

Instituto Superior Técnico
Digital Signal Processing Systems

FIR & IIR filter design

1. Using the Fourier series development method, design an ideal high-pass FIR filter with unity DC gain, cut-off at $f_{p_1} = 3$ kHz and order 9. What kind of coefficient symmetry can you expect? Compute the arithmetic format that should be used for the coefficients and for the filter output.
2. Design a low-pass IIR filter with unity DC gain and with two real poles at frequencies $f_{p_1} = 1$ kHz and $f_{p_2} = 2$ kHz using the impulse invariance method and the bilinear transformation method with pole frequency pre-distortion at the pole frequencies.

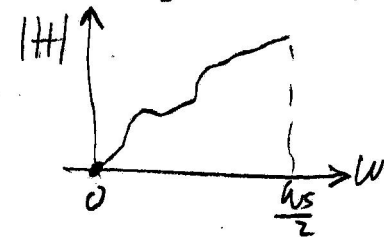
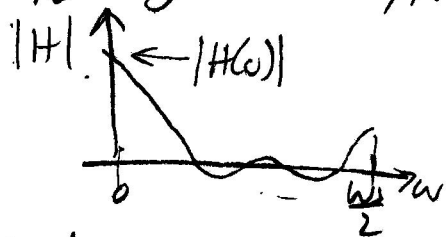
Note: Consider the sampling frequency to be $f_s = 8$ kHz.

Ideal high-pass filter, $f_c = 3\text{kHz}$, $f_s = 8\text{kHz}$, $T_s = 0.5\text{ms}$.

$$T_s = \frac{N-1}{2} T_s \rightarrow N = 2 \tau_c f_s + 1 = 2 \times 0.5 \times 10^{-3} \times 8 \times 10^3 + 1 = 9 \text{ coefficients (odd)}$$

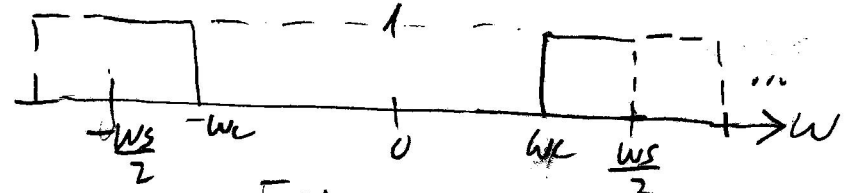
A high-pass filter requires $|H(\frac{\omega_s}{2})| \neq 0$, so there are two possibilities

$h_n \rightarrow$ symmetric, N odd $h_n \rightarrow$ anti-symmetric, N even



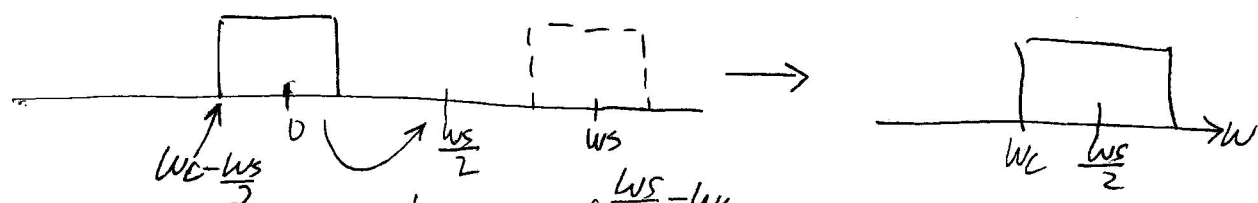
N odd \Rightarrow symmetric coefficients.

