

Circuits Theory and Electronic Fundamentals

Integrated Master in Engineering Physics, IST, University of Lisbon

Lab 2: RC Circuit Analysis

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1 Introduction

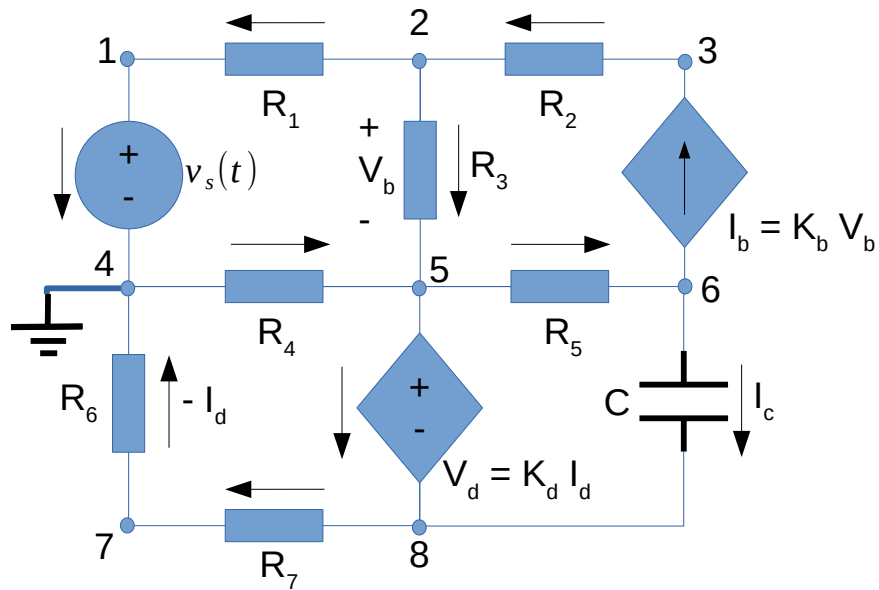


Figure 1: Circuit to be analysed in this laboratory assignment.

| Designation | Value [V, k Ω , mS or μ F] |
|-------------|---------------------------------------|
| R_1 | 1.04053890347 |
| R_2 | 2.00185929606 |
| R_3 | 3.06593231919 |
| R_4 | 4.15163583349 |
| R_5 | 3.03409481751 |
| R_6 | 2.05654586148 |
| R_7 | 1.00587575204 |
| V_s | 5.16821048288 |
| C | 1.0127707267 |
| K_b | 7.29055867767 |
| K_d | 8.22649929708 |

Table 1: Values obtained by running the file t2.datagen.py. Resistances R_i and constant K_d are in k Ω , voltage V_s is in volts, capacitance C is in microfarads and constant K_b is in milisiemens.

2 Theoretical Analysis

2.1 Exercise 1

In this section, the circuit shown in Figure 1 is analysed theoretically, by using the node method. The Kirchhoff Current Law (KCL) states that the sum of the currents converging or diverging in a node is null. The nodes considered for the following equations are those represented in Figure 1. Using KCL and Ohm's Law (which can also be written as $I = VG$) in nodes not connected to voltage sources and additional equations for nodes related by voltage sources, it is possible to obtain a linear system from which the voltages at nodes V_1 to V_8 and currents in resistances R_1 to R_7 can be determined.

The following linear system is obtained:

$$\begin{pmatrix} 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ -\frac{1}{R_1} & \frac{1}{R_1} + \frac{1}{R_2} + \frac{1}{R_3} & -\frac{1}{R_2} & 0 & -\frac{1}{R_3} & 0 & 0 & 0 \\ 0 & -K_b - \frac{1}{R_2} & \frac{1}{R_2} & 0 & K_b & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & -\frac{1}{R_3} & 0 & -\frac{1}{R_4} & \frac{1}{R_3} + \frac{1}{R_4} + \frac{1}{R_5} & -\frac{1}{R_5} & -\frac{1}{R_7} & \frac{1}{R_7} \\ 0 & K_b & 0 & 0 & -\frac{1}{R_5} - K_b & \frac{1}{R_5} & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & \frac{1}{R_6} + \frac{1}{R_7} & -\frac{1}{R_7} \\ 0 & 0 & 0 & -\frac{K_d}{R_6} & 1 & 0 & \frac{K_d}{R_6} & -1 \end{pmatrix} \begin{pmatrix} V_1 \\ V_2 \\ V_3 \\ V_4 \\ V_5 \\ V_6 \\ V_7 \\ V_8 \end{pmatrix} = \begin{pmatrix} V_s \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{pmatrix} \quad (1)$$

