

# Circuits Theory and Electronic Fundamentals

Integrated Master in Engineering Physics, IST, University of Lisbon

## Lab 2: RC Circuit Analysis

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## 1 Introduction

The objective of this laboratory assignment is to analyse the RC circuit shown in Figure 1. As shown below, the nodes have been numbered, current directions have been assigned to all branches and potential  $0V$  has been assigned to one of the nodes. By running the Python script `t2_datagen.py`, the values shown in Table 1 have been obtained.

In Section 2, a theoretical analysis of the circuit and the results obtained with the Octave math tool are presented. In Section 3, the results obtained using the Ngspice simulation tool are shown. The conclusions of this study are outlined in Section 4, in which the theoretical results obtained in Section 2 are compared to those presented in Section 3.

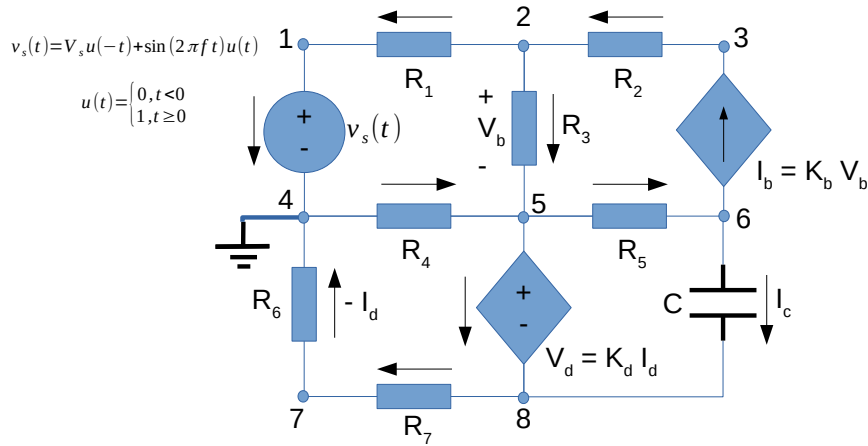


Figure 1: Circuit to be analysed in this laboratory assignment.

Designation	Value [V, k $\Omega$ , mS or $\mu$ F]
$R_1$	1.04053890347
$R_2$	2.00185929606
$R_3$	3.06593231919
$R_4$	4.15163583349
$R_5$	3.03409481751
$R_6$	2.05654586148
$R_7$	1.00587575204
$V_s$	5.16821048288
$C$	1.0127707267
$K_b$	7.29055867767
$K_d$	8.22649929708

Table 1: Values obtained by running the file t2.datagen.py. Resistances  $R_i$  and constant  $K_d$  are in k $\Omega$ , voltage  $V_s$  is in volts, capacitance  $C$  is in microfarads and constant  $K_b$  is in milisiemens.

## 2 Theoretical Analysis

### 2.1 Exercise 1

In this exercise, the circuit shown in Figure 1 is analysed theoretically for  $t < 0$ , by using the node method. The Kirchhoff Current Law (KCL) states that the sum of the currents converging or diverging in a node is null. Using KCL and Ohm's Law (which can also be written as  $I = VG$ ) in nodes not connected to voltage sources and additional equations for nodes related by voltage sources, it is possible to obtain a linear system from which the node voltages  $V_1$  to  $V_8$  are obtained. Using these values and Ohm's Law, the currents in all branches can be determined.

It is worth mentioning that the current passing through the capacitor is given by  $i_C = C \frac{dv_C}{dt}$ . However, it is assumed that the voltages in the capacitor's terminals have already achieved static values a long time ago, thus  $i_C = 0$ A.

The following linear system is obtained:

$$\begin{pmatrix} 1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ -\frac{1}{R_1} & \frac{1}{R_1} + \frac{1}{R_2} + \frac{1}{R_3} & -\frac{1}{R_2} & 0 & -\frac{1}{R_3} & 0 & 0 & 0 \\ 0 & -K_b - \frac{1}{R_2} & \frac{1}{R_2} & 0 & K_b & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & -\frac{1}{R_3} & 0 & 0 & \frac{1}{R_3} + \frac{1}{R_4} + \frac{1}{R_5} & -\frac{1}{R_5} & -\frac{1}{R_7} & \frac{1}{R_7} \\ 0 & K_b & 0 & 0 & -\frac{1}{R_5} - K_b & \frac{1}{R_5} & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & \frac{1}{R_6} + \frac{1}{R_7} & -\frac{1}{R_7} \\ 0 & 0 & 0 & 0 & 1 & 0 & \frac{K_d}{R_6} & -1 \end{pmatrix} \begin{pmatrix} V_1 \\ V_2 \\ V_3 \\ V_4 \\ V_5 \\ V_6 \\ V_7 \\ V_8 \end{pmatrix} = \begin{pmatrix} V_s \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{pmatrix} \quad (1)$$

The matrix shown above isn't symmetrical because of the presence of dependent sources in this circuit. The values obtained by solving the linear system above, using Octave, are shown in Table 2.