$$N=9 = -4 : 4$$



$$\begin{aligned} h_n &= \frac{1}{\omega_s} \left[\int_{-\omega_s/2}^{-\omega_c} e^{jn\omega T_s} d\omega + \int_{\omega_c}^{\omega_s/2} e^{jn\omega T_s} d\omega \right] \\ &= \frac{1}{\omega_s} \left[\frac{e^{jn\omega T_s}}{jnT_s} \Big|_{-\omega_s/2}^{-\omega_c} + \frac{e^{jn\omega T_s}}{jnT_s} \Big|_{\omega_c}^{\omega_s/2} \right] \\ &= \frac{1}{2\pi} \left[\frac{e^{-jn\omega_c T_s} - e^{-jn\omega_s/2 T_s}}{jn} + \frac{e^{jn\omega_s/2 T_s} - e^{jn\omega_c T_s}}{jn} \right] \\ &= \frac{-\sin n\omega_c T_s + \sin n\pi}{\pi n} = \begin{cases} 1 - \frac{\omega_c T_s}{\pi}, & n=0 \\ -\frac{\sin n\omega_c T_s}{\pi n}, & n \neq 0 \end{cases} \end{aligned}$$

Another way: A high-pass filter is a low-pass filter shifted by $\frac{\omega_s}{2}$.



low-pass filter: $h'_n = \frac{1}{\omega_c} \int_{-\omega_s/2 + \omega_c}^{\omega_s/2 - \omega_c} e^{jn\omega T_s} d\omega = \frac{\sin n(\frac{\omega_s}{2} - \omega_c)T_s}{\pi n}$

low-pass
↓

$$\begin{aligned} &= \frac{\sin n(\pi - \omega_c T_s)}{\pi n} = -\frac{\cos n\pi \sin n\omega_c T_s}{\pi n} \\ &= -(-1)^n \frac{\sin n\omega_c T_s}{\pi n}, \quad n \neq 0, \quad h'_0 = \frac{\pi - \omega_c T_s}{\pi} = 1 - \frac{\omega_c T_s}{\pi} \end{aligned}$$

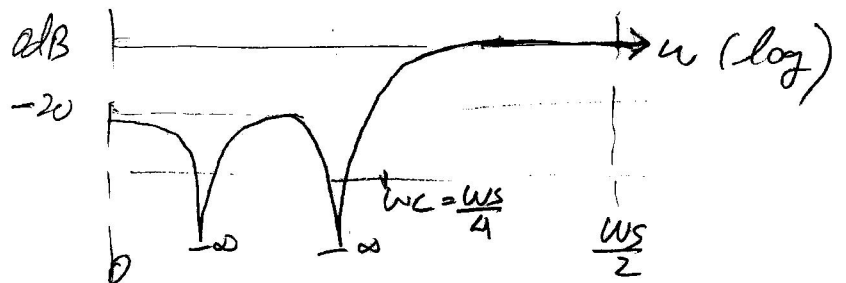
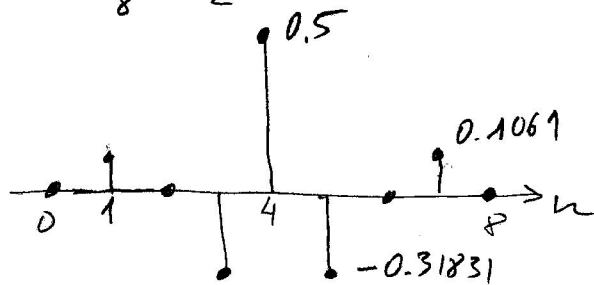
$h_n = h'_n \times e^{j\frac{\omega_s}{2} n T_s} = h'_n e^{jn\pi} = h'_n (-1)^n = \begin{cases} 1 - \frac{\omega_c T_s}{\pi}, & n=0 \\ -\frac{\sin n\omega_c T_s}{\pi n}, & n \neq 0 \end{cases}$

↑ high-pass
shifting \equiv modulation by $\frac{\omega_s}{2}$

← equal!

$$\begin{aligned}
 h_0 &= h_8 = 0 \\
 h_1 &= h_7 = 0.1061 \\
 h_2 &= h_6 = 0 \\
 h_3 &= h_5 = -0.31831 \\
 h_4 &= 0.5 = 1 - \frac{\omega_c T_s}{2} = \frac{1}{2}
 \end{aligned}$$

$$\omega_c T_s = 2\pi \times \frac{2}{8} = \frac{\pi}{2}$$



Arithmetic format:

$$y_n = \sum_{i=0}^{N-1} h_i x(n-i) \rightarrow \text{Non recursive computation.}$$