By solving the linear system 3, the following values for node voltages and branch currents (calculated by using Ohm's Law) are obtained:

| Designation | Value [A or V] |
|-------------|-----------------|
| I_1 | -2.34143283E-04 |
| I_2 | -2.45108969E-04 |
| I_3 | -1.09656866E-05 |
| I_4 | -1.19427511E-03 |
| I_5 | -2.45108969E-04 |
| I_6 | -9.60131827E-04 |
| I_7 | -9.60131827E-04 |
| I_b | -2.45108969E-04 |
| I_c | 4.33680869E-19 |
| I_{V_s} | -2.34143283E-04 |
| I_{V_d} | -9.60131827E-04 |
| V_1 | 5.16821048E+00 |
| V_2 | 4.92457529E+00 |
| V_3 | 4.43390162E+00 |
| V_5 | 4.95819534E+00 |
| V_6 | 5.70187920E+00 |
| V_7 | -1.97455514E+00 |
| V_8 | -2.94032846E+00 |

Table 2: Values of node voltages (in volts) and branch currents (in amperes). Current I_i corresponds to the current passing through resistance R_i .

2.2 Exercise 2

In this exercise we are going to analyse the system also using the node method, as explained before. In this case our goal is to get the R_{eq} , which means, to find the value of the resistance for the Norton and Thévenin equivalents. In order to calculate the resistance one must turn off all the constant sources, so, as we want to find the equivalent seen from the capacitor, we must have $V_s = 0$. That's the reason, why we do that. Now we are going to use the nodal method to determine the current going to the capacitor if we put a current source with its voltage in its place and then, as we know the current and the voltage, one can simply use the Ohm's law:

$$R = \frac{V}{I} \quad (2)$$

We can use almost all the matrix in the previous exercise. The only differences are the ones stated in the previous paragraph. As we have already determined the voltages in the nodes before, we obtain the matrix above to get the voltages in the nodes, defining V_x as the value of

$V_6 - V_8$, and knowing that $V_4 = 0$, we already simplified a little in order to make the implementation easier:

$$\begin{pmatrix} 1 & 0 & 0 & -1 & 0 & 0 & 0 & 0 \\ -\frac{1}{R_1} & \frac{1}{R_1} + \frac{1}{R_2} + \frac{1}{R_3} & -\frac{1}{R_2} & 0 & -\frac{1}{R_3} & 0 & 0 & 0 \\ 0 & -K_b - \frac{1}{R_2} & \frac{1}{R_2} & 0 & K_b & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & K_b - \frac{1}{R_3} & 0 & -\frac{1}{R_4} & \frac{1}{R_3} + \frac{1}{R_4} - K_b & 0 & -\frac{1}{R_7} & \frac{1}{R_7} \\ 0 & 0 & 0 & 0 & 0 & 1 & 0 & -1 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & \frac{1}{R_6} + \frac{1}{R_7} \\ 0 & 0 & 0 & 0 & 0 & 1 & 0 & -\frac{K_d}{R_6} \end{pmatrix} \begin{pmatrix} V_1 \\ V_2 \\ V_3 \\ V_4 \\ V_5 \\ V_6 \\ V_7 \\ V_8 \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ V_x \\ 0 \\ 0 \end{pmatrix} \quad (3)$$

| Designation | Value [A or V] |
|-------------|-----------------|
| I_1 | -0.00000000E+00 |
| I_2 | 0.00000000E+00 |
| I_3 | -0.00000000E+00 |
| I_4 | 0.00000000E+00 |
| I_5 | -2.84836440E-03 |
| I_6 | 0.00000000E+00 |
| I_7 | -0.00000000E+00 |
| I_b | 0.00000000E+00 |
| I_x | -2.84836440E-03 |
| I_{V_s} | -0.00000000E+00 |
| I_{V_d} | 2.84836440E-03 |
| V_1 | 0.00000000E+00 |
| V_2 | -0.00000000E+00 |
| V_3 | 0.00000000E+00 |
| V_5 | 0.00000000E+00 |
| V_6 | 8.64220765E+00 |
| V_7 | 0.00000000E+00 |
| V_8 | -0.00000000E+00 |

Table 3: Values of node voltages (in volts) and branch currents (in amperes). Current I_i corresponds to the current passing through resistance R_i .