Designation	Value [A or V]
$I_1$	-2.3414328285E-04
$I_2$	-2.4510896948E-04
$I_3$	-1.0965686632E-05
$I_4$	-1.1942751099E-03
$I_5$	-2.4510896948E-04
$I_6$	-9.6013182701E-04
$I_7$	-9.6013182701E-04
$I_b$	-2.4510896948E-04
$I_c$	4.3368086899E-19
$I_{V_s}$	-2.3414328285E-04
$I_{V_d}$	-9.6013182701E-04
$V_1$	5.1682104829E+00
$V_2$	4.9245752881E+00
$V_3$	4.4339016190E+00
$V_5$	4.9581953411E+00
$V_6$	5.7018791952E+00
$V_7$	-1.9745551353E+00
$V_8$	-2.9403284589E+00

Table 2: Values of node voltages (in volts) and currents (in amperes). Current  $I_i$  corresponds to the current passing through resistance  $R_i$ .

## 2.2 Exercise 2

In this exercise, the goal is to obtain  $R_{eq}$ , the value of the equivalent resistance as seen from the capacitor's terminals. According to Thévenin's Theorem, it is possible to replace the linear sub-circuit connected to the capacitor's terminals by a voltage source connected with the resistor. In order to calculate  $R_{eq}$  by Thévenin's Theorem, we must have  $V_s = 0$  (all independent sources of the sub-circuit connected to the capacitor's terminals must be switched off). By replacing the capacitor with a voltage source  $V_x = V_6 - V_8$ , where  $V_6$  and  $V_8$  are the voltages determined in Section 2.1, the current  $I_x$  supplied by  $V_x$  can be calculated by applying the node method to this new circuit - using Ohm's Law, the equivalent resistance is computed as  $R_x = \frac{V_x}{I_x}$ . The linear system and the node voltages and branch currents in this case are the following:

$$\begin{pmatrix} 1 & 0 & 0 & -1 & 0 & 0 & 0 & 0 \\ -\frac{1}{R_1} & \frac{1}{R_1} + \frac{1}{R_2} + \frac{1}{R_3} & -\frac{1}{R_2} & 0 & -\frac{1}{R_3} & 0 & 0 & 0 \\ 0 & -K_b - \frac{1}{R_2} & \frac{1}{R_2} & 0 & K_b & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & K_b - \frac{1}{R_3} & 0 & 0 & \frac{1}{R_3} + \frac{1}{R_4} - K_b & 0 & -\frac{1}{R_7} & \frac{1}{R_7} \\ 0 & 0 & 0 & 0 & 0 & 1 & 0 & -1 \\ 0 & 0 & 0 & 0 & 0 & 0 & \frac{1}{R_6} + \frac{1}{R_7} & \frac{1}{R_7} \\ 0 & 0 & 0 & 0 & 1 & 0 & -\frac{K_d}{R_6} & -1 \end{pmatrix} \begin{pmatrix} V_1 \\ V_2 \\ V_3 \\ V_4 \\ V_5 \\ V_6 \\ V_7 \\ V_8 \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ V_x \\ 0 \\ 0 \end{pmatrix} \quad (2)$$

Designation	Value [A or V]
$I_1$	-0.0000000000E+00
$I_2$	0.0000000000E+00
$I_3$	-0.0000000000E+00
$I_4$	0.0000000000E+00
$I_5$	-2.8483643966E-03
$I_6$	0.0000000000E+00
$I_7$	-0.0000000000E+00
$I_b$	0.0000000000E+00
$I_{V_x}$	-2.8483643966E-03
$I_{V_s}$	-0.0000000000E+00
$I_{V_d}$	2.8483643966E-03
$V_1$	0.0000000000E+00
$V_2$	-0.0000000000E+00
$V_3$	0.0000000000E+00
$V_4$	0.0000000000E+00
$V_5$	0.0000000000E+00
$V_6$	8.6422076540E+00
$V_7$	0.0000000000E+00
$V_8$	-0.0000000000E+00

Table 3: Values of node voltages (in volts) and branch currents (in amperes). Current  $I_i$  corresponds to the current passing through resistance  $R_i$ .

Now, the current going through the equivalent resistor can be calculated as  $I_x = I_b - I_5 = -I_{V_x}$  (KCL in node 6). It must be stated that the current going through  $R_{eq}$  (i.e., from + to - in  $R_{eq}$ ) is flowing in the opposite direction of the current “passing through” voltage source  $V_x$ , i.e., the current going from + to - in  $V_x$ , thus the equation shown before.

