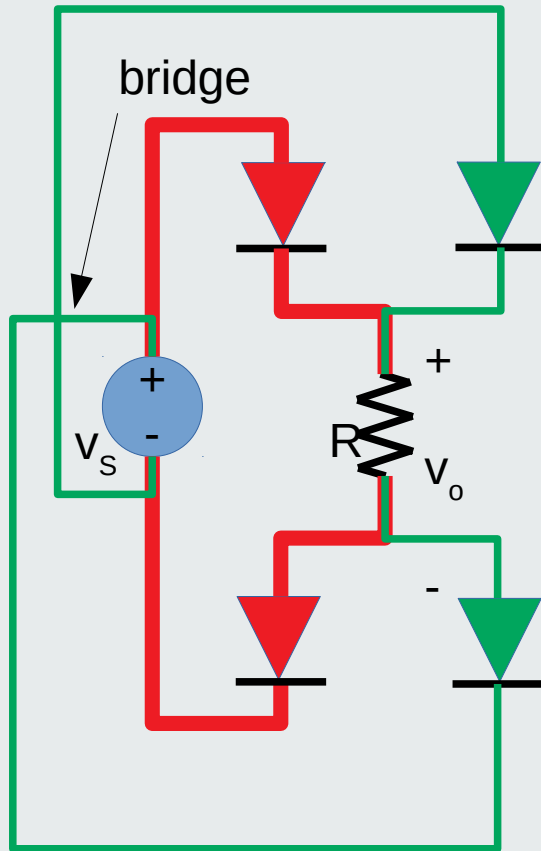
Assume ideal diodes

$$i_D = \begin{cases} 0, & v_D < 0 \\ \text{positive}, & v_D = 0 \end{cases}$$

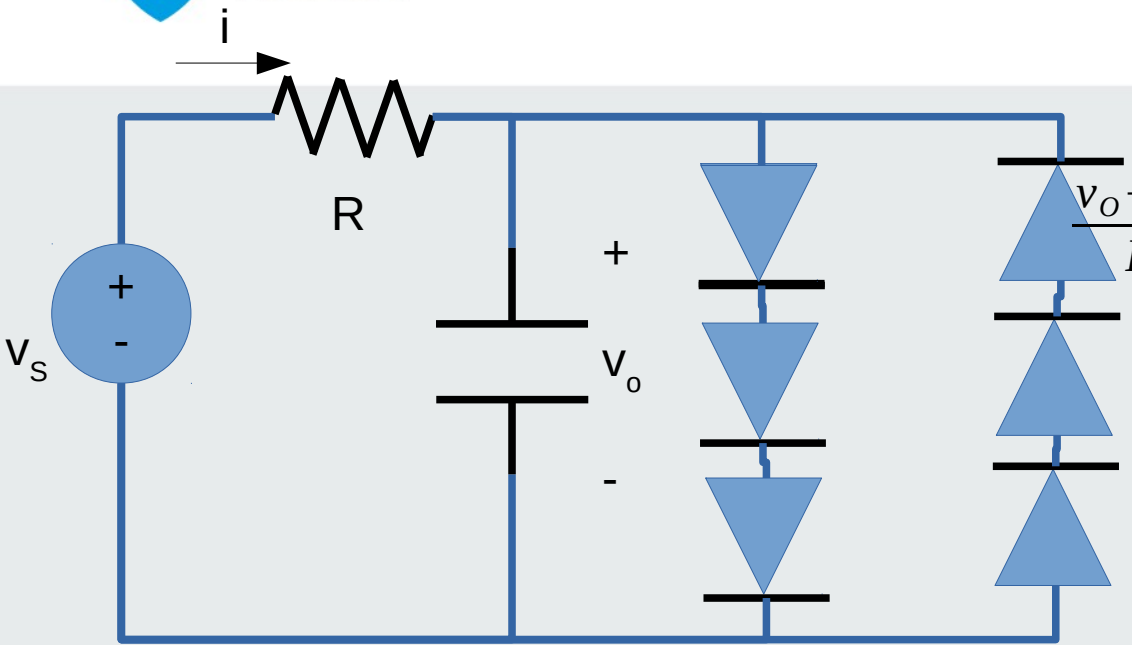
$$v_O = \begin{cases} v_S, & v_S \geq 0 \\ -v_S, & v_S < 0 \end{cases}$$

$$v_O = |v_S|$$

Full-wave rectifier computes absolute value



Limiter circuit



KCL:

$$\frac{v_o - v_s}{R} + C \frac{dv_o}{dt} + I_s (e^{\frac{v_o}{3\eta V_T}} - 1) + I_s (e^{\frac{-v_o}{3\eta V_T}}) = 0$$

Non-linear differential equation!!