Now that we have all this values, we are simply going to calculate the current going through the capacitor/voltage source as the different between the current going through R_5 and the current I_b , finally getting the result we want. We state that the current is flowing in the opposite direction of what it was supposed to flow, so, the equivalent resistance is the symmetric of the result:

| Designation | Value [A or V] |
|-------------|-----------------|
| I_b | 0.00000000E+00 |
| I_5 | -2.84836440E-03 |
| I_x | -2.84836440E-03 |
| R_{eq} | 3.03409482E+03 |

Table 4: Values of node voltages (in volts) and branch currents (in amperes). Current I_i corresponds to the current passing through resistance R_i .

2.3 Exercise 3

Using the results from the previous exercise we understand we can simplify the circuit into a circuit with a voltage source, a resistance and and the capacitor. For this case we already have that the natural solution looks like:

$$v_n(t) = A \times e^{-\frac{t}{RC}} \quad (4)$$

Where A is the value in $t = 0$ according to the previous exercise, t stands for time, R for the equivalent resistance and C for the capacitance of the capacitor. Plotting the result one gets:

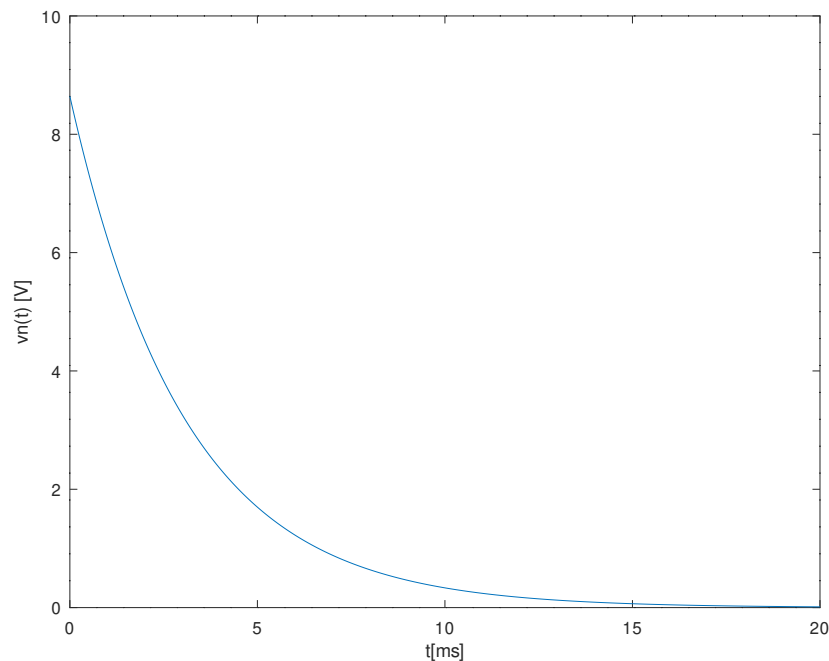


Figure 2: Natural sinusoida response

3 Simulation Analysis

3.1 Exercise 1

Table 5 shows the simulated operating point results for the circuit presented in Figure 1. Again, currents designated below as I_i refer to the currents passing through the respective resistances, R_i .

| Designation | Value [A or V] |
|-------------|----------------|
| I_1 | -2.34143e-04 |
| I_2 | -2.45109e-04 |
| I_3 | -1.09657e-05 |
| I_4 | -1.19428e-03 |
| I_5 | -2.45109e-04 |
| I_6 | -9.60132e-04 |
| I_7 | -9.60132e-04 |
| I_b | -2.45109e-04 |
| I_c | 0.000000e+00 |
| I_{V_s} | -2.34143e-04 |
| I_{V_d} | -9.60132e-04 |
| V_1 | 5.168210e+00 |
| V_2 | 4.924575e+00 |
| V_3 | 4.433902e+00 |
| V_5 | 4.958195e+00 |
| V_6 | 5.701879e+00 |
| V_7 | -1.97456e+00 |
| V_8 | -2.94033e+00 |

Table 5: Operating point analysis table. Currents I_i are in amperes; voltages V_i are in volts.