Finally, one can compute the time constant as  $\tau = R_x C$ . The final results are shown in Table 4.

Designation	Value [A or V or $\Omega$ or s]
$V_x$	8.6422076540E+00
$I_x$	2.8483643966E-03
$R_{eq}$	3.0340948175E+03
$\tau$	3.0728424132E-03

Table 4: Values determined for  $V_x$  [V],  $I_x$  [A],  $R_{eq}$  [ $\Omega$ ] and  $\tau$  [s].

This procedure must be done in order to determine  $R_{eq}$ , which is used to obtain the time constant. This static analysis also allows us to obtain the initial conditions  $v_6(0)$  and  $v_8(0)$ ,

which will also be used to compute the natural and final solutions, because we may consider that, for  $t = 0$ ,  $v_s = 0$  and  $V_6 - V_8 = V_x$ . It is worth noting that, according to the expression for  $v_s(t)$  given in Figure 1,  $v_s(0) = V_s$ , so the change in value for  $v_s$  would occur instantaneously afterwards, in an instant  $t = \delta$ ; however, it is valid to consider it to be happening at  $t = 0$ , because it doesn't change the overall solution.

### 2.3 Exercise 3

Using the results from the previous exercise, we can infer that the circuit shown in Figure 1 can be simplified into a circuit with the independent voltage source, a resistance  $R_{eq}$  and the capacitor. Thus, the general form for the wanted natural solution, as learnt in class, is given by

$$v_{6n}(t) = A \times e^{-\frac{t}{RC}} \quad (3)$$

Where  $A = v_6(0)$  (obtained in Section 2.2),  $t$  stands for time and  $R$  for the (equivalent) resistance. The graph shown below is obtained by plotting Eq.3 in Octave.

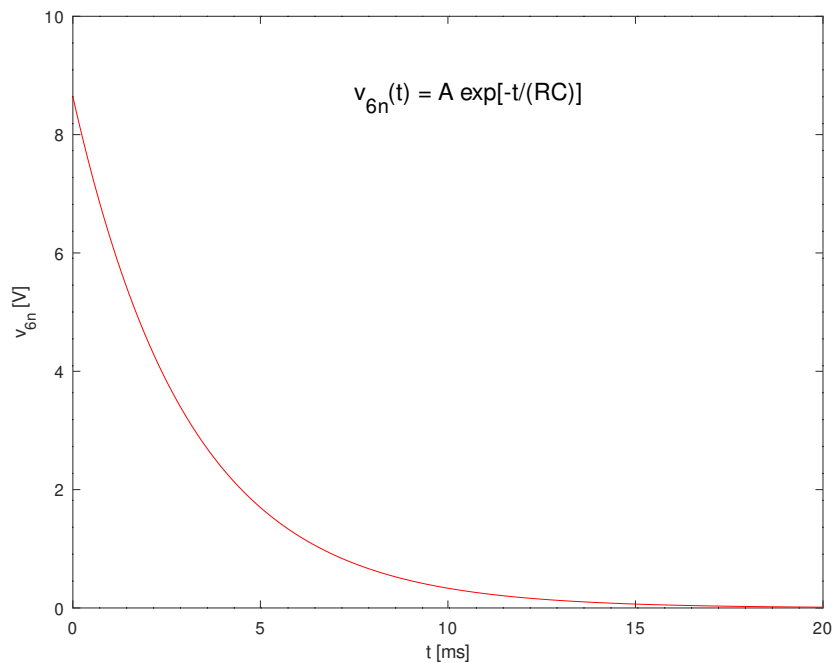


Figure 2: Natural solution  $v_{6n}(t)$  in the time interval  $[0,20]$  ms.

### 2.4 Exercise 4

In this exercise, the forced solution for the voltage in node 6,  $v_{6f}(t)$ , will be determined for the time interval  $[0,20]$  ms. Because we are dealing with a forced solution with sinusoidal excitation, given by  $v_s(t) = \sin(2\pi ft)$ , with  $f = 1\text{kHz}$ , it becomes much more efficient to use phasors. As suggested, a phasor voltage source  $V_s = 1$  will be used. The correspondent phase is  $\phi_{V_s} = 0$ ; therefore, in this forced solution analysis, the voltages will be considered as given by  $\sin$  functions, as opposed to  $\cos$  functions, as was learnt in class. This won't change the overall results, but will be important to take into account when analysing the phases plotted in Sections 2.6 and 3.5. In addition to this,  $C$  is replaced by its impedance,  $Z_C$ . This impedance is given by  $Z_C = \frac{1}{j\omega C}$ , with  $j$  being the imaginary unit and  $\omega = 2\pi f$ .