Out of the scope of this course.

Using (V_{ON}) diode model

1st order low pass filter

Using the forced solution only:

$$\tilde{V}_{LPF} = \frac{1}{1 + j\omega RC} \tilde{V}_s$$

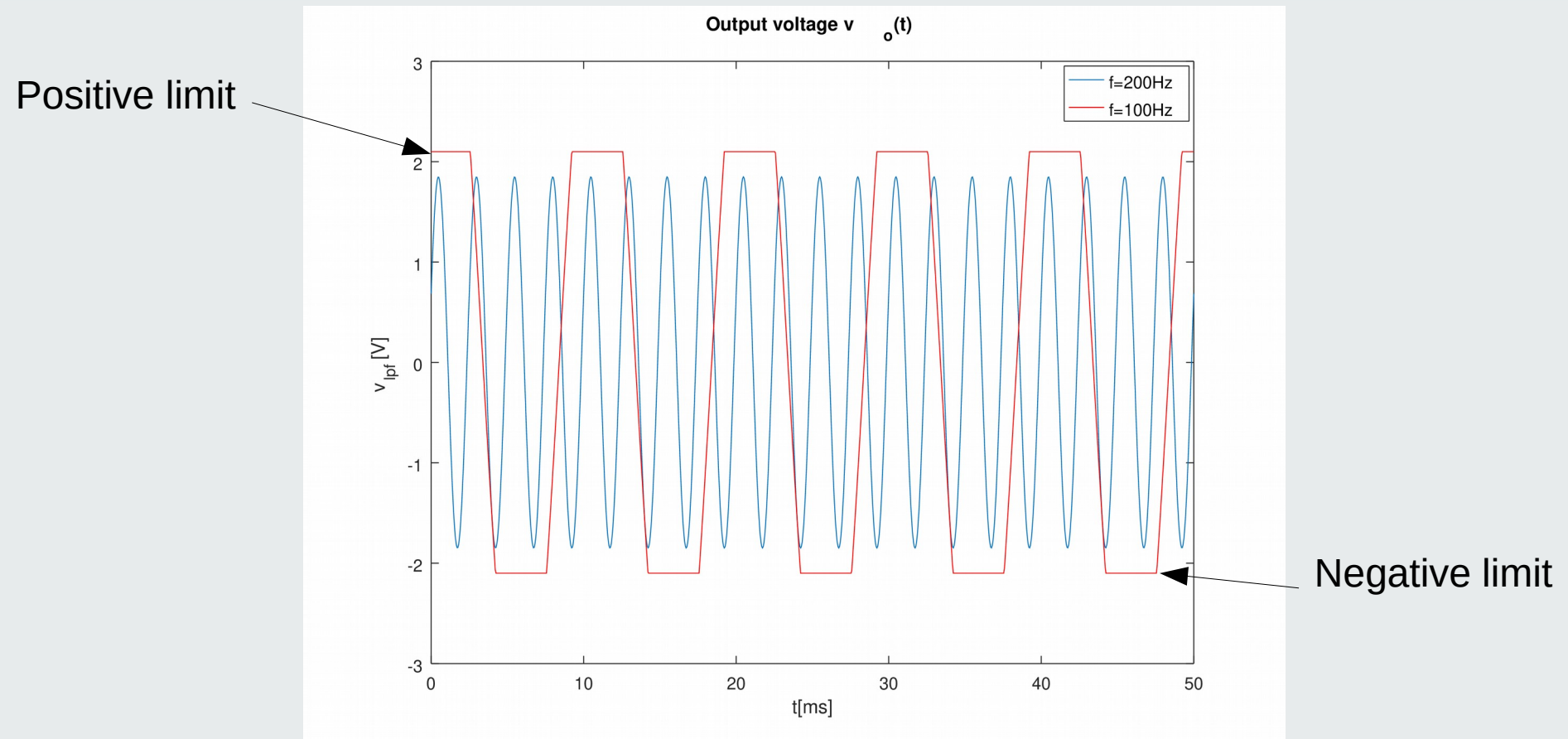
$$v_{LPF}(t) = \left| \frac{\tilde{V}_s}{1 + j\omega RC} \right| \cos(\omega t - \arctan(\omega RC))$$