Comparing the theoretical analysis results presented in Table 2 and the results in Table 5, we can notice almost no differences. This was to be expected, since the circuit has no time dependency - meaning it's equal at any point in time. There is only a small difference between the two values of I_c , although it is negligible.

3.2 Exercise 2

Now we can approach the second point of our simulation where we see how the system behaves when $v_s(0) = 0$ and the capacitor is replaced by a voltage source $V_X = V(6) - V(8)$, where the voltages are taken from 5.

| Designation | Value [A or V] |
|-------------|----------------|
| I_1 | 0.000000e+00 |
| I_2 | 0.000000e+00 |
| I_3 | 0.000000e+00 |
| I_4 | 0.000000e+00 |
| I_5 | -2.84836e-03 |
| I_6 | 0.000000e+00 |
| I_7 | 0.000000e+00 |
| I_b | 0.000000e+00 |
| I_x | -2.84836e-03 |
| I_{V_s} | 0.000000e+00 |
| I_{V_d} | 2.848365e-03 |
| V_1 | 0.000000e+00 |
| V_2 | 0.000000e+00 |
| V_3 | 0.000000e+00 |
| V_5 | 0.000000e+00 |
| V_6 | 8.642208e+00 |
| V_7 | 0.000000e+00 |
| V_8 | 0.000000e+00 |

Table 6: Operating point analysis table. Currents I_i are in amperes; voltages V_i are in volts.

3.3 Exercise 3

Now we do a transient analysis of the values. Figure 3 shows the simulated transient analysis results obtained for the voltage in node 6.

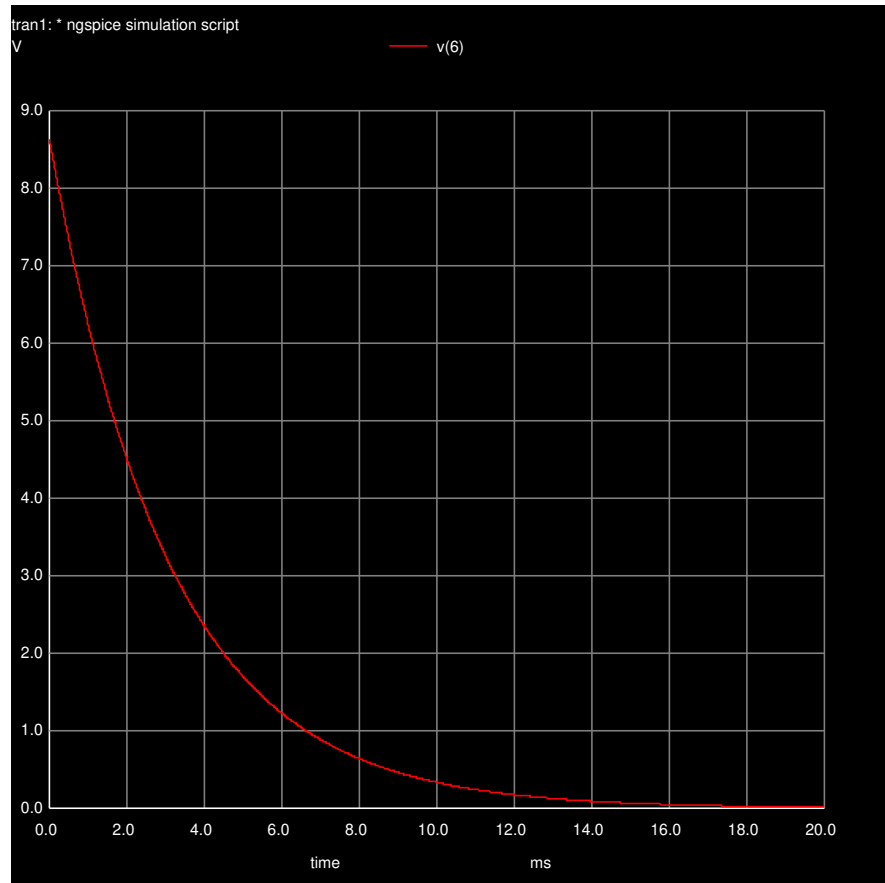


Figure 3: Natural response - value of $v_6(t)$ in the time interval $[0,20]$ ms.