By running nodal analysis as in the previous sections, the following linear system is obtained:

$$\begin{pmatrix}
1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\
-\frac{1}{R_1} & \frac{1}{R_1} + \frac{1}{R_2} + \frac{1}{R_3} & -\frac{1}{R_2} & 0 & -\frac{1}{R_3} & 0 & 0 & 0 \\
0 & -K_b - \frac{1}{R_2} & \frac{1}{R_2} & 0 & K_b & 0 & 0 & 0 \\
0 & 0 & 0 & 1 & 0 & 0 & 0 & 0 \\
0 & -\frac{1}{R_3} & 0 & 0 & \frac{1}{R_3} + \frac{1}{R_4} + \frac{1}{R_5} & -\frac{1}{R_5} - j\omega C & -\frac{1}{R_7} & \frac{1}{R_7} + j\omega C \\
0 & K_b & 0 & 0 & -K_b - \frac{1}{R_5} & \frac{1}{R_5} + j\omega C & 0 & -j\omega C \\
0 & 0 & 0 & 0 & 0 & 0 & \frac{1}{R_6} + \frac{1}{R_7} & -\frac{1}{R_7} \\
0 & 0 & 0 & 0 & 1 & 0 & \frac{K_d}{R_6} & -1
\end{pmatrix}
\begin{pmatrix}
V_1 \\
V_2 \\
V_3 \\
V_4 \\
V_5 \\
V_6 \\
V_7 \\
V_8
\end{pmatrix}
=
\begin{pmatrix}
V_s \\
0 \\
0 \\
0 \\
0 \\
0 \\
0 \\
0
\end{pmatrix}
\quad (4)$$

The complex amplitudes (phasors) in the nodes, obtained by solving the linear system above, are shown below.

Designation	Value [V]
$V_1$	1.0000000000E+00 + (0.0000000000E+00) i
$V_2$	9.5285888692E-01 + (5.3839669869E-17) i
$V_3$	8.5791815826E-01 + (9.6386837769E-16) i
$V_4$	0.0000000000E+00 + (0.0000000000E+00) i
$V_5$	9.5936405020E-01 + (-8.5138154658E-18) i
$V_6$	-5.6445199131E-01 + (-8.6377545528E-02) i
$V_7$	-3.8205780160E-01 + (3.3905477482E-18) i
$V_8$	-5.6892583392E-01 + (5.0488962587E-18) i

Table 5: Complex values of the phasors in the nodes (in volts).

Having the value of the phasor  $V_6$ , it is possible to determine the amplitude and the phase of the correspondent sine wave, which are given by  $Amplitude = \sqrt{Re(V_6)^2 + Im(V_6)^2}$  and  $\phi_{V_6} = atan(Im(V_6)/Re(V_6))$ , respectively. The sinusoidal forced solution is plotted in Figure 3.

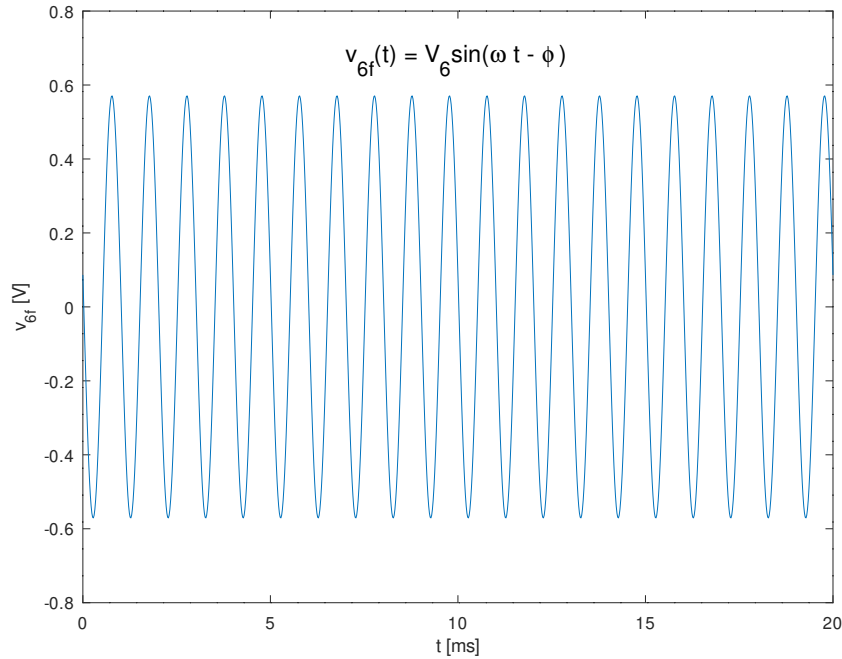


Figure 3: Forced solution  $v_{6f}(t)$  in the time interval [0,20] ms. To be noted that  $V_6$  written above refers to the amplitude of the phasor, not the phasor itself.