$$v_o(t) = \begin{cases} -3V_{ON}, & V_{LPF} \leq -3V_{ON} \\ v_{LPF}(t), & -3V_{ON} \leq V_{LPF} \leq 3V_{ON} \\ 3V_{ON}, & V_{LPF} \geq 3V_{ON} \end{cases}$$

Positive voltage limiter
 $v_o(t) \leq 3V_{ON}$

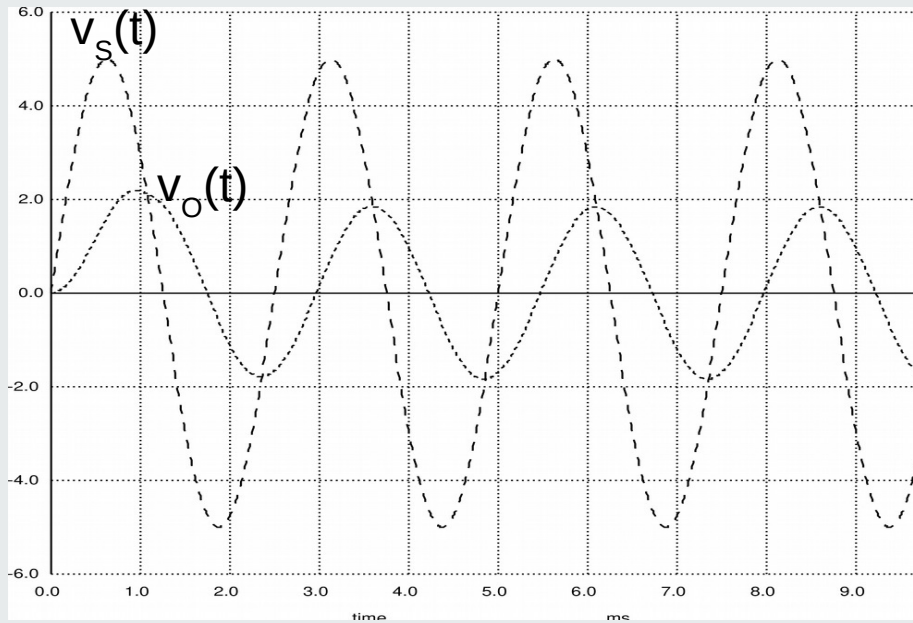
Negative voltage limiter
 $v_o(t) \geq -3V_{ON}$

Limiter circuit approximate analytical solution

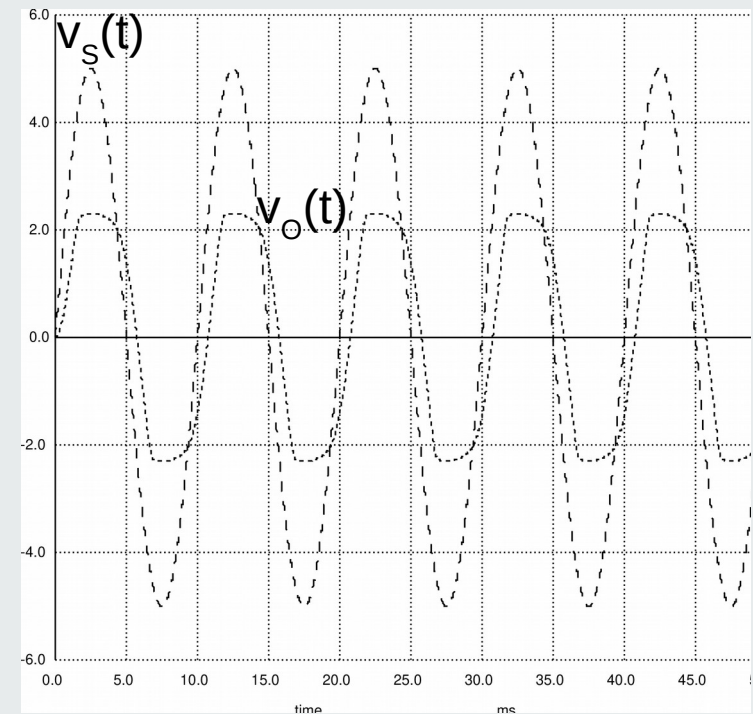


Approximate Octave solution using (V_{ON}) diode model (see I14.m)