3.4 Exercise 4

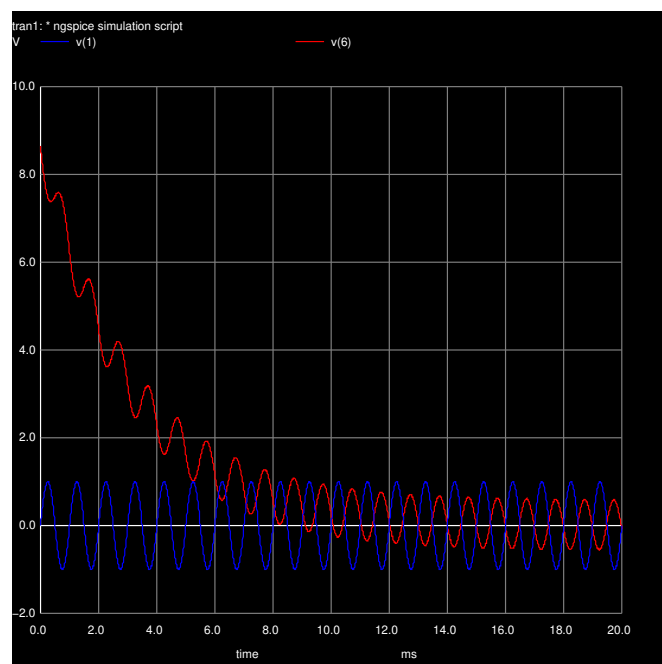


Figure 4: Forced sinusoidal response and stimulus on node 6 in time interval [0,20] ms.

3.5 Exercise 5

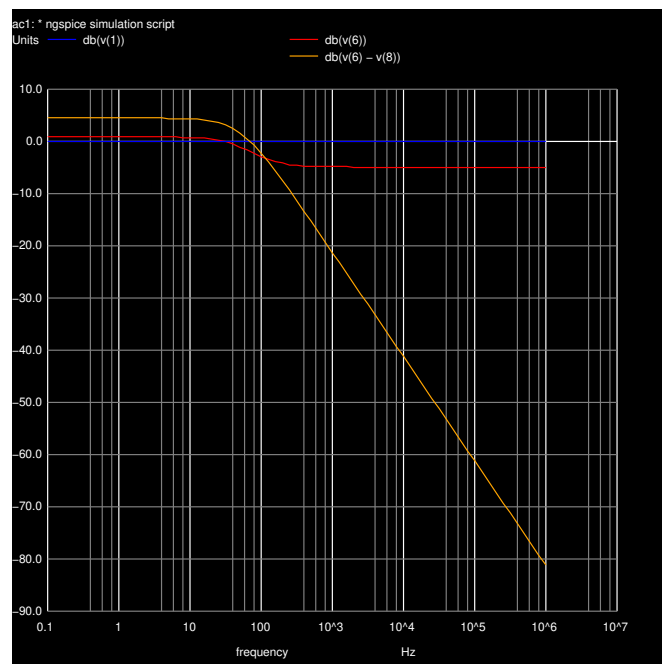


Figure 5: Frequency analysis - magnitudes of $v_6(f)$, $v_8(f)$ and $v_c(f) = v_6(f) - v_8(f)$ in interval $f=[0.1, 10^6]$ Hz and in dB.