## 2.5 Exercise 5

In Figure 4, the final solutions for  $v_6(t) = v_{6n}(t) + v_{6f}(t)$  (obtained by superimposing the natural and forced solutions, previously determined), is plotted alongside  $v_s(t)$ , which is given by the branch function presented in Figure 1.

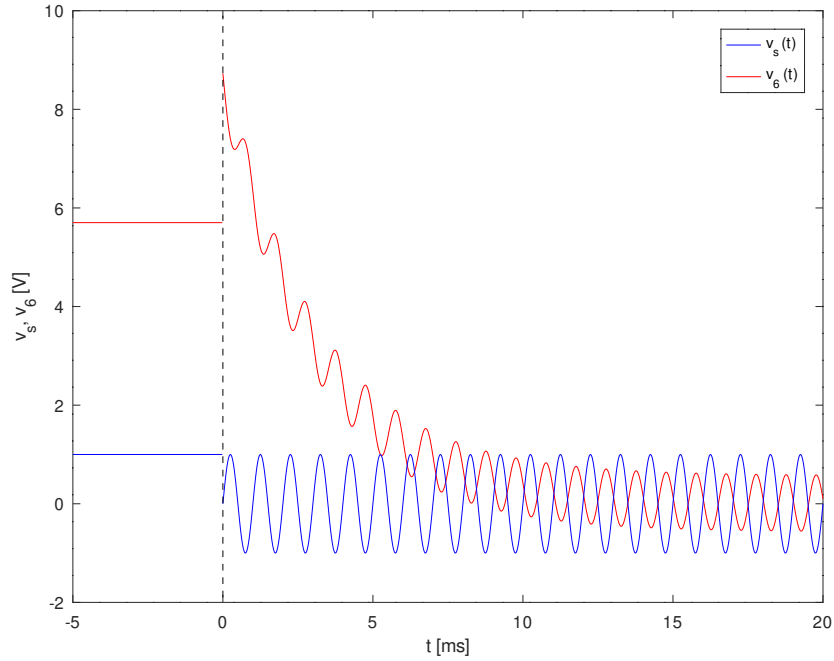


Figure 4: Final solution  $v_6(t)$  and  $v_s(t)$  in time interval  $[-5, 20]$  ms.

We can notice that neither  $v_6$  nor  $v_s$  are continuous functions. (escrever mais...)

## 2.6 Exercise 6

In this case, the magnitudes and the phases of the frequency responses  $v_c(f) = v_6(f) - v_8(f)$ ,  $v_6(f)$  and  $v_s(f)$  will be plotted.

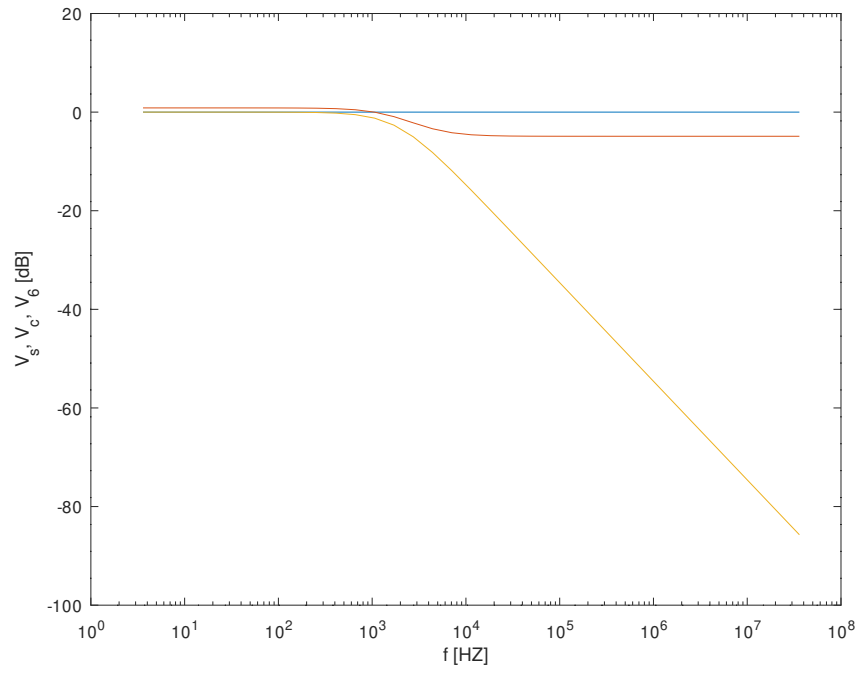


Figure 5: Magnitude of  $v_s$ ,  $v_c$  and  $v_8$ , in dB.