Limiter circuit simulation solution



$f=400\text{Hz}$



$f=100\text{Hz}$

Ngspice solution using the default diode model (see l14.net)



Ngspice's Diode Model

SPICE Diode Model Parameters

	name	parameter	units	default	example	area
1	IS	saturation current	A	1.0e-14	1.0e-14	*
2	RS	ohmic resistanc	Ohm	0	10	*
3	N	emission coefficient	-	1	1.0	
4	TT	transit-time	sec	0	0.1ns	
5	CJO	zero-bias junction capacitance	F	0	2pF	*
6	VJ	junction potential	V	1	0.6	
7	M	grading coefficient	-	0.5	0.5	
8	EG	band-gap energy	eV	1.11	1.11 Si	
9	XTI	saturation-current temp.exp	-	3.0	3.0 pn 2.0 Schottky	
10	KF	flicker noise coefficient	-	0		
11	AF	flicker noise exponent	-	1		
12	FC	coefficient for forward-bias depletion capacitance formula	-	0.5		
13	BV	reverse breakdown voltage	V	infinite	40.0	
14	IBV	current at breakdown voltage	V	1.0e-3		
15	TNOM	parameter measurement temperature	deg C	27	50	

Ngspice uses a complex 15-parameter diode model

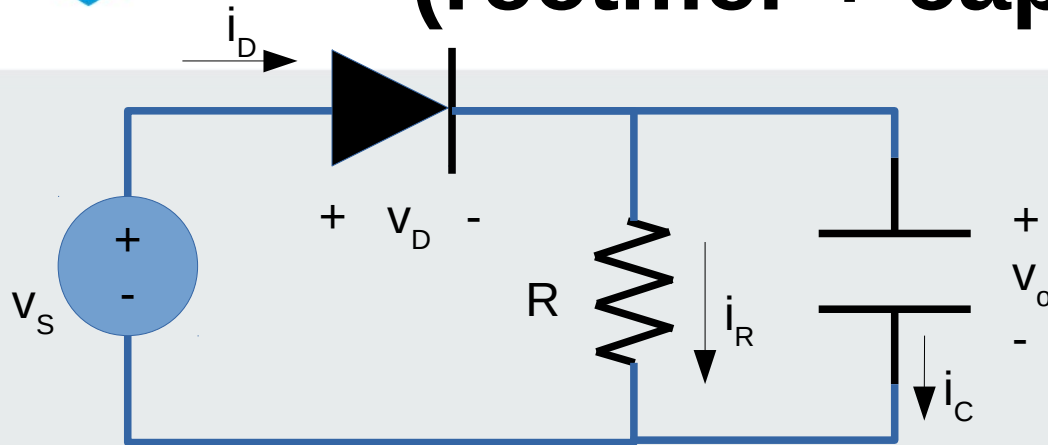
In this course we use the Default parameters

Users can override these parameters. For example:

```
.MODEL Dmine D (IS=76.9n)
```

Creates model Dmine and overrides parameter IS

Envelope detector circuit (rectifier + capacitor)