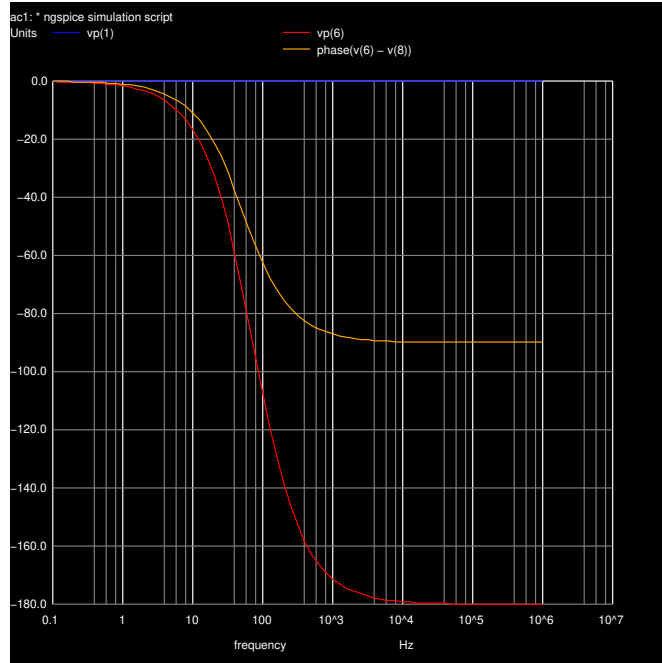


Figure 6: Frequency analysis - phases of $v_6(f)$, $v_s(f)$ and $v_c(f) = v_6(f) - v_8(f)$ in interval $f=[0.1, 10^6]$ Hz and in degrees.

4 Conclusion

| Theoretical | | Simulation | |
|-------------|-----------------|-------------|----------------|
| Designation | Value [A or V] | Designation | Value [A or V] |
| I_1 | -2.34143283E-04 | I_1 | -2.34143e-04 |
| I_2 | -2.45108969E-04 | I_2 | -2.45109e-04 |
| I_3 | -1.09656866E-05 | I_3 | -1.09657e-05 |
| I_4 | -1.19427511E-03 | I_4 | -1.19428e-03 |
| I_5 | -2.45108969E-04 | I_5 | -2.45109e-04 |
| I_6 | -9.60131827E-04 | I_6 | -9.60132e-04 |
| I_7 | -9.60131827E-04 | I_7 | -9.60132e-04 |
| I_b | -2.45108969E-04 | I_b | -2.45109e-04 |
| I_c | 4.33680869E-19 | I_c | 0.000000e+00 |
| I_{V_s} | -2.34143283E-04 | I_{V_s} | -2.34143e-04 |
| I_{V_d} | -9.60131827E-04 | I_{V_d} | -9.60132e-04 |
| V_1 | 5.16821048E+00 | V_1 | 5.168210e+00 |
| V_2 | 4.92457529E+00 | V_2 | 4.924575e+00 |
| V_3 | 4.43390162E+00 | V_3 | 4.433902e+00 |
| V_5 | 4.95819534E+00 | V_5 | 4.958195e+00 |
| V_6 | 5.70187920E+00 | V_6 | 5.701879e+00 |
| V_7 | -1.97455514E+00 | V_7 | -1.97456e+00 |
| V_8 | -2.94032846E+00 | V_8 | -2.94033e+00 |

Table 7: Exercise 1 comparison.

| Theoretical | | Simulation | |
|-------------|-----------------|-------------|----------------|
| Designation | Value [A or V] | Designation | Value [A or V] |
| I_1 | -0.00000000E+00 | I_1 | 0.000000e+00 |
| I_2 | 0.00000000E+00 | I_2 | 0.000000e+00 |
| I_3 | -0.00000000E+00 | I_3 | 0.000000e+00 |
| I_4 | 0.00000000E+00 | I_4 | 0.000000e+00 |
| I_5 | -2.84836440E-03 | I_5 | -2.84836e-03 |
| I_6 | 0.00000000E+00 | I_6 | 0.000000e+00 |
| I_7 | -0.00000000E+00 | I_7 | 0.000000e+00 |
| I_b | 0.00000000E+00 | I_b | 0.000000e+00 |
| I_x | -2.84836440E-03 | I_x | -2.84836e-03 |
| I_{V_s} | -0.00000000E+00 | I_{V_s} | 0.000000e+00 |
| I_{V_d} | 2.84836440E-03 | I_{V_d} | 2.848365e-03 |
| V_1 | 0.00000000E+00 | V_1 | 0.000000e+00 |
| V_2 | -0.00000000E+00 | V_2 | 0.000000e+00 |
| V_3 | 0.00000000E+00 | V_3 | 0.000000e+00 |
| V_5 | 0.00000000E+00 | V_5 | 0.000000e+00 |
| V_6 | 8.64220765E+00 | V_6 | 8.642208e+00 |
| V_7 | 0.00000000E+00 | V_7 | 0.000000e+00 |
| V_8 | -0.00000000E+00 | V_8 | 0.000000e+00 |

Table 8: Exercise 2 comparison.