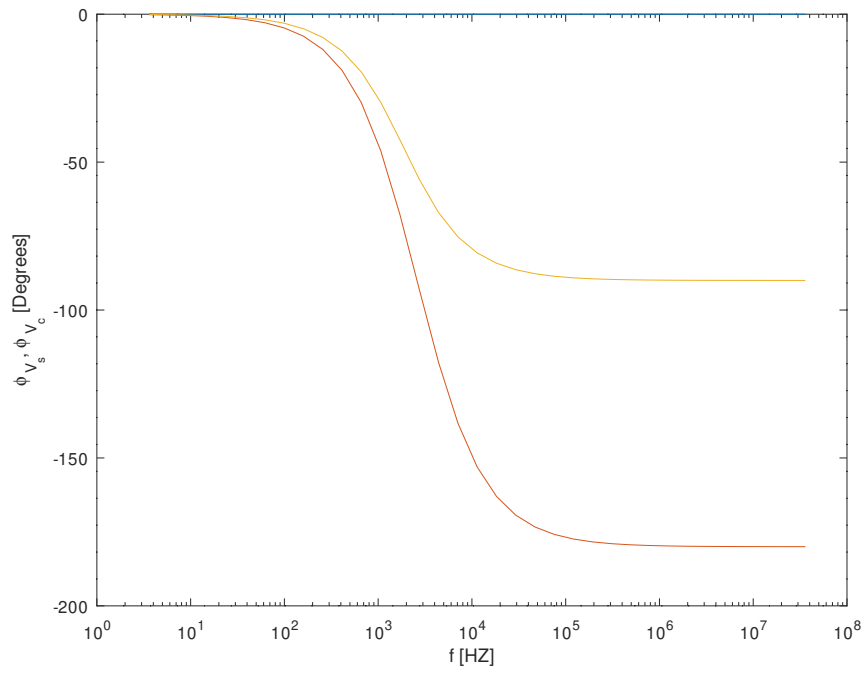


Figure 6: Phase of  $v_s$ ,  $v_c$  and  $v_8$ , in degrees.



### 3 Simulation Analysis

#### 3.1 Exercise 1

Table 6 shows the simulated operating point results for the circuit presented in Figure 1. Again, currents designated below as  $I_i$  refer to the currents passing through the respective resistances,  $R_i$ .

Theoretical		Simulation	
Designation	Value [A or V]	Designation	Value [A or V]
$I_1$	-2.3414328285E-04	$I_1$	-2.341432828e-04
$I_2$	-2.4510896948E-04	$I_2$	-2.451089695e-04
$I_3$	-1.0965686632E-05	$I_3$	-1.096568663e-05
$I_4$	-1.1942751099E-03	$I_4$	-1.194275110e-03
$I_5$	-2.4510896948E-04	$I_5$	-2.451089695e-04
$I_6$	-9.6013182701E-04	$I_6$	-9.601318270e-04
$I_7$	-9.6013182701E-04	$I_7$	-9.601318270e-04
$I_b$	-2.4510896948E-04	$I_b$	-2.451089695e-04
$I_c$	4.3368086899E-19	$I_c$	0.0000000000e+00
$I_{V_s}$	-2.3414328285E-04	$I_{V_s}$	-2.341432828e-04
$I_{V_d}$	-9.6013182701E-04	$I_{V_d}$	-9.601318270e-04
$V_1$	5.1682104829E+00	$V_1$	5.1682104829e+00
$V_2$	4.9245752881E+00	$V_2$	4.9245752881e+00
$V_3$	4.4339016190E+00	$V_3$	4.4339016190e+00
$V_5$	4.9581953411E+00	$V_5$	4.9581953411e+00
$V_6$	5.7018791952E+00	$V_6$	5.7018791952e+00
$V_7$	-1.9745551353E+00	$V_7$	-1.974555135e+00
$V_8$	-2.9403284589E+00	$V_8$	-2.940328459e+00

Table 6: Exercise 1 - comparison between theoretical analysis and operating point analysis's results. Currents  $I_i$  are in amperes; voltages  $V_i$  are in volts.

Comparing the results, we can notice almost no differences. This was to be expected, since the circuit has no time dependency - meaning it's equal at any point in time. There is only a small difference between the two values of  $I_c$ , although it is negligible.

#### 3.2 Exercise 2

Now we can approach the second point of our simulation where we see how the system behaves when  $v_s(0) = 0$  and the capacitor is replaced by a voltage source  $V_X = V(6) - V(8)$ , where the voltages are taken from ??.