Using ideal diode model

At $t=0$ D is ON

$$v_o(t) = v_s(t)$$

$$i_R = \frac{v_s}{R}$$

$$i_C = C \frac{dv_s}{dt} = -C A \omega \sin(\omega t)$$

$$i_D = i_R + i_C \quad (\text{KCL})$$

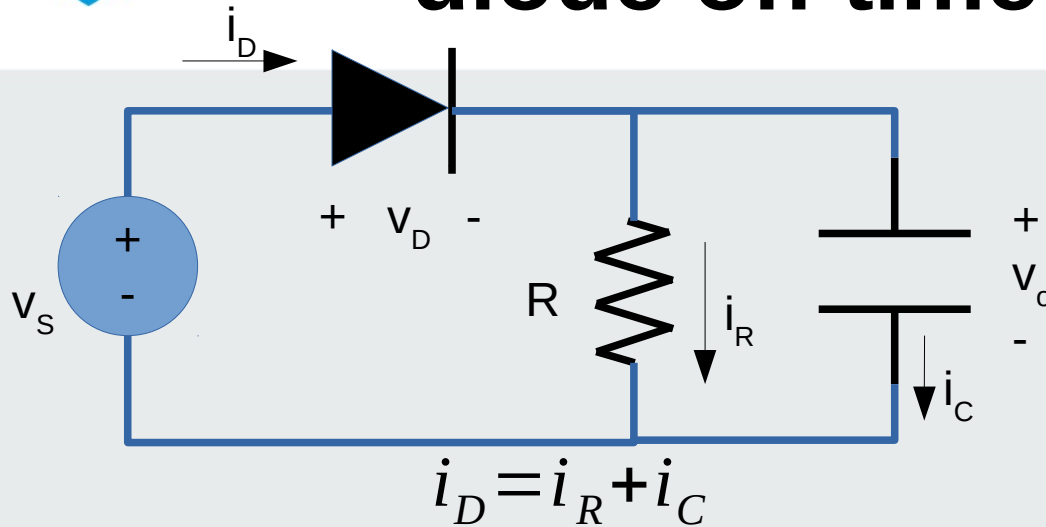
$$v_s(t) = A \cos(\omega t)$$

$$v_o = \begin{cases} v_s, & D_{ON} \\ -R i_C, & D_{OFF} \end{cases}$$

$$i_C = C \frac{dv_o}{dt}$$

i_C is negative and growing more negative with the time derivative of $v_o = v_s - V_{ON} \dots$

Envelope detector circuit: diode off time instant



i_C is negative and growing more negative with the time derivative of v_o ...

When $i_R = -i_C$, the diode current i_D becomes null
The diode goes OFF and $v_s < v_o$

C discharges through R

At $t = t_{OFF}$ D goes OFF

Compute t_{OFF} using ideal diode model:

$$i_R = -i_C$$

$$\frac{v_s}{R} = -C \frac{dv_s}{dt}$$

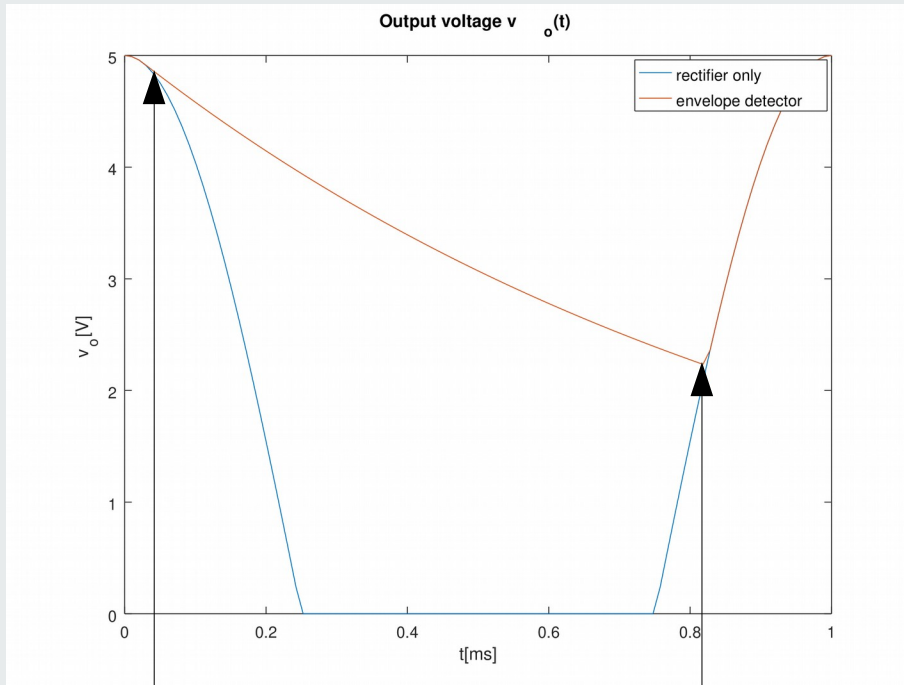
$$\frac{A}{R} \cos(\omega t_{OFF}) = C A \omega \sin(\omega t_{OFF})$$