Input samples Q_m . The worst case is when all products add up with the same sign so

$$|y_n|_{\max} = \sum_{i=0}^{N-1} |h_i| \underbrace{|x(n-i)|}_{x_{\max}} = x_{\max} \cdot \sum_{i=0}^{N-1} |h_i|$$

The format for y_n depends on $\sum_{i=0}^{N-1} |h_i| = 1.3188$ which is >1 but <2 . So y_n has to be stored in Q_{m-1} (one more integer bit than the samples). The coefficients may be stored in Q_{n-1} where n is the number of bits of the words (this is because $|h_n| < 1$ for all n).

2. Lowpass filter, $f_c = 2 \text{ kHz}$, $|H(0)| = 1 \rightarrow H(s) = \frac{\omega_c}{s + \omega_c}$

Impulse invariance:

1. $h(t) = \mathcal{L}^{-1}\{H(s)\} = \omega_c e^{-\omega_c t} u(t)$

2. $h_n = T_s h(nT_s) = \omega_c T_s e^{-\omega_c T_s n} u(n)$

3. $H(z) = \mathcal{Z}\{h_n\} = \omega_c T_s \sum_{n=0}^{\infty} e^{-\omega_c T_s n} z^{-n} = \frac{\omega_c T_s}{1 - e^{-\omega_c T_s} z^{-1}} = \frac{b_0}{1 - a_1 z^{-1}}$

$$= \frac{0.7854}{1 - 0.4559 z^{-1}}$$

$$\omega=0, z=1, |H(1)| = \frac{0.7854}{1-0.443(z^{-1})} = 1.4436! (>1)$$

This is due to aliasing of the frequency response. Need to normalize so $b_0 = 0.7854/1.4436 = 0.5441$

$$H(z) = \frac{0.5441}{1-0.4559z^{-1}}$$

3. Bilinear transformation with $f_c = 1\text{KHz}$

pre'-distortion: $\omega_a = \frac{2}{T_s} \tan \frac{\omega_d T_s}{2} = 2f_s \tan \left(\pi \frac{f_c}{f_s} \right) =$
 $= 6627.4 \text{ rad/s} = 2\pi \times \underbrace{1054.8}_{>f_c} \text{ Krad/s}$

$$\begin{aligned} H(z) &= \frac{\omega_a}{s + \omega_a} \bigg|_{s = \frac{z}{T_s} \frac{z-1}{z+1}} = \frac{\omega_a}{\frac{z}{T_s} \frac{z-1}{z+1} + \omega_a} = \frac{\omega_a \frac{T_s}{2} (z+1)}{\frac{z}{T_s} \frac{z-1}{z+1} + \omega_a} = \frac{\omega_a \frac{T_s}{2} (z+1)}{\frac{z-1 + \omega_a T_s (z+1)}{2}} \\ &= \frac{\omega_a \frac{T_s}{2} (z+1)}{\frac{z(1 + \frac{\omega_a T_s}{2}) - (1 - \frac{\omega_a T_s}{2})}{2}} = \frac{\omega_a \frac{T_s}{2} (z+1)}{1 + \frac{\omega_a T_s}{2} z - \frac{1 - \frac{\omega_a T_s}{2}}{1 + \frac{\omega_a T_s}{2}}} \\ &= \frac{\omega_a \frac{T_s}{2}}{1 + \frac{\omega_a T_s}{2} z} \cdot \frac{1 + z^{-1}}{1 + \frac{1 - \frac{\omega_a T_s}{2}}{1 + \frac{\omega_a T_s}{2}} z^{-1}} \\ &= 0.2929 \cdot \frac{1 - z^{-1}}{1 - 0.4142 z^{-1}} \end{aligned}$$