Theoretical		Simulation	
Designation	Value [A or V]	Designation	Value [A or V]
$I_1$	-0.0000000000E+00	$I_1$	0.000000e+00
$I_2$	0.0000000000E+00	$I_2$	0.000000e+00
$I_3$	-0.0000000000E+00	$I_3$	0.000000e+00
$I_4$	0.0000000000E+00	$I_4$	0.000000e+00
$I_5$	-2.8483643966E-03	$I_5$	-2.84836e-03
$I_6$	0.0000000000E+00	$I_6$	0.000000e+00
$I_7$	-0.0000000000E+00	$I_7$	0.000000e+00
$I_b$	0.0000000000E+00	$I_b$	0.000000e+00
$I_{V_x}$	-2.8483643966E-03	$I_x$	-2.84836e-03
$I_{V_s}$	-0.0000000000E+00	$I_{V_s}$	0.000000e+00
$I_{V_d}$	2.8483643966E-03	$I_{V_d}$	2.848364e-03
$V_1$	0.0000000000E+00	$V_1$	0.000000e+00
$V_2$	-0.0000000000E+00	$V_2$	0.000000e+00
$V_3$	0.0000000000E+00	$V_3$	0.000000e+00
$V_4$	0.0000000000E+00	$V_5$	0.000000e+00
$V_5$	0.0000000000E+00	$V_6$	8.642208e+00
$V_6$	8.6422076540E+00	$V_7$	0.000000e+00
$V_7$	0.0000000000E+00	$V_8$	0.000000e+00
$V_8$	-0.0000000000E+00		

Table 7: Exercise 2 comparison. Operating point analysis table. Currents  $I_i$  are in amperes; voltages  $V_i$  are in volts.

### 3.3 Exercise 3

Now we do a transient analysis of the values. Figure 7 shows the simulated transient analysis results obtained for the voltage in node 6.

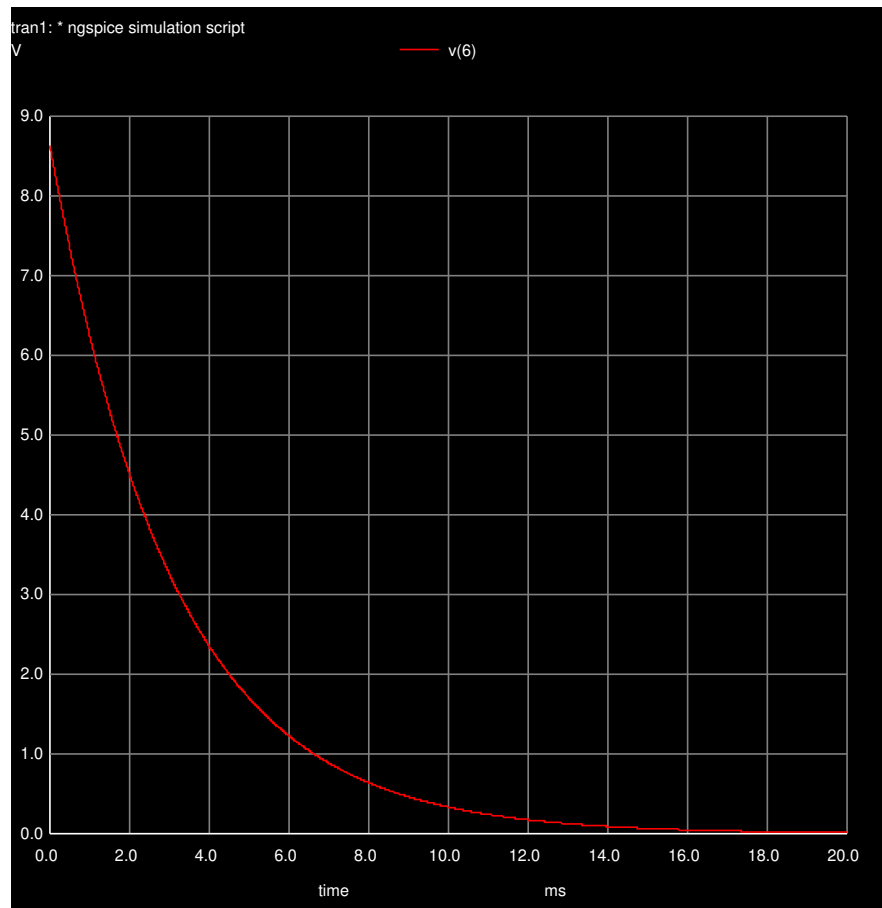


Figure 7: Natural response - value of  $v_6(t)$  in the time interval  $[0,20]$  ms.