$$t_{OFF} = \frac{1}{\omega} \operatorname{atan}\left(\frac{1}{\omega RC}\right)$$

$$t \geq t_{OFF} \Rightarrow$$

$$v_o(t) = A \cos(\omega t_{OFF}) e^{-\frac{t - t_{OFF}}{RC}}$$

Envelope detector plot



t_{OFF}

Diode goes OFF

t_{ON}

Diode goes ON

At $t=t_{ON}$ D goes ON

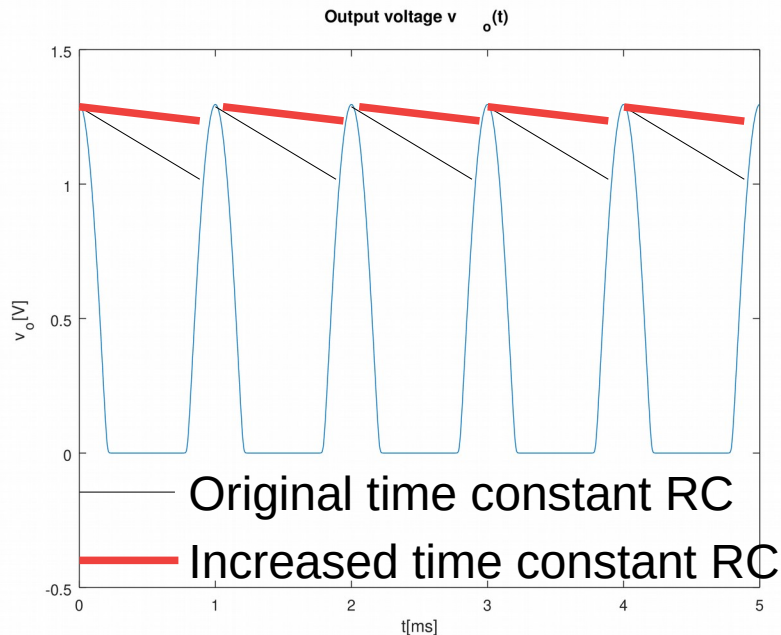
Compute t_{ON} using ideal diode model:

$$v_S(t_{ON}) = A \cos(\omega t_{OFF}) e^{-\frac{t_{ON} - t_{OFF}}{RC}}$$

$$A \cos(\omega t_{ON}) = A \cos(\omega t_{OFF}) e^{-\frac{t_{ON} - t_{OFF}}{RC}}$$

t_{ON} is given by solving the above non-linear equation approximately using Octave

Voltage ripple problem



Approximate voltage ripple
with half-wave rectifier circuit:

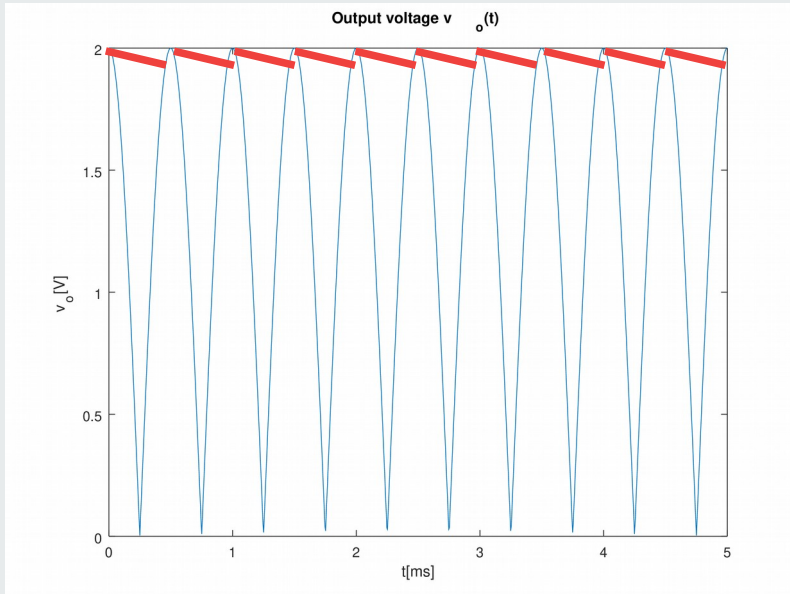
$$V_{\text{ripple}} = v_o(0) - v_o(T) = A \left(1 - e^{-\frac{T}{RC}} \right)$$

- Problem: v_o still shows oscillations at frequency f !
- A rippling power supply may affect application
 - Examples: audio or video applications
- AC/DC conversion imperfect
- Solution 1: increase time constant
 - Increase C, R or both
 - Disadvantage: larger C and R is expensive, especially in integrated circuits

• For small ripple:

$$t_{\text{OFF}} \approx 0 \text{ and } t_{\text{ON}} \approx T$$

Improving voltage ripple with full-wave rectifier circuit

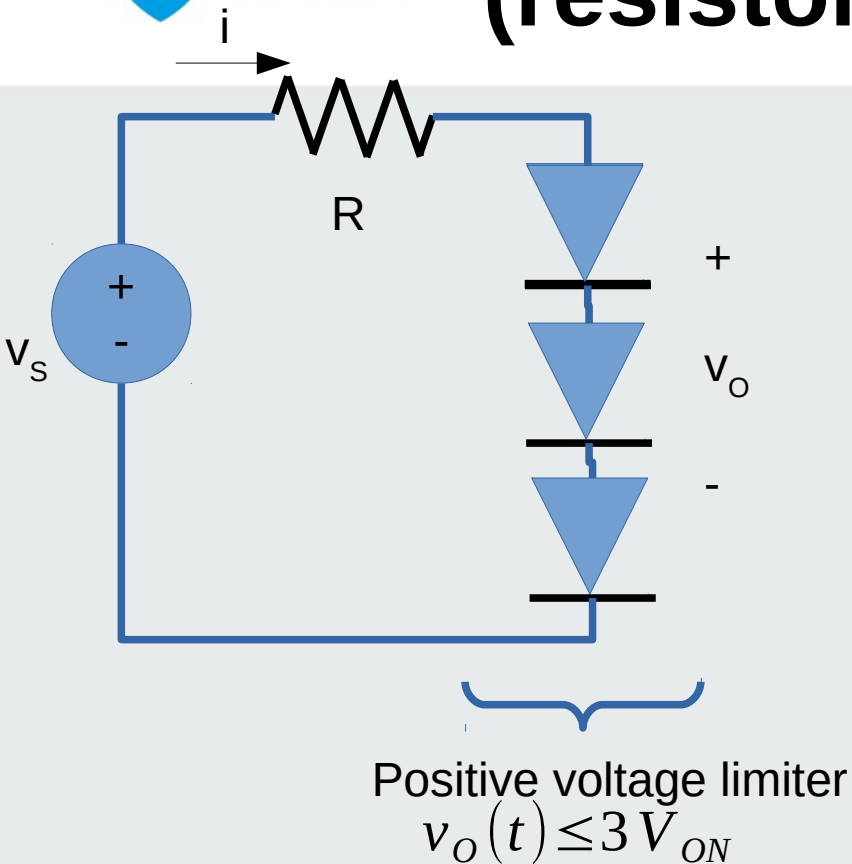


Approximate voltage ripple with full-wave rectifier circuit:

$$V_{\text{ripple}} = v_o(0) - v_o\left(\frac{T}{2}\right) = A \left(1 - e^{-\frac{T}{2RC}}\right)$$

- Solution 2: Use a full-wave rectifier
- v_o oscillates at frequency $2f$ with less amplitude
- Doubling the frequency and halving the amplitude may solve the problem in some applications
- Cheap solution for integrated circuits
 - Diodes and transistors can be very small and thus inexpensive

Voltage regulator circuit (resistor + limiter)



- The voltage regulator attenuates oscillations in the input signal without frequency dependence (unlike filters)
- Takes advantage of the non-linear diode characteristic