### 3.4 Exercise 4

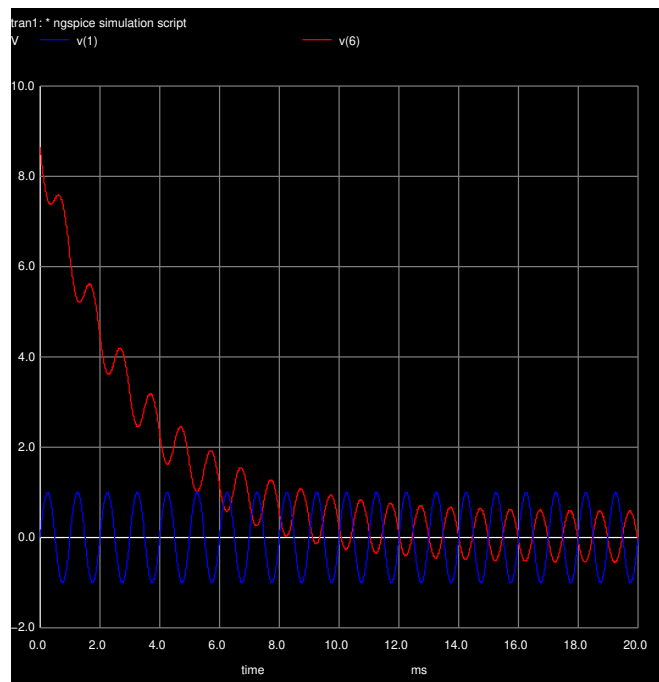


Figure 8: Forced sinusoidal response and stimulus on node 6 in time interval [0,20] ms.

### 3.5 Exercise 5

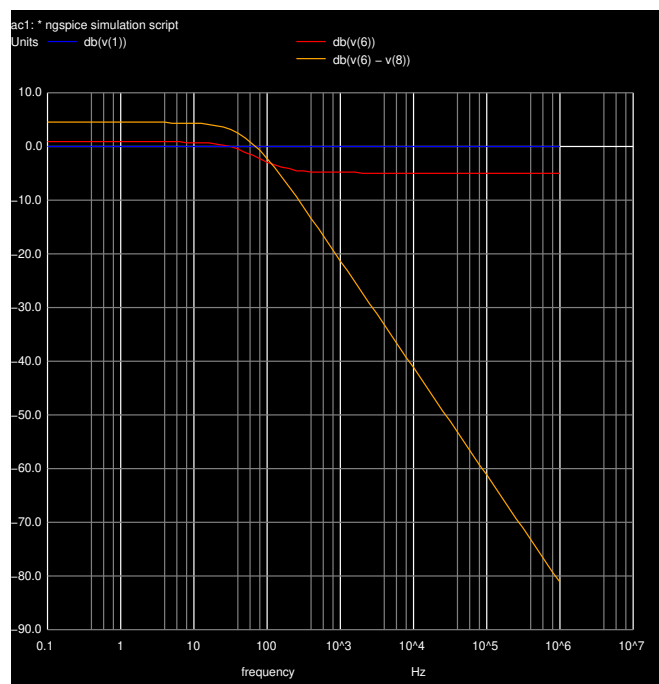


Figure 9: Frequency analysis - magnitudes of  $v_6(f)$ ,  $v_8(f)$  and  $v_c(f) = v_6(f) - v_8(f)$  in interval  $f=[0.1, 10^6]$  Hz and in dB.

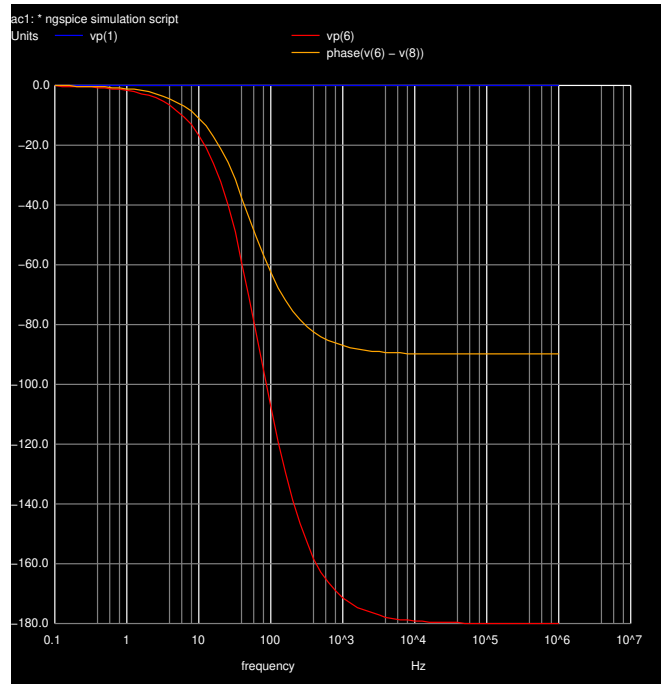


Figure 10: Frequency analysis - phases of  $v_6(f)$ ,  $v_8(f)$  and  $v_c(f) = v_6(f) - v_8(f)$  in interval  $f=[0.1, 10^6]$  Hz and in degrees.

## 4 Conclusion