Separate DC and incremental components:

$$v_s = V_s + v_s, \quad V_s > 3V_{ON}$$

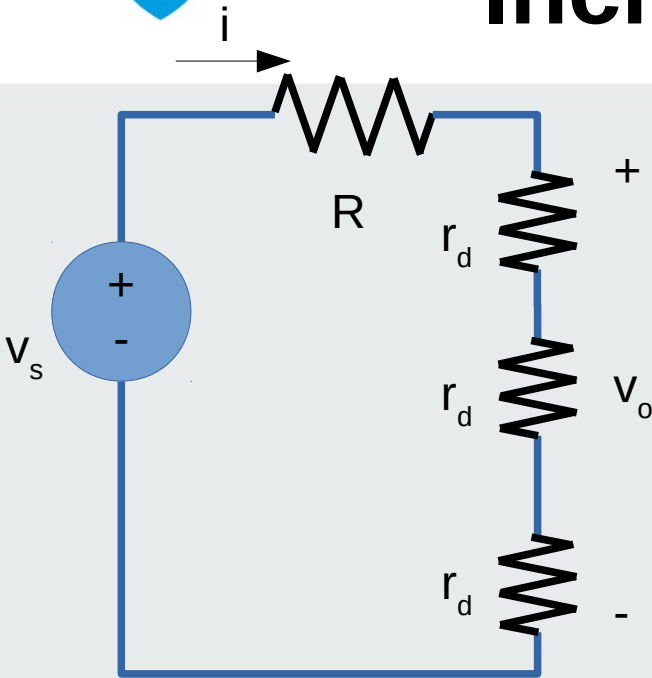
Ensures forward bias

$$v_o = V_o + v_o$$

$$V_o = 3V_{ON}$$

Show that: $\Delta v_o \ll \Delta v_s$

Voltage regulator circuit – Incremental analysis



$$v_o = \frac{3r_d}{3r_d + R} v_s$$

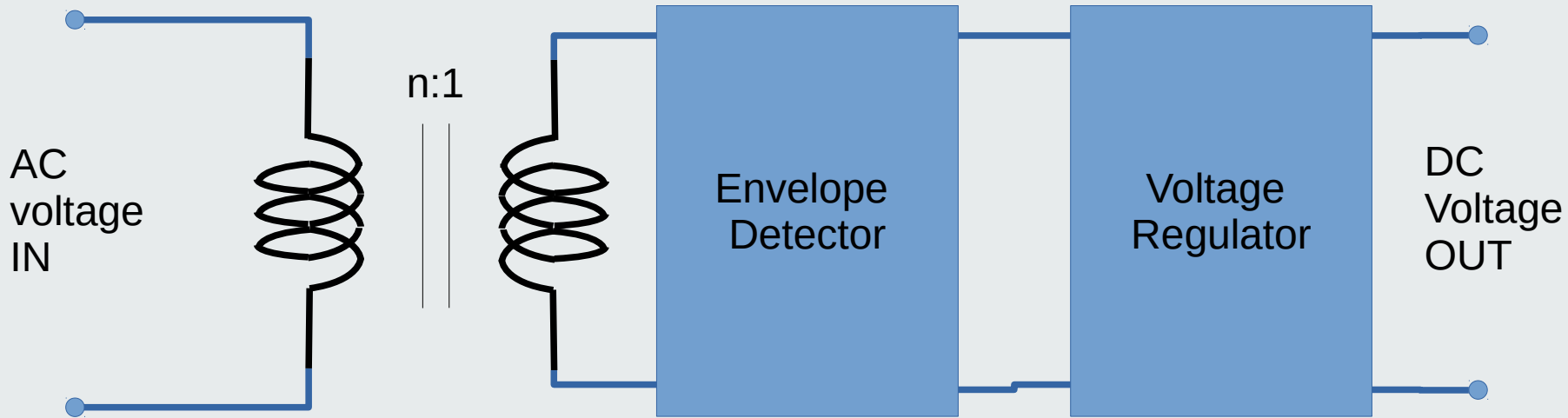
Voltage Divider!

$$3r_d \ll R \Rightarrow v_o \approx 0$$

- Problem solved!
- Choose R much greater than diode incremental resistance

$$r_d = \frac{\eta V_T}{I_s e^{\frac{V_D}{\eta V_T}}}$$

AC⚡DC CONVERTER



- You can now build an AC/DC converter
- That's what lab assignment 3 is about
- Questions welcome!

Conclusion

- **AC/DC converter**
 - Half-wave rectifier circuit revisited
 - Full-wave rectifier circuit
 - Limiter circuit
 - Envelope detector circuit
 - Voltage regulator circuit